

E.D. 410 F
Bruning 739 F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

MICROFILMED
Jan 7 1965

H	.1	.2	.4	.5	.6	.7	.8	.9	H.		
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6 + (20-16) ÷ 2 or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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K & E 360-A

TITLE

179-60
78-13
101-75
12-49-60
12-29-50
N 0° 20' 10 E

91.91
300.24
71.46
463.60

20 22
70 0
80 0.5

87-68-40
83-16
N 4° 52' 40 E

49-57
179 49 60
71-51-20
88-08 40

1400
1370
50

28-15-15
2 07 58
30 22 52

8.43
5.07
13.50
STAKE

4-R 55
3-A 10
2-R 15
1-L 84

835
100.45
108.83
100.45
209.31

179 60
98-32
81-38

4-52-40
10-13-20
15-06 00

179 59 60
6-57
149-37-07

12-90-60
4-52-40
N 8-38-20 W

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(For other Survey Data, see F.B. #1697)

PAGE	DATE
78	"JEEP" & "JEEPER" CONTROL POINTS 12-27-47

117°-26'32"

on Base, Coaster Ecc taking station
112.68 = 100 Sta.

101.08		
91.91		
112.99	776 -	105480 - (1400)
		(1452)
- 721	105400 -	1420
		1440
- 666	104400 -	1400
		1332

726

7949 ENCARNEL DATA

9-53-46
1-51-30
11-45-00

	DIST
126	710
125	768
124	778
123	772
122	776
121	808
120	830
119	840
118	825
117	710

$$\frac{386}{772}$$
$$\begin{array}{r} 71.46 \\ 303.24 \\ \hline 91.91 \\ 466.61 \end{array}$$

PROPOSED ROAD ALIGNMENT
FOR ACCESS ROAD ON NEW
DREDGED FILL IN MISSION BAY
NEAR VENTURA PLACE
GLEASON POINT

STA.	DEFL	CHORD	STA.	DEFL	CHORD
0+00	0°0'	50.00	13+50	46°52'48"	49.98
4+50	B.C.	" "	14+00	49°29'04"	"
5+00	2°36'16"	49.98	+50	52°05'20"	"
+50	5°12'32"	"	15+00	54°41'36"	"
6+00	7°48'48"	"	+50	57°17'52"	"
+50	10°25'04"	"	E.C.+50.16	57°18'15"	0.16
7+00	13°01'20"	"	16+00	0°0'	49.84
+50	15°37'16"	"	+50	"	50.00
8+00	18°13'52"	"	17+00	"	"
+50	20°50'08"	"	+50	"	"
9+00	23°26'24"	"	18+00	"	"
+50	26°02'40"	P.O.C."	+50	"	"
10+00	28°38'56"	"	19+00	"	"
+50	31°15'12"	"	+50	"	"
11+00	33°51'28"	"			
+50	36°27'44"	"			
12+00	39°04'00"	"			
+50	41°40'16"	"			
13+00	44°16'32"	"			

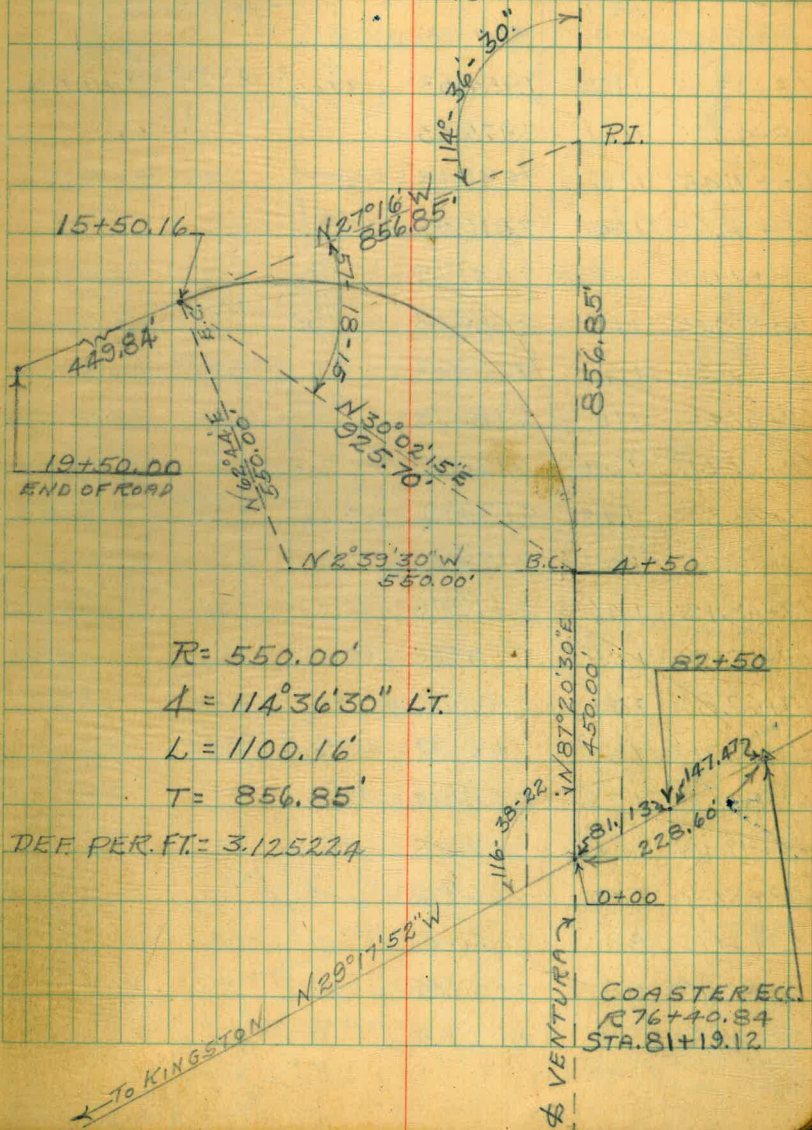
INDEXED

①

5-28-46

JUL 16 1953

DRAWN & COMPUTED BY:
THOMAS A. STAMPER



179-60
85-01
94-57

NOTE: GRID BEARING = N1°51'20"W
RANGE & GRID STATIONS ALONG
MISSION BAY WEST SHORELINE
NORTH OF VENTURA PLACE

GRID RANGE STA.	B/L RANGES	DIST. FROM R-88+67.58 TO
69+13.05	117	1954.53
68+92.25	116	1975.33
68+71.45	115	1996.13
68+50.65	114	2016.93
68+29.85	113	2037.73
68+09.05	112	2058.53
67+88.25	111	2079.33
67+67.45	110	2100.13
67+46.65	109	2120.93
67+28.39	108	2139.19
67+38.25	107	2129.33
67+48.12	106	2119.46
67+57.98	105	2109.60
67+67.84	104	2099.74
67+77.71	103	2089.87
67+87.57	102	2080.01
67+97.43	101	2070.15
68+07.30	100	2060.28
68+17.16	99	2050.42
68+27.03	98	2040.55
68+36.89	97	2030.69

ORMOND (R 69+20.67 STA. 117+36.63)
MONTEREY (R 67+27.58 STA. 108+08.31)
KINGSTON (R 68+40.88 STA. 96+59.63)

Crosses on Sidewalk & Offsets from B/L

Diagram showing a line of grid stations with bearings and distances. Key bearings include N 9° 53' 40" W, N 70° 29' 20" W, and N 29° 04' 05" W. Distances between stations are marked, such as 102.14', 100.485', 101.08, 100.25, and 85.01'. A north arrow is present.

179-60
85-01
94-57

RANGE GRID STA. DIST. FROM RANGE 88+67.58 TO B/L RANGES (2)

RANGE	GRID STA.	DIST. FROM RANGE 88+67.58 TO B/L RANGES
65+91.48	136	2276.10
66+23.18	135	2244.40
66+54.88	134	2212.70
66+86.58	133	2181.00
67+18.28	132	2149.30
67+49.98	131	2117.60
67+81.68	130	2085.90
68+13.39	129	2054.19
68+45.09	128	2022.49
68+76.80	127	1990.78
68+96.49	126	1971.09
69+11.20	125	1956.38
69+25.90	124	1941.68
69+40.61	123	1926.97
69+53.34	122	1914.24
69+46.29	121	1921.29
69+39.24	120	1928.34
69+32.19	119	1935.39
69+25.14	118	1942.44

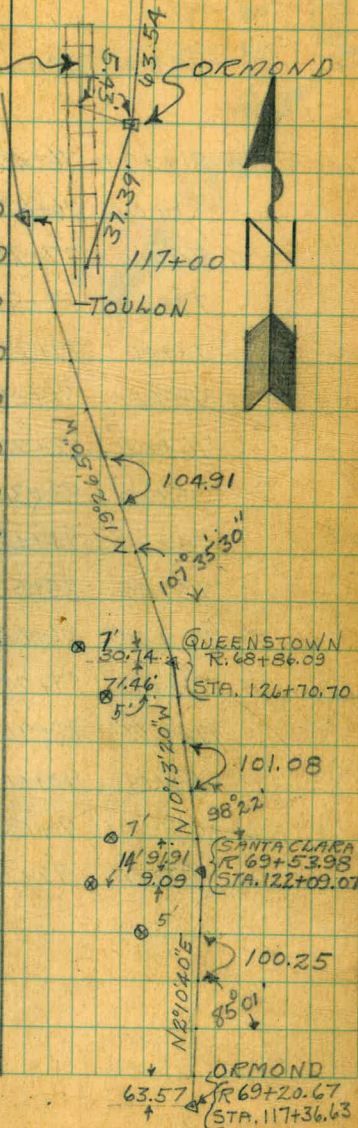
INDIVIDUAL

JUL 16 1953

E.S. WALK

THOMAS A. STAMPER

118+00 5-31-46



INDEXED

JUL 16 1953

RANGES & DISTANCES ALONG
NEW BASELINE BEARING $S50^{\circ}E$
FROM COASTER ECC.

STA	RANGE	GRIP 100' =	DISTANCE FROM	
			RANGE	WEST EAST
COASTER ECC.	81+19.12	76+40.84		
	81+00	76+62.18	28.65	1205.40
	80+00	77+73.81	149.87	1093.77
	79+00	78+85.44	"	982.14
	78+00	79+97.07	"	870.51
	77+00	81+08.70	"	758.88
	76+00	82+20.33	"	647.25
	75+00	83+31.96	"	535.62
	74+00	84+43.59	"	423.99
	73+00	85+55.22	"	312.36
	72+00	86+66.85	"	200.73
	71+00	87+78.48	"	89.10
	70+00	88+90.11	"	22.53
	69+00	90+01.74	"	134.16
	68+00	91+13.37	"	245.79
	67+00	92+25.00	"	357.42

91.45
87.75
3 27

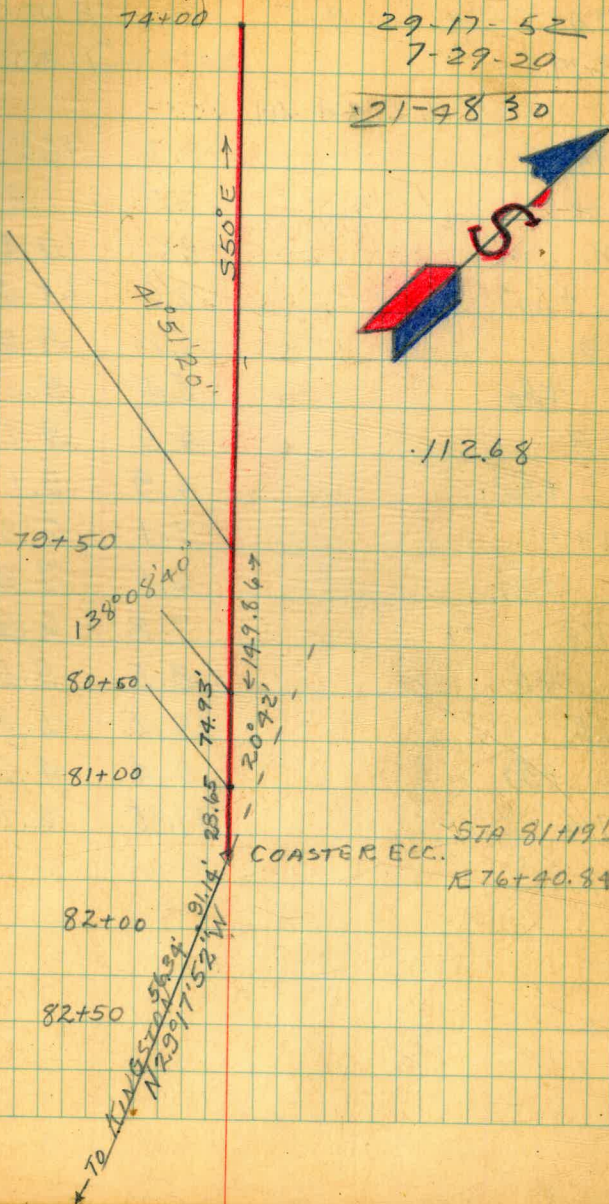
6-3-46

(3)

THOMAS A. STAMPER

29-17-52
7-29-20

21-4830



MAY ESTIMATE
MISSION BAY PROJECT A "A"

STA + H.I - ELEV.

B.M. 11.39

2.62, 14.01

81+00 3.3 10.7

+50 2.2 11.8

80 3.6 10.4

+50 2.6 11.4

79 5.1 8.9

+50 5.4 8.6

78 4.9 9.1

+50 4.9 9.1

77 7.1 6.9

+50 6.1 7.9

76 7.8 6.2

+50 8.5 5.5

75 8.5 5.5

+50 9.4 4.6

74 11.5 2.5

6-3-46

④

TOM ALLEN

TOM STAMPER

U.S.C. & G.S. COASTER

ESTIMATE CONTD.

Inst @	+	H.I	-	ELEV
Inst @ 74+00				2.5
	4.0	6.5		
29 E			4.8	1.7
<u>78 E</u>			4.5	2.0
24 W			3.7	2.8
44 W			2.5	4.0
67 W			2.5	4.0
153 W			3.9	2.6
183 W			4.2	2.3

INST @				
INST @ 75+00				5.5
	5.0	10.5		
23 E			5.5	5.0
<u>93 E</u>			7.7	2.8
63 W			5.2	5.3
84 W			3.8	6.7
94 W			0.5	10.8
106 W			4.7	6.6
118 W			7.1	4.2
160 W			8.3	3.0

INST @				
INST @ 76+00				6.2
PX	5.1	11.3		
78 W			3.8	7.5
90 W			0.1	11.2
104 W			4.8	6.5
130 W			6.1	5.1
187 W			8.1	3.2

H.I 11.3

(3)

INST @ 76+00	-	Elev
210 W	10.0	1.3
<u>76 E</u>	4.9	6.4
63 E	5.7	5.6
108 E	6.5	4.8
160 E	7.6	3.7
188 E	8.1	3.2

Inst. @	PX	H.I = 12.2	Elev
Inst. @ 77+00	5.3		6.9
14 E	5.6		6.6
44 E	5.4		6.8
46 E	4.4		7.8
80 E	4.8		7.4
113 E	5.1		7.1
158 E	6.0		6.2
202 E	6.6		5.6
240 E	7.7		4.5
280 E	8.4		3.8
334 E	9.0		3.2
<u>352 E</u>	9.4		2.8
1 W	5.0		7.2
4 W	2.8		9.4
38 W	2.3		9.9
65 W	2.3		9.9
90 W	2.3		9.9

77400 CONTD. ESTIMATE CONTD.

PX	+	HI	-	EL.
100 W			2.2	10.0
106 W			0.8	11.4
120 W			5.2	7.0
152 W			8.0	4.2
194 W			8.6	3.6
232 W			9.0	3.2
272 W			8.2	4.0
312 W			9.2	3.0
360 W			9.4	2.8

PX
Inst. @ 78400
4.9 14.0

12 W			5.0	9.0
29 W			5.0	9.0
30 W			3.9	10.1
62 W			4.3	9.7
97 W			3.7	10.3
143 W			3.1	10.9
190 W			3.8	10.2
247 W			3.9	10.1
300 W			3.8	10.2
354 W			3.9	10.1
402 W			3.9	10.1
447 W			3.5	10.5

PX. H.I. 14.0

78400 Contd.

Elev. (B)

	-	ELEV		
50 E	5.4	8.6		
140 E	7.1	6.9		
218 E	8.4	5.6		
312 E	9.4	4.6		
410 E	10.3	3.7		
460 E	11.7	2.3		
540 E	12.4	1.6		
STA	+	H.I.	-	ELEV
78400	4.9	13.8		8.9
56 W		3.8		10.0
106 W		3.5		10.3
165 W		3.7		10.1
223 W		3.6		10.2
262 W		2.7		11.1
48 E		5.9		7.9
93 E		6.5		7.3
148 E		6.9		6.9
198 E		7.7		6.1
258 E		8.5		5.3
292 E		8.8		5.0
325 E		9.5		4.3
380 E		10.1		3.7
420 E		10.5		3.3
470 E		10.7		3.1
520 E		11.7		2.1

ESTIMATE CONTD

STA	+	H.I.	-	ELEV
<u>80+00</u>				10.4
	4.8	15.2		
47E			3.5	11.7
88E			4.2	11.0
150E			6.1	9.1
195E			7.1	8.1
252E			8.2	7.0
328E			9.1	6.1
412E			10.2	5.0
470E			11.0	4.2
525E			11.0	4.2
<u>560E</u>			11.4	3.8
41W			4.8	10.4
72W			5.4	9.8
116W			4.4	10.8
170W			3.9	11.3
234W			4.3	10.9
<u>81+00</u>	4.8	15.5		10.7
7E			3.5	12.0
50E			3.4	12.1
96E			4.1	11.4
146E			3.6	11.9
195E			5.0	10.5
254E			6.8	8.7
292E			7.1	8.4
335E			7.6	7.9

81+00 CONTD

STA	+	H.I.	-	ELEV
		15.5		
390E			8.4	7.1
445E			9.1	6.4
500E			10.0	5.5
542E			9.8	5.7
588E			10.1	5.4
640E			10.6	4.9
688E			10.9	4.6

Inst. @ 82+00

4.48 15.87

"Coaster"

11.39

0			5.0	10.9
24E			4.6	11.3
66E			5.4	10.5
122E			5.3	10.6
180E			5.0	10.9
234E			5.6	10.3
290E			6.4	9.5
348E			7.1	8.8
402E			7.8	8.1
456E			8.5	7.4
503E			7.8	8.1
543E			8.4	7.5
605E			8.4	7.5

STA	+	H.I.	-	ELEV
82700	Cont'd.	15.9		
680' E			8.8	7.1
742 E			9.4	6.5

(8)

STA	+	H.I.	-	ELEV
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6-8-46

STA	+	H.I.	-	ELEV
T128	5.45	13.8		8.35
1 E			6.0	7.8
22 E			7.1	6.7
51 E			9.3	4.4
20 E			10.5	3.3
^{B/L} T127	4.75	13.20		8.44
7 W			4.75	8.44
5 E			5.1	8.1
46 E			8.2	5.0
72 E			10.4	2.8
^{B/L} T126	4.4	12.80		8.42
5 W			4.4	8.4
5 E			5.0	7.8
26 E			7.6	5.2
54 E			10.0	2.8
^{B/L} T125	5.4	13.7		8.32
2 E			6.8	6.9
30 E			9.2	4.5
58 E			10.9	2.8
^{B/L} T124	5.0	13.4		8.41
3 E			5.0	8.4
19 E			7.8	5.6
37 E			8.6	4.8
64 E			10.4	3.0

(11)

6-8-46

STA	+	H.I	-	ELEV
T123	3.28	12.60		8.34
7 W			3.3	9.3
3 W			3.8	8.8
0			5.0	7.6
30 E			7.0	5.6
72 E			8.6	4.0
INST SANTA CLARA		0° AZIM	DN QUEENSTON	
TBM			8.40	122

5.6 x 14.00

DIST	AZ	ROD	ELEV
44	350°35'	6.0	8.0
22	5°40'	6.0	8.0
12	350°05'	6.0	8.0
15	59°55'	6.0	8.0
42	89°05'	6.0	8.0
50	90°45'	6.0	8.0
46	101°	6.0	8.0
28	116°55'	6.0	8.0
26	142°40'	6.0	8.0
26	179°40'	6.0	8.0
30	198°40'	6.0	8.0
48	200°30'	6.0	8.0
69	182°	8.0	6.0
42	151°	8.0	6.0
43	115°50'	8.0	6.0
52	101°10'	8.0	6.0

H.I 1400

(12)

T SANTA CLARR 0° AZIM TO QUEENSTOWN

DIST	AZIM	ROD	ELEV
58	83°10'	8.0	6.0
54	74°10'	8.0	6.0
32	49°20'	8.0	6.0
33	46°05'	8.0	6.0
52	13°20'	8.0	6.0
74	36°05'	10.0	4.0
68	61°20'	10.0	4.0
78	81°40'	10.0	4.0
78	91°	10.0	4.0
72	109°10'	10.0	4.0
70	151°50'	10.0	4.0
100	144°25'	12.0	2.0
92	109°35'	12.0	2.0
102	97°45'	12.0	2.0
106	88°20'	12.0	2.0
100	81°10'	12.0	2.0
92	70°10'	12.0	2.0

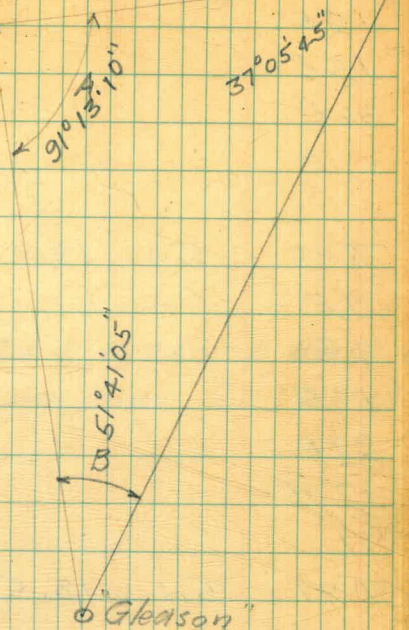
STA	+	H.I.	-	ELEV
B/L 121	5.3	13.7		8.42
3E			7.0	6.7
31E			9.0	4.7
68E			11.1	2.6
B/L T120	5.4	13.8		8.4
3E			7.4	6.4
27E			9.0	4.8
58E			11.5	2.3
B/L T119	5.4	13.7		8.34
4E			8.2	5.5
24E			9.2	4.5
52E			11.1	2.6

LOCATION OF SEXTANT PT. "WINDOW"

STA.	OBJECT	SIX ANGLES	MEAN	VERNIER
	LARGE WINDOW	①	91°13'00"	
CITY MON.				
SANTA CLARA	R	②	182°26'00"	91°13'0" 0°00'00"
CITY STA				
GLEASON	G	③	547°19'00"	
	CITY MON.			
SANTA CLARA	D	①	51°41'15"	
CITY STA.				
GLEASON	R	②	103°22'30"	51°41'05" 0°00'00"
	LARGE WINDOW	③	310°06'30"	

Center Large Window, White House on Bluff
at Crown Point
"Santa Clara" Δ

A
① 91°13'00"
② 182°26'00"
③ 547°19'00"
91°13'10"



INDEXED
JUL 16 1953

6-8-46
TOM ALLEN
TOM STAMPER

6-18-46

STA.	+	H.I.	-	ELEV.
π96 ^{BL}	5.4	14.0		8.6
15E			5.5	8.5
15E			7.7	6.3
36E			9.7	4.3
51E			12.2	1.8

π95	5.4	13.9		8.5
7E			5.4	8.5
x 7E			7.9	6.0
17E			9.2	4.7
97E			9.5	4.4
120E			12.3	1.6

π97	5.1	13.5		8.4
27E			5.6	7.9
31E			7.8	5.7
55E			11.7	1.8

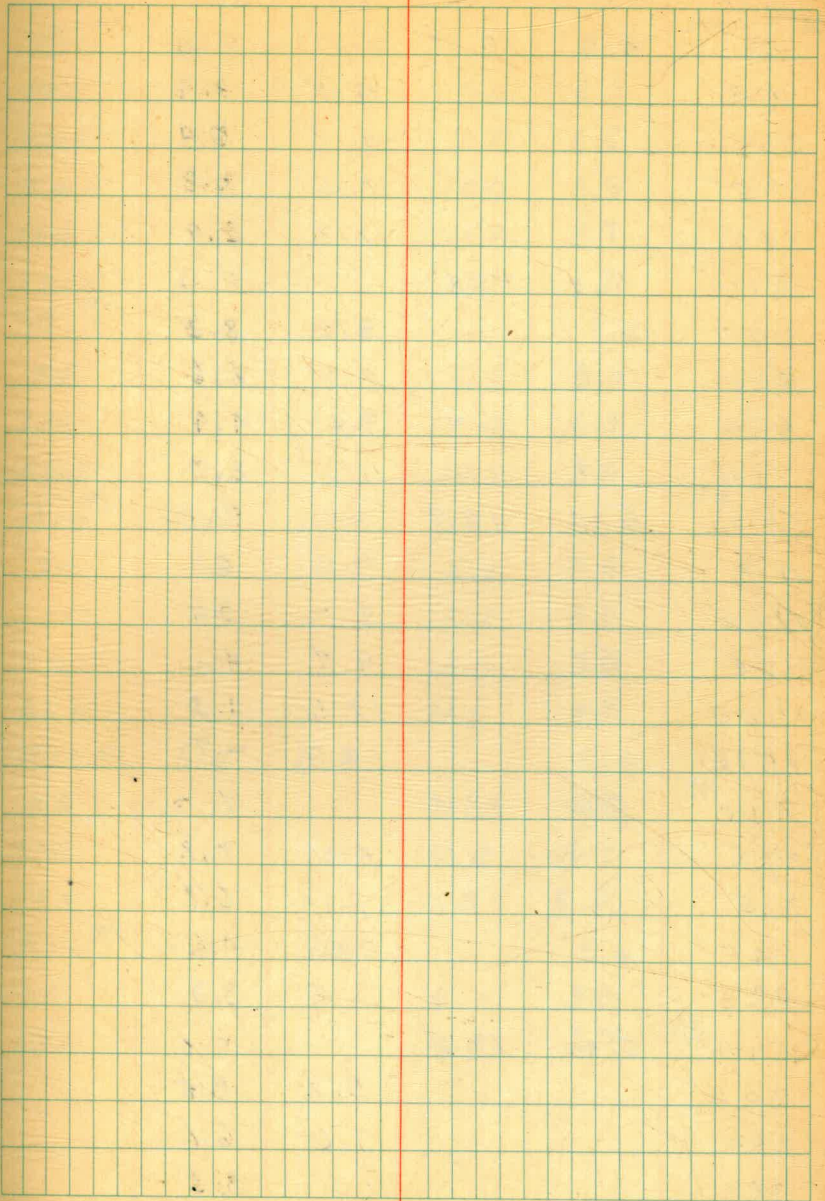
π98	5.0	13.4		8.4
13W			5.0	8.4
0			5.0	8.4
11E			5.4	8.0
27E			8.0	5.4
48E			11.6	1.8

(19)

NOTE: Sta 95+00 Av. with 95+20 which
will have same Sec. 95 96+00

STA	+	H.I.	-	ELEV.
$\pi 99$ ^{B/L}	2.8	11.3		8.5
11 W			2.8	8.5
0			5.0	6.3
10 E			6.5	4.8
53 E			8.6	2.7
58 E			9.7	1.6
$\pi 100$ ^{B/L}	0.8	9.3		8.5
28 W			0.5	8.8
0			5.1	4.2
18 E			6.7	2.6
31 E			6.8	2.5
37 E			7.2	2.1
$\pi 101$ ^{B/L}	<u>-0.2</u>	8.2		8.4
38 W			0.2	8.0
19 W			3.4	4.8
0			5.0	3.2
13 E			6.1	2.1
$\pi 102$ ^{B/L}	0.2	8.6		8.4
34 W			0.4	8.2
23 W			2.9	5.7
0			4.8	3.8
23 E			6.3	2.3

STA	+	H.L.	-	ELEV
$\bar{T}_{103}^{B/L}$	0.4	8.9		8.5
43W			0.3	8.6
22W			3.0	5.9
0			5.1	3.8
12E			6.5	2.4
$\bar{T}_{104}^{B/L}$	0.9	9.3		8.4
32W			1.0	8.3
32W			1.8	7.5
21W			3.4	5.9
0			5.0	4.3
20E			7.0	2.3
\bar{T}_{105}	0.6	9.0		8.4
28W			2.0	7.0
0			4.7	4.3
26E			6.5	2.5
\bar{T}_{106}	1.6	10.0		8.4
33W	1.6		1.6	8.4
19W			2.5	7.5
0			5.0	5.0
24E			7.6	2.4
$\bar{T}_{107}^{B/L}$	4.5	12.9		8.4
0			4.9	8.0
17W			4.5	8.4
14E			6.2	6.7
41E			8.3	4.6
57E			9.3	3.6
65E			10.4	2.5



STA	+	H.I.	-	ELEV.
$\bar{\Delta}$ 108 ^{B/L}	4.8	13.2		8.4
6E			4.8	8.4
24E			4.8	8.4
37E			7.4	5.8
76E			10.3	2.9
$\bar{\Delta}$ 109 ^{B/L}	5.4	13.8		8.4
20E			5.6	8.2
32E			7.2	6.6
62E			9.4	4.4
81E			11.1	2.7
$\bar{\Delta}$ 94 ^{B/L}	5.4	13.9		8.5
4E			7.0	6.9
91E			8.3	5.6
118E			9.8	4.1
150E			12.6	1.3
159E			14.6	-7
$\bar{\Delta}$ 110 ^{B/L}	5.5	13.8		8.3
28E			5.6	8.2
31E			7.1	6.7
64E			9.2	4.6
93E			10.5	3.3
$\bar{\Delta}$ 111 ^{B/L}	5.4	13.8		8.4
20E			5.2	8.6
28E			7.6	6.2
78E			10.5	3.3
121E			11.3	2.5

STA	+	H.I.	-	ELEV.
$\bar{\Delta}$ 112 ^{B/L}	5.4	13.9		8.5
10E			5.6	8.3
22E			7.7	6.2
54E			10.0	3.9
104E			11.2	2.7
121E			12.7	1.2
$\bar{\Delta}$ 113 ^{B/L}	5.4	13.8		8.4
3E			5.8	8.0
17E			7.4	6.4
56E			10.2	3.6
$\bar{\Delta}$ 114 ^{B/L}	5.4	13.8		8.4
3E			5.4	8.4
14E			7.7	6.1
52E			10.0	3.8
65E			11.1	2.7
$\bar{\Delta}$ 115 ^{B/L}	5.4	13.8		8.4
3E			7.0	6.8
31E			9.4	4.4
53E			11.3	2.5
$\bar{\Delta}$ 116 ^{B/L}	5.4	13.8		8.4
3E			8.0	5.8
53E			11.5	2.3

JUNE ESTIMATE

MISSION BAY PROJECT No 4-"A"

STA.	+	H.I.	-	ELEV.
B.M.	1.26	12.65		11.39
81			1.5	11.1
80			2.5	10.1
79			2.2	10.9
78			3.5	9.1
77			3.5	9.1
76			2.8	9.8
75			4.6	8.0
74			6.3	6.3
73			7.0	5.6
72			6.4	6.2
71			6.9	5.7
70			7.8	4.8
69			8.0	4.6
T 69 ^{too}	5.0	9.6		4.6
E 26			5.4	4.2
E 94			7.4	2.2
E 110			8.0	1.6
W 45			4.4	5.2
W 110			3.9	5.7
W 168			2.7	6.9
W 202			3.7	5.9
W 240			2.7	6.9
W 290			3.8	5.8

7-1-46

NOTE: SEE R/L SKETCH

P. 3

U.S.C. & G.S. A COASTER.

T. ALLEN

G. WILLIAMS

T. STAMPER

STA	+	H.I.	-	ELEV
		9.6		
W 378			7.2	2.4
T 70 ^{too}	4.6	9.4		4.8
W 628			6.8	2.6
W 480			6.5	2.9
W 360			6.8	2.4
W 260			5.2	4.2
W 200			2.3	7.1
W 180			1.1	8.3
W 140			3.2	6.2
W 84			4.4	5.0
W 36			4.6	4.8
E 58			3.6	5.8
E 130			3.2	6.2
E 150			2.2	7.2
E 230			3.8	5.6
E 320			6.9	2.5

	+	NI.	-	EI.
π 71100	4.9	10.6	—	5.7
W. 54			4.4	6.2
W. 164			5.4	5.2
W. 182			0.8	9.8
W. 195			6.1	4.5
W 270			7.5	3.1
W 350			7.9	2.7
W 432			7.4	3.2
W 500			7.9	2.7
E. 115			7.1	3.5
E 221			6.4	4.2
E. 335			6.3	4.3
E. 418			8.1	2.5
E. 494			8.0	2.6
π 72100	5.0	11.2		6.2
E. 584			8.4	2.8
E. 530			6.7	4.5
E. 490			8.2	3.0
E. 368			8.0	3.2
E. 280			7.9	3.3
E. 170			6.8	4.4
E. 52			4.7	6.5
W. 96			5.9	5.3
W. 110			1.6	9.6

	+	NI.	-	EI.
W. 128			7.0	4.2
W. 202			8.8	2.4
π 73100	4.8	10.4		5.6
W. 198			7.4	3.0
W. 118			5.8	4.6
W. 96			1.2	9.2
W. 78			4.9	5.5
W. 15			5.4	5.0
E. 58			4.1	6.3
E. 156			5.2	5.2
E. 316			6.7	3.7
E. 400			7.5	2.9
E. 450			7.2	3.2
E. 504			8.0	2.4
π 74100	5.0	11.3		6.3
E. 510			8.4	2.9
E. 418			8.6	2.7
E. 266			7.3	3.0
E. 187			6.6	4.7
E. 56			4.7	6.6
W. 76			6.1	5.2
W. 102			1.8	9.5

	+	11.3 HZ	-	EI
74400				
W. 120			6.6	4.7
W. 162			8.4	2.9

Δ 75400	4.9	12.9		8.0
W. 150			10.1	2.8
W. 121			8.6	4.3
W. 96			2.6	10.3
W. 86			5.1	7.8
W. 40			3.9	9.0
E. 58			5.9	7.0
E. 169			6.4	6.5
E. 317			8.6	4.3
E. 402			9.7	3.2

Δ 76400	4.7	14.5		9.8
E. 515			12.0	2.5
E. 398			12.0	2.5
E. 382			10.9	3.6
E. 267			9.3	5.2
E. 98			7.0	7.5
E. 20			4.2	10.3
W. 42			3.2	11.3
W. 88			4.1	10.4
W. 112			9.5	5.0

(21)

	+	14.5 HI	-	Elev.
W. 183			11.4	3.1
Δ 77400	4.9	14.0		9.1
W. 292			10.5	3.5
W. 257			10.1	3.9
W. 220			10.3	3.7
W. 88			4.8	9.2
W. 22			3.8	10.2
E. 54			6.0	8.0
E. 160			6.8	7.2
E. 256			7.8	6.2
E. 458			10.9	3.1
E. 623			10.6	3.4
E. 708			10.8	3.2
Δ 78400	5.0	14.1		9.1
E. 748			10.8	3.3
E. 670			7.0	7.1
E. 657			7.3	6.8
E. 597			10.8	3.3
E. 532			10.4	3.7
E. 468			10.3	3.8
E. 340			9.1	5.0
E. 223			8.4	5.7
E. 68			5.0	9.1

	+	#Z	-	EL.
W.		14.1		
W 26			4.4	9.7
W 4.8			3.5	10.6
W 65			4.5	9.6
W 129			4.0	10.1
W 288			3.8	10.3
W 440			3.5	10.6
<hr/>				
Σ 79+00	4.6	15.0		10.4
W 262			3.6	11.4
W 225			4.7	10.3
W 125			5.0	10.0
W 82			4.6	10.4
W 61			5.1	9.9
W 23			4.7	10.3
E 26			5.0	10.0
E 108			4.5	10.5
E 206			6.8	8.2
E 328			9.5	5.5
E 411			10.6	4.4
E 505			10.7	4.3
E 595			11.0	4.0
E 664			10.9	4.1
E 686			8.1	6.9
E 712			9.2	5.8

(22)

	+	HT	-	ELEV.
E 800		15.0	11.8	3.2
<hr/>				
Σ 80+00	4.9	15.0		10.1
E 783			11.6	3.4
E 730			10.6	4.4
E 700			10.1	4.9
E 686			7.0	8.0
E 682			9.8	5.2
E 633			10.1	4.9
E 528			9.5	5.5
E 422			10.0	5.0
E 392			9.2	5.8
E 263			7.3	7.7
E 134			5.1	9.9
E 48			4.8	10.2
W 45			4.6	10.4
W 54			3.4	11.6
W 70			5.5	9.5
W 100			5.0	10.0
W 118			4.4	10.6
<hr/>				
Σ 81+00	4.7	15.8		11.1
W 5			4.7	11.1
E 73			4.6	11.2
E 176			5.1	10.7

	+	H.I	-	ELEV.
E 228		15.8	5.5	10.3
E 370			8.1	7.7
E 500			9.8	6.0
E 570			9.5	6.3
E 685			8.0	7.8
E 728			8.3	7.5
E 735			5.9	9.9
E 755			11.4	4.4
E 775			11.2	4.6
E 804			12.3	3.5
<i>Coaster</i>				11.39
T 82+00	4.40	15.8	4.9	10.9
E 846			9.8	6.0
E 940			10.9	4.9
E 966			12.4	3.4
E 828			6.2	9.6
E 817			7.4	8.4
E 807			6.0	9.8
E 786			8.2	7.6
E 755			8.8	7.0
E 644			8.6	7.2
E 573			8.3	7.5
E 454			8.4	7.4
E 320			6.8	9.0
E 272			5.3	10.5

0

4.1 10.5

(23)

	+	H.I	-	ELEV
E 174		15.8	4.6	11.2

MISSION BAY AREA
TRIANGULATION
OF STA "CAUSEWAY"

STA.	OBJECT	SIX ANGLES	VERNIER	MEAN
	U.S.C.&G.S. COASTER	1.	73° 10' 00"	
	U.S.C.&G.S. B.M.#1	2.	146° 20' 00"	0° 00' 00" 73° 10' 00"
	U.S.E.D. WATSON	6.	139° 00' 00"	
	U.S.C.&G.S. B.M.#1	1.	65° 13' 00"	
	U.S.E.D. WATSON	2.	130° 25' 15"	0° 00' 00" 65° 12' 30"
	U.S.C.&G.S. COASTER	6.	391° 15' 00"	
	U.S.E.D. WATSON	1.	41° 38' 00"	
	U.S.C.&G.S. COASTER	2.	83° 15' 00"	0° 00' 00" 41° 37' 40"
	U.S.C.&G.S. B.M.#1	6.	249° 46' 00"	
	U.S.C.&G.S. B.M.#1	1.	16° 09' 00"	
	U.S.C.&G.S. COASTER	2.	32° 17' 30"	0° 00' 00" 16° 08' 55"
	MARSTONS TOWER	6.	96° 53' 30"	

INDEXED

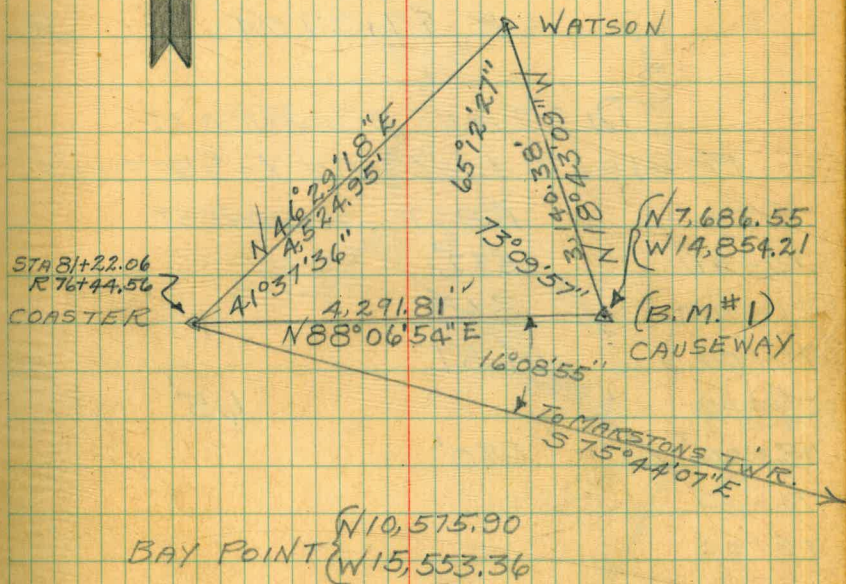
JUL 16 1953

BUFF & BERGER
INST. NO. 2091

7-12-46

G. WILLIAMS
T. STAMPER

WARM-HAZY



JULY ESTIMATE
MISSION BAY PROJECT 4-"A"

STA	+	H.I.	-	ELEV.
B.M.	2.15	13.54		11.39
82+00			3.9	9.6
81			4.0	9.5
80			4.3	9.2
TP (on 80+00)	5.81	15.55	3.80	9.74
79			5.2	10.3
78			4.7	10.8
77			5.0	10.6
76			5.5	10.0
75			8.3	7.3
74			8.8	6.7
73			9.3	6.3
72+50			6.5	9.0
TP			5.68	9.87
	3.85	13.72		
72			7.2	6.5
71			6.9	6.8
70			4.9	8.8
69	9.30	14.70	8.3	5.4
E 81			11.6	3.1
E 48			10.7	4.0
E 08			10.1	4.6
W 15			7.9	6.8
W 24			5.3	9.4
			9.0	5.7

U.S.C. & G.S. COASTER

On 80+00

On 72+50

4.0

AV. ELEV. FOR STA. TO END AREA

(26)

7-29-46

T. ALLEN

G. WILLIAMS

T. STAMPER

14.7

STA	+ H.I.	-	ELEV.
W 40		4.4	10.3
W 110		4.0	10.7
W 203		4.4	10.3
W 215		7.8	6.9
W 260		10.7	4.0
W 335		12.7	2.0

Σ 70+00	4.6	13.4	8.8
---------	-----	------	-----

E 23		2.3	11.1
------	--	-----	------

E 38		6.5	6.9
------	--	-----	-----

E 88		9.3	4.1
------	--	-----	-----

<u>E 163</u>		10.3	3.1
--------------	--	------	-----

W 51		5.9	7.5
------	--	-----	-----

W 86		5.9	7.5
------	--	-----	-----

W 165		7.8	5.6
-------	--	-----	-----

W 296		8.0	5.4
-------	--	-----	-----

W 230		9.0	4.4
-------	--	-----	-----

W 380		7.9	5.5
-------	--	-----	-----

W 410		2.4	11.0
-------	--	-----	------

W 426		6.7	6.7
-------	--	-----	-----

W 437		9.2	4.2
-------	--	-----	-----

W 487		12.2	1.2
-------	--	------	-----

Σ 71+00	5.1	11.9	6.8
---------	-----	------	-----

W 573		7.6	4.3
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7-29-46

(27)

20-04-16

50

70 04-16

179 59 60

109-55 44

	+	11.9 H.I.	-	ELEV
W 562			5.2	6.7
W 560			1.4	10.5
W 540			6.6	5.3
W 470			6.8	5.1
W 412			5.8	6.1
W 368			6.7	5.2
W 187			6.6	5.3
W 277			8.1	3.8
W 80			4.4	7.5
W 30			5.1	6.5
E 21			0.2	11.7
E 33			5.2	6.7
E 64			6.7	5.2
E 82			8.1	3.8
E 182			9.1	2.8
W 72400	5.1	11.6		6.5
E. 82			8.0	9.6
E 157			9.5	2.1
E 32			5.8	5.8
E. 28			4.8	6.8
E. 18			0.4	11.2
E. 5			4.5	7.1

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(28)

	W 72400	HI. 11.6	-	EI.
W. 16'			6.0	5.6
W. 68'			5.3	6.3
W. 106			6.2	5.4
W. 283			7.5	4.1
W. 460			6.4	5.2
W 560			5.2	6.4
W 640			6.7	4.9
W. 673			6.2	5.4
W. 686			1.8	9.8
W. 695			4.9	6.7
W. 708			6.7	4.9
W. 810 ±			± 7.7	3.9
W 77400	11.5		5.2	6.3
W 925			± 8.5	3.0
W 850			7.5	4.0
W 800			6.5	5.0
W 793			4.5	7.0
W 770			1.0	10.5
W. 750			5.9	5.6
W. 620			5.9	5.6
W. 590			5.5	6.0
W 270			± 7.0	4.5
W. 58			5.9	5.6
E. 66			4.8	6.7
E. 86			2.5	9.0

	+	HI	-	EI.
π 73+00 (Contd)	9.9	16.2		6.3
E. 97			5.0	11.2
E. 112			10.6	5.6
E. 125			11.2	5.0
E. 131			13.4	2.8
E. 160		±	15.5	0.7

π 74+00	5.1	11.8		6.7
E. 310			± 10.0	1.8
E. 248			4.9	6.9
E. 286			7.0	4.8
E. 300			9.1	2.7
E. 238			0.3	11.5
E. 226			3.8	8.0
E. 133			4.8	7.0
E. 58			5.2	6.6
W. 80			5.9	5.9
W. 300			5.7	6.1
W. 492			6.2	5.6
W. 620			5.2	6.6
W. 730			6.5	5.3
W. 752			6.1	5.7
W. 778			2.0	9.8
W. 788			5.0	6.8
W. 804			7.1	4.7

7-29-46 (29)

	+	HI	-	EI.
π 74 11816				8.1 3.7
π 75+00	5.0	12.3		7.3
W. 784				7.2 5.1
W. 820				8.9 3.4
W. 785				1.8 10.5
W. 763				4.6 7.7
W. 680				5.0 7.3
W. 602				5.5 6.8
W. 530				6.4 5.9
W. 465				6.1 6.2
W. 342				4.7 7.6
W. 230				3.2 9.1
W. 188				2.8 9.5
W. 78				5.3 7.0
E. 108				4.6 7.7
E. 180				4.9 7.4
E. 312				1.7 10.6
E. 352				2.7 9.6
E. 365				0.0 12.3
E. 372				5.4 6.9
E. 416				6.9 5.4
E. 430				9.2 3.1

	+	HI	-	EI.
\bar{X} 76+00	5.1	15.1		10.0
E. 512			9.9	5.2
E. 480			7.8	7.3
E. 470			3.9	11.2
E. 463			5.0	10.1
E. 330			6.5	8.6
E. 210			5.3	9.8
<u>E. 102</u>			5.4	9.7
W 37			4.2	10.9
W 100			5.9	9.2
W 155			5.2	9.9
W 242			4.5	10.6
W 278			5.3	9.8
W 366			7.5	7.6
W 473			8.7	6.4
W 522			8.5	6.6
W 620			6.5	8.6
W 670			4.2	10.9
W 730			4.8	10.3
W 790			8.7	6.4
W 860			12.2	2.9
\bar{X} 77+00	4.9	15.5		10.6
W 680			6.3	9.2
W 740			5.3	10.2

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15.5

(30)

(77)	+	HI	-	Elev.
W 823			9.3	6.2
W 960			12.2	3.3
W 606			7.2	8.3
W 480			8.4	7.1
W 430			9.1	6.4
W 335			6.5	9.0
W 222			4.6	10.9
<u>W 80</u>			4.8	10.7
E 60			7.5	8.0
E 70			10.7	4.8
E 108			12.4	3.1
E 144			12.5	3.0
E 134			14.5	1.0
E 212			8.1	7.4
E 224			4.5	11.0
E 285			4.3	11.2
E 384			4.1	11.4
E 480			3.2	12.3
E 542			4.5	11.0
E 553			2.8	12.7
E 562			8.0	7.5
E 606			12.5	3.0
\bar{X} 78+00	4.7	15.5		10.8
E 620			3.7	11.8

(278)

15.5

+

HI

-

ELEV.

EG30

8.7

6.8

E666

12.8

2.7

E612

5.7

9.8

E548

3.3

12.2

E430

5.7

9.8

E418

3.6

11.9

E400

10.1

5.4

E388

11.4

4.1

E345

12.7

2.8

*
BOAT BASIN
± 8

E106

12.6

2.9

E48

9.4

6.1

E28

4.1

11.4

E17

5.0

10.5

W52

4.8

10.7

W162

4.1

11.4

W260

6.8

8.7

W338

8.9

6.6

W419

10.8

5.5

W500

8.9

6.6

W595

6.7

8.8

W704

5.8

9.7

T79+00

4.98

15.3

10.3

W680

5.1

10.2

W560

5.6

9.7

W493

6.9

8.4

7-29-46

(279)

+

HI
15.3

-

Elev.

W416

8.6

6.7

W340

9.5

5.8

W266

8.4

6.9

W214

8.1

7.2

W95

4.8

10.5

W62

3.9

11.4

E19

5.3

10.0

E27

2.8

12.5

E43

7.5

7.8

E165

10.9

4.4

E130

12.9

2.4

steep bank.

T80+00

4.9

14.1

9.2

E114

11.1

3.0

E53

9.2

4.9

E34

2.0

12.1

E17

4.6

9.5

W40

5.6

8.5

W78

6.5

7.6

W192

6.0

8.1

W330

7.8

6.3

W370

7.0

2.1

W464

5.5

8.6

W530

4.2

9.9

W680

3.8

10.3

	+	#	-	E1.
π 81400	4.25	15.64		11.39
E. 164			5.1	10.5
E. 230			5.9	9.7
E. 360			8.3	7.3
E 440			7.6	8.0
E 540			6.3	9.3
E. 654			4.2	11.4
E 730			6.0	9.6
E. 740			3.2	12.4
E 760			11.2	14.4
E 810			12.7	2.9

π 82200	4.39	15.78		11.39
E 790			5.4	10.4
E 860			11.9	3.9
E 900			11.8	4.0
E 736			4.2	11.6
E. 630			4.9	10.9
E. 510			7.2	8.6
E 410			7.9	7.9
E 272			5.5	10.3
E. 172			4.7	11.1
0			5.0	10.3

7/30/46

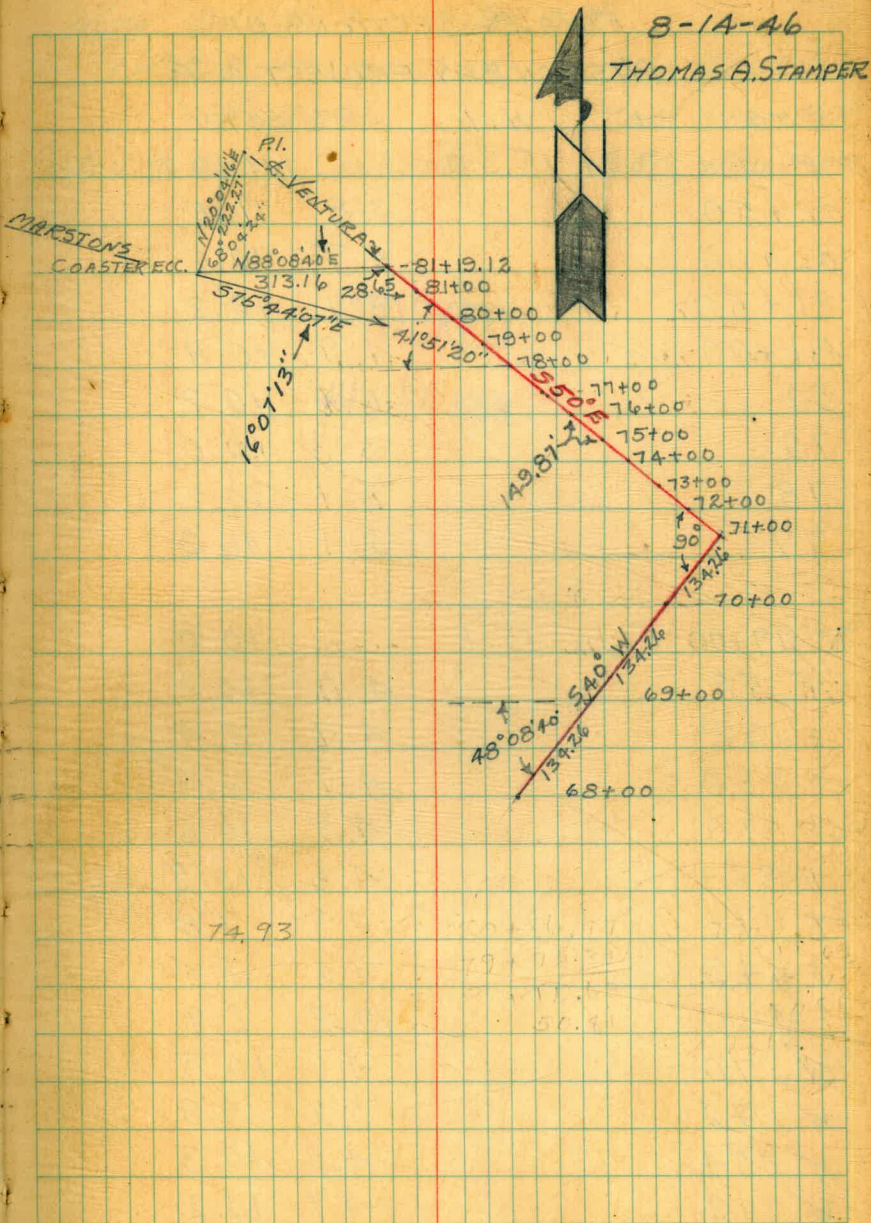
(32)

Old BL

BASELINE LAYOUT FOR
FINAL X-SECTIONS OF
MISSION BAY PROJECT NO. A-"A"

OFFSET STATIONS & RANGES 313.16' E. OF

STA	RANGE	DIST	EAST	WEST
81+19.12	79+54		313.16	
81+00	79+75.34		313.16	
80	80+86.97		313.16	
79	81+98.60		313.16	
78	83+10.20		313.16	
77	84+21.86		313.16	
76	85+33.49		313.16	
75	86+45.12		313.16	
74	87+56.75		313.16	
73	88+68.38		313.16	
72	89+80		313.16	
71	90+91.64		313.16	
70	90+02.05		111.94	
69	89+12.46			89.28
68	88+22.87			290.50
67	87+33.28			491.72
82+00	78+63.71			
82+50	78+12.90			
82+72	77+88.34			
83+00	77+52.08			



FINAL X-SECTIONS OF
MISSION BAY PROJECT 4-"A"

STA.	+	H.I.	-	ELEV
B.M.	3.91	15.30		11.39
82+50			3.8	11.5
82+00			4.7	10.6
81+50			5.1	10.2
81+00			4.9	10.4
80			5.1	10.2
79			5.3	10.0
78			5.1	10.2
77			5.1	10.2
79+00	5.1	15.1		10.0
E 58			4.9	10.2
E 132			4.7	10.4
E 230			4.7	10.4
E 310			4.5	10.6
E 368			4.6	10.5
E 412			7.3	7.8
E 443			9.6	5.5
E 490			12.2	2.9
W 70			4.6	10.5
W 170			5.2	9.9
W 254			4.8	10.3
W 312			4.9	10.2

NOTE: SEE B/L SKETCH (PG. 34)

INST. BUFFA BERGER
No. 2091
U.S.C. & G.S. A COASTER

TOM ALLEN
TOM STAMPER
GEO. WILLIAMS

INDEXED

JUL 16 1953

8/21/46

Sta	+	H.I.	-	Elev
$\bar{\Lambda}$ 79 cont.		15.1		
W 410			4.9	10.2
W 500			4.9	10.2
W 542			4.7	10.4
<u>W 568</u>			4.1	11.0
$\bar{\Lambda}$ 80+00	5.1	15.3		10.2
W 460			3.9	11.4
W 436			4.4	10.9
W 383			5.2	10.1
W 322			5.2	10.1
W 262			5.0	10.3
W 190			5.2	10.1
W 119			5.2	10.1
<u>W 34</u>			5.1	10.2
E. 124			4.9	10.4
E. 221			4.8	10.5
E. 350			4.7	10.6
E. 373			5.2	10.1
E. 439			9.6	5.7
<u>E 470</u>			12.0	3.3
$\bar{\Lambda}$ 81+00	5.0	15.4		10.4
E. 500			12.5	12.9
E 466			10.2	5.2

(36)

	+	H.I.	-	Elev.
81+00 Cont.		15.4		
E. 398			4.8	10.6
E. 340			4.5	10.9
E. 218			5.2	10.2
<u>E 100</u>			5.2	10.2
W 96			4.9	10.5
W. 218			5.0	10.4
<u>W. 322</u>			4.2	11.2
$\bar{\Lambda}$ 82+00	5.1	15.6		10.6
W 263			4.8	10.8
W 208			4.7	10.9
<u>W 79</u>			4.6	11.0
E. 102			5.0	10.6
E. 231			5.3	10.3
E. 390			5.1	10.5
E 505			4.4	11.2
E 543			5.4	10.2
E 605			10.4	5.2
<u>E 640</u>			12.8	2.8
82+50	5.0	16.5		11.5
E. 760			13.4	3.1
E 700			10.9	4.7

8-26-44

STA.	+	H.I.	-	ELEV.
B.M.	5.03	16.42		11.39
TP.			5.57	10.85
	5.05	15.90		

630E

82+72		5.0	10.9
44E		5.1	10.8
98E		9.1	6.8
125E		11.1	4.8
164E		12.1	3.8

630E

83+00	5.13	15.98	10.85
-		11.7	
220E		11.9	4.1
233E		11.9	4.1
180E		9.9	6.1
118E		4.8	11.2
65E		4.9	11.1
0		4.8	11.2

EAST

83+00	-	732
82+50	-	630
82+00	-	533
81+00	-	400
80+00	-	370
79+00	-	370
78+00	-	370

630E

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U.S.C. & G.S. COASTER

8/27/46

STA 82+50 (630' EAST)

DIST		SOUND		DIST		SOUND	
(9:05)	(3.2)						
E 119	0.0	W.S. + 3.7	350	10.0	-6.2		
130	1.0	+2.7	360	10.0	-6.2		
140	2.0	+1.7	370	10.1	-6.3		
(3.7) 150	3.8	-0.1	380	10.7	-6.9		
160	6.0	-2.3	390	10.6	-6.8		
170	6.8	-3.1	400	10.6	-6.8		
180	7.0	-3.3	410	10.5	-6.7		
190	9.2	-5.5	420	10.3	-6.5		
200	10.0	-6.3	430	10.0	-6.2		
210	10.7	-7.0	440	9.7	-5.9		
220	10.7	-7.0	450	10.9	-7.1		
(9:10) 230	10.7	-7.0	460	12.9	-9.1		
240	10.7	-7.0	470	12.9	-9.1		
250	10.2	-6.5	480	12.5	-8.7		
260	10.0	-6.3	490	12.1	-8.3		
270	10.5	-6.8	500	12.0	-8.2		
(3.8) 280	11.7	-7.9	510	11.8	-8.0		
290	12.1	-8.3	520	11.6	-7.8		
300	12.2	-8.4	530	11.3	-7.5		
310	12.1	-8.3	540	12.0	-8.2		
320	11.0	-7.2	550	14.1	-10.3		
330	10.5	-6.7	560	14.3	-10.5		
340	10.3	-6.5	570	14.3	-10.5		

Dist.		Sound		El.		Dist.		Sound	
(9:15)				82+50	Contd.				
580	14.2	-10.3	820	11.9	-8.0				
590	15.2	-11.3	830	11.6	-7.7				
600	14.8	-10.9	840	11.7	-7.8				
610	14.0	-10.1	850	(9:20) 11.6	-7.6				
620	13.3	-9.4	860	11.3	-7.3				
630	12.6	-8.7	870	11.2	-7.2				
640	12.3	-8.4	880	11.6	-7.6				
650	12.8	-8.9	890	12.1	-8.1				
660	13.9	-10.0	900	12.2	-8.2				
670	15.0	-11.1	910	12.1	-8.1				
680	14.3	-10.4	920	12.7	-8.7				
690	13.0	-9.1	930	13.0	-9.0				
(9:25) 700	13.1	-9.2	940	14.1	-10.1				
710	13.1	-9.2	950	13.8	-9.8				
720	13.6	-9.7	960	14.0	-10.0				
730	13.3	-9.4	970	14.0	-10.0				
740	12.1	-8.2	980	12.0	-8.0				
750	11.3	-7.4	990	9.0	-5.0				
760	11.3	-7.4	1000	3.0	+1.0				
770	12.0	-8.1	(9:30)						
780	12.0	-8.1							
790	12.0	-8.1							
800	11.7	-7.8							
810	11.7	-7.8							

Dist. Sound El. Dist. Sound El.
83+00 8/27/46 (732 East)

Dist.	Sound	El.	Dist.	Sound	El.	
(9.43)						
105	0.0	+4.2	340	11.0	-6.8	
110	0.2	+4.0	350	11.6	-7.4	
120	0.8	+3.4	360	12.1	-7.9	
130	4.1	+0.1	370	11.6	-7.4	
140	6.8	-2.6	380	10.7	-6.5	
150	7.0	-2.8	390	10.6	-6.4	
160	9.0	-4.8	400	10.5	-6.3	
170	9.3	-5.1	410	10.2	-6.0	
180	9.3	-5.1	420	10.3	-6.1	
(9.45)	190	10.9	-6.7	430	10.5	-6.3
200	10.9	-6.7	440	10.3	-6.1	
210	11.1	-6.9	450	11.1	-6.9	
220	11.4	-7.2	460	11.8	-7.6	
230	11.5	-7.3	470	12.0	-7.8	
240	11.3	-7.1	480	12.2	-8.0	
250	11.2	-7.0	490	12.4	-8.2	
(9.47)	260	11.4	-7.2	500	11.5	-7.3
270	11.8	-7.6	510	11.1	-6.9	
280	12.0	-7.8	520	11.8	-7.6	
290	12.5	-8.3	530	11.7	-7.5	
300	10.3	-6.1	540	11.5	-7.3	
310	8.5	-4.3	550	11.9	-7.7	
320	9.2	-5.0	560	14.5	-10.3	
330	10.2	-6.0	570	14.6	-10.4	

(20)

Dist.	Sound	Dist.	Sound
(9.50)		830	12.8 - 8.4
580	14.7 -10.4	840	13.0 -8.6
590	14.8 -10.5	850	12.9 -8.5
600	14.1 -9.8	860	12.5 -8.1
610	14.0 -9.7	870	12.5 -8.1
620	14.0 -9.7	880	12.7 -8.3
630	14.0 -9.7	890	13.0 -8.6
640	13.0 -8.7	900	13.2 -8.8
650	12.1 -7.8	910	12.1 -8.7
660	13.2 -8.9	920	8.1 -3.7
670	13.6 -9.3	930	3.0 +1.1
680	13.3 -9.0	940	1.9 +2.5
690	12.6 -8.3	950	1.0 +3.4
700	12.4 -8.1		
710	12.7 -8.4		
720	11.4 -7.1		
730	11.6 -7.3		
740	11.7 -7.4		
750	11.9 -7.6		
770	11.8 -7.5		
780	11.9 -7.6		
790	12.1 -7.8		
800	12.6 -8.3		
810	12.7 -8.4		
820	12.8 -8.5		

8/27/06

Dist	Sound		Dist	Sound	
82	0.0	+4.5	320	13.6	-9.1
90	0.3	+4.3	330	13.6	-9.1
100	0.4	+4.1	340	13.5	-9.0
110	0.8	+3.7	350	11.8	-7.3
120	1.8	+2.7	360	11.2	-6.7
130	6.0	-1.5	370	11.0	-6.5
140	6.8	-2.3	380	11.0	-6.5
150	6.8	-2.3	390	11.3	-6.8
160	7.2	-2.7	400	11.5	-7.0
170	8.0	-3.5	410	11.3	-6.8
180	8.9	-4.4	420	11.0	-6.5
190	9.5	-4.7	430	10.6	-6.1
200	9.2	-4.7	440	10.6	-6.1
210	9.8	-5.3	450	11.0	-6.5
220	10.0	-5.5	460	11.1	-6.6
230	10.2	-5.7	470	11.7	-7.2
240	10.3	-5.8	480	13.5	-9.0
250	11.1	-6.6	490	13.0	-8.5
260	11.3	-6.8	500	13.2	-8.7
270	12.2	-7.7	510	13.0	-8.5
280	12.5	-8.0	520	12.9	-8.4
290	12.4	-7.9	530		
300	12.7	-8.2	540		
310	13.1	-8.6	550	12.5	-8.0

(41)

Dist	Sound		Dist	Sound	
560	12.8	-8.3	800	14.9	-10.3
570	15.2	-10.6	810	14.0	-9.4
580	15.6	-11.0	820	13.1	-8.5
590	15.0	-10.4	830	13.2	-8.6
600	14.7	-10.1	840	13.2	-8.6
610	13.8	-9.2	850	13.1	-8.5
620	15.2	-10.6	860	13.0	-8.4
630	16.5	-11.9	870	12.9	-8.3
640	17.0	-12.4	880	12.2	-7.6
650	16.0	-11.4	890	11.9	-7.3
660	14.2	-9.6	900	11.9	-7.3
670	14.0	-9.4	910	12.2	-7.6
680	14.3	-9.7	920	12.3	-7.7
690	14.3	-9.7	930	12.5	-7.9
700	14.0	-9.4	940	12.2	-7.6
710	14.5	-9.9	950	12.0	-7.4
720	14.7	-10.1	960	12.4	-7.8
730	14.8	-10.2	970	12.8	-8.2
740	14.3	-9.7	980	13.2	-8.6
750	14.0	-9.4	990	13.6	-9.0
760	15.0	-10.4	1000	14.2	-9.6
770	15.9	-11.3	1010	14.3	-9.7
780	15.3	-10.7	1020	14.3	-9.7
790			1030	13.0	-8.4

Dist.	Sound	Dist.	Sound
<u>10:35</u>			
1040	12.8 - 8.2	190	11.0 - 6.4
1050	12.0 - 7.4	200	10.9 - 6.3
1060	10.0 - 5.4	210	10.9 - 6.3
1070	5.8 - 1.2	220	10.9 - 6.3
1080	2.8 + 1.8	230	11.1 - 6.5
1090	2.2 + 2.4	240	11.2 - 6.6
1100	2.3 + 2.3	250	11.9 - 7.3
<u>10:40</u>		260	11.5 - 6.9
<u> </u>		270	13.1 <u>10:50</u> 8.5
		280	13.4 - 8.8
(400 East)		290	13.2 - 8.6
81400 <u>10:45</u>		300	12.9 - 8.3
73	0.0 + 4.6	310	12.7 - 8.1
80	0.6 + 4.0	320	12.8 - 8.2
90	0.6 + 4.0	330	13.0 - 8.4
100	1.5 + 3.1	340	13.9 - 9.3
110	1.8 + 2.8	350	14.0 - 9.4
120	4.0 + 0.6	360	13.5 - 8.9
130	6.5 - 1.9	370	12.9 - 8.3
140	7.0 - 2.4	380	12.8 - 8.2
150	8.5 - 3.9	390	13.0 - 8.4
160	7.9 - 3.3	400	14.0 - 9.4
170	8.8 - 4.2	410	13.5 <u>11:00</u> 8.9
180	9.9 - 5.3	420	14.0 - 9.3

(42)

Dist.	Sound	Dist.	Sound	El.
430	13.5 - 8.8	680	14.8 <u>11:15</u> - 10.1	
440	14.0 - 9.3	690	14.9 - 10.2	
450	13.5 - 8.8	700	14.8 - 10.1	
460	13.1 - 8.4	710	14.0 - 9.3	
470	12.8 - 8.1	720	13.5 - 8.8	
480	12.6 <u>11:12</u> - 7.9	730	12.9 - 8.2	
490		740	12.4 - 7.7	
500	12.2 - 7.5	750	12.8 - 8.1	
510	12.0 - 7.3	760	13.0 - 8.3	
520	13.3 - 8.6	770	13.1 - 8.4	
530	13.0 - 8.3	780	14.2 - 9.5	
540	13.5 - 8.8	790	14.1 - 9.4	
550	12.9 - 8.2	800	14.9 - 10.2	
560	14.0 - 9.3	810	14.3 - 9.6	
570	14.1 - 9.4	820	14.3 - 9.6	
580	15.0 - 10.3	830	14.3 - 9.6	
590	15.0 - 10.3	840	14.3 - 9.6	
600	15.0 - 10.3	850	14.9 - 10.2	
610	14.4 - 9.7	860	14.8 - 10.1	
620	14.2 - 9.5	870	14.6 - 9.9	
630	14.7 - 10.0	880	14.1 - 9.4	
640	15.5 - 10.8	890	13.8 - 9.1	
650	15.6 - 10.9	900	13.3 - 8.6	
660	15.5 - 10.8	910	13.1 - 8.4	
670	15.2 - 10.5	920	13.0 - 8.3	

Dist	Sound	Dist	Sound
(11:20)		1170	4.2 +0.5
930	12.8 -8.1	1180	3.2 +1.5
940	12.6 -7.9	1190	2.8 +1.9
950	12.2 -7.5	1200	2.3 +2.4
960	12.1 -7.4	(11:22)	
970	11.9 -7.2		
980	11.9 -7.2		
990	12.0 -7.3		
1000	12.8 -8.1		
1010	13.1 -8.4	(370 East)	
1020	13.1 -8.4	80+00 (11:35)	
1030	13.0 -8.3	84	0.0 +4.6
1040	12.8 -8.1	90	0.6 +4.0
1050	13.0 -8.3	100	0.6 +4.0
1060	13.3 -8.6	110	2.8 +1.8
1070	13.4 -8.7	120	3.8 +0.8
1080	13.5 -8.8	130	5.3 -0.7
1090	13.0 -8.3	140	5.1 -0.5
1100	13.0 -8.3	150	4.5 +0.1
1110	13.2 -8.5	160	5.1 -0.5
1120	13.2 -8.5	170	8.5 -3.9
1130	12.0 -7.3	180	10.2 -5.6
1140	8.0 -3.3	190	11.0 -6.4
1150	6.1 -1.4	200	11.2 -6.6
1160	5.3 -0.6	210	11.9 -7.3
		220	11.1 -6.5

8/7/46

(43)

Dist	Sound	El.	Dist	Sound
230	11.5 -7.0		480	11.2 -6.7
240	12.2 -7.7		490	10.9 -6.4
250	12.6 -8.1		500	13.3 -8.8
260	12.5 -8.0		510	15.0 -10.5
270	12.0 -7.5		520	15.1 -10.6
280	13.0 -8.5		530	15.6 -11.1
290	13.9 -9.4		540	15.6 -11.1
300	14.1 -9.6		550	15.0 -10.5
310	14.3 -9.8		560	15.0 -10.5
320	14.1 -9.6		570	15.6 -11.1
330	13.2 -8.7		580	15.3 -10.8
340	13.7 -9.2		590	16.0 -11.5
350	13.0 -8.5		600	15.3 -10.8
360	12.7 -8.2		610	14.0 -9.5
370	12.5 -8.0		620	12.0 -7.5
380	13.1 -8.6		630	13.2 -8.7
390	14.1 -9.6		640	13.8 -9.3
400	14.9 -10.4		650	13.2 -8.7
410	14.9 -10.4		660	12.0 -7.5
420	14.5 -10.0		670	11.5 -7.0
430	14.3 -9.8		680	11.6 -7.1
440	13.0 -8.5		690	11.7 -7.2
450	12.0 -7.5		700	12.0 -7.5
460	11.9 -7.4		710	11.9 -7.4
470	11.9 -7.4		720	11.8 -7.3

8/27/66

(49)

Dist.	Sound	El.	Dist.	Sound	El.
730	12.1	11.50 -7.6	970	12.5	-8.1
740	11.9	-7.4	980	12.4	-8.0
750	11.9	-7.4	990	12.2	-7.8
760	12.3	-7.8	1000	13.0	-8.6
770	12.3	-7.8	1010	13.2	-8.8
780	12.3	-7.8	1020	14.9	-10.5
790	12.3	-7.8	1030	13.4	-9.0
800	12.2	-7.7	1040	12.8	-8.4
810	12.1	-7.6	1050	12.7	-8.3
820	12.5	-8.0	1060	11.9	-7.5
830	13.1	-8.6	1070	10.9	-6.5
840	13.5	-9.0	1080	9.3	-4.9
850	13.9	-9.4	1090	7.2	-3.8
860	13.8	-9.3	1080	5.2	-0.8
870	13.3	-8.8	1110	4.2	+0.2
880	13.5	-9.0	1120	3.0	+1.4
890	13.6	-9.1			
900	13.7	11.50 -9.2			
910	14.0	-9.5			
920	14.1	-9.6			
930	13.8	-9.3			
940	13.1	-8.6			
950	12.4	-7.9			
960	12.3	-7.8			

Dist.	Sound	El.	Dist.	Sound	El.
79400		(12:05) (370 East)			(2:10)
92	0.0	+4.3	330	12.8	-8.5
100	0.1	+4.2	340	12.3	-8.0
110	0.8	+3.5	350	12.3	-8.0
120	1.0	+3.3	360	12.2	-7.9
130	2.2	+2.1	370	12.1	-7.8
140	6.0	-1.7	380	12.7	-8.4
150	6.9	-2.6	390	13.4	-9.1
160	8.9	-4.6	400	13.5	-9.2
170	11.2	-6.9	410	13.0	-8.7
180	12.1	-7.8	420	12.5	-8.2
190	13.3	-9.0	430	11.5	-7.2
200	13.8	-9.5	440	11.8	-7.5
210	13.7	-9.4	450	11.9	-7.6
220	14.1	-9.8	460	13.1	-7.8
230	14.3	-10.0	470	13.3	-8.0
240	14.8	-10.5	480	12.3	-7.0
250	14.6	-10.3	490	9.8	-5.5
260	14.6	-10.3	500	9.4	-5.1
270	14.0	-9.7	510	8.8	-4.5
280	13.3	-9.0	520	7.2	-2.9
290	13.5	-9.2	530	5.3	-1.0
300	12.8	-8.5	540	3.4	+0.9
310	12.5	-8.2	550	3.5	+0.8
320	12.9	-8.6	560	3.2	+1.1

Dist.	Sound	Dist.	Sound
570	2.5 +1.7	810	13.2 -9.0
580	2.5 +1.7	820	14.0 -9.8
590	2.5 +1.7	830	13.5 -9.3
600	2.4 +1.8	840	13.1 -8.9
610	2.5 +1.7	850	13.2 -9.0
620	2.6 +1.6	860	14.0 -9.8
630	2.6 +1.6	870	13.9 -9.7
640	2.8 +1.4	880	13.7 -9.5
650	2.9 +1.3	890	13.3 -9.1
660	2.8 +1.4	900	13.0 -8.8
670	3.1 +1.1	910	12.9 -8.7
680	3.8 +0.4	920	13.2 -9.0
690	3.3 +0.9	930	13.2 -9.0
700	3.2 +1.0	940	13.2 -9.0
710	3.3 +0.9	950	13.5 -9.3
720	3.2 +1.0	960	13.8 -9.6
730	3.1 +1.1	970	14.0 -9.8
740	2.3 +1.9	980	14.8 -10.6
750	3.1 +1.1	990	15.1 -10.9
760	5.9 -1.7	1000	15.5 -11.3
770	7.1 -2.9	1010	15.0 -10.8
780	10.9 -6.7	1020	14.3 -10.1
790	11.8 -7.6	1030	13.0 -9.8
800	12.6 -8.4	1040	9.9 -5.7

4.2

8/27/46 (45)

Dist.	Sound	El.	Dist.	Sound	El.
1050	4.0	+0.2			
1060	3.1	+1.1	250	13.1	-9.1
1070	2.6	+1.6	260	12.2	-8.2
1080	2.7	+1.5	270	11.1	-7.1
			280	8.2	-4.2
			290	8.2	-4.2
			300	7.3	-3.3
(370 East)			310	6.3	-2.3
78+00	(12:30)		320	5.3	-1.3
95	0.0	+4.1	330	4.4	-0.4
100	0.2	+3.9	340	1.9	+2.1
110	0.8	+3.3	350	1.0	+3.0
120	1.6	+2.5	360	0.3	+3.7
130	2.0	+2.1	364	0.0	+4.0
140	1.9	+2.2			
150	2.3	+1.8			
160	5.1	-1.0			
170	9.8	-5.7			
180	12.0	-7.9			
190	12.3	-8.2			
200	11.8	-7.7			
210	14.3	-10.2			
220	14.2	-10.1			
230	14.0	-9.9			
240	14.1	-10.0			

(12:36)

3.6 @ 1:12 ✓

STA.	+	H.I.	-	ELEV
		EAST		
83+50	-	1,010		
84+00		1,080		
85+00		1,220		
(1,010E)				
83+50	5.37	16.22		10.85
0			4.8	11.4
11E			5.4	10.8
52E			9.4	6.8
89E			12.0	4.2
118E			12.2	4.0
129E			13.7	2.5
TP.			9.28	6.94
(1,080E)				
84+00	9.42	16.36		
114E			13.4	3.0
107E			12.2	4.2
82E			12.2	4.2
57E			9.8	6.6
14E			6.0	10.4
0			4.9	11.5
(1,220E)				
85+00	9.18	16.12		6.94
116E			13.0	3.1
90E			12.0	4.1
78E			11.3	4.8
54E			9.6	6.5
15E			6.2	9.9
0			4.8	11.3

112.68
56.34

(46)

169.02

82 - 56.34
85 - 112.68
2 112.68
86 - 281.70
112.68
87 394.38

See TP. (Pg. 38)

85 - 112.68
84 - 112.68
225.36

8/29/46

Dist	Sound	Dist	Sound
8:12 AM (+2.8)			
83+50	(8:25) (3.0)	350	10.4 -7.3
128	0.0 +3.0	360	8.7 -5.6
130	1.0 +2.0	370	8.8 -5.7
140	3.2 -0.1	380	8.8 -5.7
150	5.7 -2.7	390	8.8 -5.7
160	6.7 -3.7	400	8.5 -5.4
170	7.1 -4.1	410	8.2 -5.1
180	8.8 -5.8	420	9.2 -6.1
190	10.0 -7.0	430	10.2 -7.1
200	10.5 -7.5	440	10.3 -7.2
210	10.8 -7.8	450	10.6 -7.5
220	10.4 -7.4	460	10.9 -7.8
230	10.1 -7.1	470	10.9 -7.8
240	10.3 -7.3	480	10.5 -7.4
250	11.0 -8.0	490	10.1 -7.0
260	10.3 -7.3	500	10.8 -7.7
270	10.7 -7.7	510	10.3 -7.2
280	9.1 -6.1	520	11.7 -8.6
290	7.9 -4.9	530	12.3 -9.2
300	(8:30) 8.5 (3.1) -5.4	540	12.2 -9.1
310	9.5 -6.4	550	12.1 -9.0
320	10.9 -7.8	560	11.9 -8.8
330	11.0 -7.9	570	11.7 -8.6
340	11.3 -8.2	580	11.9 -8.8

(8:35) (3.1)

(47)

Dist	Sound	Dist	Sound
8:35			
590	11.2 -8.1	830	11.3 -8.2
600	12.3 -8.2	840	11.2 -8.1
610	12.5 -8.4	850	10.0 -6.9
620	12.1 -9.0	860	5.5 -2.4
630	10.8 -7.7	870	1.0 +2.1
640	11.2 -8.1	(8:40) (3.1)	
650	10.8 -7.7		
660	10.9 -7.8		
670	11.1 -8.0		
680	11.2 -8.1	84400	(8:45) (3.2)
690	11.1 -8.0	117	0.0 +3.2
700	11.1 -8.0	120	0.4 +2.8
710	11.0 -7.9	130	2.8 +0.4
720	10.6 -7.5	140	4.9 -1.7
730	10.8 -7.7	150	6.4 -3.2
740	10.9 -7.8	160	7.0 -3.8
750	10.8 -7.7	170	7.6 -4.4
760	11.1 -8.0	180	9.3 -6.1
770	11.2 -8.1	190	11.1 -7.9
780	11.2 -8.1	200	11.9 -8.7
790	11.3 -8.2	210	11.3 -8.1
800	11.6 -8.5	220	11.2 -8.0
810	11.7 -8.6	230	11.5 -8.3
820	11.5 -8.4	240	11.1 -7.9

(8:50) (3.2)

8/19/46

Dist	Sound		Dist	Sound	
250	11.1	-7.9	500	10.9	-7.6
260	11.3	-8.1	510	11.1	-7.8
270	10.6	-7.4	520	10.9	-7.6
280	9.6	-6.4	530	11.8	-8.5
290	10.0	-6.8	540	12.0	-8.7
300	10.1	-6.9	550	12.3	-9.0
310	10.0	-6.8	560	12.1	-8.8
320	10.0	-6.8	570	12.1	-8.8
330	9.0	-5.8	580	11.9	-8.6
340	8.3	-5.1	590	11.3	-8.0
350	8.3	-5.1	600	11.5	-8.2
360	8.7	-5.5	610	12.1	-8.8
370	8.8	-5.6	620	11.9	-8.6
380	8.5	-5.3	630	12.0	-8.7
390	9.9	-6.7	640	12.3	-9.0
400	10.2	-7.0	650	12.2	-8.9
410	10.3	-7.1	660	11.9	-8.6
420	10.4	-7.2	670	11.7	-8.4
430	11.2	-8.0	680	11.5	-8.2
440	11.3	-8.1	690	11.3	-8.0
450	11.0	-7.8	700	11.2	-7.9
460	11.0	-7.8	710	10.7	-7.4
470	10.8	-7.6	720	11.1	-7.8
480	10.4	-7.2	730	11.4	-8.1
490	10.3	-7.1			

(48)

Dist.	Sound	El.	Dist.	Sound	El.
740	11.3	-8.0	200	10.5	-7.1
750	11.5	-8.2	210	10.4	-7.0
760	13.2	-9.9	220	10.2	-6.8
770	14.8	-11.5	230	9.1	-5.7
780	13.2	-9.9	240	9.8	-6.4
790	9.8	-6.5	250	10.0	-6.6
800	2.8	+0.5	260	10.2	-6.8
810	1.0	+2.3	270	10.9	-7.5
9.00 AM	(3.3)		280	11.2	-7.8
820	0.4		290	11.2	-7.8
			300	11.1	-7.7
			310	11.0	-7.6
			320	10.9	-7.5
			330	11.2	-7.7
85+00	(3.4)		340	11.4	-7.9
118	0.0	+3.4	350	12.0	-8.5
120	0.7	+2.7	360	11.5	-8.0
130	4.0	-0.6	370	12.0	-8.5
140	6.2	-2.8	380	13.2	-9.7
150	7.6	-4.2	390	12.8	-9.3
160	10.6	-7.2	400	10.3	-6.8
170	11.0	-7.6	410	11.1	-7.6
180	11.0	-7.6	420	11.4	-7.9
190	10.8	-7.4	430	11.5	-8.0
			9:15	(3.5)	

Dist Sound

(9:15) (3.5)

440	11.5	-8.0	680	3.2	+0.3
450	11.5	-8.0	690	3.2	+0.3
460	11.8	-8.3	700	3.8	+0.3
470	11.9	-8.4	710	2.0	+1.5
480	11.8	-8.3	720	0.6	+2.9
490	11.5	-8.0	725	0.0	
500	11.5	-8.0			
510	11.5	-8.0			
520	11.6	-8.1			
530	11.4	-7.9			
540	11.8	-8.3			
550	12.1	-8.6	Sounding @ 83+00		
560	12.0	-8.5	to find high Point		
570	11.5	-8.0	(9:35 AM)	(3.7)	
580	11.3	-7.8	300	4.8	
590	11.1	-7.6	310	2.2	+1.5 on line
600	10.3	-6.8	310	4.3	50 So.
610	10.4	-6.9	320	4.9	50 So.
620	10.9	-7.4	320	4.1	25 So.
630	11.2	-7.7	320	3.9	-0.2 miles
640	11.5	-8.0	320	3.5	15 No.
650	12.2	-8.7	320	3.2	25 No.
660	13.0	-9.5	320	3.1	35 No.
670	11.9	-8.4	320	2.8 (3.8)	40 No.

(9:43 AM)

(4.0 10:00)

24 - 90° DIST

25 DEF. LT. 0° 56.80'

26 = 8° 69.59'

27 = 16° "

28 = 24° "

29 = 32° "

30 = 40° 24' 05" 73.05 E.C.

31 = 40° 24' 05" 160'

32 = TAN 200'

33 = " 240'

34 = " 160'

STA OBJ. ANGLE CHORD.

ELCARNEL

"A"

10

9

8

7

6

5

10

5

4

3

2

1

INT. RT.

PRC.

98° 42' 23"

107° 42' 23"

116° 42' 23"

125° 42' 23"

134° 42' 23"

44° 42' 23"

TAN

"

"

75.69'

78.22

"

"

" E.C.

118.41

150'

200'

200'

170° 12' 56"

15

34° 13' 14"

34° 13'

34° 12'

34° 11'

34° 10'

34° 13'

68' 13'

102' 13'

136' 13'

170' 13'

(49)

PROJECT 4-"A"
FINAL X-SECTIONS CONTD.

STA	+	H.I.	-	ELEV,
B.M.				11.39
	3.84	15.23		
79+00			5.3	9.9
78+00			5.0	10.2
77+00			5.1	10.1
76+00			4.7	10.5
75+00			5.4	9.8
74+00			4.5	10.7
73+00			4.1	11.1
72+00			4.2	11.0
TP 71+00			4.1	11.1
	5.0	16.1		
70+00			4.8	11.3
69+00			5.6	10.5
71+00	5.0	16.1		11.1
0			5.0	11.1
E 70			6.1	10.0
E 96			7.9	8.2
E 148			12.0	4.1
W 40			5.2	10.9
W 143			5.2	10.9
W 223			6.0	10.1
W 314			5.2	10.9
W 431			5.6	10.5

9-11-46

(50)

U.S.C. & G.S. COASTER

TOM STAMPER
GEO. WILLIAMS
PAPPY GREEN

CLEAR-COOL

STA	+	H.I.	-	ELEV.
		16.1		
W482			7.3	8.8
W523			11.6	4.5
π70+00	5.0	16.3		11.3
W381			11.3	5.0
W345			7.7	8.6
W281			5.1	11.2
W192			5.5	10.8
W152			6.2	10.1
W112			6.4	9.9
W109			5.5	10.8
W61			4.5	11.8
0	5.0		5.0	11.3
E52			5.1	11.2
E87			7.4	8.9
E122			10.0	6.3
E144			11.9	4.4
π69+00	4.8	15.3		10.5
E106			10.8	4.5
E76			9.0	6.3
E42			7.1	8.2
E14			5.1	10.2
0			4.8	10.5
W33			5.1	10.2

9-11-46 15.3 (51)

STA	+	H.I.	-	ELEV.
W80			4.8	10.5
W115			6.2	9.1
W155			7.1	8.2
W167			9.3	6.0
W193			10.8	4.5
* NOTE: USE STA 69 AREA SOUTH AS WEDGE FOR 25'				
π72+00	5.1	16.1		11.0
0			5.1	11.0
W65			5.5	10.6
W154			5.6	10.5
W202			4.5	11.6
W286			5.2	10.9
W360			5.6	10.5
W410			7.0	9.1
W450			11.1	5.0
E81			4.5	11.6
E156			3.0	13.1
E201			2.1	14.0
E228			5.0	11.1
E280			7.2	8.9
E310			9.4	6.7
E332			11.5	4.6

STA	+	H. I.	-	ELEV
T73+00	5.2	16.3		11.1
0			5.2	11.1
W 54			4.8	11.5
W114			5.1	11.2
W 230			6.3	10.0
W 343			6.0	10.3
W 398			7.7	8.6
W 446			11.2	5.1
E 67			4.7	11.6
E 192			3.9	12.4
E 261			2.4	13.9
E 304			1.2	15.1
E 350			0.8	15.5
E 388			1.2	15.1
E 408			4.7	11.6
E 462			8.1	8.2
E 490			11.5	4.8

T74+00	5.1	15.8		10.7
W 87			5.6	10.2
W 174			5.4	10.4
W 300			5.5	10.3
W 370			5.8	10.0
W 418			8.4	7.4
W 450			10.9	4.9

STA	+	H. I.	-	ELEV.	
E 41			4.3	11.5	
E 83			3.1	12.7	
E 132			4.0	11.8	
E 181			3.8	12.0	
E 243			3.0	12.8	
E 308			2.2	13.6	
E 380			0.9	14.9	
E (415)	4.9	20.6	0.1	15.7	T.P.
E 447			4.5	16.1	
E 490			4.4	16.2	
E 520			5.0	15.6	
E 553			10.3	10.3	
E 591			10.8	9.8	
E 620			13.7	6.9	
E 639			15.2	5.4	
T. 75+00	5.1	14.9		9.8	
W 58			4.8	10.1	
W 134			4.7	10.2	
W 213			4.8	10.1	
W 310			4.4	10.5	
W 360			4.7	10.2	
W 405			7.3	7.6	
W 445			10.0	4.9	
E 58			4.8	10.1	

STA	+	14.9 H. I.	-	ELEV.	
E 143			4.3	10.6	
E 179			4.0	10.9	
E 210			1.9	13.0	
E 250			1.7	13.2	
E (301)	5.0	19.4	0.5	14.4	T. P.
E 344			4.3	15.1	
E 411			3.5	15.9	
E 465			3.2	16.2	
E 523			2.5	16.9	
E 567			1.3	18.1	
E 601			0.9	18.5	
E 625			3.0	16.4	
E 649			5.8	13.6	
E 670			9.2	10.2	
E 719			9.6	9.8	
E 745			12.5	6.9	
E 773			14.4	5.0	
K 76+00	5.1	15.6		10.5	
W 52			5.4	10.2	
W 148			5.4	10.2	
W 250			5.2	10.4	
W 342			5.7	9.9	
W 376			5.7	9.9	
W 410			7.8	7.8	

STA	+	²³⁶ 15.6 H. I.	-	ELEV.	
W 448			10.8	4.8	
E 86			5.6	10.0	
E 233			5.4	10.2	
E 341			5.5	10.1	
E 411			5.6	10.0	
E 443			5.0	10.6	
E (470)	4.3	19.8	0.1	15.5	T. P.
E 484			2.2	17.6	
E 500			2.0	17.8	
E 590			1.2	18.6	
E 636			1.5	18.3	
E 690			1.5	18.3	
E 720			4.1	15.7	
E 752			8.8	11.0	
E 802	5.0	15.6	9.2	10.6	
E 820			5.9	9.7	
E 842			7.7	7.9	
E 862			9.8	5.8	
E 879			17.0	4.6	
K 77+00	5.0	15.1		10.1	
W 72			4.9	10.2	
W 168			4.8	10.3	
W 270			5.2	9.9	
W 362			5.4	9.7	

STA	+	15.1 H. I.	-	ELEV.
W 396			5.9	9.2
W 440			8.1	7.0
W 490			10.0	5.1
W 532			11.4	3.7
W 600			11.7	3.4
E 42			4.9	10.2
E 150			4.9	10.2
E 280			4.9	10.2
E 375			5.1	10.0
E 410			7.2	7.9
E 450			10.0	5.1
E 482			11.9	3.2
E 537			10.6	4.5
E 572			8.0	7.1
E 610			5.3	9.8
E 710			4.7	10.4
E 823			4.5	10.6
E 880			4.5	10.6
E 910			5.1	10.0
E 940			9.0	6.1
E 964			11.8	3.3
T 78+00	5.1	15.3		10.2
E 1010			9.4	5.9
E 1024			12.1	3.2

STA	+	15.3 H. I.	-	ELEV.
E 1000			7.6	7.7
E 968			4.9	10.4
E 882			4.8	10.5
E 822			5.1	10.2
E 782			7.4	7.9
E 746			10.4	4.9
E 712			12.3	3.0
E 466			11.3	4.0
E 440			9.8	5.5
E 400			6.9	8.4
E 370			5.0	10.3
E 294			4.9	10.4
E 204			4.9	10.4
E 130			5.4	9.9
E 54			5.1	10.2
0			5.1	10.2
W 57			5.2	10.1
W 149			5.1	10.2
W 270			5.3	10.0
W 370			5.5	9.8
W 466			5.1	10.2
W 570			5.3	10.0
W 660			5.1	10.2

+ H.I. ELEV.
 STA 76 INST. AT 590' E
 0° AZ. EQUALS 588° 08' 40" W
 AZ, CLOCKWISE

8.1 23.6 15.5

H.I. = 23.6

STA. AZ. DIST. ROD ELEV.

76 1° 05' 138 12.6 11.0

21° 55' 101 12.6 11.0

67° 40' 73 12.6 11.0

114° 40' 86 12.6 11.0

143° 15' 120 12.6 11.0

170° 15' 156 12.6 11.0

180° 00' 170 12.6 11.0

180° 00' 110 5.6 18.0

151° 00' 83 5.6 18.0

108° 10' 56 5.6 18.0

58° 00' 50 5.6 18.0

18° 15' 78 5.6 18.0

0° 00' 103 5.6 18.0

EAST. WEST.

86+00 1300

87+00 1380

78+00 965

77+00 908 383

76+00 826 375

69+00 68 165

STA + H.I. - ELEV

78+00 5.1 15.3 10.2

TP. 5.2 15.7 4.8 10.5

77+00

E908 5.1 10.6

E910 5.2 10.5

E934 7.7 8.0

E951 9.6 6.1

E966 10.9 4.8

78+00 5.0 15.2 10.2

E1033 10.8 4.4

E1022 7.7 5.5

E1007 8.3 6.9

E983 6.3 8.9

PROJECT NO. 6
 PROFILE LEVELS W. SHORELINE

STA	+	H.I.	-	ELEV	PAINTED INS. WALK
129				8.49	
	5.33	13.82			
130			5.38	8.44	"
131			5.35	8.47	"
132			5.33	8.49	"
133			5.40	8.42	"
134			5.42	8.40	"
135			5.39	8.43	"
136			5.36	8.46	"
137			5.38	8.44	"
138			5.40	8.42	"
139			5.38	8.44	"
140			5.38	8.44	"
141			5.42	8.40	"
TP 141+29 ³¹			5.42	8.40	"

9-12-46

(56)

TOM STAMPER
 GEO. WILLIAMS

SEE PG. 10

X-SECTION STATION 130

STA	+	H.I.	-	ELEV
	5.4	13.8		8.44
E 3			5.4	8.4
E 5			5.0	8.8
E 6			4.5	9.3
E 48			4.3	9.5
E 80			7.6	6.2
E 110			9.2	4.6
E 130			10.2	3.6

STA 77+00

0+00 = 383 W Sound WEST					
#00	(11.00)	0.1	+5.3		
10		0.8	+4.6	40	3.1 +2.3
20	(5.4)	1.4	+4.0	50	3.2 +2.2
30		1.6	+3.8	60	3.5 +1.9
40		1.8	+3.6	70	3.7 +1.7
50		2.0	+3.4	80	4.1 +1.3
60		1.9	+3.5	90	5.3 +0.1
70		1.9	+3.5	A+00	— -0.9
80		2.0	+3.4	10	— —
90		2.3	+3.1	20	6.0 -0.6
2+00		2.2	+3.2	30	7.0 -1.6
10		2.3	+3.1	40	6.1 -1.7
20		2.2	+3.2	50	5.0 +0.4
30		2.1	+3.3	60	5.0 +0.4
40		2.4	+3.0	70	5.5 -0.1
50		2.8	+2.6	80	6.0 -0.6
60	(11.05)	2.7	+2.7	90	8.0 -2.6
70		2.6	+2.8	5+00	5.3 +0.1
80		2.5	+2.9	10	4.7 +0.8
90		2.2	+3.2	20	(11.10) 5.8 -0.3
3+00	(5.4)	2.7	+2.7	30	(5.5) 6.8 -1.3
10		2.9	+2.5		
20		3.0	+2.4		
30		3.1	+2.3		

STA 76+00

0+00 = 375 W Sound WEST		
0+00	(11.18)	0.0 +5.5
+70	(5.5)	0.2 +5.3
80		0.9 +4.6
90		1.4 +4.1
1+00		.8 +4.7
10		2.0 +3.5
20		2.1 +3.4
30		3.0 +2.5
40		3.6 +1.9
50		5.0 +0.5
60		5.5 0.0
70		5.2 +0.3
80		7.0 -1.5
90		8.0 -2.5
2+00	(11.23)	8.8 -3.3
10	(5.5)	8.2 -2.7

~~6+00 (12.25)~~

DIST SOUND ELEV.
STA 68+00 SOUND WEST

0+00	(1229)	7.0	-1.9
10	(5.1)	7.2	-2.1
20		7.3	-2.2
30		6.5	-1.4
40		—	—
50		7.5	-2.4
60		7.7	-2.6
70		7.3	-2.2
80		6.5	-1.4
90		7.0	-1.9
1+00		7.2	-2.1
10		7.2	-2.1
20		7.1	-2.0
30		6.8	-1.7
40		5.8	-0.7
50		6.8	-1.7
60		7.3	-2.2
70		7.8	-2.7
80		7.5	-2.4
90	(5.1)	7.0	-1.9
2+00	(232)	7.5	-2.4
10		—	—

68+00 SOUND EAST

(1237)
0+10 (5.1) 5.5

(58)
DIST SOUND ELEV.

20		5.9	-0.9
30		6.7	-1.7
40		7.5	-2.5
50		8.2	-3.2
60		8.0	-3.0
70		7.8	-2.8
80		7.8	-2.8
90		7.8	—
1+00		7.8	-2.8
10		7.7	-2.7
20		8.0	-3.0
30		8.0	-3.0
40		8.2	-3.2
50		8.3	-3.3
60		9.4	-4.4
70	(5.0)	9.0	-4.0
80	(237)	9.8	-4.8
90		11.0	-6.0

69+00 SOUND WEST

Q+00 = 165 W

(1246)
30 (190.2) +4.7
40 0.8 +4.1
50 1.2 +3.7

DIST. SOUND ELEV.
69+00 CONT.

60	1.8	+3.1
70	2.5	+2.4
80	3.1	+1.8
90	—	—
1+00	3.0	+1.9
10	3.1	+1.8
20	3.3	+1.6
30	3.2	+1.7
40	3.4	+1.5
50	3.6	+1.3
60	3.6	+1.3
70	3.8	+1.1
80	3.7	+1.2
90	3.8	+1.1
2+00	3.8	+1.1
10	3.8	+1.1
20	3.8	+1.1
30	3.8	+1.1
40	4.0	+0.9
50	3.9	+1.0
60	3.9	+1.0
70	3.9	+1.0
80	4.1	+0.8

69+00 SOUND EAST

0+00 = 68' EAST

DIST SOUND ELEV. (59)

0+10	0.0	+4.8
20	0.0	+4.8
30	0.0	+4.8
40	0.4	+4.4
50	1.0	+3.8
60	2.5	+2.3
70	2.2	+2.6
80	4.3	+0.5
90	7.2	-2.4
1+00	9.2	-4.4
10	10.5	-5.7
20	11.2	-6.4
30	11.5	-6.7
40	11.6	-6.8
50	12.1	-7.3
60	12.7	-7.9
70	12.9	-8.1
80	13.5	-8.7
90		
2+00		

SOUND ELEV.
DIST 76+00

0+00 = 826' EAST SOUND EAST

(1118)

0+70 0.4 +4.3

80 A. 2.0 +2.7

90 3.6 +1.1

1+00 5.5 -0.8

+10 7.1 -2.4

20 8.2 -3.5

30 9.8 -5.1

40 10.5 -5.8

50 11.3 -6.6

60 (1122) 12.0 -7.3

A.6

77+00

0+00 = 908' EAST SOUND EAST

(1131)

0+70 A.A. 0.7 +3.7

80 2.0 +2.4

90 2.8 +1.6

1+00 4.0 +0.4

10 5.2 -0.8

20 7.5 -3.1

30 9.3 -4.9

40 10.7 -6.3

50 11.5 -7.1

(60)
DIST SOUND ELEV.

60 - -

70 12.8 -8.4

(1133)

A.A.

78+00

0+00 = 965' EAST SOUND E

0+70 (1140) 0.0

80 2.0

90 3.0

0+10 3.0

(1142)

0+72 0.0 +4.4

80 1.0 +3.4

90 2.2 +2.2

1+00 A.A. 3.0 +1.4

10 3.5 +0.9

20 4.5 -0.1

30 5.0 -0.6

86+00 SOUND EAST

0400 = 1300E

DIST SOUND

DIST SOUND

1+	15	(3.7)	0.0	+3.7	30	10.8	-7.1
	20		0.2	+3.5	40	10.7	-7.0
			1.0	+2.7	50	10.6	-6.9
			3.0	+0.7	160	11.8	-8.1
	50		6.5	-2.8	70	12.5	-8.8
	60				80	12.9	-9.2
	70		7.6	-3.9	(232) 90	12.4	-8.7
	80		8.1	-4.4	4+00 12.2		-8.5
	90		8.6	-4.9	10 12.3		-8.6
2+	400		8.9	-5.2	(3.7) 20	12.1	-8.4
	16		9.0	-5.3	30	12.0	-8.3
	20		9.9	-6.2	40	11.7	-8.0
	30		9.8	-6.1	50	11.5	-7.5
	40		9.9	-6.2	160 12.3		-8.6
	50		10.1	-6.4	70 12.5		-8.8
			10.4	-6.7	80 12.5		-8.8
			10.8	-7.1	90 12.5		-8.8
	80		11.0	-7.3	5+00 12.4		-8.7
	90		11.1	-7.4	10 12.2		-8.5
3+	00		10.9	-7.2	20 12.2		-8.5
	10		10.6	-6.9	30 12.3		-8.6
	20	(3.7)	10.6	-6.9	40 12.1		-8.4

231

DIST SOUND

(61)

50 12.0 -8.3

60 11.7 -8.0

70 11.1 -7.4

6+00 3.6 +0.1

RANGE	GRID STA.	B/L. DIST. PER 100'
115+75.10	103+00	101.07'
115+60.44	104+00	"
115+45.78	105+00	"
115+31.12	106+00	"
115+16.46	107+00	"
115+01.80	108+00	"
114+87.14	109+00	"
114+72.48	110+00	"

NOTE: FOR STAS & RANGES
 CONT'D N. SEE F.B.#
 14-PG# 4

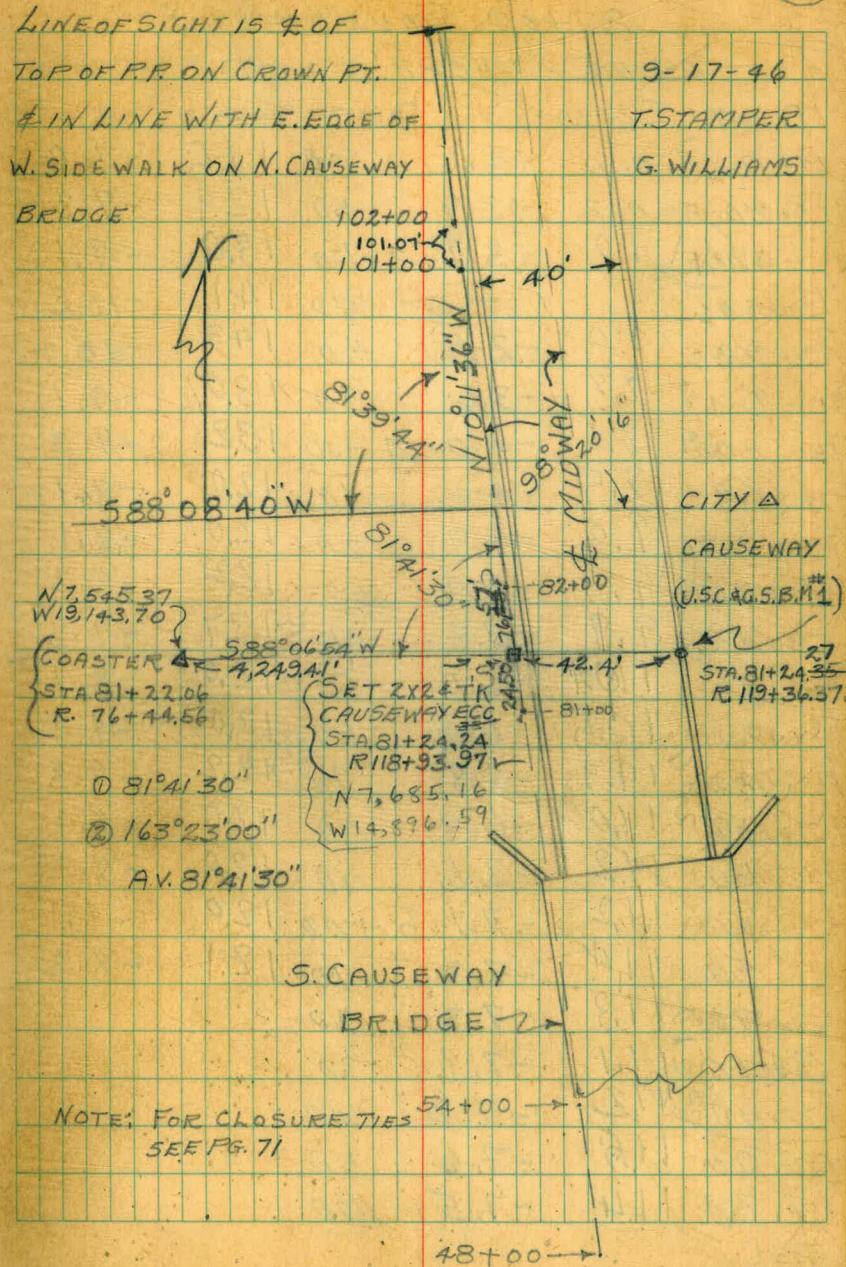
BASELINE FOR CROSS
SECTIONS OF PROJECT No. 6

RANGE	GRID STA.	DIST. FROM R 88+67.58 TO B/L RANGES
115+89.76	102	2722.18
116+04.42	101	2736.84
116+19.07	100	2751.49
116+33.73	99	2766.15
116+48.39	98	2780.81
116+63.04	97	2795.46
116+77.70	96	2810.12
116+92.36	95	2824.78
117+07.01	94	2839.43
117+21.67	93	2854.09
117+36.32	92	2868.74
117+50.98	91	2883.40
117+65.63	90	2898.05
117+80.29	89	2912.71
117+94.94	88	2927.36
118+09.60	87	2942.02
118+24.26	86	2956.68
118+38.91	85	2971.33
118+53.57	84	2985.99
118+68.22	83	3000.64
118+82.88	82	3015.30
118+93.97	81+24.33	3026.39
118+97.54	81+00	3029.96

NOTE SEE PG. 61
FOR STA 102 TO 110
PG 64 FOR RANGES
SOUTH

CONTD. ON PG. 64

INITIAL
JUL 16 1958



87+00 SOUND EAST

0+00 = 1380' EAST

DIST	SOUND		DIST	SOUND	
1+10	0.0	+4.1	40	11.5	-7.6
20	0.2	+3.9	50	12.9	-9.0
30	1.0	+3.1	60	13.0	-9.1
40		-	70	14.1	-10.2
50	7.0	-2.9	80	14.3	-10.4
60	7.7	-3.6	90	13.0	-9.1
70	8.1	-4.0	4+00	13.2	-9.3
80	8.5	-4.4	10	12.0	-8.1
90	9.0	-4.9	20	12.0	-8.1
2+00	9.5	-5.4	30	12.2	-8.3
10	9.9	-5.8	40	13.7	-9.8
20	10.1	-6.0	50	12.0	-8.1
30	10.5	-6.4	60	12.0	-8.1
40	10.9	-6.8	70	12.2	-8.3
50	11.0	-6.9	80	12.0	-8.1
60	11.2	-7.1	90	12.0	-8.1
70	11.2	-7.1	5+00	12.0	-8.1
80	11.4	-7.3	10	12.1	-8.2
90	11.3	-7.3	20		
3+00	11.1	-7.1	30		
10	11.2	-7.2	40		
20	11.6	-7.6	50		
30	11.4	-7.5	60		

87+00

(63)

DIST SOUND DIST SOUND

70

80

90

6+00

10

20

30

40

50

60

70

80

90

7+00

BASELINE CONTD.

DIST. FROM R-88+67.58 TO

RANGE	STA.	B/L RANGES
119+12.20	80	3044.62
119+26.85	79	3059.27
119+41.51	78	3073.94
119+56.16	77	3088.58
119+70.82	76	3103.24
119+85.47	75	3117.89
120+00.13	74	3132.55
120+14.79	73	3147.21
120+29.44	72	3161.86
120+44.10	71	3176.52
120+58.75	70	3191.17
120+73.41	69	3205.83
120+88.06	68	3220.48
121+02.72	67	3235.14
121+17.38	66	3249.80
121+32.03	65	3264.45
121+46.69	64	3279.11
121+61.34	63	3293.76
121+76.00	62	3308.42
121+90.66	61	3323.08
122+05.31	60	3337.73
122+19.97	59	3352.39
122+34.62	✓58	3367.04

GRID

DIST. FROM R-88+67.58 TO

(64)

RANGE	STA.	B/L RANGES
122+49.28	57	3381.70
122+63.94	56	3396.36
122+78.59	55	3411.01
122+93.25	54	3425.67
123+07.90	53	3440.32
123+22.56	52	3454.98
123+37.21	51	3469.63
123+51.87	50	3484.29
123+66.52	49	3498.94
123+81.18	48	3513.60

8-19-46

TOM STAMPER

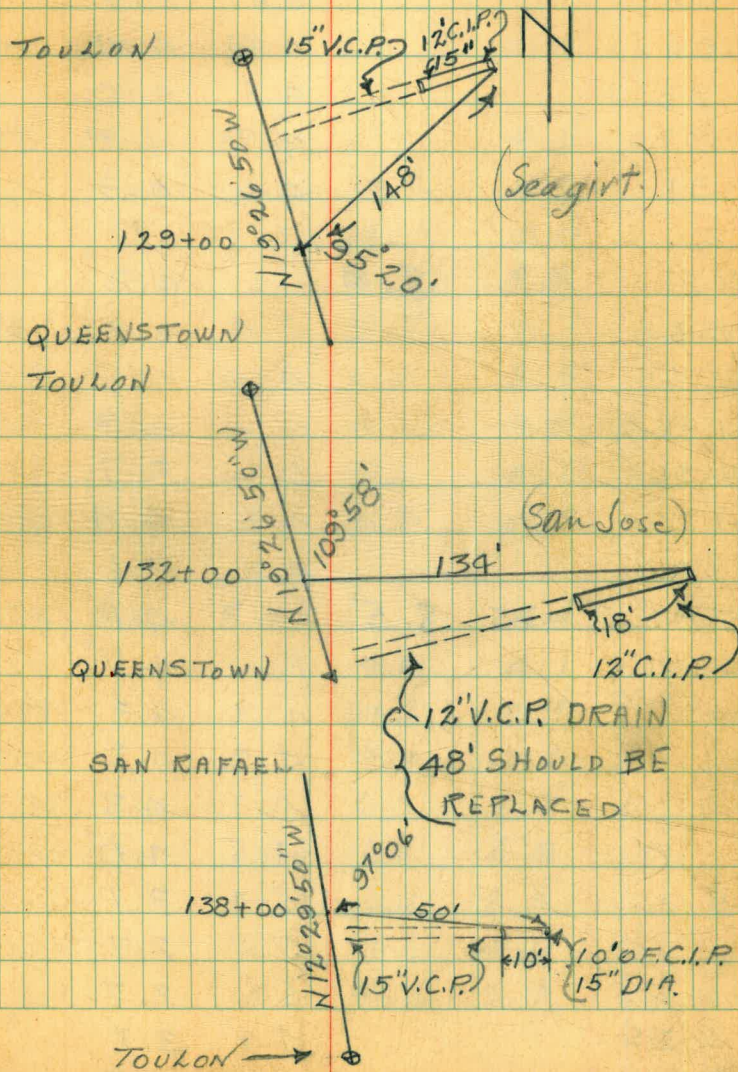
DRAIN LOCATIONS
ALONG W. SHORELINE B/L.
MISSION BAY AREA

INDENTED
JUL 16 1953

9-23-46

(67)

TOM STAMPER
GEO. WILLIAMS



INDEXED

MISSION BAY AREA
SECTIONS ALONG RANGE

JUL 16-1953

100+00 FOR SHOAL DISPOSAL

STA	T	H. I	-	ELEV
	6.0	8.9		2.9
95			6.0	2.9
94			4.8	4.1
93			4.9	4.0
92			4.9	4.0
91			4.6	4.3
T 91	4.6	8.9		4.3
W 50			5.0	3.9
W 165			4.4	4.5
W 260			4.6	4.3
W 265			5.2	3.7
W 270			4.5	4.4
W 360			4.3	4.6
T 92	4.5	8.5		4.0
W 356			3.8	4.7
W 230			4.2	4.3
W 152			4.2	4.3
W 65			4.2	4.3
0			4.5	4.0
E 10			5.4	3.1
E 16			5.8	2.7
E 43			5.8	2.7
G 55			4.8	3.7
E 112			4.2	4.3

9-26-46

TOM STAMPER
GEO. WILLIAMS

(68)

WATER LEVEL AT 3:04 P.M. 9-26-46

STA	T	H. I	-	ELEV
T 93	4.5	8.5		4.0
E 112			4.2	4.3
0			4.5	4.0
W 74			4.7	3.8
W 90			5.8	2.7
W 128			6.0	2.5
W 146			4.5	4.0
W 194			4.5	4.0
W 320			4.2	4.3
T 94	4.4	8.5		4.1
W 329			4.4	4.1
W 270			4.6	3.9
W 245			4.4	4.1
W 235			6.0	2.5
W 226			6.5	2.0
W 212			6.0	2.5
W 203			4.5	4.0
W 163			4.6	3.9

9-26-46

STA	+	H. I	-	ELEV
T 94	4.4	8.5		4.1
W 125			4.5	4.0
W 60			4.6	3.9
0			4.4	4.1
E 11			5.0	3.5
E 28			5.8	2.7
E 54			5.8	2.7
E 72			5.3	3.2
E 96			4.7	3.8
E 108			5.5	3.0
E 126			4.6	3.9
E 176			4.4	4.1
E 230			4.8	3.7
T 95	4.4	7.3		2.9
E 240			3.8	3.5
E 200			4.0	3.3
E 150			4.7	2.6
E 106			4.0	3.3
W 68			4.5	2.8
W 166			4.7	2.6
W 198			3.3	4.0
W 270			3.3	4.0
W 320			3.2	4.1

(69)

MISSION BAY AREA
TRIANGULATION OF

STA. 90+00 RANGE 100+00

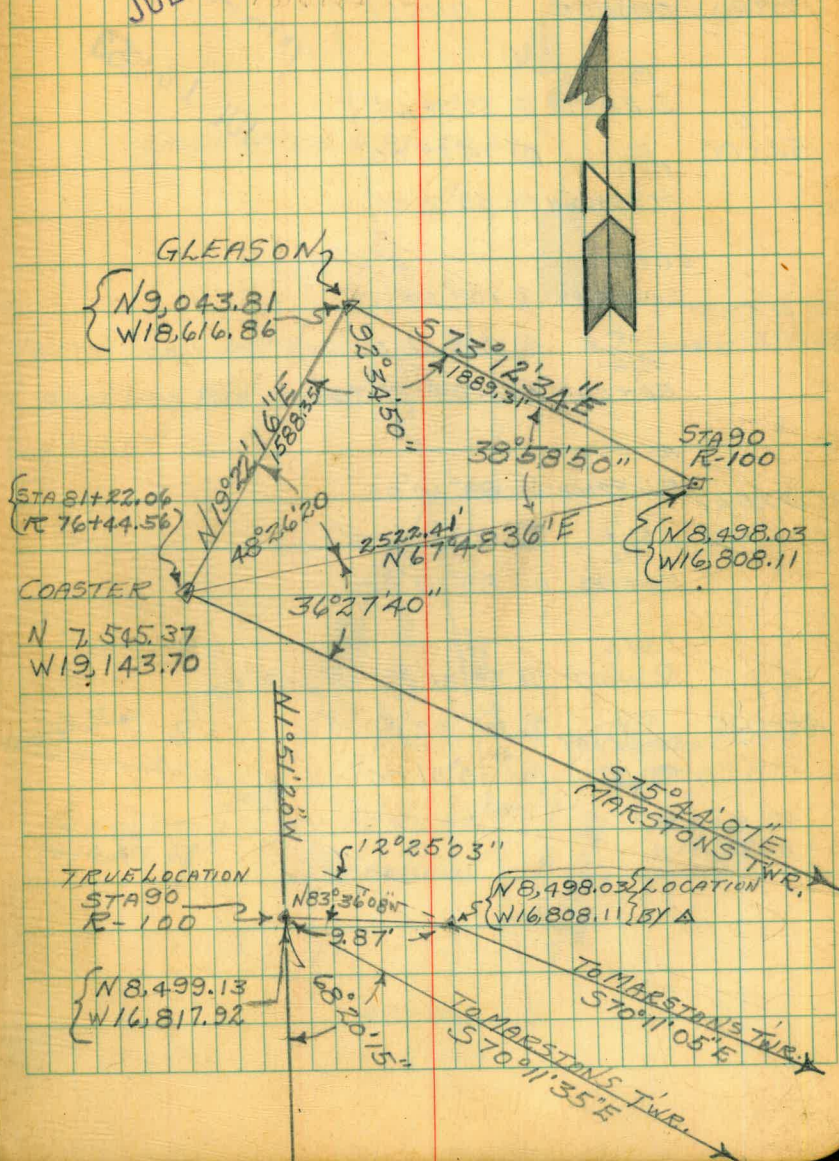
STA	OBJECT	ANGLE	VERNIER
	R100 STA 90	① 92° 35' 00"	
GLEASON	R7	② 185° 10' 00"	0° 00' 00"
	COASTER	③ 545° 29' 00"	
		AV. 92° 34' 50"	
	GLEASON	④ 48° 27' 00"	
COASTER	R7	⑤ 96° 53' 00"	0° 00' 00"
	R-100 STA 90	⑥ 290° 38' 00"	
		AV. 48° 26' 20"	
	R-100 STA 90	⑦ 36° 28' 00"	
COASTER	R7	⑧ 72° 56' 00"	0° 00' 00"
	MARSTON'S TOWER	⑨ 218° 46' 00"	
		AV. 36° 27' 40"	

89-59-60
68-20-15
21-37-45

9-27-46

JUL 16 1953

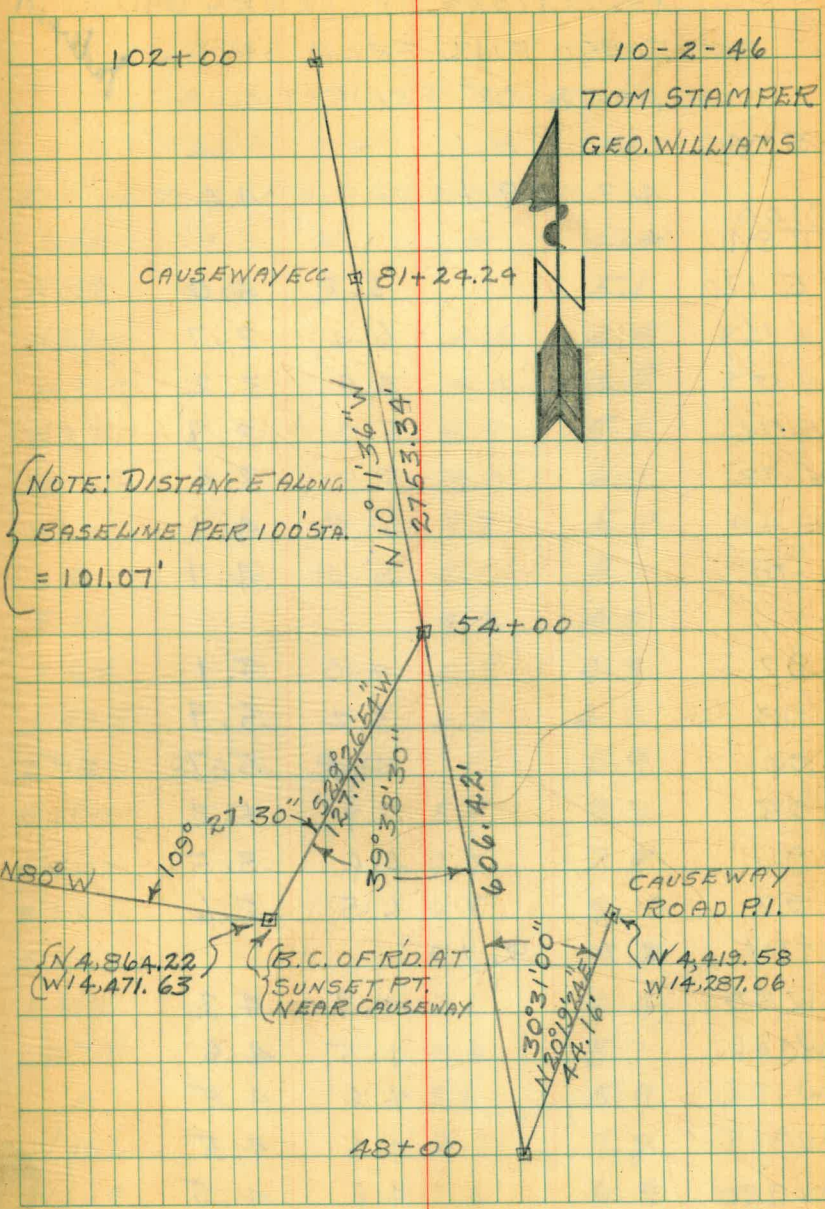
(70)
TOM STAMPER
GEO. WILLIAMS



CLOSURE TIES OF CAUSEWAY
BASELINE TRAVERSE

STA.	OBJECT	ANGLE
	B.L.	
	S. EAST	① 39°38'45"
B.L.		
54+00	R ₂	② 79°17'00"
	B.C. OF RD.	
	AT S.S. & C'SWAY	AV. 39°38'30"
	E.C. OF RD. AT	
	SUNSET PT.	① 109°27'30"
B.C. OF RD. AT		
SUNSET & CAUSEWAY	R ₂	② 218°55'00"
	B/L	
54+00	AV.	109°27'30"
	VENTURA	
B.L. 82+00		① 89°10'00"
B.C. OF RD. AT		
S.S. & C'SWAY	R ₂	② 178°20'00"
	B/L	
54+00	AV.	89°10'00"
	B/L	
	N. WEST	① 30°31'00"
B/L		
48+00	R ₂	② 61°02'00"
	CAUSEWAY	
	RD. P.I.	AV. 30°31'00"

VENTURA
JUL 16 1953



RANGE 100+00
X-SECTIONS OF TERRA DEL
FUEGO FILL FROM SHOAL
AREA OF PROJECT A-A

Indexed

STA	+	H.I.	-	ELEV.
R100	4.7	9.1		4.4
T91	+			
E 170			5.1	4.0
E 163			6.4	2.7
E 123			5.9	3.2
E 116			5.2	3.9
E 73			5.3	3.8
E 44			5.0	4.1
0			5.0	4.1
92			4.0	5.1
93			3.2	5.9
94			3.4	5.7
95			3.9	5.2
96			5.6	3.5
97			6.5	2.6
T91	4.7	9.1		
W 50			4.9	4.2
W 106			4.5	4.6
W 192			4.6	4.5
W 318			4.6	4.5
W 390			4.6	4.5

10-14-46

(72)

				T. STAMPER
				G. WILLIAMS
				FAIR-COOL
				3.7
ROD ON TOP OF H ₂ O AT 2:35 P.M.				
STA	+	H.I.	-	ELEV
T92	4.0	9.1		5.1
W394			4.6	4.5
W312			4.3	4.8
W276			3.9	5.2
W164			3.0	6.1
W 70			3.3	5.8
0			4.0	5.1
E 56			4.3	4.8
E 68			4.8	4.3
E 125			4.9	4.2
T93	3.6	9.5		5.9
E 250			5.8	3.7
E 244			6.7	2.8
E 225			6.5	3.0
E 202			5.6	3.9
E 113			5.1	4.4
E 70			4.4	5.1
0			3.6	5.9
W 102			2.3	7.2
W 148			2.6	6.9
W 288			3.9	5.6
W 355			4.9	4.6
W 390			4.9	4.6

STA	+	H.I	-	ELEV
0+00 = R 100				
T 94	3.5	9.2		5.7
W 380			5.1	4.1
W 310			4.7	4.5
W 280			4.0	5.2
W 180			3.0	6.2
W 60			2.8	6.4
0			3.5	5.7
E 70			4.2	5.0
E 112			5.3	3.9
E 170			5.2	4.0
T 95	3.9	9.1		5.2
E 242			5.5	3.6
E 205			5.8	3.3
E 180			6.1	3.0
E 135			6.1	3.0
E 105			5.9	3.2
E 70			5.7	3.4
E 36			4.5	4.6
0			3.9	5.2
W 82			3.6	5.5
W 178			3.5	5.6
W 250			4.4	4.7
W 270			4.8	4.3
W 340			4.9	4.2

10-19-46 (73)

STA	+	H.I	-	ELEV
T 96	4.3	7.8		3.5
W 340			3.7	4.1
W 303			4.2	3.6
W 272			4.9	3.4
W 260			4.1	3.7
W 240			4.0	3.8
W 210			4.4	3.4
W 178			4.0	3.8
W 148			3.2	4.6
W 130			3.8	4.0
W 85			3.5	4.3
W 32			3.6	4.2
0			4.3	3.5
E 28			4.6	4.2
E 65			5.2	3.6
E 155			4.9	2.9
E 185			4.9	2.9

0400 = R100

STA	+	H.I	-	ELEV
T97	4.7	7.3		2.6
E145			4.1	3.2
E 70			4.6	2.7
0			4.7	2.6
W 62			4.5	2.8
W 150			4.5	2.8
W 206			4.7	2.6
W 283			4.3	3.0

4.0 3.3

10-14-46

(74)

H2O LEVEL AT 4:05 P.M.

MISSION BAY AREA TRIANGULATION
OF SEXTANT POINTS FOR ARC.
SHEET PREPARATION

STA	OBJECT	SIX	ANGLES	MEAN	VERNIER
	KENDALL	①	29° 28' 45"		
<u>USC #65</u> MORENA	R 2	②	58° 56' 00"	29° 28' 20"	0° 00' 00"
<u>USED</u> BOND		③	176° 50' 00"		
<u>USED</u> BOND		④	37° 20' 00"		
<u>USC #65</u> MORENA	R 2	⑤	74° 38' 30"	37° 19' 15"	0° 00' 00"
	BERET	⑥	223° 55' 30"		
	BERET	①	48° 31' 00"		
<u>USED</u> BOND	R 2	②	97° 02' 00"	48° 31' 00"	0° 00' 00"
<u>USC #65</u> MORENA		③	291° 06' 00"		
<u>USC #65</u> MORENA		①	92° 22' 00"		
<u>USED</u> BOND	R 2	②	184° 43' 00"	92° 21' 40"	0° 00' 00"
	KENDALL	③	554° 10' 00"		
	PENT	④	37° 35' 30"		
CAUSEWAY	R 2	⑤	75° 11' 00"	37° 35' 25"	0° 00' 00"
<u>USC #65</u> COASTER		⑥	225° 32' 30"		
<u>MARSTON</u> TOWER		①	121° 09' 00"		
CAUSEWAY	R 2	②	242° 17' 30"	121° 08' 50"	0° 00' 00"
	PENT	③	726° 53' 00"		

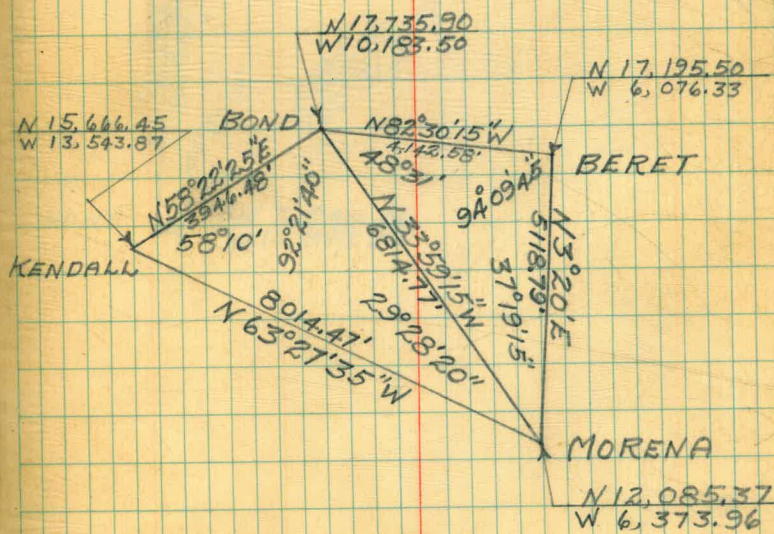
11-22-46

INST. BERGER
2091

TOM STAMPER
GEO. WILLIAMS

WEATHER:

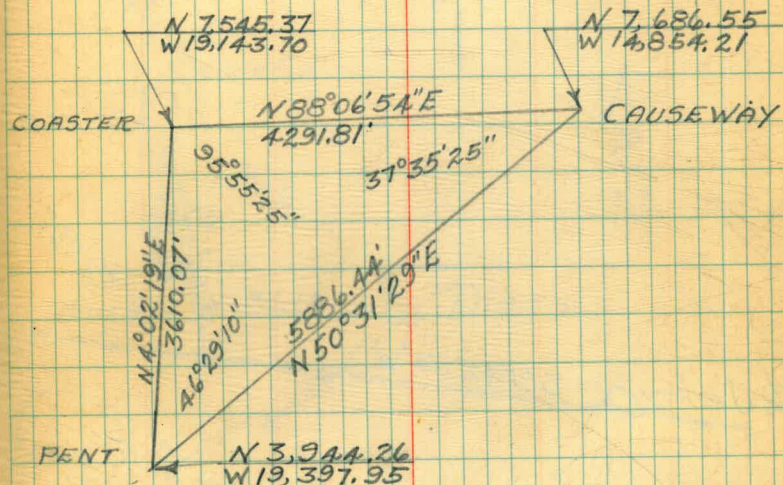
HIGH CEILING & COOL
GOOD VISIBILITY



STA	OBJECT	SIX ANGLES	MEAN	VERNIER
	CAUSEWAY	①	95° 55' 30"	
VSC & G.S. COASTER	R 2	②	191° 51' 00"	95° 55' 25" 0° 00' 00"
	PENT	⑥	575° 32' 30"	
	MARSTON'S TOWER	①	79° 47' 00"	
VSC & G.S. COASTER	R 2	②	—	79° 46' 37.5" 0° 00' 00"
	PENT	⑥	478° 39' 45"	

11-22-46

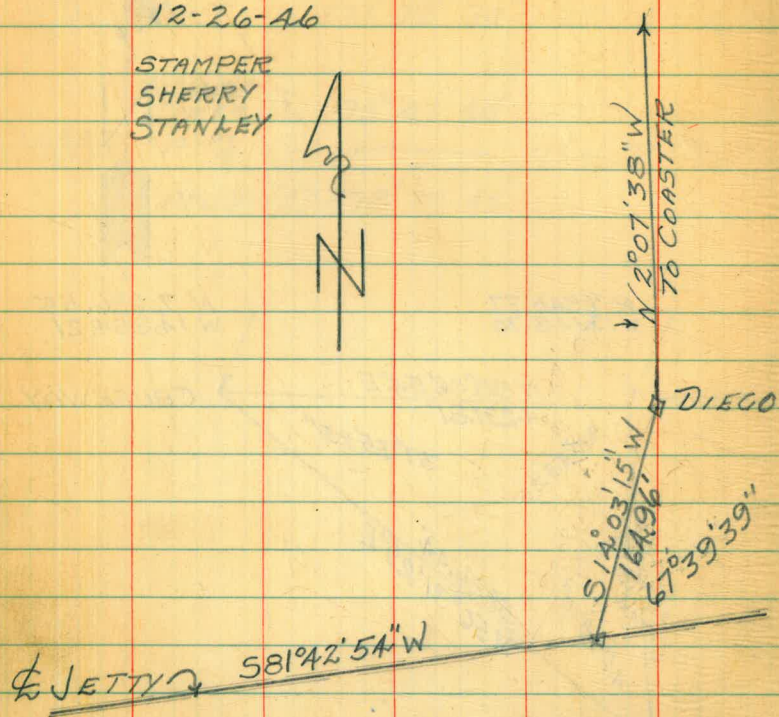
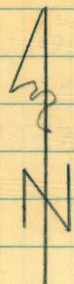
TOM STAMPER



NORTH JETTY &
LOCATION TO ENTRANCE
CHANNEL

12-26-46

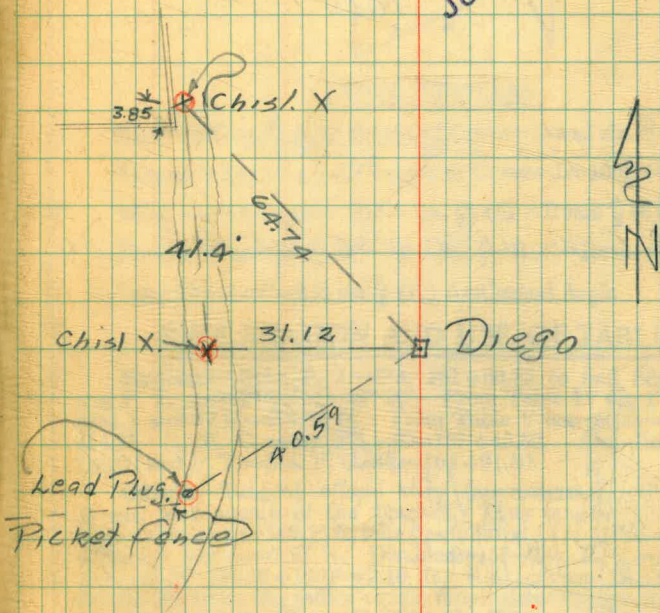
STAMPER
SHERRY
STANLEY



199.100
70.59
159.41
200.00

REFERENCE TIES TO
U.S.E.D. MON. DIEGO
12-27-46

INDEXED
JUL 16 1953



ERD.
B.L.
EAST

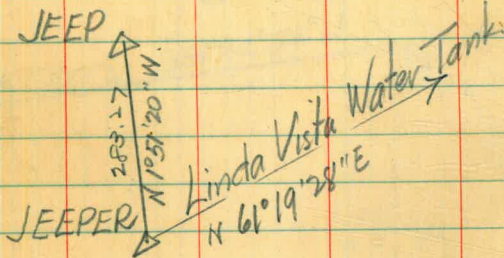
SHORE
B.L.
EAST

78

80+00		
81+00	400	
82+00	533	
83+00	732	
84+00		1080
85+00		1220
T		1010

12-26-46

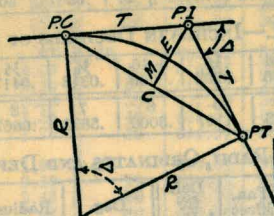
17,978 C.Y. APPROVED FOR STOCKPILE



11-26
60 88
02 081

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



533
313
846

533
215
748

CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) = $R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) = $R \div \cos \frac{\Delta}{2} - R$ (8) = $R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ =Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta=32^\circ 10'$ $D=8^\circ 20'$. From Table IV for 1° curve $T=3454.1$ and $+8\frac{1}{2}=414.49$ ft. From Table V correction=.36 or $T=414.85$ ft. P. C.=Sta. P.I.— $T=157+45.50$. Also from (4) $L=746.00$ and P. T.=Sta. P. C. + $L=164+91.50$.

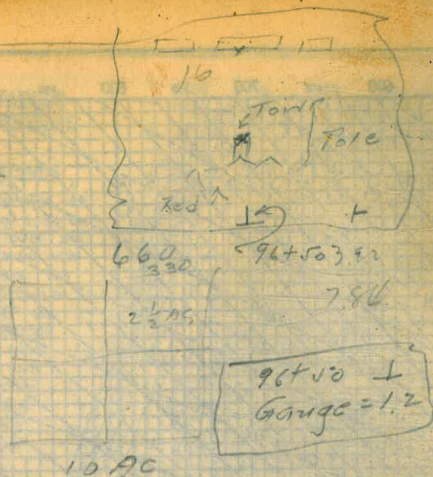
Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset= $7.27 (54.50 \div 100)^2=2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)=2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.=(in minutes) $.3 \times C \times D^\circ$ or=defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve= $.3 \times 54.5 \times 8\frac{1}{2}=136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5=136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2=6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E=960.6$ for $8^\circ 20'=960.6 \div 8\frac{1}{2}=91.27$ and from Table V correction=.10 or $E=91.37$ ft. Or suppose $\Delta=32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E=230.9$ and $+42=5.5$ or $D=5^\circ 30'$.

840
6.08
H.I. 1448
11

3.48



65
18

43

965
68

1033
64
42

26
1007

149.87
22

29974
29974

329714

88-08-40
10-11-36

98 20-16
179-59-60

81-39-94

117 26 30
95 38

21 48 30
90

68-18 30

780
760 117 27

75-38
21-47

TOWARDS Coaster 42.40

117-26-30
95 38

21 48 30
90

180
88-06-54

68-11-30

268-06-54
81-41-30

349-48-24
359-59-60

N 10-11-36 W

68-11-30

28-92-L11
29-61-52
97-80-88

179-60
137 24

42-36

137-23-60
42 35 46

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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Handwritten notes and calculations on the left page of the notebook, including various numbers, fractions, and diagrams. Some visible text includes:

- 101.09, 71.96, 192', 172.57
- 6/391, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40
- 6/15, 12, 6/54, 139, 53, 75, 12
- N 88-08-40, 9-26, 30
- 107-31-30
- 460, 106, 566, 289
- 93 + 20 - 1
- 51-41-05, 91-13-10, 142 54 15, 179-59-60, 37-05-45, 92 34-30, 48-26-10, 741-01-00, 179-60-60, 38-59, 8-7-20-30, 50, 137-20-30, 179-59-60, 42-39-30
- 183, 2, 766, 25, 30, 34, 35, 36, 37, 38, 39, 40
- 390, 450, 940, 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, 694, 695, 696, 697, 698, 699, 700
- 25° 01' 00", 50° 02' 00", 150° 09' 45"
- 92 + 49, 88 + 67, 58 + 67, 650, 95 + 47