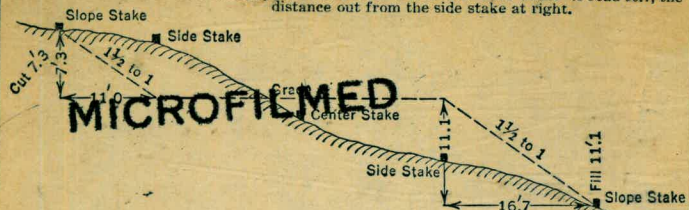


KOLLEGE
LEVEL
WEST

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

Roadway of any Width. Side Slopes 1/2 to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	Distance out from Side or Shoulder Stake										Cut or Fill
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

KEUFFEL & ESSER CO., N. Y.

Book No 22

12:59 - 153700

3.81

H.1 = 16.40

17960

70233

77270

95.20 B/207400 H.W.

198400 H.W.

176 - 947

172 - 878

168 - 291

The paper in this book No. 373A is made of 50% high grade rag stock with a WATER RESISTING surface sizing.

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BARTINGAN
SIBATA
STANLEY
8-28-47
CLEAR
C.M.M.

8-28-47
①

PROFILE LEVELS OF DE-ANZA POINT

BASELINE					STATION	B.S.	H.I.	F.S.	ELEV.	
					N158+00		16.26	5.49	10.77	Indexed
					N159+00			5.79	10.47	
STATION & MORENA	B.S.	H.I.	F.S.	ELEV.	T.P.	4.94	15.41		10.47	TOP HUB N159+00
T.P.	2.97	20.41	6.22	17.44	N160+00			5.00	10.41	
T.P.	2.15	16.17	6.32	14.02	N161+00			5.18	10.23	
T.P.	5.33	17.25	4.25	11.92	N162+00			5.36	10.05	
T.P.	5.19	18.18	4.26	12.99	N163+00			5.65	9.76	
T.P.	5.31	19.48	4.01	14.17	T.P.	5.11	14.87		9.76	TOP HUB N163+00
T.P.	3.93	18.51	4.90	14.58	N164+00			5.03	9.84	
STA N149+00			5.04	13.47 12.47	N165+00			5.13	9.74	
N150+00			5.35	13.16	N166+00			4.73	10.14	
N151+00 T.P.			5.93	12.58	T.P.	6.03	16.17		10.14	TOP HUB N166+00
N152+00			5.59	12.92	N167+00			5.79	10.38	
T.P.	4.76	17.68		12.92	N168+00			5.48	10.69	
N153+00			5.09	12.59	W73+00			4.48	11.69	
N154+00			5.50	12.18	W74+00			4.20	11.97	
N155+00			5.61	12.09	T.P.	4.75	16.72		11.97	TOP HUB W74+00
T.P.	4.19	16.26		12.07	N155+00 W75+00			5.10	11.62	
N156+00			4.79	11.47	W76+00			4.79	11.93	
N157+00			4.98	11.28	W77+00			4.24	12.48	

PROFILE LEVELS DE-ANZA B/H					(CONT.)					8-28-97 (2)	
STATION	B.S.	H.I.	F.S.	ELEV	STATION	B.S.	H.I.	F.S.	ELEV		
T.P. 3	4.27	16.75		12.48	To P Hub W77+00	W93+00		11.28	4.80	6.48	
W78+00			4.97	11.78		T.P.	6.45	12.93		6.48	Top Hub W93+00
4 STATE			4.51	12.09	conc. Mon Top Lead City Mon	W94+00			5.93	7.00	
W79+00			4.95	11.80		W95+00			5.00	7.93	
W80+00			6.28	10.47		W96+00			5.06	7.87	
W81+00			9.91	6.84		W97+00			5.19	7.74	
T.P.	3.78	10.62		6.84	To P Hub W81+00	T.P.	5.08	12.82		7.74	Top Hub W97+00
W82+00			4.51	6.11		W98+00			5.15	7.67	
W83+00			4.65	5.97		W99+00			4.86	7.96	
W84+00			5.02	5.60		W100+00			6.02	6.80	
W85+00			5.22	5.40		W101+00			4.56	8.26	
T.P.	4.55	9.95		5.40	To P Hub W85+00	T.P.	4.26	12.52		8.26	Top Hub W101+00
W86+00			4.29	5.66					3.64	8.88 =	8.804 A BOND U.S.E.P.
W87+00			5.03	4.92		Δ BOND	4.53	13.33		8.804	U.S.E.P. Δ Top Brass Cap
W88+00			4.61	5.34		W102+00			5.50	7.83	
W89+00			4.05	5.90		W103+00			5.15	8.18	
T.P.	5.38	11.28		5.90	Top Hub W89+00	W104+00			5.96	7.37	
W90+00			5.14	6.14		T.P.	5.95	13.32		7.37	Top Hub W104+00
W91+00			5.29	5.99		W105+00			5.50	7.82	W-105+00
W92+00			4.75	6.53		W106+00			4.95	8.37	W-106+00
						W107+00			8.77	4.55	W-107+00
						T.P.	5.58	13.77	5.13	8.13	T.P.
						A BOND			4.97	8.80 = 8.80	BOND Δ U.S.E.P.

- ORIGINAL -

BARRAGAN
SHEPPY
STANLEY 9-2-47
CLEAR
CALM
HOT

X-SECTIONS OF FILL AREA OF PROJECT # 3-1

STA-106+00 W

105
-5.09-1183
+4.5 C-106+00 (3)

SECTIONS TO W95+00 ARE AT 75° 37' 15" TO B/L.

0+00 = W106+00 ON B/L

STA-W107+00 THRU W109+00 COMPLETED IN BX #23 PARTIAL

STA	+	H.I.	-	ELEV	PX
		13.13		7.66	T.P. HUB
	5.47	13.29		7.82	W 105+183

STA-107+00 W

S-10+00

8.2 4.9

0+00 = STA-107+00 ON B/L: SECT. AT 90° TO B/L

PX

S-3+50

8.1 5.0

STA + H.I. - ELEV

S-3+05

7.6 5.5

1.25 9.62
9.44

8.37 T.P. HUB

~~8.19~~ W106+00

S-8+40

8.0 5.1

Indefinite

0+00

5.1 4.5

S-7+80

8.0 5.1

S-0+50

4.9 4.7

S-7+35

9.9 3.2

S-1+10

5.0 4.6

S-6+80

9.8 3.3

S-1+80

4.9 4.7

S-6+25

9.1 4.0

S-2+68

5.3 4.3

S-5+70

9.2 3.9

S-2+80

2.7 6.9

S-5+20

9.6 3.5

S-3+50

3.6 6.0

S-4+65

9.1 4.0

S-4+30

3.6 6.0

S-3+95

8.9 4.2

S-5+05

3.9 5.7

S-3+20

9.1 4.0

S-5+75

4.5 5.1

S-2+50

9.4 3.7

S-6+40

4.8 4.7

S-2+05

6.0 7.1

S-7+05

4.7 4.9

S-1+58

5.8 7.3

S-7+80

4.8 4.8

S-0+80

5.5 7.6

S-8+35

4.8 4.8

S-9+10

4.5 5.1

S-0+00

5.1 8.0

S-

9-2-97					W-105+00			9-2-97	
0+00 =	STA- W 105+00	ON	B/L PT	STA	+	H.I.	-	ELEV	PT ①
STA	+	H.I.	-	ELEV					
	4.56	12.93		8.37	S-8+50	11.05	7.2	3.8	
					S-8+90		6.8	4.2	
0+00			5.2	7.7	S-9+30		7.0	4.0	
S-0+55			5.2	7.7	S-9+40		8.0	3.0	
S-1+10			5.5	7.4	S-9+80		8.2	2.8	
S-1+65			5.5	7.4	S-10+40		8.2	2.8	
S-2+25			5.3	7.6	S-11+05		8.3	2.7	
S-2+65			6.1	6.8	S-11+65		8.0	3.0	
S-3+15			6.0	6.9	S-12+00		8.1	2.9	
S-3+70			6.4	6.5					
S-4+25			7.5	5.4					
S-4+70			7.3	5.6					
S-5+30			7.2	5.7					
S-6+00			7.1	5.8					
T.P.	4.55	11.05	6.43	6.50					
S-6+40			5.7	5.3					
S-6+65			6.8	4.2					
S-7+05			7.1	3.9					
S-7+63			7.4	3.6					
S-8+05			6.9	4.1					

600' SOUTH
ON LINE

STA	T	H.I.	ELEV	9-2-17
0+00			5.2	9-2-17
STA-104+00 W			ON B/L	
STA	T	H.I.	ELEV	9-2-17
	9.79	12.61	7.82	9-2-17
0+00			5.2	9-2-17
S-0+60			5.3	9-2-17
S-1+10			5.4	9-2-17
S-1+75			5.6	9-2-17
S-2+30			5.5	9-2-17
S+2+85			5.4	9-2-17
S-3+35			5.7	9-2-17
S-3+90			5.8	9-2-17
S-4+50			7.9	9-2-17
S-5+10			8.1	9-2-17
S-5+75			7.7	9-2-17
S-6+30			8.1	9-2-17
S-6+90			7.8	9-2-17
S-7+45			7.9	9-2-17
S-8+00			7.8	9-2-17
T.P.	4.59	9.69	7.51	9-2-17
S-8+65			4.8	9-2-17
S-9+30			4.4	9-2-17

STA	T	H.I.	ELEV	9-2-17
W-104+00			9.69	9-2-17
S-10+05			4.5	9-2-17
S-10+65			5.7	9-2-17
S-11+50			6.2	9-2-17
S-12+35			6.2	9-2-17
S-13+05			6.3	9-2-17
S-13+80			6.9	9-2-17
S-14+45			6.9	9-2-17
S-15+30			7.0	9-2-17
S-16+00			6.8	9-2-17

5

PX

STA-103+00-W				9-2-97	W. 103+00			9-2-97	(6)			
0+00 = W 103+00 ON B/L.					STA-	+	H.I.	-	ELEV			
STA-	+	H.I.	-	ELEV	PX	S-2+00						
	5.63	13.00		7.37	W 104+00	T.P.	4.83	9.58	8.25	4.75	PX	ON LINE 300' SOUTH W 103+00
0+00			5.0	8.0		S-9+45			5.1	4.4		
S-0+50			5.2	7.8		S-9+35			4.9	4.6		
S-1+05			5.3	7.7		S-10+42			4.7	4.8		
S-1+55			5.6	7.4		S-10+85			4.7	4.8		
S-2+10			5.8	7.2		S-11+90			4.4	5.1		
S-2+60			7.1	5.9		S-11+85			4.5	5.0		
S-3+10			6.7	6.3		S-12+40			4.4	5.1		
S-3+60			6.4	6.6		S-13+10			4.4	5.1		
S-4+10			6.4	6.6		S-13+50			4.6	4.9		
S-4+60			7.8	5.2		S-14+05			4.7	4.8		
S-5+10			8.7	4.3		S-14+60			4.7	4.8		
S-5+50			8.7	4.3		S-15+25			5.1	4.4		
S-5+90			8.7	4.3		S-15+80			5.1	4.4		
S-6+25			8.7	4.3		S-16+15			5.3	4.2		
S-6+85			8.8	4.2		S-16+50			5.7	3.8		
S-7+35			8.6	4.4		S-16+60			7.1	2.4		
S-7+95			8.7	4.3		S-16+90			7.5	2.0		
S-8+35			8.8	4.2		S-17+25			7.5	2.0		
						S-18+00			7.1	2.4		

PX

W-102+00

9-2-77

STA

+

W-102+00

9-2-77

H.I.

ELEV

⑦

0+00 = STA W-102+00 ON B/L

10+50

12.86.

PX

STA-	+	H.I.	-	ELEV	T.P.				
T.B.M.	4.68	12.86		8.18	60	4.21	8.32	8.75	4.11
					TOP HIG				
					W-103+00			4.0	4.3
S 0+00			5.1	7.7	130			3.6	4.7
S S-0+70			5.3	7.5	135			3.1	5.2
S S-1+40			5.6	7.2	145			4.0	4.3
S S-2+05			5.6	7.2	145			4.2	4.1
S S-2+75			6.2	6.6	150			4.2	4.1
S S-3+40			6.4	6.4	155			4.5	3.8
S S-3+85			8.0	4.8	165			4.3	4.0
S S-4+05			6.7	6.1	175			4.2	4.1
S S-4+70			7.0	5.8	175			4.2	4.1
S S-5+45			8.4	4.4	180			4.5	3.8
S S-6+10			8.7	4.1	180			5.9	2.4
S S-6+80			9.0	3.8	190			6.0	2.3
S S-7+50			8.6	4.2	190			5.9	2.4
S S-8+05			8.7	4.1					
S S-8+70			8.8	4.0					
S S-9+30			8.8	4.0					
S 10+00			8.7	4.1					

PROJ-#3-1

BARRAGAN
SHEPPARD
STANLEY
9-18-47
CLARK
CARR
2002

W-83+00

9-18-47

(8)

PX

STA-83+00-W

DIST SOUND

DIST SOUND

0+00 = { STA W-83+00
N-168+69.30 } SOUND SOUTH AT 90° TO N-168+69.30

3+60 2.9 +1.3 5+60 3.2 +1.1

DIST SOUND DIST SOUND (4.2) 3.0 +1.2 09:15 3.3 +1.0

0+00 2.1 +2.1 1+80 2.6 +1.6 09:13 3.0 — 3.3 —

09:07 2.1 — (1.2) 2.6 — (4.3) 3.0 +1.3 (4.3) 3.3 —

(4.2) 2.1 — 2+00 2.7 +1.5 4+00 3.0 — 6+00 3.3 —

2.2 +2.0 2.8 +1.4 3.0 — PX 3.3 —

2.2 — 09:10 2.8 — 3.0 — 3.3 —

50 2.2 — 2.8 — 3.0 — 3.3 —

2.4 +1.8 2.8 — 3.0 — 3.3 —

2.4 — 50 2.8 — 50 3.0 — 50 3.3 —

2.4 — 2.9 +1.3 3.0 — 3.3 —

2.5 +1.7 2.9 — 3.0 — 3.3 —

1+00 2.4 +1.8 2.9 — 3.1 +1.2 3.3 —

2.5 +1.7 2.9 — 3.1 — 3.3 —

2.5 — 3+00 2.9 — 5+00 3.1 — 7+00 3.3 —

2.6 +1.6 2.9 — 3.1 — 3.3 —

2.6 — 2.9 — 3.1 — 3.4 +0.9

50 2.6 — 2.9 — 3.2 +1.1 3.4 —

2.6 — 2.9 — 3.2 — 3.4 —

1+70 2.6 — 3+50 2.9 — 5+50 3.2 — 7+50 3.4 —

W-83+00 9-18-97

DIST	SOUND	DIST	SOUND
16+10	1.2 +0.2		
	1.2		
(1.9)	1.2		PX
	1.2		
50	1.2		
	1.2		
	1.2		
	1.2		
	1.2		
17+00	1.2		
09:22			

W-83+00 9-18-97 (10)

SOUND NORTH AT 30° TO N. 168° 69.96 LINE.

DIST	SOUND	DIST	SOUND	PX
0+10	2.3 +2.2	2+00	2.0	+2.5
09:32	2.5 +2.0	09:35	2.0	
	2.1 +2.1		2.0	
(4.5)	2.1	(4.5)	2.0	
50	2.1		2.0	
	2.1	50	2.0	
	2.1		1.9	+2.6
	2.1		1.7	+2.8
	2.1		1.7	
50	2.1		1.7	
	2.2 +2.3	3+00	1.7	
	2.2		1.7	
	2.2	3+20	1.6	+2.9
	2.2	09:37		
50	2.2			
	2.2	50		
	2.1 +2.4			
	2.1			
1+30	2.0 +2.5			

PX

W-82+00

3-18-47

DIST SOUND

$$0+00 = \begin{cases} W-82+00 \\ N-168+69.36 \end{cases} \text{ SOUND SOUTH AT } 90^\circ \text{ TO } N-168+69.36$$

DIST SOUND DIST SOUND

0+00 2.5 +2.2 1+80 3.1 +1.3 (4.7)

09:13 2.5 — 3.1 —

2.5 — 2+00 3.1 —

(4.7) 2.6 +2.1 (4.7) 3.1 —

2.6 — 3.1 —

50 2.7 +2.0 3.1 —

2.9 +1.8 3.1 —

2.9 — 50 3.1 —

2.9 — 3.1 —

09:15 2.9 — 3.1 —

1+00 3.0 +1.7 3.1 —

3.0 — 3.1 —

3.0 — 3+00 3.1 —

3.0 — 3.1 —

3.1 +1.6 3.1 —

50 3.3 +1.4 3.1 —

3.1 +1.3 3.1 —

1+70 3.1 — 3+50 3.1 —

W-82+00

3-18-47

DIST SOUND

PX (11)

+1.2 5+60 3.8 +0.9

3.5 — 3.8 —

3.5 — (4.7) 3.8 —

3.5 — 3.9 +0.8

4+00 3.5 — 6+00 3.9 —

3.5 — 3.9 —

3.5 — 3.9 —

3.6 +1.1 3.9 —

3.6 — 3.9 —

50 3.6 — 50 3.9 —

3.7 +1.0 (4.7) 3.9 —

3.7 — 09:50 3.9 —

3.7 — (4.8) 3.9 +0.9

3.7 — 3.9 —

3.7 — 7+00 3.9 —

3.7 — 3.9 —

3.8 +0.9 3.9 —

3.8 — 3.9 —

3.8 — 3.9 —

4+50 3.8 — 7+50 3.9 —

W-82+00			9-18-17		
DIST	SOUND		DIST	SOUND	
7+60	3.9	+0.9	9+60	4.1	+0.7
	3.9	—	09:53	4.1	—
(4.8)	4.0	+0.8	(9.8)	4.1	—
	4.0	—		4.1	—
8+00	4.0	—	10+00	4.1	—
	4.0	—		4.1	—
	4.0	—		4.1	—
	4.0	—		4.1	—
	4.0	—		4.2	+0.6
50	4.0	—	50	4.2	—
	4.0	—		4.2	—
	4.0	—		4.2	—
	4.0	—		4.2	—
	4.1	+0.7		4.2	—
9+00	4.1	—	11+00	4.2	—
	4.1	—		4.2	—
	4.1	—		4.2	—
	4.1	—		4.2	—
	4.1	—		4.2	—
9+50	4.1	—	11+50	4.2	—

W-82+00			9-18-17		
DIST	SOUND		DIST	SOUND	
11+60	4.2	+0.6	13+60	4.4	+0.4
	4.3	+0.5		4.4	—
(4.8)	4.3	—	(7.8)	4.4	—
	4.3	—		4.4	—
12+00	4.3	—	14+00	4.4	—
03:55	4.3	—		4.5	+0.3
	4.3	—		4.5	—
	4.3	—		4.5	—
	4.3	—		4.5	—
50	4.3	—	50	4.5	—
	4.3	—		4.5	—
	4.3	—		4.5	—
	4.3	—		4.5	—
	4.3	—		4.5	—
	4.3	—		4.5	—
13+00	4.4	+0.4	15+00	4.5	—
	4.4	—		4.5	—
	4.4	—		4.6	+0.2
	4.4	—		4.6	—
	4.4	—		4.6	—
13+50	4.4	—	50	4.7	+0.1

W-82+00 9-18-17

DIST	SOUND	DIST	SOUND
15+60	4.7	+0.1	
(4.8)	4.7	—	
	4.7	—	
	4.7	—	
16+00	4.7	—	
	4.7	—	
16+20	4.7	—	
10:00			

W-82+00 9-18-17 (13)
 SOUND NORTH AT 90° TO N468+696 LINE.

DIST	SOUND	DIST	SOUND
16+10	2.9	+2.1	2+00 2.5 +2.5
16:05	2.9	—	PX 2.1 +2.6
	2.9	—	2.1 —
(5.0)	2.9	—	(5.0) 2.1 —
50	2.9	—	2.1 —
	2.9	—	50 2.1 —
	2.9	—	2.3 +2.7
	2.9	—	2.3 —
	2.9	—	2.2 +2.8
1700	2.9	—	2.2 —
	2.8	+2.2	3+00 2.2 —
	2.8	—	2.2 —
	2.8	—	2.1 +2.9
	2.7	+2.3	2.0 +3.0
50	2.7	—	2.0 —
	2.6	+2.4	50 2.0 —
	2.6	—	3+60 1.9 +3.1
	2.6	—	10:10
1730	2.5	+2.5	

PX W-81+00 9-18-17
 0+00 = $\begin{cases} SW-81+00 \\ N-168+67.96 \end{cases}$ SOUND SOUTH At 90° T. N. 168+51.2

DIST	SOUND		DIST	SOUND	
0+00	3.2	+2.0	1+80	3.7	+1.5
	3.2	—		3.7	—
10:18	3.2	—	2+00	3.7	—
(5.2)	3.2	—	(5.2)	3.8	+1.4
	3.2	—		3.8	—
50	3.2	—		3.8	—
	3.3	+1.9		3.8	—
	3.3	—	50	3.9	+1.3
	3.4	+1.8		3.9	—
	3.4	—		3.9	—
1+00	3.5	+1.7	10:20	3.9	—
	3.5	—		3.9	—
	3.5	—	3+00	3.9	—
	3.5	—		3.9	—
	3.7	+1.5		4.0	+1.2
50	3.7	—		4.0	—
	3.7	—		4.0	—
1+70	3.7	—	3+50	4.0	—

W-81+00 9-18-17 (14)
 DIST SOUND PX DIST SOUND
 3+60 4.0 +1.2 5+6.0 4.2 +1.0
 4.0 — 4.2 —
 4.0 — 4.2 —
 (5.2) 4.0 — (5.2) 4.2 —
 4.0 — 4.2 —
 4+00 4.0 — 6+00 4.3 +0.9
 4.0 — 4.3 —
 4.0 — 4.3 —
 4.0 — 4.3 —
 4.0 — 4.3 —
 50 4.0 — 50 4.3 —
 4.0 — 4.3 —
 4.1 +1.1 4.3 —
 4.1 — 4.3 —
 4.1 — 4.3 —
 5+00 4.1 — 7+00 4.3 —
 4.2 +1.0 4.3 —
 4.2 — 4.3 —
 4.2 — 4.4 +0.8
 4.2 — 4.4 —
 10:24 4.4 —
 5+50 4.2 — 7+50 4.4 —

W-81+00			9-18-17		
DIST	PX	SOUND	DIST	SOUND	
7+60	4.4	+0.8	9+60	4.5	+0.7
10:25	4.4	—		4.5	—
	4.4	—		4.5	—
(5.2)	4.4	—	(5.2)	4.5	—
8+00	4.4	—	10+00	4.5	—
	4.4	—		4.5	—
	4.5	+0.7		4.5	—
	4.5	—		4.5	—
	4.5	—		4.6	+0.6
50	4.5	—	50	4.6	—
	4.5	—		4.6	—
	4.5	—		4.6	—
	4.5	—		4.6	—
	4.5	—		4.6	—
9+00	4.5	—	11+00	4.6	—
	4.5	—		4.6	—
	4.5	—		4.6	—
	4.5	—		4.6	—
	4.5	—		4.6	—
9+50	4.5	—	11+50	4.6	—

W-8400			9-18-17		
DIST	PX	SOUND	DIST	SOUND	
11+60	4.7	+0.5	13+60	4.8	+0.4
	4.7	—		4.8	—
	4.7	—	(5.2)	4.8	—
(5.2)	4.7	—	10:30	4.8	—
12+00	4.7	—	14+00	4.8	+0.5
10:28	4.7	—	(5.3)	4.9	+0.4
	4.8	+0.4		4.9	—
	4.8	—		4.9	—
	4.8	—		4.9	—
50	4.8	—	50	4.9	—
	4.8	—		4.9	—
	4.8	—		4.9	—
	4.8	—		4.9	—
	4.8	—		4.9	—
13+00	4.8	—	15+00	4.9	—
	4.8	—		4.9	—
	4.8	—		4.9	—
	4.8	—		4.9	—
	4.8	—		4.9	—
13+50	4.8	—	15+50	4.9	—

W- 81+00 9-18-17

DIST	SOUND	PX	DIST	SOUND	PX
15+60	4.9	+0.4	16+10	5.0	+0.3
(5.3)	4.9	—	(5.3)	5.0	—
	4.9	—		5.0	—
	1.9	—		5.0	—
16+00	5.0	+0.3	16+50	5.0	—
			10:33		

W- 81+00 9-18-17 (26)

SW- 81+00
 0+00 = (N-168+69.96) SOUND NORTH AT 90° TO N-168+69.96 LINE.

DIST	SOUND	PX	DIST	SOUND	PX
0+10	3.2	+2.2	2+00	3.0	+2.4
	3.2	—		3.0	—
10:39	3.3	+2.1	(5.4)	2.9	+2.5
(5.1)	3.3	—	10:42	2.8	+2.6
50	3.3	—		2.8	—
	3.3	—	50	2.8	—
	3.3	—		2.7	+2.7
	3.2	+2.2		2.7	—
	3.2	—		2.7	—
1+00	3.2	—		2.6	+2.8
	3.2	—	3+00	2.6	—
	3.2	—		2.5	+2.9
	3.2	—		2.5	—
50	3.1	+2.3		2.5	—
	3.0	+2.4	50	2.5	—
	3.0	—		2.5	—
	3.0	—	10:45	2.4	+3.0
1+30	3.0	—	4+00	2.4	—
			4+10	2.2	+3.2
			4+20	2.2	—
			4+30	2.2	+3.4
				3.0	—

W. 80+00				W. 80+00				
DIST	SOUND	PX	DIST	SOUND	PX	DIST	SOUND	
7+60	4.8	+0.7	9+60	5.0	+0.5	11+60	5.2	
(5.5)	4.8	—	(5.5)	5.0	—		5.2	
	4.8	—		5.0	(5.5)	(5.5)	5.2	
	4.8	—		5.0	—		5.2	
8+60	4.8	—	10+60	5.0	—	12+60	5.2	
	4.9	+0.6		5.0	—		5.2	
	4.9	—	11:03	5.0	—		5.2	
	4.9	—		5.0	—		5.2	
	4.9	—		5.0	—		5.3	
50	4.9	—	50	5.0	—	50	5.3	
	4.9	—		5.0	—		5.3	
	4.9	—		5.0	—		5.3	
	4.9	—		5.0	—		5.3	
	4.9	—		5.0	—	11:08	5.3	
9+60	4.9	—	11+60	5.0	—	13+60	5.3	
	4.9	—		5.0	—		5.3	
	5.0	+0.5		5.0	—		5.3	
	5.0	—		5.0	—		5.3	
	5.0	—		5.0	—		5.3	
9+50	5.0	—	11+50	5.0	—	13+50	5.2	
						+0.3	15+50	5.3

W-80+00 9-18-47

DIST	SOUND	Px	DIST	SOUND
15+60	5.3	+0.2	17+10	5.9
(5.5)	5.9	+0.1		5.9
	5.9	—	(5.5)	5.9
	5.9	—	<u>11:10</u>	5.9
16+00	5.9	—	50	5.4 +0.2
	5.9	—	(5.6)	5.9
	5.9	—		5.5 +0.1
	5.9	—		5.5
	5.9	—		5.5
50	5.9	—	18+00	5.5
	5.9	—		5.5
	5.9	—		5.5
	5.9	—		5.5
	5.9	—		5.5
17+00	5.9	—	18+50	5.5

W-80+00 9-18-47 (19)
 SW-80+00
 1+00 = (N-150+67.36) SOUND NORTH AT 90° TO N-160+69.96 d.

DIST	SOUND	Px	DIST	SOUND
0+10	3.8	+1.9	2+00	3.3 +2.4
	3.8	—		3.3
<u>11:24</u>	3.8	—		3.3
(5.7)	3.8	—	(5.7)	3.2 +2.5
50	3.8	—		3.1 +2.6
	3.7	+2.0	50	3.1
	3.7	—		3.1
	3.7	—		3.0 +2.7
	3.7	—		3.0
1+00	3.7	—		3.0
	3.7	—	3+00	3.0
	3.7	—		3.0
	3.7	—		3.0
	3.7	—		3.0
50	3.6	+2.1		2.9 +2.8
	3.6	—	50	2.8 +2.9
	3.5	+2.2		2.8
	3.5	—		2.7 +3.0
<u>11:22</u>				2.6 +3.1
1+30	3.4	+2.3	3+90	2.5 +3.2

W-79400			9-18-17		
DIST	SOUND		DIST	SOUND	
7+60	5.2	+0.5	9+60	5.4	+0.3
	5.2	—		5.4	—
(5.7)	5.2	—	(5.7)	5.4	—
	5.3	+0.4		5.4	—
8+00	5.3	—	10+00	5.4	—
	5.3	—		5.4	—
	5.3	—		5.4	—
	5.3	—		5.4	—
	5.3	—		5.4	—
50	5.3	—	50	5.4	—
	5.3	—		5.4	—
<u>12:35</u>	5.3	—		5.4	—
	5.4	+0.3		5.4	—
	5.4	—		5.4	—
9+00	5.4	—	11+00	5.4	—
	5.4	—		5.4	—
	5.4	—		5.4	—
	5.4	—		5.4	—
	5.4	—		5.4	—
9+50	5.4	—	11+50	5.4	—

W-79400			9-18-17 (2)		
DIST	SOUND		DIST	SOUND	
11+60	5.4	+0.3	13+60	5.5	+0.2
	5.4	—		5.6	+0.1
(5.7)	5.4	—		5.6	—
	5.4	—	(5.7)	5.6	—
12+00	5.5	+0.2	14+00	5.6	—
	5.5	—	<u>12:40</u>	5.6	—
	5.5	—		5.6	—
<u>12:38</u>	5.5	—		5.6	—
	5.5	—		5.6	—
50	5.5	—	50	5.6	—
	5.5	—		5.6	—
	5.5	—		5.6	—
	5.5	—		5.6	—
	5.5	—		5.6	—
13+00	5.5	—	15+00	5.6	—
	5.5	—		5.6	—
	5.5	—		5.6	—
	5.5	—		5.6	—
	5.5	—		5.6	—
13+50	5.5	—	15+50	5.6	—

W-79+00
9-18-17

DIST	SOUND	PX	DIST	SOUND	
15+60	5.6	+0.1	17+60	5.8	-0.1
	5.6	—		5.8	—
(5.7)	5.6	—	(5.7)	5.8	—
	5.6	—		5.8	—
16+00	5.6	—	18+00	5.8	—
	5.7	0.0		5.8	—
	5.7	—		5.8	—
	5.7	—		5.8	—
	5.7	—		5.8	—
50	5.7	—	50	5.8	—
12:43	5.7	—		5.8	—
	5.7	—		5.8	—
	5.7	—		5.8	—
	5.7	—		5.8	—
17+00	5.8	-0.1	19+00	5.8	—
	5.8	—	12:45		
	5.8	—			
	5.8	—			
	5.8	—			
17+50	5.8	—			

SW-79+00
9-18-17
0+00 (W-79+00 N-168+67.36) SOUND NORTH AT 90° TO N 168° 49' 24"

(22)

DIST	SOUND		DIST	SOUND	
0+10	3.7	+1.9	2+00	3.2	+2.4
12:54	3.7	—		3.1	+2.5
	3.7	—		3.1	—
(5.6)	3.7	—	(5.6)	3.0	+2.6
50	3.6	+2.0		3.0	—
	3.6	—	50	3.0	—
	3.6	—		3.0	—
	3.6	—		2.9	+2.7
	3.6	—		2.9	—
400	3.6	—		2.9	—
	3.6	—	3+00	2.9	—
	3.5	+2.1		2.8	+2.8
	3.5	—		2.8	—
	3.5	—		2.8	—
	3.5	—		2.8	—
50	3.5	—		2.7	+2.9
	3.4	+2.2	50	2.6	+3.0
	3.4	—		2.5	+3.1
	3.3	+2.3	12:57	2.3	+3.3
		—		2.0	+3.6
1+00	3.3	—		2.0	+3.7
		—	1+00	1.9	+3.7

		W-78+00		9-18-47	
DIST	SOUND	DIST	SOUND	DIST	SOUND
7+60	1.9	+0.6	9+60	5.1	+0.4
PX	1.9	—		5.1	—
(5.5)	1.9	—	(5.5)	5.1	—
	4.9	—		5.1	—
8+00	4.9	—	10+00	5.1	—
	4.9	—		5.1	—
	4.9	—		5.1	—
	5.0	+0.5		5.1	—
	5.0	—		5.1	—
50	5.0	—	(5.5) 50	5.1	—
13:13	5.0	—	13:15	5.1	—
	5.0	—		5.1	+0.3
	5.0	—	(5.4)	5.1	—
	5.0	—		5.1	—
9+00	5.0	—	11+00	5.1	—
	5.0	—		5.1	—
	5.1	+0.4		5.1	—
	5.1	—		5.1	—
	5.1	—		5.1	—
9+50	5.1	—	11+50	5.1	—

		W-78+00		9-18-47	
DIST	SOUND	DIST	SOUND	DIST	SOUND
11+60	5.1	+0.3	13+60	5.2	+0.2
	5.1	—	13:18	5.2	—
(5.4)	5.1	—	(5.4)	5.2	—
	5.1	—		5.2	—
12+00	5.1	—	14+00	5.2	—
	5.1	—		5.2	—
	5.1	—		5.2	—
	5.1	—		5.2	—
50	5.1	—	50	5.2	—
	5.1	—		5.2	—
	5.1	—		5.2	—
	5.1	—		5.2	—
	5.2	+0.2		5.3	+0.1
13+00	5.2	—	15+00	5.3	—
	5.2	—		5.3	—
	5.2	—		5.4	0.0
	5.2	—		5.4	—
	5.2	—		5.4	—
13+50	5.2	—	15+50	5.4	—

DIST. PX SOUND		W - 78+00		9-18-17	
DIST.	SOUND	DIST.	SOUND		
15+60	5.7	0.0	17+60	5.5	-0.1
13:20	5.7	—	5.5	—	
(5.4)	5.7	—	(5.4)	5.5	—
	5.7	—	5.5	—	
16+00	5.7	—	18+00	5.5	—
	5.7	—	13:23		
	5.7	—			
	5.7	—			
	5.5	-0.1			
50	5.5	—			
	5.5	—			
	5.5	—			
	5.5	—			
	5.5	—			
17+00	5.5	—			
	5.5	—			
	5.5	—			
	5.5	—			
17+50	5.5	—			

W - 78+00			9-18-17		
DIST.	SOUND		DIST.	SOUND	PX
0+00 = $\sqrt{W-78+00}$ $(N-168+67.9) \text{ dms}$			SOUND NORTH AT 90° To N-168+67.9 dms		(25)
0+10	3.5	+1.8	2+00	2.7	+2.6
	3.5	—		2.7	—
13:30	3.5	—	(5.3)	2.7	—
	3.4	+1.9		2.7	—
50	3.4	—	PX	2.5	+2.8
(5.3)	3.4	—	50	2.5	—
	3.4	—		2.4	+2.9
	3.4	—		2.3	+3.0
	3.3	+2.0		2.2	+3.1
1+00	3.3	—		2.1	+3.2
	3.2	+2.1	3+00		
	3.1	+2.2	13:32		
	3.0	+2.3			
	3.0	—			
50	2.9	+2.4			
	2.9	—			
	2.9	—			
	2.8	+2.5			
1+90	2.8	—			

PX

W-77+00

9-18-17

W-77+00

9-18-17

(20)

DIST SOUND

DIST SOUND

PX

0+00 = $\begin{cases} W-77+00 \\ N-168+69.96 \end{cases}$

SOUND SOUTH AT 90° TO N. WIND

3+60

4.0

+0.9

5+60

4.1

+0.8

DIST SOUND

DIST SOUND

4.0

4.1

0+00

3.2

+1.7

1+60

3.8

+1.1

(4.9)

4.0

—

(4.9)

4.2

+0.7

11:03

3.1

+1.8

11:05

3.8

—

4.0

—

4.3

+0.6

3.1

—

2+00

3.9

+1.0

4+00

4.0

—

6+00

4.3

—

(4.9)

3.2

+1.7

(4.9)

3.9

—

4.0

—

4.3

—

3.2

—

3.9

—

4.0

—

4.3

—

50

3.2

—

4.0

+0.9

4.0

—

4.3

—

3.2

—

4.0

—

4.0

—

4.3

—

3.2

—

50

4.0

—

50

4.0

—

50

4.3

—

3.4

+1.5

4.0

—

4.0

—

(4.9)

4.3

—

3.5

+1.4

4.0

—

4.1

+0.8

11:10

4.1

+0.5

1+00

3.5

—

4.0

—

4.1

—

(4.8)

4.1

+0.4

3.6

+1.3

4.0

—

14:00

4.1

—

4.1

—

3.6

—

3+00

4.0

—

5+00

4.1

—

7+00

4.1

—

3.6

—

4.0

—

4.1

—

4.1

—

3.6

—

4.0

—

4.1

—

4.1

—

50

3.7

+1.2

4.0

—

4.1

—

4.1

—

3.7

—

4.0

—

4.1

—

4.1

—

1+70

3.8

+1.1

3+50

4.0

—

5+50

4.1

—

7+30

4.1

—

DIST PX		W-77+00		9-18-17		DIST SOUND		W-77+00		9-18-17		DIST SOUND PX	
DIST	SOUND	DIST	SOUND	DIST	SOUND	DIST	SOUND	DIST	SOUND	DIST	SOUND	DIST	SOUND
8+60	4.4	+0.4	10+60	4.5	+0.3	12+60	4.6	+0.2	14+60	4.9	-0.1		
	4.4	—		4.6	+0.2		4.6	—		4.9	—		
(4.8)	4.4	—	(4.8)	4.6	—	(4.8)	4.6	—	(4.8)	4.9	—		
	4.4	—		4.6	—		4.6	—		4.9	—		
9+00	4.4	—	11+00	4.6	—	13+00	4.6	—	15+00	4.9	—		
	4.4	—		4.6	—		4.6	—		4.9	—		
	4.4	—		4.6	—	14.15	4.7	+0.1	14.18	4.9	—		
	4.4	—		4.6	—		4.7	—		4.9	—		
	4.4	—		4.6	—		4.8	0.0		4.9	—		
50	4.4	—	50	4.6	—	50	4.8	—	50	4.9	—		
	4.4	—		4.6	—		4.8	—		4.9	—		
	4.5	+0.3		4.6	—		4.8	—		4.9	—		
	4.5	—		4.6	—		4.8	—		4.9	—		
	4.5	—		4.6	—		4.8	—		4.9	—		
10+00	4.5	—	12+00	4.6	—	14+00	4.8	—	16+00	4.9	—		
	4.5	—		4.6	—		4.8	—		4.9	—		
	4.5	—		4.6	—		4.8	—		4.9	—		
	4.5	—	14.13	4.6	—		4.8	—		4.9	—		
	4.5	—		4.6	—		4.8	—		4.9	—		
50	4.5	—	12+50	4.6	—	14+50	4.8	—	16+50	4.9	—		

W-77+00		9-18-17	
DIST	SOUND	DIST	SOUND
16+60	4.9	-0.1	
<u>14:20</u>	4.9	—	
	4.9	—	
(4.8)	4.9	—	
17+00	4.9	—	
	4.9	—	
	4.9	—	
	4.9	—	
	4.9	—	
50	4.9	—	
	4.9	—	
	4.9	—	
	4.9	—	
	4.9	—	
18+00	4.9	—	
	4.9	—	
	4.9	—	
	4.9	—	
<u>14:23</u>	4.9	—	
18+50	4.9	—	

W-77+00		9-18-17	
(W-77+00 0+00 = (W-168+14.96))		PROS-#3-1 NORTH AT 90° To N. 168+14.96	
DIST	SOUND	DIST	SOUND
0+10	2.8	+1.8	2+00 2.0 +2.6
	2.8	—	2.0 —
<u>14:30</u>	2.7	+1.9	(4.6) 1.9 +2.7
(4.6)	2.7	—	1.8 +2.8
50	2.7	—	2+10 1.7 +2.9
	2.6	+2.0	
	2.6	—	
	2.6	—	
	2.5	+2.1	
1+00	2.5	—	
	2.3	+2.3	
	2.3	—	
	2.2	+2.4	
	2.1	+2.5	
50	2.0	+2.6	
	2.0	—	
	2.0	—	
	2.0	—	
1+90	2.0	—	

PX

FLOWLINE ELEV'S OF
 CULVERTS ALONG HI-WAY
 101-PROJECT No. 3-1

12.68
 3.64
 9.94
 5.90
 15.37
 8.81
 .57

Indexed

9-24-97

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STA	+ H.I.	-	ELEV.	GRADE		
T.B.M.	5.64	18.22	12.58		TOP HUB 151+00	(SEE PG 1)
⁸⁰ 151+58			10.84	1%	F.L. WEST 48" CULV	92' LONG
⁸⁰ 151+58			9.85	8.37	F.L. EAST " "	
T.B.M.	5.22	15.63	⁴¹ 10.47		TOP HUB 160+00	
⁵⁹ 159+30			10.98	3.7%	F.L. WEST 12" CULV.	110' LONG
⁵⁴ 159+30			6.90	8.73	" EAST " "	
T.B.M.	5.40	15.24	9.84		TOP HUB 164+00	
⁵⁴ 164+20			8.81	1%	F.L. WEST 24" CULV.	90' LONG
164+20			7.66	7.58	" EAST " "	
T.B.M.	5.68	16.06	10.38		TOP HUB 167+00	
167+15			9.02	1.5%	F.L. WEST 24" CULV	96' LONG
167+15			7.49	8.57	" EAST 24" "	
T.B.M.	6.18	16.87	10.69		TOP HUB 168+00	
⁵⁴ W 73+35			10.12	6.75	F.L. WEST 36" CULV.	100' LONG.
73+35			8.52	8.35	" EAST " "	
T.B.M.	5.15	17.08	11.93		TOP HUB 76+20 W	55' PAV.
W 77+40			9.00	8.08	F.L. WEST 30" CULV.	80' LONG Rdw. 75
W 77+40			8.30	8.78	" EAST " "	

BARRAGAN 12-17-47
 SHREVE CLOUDY
 STANLEY COOL
 CLEAR

12-17-47

(30)

TOPOGRAPHIC FEATURES OF ROSE CREEK

H.I. = 13.25

AND BANKS

N 17,244.60

STA 106+00 W 10,600 (SEE PAGE 29 FOR CONTROL POINTS)

W 105+00 EL. 7.82 + 5.93 H.I. = 13.25

STA	AZIM.	DIST	POD	ELEV	OBJECT
W 106+00	75°37'15"				STAGSW
1	"	90	5.7	7.5	
2	"	50	5.5	7.7	
3	"	25	5.1	8.1	
4	"	20	5.3	7.9	
1	235°37'15"	32	5.7	7.5	
2	"	4.0	5.5	7.7	
3	"	46	6.8	6.4	
4	"	65	7.0	6.2	
5	"	70	8.7	4.5	
6	"	75	9.2	4.0	
7	"	105	9.0	4.2	
8	"	132	8.7	4.5	
9	"	157	8.5	4.7	
10	"	162	7.2	6.0	
11	"	165	5.5	7.7	
12	"	172	4.9	8.3	

STA	AZIM	DIST	POD	ELEV
106+00W	235°37'15"	190	5.5	7.7
14	"	232	4.9	8.3
15	"	295	5.0	8.2
16	"	365	4.5	8.7
1	226°35'	420	6.2	7.0
2	209°30'	395	6.2	7.0
3	200°03'	370	6.7	6.5
4	199°	350	7.3	5.9
5	195°12'	337	6.7	6.5
6	199°28'	346	9.5	3.7
7	192°30'	325	9.1	3.8
8	186°40'	370	9.2	4.0
9	182°36'	302	8.8	4.4
10	177°30'	300	9.5	3.7
11	176°49'	297	7.3	5.9
12	175°05'	295	6.0	7.2
13	169°15'	290	6.6	6.6
14	153°53'	300	6.1	7.1
15	150°55'	255	5.9	7.3

Indicated

X-SECTION
 ALONG
 DE ANZAB/L
 CONT'D.

X-SECTION
 ALONG
 DE ANZAB/L

12-17-47

STA	AZIM	DIST	POD	ELEV
Δ 106+00W			H.I. = 13.25	
	161°30'	240	6.4	6.8
	171°08'	235	6.3	6.9
	178°07'	235	5.8	7.4
	180°43'	235	9.1	4.1
	186°26'	240	9.3	3.9
	189°14'	243	9.7	3.5
	192°35'	248	9.3	3.9
	199°23'	260	8.4	4.8
	204°12'	272	9.0	4.2
	205°28'	280	6.1	7.1
	210°32'	300	6.5	6.7
	216°30'	327	6.0	7.2
	221°06'	365	5.6	7.6
	225°22'	415	6.0	7.2
	232°36'	390	5.6	7.6
	230°10'	345	5.3	7.9
	226°42'	295	5.5	7.7
	222°43'	260	5.9	7.3
	217°04'	230	5.7	7.5

12-17-47

(31)

STA	AZIM	DIST	POD	ELEV	OBJ.
Δ 106+00W			H.I. = 13.25		
	216°37'	230	7.7	5.8	
	216°47'	226	8.6	4.6	
	208°30	205	8.4	4.8	
	199°45'	182	9.8	3.7	
	189°43'	167	9.6	3.6	
	188°02'	165	7.7	5.5	
	186°25'	165	6.6	6.6	
	180°14'	164	6.1	7.1	
	163°33'	160	5.8	7.4	
	155°15'	162	6.5	6.7	
	142°19'	175	5.9	7.3	
Δ 106+00W	75°37/15	STA-105+00W EL = 7.82 + 5.33 = 13.15		H.I. (12-18-47)	
	118°34'	105	5.4	7.7	
	136°42'	75	5.4	7.7	
	174°40'	60	5.2	7.9	
	201°30'	68	5.9	7.2	
	213°05'	84	6.6	6.5	
	221°45'	87	10.3	2.8	
	224°15'	93	10.6	2.6	

STA T 106+00W	AZIM	DIST	POD H.I. = 13.15	ELEV
	227°35'	100	9.0	4.1
	234°20'	128	9.0	4.1
	239°30'	147	9.1	4.0
	239°36'	156	8.1	5.0
	242°05'	173	7.3	5.8
	242°15'	180	5.9	7.2
	242°00'	185	5.6	7.5
	245°55'	210	5.2	7.9
	246°20'	245	5.2	7.9
	248°05'	295	5.4	7.7
	248°10'	340	4.7	8.4
	264°30'	358	4.6	8.5
	266°45'	310	4.8	8.3
	268°22'	280	4.1	9.0
	270°41'	245	4.7	8.4
	274°05'	208	4.7	8.4
	278°07'	172	4.6	8.5

Sta T W106+00	AZIM	Dist	Rod	Elev
	278°37'	168	7.0	6.1
	280°12'	157	9.0	4.1
	282°51'	142	9.3	3.8
	288°05'	120	8.8	4.3
	297°30'	95	9.2	3.9
	301°30'	88	9.4	3.7
	303°20'	85	6.5	6.6
	316°27'	60	6.8	6.3
	321°05'	60	7.5	8.6
	08°15'	55	4.7	8.4
	39°35'	98	5.0	8.1
	28°45'	196	5.1	8.0
	19°25'	126	5.3	7.8
	356°36'	116	4.5	8.6
	336°10'	124	4.4	8.7
	333°41'	125	6.4	6.7
	322°51'	140	7.0	6.1
	327°06'	142	8.9	4.2
	318°30'	148	8.3	4.8

12-18-47

H.I. = 13.15

STA T	AZIM	DIST	ROD	ELEV
W106+00	314°40'	157	7.9	5.2
	313°30'	160	8.6	4.5
	308°00'	175	8.8	4.3
	303°33'	190	9.1	4.0
	301°45'	202	8.9	4.2
	301°07'	205	6.5	6.6
	300°06'	208	4.9	8.2
	295°28'	237	4.6	8.5
	289°05'	282	4.6	8.5
	284°50'	327	4.6	8.5
	293°15'	360	4.4	8.7
	298°00'	320	5.0	8.1
	304°10'	280	4.9	8.2
	310°32'	255	5.4	7.7
	311°00'	250	6.9	6.2
	311°30'	252	9.3	3.8
	313°16'	245	9.3	3.8
	316°45'	240	8.9	4.2
	321°55'	225	8.6	4.5

12-18-47

33

H.I. = 13.15

STA T	AZIM	DIST	ROD	ELEV
106+00	322°48'	225	7.6	5.5
	326°20'	216	7.8	5.3
	328°55'	211	8.6	4.5
	330°10'	210	8.7	4.4
	332°05'	206	7.2	5.9
	335°48'	203	6.2	6.9
	337°37'	202	7.0	9.1
	354°20'	197	4.5	8.6
	02°12'	202	4.6	8.5
	02°28'	275	4.4	8.7
	349°52'	270	4.4	8.7
	338°36'	271	4.0	9.1
	336°46'	272	5.3	7.8
	334°55'	275	8.1	5.0
	331°16'	280	8.4	4.7
	330°	282	7.6	5.5
	327°20'	285	8.4	4.7
	321°49'	300	9.1	4.0
	318°36'	303	9.7	3.4

STA	AZIM	DIST	ROD	ELEV	OBJ.
H.I. = 13.15					
W106+00	318°00'	304	9.3	3.8	
	317°25'	307	6.6	6.5	
	316°45'	310	4.9	8.2	
	308°40'	340	4.4	8.7	
	301°15'	395	4.1	9.0	
T.B.M #1 EL. 9.78 + 9.67 = 19.45 H.I.					
5+00 N	165°00"				106+000
	345°00'00"				
	223°45'	290	4.9	9.5	
	220°	262	5.3	9.1	
	214°25'	235	5.7	8.7	
	210°05'	222	6.7	7.7	
	207°20'	210	7.2	7.2	
	206°	205	10.2	4.2	
	202°05'	198	10.2	4.2	
	195°25'	185	10.1	4.3	
	189°43'	170	9.5	4.9	
	183°07'	170	8.1	6.3	
	181°10'	168	8.0	6.4	
	179°40'	165	5.2	9.2	
	158°35'	165	5.0	9.2	

STA	AZIM	DIST	ROD	ELEV	OBJ.
H.I. = 14.45					
5+00 N	131°15'	198	5.4	9.0	
	121°45'	158	5.3	9.1	
	135°35'	123	5.2	9.2	
	160°42'	96	4.4	10.0	
	197°05'	93	4.1	10.3	
	198°12'	96	7.2	7.2	
	206°00'	100	9.0	5.4	
	207°35'	100	10.1	4.3	
	212°30'	122	11.7	2.7	
	224°00'	135	10.5	3.9	
	225°00'	137	9.1	5.3	
	229°30'	152	7.9	6.5	
	234°42'	175	6.7	7.7	
	239°10'	210	7.4	7.0	
	243°03'	245	7.0	7.4	
	247°00'	282	6.5	7.9	
	259°	277	6.0	8.4	
	259°30'	250	6.5	7.9	
	258°35'	190	7.3	7.1	
	258°35'	160	6.7	7.7	

H.I. = 14.45

STA ↑	AZIM	DIST	ROD	ELEV
5+00N	257°40'	114	8.3	6.1
	257°40'	105	10.2	4.2
	258°25'	80	11.2	3.2
	257°10'	62	10.2	4.2
	257°10'	61	8.5	5.9
	258°45'	55	5.5	8.9
	258°45'	50	3.9	10.5
	162°05'	10'	4.8	9.6
	93°30'	67	5.3	9.1
	86°50'	166	5.3	9.1
	63°47'	170	5.3	9.1
	60°47'	100	5.5	8.9
	349°49'	52	4.8	9.6
	307°20'	78	4.8	9.6
	303°15'	87	8.5	5.9
	303°	89	10.2	4.2
	302°50'	91	11.7	2.7
	299°40'	105	12.2	2.2
	290°10'	117	11.3	3.1
	289°15'	120	9.3	5.1

12-18-97

H.I. = 14.45

STA ↑	AZIM	DIST	ROD	ELEV
5+00N	286°45'	130	7.8	6.6
	281°15'	161	6.8	7.6
	278°	185	6.2	8.2
	275°	225	6.1	8.3
	288°45'	260	5.9	8.5
	291°30'	290	6.8	7.6
	296°10'	210	6.4	8.0
	302°05'	186	7.5	6.9
	305°05'	175	9.2	5.2
	305°45'	174	11.1	3.3
	312°55'	162	12.0	2.1
	320°35'	140	10.2	4.2
	321°45'	136	8.0	6.4
	324°32'	130	4.9	9.5
	348°	105	4.7	9.7
	22°35'	117	5.0	9.4
	31°02'	130	6.9	7.5
	40°25'	158	5.2	9.2
	51°	208	5.4	9.0

12-18-97

STA T _Δ 5+00N	AZIM	H.I. = 14.45 DIST	ROD	ELEV
	39° 55'	240	4.6	9.8
	29° 30'	194	4.7	9.7
	00° 13'	182	4.5	9.9
	353° 30'	185	6.6	7.8
	348° 30'	184	5.2	9.2
	332° 30'	200	4.1	10.3
	329° 35'	204	9.5	4.9
	325° 17'	210	9.2	5.2
	323° 05'	212	11.7	2.7
	320° 45'	218	10.7	3.7
	320° 09'	220	8.9	5.5
	314° 50'	235	9.3	5.1
	311° 40'	245	9.3	5.1
	310° 30'	250	6.8	7.6
	309° 30'	255	5.6	8.8
	307° 45'	266	6.1	8.3
	302°	290	6.0	8.4
	297° 45'	327	6.4	8.0
	304° 10'	390	4.0	10.4

12-18-47

STA T _Δ 5+00N	AZIM	H.I. = 14.45 DIST	ROD	ELEV
	367° 45'	365	4.1	10.3
	311° 40'	345	4.4	10.0
	314° 30'	330	5.4	9.0
	317° 10'	322	6.7	7.7
	319° 45'	312	7.6	6.8
	320° 15'	318	10.1	4.3
	321° 20'	310	11.7	2.7
	323° 33'	305	8.5	5.9
	322° 35'	290	8.6	5.8
	333° 05'	280	8.5	5.9
	334° 13'	276	11.0	3.4
	334° 57'	280	10.1	4.3
	336° 42'	275	4.5	9.9
	338° 16'	272	5.7	8.7
	340°	270	5.3	9.1
	343° 07'	265	4.3	10.1
	356°	260	4.4	10.0
	11° 32'	280	4.1	10.3

12-18-47

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12-18-97

T.B.M. #2 E.L. 2.28 + 5.07 = 15.05 H.I.

0

STA T Δ 10+00 N	AZIM	DIST	ROD	ELEV	OBJ.
	165°00'				106+000
	127°30'	235	5.6	9.4	
	138°50'	200	4.6	10.4	
	154°15'	170	4.8	10.2	
	174°10'	160	4.9	10.1	
	176°	160	6.6	8.4	
	178°40'	161	6.2	8.8	
	181°	163	9.5	5.5	
	187°45'	165	9.4	5.6	
	185°30'	166	10.9	4.1	
	188°05'	167	12.5	2.5	
	191°15'	170	10.9	4.1	
	191°40'	170	10.0	5.0	
	198°40'	175	9.5	5.5	
	207°40'	190	9.5	5.5	
	207°50'	193	7.9	7.1	
	209°20'	196	5.7	9.3	
	215°13'	212	5.5	9.5	

H.I. = 15.05

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STA T 10+00 N	AZIM	DIST	ROD	ELEV
	219°30'	247	4.4	10.6
	226°50'	285	5.0	10.0
	238°15'	250	4.8	10.2
	236°	210	4.5	10.5
	237°30'	172	5.1	9.9
	229°45'	142	5.3	9.7
	228°53'	135	7.7	7.3
	227°45'	130	9.6	5.4
	220°45'	105	9.4	5.6
	219°45'	105	12.6	2.4
	215°55'	95	12.2	2.8
	215°	92	9.3	5.7
	199°22'	75	9.2	5.8
	197°55'	74	10.1	4.9
	195°	72	7.9	7.1
	192°	68	4.4	10.6
	155°30'	78	3.0	12.0
	154°50'	76	6.3	8.7
	151°05'	78	8.8	6.2

H.I. = 15.05

12-18-47

STA T 10+00N	AZIM	DIST	ROD	ELEV
	123°	112	8.4	6.6
	165°07	170	7.1	7.9
	87°40'	164	8.7	6.3
	89°10'	95	7.1	7.6
	85°30'	28	9.7	5.3
	85°30'	26	7.6	7.4
	85°30'	24	4.5	10.5
	00°	00	7.9	10.1
	160°05	120	4.0	11.0
	156°45	120	8.1	6.9
	134°	195	8.9	6.1
	131°45'	200	7.9	10.1
	108°30'	253	4.6	10.4
	107°06'	250	9.0	6.0
	¹ 259°55'	24	5.0	10.0
	¹ 259°55'	26	7.7	7.3
	260	28	8.8	6.2
	256°	30	10.9	4.1
	256°50	35	10.6	4.4

H.I. = 15.05

12-18-47

STA T 10+00N	AZIM	DIST	ROD	ELEV
	257°	37	9.3	5.7
	258°50'	77	9.2	5.8
	258°50'	80	12.1	2.9
	258°25'	87	11.7	3.3
	257°45'	95	9.7	5.3
	257°45'	112	9.0	6.0
	258°35'	120	6.0	9.0
	258°33'	125	5.0	10.0
	258°30'	162	5.0	10.0
	258°35'	205	4.6	8.1
	258°34'	250	4.9	10.1
	275°45'	263	4.7	10.3
	278°45'	227	4.7	10.3
	283°20'	196	4.7	10.3
	291°	152	5.5	9.5
	293°22'	145	8.3	6.7
	294°05'	142	11.1	3.9
	297°40'	130	10.4	4.6
	298°30'	130	9.2	5.8

STA	AZIM	H.I. = 15.05 DIST	ROD	ELEV
TION				
	306°15'	111	8.7	6.3
	312°05'	98	9.5	5.5
	311°55'	93	9.7	5.3
	329°	85	9.4	5.6
	331°20'	80	5.4	9.6
	09°56'	73	4.3	10.7
	19°20'	80	8.7	6.3
	17°15'	118	7.5	7.5
	57°15'	182	6.9	8.1
	78°13'	219	7.1	7.9
	28°17'	193	7.1	7.9
	14°22'	168	8.6	6.4
	01°25'	155	8.1	6.9
	359°25'	155	7.0	11.0
	336°08'	158	4.6	10.4
	333°50'	159	9.8	5.2
	331°50'	161	9.6	5.4
	327°05'	166	8.9	6.1
	320°02'	173	8.8	6.2

STA	AZIM	H.I. = 15.05 DIST	ROD	ELEV
10+00N				
	320°	175	11.6	3.4
	317°02'	181	11.8	3.2
	315°35'	185	11.0	4.0
	315°	186	9.5	5.5
	311°20'	195	9.2	5.8
	309°20'	202	6.4	8.6
	308°26'	205	5.1	9.9
	301°15'	230	5.4	9.6
	293°37'	262	4.9	10.1
	288°05'	297	4.4	10.6
	300°35'	355	4.3	10.7
	304°40'	330	4.2	10.8
	309°40'	307	4.3	10.7
	308°45'	278	4.6	10.4
	319°35'	275	7.3	7.7
	321°	272	8.7	6.3
	325°10'	268	9.7	5.3
	325°45'	267	12.3	2.7
	327°35'	263	11.8	3.2

	H.I. = 15.05		12-18-47	
STA ↑ 10+00N	AZIM	DIST	ROD	ELEV
	328°10	261	9.6	5.4
	329°55'	258	9.0	6.0
	337°15'	248	9.2	5.8
	339°30'	243	9.6	10.4
	348°30'	237	9.8	10.2
	00°15'	228	9.2	10.8
	02°15'	230	8.2	6.8
	14°55'	292	8.7	6.3
	31°50'	280	6.6	8.4
	29°45'	332	7.2	7.8
	15°10'	365	7.7	7.3
	67°02'	295	7.6	7.4
	06°18'	295	3.8	11.2
	353°27'	297	3.8	11.2
	340°53'	300	3.9	11.1
	340°13'	302	7.3	7.7
	338°30'	305	9.2	5.9
	335°45'	310	9.3	5.7
	335°15'	313	11.1	3.9

	H.I. = 15.05		12-18-47	
STA ↑ 10+00N	AZIM	DIST	ROD	ELEV
	333°55'	315	11.9	3.6
	330°55'	325	10.9	4.6
	330°36'	326	9.5	5.5
	327°18'	330	7.9	7.1
	329°57'	332	7.2	7.8
	323°40'	335	5.6	9.9
	317°45'	352	9.5	10.5
	311°30'	379	3.9	11.1
	305°46'	400	3.7	11.3
	313°15'	465	3.2	11.8
	316°45'	450	3.3	11.7
	321°50'	425	3.7	11.3
	323°45'	415	5.7	9.3
	327°26'	398	7.8	7.2
	332°	385	8.7	6.3
	336°12'	372	9.9	5.6
	336°50'	372	11.0	4.0
	337°50'	371	11.6	3.4
	339°57'	362	10.6	4.4

H.I. = 15.05

12-18-47

STA T 10+00N	AZIM	DIST	ROD	ELEV
	340°22'	360	6.7	8.8
	345°36'	353	3.5	11.5
	355°45'	348	3.8	11.2
	08°47'	365	4.3	10.7
	09°50'	330	3.8	11.2
	10°15'	323	7.4	7.6
	17°32'	370	7.2	7.8
	16°50'	380	4.5	10.5
	14°45'	415	4.0	11.0
	14°45'	420	0.9	14.1
	04°22'	380	3.8	11.2
	04°22'	390	0.1	14.9
	346°18'	363	2.7	12.3
	346°18'	367	40.3	15.3
	342°41'	368	0.3	14.7
	341°18'	369	5.9	9.1

12-18-47

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T.B.M. #3 E.L. 13.23 + 4.53 = 17.76 H.I.

STA T 15+00N	AZIM	DIST	ROD	ELEV	OBJECT
	165°00'00"				106+00W
	245°50'	225	5.3	12.5	
	249°56'	192	5.5	12.3	
	242°10'	152	6.4	11.4	
	243°48'	142	8.1	9.7	
	243°07'	130	10.1	7.7	
	237°15'	96	10.8	7.0	
	223°07'	80	11.8	6.0	
	228°50'	76	13.9	3.9	
	227°45'	70	12.5	5.3	
	224°26'	55	11.6	6.2	
	204°15'	35	9.2	8.6	
	261°	29	5.1	12.7	
	113°45'	57	4.9	12.9	
	100°25'	148	5.3	12.5	
	112°10'	178	5.1	12.4	
	114°	184	3.1	14.7	
	132°20'	137	3.4	14.4	

H.I. = 17.76
12-18-97

STA T Δ 15+00 N	AZIM	DIST	ROD	ELEV
	130°30'	132	5.6	12.2
	168°	108	5.5	12.3
	169°22'	115	2.2	15.6
	82°45'	152	5.3	12.5
	76°30'	63	5.1	12.7
	00	00	5.0	12.7
	261°	22	5.2	12.6
	261°40'	35	11.6	6.2
	261°15'	43	11.8	6.0
	261°	61	11.3	6.5
	260°45'	64	12.2	5.6
	260°20'	70	12.1	5.4
	260°	72	13.3	4.5
	260°	75	11.1	6.7
	259°	106	10.8	7.0
	259°	137	9.5	8.3
	258°45'	142	6.9	10.9
	259°	147	5.6	12.2
	259°	195	5.2	12.6

H.I. = 17.76
12-18-97

STA T Δ 15+00 N	AZIM	DIST	ROD	ELEV
	259°	248	4.9	12.9
	274°35'	275	4.9	13.4
	277°	245	4.6	13.2
	282°45'	200	4.7	13.1
	283°30'	190	5.8	12.0
	283°40'	182	8.0	9.8
	289°	162	10.2	7.6
	297°55'	135	11.4	6.4
	303°16'	121	11.9	5.9
	306°50'	110	12.1	5.7
	312°50'	108	10.9	6.9
	319°10'	103	11.6	6.2
	324°30'	97	7.8	10.0
	330°15'	93	6.9	10.9
	332°45'	92	5.0	12.8
	15°	103	5.2	12.6
	40°10'	159	5.0	12.8
	25°40'	208	5.6	12.2
	03°10'	176	4.9	12.9

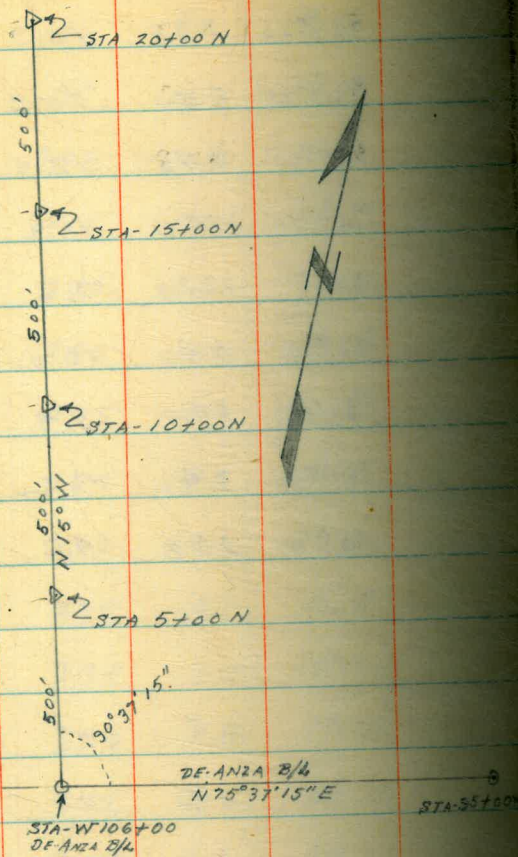
STA T 15+00X ^A	H.I. = 17.76	12-18-47	AZIM	DIST	ROD	ELEV
			334°40'	180	4.6	13.2
			333°30'	182	6.1	11.4
			330°13'	185	8.7	9.1
			329°15'	195	10.4	7.4
			321°42'	206	10.4	7.4
			316°50'	215	10.8	7.0
			310°50'	205	10.8	7.0
			297°55'	240	9.3	8.5
			296°45'	255	8.3	9.5
			295°35'	264	5.7	12.1
			295°30'	267	4.6	13.2
			290°23'	295	4.1	13.7
			287°15'	340	3.7	14.1
			297°20'	390	3.8	14.0
			299°25'	375	3.6	14.2
			303°05'	355	3.7	14.1
			303°40'	350	5.2	12.5
			306°05'	342	8.7	9.1
			309°10'	325	8.4	9.4

STA T 15+00N	H.I. = 17.76	12-18-47	AZIM	DIST	ROD	ELEV
			311°	315	10.5	7.3
			316°30'	295	10.6	7.2
			320°22'	288	10.9	6.9
			323°25'	280	10.0	7.8
			329°40'	275	12.4	5.4
			325°40'	270	11.9	5.9
			326°	270	9.6	8.2
			339°05'	250	10.0	7.8
			338°55'	250	5.4	12.4
			357°50'	242	4.2	13.6
			05°55'	258	4.3	13.5

LOCATION OF
CONTROL POINTS FOR TOPOGRAPHY OF

ROSE CREEK

BARRISAN
SHERIDY
STANLEY 12-19-97



BENCH LEVELS FOR TOPOGRAPHY OF

ROSE CREEK

BARRISAN
SHERIDY
STANLEY 12-19-97

(44)

Indexed

STA	+	H.I.	-	ELEV	
T.B.M.					TOP HUB W106+00
W106+00	6.23	14.05		7.82	DE ANZA B/L
T.B.M.					20' N/OF
# 1	5.35	15.13	4.27	9.78	45+00 N
T.B.M.					20' N/OF
# 2	7.99	17.97	5.15	9.98	410+00 N
T.B.M.					20' N/OF
# 3	5.29	18.52	4.74	13.23	415+00 N
T.B.M.					20' N/OF
# 4			3.49	15.03	420+00 N

2-6-48

2-6-48

④

PX
0+00 W-105+00

W. 105+00 Cont.

Induced

DIST.	+	HI	-	ELEV.
W-105+00	4.65	12.83		8.18
0+00			5.0	7.8
0+45			5.1	7.7
1+30			4.9	7.9
2+30			4.1	8.7
3+45			4.2	8.6
4+35			4.4	8.4
4+45			3.5	9.3
5+25			3.4	9.4
5+40			5.3	7.5
5+75			5.1	7.7
5+80			3.4	9.4
6+48			3.3	9.5
6+80			4.9	7.9
7+10			4.1	8.7
7+75			3.5	9.3
8+90			2.9	9.9
8+95			5.0	7.8

STA
W103+00

DIST.	+	HI	-	ELEV.
		12.83		
9+80			4.7	8.1
10+75			4.1	8.7
11+80			4.3	8.5
12+90			3.9	8.9
13+60			3.5	9.3
14+10			1.4	11.4
14+20			0.3	12.5

2-6-48

STA. W 104+00

2-6-48

(46)

0+00	STA. W 104+00			
DIST.	+	HI	-	ELEV
	4.40	12.58		8.18 ^{STA. W 103+00}
14+30			3.1	9.4
13+20			3.4	9.1
12+30			3.6	8.9
11+40			4.0	8.5
10+30			4.3	8.2
9+40			4.9	7.6
9+00			3.1	9.4
8+60			3.9	8.6
8+25			3.1	9.4
7+25			3.1	9.4
6+35			3.8	8.7
5+45			5.1	7.4
4+90			3.9	8.6
4+05			3.6	8.9
3+35			3.6	8.9
2+50			4.1	8.4

DIST.	+	HI	-	ELEV.
		12.58		7.2

1+85			4.5	8.0
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1+00			4.7	7.8
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0+00			7.7	7.4
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2-6-48

0+00 = W 103+00

DIST	+	H.I.	-	ELEV	STA
	5.29	13.12		7.83	W102+00
0+00			5.1	8.0	
0+65			5.2	7.9	
1+30			5.1	8.0	
2+10			4.9	8.2	
3+00			4.0	9.1	
4+05			5.4	7.7	
4+15			4.5	8.6	
4+45			5.6	7.5	
5+50			4.1	9.0	
6+30			4.7	8.4	
6+40			4.2	8.9	
7+30			3.9	9.2	
8+45			3.6	9.5	
9+00			4.2	8.9	
10+20			3.3	9.8	
11+00			3.2	9.9	
11+80			3.5	9.6	

W 103+00 Cont.

2-6-48

(47)

DIST	+	HI	-	ELEV
		13.12		
12+70			2.2	10.9
13+30			2.1	11.0
13+70			2.2	10.9
14+10				EDGE RR GRADE

0+00 = W 102+00

2-6-48

DIST.	+	H.I.	-	ELEV	STA.
	4.95	13.21	5.4	8.26	W101+00
14+15			+0.4	13.6	
13+70			0.4	12.8	
13+60			1.7	11.5	
12+70			2.5	10.7	
11+50			3.0	10.2	
10+55			5.1	8.1	
9+60			4.6	8.6	
9+00			4.4	8.8	
8+10			3.7	9.5	
7+15			4.8	8.4	
5+75			4.7	8.5	
4+40			5.7	7.5	
3+15			5.7	7.5	
2+05			5.1	8.1	
1+05			5.0	8.2	
0+00			5.4	7.8	

0+00 = W 101+00

2-6-48

(48)

DIST.	+	H.I.	-	ELEV.	STA.
	6.68	13.48		6.80	W-100+00
0+00				5.3	8.7 ²
0+50				5.8	7.6 ⁷
1+30				5.5	8.0 7.9
2+25				6.2	7.3 7.2
2+85				6.2	7.2 ³
4+30				6.1	7.3 ⁴
5+15				5.3	8.1 ²
6+30				4.9	8.5 ⁶
7+50				5.1	8.3 ⁴
8+95				5.5	8.0
9+75				3.8	9.7
10+60				4.0	9.5
11+35				3.4	10.1
12+35				2.8	10.7
13+60				1.9	11.6
13+70			+0.2		13.7

STA 2-6-48
0+00 = W100+00

DIST.	+	H.I.	-	ELEV.	STA.
	4.20	12.16		7.96	W99+00
					S EDGE RR GRADE
13+65					
13+55			+0.1	12.3	
13+50			1.4	10.8	
12+30			2.0	10.2	
11+25			2.0	10.2	
10+15			2.7	9.5	
9+05			4.0	8.2	
7+95			4.2	8.0	
6+60			4.0	8.2	
5+40			4.2	8.0	
4+25			4.5	7.7	
3+25			4.5	7.7	
2+40			4.2	8.0	
1+30			4.6	7.6	
0+00			5.4	6.8	

STA. 2-6-48 (49)
0+00 = W99+00

DIST.	+	H.I.	-	ELEV.	STA.
	5.58	13.25		7.67	W98+00
0+00				5.4	7.8
0+50				5.3	7.9
1+05				5.6	7.6
2+05				5.0	8.2
3+00				5.3	7.9
4+35				5.5	7.7
5+40				5.7	7.5
6+40				5.4	7.8
7+60				5.2	8.0
8+30				5.1	8.1
9+50				3.9	9.3
10+35				3.4	9.8
11+55				3.4	9.8
12+45				3.0	10.2
13+20				2.5	10.7
13+30				0.6	12.6

2-6-48

0+00 = STA. W 98+00

DIST.	+	H.I.	-	ELEV
0	5.16	12.90		7.74
				STA W. 97+00
13+10			0.2	12.7
13+00			2.2	10.7
12+00			2.9	10.0
10+75			3.0	9.9
9+50			3.4	9.5
8+45			4.6	8.3
7+10			5.4	7.5
6+05			5.5	7.4
4+60			5.6	7.3
3+55			5.3	7.6
2+40			5.2	7.7
1+55			5.2	7.7
0+70			5.0	7.9
0+00			5.3	7.6

2-6-48 (50)

0+00 = STA. W 97+00

DIST	+	H.I	-	ELEV
	5.16	13.03		7.87
				STA W 96+00
0+00			5.4	7.6
0+60			5.4	7.6
1+50			5.6	7.4
2+30			5.9	7.1
3+30			5.6	7.4
4+55			5.6	7.4
5+80			5.2	7.8
6+65			5.2	7.8
8+00			4.8	8.2
9+15			3.7	9.3
10+50			3.7	9.3
11+75			3.6	9.4
12+70			2.1	10.9
12+82			Top RR GRADE	14.0

2-6-48

PX 0+00 = STA. W 96+00

DIST.	+	H.I.	-	ELEV.	STA
	5.00	12.93		7.93	95+00
12+50			Top RR GRADE		
12+35			1.9	11.0	
11+50			3.3	9.6	
10+75			3.6	9.3	
9+85			4.1	8.8	
8+80			4.2	8.7	
7+85			5.1	7.8	
6+75			5.3	7.6	
5+80			5.6	7.3	
4+65			5.7	7.2	
3+45			5.6	7.3	
2+50			5.8	7.1	
1+30			5.5	7.4	
0+00			5.1	7.8	

2-6-48 (51)

PX 0+00 = STA. W 95+00

DIST.	+	H.I.	-	ELEV.	STA
	5.39	13.26		7.87	96+00
0+00			5.4	7.9	
0+80			5.8	7.5	
1+95			6.2	7.1	
3+25			6.2	7.1	
4+55			6.1	7.2	
5+95			6.0	7.3	
7+50			5.5	7.8	
8+85			5.2	8.1	
10+20			4.8	8.5	
11+05			4.1	9.2	
11+85			2.7	10.6	
12+00			0.0	13.3	
12+10			Top RR GRADE		

PX 0+00 = STA W. 94+00

DIST.	+	HI	-	ELEV.	STA
	4.78	12.71		7.93	W 95+00
			TOP R.R. GRADE		
11+55					
11+40			0.0	12.7	
11+30			2.6	10.1	
10+50			3.3	9.4	
9+25			4.2	8.5	
8+20			5.1	7.6	
7+25			5.3	7.4	
6+15			5.5	7.2	
5+00			5.7	7.0	
4+00			5.8	6.9	
2+85			5.8	—	
1+40			5.8	—	
0+00			5.3	7.4	

PX

Sta - 119+00

DIST	+	HI	-	Elev	T.B.M.
	3.38	12.18		8.80	Sta. 120+00
			5.2	7.0	
			5.1	7.1	
			4.8	7.4	
			4.5	7.7	
			4.3	7.9	
			3.7	8.5	
			3.7	—	
			2.8	9.4	
			2.1	10.1	
			1.0	11.2	

2-10-48

PX

Sta 118+00

Dist	+	H.I.	-	Elev	T.B.M. Sta 117+00
	4.51	12.41		7.90	
8+45			1.8	10.6	
6+80			2.2	10.2	
6+30			2.5	9.9	
5+75			2.8	9.6	
5+05			3.6	8.8	
4+55			3.9	8.5	
3+85			4.3	8.1	
3+70			4.6	7.8	
2+25			5.0	7.4	
1+70			4.9	7.5	
0+75			5.0	7.4	
0+00			5.2	7.2	

2-10-48

(53)

PX

Sta. 117+00

Dist	+	H.I.	-	Elev.	T.B.M. Sta. 118+00
	4.80	12.56 ⁶		7.76	
8+00			5.3	7.3	
6+95			5.0	7.6	
4+85			5.0	—	
2+70			4.7	7.9	
3+95			4.1	8.5	
5+30			3.6	9.0	
5+40			2.0	10.6	
5+45			3.9	8.7	
5+60			2.7	9.9	
5+70			3.4	9.2	
6+70			3.2	9.4	
7+60			3.3	9.3	
8+50			3.0	9.6	
9+45			2.6	10.0	
10+80			1.5	11.1	
11+55			1.0	11.6	

PX

Sta. 116+00

Dist	+	HI	-	Elev	T.B.M.
T.B.M.	4.52	12.62		8.10	15' South STA 116+00
12+55			0.8	11.8	
11+15			2.0	10.6	
10+00			2.1	10.5	
9+90			3.4	9.2	
9+80			2.6	10.0	
8+55			3.3	9.3	
7+40			3.9	8.7	
6+15			4.3	8.3	
5+15			3.5	9.1	
5+00			4.3	8.3	
4+85			4.0	8.6	
3+75			4.3	8.3	
2+55			4.7	7.9	
1+65			4.8	7.8	
0+55			5.1	7.5	
0+00			5.2	7.4	

PX

STA 115+00

Dist	+	HI	-	ELEV	T.B.M.
	4.21	12.81		8.10	7. B.M. 15' So. of Sta. 116+00
0+00			5.3	7.5	
0+50			4.7	8.1	
2+10			5.2	7.6	
3+35			5.0	7.8	
4+45			4.8	8.0	
5+55			4.7	8.1	
6+50			4.5	8.3	
8+45			2.1	10.7	
8+60			4.1	8.7	
8+70			2.7	10.1	
9+95			2.2	10.6	
11+50			1.3	11.5	
12+85			0.8	12.0	

2-10-48

PK

Sta. 114+00

Dist	+	HI	-	Elev
	4.50	13.21		8.71
14+60			0.4	12.8
13+80			1.3	11.9
12+90			1.6	11.6
11+70			2.6	10.6
10+75			2.5	10.7
9+90			3.0	10.2
8+90			3.7	9.5
7+85			4.0	9.2
7+30			4.0	—
7+15			4.9	8.3
7+05			3.7	9.5
6+60			4.6	8.6
5+90			4.9	8.3
5+15			5.1	8.1
4+15			5.2	8.0

2-10-48

(55)

Sta 114+00 Cont. PK

Dist	+	HI	-	Elev
3+50		13.21	5.1	8.1
2+75			5.2	8.0
1+90			5.0	8.2
1+70			5.0	—
0+80			5.6	7.6
0+00			5.4	7.8

2-10-48

PX

Sta 113+00

Dist	+	H.I.	-	Elev	T.B.M. Sta 113
	4.78	13.70		8.92	
0+00			5.3	8.4	11150
0+95			5.4	8.3	11140
2+30			5.2	8.5	11205
3+55			5.0	8.7	11125
4+45			5.1	8.6	10+25
5+65			5.6	8.1	9+50
6+90			5.2	8.5	8+50
8+25			5.0	8.7	7+50
9+30			4.3	9.4	6+50
9+85			5.0	8.7	5+25
10+20			3.6	10.1	4+20
11+25			3.5	10.2	3+15
12+30			3.3	10.4	2+15
13+30			3.4	10.3	1+05
14+50			1.4	12.3	0+00

2-10-48

(56)

PX

STA 112+00

Dist	+	H.I.	-	ELEV	T.B.M. STA. 111+00
	4.95	13.74		8.79	
			2.0	11.7	
			2.7	11.0	
			3.6	10.1	
			3.9	9.8	
			4.7	9.0	
			4.2	9.5	
			4.4	9.3	
			4.4	—	
			4.4	—	
			4.5	9.2	
			4.8	8.9	
			4.7	9.0	
			5.0	8.7	
			5.5	8.2	
			5.3	8.4	

2-10-48

PX Sta. 111+00

Dist.	+	H.I.	-	Elev.	TBM
	4.60	13.52		8.92	Sta. 111
0+00			5.3	8.2	
0+70			4.7	8.8	
1+65			4.6	8.9	
2+60			4.5	9.0	
3+45			4.4	9.1	
4+45			4.3	9.2	
5+30			4.0	9.5	
6+30			3.8	9.7	
7+30			3.8	—	
8-25			4.1	9.4	
9+20			3.6	9.9	
10+30			3.5	10.0	
11+00			3.4	10.1	
11+90			3.4	—	
12+80			3.0	10.5	
13+60			2.1	11.4	

2-10-48

(57)

PX Sta. 110+00

Dist.	+	H.I.	-	Elev.	TBM
	4.56	13.35		8.79	Sta.
15+20			1.2	12.1	
16+10			4.2	9.1	
17+70			7.6	5.7	
18+60			9.0	4.3	
19+50			9.4	3.9	
20+40			7.2	6.1	
21+20			7.7	5.6	
22+10			9.1	4.2	
23+50			9.9	3.4	
24+60			10.9	2.4	
25+50			8.6	4.7	
26+70			8.2	5.1	
27+50			6.3	7.0	
28+15			4.0	9.3	
29+45			4.1	9.2	

PX

Sta. 110+00 Cont.

Dist	H.I.	-	Elev.
9+45	13.35	3.2	10.1
8+55		3.0	10.3
7+85		3.5	9.8
7+70		5.2	8.1
6+50		5.6	7.7
6+00		3.9	9.4
5+60		5.2	8.1
4+85		5.6	7.7
4+20		5.6	—
3+25		4.8	8.5
2+80		6.0	7.3
2+35		7.1	6.2
2+00		6.7	6.6
1+65		6.2	7.1
1+60		5.2	8.1
1+15		4.9	8.4
0+55		5.0	8.3
0+00		5.3	8.0

PX

Sta. 109+00

Dist	T	H.I.	-	Elev.	T.B.M.
	5.22	13.86		8.67	Sta. 110+00
0+00			5.2	8.7	
0+15			5.2	—	
0+60			5.4	8.5	
0+30			5.2	8.7	
0+20			5.1	8.8	
0+75			4.7	9.2	
0+25			6.4	7.5	
0+75			6.9	7.0	
0+60			6.0	7.9	
0+20			6.0	—	
0+60			7.1	6.8	
0+90			10.0	3.9	
0+35			9.2	4.7	
0+70			10.1	3.8	
0+80			8.2	5.7	
0+35			8.2	—	

PX STA 109+00 CONT.

STA 108+00 P.V.

DIST	+	H.I.	-	ELEV
	5.22	13.26		8.64

T.B.M. STA 109+00

DIST	+	H.I.	-	ELEV
	4.95	13.37	8.42	

T.B.M. 910.1

8+40			10.7	3.2
8+50			9.4	4.5
9+15			8.5	5.4
9+20			11.1	2.8
9+45			10.8	3.1
9+48			9.1	4.8
10+65			8.5	5.4
11+15			4.4	9.5
12+25			3.0	10.9
12+50			5.0	8.9
12+70			4.2	9.7
13+40			2.9	11.0
13+70			2.3	11.6
14+10			0.3	13.6
14+20			+1.2	15.1

14+00			+1.0	14.4
13+96			0.8	12.6
13+90			2.3	11.1
13+40			2.4	11.0
13+20			6.0	7.4
12+80			7.0	6.4
12+10			7.0	—
9+00			6.6	6.8
8+90			3.1	10.3
8+10			3.5	9.9
7+65			3.7	9.7
7+50			4.7	8.7
7+40			3.9	9.5
6+70			3.5	9.9
6+20			3.4	10.0
5+95			6.1	7.3

2-10-48

PX

STA 108+00 CONT.

Dist	+	H.I.	-	ELEV.
		13.37 ⁴		
5+75			7.6	5.8
5+65			10.2	3.2
4+25			9.6	3.8
3+25			9.1	4.3
2+50			9.8	3.6
2+45			5.7	7.7
1+45			4.6	8.8
0+85			5.4	8.0
0+00			5.3	8.1
T.P.			8.32	

2-10-48

60

PX

STA 107+00

Dist	+	H.I.	-	Elev	T.P.
				5.05 ⁵	
4.41		9.46 ⁵			
5+00			5.2	4.3	
4+75			5.0	4.5	
4+65			4.7	4.8	
4+05			4.4	5.1	
3+60			2.0	7.5	
2+80			1.1	8.4	
3+00			0.5	9.0	
T.P.			0.60	8.86	
5.30		19.16 ²			
3+10					
3+85			4.6	9.6	
3+80			4.7	9.5	
3+00			4.7	—	
5+80					
5+90			6.7	7.5	
6+00			5.0	9.0	

PX Sta 107+00 Cont.

Dist	+ HI	- Elev
300 6+35	14.16 ²	4.6 9.6
300 6+50		6.9 7.3
310 6+75		4.7 9.5
300 7+05		4.4 9.8
300 8+55		3.3 10.9
300 8+65		7.6 6.6
300 10+05		6.9 7.3
300 10+10		3.1 11.1
300 10+20		2.9 11.3
300 10+30		6.6 7.6
300 11+85		6.6 —
300 12+75		5.8 8.4
300 13+30		6.2 8.0
300 13+70		3.9 10.3
310 14+00		3.1 11.1
14+20		0.0 14.2

PX

Dist	+ HI	- Elev	TRX
580	13.62	7.82	Sta. 105+00
14+20		+ 0.1 13.7	
14+00		2.2 11.4	
13+50		4.5 9.1	
12+10		5.1 8.5	
12+00		3.7 9.9	
10+50		5.2 8.4	
10+30		3.7 9.9	
10+00		5.2 8.4	
9+80		7.8 5.8	
9+60		6.7 6.9	
8+90		7.6 6.0	
8+85		4.0 9.6	
8+00		4.5 9.1	
7+80		3.7 9.9	
6+00		4.5 9.2	
5+85		7.0 6.6	

Sta 106+00 Cont.

Dist + H.I. - Elev

PX

13.62

5+65

4.5 9.1

5+00

4.3 9.3

4+25

4.3 —

3+65

4.6 9.0

3+35

3.5 10.1

3+05

5.2 8.4

2+75

4.6 9.0

2+20

5.0 8.6

1+25

5.4 8.2

0+80

5.2 8.4

0+00

5.4 8.2

61

ORIGINAL

BARRAGAN
SHERRY
STANLEY
3-5-78
CLEAR
CALM
WARM

SOUNDINGS OF APPROACH CHANNEL SECT. "B"

PROJ - #3-1

STA - (-2+00)

0+00 = STA (-2+00) SECT. "B" Bk. SOUND EAST AT 90° TO Bk.

DIST	SOUND		DIST	SOUND	
0+00	1.4	+2.2	1+70	1.5	+2.1
+10	1.4	—	09:20	1.8	+1.8
09:18	1.4	—	(3.6)	2.1	+1.5
(3.6)	1.3	+2.3	2+00	2.5	+1.1
	1.4	+2.2		5.5	-1.9
50	1.3	+2.3		7.1	-3.5
	1.3	—		8.0	-4.4
	1.3	—		8.0	—
	1.3	—	50	8.5	-4.9
	1.3	—		9.1	-5.5
1+00	1.3	—		9.5	-5.9
	1.3	—		9.2	-5.6
	1.4	+2.2		9.1	-5.5
	1.4	—	3+00	8.0	-4.4
	1.4	—		7.2	-3.6
50	1.4	—		6.5	-2.9
1+60	1.4	—	3+30	6.0	-2.4

STA - (-2+00) 3-5-78

DIST SOUND

DIST SOUND

3+40 5.3 -1.7

50 5.0 -1.4

5.0 —

(3.6) 5.5 -1.9

6.2 -2.6

7.6 -4.0

4+00 9.0 -5.4

9.6 -6.0

10.1 -6.5

10.6 -7.0

11.2 -7.6

50 11.5 -7.9

11.5 —

11.5 —

11.8 -8.2

12.3 -8.7

5+00 12.5 -8.9

09:25

(62)

PX Indexed

3-5-18

STA-(-3700)

(63)

STA-(-3700)

DIST SOUND

DIST SOUND

0700 = STA-(-3700) SECT. "B" 8/4: SOUND EAST AT 9° 7.2'

3760 12.0 -8.6

DIST SOUND DIST SOUND

13.1 -9.7

0700 1.7 +1.7 1780 1.6 +1.8

(37) 13.2 -9.8

+10 1.5 +1.9 (37) 2.4 +1.0

13.5 -10.1

09:37

1.5 — 2700 2.9 +0.5

7700 13.9 -10.5

(37)

1.5 — 09:40 6.0 -2.6

13:43 14.0 -10.6

1.4 +2.0 — 7.0 -3.6

14.0 —

50 1.4 — — 7.9 -4.5

14.1 -10.7

1.3 +2.1 — 8.4 -5.0

14.1 —

1.2 +2.2 50 8.8 -5.4

50 13.8 -10.4

1.2 — — 8.9 -5.5

1.2 — — 8.9 —

1400 1.2 — — 8.8 -5.4

1.2 — — 8.7 -5.3

1.2 — 3700 8.0 -4.6

1.2 — — 8.5 -5.1

1.3 +2.1 — 10.5 -7.1

50 1.2 +2.2 — 11.0 -7.6

1.3 +2.1 — 11.4 -8.0

1770 1.5 +1.9 3750 11.4 —

3-5-18

STA-(-4+00)

0+00 = STA-(-4+00) SECT "B" B/L: SOUND EAST AT 90° 7.2/4

DIST	SOUND	DIST	SOUND
0+00	1.0	+2.2	1+90 6.0 -2.8
+10	1.1	+2.1	2+00 6.8 -3.6
09:50	1.1	—	2.8 -4.6
(3.2)	1.1	—	(3.2) 9.3 -6.1
	1.2	+2.0	11.5 -8.3
50	1.2	—	12.9 -9.7
	1.1	+2.1	50 15.0 -11.8
	1.0	+2.2	16.0 -12.8
	1.0	—	16.2 -13.0
	1.1	+2.1	16.4 -13.2
1+00	1.1	—	16.7 -13.5
	1.1	—	3+00 16.4 -13.2
	1.1	—	16.1 -12.9
	1.1	—	16.2 -13.0
	1.2	+2.0	16.0 -12.8
50	1.4	+1.8	16.0 —
	1.7	+1.5	50 16.5 -13.3
09:53	1.5	+1.7	16.5 —
1+80	1.4	-1.2	3+70 16.5 —

3-5-18

STA-(-4+00)

(69)

DIST	SOUND	DIST	SOUND
3+80	16.6	-13.4	
	16.6	—	
4+00	16.2	-13.0	
	16.0	-12.8	
(3.2)	15.0	-11.8	
	14.5	-11.3	
	14.2	-11.0	
50	14.0	-10.8	

09:55

STA. (-5+00)

3-5-18

3-5-18

0+00 = STA. (-5+00) SECT "B" 3/4. SOUND EAST 90° T.B. END SECTION 150' EAST STA. (-4+00)

DIST SOUND DIST SOUND

0+00 0.7 +2.3

+10 0.7 —

10:10
10:08

0.7 —

(3.0) 0.7 —

0.7 —

50 0.7 —

0.7 —

0.7 —

0.7 —

1.2 +1.8

1+00 1.5 +1.5

2.0 +1.0

2.4 +0.6

PT. 150' EAST STA. (-4+00): SOUND SOUTH AT 90°

DIST SOUND DIST SOUND

0+10 1.0 +1.8 1+00 18.1 -15.3

+20 1.0 — 2+00 17.5 -14.7

10:20

1.1 +1.7

(2.8) 1.5 +1.3 (2.8)

50 1.5 —

2.0 +0.8

2.8 0.0

5.5 -2.7

10.1 -7.3

1+00 14.0 -11.2

17.2 -14.4

17.0 -14.2

16.0 -13.2

16.0 —

50 16.7 -13.9

16.7 —

17.0 -14.2

1+80 18.0 -15.2

(65)

3-5-48

END SECTION

3-5-48

(66)

END SECT. 250' EAST OF STA. (-1+00)

DIST

SOUND

DIST

SOUND

0+00 = Pt. 250' EAST STA. (-1+00) SECT. B/K. SOUND SOUTH

3+60

17.0

-14.4

DIST SOUND

DIST SOUND

17.2 -14.6

0+00 7.5 -4.9

1+80 7.6 -5.0

(2.6)

17.6 -15.0

+10 7.6 -5.0

7.8 -5.2

17.8 -15.2

10:35 7.5 -4.9

2+00 7.8

4+00

18.0 -15.4

(2.6) 7.5

7.8

10:46

7.5

(2.6) 8.0 -5.4

50 7.5

8.0

7.5

8.0

7.9 -4.8

50 8.0

7.9

8.0

7.9

8.9 -5.8

1+00 7.9

9.1 -6.5

7.9

11.0 -8.4

7.7 -5.1 3+00 13.0 -10.4

7.9 -5.3 19.9 -11.8

8.0 -5.4 15.2 -12.6

50 8.0 16.0 -13.4

8.0 16.4 -13.8

1+20 7.7 -5.1 3+50 16.7 -14.1

SOUNDINGS APPROACH CHANNEL SECT. "A" PROJ-3-1

PX STA- 1+00

0+00 = STA- 1+00 SECT. "A" B/L: SOUND SOUTH AT 90° T. B/L

DIST	SOUND		DIST	SOUND
0+00	4.0	-2.8	1+70	11.5 -10.3
+10	2.9	-1.7		12.5 -11.3
12:45	4.8	-3.6	(1.2)	12.6 -11.4
(1.2)	4.7	-3.5	2+00	12.0 -10.8
	4.0	-2.8		11.4 -10.2
50	2.5	-1.3		11.6 -10.4
	4.5	-3.3		11.4 -10.2
	4.2	-3.0		10.1 -9.2
	5.0	-3.8	50	10.2 -9.0
	4.8	-3.6		11.0 -9.8
1+00	5.5	-4.3		11.0 —
	10.2	-9.0		10.3 -9.1
	12.7	-11.5		9.7 -8.5
	12.5	-11.3	3+00	9.0 -7.8
	11.0	-9.8		9.0 —
50	12.5	-11.3		7.0 -5.8
1+60	12.6	-11.4	12:50	0.9 +0.3
			3+30	0.9 +1.2
			3+75	

PX STA- 0+80

0+00 = STA- 0+80 SECT. "A" B/L: SOUND SOUTH // TO BRIDGE

DIST	SOUND		DIST	SOUND
			1+60	13.0 -12.0
+10	2.5	-1.5		13.6 -12.6
13:00	4.2	-3.2	(1.0)	14.7 -13.7
(1.0)	3.0	-2.0		15.2 -14.2
	2.7	-1.7	2+00	13.0 -12.0
50	4.0	-3.0		10.0 -9.0
	3.7	-2.7		8.5 -7.5
	4.5	-3.5		9.0 -8.0
	5.0	-4.0		12.1 -11.1
	5.7	-4.7	50	12.3 -11.3
1+00	6.5	-6.5		9.3 -8.3
	9.5	-8.5		9.9 -8.9
	13.5	-12.5		10.0 -9.0
	11.0	-10.0		10.7 -9.7
	11.0	—	3+00	9.0 -8.0
1+50	13.6	-12.6	3+10	10.3 -9.3

		0+80	
DIST	SOUND	DIST	SOUND
3+20	8.5		-7.5
	6.0		-5.0
(1.0)	6.5		-5.5
50	6.1		-5.1
<u>13.05</u>	1.6		-0.6
⁷¹⁰ 3+20	0.0		+1.0

3-5-48 (68)

RX

STA - 0+70

100-STA-0+70 SECT "A" 1/4" SOUND SOUTH // T. BRIDGE

DIST	SOUND	DIST	SOUND	DIST	SOUND
0+20	1.5	-0.6	1+80	11.0	-10.1
<u>1110</u>	2.5	-1.6		10.5	-9.6
(0.9)	2.0	-1.1	2+00	10.6	-9.7
50	2.8	-1.9	(0.9)	10.5	-9.6
	3.4	-2.5		10.0	-9.1
	3.4	—		9.8	-8.9
	3.5	-2.6		10.0	-9.1
	4.2	-3.3	50	9.0	-8.1
1+00	5.0	-4.1		8.5	-7.6
	8.5	-7.6		11.0	-10.1
	10.3	-9.4		10.8	-9.9
	11.8	-10.9		10.1	-9.2
	11.2	-10.3	3+00	10.1	—
50	10.8	-9.9		10.7	-9.8
	10.5	-9.6		10.0	-9.1
1+70	9.3	-8.4	3+30	9.5	-8.6

0+70

3-5-78

DIST SOUND

DIST SOUND

3+70 9.1 -8.2

~~50 8.5 -7.6~~

~~3.0 -2.1~~

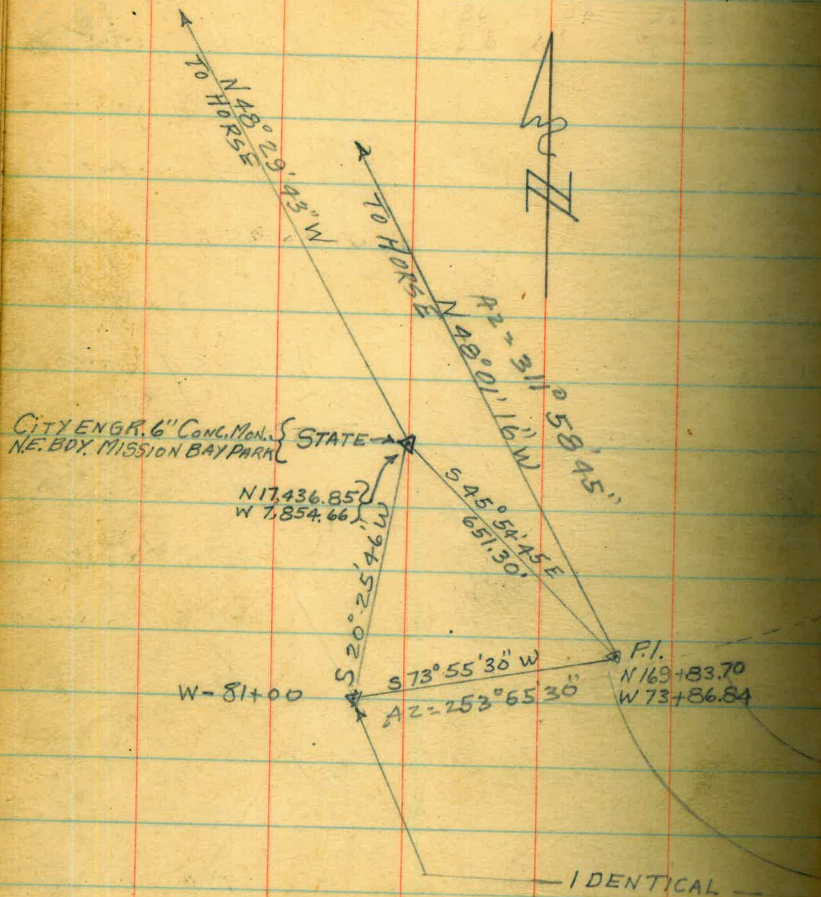
3+70 0.0 +0.9

(0.9)

(69)

DE ANZA COVE BASELINE FOR
SOUNDINGS OF DREDGED AREA
MISSION BAY PROJECT No. 3.1

S 85° 12' 44" W	S 89° 59' 60" W
N 147° 16" W	S 85° 12' 44" W
00	N 9° 42' 16" W
	S 20° 25' 46" W
	S 25° 18' 02" W

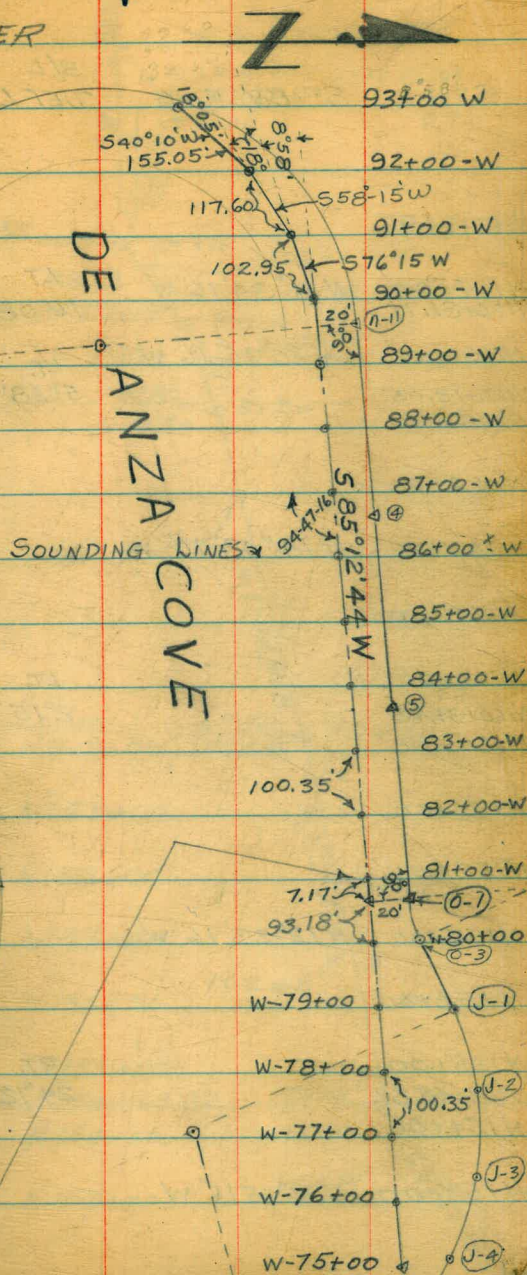


4-15-48

T.A. STAMPER

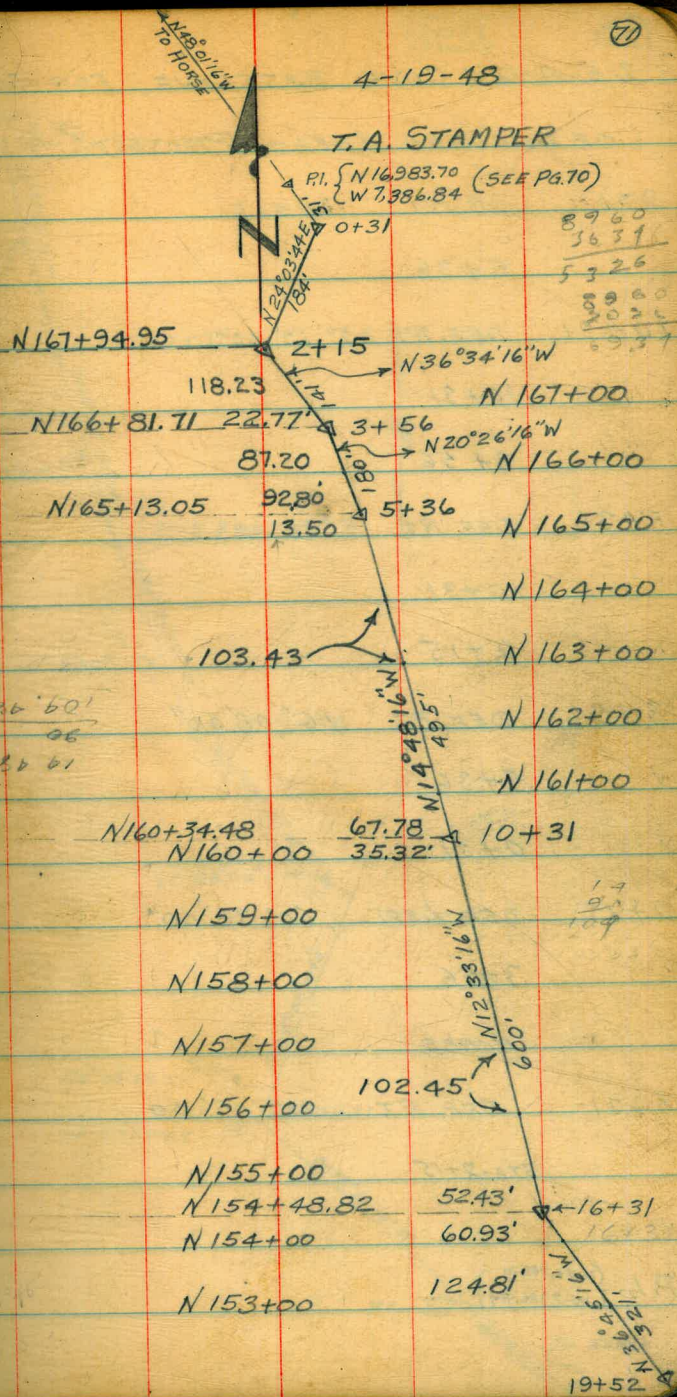
Indexed

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DE ANZA BASELINE CONTD

STA	BEARING	B/L DEFL	B/L DIST	SOUNDING ANGLE
N167+94.95				
N167+00	N36°34'16"W	LT	118.23	53°25'44"
N166+81.71		16°08'	22.77	
N166+00	N20°26'16"W	LT	87.20	69°33'44"
N165+13.05		5°38'	92.80	
N165+00			13.50	
N164+00				
N163+00	N14°48'16"W		103.43	75°11'44"
N162+00				
N161+00		LT		
N160+34.48		2°15'	67.78	
N160+00			35.32	
N159+00				
N158+00				77°26'44"
N157+00	N12°33'16"W		102.45	
N156+00				
N155+00		RT		
N154+48.82		24°12'	52.43	
N154+00			60.93	
N153+00	N36°45'16"W		124.81	53°14'44"



DE ANZA COYE BASELINE FOR SOUNDINGS

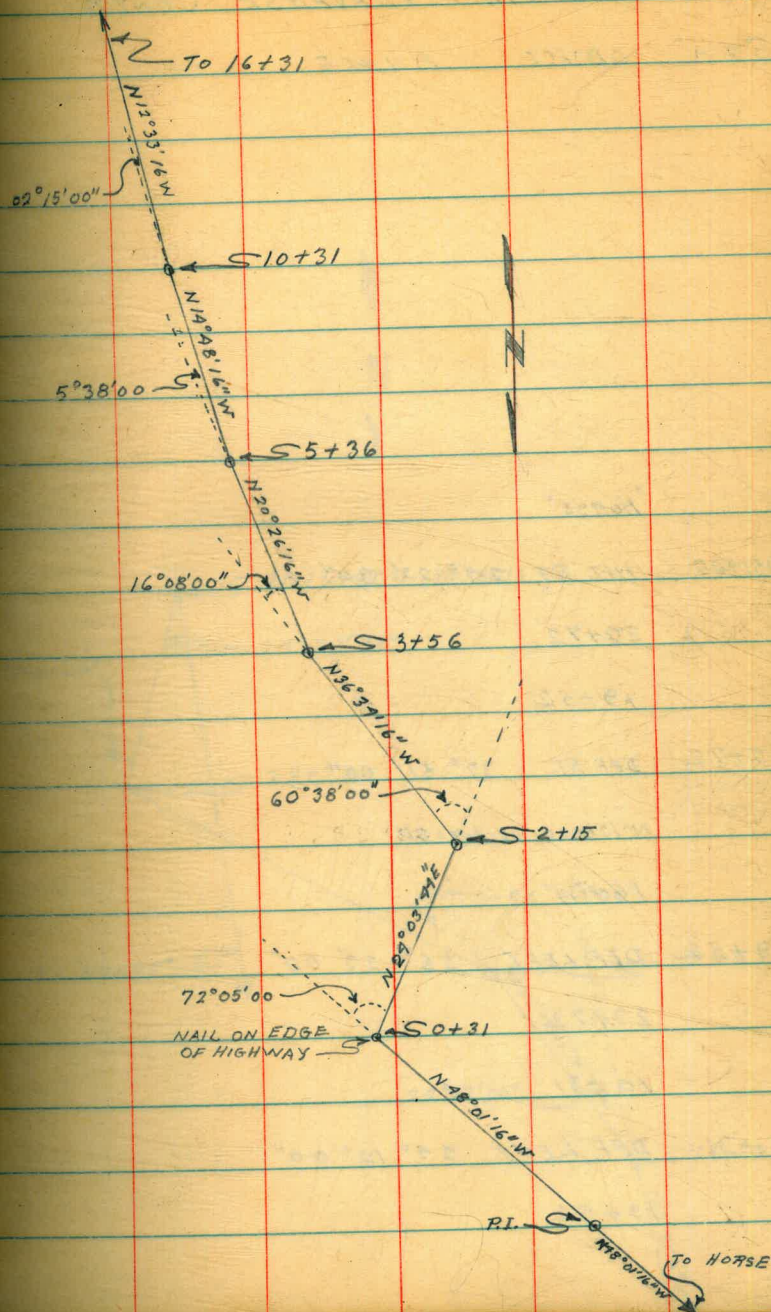
OF DREDGED AREA - PROJECT # 3-1

STA	OBJECT	ANGLE
5+36		
10+31	DEF. RT.	02° 15' 00"
16+31		
3+56		
5+36	DEF. RT.	5° 38' 00"
10+31		
2+15		
3+56	DEF. RT.	16° 08' 00"
5+36		
0+31		
2+15	DEF. LEFT.	60° 38' 00"
3+56		
	HORSE	
0+31	DEF. RT.	72° 05' 00"
	STA-2+15	

P.I. { N-16,383.70
W-7,386.84 }

BARRAGAN
SHERR'S
STANLEY

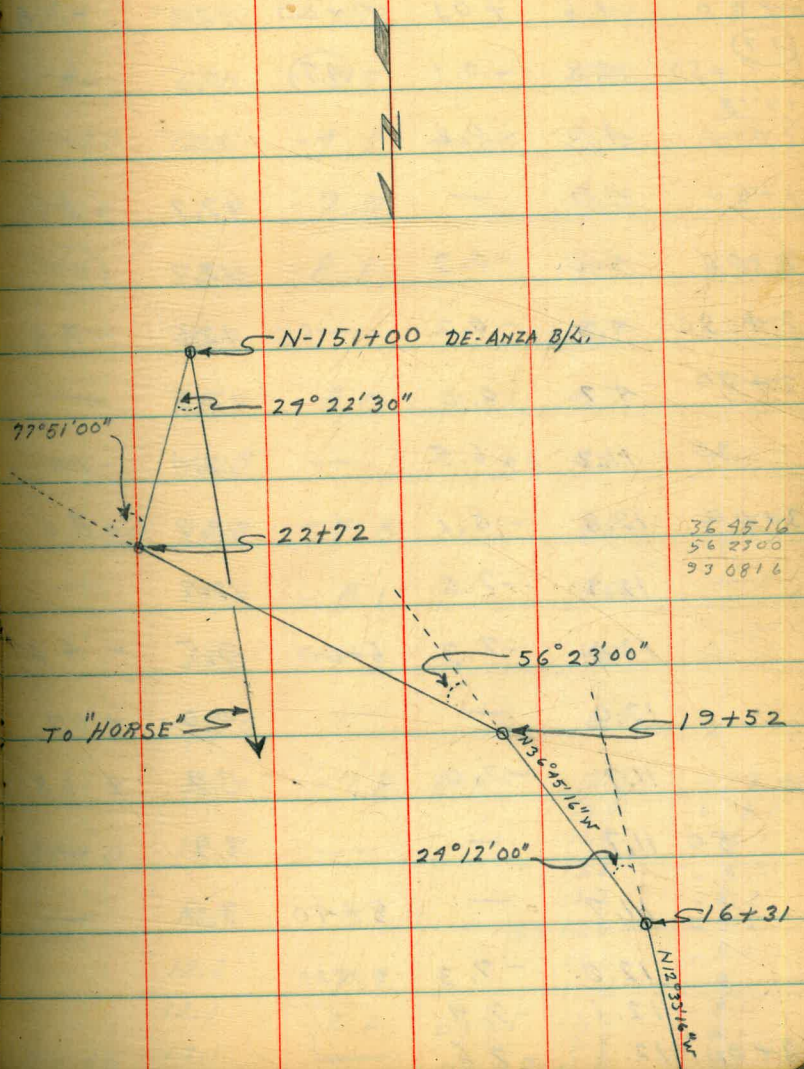
(72)



COYE BASELINE TRAVERSE CONT'D.

STA OBJECT ANGLE

STA	OBJECT	ANGLE
	"HORSE"	
N-151+00	INT. RT	29° 22' 30"
22+72		
19+52		
22+72	DEF. RT.	77° 51' 00"
N-151+00	DE-ANZA B/L	
16+31		
19+52	DEF. LEFT.	56° 23' 00"
22+72		
10+31		
16+31	DEF. LEFT.	29° 12' 00"
19+52		



P.X

FINAL

BARRAGAN
SHERTS
STANLEY'S

7-22-98

STA-61+00

7-22-98

0+00=PT. 900' N/2 STA-61+00 "D" B/L: SOUND SOUTH

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SOUNDINGS OF BORROW AREA NORTH OF STA 61+00 TO 65+00 "D" B/L

DIST SOUND

DIST SOUND

END SECTION 350' N/2 STA-60+10 "D" B/L.

0+00 4.7 -0.2 3+50 12.0 -7.1

0+00=PT. 350' N/2 STA-60+00 "D" B/L: SOUND EAST

0 +50 4.9 0.0 12.0 -

DIST SOUND DIST SOUND

1+00 5.0 -0.1 (4.9) 12.3 -7.1

0+00 4.6 +0.1 4+00 12.5 -7.8

09:35 1450 5.2 -0.3 13.0 -8.1

(4.7) +50 4.8 -0.1 (4.7) 12.5 -

1480 5.4 -0.5 12.8 -7.9

09:18
1+00 4.9 -0.2 12.5 -

90 9.5 -4.6 4+00 12.0 -7.1

1+50 4.9 - 12.7 -8.0

2+00 12.8 -7.9 10.0 -5.1

2+00 5.0 -0.3 12.7 -

(4.9) 13.0 -8.1 4.7 +0.2

2+50 4.9 -0.2 50 12.5 -7.8

13.0 - 4.7 -

2+80 4.7 0.0 12.5 -

12.9 -8.0 4.7 -

90 11.2 -6.5 12.4 -7.7

12.9 - 50 4.6 +0.3

3+00 12.8 -8.1 12.7 -8.0

50 12.7 -7.8 4.5 +0.4

12.3 -7.6 12.7 -

13.0 -8.1 4.5 -

12.0 -7.3 5+00 9.5 -4.8

13.0 - 4.5 -

12.0 - 4.0 +0.7

13.0 - 6.5 -1.6

11.7 -7.0 3.9 +0.8

12.7 -7.8 5+00 12.3 -7.4

50 11.7 - 3.9 -

13.0 -8.1 13.0 -8.1

11.7 - 5+40 3.9 -

13.2 -8.3 13.2 -8.3

12.0 -7.3 09:25

50 13.2 -8.3 13.0 -8.1

12.1 -7.4

13.0 -8.1 13.0 -8.1

3+90 12.3 -7.6

12.1 -7.2 09:42 13.0 -8.1

3+40 12.1 - 6+00 13.2 -8.3

STA-62+0.8 7-22-78

0+00=PT. 100' N/OF STA-62+00"0" B/K: SOUND SOUTH.

DIST	SOUND	DIST	SOUND	SOUTH.	SOUND
0+00	4.8	+0.2	3+40	12.8	-7.8
09:55			10:00		
0+50	5.0	0.0	50	12.8	-
1+00	5.1	-0.1		12.5	-7.5
1+40	5.2	-0.2			
1+50	13.0	-8.0		12.9	-7.4
(5.0)	13.0	-	(5.0)	12.2	-7.2
	13.0	-		12.2	-
	13.0	-	4+00	12.2	-
	12.9	-7.9		12.2	-
2+00	12.7	-7.7		12.0	-7.0
	12.5	-7.5		9.8	-4.8
	12.5	-		6.4	-1.4
	12.4	-7.4	50	5.1	-0.1
	12.4	-		4.5	-0.5
50	12.4	-		4.5	-
	12.4	-		4.5	-
	12.5	-7.5	+90	5.5	-
	12.5	-	5+00	11.1	-6.1
			10	13.7	-8.7
			20	13.5	-8.5
			30	13.2	-8.2
			40	13.2	-8.2
			50	13.0	-8.0
3+00	12.8	-7.8	60	13.0	-
	13.0	-8.0	70	13.0	-
10	13.0	-	80	13.0	-
20	13.0	-	90	13.0	-
3+30	13.0	-	6+00	13.1	-8.1

STA-63+00 7-22-78

400=PT. 100' N/OF STA-63+00"0" B/K: SOUND SOUTH

DIST	SOUND	DIST	SOUND	SOUTH	SOUND	
0+00	4.7	+0.3	2+10	13.0	-8.0	
10:11						
+10	4.7	-		13.0	-	
(5.0)	4.7	-	(5.0)	12.9	-7.9	
	4.8	+0.2		12.9	-	
	8.0	-3.0	50	12.8	-7.8	
	50	12.5	-7.5	10:15	12.8	-
	13.0	-8.0		12.8	-	
	12.3	-7.3		12.5	-7.5	
	12.1	-7.1		12.1	-7.1	
	12.3	-7.3	3+00	12.1	-	
1400	12.5	-7.5		12.1	-	
	12.5	-		12.2	-7.2	
10:13				12.2	-	
	12.7	-7.7		12.2	-	
	12.7	-		12.4	-7.4	
	12.8	-7.8	50	12.4	-	
50	12.8	-		12.4	-	
	12.8	-		12.4	-	
	13.0	-8.0		12.2	-7.2	
	13.0	-		12.2	-	
	13.0	-	4+00	12.2	-	
2+00	13.0	-				

STA-63+00

4-22-48

DIST	SOUND	DIST	SOUND
4+10	12.0	-7.0	
	12.0	-	
(5.0)	12.5	-7.5	
	12.7	-7.7	
50	12.7	-	
<u>10:18</u>	12.0	-7.0	
	12.4	-7.4	
	12.0	-7.0	
	12.5	-7.5	
5+00	12.5	-7.5	
	12.5	-7.5	
	12.5	-7.5	
	12.8	-7.8	
	13.0	-8.0	
50	13.1	-8.1	
	13.1	-	
	13.2	-8.2	
	13.1	-8.1	
<u>10:20</u>	13.0	-8.0	
6+00	13.0	-8.0	

STA-65+00

4-22-48

(76)

1+00 = PT. 400' N/1/2 STA-65+00 D 3/4. SOUND SOUTH.

DIST	SOUND	DIST	SOUND
0+00	9.0	+1.0	1+00 11.9 -6.4
+10	9.0	-	2+00 11.0 -6.0
<u>10:28</u>	9.0	-	11.0 -
(5.0)	9.1	+0.9	(5.0) 11.4 -6.4
	9.2	-	12.3 -7.3
50	9.5	-4.5	12.3 -
	11.8	-6.8	50 12.0 -7.0
	12.0	-7.0	12.2 -7.2
	11.8	-6.8	12.3 -7.3
	10.8	-	12.0 -7.0
1+00	10.0	-5.0	12.0 -
	8.2	-3.2	3+00 11.8 -6.8
	9.7	-4.7	11.5 -6.5
	11.5	-6.5	11.8 +0.8 -6.8
	11.3	-6.3	12.0 -7.0
50	11.0	-6.0	12.0 -
	12.0	-7.0	50 12.0 -
<u>10:30</u>	11.8	-6.8	11.4 -6.4
1+00	11.2	-6.2	3+70 11.0 -6.0

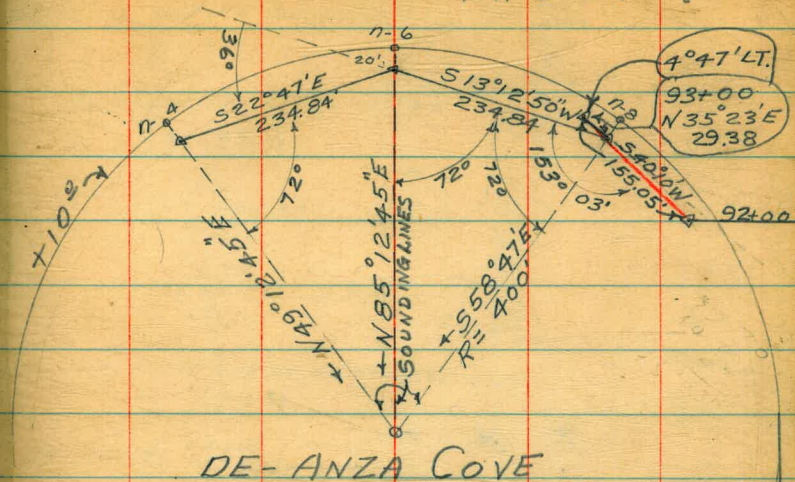
STA-65+00

4-22-48

DIST	SOUND		DIST	SOUND	
3+80	11.0	-6.0	5+80	12.5	7.5
<u>10:33</u>	11.0	-		12.7	7.7
4+00	11.5	-6.5	6+00	12.7	7.7
	11.5	-	(5.0)		
(5.0)	12.5	-			
	12.8	-7.8			
	13.0	-8.0			
50	14.5	-9.5			
	14.5	-			
	14.0	-9.0			
	14.0	-			
	14.0	-			
5+00	14.4	-9.4			
	14.4	-			
<u>10:35</u>	14.0	-9.0			
	14.0	-			
	13.5	-8.5			
50	13.8	-8.3			
	13.2	-8.2			
5+70	12.7	-7.7			

5-11-48
T.A. STAMPER

(79)



BASELINE FOR RADIAL SOUNDINGS
OF PROJECT NO. 3.1

Indexed

0+31' P.I.
HORSE
184' P.I. DEF RT. 72°05'00"

STA-215

0+31

38' 00"
STA-2+15 DEF RT. 60°40'00"

STA-3+56

2+15
STA-3+56 DEF RT. 16°08'00"

5+36

3+56
STA-5+36 DEF RT. 5°38'00"

10+31

5+36
STA-10+31 DEF RT. 0°56'00" 02°15'00"

16+31

10+31
STA 16+31 DEF LEFT 24°12'00"

19+52

16+31
STA-19+52 DEF LT. 56°23'00"

22+72

19+52
22+72 DEF RT. 77°51'00"

N-151+00 DE ANZA 5/4

HORSE
N-151+00 INT. RT. { 24°23'00" } 24°22'30"
22+72 { 48°45'00" }

N-151+58 - 48"

N-159+30 - 12"

N-164+00 - 29"

N-166+05 - 14"

N-168+35 - 36"

W-76+30W - 30"

S-75-37-15W

P.I.

31'

0+31

184'

2+15

1+1'

3+56

180'

5+36

195'

10+31

600'

16+31

321'

19+52

320'

22+72

113.56'

23+8.55C = N-151+00 DE ANZA 5/4

215

141

356

01°56'00

287

31

321

56°23'00"



$$= \frac{c}{a}$$

$$\frac{1}{2}$$

$$\frac{a^2}{c^2}$$

C
A

+B)

+B)

79-80

157.54'

15°55' → P.I.

179°60'

75°55'

139°05'

by the
8.4 ft
10' =

slope
in the
flow

STA-106-395 FOR CONTROL LINE

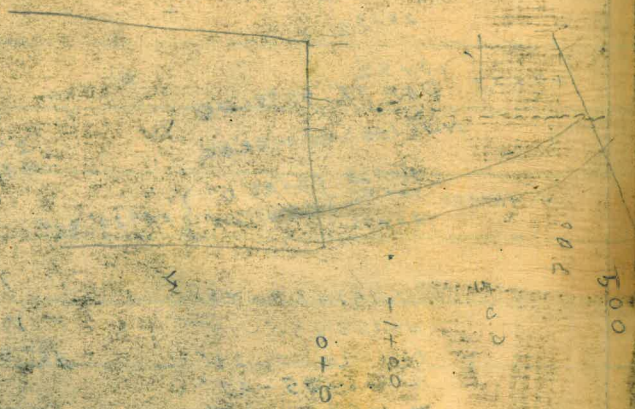
105+00 + 6.23 = EL. 7.82

N-151+00

1.905 - H.I.
 - 4.27
 T.B.M. ① 2.978 - (20) 5+00
 + 5.25
 15.13 - H.I.
 - 5.12
 T.B.M. ② 9.98 - (20) 10+00
 + 7.33
 17.97 - H.I.
 - 4.74
 T.B.M. ③ 13.23 - (20) 15+00
 + 5.29
 18.52 - H.I.
 - 3.49
 T.B.M. ④ 15.03 - (20) 20+00

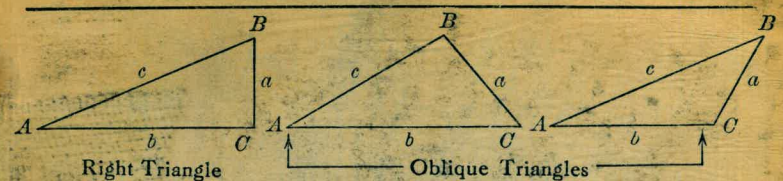
CONTROL LEVELS

8,804 = 24, BAND



4-13-35 7-12-35

TRIGONOMETRIC FORMULÆ



Solution of Right Triangles

For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{a}$, $\text{cosec} = \frac{c}{b}$

Given	Required	Formula
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B, c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B, b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A, b = a \cot A, c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A, a = b \tan A, c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A, a = c \sin A, b = c \cos A$

Solution of Oblique Triangles

A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}, C = 180^\circ - (A + B), c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}, C = 180^\circ - (A + B), c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C, \tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}, \sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}, C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}, \text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance - 319.4 ft. Vert. angle = $5^\circ 10'$. From Table, Page IX. $\cos 5^\circ 10' = .9959$. Horizontal distance = $319.4 \times .9959 = 318.09$ ft. Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\text{Cosine } 5^\circ 10' = .9959$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.09$

When the rise is known, the horizontal distance is approximately the square of the rise divided by twice the slope distance. $\text{slope distance} = 302.6$ ft. $\text{Horizontal distance} = 302.6 - \frac{14 \times 14}{2 \times 302.6}$