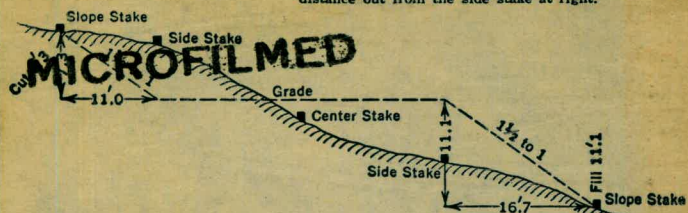


MISSION BAY

43
43

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 Roadway of any Width. Side Slopes 1½ to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	Distance out from Side or Shoulder Stake																			Cut or Fill	
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	0	.1	.2	.3	.4	.5	.6	.7	.8		.9
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4

KEUFFEL & ESSER CO., N. Y.

43
 S/R TO "CLARA" N 1° 14' 42" W
 (358° 45' 18")

@ FARMROSS BLVD
 R.R. BRIDGE
 1/2 MI. N. ST. @ N.W. COR W. END
 E. 13.51

The paper in this book No. 373A
 is made of 50% high grade rag stock
 with a WATER RESISTING surface sizing.

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CURVE DATA VENTURA BLVD

T. STAMPER

☒ OF SOUTH TRAFFIC LANE

STA	DEF L	CHORD	BEARING
B.C. RT 63+91.02	0	0	57°43'32"
64+00	0°30'07"	8.98	
+50	3°17'49"	50.00	
65	6°05'31"	50.00	
+50	8°53'12"	50.00	
66	11°40'54"	50.00	
+50	14°28'36"	50.00	
67	17°16'17"	50.00	
E.C. 67+27.71	18°49'13"	27.71	
+50		22.29	
68		50.00	
+50		50.00	53°05'06"
69		50.00	
+50		50.00	
B.C. LT. 69+70.80		20.80	
70	0°59'12"	29.20	
+50	2°40'34"	50.00	
71	4°21'55"	50.00	

$\Delta = 37^{\circ}38'26''$
 $R = 512.5$
 $L = 336.69$
 $T =$

STA	DEF L	CHORD	BEARING
EC. 71+54.03	6°11'27"	54.03	
72+00		45.97	
+50		50.00	S 45°28' E
73+00		50.00	
+50		50.00	
73+71.60		21.60	S. END OF PROJ.

N.G.
REVISED

ORIGINAL X-SECTIONS OF CURVE RUNNING

STA - 69 + 00

SOUTH ON VENTURA BLVD. TO AN INTERSECTION DIST + H.I. - ELEV

WITH MIDWAY DRIVE - ϕ OF SOUTH TRAFFIC LANE -

8.51
17.51

EQUALS ϕ FOR X-SECTIONS -

5.1 + 3.4

STA - 63 + 91⁰² (B.C.)

DIST + H.I. - ELEV

T.B.M. 6.33

17.51

11.18

0.6 NORTH
SIDE IN CURVE
LAMP POST

5.4 + 3.1

5.6 + 2.9

ϕ 1.9 + 3.6

5.7 + 2.8

REVISIONS

LEFT 25'

5.1 + 3.4

LEFT 50'

5.4 + 3.1

RIGHT 25'

5.2 + 3.3

RIGHT 50'

5.7 + 2.8

STA - 64 + 50

DIST + H.I. - ELEV

8.51
17.51

5.1 + 2.4

5.8 + 2.7

5.3 + 3.2

6.1 + 2.4

6.0 + 2.5

NOTE: ELEV. REDUCED TO CITY DATUM

STA- 65+00

STA- 66+00

17
24
37.520
25
57

(3)

DIST	+	H.I.	-	ELEV
8		8.5 17.51	6.2	+2.3
LEFT 25'			6.3	+2.2
LEFT 50'			5.9	+2.6
RIGHT 25'			6.1	+2.4
38'				
RIGHT 50'			6.2	+2.3
RIGHT 50			7.8	+1.7

DIST	+	H.I.	-	ELEV
8		8.5 17.51	11.4	-2.9
LEFT 29			10.9	-2.4
LEFT 40			5.0	+3.5
LEFT 54			6.4	+2.1
RIGHT 25			11.7	-3.2
RIGHT 50			12.0	-3.5

TOP
WEST CURB

5

STA- 65+50

STA- 66+55

DIST	+	H.I.	-	ELEV
8		8.5 17.51	8.3	+ 2
LEFT 25'			6.2	+2.3
LEFT 50'			5.9	+2.6
RIGHT 30'			11.2	-2.1
RIGHT 50'			11.6	-3.1

TOE
FILL

DIST	+	H.I.	-	ELEV
8		8.5 17.51	11.9	-3.4
LEFT 13			11.7	-3.2
LEFT 24			6.3	+2.2
LEFT 34			6.4	+2.1
LEFT 45			5.30	+3.2
RIGHT 25			5.37	+3.1
RIGHT 50			12.0	-3.5
RIGHT 50			12.2	-3.7

TOP
WEST CURB
GUTTER WEST
& MIDWAY

STA- 67+00

67+50

⑦

DIST	+	H.I.	-	ELEV		DIST	+	H.I.	-	ELEV	
T.B.M.	4.67	6.8 16.82 15.82		+2.2 11.18	0.5' W/LEAD CURB	R		6.8 16.82 15.82	7.3	-5	
℄			10.6	-3.8		LEFT-5'			9.7	-13.1	
LEFT-12'			4.6	+2.2	TOP CURB	LEFT-15'			9.27	+21	TOP CURB
LEFT-22'			4.7	+2	TOP WEST						WEST
LEFT-22 ²			5.36	+1.4	WEST GUTTER	LEFT-25'			5.39	+7.4	GUTTER
LEFT-44'			5.40	+1.4	RAMPWAY	LEFT-36'			5.48	+7.3	℄
RIGHT-25'			10.7	-3.9		RIGHT-2'			10.6	-3.8	
RIGHT-50'			10.6	-3.8		RIGHT-15'			10.8	-4.0	
						RIGHT-23'			11.2	-4.4	

STA- 67+27²¹ (E.C)

DIST	+	H.I.	-	ELEV		DIST	+	H.I.	-	ELEV	
℄		6.8 16.82 15.82	8.8	-2.0		RIGHT-25'			10.7	-3.9	
LEFT-6'			4.9	+1.9		RIGHT-18'			10.5	-3.7	
LEFT-17'			4.7	+2.1		RIGHT-50'			10.7	-3.9	
LEFT-18'			5.35	+1.4	GUTTER						
LEFT-38'			5.46	+1.3	℄ RAMPWAY						
LEFT-58'			6.21	0.0	EAST						
RIGHT-4'			10.7	-3.9							
RIGHT-25'			11.1	-4.3							
RIGHT-38'			10.4	-3.6							
RIGHT-50'			10.7	-3.9							

STA - 68+00

DIST	+	H.I.	-	ELEV
¢		68 16.82 15.82	5.0	+1.8
LEFT - 12'			4.73	+2.1
LEFT - 12 ⁵ '			5.92	+2.4
LEFT - 33'			5.55	+1.2
RIGHT - 9'			9.7	-2.9
RIGHT - 13'			10.8	-4.0
RIGHT - 24'			11.1	-4.3
RIGHT - 28'			10.8	-4.0
RIGHT - 50'			10.7	-3.9

STA - 68+50

DIST	+	H.I.	-	ELEV
¢		68 16.82 15.82	9.8	+2.0
LEFT - 3'			7.81	+2.0
LEFT - 9.5'			5.95	+1.3
LEFT - 30'			5.55	+1.2
RIGHT - 3'			9.8	+2.0
RIGHT - 11'			10.9	-4.0
RIGHT - 19'			11.0	-4.2
RIGHT - 31'			10.9	-3.9
RIGHT - 50'			10.7	-3.9

N.G.

5

STA - 69+00

69+50

DIST	+	H.I.	-	ELEV		DIST	+	H.I.	-	ELEV	
℄		^{6.8} 16.82 15.82	4.7	+21		℄		^{6.8} 16.82 15.82	4.7	+21	
LEFT - 7'			4.86	+1.9	TOP CURB	LEFT - 7'			4.83	+20	TOP CURB
LEFT - 7 ^{1/2} '			5.50	+1.3	WEST GUTTER	LEFT - 7 ^{1/2} '			5.46	+1.3	WEST GUTTER
LEFT - 28'			5.64	+1.2	MIDWAY	LEFT - 28'			5.61	+1.2	MIDWAY
RIGHT - 3'			4.8	+20		RIGHT - 3'			4.7	+21	
RIGHT - 10'			7.5	-1.7		RIGHT - 10'			10.6	-3.8	
RIGHT - 15'			10.6	-3.8		RIGHT - 15'			10.7	-3.9	
RIGHT - 30'			10.6	-3.8		RIGHT - 30'			11.0	-4.2	
RIGHT - 50'			10.6	-3.8		RIGHT - 50'			10.6	-4.8	

11.9

STA- 69+70.8 (B.C.)

STA-70+00

	DIST	+	H.I.	-	ELEV		DIST	+	H.I.	-	ELEV	
	T.B.M.	4.27	15.95		11.18	0.5' H.I. OF B.M. CUTS TO GRADE BY SPINNING IN PLACE AND DIST. 7'	6.5	15.19	9.9		+2.1	
A	T.B.M.		6.5	4.76	11.19				4.35		+2.1	TOP W/CURB
A	T.B.M.	4.30	15.19		11.19				5.03		+1.5	W/GUTTER
A	Φ			4.3	+2.2				5.13		+1.4	Φ MIDWAY
B	LEFT 7'			4.43	+2.1				4.4		+2.1	
D	LEFT 7.5'			5.10	+1.4				9.9		-3.4	
A	LEFT			5.18	+1.3				10.6		-3.9	
B	RIGHT-4'			4.6	+1.4				19.6		-8.1	
A	RIGHT-17'			10.3	-38				10.6		-39	
	RIGHT-25'			10.3	-38							
	RIGHT-50'			10.1	-39							

STA 70+50.7 C				71+0.0				10.1	
DIST	+	H.I.	-	ELEV	DIST	+	H.I.	-	ELEV
℄		6.5 15.49	4.2	+2.3	℄		6.5 15.49	4.5	+2.0
LEFT - 5'			7.32	+2.2	TOP W/GUTTER - 4'			7.36	+2.1
LEFT - 5 ⁵ '			5.00	+1.5	W/GUTTER - 4 ⁵ '			4.25	+1.5
LEFT -			5.02	+1.5	℄ MIDWAY			4.90	+1.6
RIGHT - 8'			5.9	+1.1	RIGHT - 5'			5.7	+0.8
RIGHT - 22'			11.5	-5.0	RIGHT - 22'			6.6	-1
RIGHT - 39'			11.1	-4.6	RIGHT - 31'			10.2	-3.7
RIGHT - 50'			10.5	-4.0	RIGHT - 50'			10.7	-3.9

EC. 71+54.03

STA- 72+50

DIST	+	H.I.	-	ELEV
		6.5		
£		15.49	1.9	+1.6
LEFT-21'			4.92	+1.6
RIGHT-15'			5.7	+1.8
RIGHT-30'			6.8	-1.3
RIGHT-50'			7.8	-1.3

W/EDGE LEFT
PAVEMENT
(NO CURB)
£

MIDWAY ST 2E

DIST	+	H.I.	-	ELEV
		6.5		
£		15.49	4.90	+1.6
			4.80	+1.7
			4.79	+1.7
			4.10	+2.4
			3.9	+2.6
			4.4	+2.1
			10.5	-4.0
			11.7	-5.2
			11.7	-5.2
			10.2	-3.7

£ MIDWAY
£ CURVE

GUTTER
TOP
CURB

STA- 72+00

DIST	+	H.I.	-	ELEV
LEFT 15'		6.5	1.92	+1.6
£		15.49	4.81	+1.7
RT- 5'			4.80	+1.7
RT- 5E			4.13	+2.4
RT- 12'			4.1	+2.4
RIGHT-18'			4.9	+1.6
RT- 28'			9.7	-3.2
RT- 30'			11.8	-5.3
RT- 35'			11.8	-5.3
RT. 40'			10.3	-3.8
RT. 50'			10.3	-3.8

£ MIDWAY

£ CURVE RT-50'
GUTTER

TOP CURB

			11.7	-5.2
			11.7	-5.2
			10.2	-3.7

STA-73+00

STA-73+50

DIST	+	H.I.	-	ELEV
LEFT-10'		6.5 15.49	1.80	+2.3
ℓ			4.76	+2.3
RT-11'			4.78	1.9°
RT-11.5'			4.12	+2.4
RT-12.5'			4.1	+2.4
RT-22			3.7	+2.8
RT-33			2.8	-3.3
RT-43'			10.4	-3.9
RT-44'			11.7	-5.2
RT-50'		11.3 10.3		-4.8
RT-52'			10.2	-3.7

DIST	+	H.I.	-	ELEV	ℓ
MIDWAY	8'	6.5 15.49	4.70	+1.8	MIDWAY
ℓ			4.70	+1.8	
WEST JTS					
GUTTER	12'		4.72	+1.8	W/GUTTER
TIP					TOP
CURB	12.5'		4.05	+2.4	CURB
RT-22			4.9	+2.1	
RT-33			2.5	-3.0	
RT-45			10.3	-3.8	
RT-46			11.8	-5.3	
RT-47			11.8	-5.3	
RT-51			10.7	-3.8	

3-16-43

STA-73+71⁶⁰ (END PROJ.)

DIST	+	H.I.	-	ELEV	
LEFT- 7'		65 15.49	4.77	+1.7	MIAN
⊕			4.70	+1.8	⊕
RT. - 12'			4.65	+1.8	W/EUT
RT. - 12 ⁵ '			4.03	+2.5	CURB
RT. - 24'			4.1	+2.4	
RT. - 35'			3.7	-3.2	
RT. - 38'			10.3	-3.8	
RT. - 39'			11.7	-5.2	
RT. - 45'			11.7	-5.2	
RT. - 46'			10.2	-3.7	
RT. - 50'			10.2	-3.7	

N.G.
REVISED

8-29-98 (2)

ORIGINAL X-SECTIONS OF PROPOSED

PX 0+50

DETOUR NASHVILLE ST. TO MIDWAY DR

DIST +

H.I.

ELEV

(0+00 = Cu. Disk P.I. Midway & Nashville)

B.M.

2.38

14.07

~~14.17~~

11.69

Fire Plug
NASHVILLE &
MIDWAY DRIVE

RT-24'

3

PROP. LINE

RT-15'

8.00

9.07

T. Curb

PX

0+00

RT-15'

6.00

8.07

Gutter

STA

+

H.I.

ELEV

B.M.

5.20

8.89

E

B.M.

1.63

13.32

11.69

RT-15'

5.35

8.72

Gutter

RT-15'

2.65

10.66

RT-15'

5.10

8.97

T. Curb

E

2.74

10.58

RT-24'

5.11

8.96

PROP. LINE

LT-15'

2.77

10.55

PX

0+30

B.M.

14.00

DIST

+

H.I.

ELEV

RT-24'

14.07

4.87

9.20

PROP. LINE

RT-24'

2.65

10.67

PROP. RT-15'

5.08

8.99

T. CURB

RT-15'

2.83

10.49

TOP CURB RT-15'

5.89

8.18

Gutter

RT-15'

3.47

9.85

Gutter E

5.46

8.67

E

E

3.30

10.02

E RT-15'

5.66

8.41

Gutter

LT-15'

3.45

9.87

Gutter RT-15'

?

TOP CURB

LT-15'

3.25

10.07

TOP CURB RT-24'

5.49

8.58

PROP. LINE

LT-24'

3.20

10.12

PROP. RT-24'

Sta	+	-	H.I.	Elev
			14.07	
PX				
Rt. 24'		5.95		8.12 Propline
Rt. 15'		5.66		8.41
£		5.50		8.57 £
L. 15'		5.73		8.34
L. 24'		5.37		8.70 Propline

Sta	+	-	H.I.	Elev
			14.07	
PX				
R. 24'		5.16		8.91 Propline
R. 15'		5.26		8.81 Top
R. 15'		6.05		8.02 Cutler
£		5.56		8.57 £
L. 15'		5.83		8.24 Top
L. 15'		5.20		8.87
L. 24'		5.09		8.98

Sta	+	-	H.I.	Elev
			14.07	
PX				
R. 24'		5.33		8.74 Propline
R. 15'		5.42		8.65 T.C.
R. 15'		6.10		7.97 Cutler
£		5.54		8.53 £
L. 15'		6.00		8.07 Cutler
L. 24'		5.45		8.62 T. Curb
L. 24'		5.28		8.79

Sta	+	-	H.I.	Elev
			14.07	
PX				
R. 24'		5.80		8.27 Propline
R. 15'		5.47		8.50
R. 15'		5.56		8.51 £
R. 15'		5.30		8.77
£		5.28		8.79 Propline
L. 15'		6.4		5.53 8.64

END OF CUTS
RETURN NORTH
W/SIDE L. S. S. S.

8-29-40 (14)

Sta 7+00

Dist

+

H.I.

-

Elev

PX

12.75

12.85

DIST

+

H.I.

-

ELFV

END OF
RET. DIST

12.75

8.34

12.85

8.69

Pt. 24

4.70

8.05

PROP. LINE

RT-24'

4.17

8.58

PROP. LINE RT 15'

4.85

7.90

T.C.

RT-15'

4.26

8.49

T.C. RT 15'

4.85

7.90

Gutter

RT-15'

4.55

8.20

Gutter 9'

4.53

8.22

E

4.00

8.75

L 15'

4.96

7.85

Gutter

LT-15'

4.75

8.00

Gutter 15'

4.70

7.85

T.C.

LT-15'

4.20

8.55

T.C. RT 24'

4.74

8.01

PROP. LINE

LT-24'

4.06

8.69

PROP. LINE Sta

8+00

PX

5.19

6+00

Pt. 24

12.75

5.06

7.69

PROP. LINE

Pt. 24

12.75

4.55

8.20

PROP. LINE RT 15'

5.18

7.57

T.C.

Pt. 15

4.54

8.21

T.C. RT 15'

5.60

7.15

Gutter

Pt. 15

4.92

7.83

Gutter 9'

4.92

7.83

E

4.30

8.45

L 15'

5.23

7.52

Gutter

L 15'

4.87

7.91

Gutter 15'

5.23

7.52

T. CURB

L 15'

4.56

8.19

T.C. RT 24'

5.07

7.68

PROP. LINE

L 24'

4.40

8.35

PROP. LINE

8-29-49⁽¹⁵⁾

Sta 9+00

Sta 11+00

Dist

+

H1

-

Elev

Dist

+

H1

PX

Elev

PX

12.75
+2.85

T.P.

2.80

12.82
~~11.44~~10.02
~~8.64~~

Stamp

R 24

5.35

7.40

Punch

5.10

7.92

R 15

5.40

7.35

T.C.

5.25

7.57

R 15

5.65

7.10

Cutter

4.95

7.87

E

5.44

7.31

Punch

5.25

7.57

L 15

5.65

7.10

Butter

5.10

7.72

L 15

5.45

7.30

T.C.

L 24

5.30

7.45

Punch

12+00

PX

Sta 10+00

12.75

4.40

8.35

Punch

12.82

5.5

7.3

PX

R 50

4.50

8.25

Punch

4.7

8.1

R 25

4.80

7.95

Punch

4.7

8.1

E

5.30

7.45

Punch

4.8

8.0

L 25

5.25

7.50

Punch

4.9

7.9

L 50

10.02

12.85

2.73

10.12

T.P.

Sta. 13+00

12.82

5.4

7.4

PX

T.P.

5.0

7.8

5.2

7.6

5.85

6.97

5.4

7.4

8-29-49⁽¹⁾

Sta 14+00

Sta 17+00

PX
 DIST + HI - Elev
 12.82
~~11.44~~

DIST + HI - Elev
 3.84 11.64
~~4.25 7.80~~
~~6.42~~

R. 50 5.70 7.12
 R. 25 5.65 7.17
 Q 5.40 7.42
 L. 25 5.35 7.47
 L. 50 5.3 7.5

R. 50 4.35 7.29
 R. 25 4.25 7.39
 E 5.15 6.49
 L. 25 4.60 7.04
 L. 50 4.60 7.04

Sta 15+00

Sta 18+00

PX
 R. 50 12.82 5.60 7.22
 R. 25 6.10 6.72
 Q 5.25 7.57
 L. 25 5.55 7.27
 L. 50 5.25 7.57

R. 50 11.64 4.60 7.04
 R. 25 4.75 6.89
 Q 4.55 7.09
~~6.09~~
 L. 25 4.40 7.14
 L. 50 4.75 6.89

Sta 16+00

Sta 19+00

PX
 R. 50 12.82 5.70 7.12
 R. 25 5.75 7.07
 Q 5.45 7.37
 L. 25 5.80 7.02
 L. 50 5.60 7.22
 T.P. 5.02 7.80
~~6.42~~

R. 50 11.64 5.10 6.54
 R. 25 5.15 6.49
 E 5.00 6.64
 L. 25 4.80 6.84
 L. 50 4.70 6.94

T.P.

T.P.
Sta 15

9-29-49 17
8-29-49

Sta 20+00

Dist	H _i	Elev
	11.64 +0.26	
Rt 50	5.70	6.54
R. 50	5.10	6.54
±	5.40	6.24
L. 25	5.50	6.14
L. 50	5.10	6.54

PX

Sta 21+00

Rt. 50	11.64	4.95	6.69
Rt. 25		4.90	6.74
±		5.10	6.54
L. 25		5.40	6.24
L. 50		5.60	6.04

PX

Sta 22+00

Rt 50	11.64	4.90	6.74
Rt 25		5.10	6.54
±		5.15	6.49
L. 25		5.30	6.34
L. 50		5.25	6.39

PX

T.P.

4.45
+4.5
7.19 Top L
5.81

Sta 23+00

Dist	H _i	Elev
T.P.	3.77	10.96 9.58
Rt 50		4.85
Rt 25		4.70
±		4.80
L. 25		4.75
L. 50		4.80

PX

Sta 24+00

Rt 50	10.96	4.85	6.11
Rt 25		4.75	6.21
±		4.75	6.21
L. 25		4.85	6.11
L. 50		4.90	6.06

PX

Sta 25+00

Rt 50	10.96	4.95	6.01
Rt 25		5.00	5.96
±		4.90	6.06
L. 25		4.80	6.16
L. 50		4.70	6.26

PX

Sta 26100

Dist	+	HI	-	Elev	
		10.96			
Rt 50		9.58	4.30	6.66	
Rt 25			4.50	6.46	
E			4.70	6.26	
L. 25			4.70	6.26	
L. 50			4.70	6.26	
			4.57	5.21	Top. H. 100
<u>T.P.</u>			4.37	6.59	P.I.
				7.16	Top. L. 100
T.T.P.			3.80	5.78	Sta. 250
		11.79			
	4.58	10.36			
				7.76	Top. L. 100
T.P.			3.98	6.37	Sta. 100
		12.68			
I.P.	4.92	11.29			
				9.94	Sta. 100
I.P.			2.74	8.56	
		12.66			
T.P.	2.72	12.27			
				8.45	N.W. C.
T.P.			4.21	8.06	C.P.A.
		14.11			
T.P.	5.66	13.76			
				11.57	Pire
			2.54	11.22	

8-29-49 19

STA - 27+04⁸⁸Sta 29+66⁶⁸ EC

DIST	+	H.I.	-	ELEV		DIST	+	H.I.	-	Elev
				<small>CORR.</small>	<small>TOP Hgt</small>					
					<small>P.I.</small>					
T.B.M	4.35	11.04		6.69		B.50		11.04	4.80	6.24
B.T. 30			4.40	6.64		B.15			4.80	6.24
B.T. 25			4.40	6.64		¢			4.80	6.24
¢			4.45	6.59		¢			4.70	6.34
L.T. 25			4.50	6.54		¢			4.50	6.54
L.T. 50			4.95	6.09						

Sta. 28+00

Sta 30+00

						B.50			4.60	6.44
Px						B.25			4.80	6.24
B.T. 50			4.50	6.54		¢			4.80	6.24
B.T. 25			4.25	6.79		¢			4.60	6.44
¢			4.20	6.84		¢			4.65	6.39
B.T. 25			4.20	6.84						
B.T. 42			4.4	6.64						

Sta 29+00

Sta. 31+00

						B.50			4.80	6.24
Px						B.25			4.60	6.44
B.T. 50			4.80	6.24		¢			5.7	5.3
B.T. 25			4.70	6.34		¢			6.7	4.3
¢			4.60	6.44		¢			5.0	6.0
L. 25			4.5	6.54		¢			5.0	6.0
L. 50			4.4	6.6		¢			4.8	6.2

8-29-47²⁰

Sta 32+00			
Dist	H.I.	*	Elev
PT 50	11.04	4.9	6.1
PT 25		5.0	6.0
⊥		5.1	5.9
PT 25		4.8	6.2
R. 50		5.0	6.0
T.P.	11.04	4.18	6.86

Dist	H.I.	*	Elev
T.P.	4.35	11.24	
Sta. 33			
PT 50		5.4	5.8
PT 25		5.2	6.0
⊥		5.1	6.1
L. 25		5.1	6.1
L. 50		5.1	6.1

Sta 34+00			
AT. 50		5.2	6.0
25'		5.2	6.0
⊥		5.3	5.9
L. 25'		5.3	5.9
L. 50		5.2	5.9

T.P. ³				
Dist	+	H.I.	-	Elev
TBM		11.21	4.99	6.22
T.P.	4.92	11.14		
T.P.			4.46	6.68
T.P.	4.52	11.20		
T.P.			3.99	7.21

Sta 35+00				
Dist	+	H.I.	-	ELEV
T.B.M.	5.90	12.12		6.22
PT-50'			6.1	6.0
PT-25'			6.2	5.9
⊥			6.2	5.9
PT-08'			6.4	5.7
PT-09'			8.5	3.6
PT-18'			6.8	5.3
PT-25'			6.4	5.7
PT-50'			6.2	5.9

50' SW STA-37+00
(1x2" IN CLEARING)

TOP LATH

Sta 22+00

3-7-19

1"x2" IN CLEARING
±50' SW STA 37+00

B.C. 35+70 ⁰⁹

DIST	+	H.I.	-	ELEV
T.B.M	5.90	12.12		6.22
RT-50'			6.2	5.9
RT-31'			6.2	5.9
RT-27'			9.3	2.8
RT-24'			8.6	3.5
RT-02'			7.2	4.9
• Q			6.1	6.1
LT-25'			5.8	6.3
LT-47'			2.6	9.5
LT-50'			2.0	10.1
T.B.M.			1.77	10.65

SEE PAGE 29

Top of
36+00

SEPT 10, 1949

SOUNDINGS OF SUBMARINE

SEWER MISSION BEACH

TO OCEAN BEACH

ANGLE S. JETTY TO MIDDLE

CHANNEL $\phi = 71^\circ 25'$

ANGLE ϕ CHANNEL TO N. JETTY

$\phi = 42^\circ 50' = 0+00$

DIST SOUND

DIST SOUND

0+00 22.3 -17.1

21.0 -15.0-80

(5.2) 22.3 -17.1

21.3 -16.0

23.0 -17.8

21.4

11:35 23.3 -18.1

50 21.8

23.0 -17.8

21.3

50 22.4 -17.2

21.7

21.8 -16.6

11:38 21.5

21.6 -16.4

21.2

21.9 -16.7

2+00 21.3

21.5 -16.3

(5.2) 21.7

1+00 21.6 -16.4

21.5

21.4 -16.2

21.7

2+40 21.7

DIST SOUND

0-10 21.5

0-20 21.7

0-30 21.8

(5.2) 0-40 21.0

0-50 21.0

0-60 21.0

0-70 21.0 = 17+50

= 17+00

16+70

2+00

14+30 ✓

A!
F. B.
IN PAGE (55)

240

80

320

1750

32

1430

1848

22

76

1752 330

Barge-75'

Add +1.2' to f.l. grade
 Soundings on top of pipe

Dist	Sound	+80 = 0 + 00	Grade
30 ⁰⁰		+2.2	
30	1.3	+3.4	12:23 +1.2
(4.7)		+2.2	
40 ⁰⁰	2.5	+2.2	+0.8
50 ⁰⁰	2.7	+0.8	
		+2.0	+0.4
60 ⁰⁰	2.7	+0.8	
		+2.0	12:25 0.0
70 ⁰⁰	3.2	+0.3	
		+1.5	-0.4

X-SECTIONS OF 500' R. CURVE AT INTERSECTION
OF PROPOSED DETOUR & MIDWAY

36+25

PX

NOTE
(B.C.=35+70⁰⁹)

36+00 (ON CURVE)

DIST	+	H.I.	-	ELEV	DIST	+	H.I.	-	ELEV
		19.89		10.65	LT-47		17.89	7.5	10.4
		19.89		10.65	LT-25			7.87	10.02
T.B.M	4.24	19.89		10.65	LT-25'			7.24	10.65
					LT-13'			5.9	9.0
BT-50'			8.8	6.1	LT-07			8.4	6.5
-25'			8.7	6.2	LT-01			9.0	5.9
¢			8.9	6.0	LT-25			8.8	6.1
LT. -20'			8.9	6.0	LT-50'			8.8	6.1
LT. -18'			7.6	10.3					
LT-38 ²			7.25	10.64					
LT-38 ⁵			7.3	10.0					
LT-50'			7.71	10.18					

TOPOG. MAP
36+00

5%

90%

PAVING

GUTTER

CURB

PX 36+50

DIST	+	H.I.	-	ELEV
RT-50'		² 14.89	9.0	5.9
RT-25'			9.2	5.7
RT-09'			9.2	5.7
⊥			7.3	7.6
LT-07			9.4	10.5
LT-19'			9.2	10.68 CURB
LT 19'			9.82	10.07 GUTTER
LT 36			9.53 [?]	10.36

36+75

PX

DIST	+	H.I.	-	ELEV
LT-25'		² 14.89	9.52	10.37
RT-05			9.02	10.07 GUTTER
RT-05			9.23	10.66 CURB
⊥			9.3	10.6
RT-07			5.0	9.9
RT-19'			9.3	5.6
RT-25'			9.3	5.6
RT-50'			9.1	5.8

37+60

DIST	H.I.	-	ELEV
PT-50	14.89	9.2	5.7
PT-25'		9.3	5.6
PT-20'		9.3	5.6
PT-15'		9.8	10.1
PT-2 ⁵ '		9.29	10.60 CURB
PT-2 ⁵ '		9.86	10.03 GUTTER
⊥		9.80	10.09
LT.-18 ³ '		9.55	10.39

37+25

(26)

DIST	H.I.	-	ELEV
LT-12	14.89	9.18	10.91
⊥		9.72	10.17
PT-09		9.85	10.04 GUTTER
PT-08		9.20	10.69 CURB
PT-18		9.8	10.1
PT-25		9.3	5.6
PT-50		9.3	5.6

DIST	H.L.	-	FLEV
37+50			
RT-50	14.89	9.3	5.6
RT-31		9.3	5.6
RT-23		4.5	10.9
RT-13'		9.11	10.78
RT-13'		9.79	10.10
℄		4.51	10.38
LT-07		4.41	10.48

PROFILE 40' EAST OF ℄

0+60 ℄
0+40 EAST

DIST	H.L.	-	FLEV
STA +			
B.M.	4.72	13.06	9.33
0+70		9.9	3.2
0+60		8.5	4.6
0+50		7.1	6.0
0+40		6.6	6.5
0+30		5.7	7.4

U.S.E.D. DIEGO

PROFILE ALONG ℄ OF SEWER LINE

0+80

DIST	H.L.	-	FLEV
0+85		13.06	3.7
0+80		7.8	5.3
0+70		6.9	6.2
0+60		6.2	6.9
0+50		5.5	7.6
0+40		5.1	7.7

CHECK SOUNDINGS ALONG ℄ PARALLEL
TO CENTER LINE AND CROSS SECTIONS
OF DREDGED CHANNEL FOR SUBMARINE SEWER
MISSION BEACH SHORE
0+00 FOR ℄ = PT. 112' S 56° 42' 40" W OF U.S.E.D. DIEGO

NOTE

SOUNDINGS IN F.B. NO 41 P.P. 62-68

(0+60 &
0+90 WEST)
PROFILE 40' WEST OF R

STA	+	H.I.	-	ELEV
0+65		13.06 ¹	5.2	7.9
0+60			4.9	8.2
0+50			4.2	8.9
0+40			4.3	8.8
0+30			4.21	8.75
0+28			4.10	8.96

(0+85 WEST
0+60 &)
PROFILE 85' WEST OF R

STA	+	H.I.	-	ELEV
1+15		13.06 ¹	7.1	6.0
1+10			6.7	6.9
1+00			5.8	7.3
0+90			5.0	8.1
0+80			4.7	8.4
0+70			4.5	8.6
0+67			4.3	8.8
0+61			4.2	8.9
0+60			4.2	8.9

(0+80 WEST
1+00 &)
9-18-43
X-SECTION

(28)

STA	+	H.I.	-	ELEV
0+80W		13.06 ¹	8.0	5.1
0+90W			5.5	7.6
1+00W			5.1	8.0
1+10W			4.8	8.3
1+20W			4.2	8.9

(1+50 &
1+40W)
X-SECTION

STA	+	H.I.	-	ELEV
1+36W		13.06 ¹	7.3	5.8
1+40W			7.5	5.6
1+42W			6.7	6.1
1+50W			6.5	6.5
1+60W			6.3	6.8
1+70W			6.1	7.0
1+80W			3.9	9.2

SOUTH

SIDEWALK

NORTH
SIDEWALK

SIDE
WALK

SIDE
WALK

(2+00 ±
1+50 WEST) X-SECTION

STA	+	H.I.	-	ELEV
1+40W		13.06	10.0 9.8	3.1
1+50W			9.8	3.3
1+60W			9.1	4.0
1+70W			7.6	5.5
1+74 W			6.5	6.6
1+80W			6.2	6.9
1+85W			5.1	8.0

(1+70W
2+50 ±) - X-SECTION

STA	+	H.I.	-	ELEV
1+65W		13.06	7.1	6.0
1+70W			5.2	7.9
1+85W			1.8	8.3
1+90W			4.6	8.5

TOPO FOR DRAINAGE - SANTA CLARA POINT

STAMPES BARRAGAN WATSON 9-20-49

30

X @ SOUTH RADIUS SANTA CLARA POINT AZIM. TO CLARA =
H.I. = 16.22 [358° 45' 18"]

STA	DIST	AZIM	ROD	ELEV
1	123'	33° 13'	5.14	11.08
2	116'	37° 12'	5.20	11.02
3	103'	41° 30'	5.23	10.99
4	103'	47° 12'	5.27	10.93
5	96'	54° 53'	5.39	10.85
6	83'	50° 06'	5.40	10.82
7	72'	57° 45'	5.35	10.80
8	60'	60° 40'	5.29	10.79
9	49'	57° 20'	5.29	10.78
10	39'	76° 15'	5.26	10.75
11	27'	89° 05'	5.28	10.74
12	17'	112° 15'	5.27	10.73
13	10'	164° 20'	5.28	10.72
14	15'	222° 05'	5.24	10.71
15	33'	296° 35'	5.24	10.70
16	39'	259° 55'	5.26	10.70
17	50'	270° 09'	5.25	10.69
18	63'	275° 32'	5.37	10.85
19	75'	275° 10'	5.45	10.77

STA	DIST	AZIM	ROD	ELEV
20	83'	290° 00'	5.49	10.73
21	91'	290° 00'	4.86	11.36 Top Wk
22	85'	281° 35'	4.90	11.32
23	84'	279° 40'	4.90	11.32 Top Wk
24	84'	276° 35'	4.88	11.34 Boathse.
25	83'	274° 50'	4.91	11.31
26	109'	271° 25'	4.92	11.30
27	128'	269° 13'	4.89	11.33
28	97'	57° 50'		(35° To Payment)
29	130'	62° 18'		} = PT. ON R
			5.	
				+0.41
				15.81
				H.I. = 16.22

Elev. Top OF FIRE HYDRANT

(DRAIN PROFILE) 27 9-20-43

PROFILE SOUTH OF BOAT HOUSE - SANTA CLARA RIVER

0+00 = PT. 2' SOUTH OF SE COR. CONC. PAD. IN THE STA

STA DIST AZIM ROD ELEV

0+00 82' 275° 00' 5.43 10.73 0+05

0+15 H.I. = 16.22 5.1 11.1 0+10

0+25 5.2 11.3 0+20

0+50 130' 88° 20' 268° 20' 5.2 11.0 0+30

0+60 5.9 10.3 0+40

0+70 6.0 10.1 0+50

0+80 7.5 8.7 0+60

0+90 9.5 6.7 0+70

1+00 10.1 5.9 0+80

1+10 11.7 4.8 0+90

1+20 12.6 3.6 1+00

1+30 13.7 2.9 1+10

1+40 13.2 3.0 1+20

1+50 230' 13.0 1.15 14.2 2.0

65
+05

70

9-20-43 (31) 2-27-43

(DRAIN PROFILE)

PROFILE @ EAST SHORE OF SOUTH RADIUS

DIST AZIM ROD ELEV

137' 54° 50' H.I. = 16.22 > 5.4 10.8

4.9 11.3

4.8 11.4

5.0 11.2

5.5 10.7

6.4 9.8

7.5 8.7

8.3 6.9

9.7 6.5

10.1 6.1

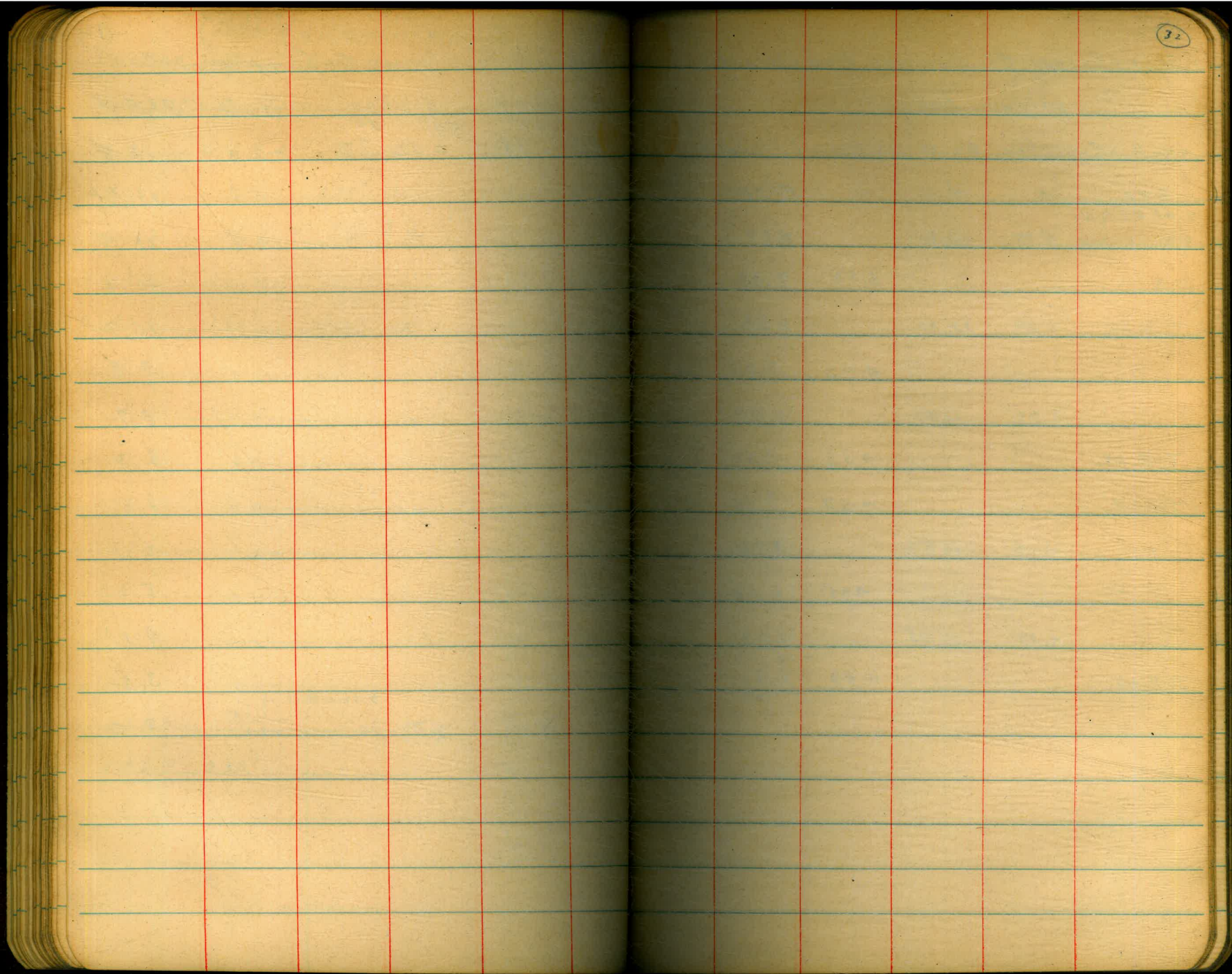
11.0 5.2

12.1 4.1

12.9 3.3

Bottom Hair 13.1 1.05 14.2 2.0

Bottom Hair 13.1
1.05
14.2



SLOPE STAKES & GRADES FOR DETOUR

MIDWAY DRIVE

0+00 = COPPER DISC P.I. MIDWAY DRIVE & NASHVILLE

STA	F	H.I.	-	ELEV
CURB RETURN				
W/SIDE DISC	4.37	12.91		8.54
T.B.M.			5.53	7.38
T.B.M.	5.49	12.87		7.38
"			4.90	7.37
"	3.96	11.93		7.97
T.B.M.			4.53	7.40
T.B.M.			4.59	7.34
"	4.19	11.53		7.34
T.P.			4.95	6.58
"	4.87	11.45		6.58
T.B.M.			4.89	6.59
				6.56
				.03

6.59 P.I.

(33)

7.34	6.58
4.19	4.87
11.53	11.45
	4.89
	6.56

11.5
5.0
6.5

242
RIGHT
1970
200
LEFT
13700
" "
240 @ P.I.
" " EL-510

LOCATION OF CONTOURS FOR PROPOSED FILL ---

OCEAN BEACH PARK ANNEX & TOPO ALONG REAR
OF LOTS

STA	+	H.I.	-	ELEV	U.S.S.
B.M	3.80	18.89		9.09	" JEEP
T.P. #1	4.31	17.37	5.78	13.06	"
T.P. #2	4.50	18.90	2.97	14.90	"
B.M	1.76				
B.M.	1.76	3,4.81		33.05	
	2.68	24.94	12.55	22.26	
B.M	3.02	36.07		33.05	
	0.41	30.91	5.57	30.50	
			9.70		
		26.24	5.04	21.21	
		26.29	5.43	20.81	
	1.17	24.17		20.00	
			3.79	20.38	

WALK TIP WALK LOTS - 34-35

FOUNDATION BUILDING BEHIND LOTS 36-37

CONTOURS FOR PROPOSED FILL

STA	+	H.L.	-	ELEV
B.M.	4.67	37.72		33.05
T.P.	3.14	28.13	12.73	29.99
			2.0	21.1
			2.1	21.0
T.P.	3.14	23.96	7.31	20.82
			4.43	19.53
			3.65	20.31
			2.50	21.96
			2.31	21.65
			1.96	22.00
T.P.	9.05	29.05		22.00
			4.60	24.95
				20.81
				20.0
				20.0
				18.0
				21.5
				12.0
				17.7

TOP OF RETAINING WALL LOT-38-39

TOP OF RETAINING WALL LOT-39-40-41

T.P. OF WALL (CONC) LOT-42-43

TOP OF CONC STEPS LOT-44-

FLOOR LEVEL HOUSE REAR LOT 44-

TOP OF RAMPING OF STAIRS (CONC) LOT-46

TOP OF WALL LINE LOT 3-

T.P.

FLOOR LEVEL BASEMENT GAR HOUSE-LOT 3-7

TOP OF RETAINING WALL (CONC) - 32-33

TOP IN BANK LOTS - 30-31 (VACANT)

TOP CONC STEPS LOTS - 28-29

BASE FOOTING HOUSE REAR LOT-28

BASE FOOTING HOUSE REAR LOT-27

HOUSE IN REAR

TOP CONC LANDING HEAD OF STAIRS - 24-25

TOP RETAINING WALL (WOODEN) LOT-24

CONTOURS FOR PROPOSED FILL

20.5
1.6
18.9

(30)

STA	+	H.L.	-	ELEV	
				16.00	GROUND EL. @ FOOTING (WOOD) LATH HOUSE E
				18.0	SUN DECK REAR HOUSE - LOT - 22-23 EL. OF GROUND INSIDE CONC BLOCK WALL REAR HOUSES LOT - 20-21
				15.0	EL. REAR LATH HOUSE (DIRT) REAR HOUSE LOT-16-17
				18.9	GROUND EL. @ REAR HOUSE - 16-17
T.B.M.	4.53	20.53		16.00	100- FEET CONTOUR
			3.3	17.2	EL. OF GROUND @ CORN FOOTING OF GAR
			1.2	12.3	FLOOR LEVEL SAME GAR REAR - LOT-19-15
			1.07	19.46	FLOOR EL BASEMENT HOUSE REAR
			0.95	19.50	GROUND EL. @ FOOT OF NORTH WALL HOUSE - W LOT-10-11
			4.15	16.38	EL. OF GROUND NORTH END OF GARDEN (LAWN)
			5.5		HOUSE LOTS - 10-11
			5.5	15.0	VACANT PRK IN BANK REAR LOTS - 3-9 INCLUSIVE
			7.85	12.68	EL. OF GROUND @ NORTH WALL GAR. REAR LOT-1-2
T.P	4.40	20.40		16.00	T.P
			6.5	13.9	GROUND EL. @ NORTH WALL SMALL BUILDING (GAR.?) REAR LOT - T-4

CONTINUATION OF LEVEL FOR PROPOSED FILL

(CONT.)

STA	+ H.I.	-	ELEV
T.B.M. I	4.85	40.09	35.24
T.P.	1.38	29.81	11.66 28.93
		4.47	25.39
		3.71	26.10
		12.3	17.5
			-4.5
			13.0
		12.7	17.1
			-2.8
			14.3
			26.10
			2
			25.90
T.B.M.	3.53	38.82	35.24
T.P.	6.10	34.92	10.50 28.32
		4.55	23.87
		10.12	24.30
		14.00	23.92
			3.1
			20.0
T.P.	0.80	29.23	28.43
		5.95	23.28
		3.42	25.81
T.P.	8.18	36.26	1.15 28.08

(21-22) 27.81
3.31
24.50
9-10 (38)

39.46
28.00
16.92

LOTS (11-12)
10-11

(conc)
TOP CONC WALL REAR LOTS (11-12) (HIGHEST)

" " " " " (9-10)

(conc)
UPPER RET. WALL LOTS (9-10)

(conc)
LOWER WALL LOTS (9-10)

LOWER WALL (conc) LOTS (11-12)

TOP OF CONC FOUNDATION SHED IN REAR LOTS (7-8)
(GAR.?)

NO. I

GRAND CONC WALL HOUSE LOTS (8-7)

GRAND CONC FENCE REAR " (8-7)

TOP RETAINING WALL (WOOD & CONC) REAR LOT (7)

" " " " " " " " " " " LOT (8)

CONC LANDING TOP CONC STAIRS REAR LOT - 13

GRAND CONC WALL HOUSE REAR LOT - 14

WIND OF YARD LOTS (15-17) VACANT

CONTOURS & LEVELS FOR PROPOSED FILL (CONT'D)

STA + H.I. - ELEV

T.P 8.18 36.26 28.08

4.73 32.53

9.0 27.3

11.05 25.21

NO IV

T.B.M 0.30 38.33 38.03

6.50 31.83

8.4 29.9

3.40 39.93

5.50 32.83

T.P 9.05 37.05 28.00

5.0 32.0

11.43 25.52

N^o V

T.B.M. 1.28 38.25 37.07

10.4 27.9

7.80 30.55

7.05 31.30

T.P, 4.32 35.62 31.30

5.87 29.75

6.51 29.11

GRAND @ N/WALL HOUSE LOTS (17-18) 36.26
38
38.26

TOP OF SLOPE OF BANK (19-20) VACANT
(HANK IMPROVED)

CONC PATIO REAR HOUSE (21-22)

N^o IV @ E/SIDE WALK

CONC PAD REAR HOUSE LOTS (21-22) APPROX FILL

GRAND @ TOP OF SLOPE VACANT (23-24)

FIR FL. GAR REAR LOTS (25-25) & (26)

T.P RETAINING WALL (WOODEN) LOT (27-28)

T.P GRAND FOOT OF RETAINING WALL

FLOOR FL. OF TOOL SHED REAR LOTS (29-30)

T.P OF SLOPE (VACANT) (31-38) (INC)

T.P DIRT PATIO FLOOR LOT (39)

T.P CONC RET. WALL LOT (40)

GRAND @ N/WALL OF HOUSE LOTS (41-42)

FLOOR BUILT FOR CONC RET. WALL LOTS (41-42)

LEVELS FOR PROPOSED FILL (CONT'D)

STA	+	H.L.	-	ELEV	
T.B.M. N ^o VII	0.75	36.88		36.13	
			8.3	28.6	GROUND EL. @ N/END OF WIRE FENCE & WEDGE LOTS - (47-49)
			8.9	28.0	FL. GRND OUTSIDE FENCE (REAR) LOTS - (47-49)
			7.0	29.9	FLOOR LEVEL GARAGE (REAR) LOTS - (47-49)
			8.9	28.0	GRND EL. @ N/WALL OF GAR (REAR) LOTS - (47-49)
			8.9	28.0	SETBACK (VACANT) LOTS (45-46)
			8.47	28.41	TOP CONC BLOCK WALL AROUND PATIO (NEW) (47-48)
			7.37	27.61	FLOOR (CONC) OF PATIO (NEW) (47-48)
			9.5	27.4	GROUND EL. @ T/OARD FENCE REAR LOT - (48)
T.P.	4.71	32.29	9.30	27.59	T.P. N/E COR CONC PATIO
			6.4	25.9	GRND EL. @ N/SIDE OF CONC WALL LOTS (49-50)
			+0.10	32.4	T/O OF WALL CONC LOTS (49-50)
			3.7	28.6	GRND EL. INSIDE WALL LOTS (49-50)
			3.9	28.4	T/O OF STEPS (CONC) LOTS - (49-50)
T.P.	4.31	32.31		28.00	
			2.8	29.5	T/O OF STEPS & GRND EL. OF YARD LOTS - (51-52)
			1.2	31.1	GRND EL. AT N/FENCE (53) -
			10.8	21.5	FLOOR EL. 2 STORY SMALL BUILDING REAR LOTS - (53-54)
			1.7	30.6	FL. @ GATE TO MAIN YARD LOTS (53-54)

32.20
492
27.57

± LEVELS

CONTOURS FOR PROPOSED FILL-OCEAN BEACH CONCLUDE

STA	+	H.L.	-	ELEV.
B.M.	0.55	39.68		39.13
			11.68	28.0
			11.68	28.0
B.M.	-0.10	39.03		39.13
			11.03	28.0

39.0
 9.1
 39.7

(4)

39.09
 21.68

TOP FIRE HYDRANT SEASIDE LANE W/ POINT LOMA
 SET HUB NO IMPROVEMENTS (REAR) LOTS - (55-56)
 (SET HUB) (NO IMPROVEMENTS VACANT) LOTS - (57-58)
 IN MIDDLE (59-60) (61-62) (ALL VACANT),
 TOP FIRE HYDRANT SEASIDE LANE
 SET HUB IN CENTER OF YARD MARKED 28.0 CONTOUR
 ± @ FOOT OF OLD CONC. FOUNDATION
 ALSO ON WOODEN STEPS ON S/E SLOPE

SITUATION SURVEY NEAR GLEN'S DRIVE IN (LOTS 53 TO 58)
FOR PROPOSED STORM DRAIN EXTENSION

(BLOCK 103 OCEAN BAY BEACH)

STAMPER
BARRAGAN
WATSON
SHERRY

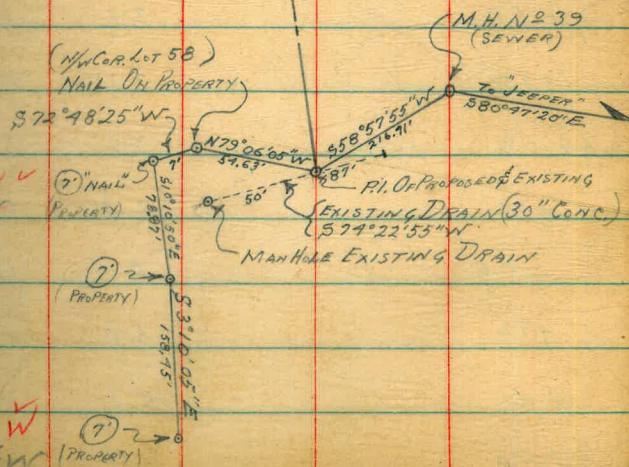
11-1-49

(42)

STA. OBJECT ANGLE DIST BEARING

STA.	OBJECT	ANGLE	DIST	BEARING
	"JEEPER"	① 70° 15'		S 80° 47' 26" E To "JEEPER"
M.H.N. 39	DEF. LT.	② 80° 29' 30"		
	P.I. EXISTING DRAIN & PROPOSED DRAIN	AV 70° 14' 45" ✓	216.71'	S 58° 57' 55" W ✓
	M.H.N. 39	① 67° 07' 33" ✓		
P.I.	∠ LT. -			
	∠ PROPOSED DRAIN		(NOT CHANGED)	N 8° 09' 38" W ✓
	M.H.N. 39	① 164° 35'		
P.I.	∠ LT.			
	EXISTING M.H. DRAIN		50.00'	S 74° 22' 55" W ✓ S 43° 17' 55" W
	M.H.N. 39	① 138° 04'		
P.I.	∠ LT.			
	To TACK PROP LINE		54.63'	N 79° 06' 05" W ✓ S 17° 01' 55" W
	P.I. DRAINS	① 151° 54' 30"		
TACK ON PROP	∠ RIGHT			
	7' "NAIL" OFF		7.00'	S 72° 48' 25" W ✓ S 45° 07' 35" W (PROPERTY)

Profile To 1100 (CAND.) (EA = 2.6)



STA	+	H.I.	-	ELEV	
T.B.M	7.00	20.20		13.2	RIM OF M.H. NO. 37
BOTTOM M.H. (DRAIN)			12.90	<u>7.30</u>	TRUNK (UNDER) BOTTOM M.H. DRAIN
RIM M.H. DRAIN			4.43	15.77	RIM M.H.
50' FROM EXISTING M.H. (DRAIN)			5.30	14.90	P.I. POINT EXISTING DRAIN
72' FROM M.H. (EXISTING)			5.5	14.7	GROUND
87'					F.L. END OF 30" RCP.
89' " " (F.L.)					DRAIN outlet
		TOP PIPE 12.08		5.37	
		PIPE THICKNESS + 2.75			
		Red on Fl. = 19.83		5.4	
T.P.	3.30	18.82	4.68	15.52	RIM OF SEWER MAN HOLE
0+00			3.9	14.9	
+12'			3.4	15.4	
+25'			3.4	15.4	
+50'			3.4	15.4	
+75'			3.35	15.5	
1+00			3.5	15.3	
+25			3.85	14.9	
+50			4.35	13.5	
+72			5.0	13.8	
+81			5.1	13.7	
2+00			6.4	12.4	

7.30
 $2.22\% \text{ Grade} \times 50' = -1.11 = 6.22 \text{ FL.}$
 at 0+00 of Proposed Drain

STA	+	H.I.	-	ELEV
2+25		18.82	6.8	12.2
+50			7.1	11.7
+75			7.3	11.5
3+00			7.8	11.0
+25			8.0	10.8
+33			8.1	10.7
+36			8.5	10.3
+39			10.1	8.7
+51			11.0	7.8
+80			13.1 14.1 +2.0 15.7	3.4
4+00			13.2 13.0 16.2	2.6
SEWER			10.00	8.87
M.H.				

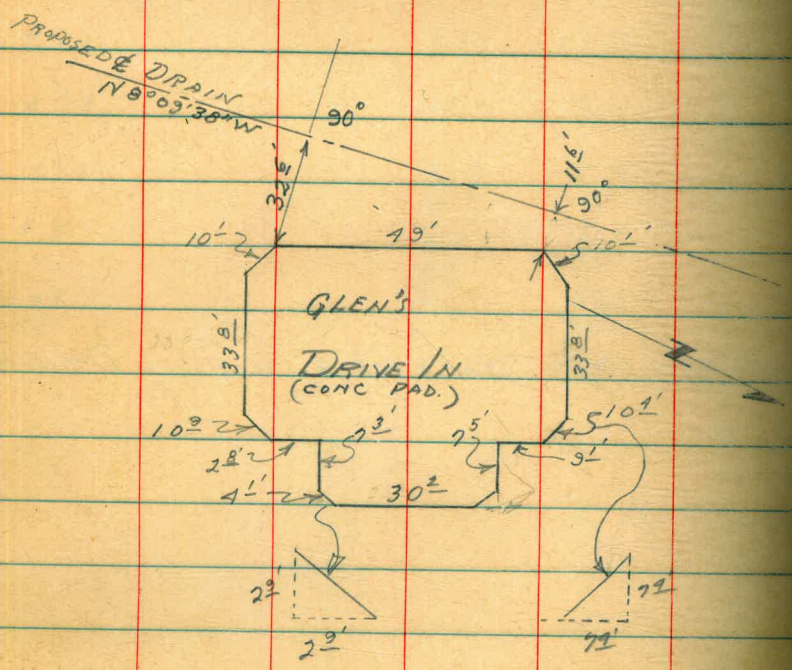
FLOW LINE
23' TO RL

(15.52 - 6.70)

23' FROM M.H. TO STA-0+25 & PROPOSED DRAIN

LOCATION OF GLEN'S DRIVE IN
 0+00= P.I. OF EXISTING DRAIN & PROPOSED EXTENSION

	15.3	20.4	
	@ 90° To $\frac{BL}{EAST}$		
0+65 ³	32 ⁶		
0+70 ⁴	23 ⁹	"	
1+17 ²	11 ⁶	"	
1+26 ⁶	16 ⁸	"	
1+35 ⁰	49 ⁵		



LOCATION OF E
PROFILE OF PROPOSED DRAIN AT NORTH

SIDE OF BOAT BUILDING SANTA CLARA

STA	+	H.I.	-	ELEV
B.M.	1.30	17.11		15.81

			5.81	11.30
			5.82	11.29

0+00 = POINT AT EDGE OF A.C. PAVING

STA	+	H.I.	-	ELEV
T.B.M	4.20	15.49		11.29

0+00			4.61	10.9
------	--	--	------	------

+10			4.5	11.0
-----	--	--	-----	------

+20			4.8	10.7
-----	--	--	-----	------

+30			5.0	10.5
-----	--	--	-----	------

+			5.2	10.3
---	--	--	-----	------

+39			7.1	8.9
-----	--	--	-----	-----

+50			9.0	6.5
-----	--	--	-----	-----

+60			10.0	5.5
-----	--	--	------	-----

+70			10.8	4.7
-----	--	--	------	-----

+80			11.7	3.8
-----	--	--	------	-----

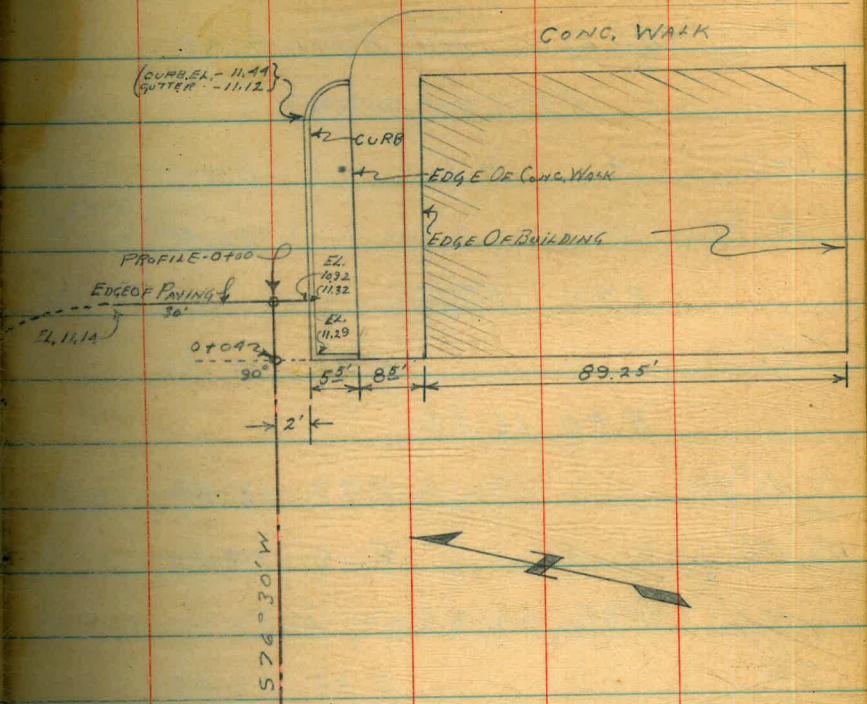
+90			12.4	3.1
-----	--	--	------	-----

0+99			13.5	1.9
------	--	--	------	-----

1/2" COR. OF CONC. PAD OF B.A.D.S.
1/4" COR. OF CONC. PAD OF B.A.D.S.

1/4" COR. CONC. PAD OF DRAIN TO P. OF WEST EDGE OF PAVING

EDGE OF WATER



H.I. = 15.49

STA	- ROD CURB	- ROD GUTTER	ELEV CURB	ELEV GUTTER
ELEVATIONS ALONG TOP OF CURB & GUTTER				
0	-4.20		11.29	
4'E	-4.17	-4.57	11.32	10.92
10'E	-4.17	-4.50	11.32	10.99
20'E	-4.11	-4.43	11.38	11.06
30'E	-4.09	-4.49	11.40	11.00
36'E	-4.05	-4.39	11.44	11.12
ELEVATIONS ALONG PAVING				
10' NORTH		-4.51		10.98
20' NORTH		-4.44		11.05
30' NORTH		-4.35		11.14

TRUNK SEWER N^o 4 ALONG
(ABANDONED)
OLD ELECTRIC RAILROAD

June 9, 1950 T. Stampler

T H. Brown
φ A. Sherry

(17)

BENCH LEVELS

Datum = U.S. C. & G. S. M. L. L. W.

Sta	+	H.I.	-	Elev.	
B. M.				12.12	in East Curb Brass Plug About 10' South of South End of Mission Beach Bridge
	2.97	15.09			
TP.			4.33	10.76	
	5.50	16.26			
M. H. #39			3.27	12.99	Top of Cover on φ M. H. side Shot
TP B. M.			2.16	14.10	U.S.E.D. Jeepers 6"x6" Conc Man. Approx 200' E of Glenns Cafe & on Sly Crest of old RR Dike
	4.55	18.65			
TP.			5.32	13.33	
	5.09	18.42			
M. H. #40			5.62	12.80	Top of Cover φ M. H.
TP M. H. #41			6.33	12.09	Top of Cover φ M. H.
	5.48	17.57			
TP M. H. #42			4.92	12.65	Top of Cover φ M. H.
	6.56	19.21			
TP M. H. #43			7.13 7.17	12.09 12.04	Top of Cover φ M. H.
	6.69	18.78			
TP M. H. #44			7.03	11.75	Top of Cover φ M. H.

BENCH LEVELS CONT'D.

June 9, 1950

48

Sta	+	HI	-	Elev.	
TP MH #44				11.75	Top of cover & M.H.
	3.91	15.66			
TP MH #45			3.01	12.65	Top of cover & M.H.
	5.12	17.77			
TP MH #46			4.53	13.24	Top of cover & M.H.
	3.76	17.00			
B.M. TP			5.41	11.59 - .41	Conc. Mon. City Engineers, "Famosa"
Elec. M.H.			5.41	11.59	Top of cover & M.H. ^{south west side of bridge}
B.M.			3.45	13.55	Cluster of 3 nails in stringer at N.W. Corr. west end of R.R. Bridge Famosa Bl.
Elec. M.H.				11.59	South West Corner R.R. Bridge
	5.85	17.44			
M.H. #47			6.48	10.96	Top of cover & M.H.

Aug 6. 1950

PX

Sta 8+50

0+00 = sta 8+50 on $\frac{3}{4}$ Sound South

Dist	Sound		Dist	Sound	
0+00	?		3+10	14.0	-11.1
1+38	0.0	2.9	+70	13.5	-10.6
+40	5.5	-2.6	+30	12.8	-9.9
+50	10.6	-7.7	+40	12.9	-10.0
+60	14.3	-11.4	+50	12.9	-10.0
+70	14.6	-11.7	+60	13.2	-10.3
+80	13.7	-10.8	+70	13.5	-10.6
+90	12.0	-9.1	+80	13.2	-10.3
2+00	12.0	-9.1	+90	13.7	-10.6
+10	12.0	-9.1	4+00	13.6	-10.7
+20	11.9	-9.0	+10	12.9	-10.1
+30	13.0	-10.1	+20	11.2	-8.3
+40	13.6	-10.7	+30	7.7	-4.1
+50	13.9	-11.0	+40	1.8	+1.1
+60	14.3	-11.4	(10.09)		
+70	14.4	-11.5	(3.0)		
+80	14.7	-11.8			
+90	14.8	-11.9			
3+00	14.5	-11.6			

PX

Sta 9+00

(50)

0+00 = sta 9+00 on $\frac{3}{4}$ Sound South

Dist	Sound		Dist	Sound	
0+00	?		3+10	14.3	-11.3
1+27	0.0	3.0	+70	13.7	-10.1
+30	0.5	12.5	+30	13.3	-10.3
+40	3.1	-0.1	+40	13.7	-10.7
+50	6.0	-3.0	+50	13.6	-10.6
+60	9.0	-6.0	+60	13.9	-10.9
+70	10.3	-7.3	+70	13.8	-10.8
+80	11.5	-8.5	+80	13.1	-10.1
+90	12.7	-9.7	+90	12.4	-9.4
+10	13.8	-10.3	4+00	12.8	-9.8
+20	13.5	-10.5	+10	16.0	-13.0
+30	13.1	-10.1	+20	16.4	-13.4
+40	13.7	-10.7	+30	13.8	-10.8
+50	14.1	-11.1	+40	11.3	-8.3
+60	12.6	-9.6	+50	8.7	-5.7
+70	13.2	-10.2	+60	4.7	-1.7
+80	13.1	-10.1	+70	3.1	-0.1
+90	13.9	-10.9	+80	1.0	+2.0
+10	14.3	-11.3	(10.20)		
3+00	14.4	-11.4			

Px Sta 9+50

0+00 = Sta. 9+50 on $\frac{3}{4}$ Sound South

Dist	Sound		Dist	Sound	
0+00	?		3+40	14.6	-11.2
(10.25)					
1+51 (3.4)	0.0	+3.4	+50	14.5	-11.1
+60	3.1	+0.3	+60	14.8	-11.4
+70	6.2	-2.8	+70	15.0	-11.6
+80	9.9	-6.5	+80	15.1	-11.7
+90	12.8	-9.4	+90	14.9	-11.5
2+00	13.3	-9.9	4+00	13.3	-9.9
+10	14.1	-10.7	+10	12.7	-9.3
+20	15.2	-11.8	+20	12.8	-9.4
+30	14.0	-10.6	+30	12.0	-8.6
+40	14.7	-11.3	+40	12.9	-9.5
+50	14.9	-11.5	+50	13.9	-10.5
+60	14.8	-11.4	+60	12.8	-9.4
+70	14.7	-11.3	+70	9.1	-5.7
+80	13.9	-10.5	+80	8.0	-4.6
+90	13.3	-9.9	+90	3.9	-0.5
3+00	14.0	-10.6			
+10	15.1	-11.7	5+00	1.3	+2.1
+20	15.2	-11.8			
+30	14.9	-11.5	(10.33)		
			(3.4)		

Px Sta. 10+00

0+00 = Sta. 10+00 on $\frac{3}{4}$ Sound South

Dist	Sound		Dist	Sound	
0+00	?		3+10	13.1	-9.7
(3.4)					
+97	0.0	+3.4	+20	14.2	-10.8
+110	0.3	+3.1	+30	14.8	-11.4
+20	0.6	+2.8	+40	14.6	-11.2
+30	1.0	+2.4	+50	14.7	-11.3
+40	1.3	+2.1	+60	15.0	-11.6
+50	1.5	+1.9	+70	15.5	-12.1
+60	2.0	+1.4	+80	15.2	-11.8
+70	3.0	+0.4	+90	15.0	-11.6
+80	6.8	-3.4	4+00	14.1	-10.7
+90	10.0	-6.6	+10	14.0	-10.6
2+00	14.8	-11.4	+20	16.2	-11.8
+10	15.9	-12.5	+30	14.4	-11.0
+20	13.7	-10.3	+40	15.0	-11.6
+30	13.8	-10.4	+50	15.9	-12.5
+40	14.8	-11.4	+60	15.9	-12.5
+50	15.7	-12.3	+70	14.7	-11.3
+60	15.2	-11.8	+80	10.4	-7.0
+70	15.1	-11.7	+90	5	
+80	15.0	-11.6	+100	5.3	-1.9
+90	15.1	-11.7	3+00	3.8	-0.4
3+00	14.0	-10.6	+10	2.0	+1.4
			+20	1.0	+2.4

PX

Sta 10+00

0+00 = Sta 10+00 on $\frac{3}{4}$ Sound at 45° to $\frac{3}{4}$

Dist	Sound		Dist	Sound	
0+00	(4.2)		2+70	2.9	+1.3
10:58					
+64	0.0	+4.2	+80	2.2	+2.0
+70	1.0	+3.2	+90	2.3	+1.9
+80	1.8	+2.4	3+00	2.5	+1.7
+90	2.6	+1.6	+10	2.6	+1.6
1+00	5.6	+0.6	+20	3.0	+1.2
+10	3.5	+0.7	+30	3.7	+0.5
+20	4.0	+0.2	+40	4.2	0.0
+30	4.5	-0.3	+50	6.3	-2.1
+40	5.0	-0.8	+60	7.3	-3.2
+50	4.6	-0.4	+70	7.3	-3.2
+60	4.5	-0.3	+80	8.5	-4.3
+70	4.5	-0.3	+90	10.0	-5.8
+80	4.8	-0.6	4+00	7.3	-3.1
+90	5.0	-0.8			
2+00	5.0	-0.8	+10	11.2	-7.0
+10					
+20	4.1	+0.1	+20	13.0	-8.8
+30	3.9	+0.3			
+40	3.2	+1.0	+30	13.2	-9.0
+50	2.8	+1.4			
+60	3.2	+1.0	+40	13.3	-9.1
	2.9	+1.3			

7-1-50

(52)

PX

Dist	Sound	
3+50	13.2	-9.0
40	12.5	-8.3
50	12.4	-8.2
60	12.0	-7.8
70	12.5	-8.3
80	12.8	-8.6
90	13.0	-8.8
100	13.0	-8.8
110	13.2	-9.0
120	13.0	-8.8
130	13.0	-8.8

11:18
(4)

(A.2) Sta 10+00 P+

7-150

(53)

PX

0+00 - Sta 10+00 on Bl Sound West

Dist	Sound		Dist	Sound		Dist	Sound	
0+00			2+30	2.4	+1.8	4+10	10.7	-6.5
11:14								
+67	0.0	+4.2	+40	2.1	+1.8	+20	11.6	-7.4
+70	0.8	+3.4	+50	2.0	+2.2	+30	12.1	-7.9
+80	1.5	+2.7	+60	2.1	+1.8	+40	12.8	-8.6
+90	2.0	+2.2	+70	2.8	+1.4			
1+00	2.8	+1.4	+80	3.0	+1.2			
+10	3.1	+1.1	+90	3.2	+1.0			
+20	5.6	-1.4	3+00	3.2	+1.0			
+30	6.2	-2.0	+10	3.8	+0.4			
+40	6.5	-2.3	+20	4.0	+0.2			
+50	6.2	-2.0	+30	3.8	+0.4			
+60	6.2	-2.0	+40	4.0	+0.2			
+70	4.0	+0.2	+50	4.0	+0.2			
+80	3.0	+1.2	+60	4.8	-0.6			
+90	3.0	+1.2	+70	5.5	-1.3			
2+00	3.0	+1.2	+80	5.9	-1.7			
+10	2.8	+1.4	+90	6.8	-2.6			
+20	2.6	+1.6	4+00	8.7	-4.5			
				10.0	-5.8			

Soundings East Slope QUIVERA Basin

PX Sta. 1+00E

0+00 = sta. 1+00 on $\frac{1}{2}$ Sound West.

Dist	Sound		Dist	Sound	
0+00	?		1+90	16.1	-11.1
1.53 (3.0)					
0+04	1.1	+6.1	2+00	16.0	-11.0
0+04	0.0	+5.0			
0+10	2.5	+2.5			
+20	4.8	+0.2			
+30	6.2	-1.2			
+40	9.1	-4.1			
+50	10.8	-5.8			
+60	12.0	-7.0			
+70	13.0	-8.0			
+80	13.0	-8.0			
+90	13.9	-8.9			
1+00	14.0	-9.0			
+10	14.0	-9.0			
+20	14.5	-9.5			
+30	13.9	-8.9			
+40	13.8	-8.8			
+50	13.3	-8.3			
+60	14.0	-9.0			
+70	14.4	-9.4			
+80	15.2	-10.2			

Soundings East Slope QUIVERA Basin

PX Sta. 2+00E

0+00 = sta. 2+00 on $\frac{1}{2}$ Sound West

Dist	Sound		Dist	Sound	
0+00	?		1+60	15.5	-10.6
+10	+10	+5.9	+70	15.6	-10.7
+10	0.0	+4.9	+80	15.8	-10.9
+20	5.0	-0.1	+90	14.0	-9.1
+30	6.0	-1.1	2+00	13.6	-8.7
+40	7.0	-2.1	+10	13.5	-8.6
+50	10.9	-6.0	+20	14.0	-9.1
+60	12.1	-7.5	+30	14.7	-9.8
+70	12.9	-8.0	+40	14.8	-9.9
+80	13.8	-8.9	+50	15.3	-10.4
+90	14.7	-9.8	+60	14.7	-9.8
+100	14.8	-9.9	+70	16.0	-11.1
+110	14.7	-9.8	+80	16.2	-11.3
+120	15.3	-10.4	+90	14.7	-9.8
+130	15.0	-10.1	3+00	15.1	-10.2
+140	14.2	-9.3	+10	15.3	-10.4
+150	15.8	-10.9	+20	16.0	-11.1

Px

2+0 ^E (EAST SLOPE)

DIST	SOUND	
+30	16.1	-11.2
+40	16.5	-11.6
+50	16.1	-11.2
+60	15.9	-11.0
+70	15.6	-10.7
+80	15.3	-10.4
+90	15.0	-10.1
4+00	14.9	-10.0
+10	14.8	-9.7
+20	14.5	-9.6
+30	14.7	-9.8
+40	15.0	-10.1
+50	15.2	-10.3
+60	15.5	-10.6
+70	15.2	-10.3
+80	14.9	-10.0

12/49

Soundings East Slope Quincea Basin

Px Sta 2+15 E

Dist. Sound			Dist. Sound		
170	?		1+70	15.9	-11.1
173	10.8	+5.7	+80	17.0	-12.2
175	9.0	+4.9	+90	17.0	-12.2
178	7.1	+2.8	2+00	16.8	-12.0
180	5.8	-0.9	+10	16.0	-11.2
185	6.9	-2.0	+20	16.2	-11.4
190	7.0	-4.1	+30	15.8	-11.0
195	9.0	-4.1	+40	15.9	-11.1
200	6.9	-2.0	+50	15.1	-10.3
205	5.8	-0.6	+60	15.0	-10.2
210	5.6	-0.7	+70	15.0	-10.2
215	5.9	-1.0	+80	15.0	-10.2
220	9.8	-4.9	+90	14.9	-10.1
225	11.9	-6.0	3+00	14.8	-10.0
230	12.0	-7.1	+10	15.0	-10.2
235	13.2	-8.3	+20	15.2	-10.4
240	15.1	-10.2	+30	15.1	-10.3

over

Rx STA -2+75E (EAST SLOPE)

Dist	Sound	
3+40	15.0	-10.3
+50	15.7	-11.0
+60	15.6	-10.9
+70	15.5	-10.8
+80	15.2	-10.5
+90	14.9	-10.2
4+00	15.2	-10.5
+10	15.2	-10.5
+20	15.6	-10.9
+30	15.4	-10.7
+40	15.0	-10.3
+50	14.9	-10.2
+60	14.8	-10.1
+70	15.0	-10.3
+80	15.0	-10.3
+90	15.0	-10.3
5+00	15.2	-10.5

(4.7)

EXTENSION ON
 Sta. 4+00
 SECTION @ 90° T. 9%

Sound South

Dist	Sound		Dist	Sound	
4+00	14.0	-9.3	+80	14.6	-9.9
+10	13.2	-8.5	+90	14.8	-10.1
+20	13.3	-8.6	6+00	14.8	-10.1
+30	13.8	-9.1	+10	14.8	-10.1
+40	14.0	-9.3	+20	14.9	-10.7
+50	15.1	-10.4	+30	14.5	-9.8
+60	15.2	-10.5	+40	14.5	-9.8
+70	15.2	-10.5	+50	14.3	-9.6
+80	15.8	-11.1	+60	13.0	-8.3
+90	15.8	-11.1	+70	11.5	-7.8
7+00	15.9	-11.2	+80	5.5	-0.8
+10	15.0	-10.3	+90	4.5	+3.2
+20	15.0	-10.3			
+30	15.0	-10.3			
+40	15.2	-10.5			
+50	15.1	-10.4			
+60	15.0	-10.3			
+70	14.6	-9.9			

SHORE SECTIONS OF SLOPES (QUIVETA BASIN)

Px

SEE PAGE (61) (BASELINE LAYOUT)

STA - 0-50

STA	+	H.I.	-	ELEV
-----	---	------	---	------

T.P.	2.45	11.32		8.87
------	------	-------	--	------

0+00			4.2	7.1
------	--	--	-----	-----

S + 07			5.1	6.2
--------	--	--	-----	-----

S + 11			4.2	7.1
--------	--	--	-----	-----

S + 22			4.5	6.8
--------	--	--	-----	-----

S + 28			5.2	6.1
--------	--	--	-----	-----

S + 35			4.6	6.7
--------	--	--	-----	-----

S + 41			4.9	6.4
--------	--	--	-----	-----

S + 45			4.3	7.0
--------	--	--	-----	-----

S + 50			4.2	7.1
--------	--	--	-----	-----

+ 58			6.2	5.1
------	--	--	-----	-----

NORTH 20'			1.9	9.4
-----------	--	--	-----	-----

N + 50'			0.5	10.8
---------	--	--	-----	------

N + 1+00'			+0.1	11.4
-----------	--	--	------	------

0+00

STA	+	H.I.	-	ELEV
-----	---	------	---	------

1+00			0.1	11.5
------	--	--	-----	------

2+50			0.4	10.9
------	--	--	-----	------

2+23			1.2	10.1
------	--	--	-----	------

2+00		11.32	2.7	8.6
------	--	-------	-----	-----

2+15			4.0	7.3
------	--	--	-----	-----

2+25			5.6	5.7
------	--	--	-----	-----

2+29			7.5	3.7
------	--	--	-----	-----

1+00

STA	+	H.I.	-	ELEV
-----	---	------	---	------

1+00		11.32		11.3
------	--	-------	--	------

1+50				10.8
------	--	--	--	------

2+25			1.2	10.1
------	--	--	-----	------

2+00		11.32	2.9	8.4
------	--	-------	-----	-----

2+10			4.2	7.1
------	--	--	-----	-----

2+28			7.4	3.9
------	--	--	-----	-----

2+00

STA	+	H.I.	-	ELEV
-----	---	------	---	------

2+26			0.0	11.3
------	--	--	-----	------

2+13			1.1	10.2
------	--	--	-----	------

2+02			2.2	9.1
------	--	--	-----	-----

2+00		11.32	3.3	8.0
------	--	-------	-----	-----

2+13			5.0	6.3
------	--	--	-----	-----

2+25			7.3	4.0
------	--	--	-----	-----

2+50			0.4	11.9
------	--	--	-----	------

2+00			+1.0	12.3
------	--	--	------	------

(58)

STATION	+	<u>3+00</u> H.I.	-	ELEV
N	1+00		0.5	10.8
N	+50	P+	0.9	10.4
N	+25		1.9	9.4
	0+00	11.32	3.7	7.6
S	+15 ^S		5.4	6.9
S	+25		7.4	3.9

STATION	+	<u>4+00</u> H.I.	-	ELEV
N	1+00		+0.4 (1.0)	11.7
	+96		0.6	10.7
N	+50	PX.	1.3	10.0
	+25		2.1	9.2
	0+00	11.32	4.1	7.2
S	+15		5.7	6.6
S	+24 ^S		7.4	3.9

5+00

SECTION AT 45° TO B/L (EAST) SOUND SOUTH EAST

N	0+50		+0.7 (0.7)	12.0
N	+29		0.0	11.3
N	+22	P+	0.7	10.6
	0+00	11.32	1.6	9.7
S	+25		2.9	8.4
S	+48		4.2	7.1
S	+70		7.3	4.0

STATION	+	<u>6+00</u> H.I.	-	ELEV
	+50		+0.9 (0.5)	12.2
	+32		+0.2 (1.2)	11.5
	+25		0.6	10.7
	0+00	11.32	2.0	9.3
	+20		4.3	7.0
	+35		5.3	6.0
	+46		7.3	4.0

STATION	+	<u>7+00</u> H.I.	-	ELEV
	+50		+0.6 (0.8)	11.9
	+35		0.0	11.3
	+30		1.0	10.3
	0+00	11.32	2.7	8.3
	+22		3.9	7.4
	+34		5.0	6.3
	+49		7.3	4.0

SECT AT 90° To 1/2 (N)

8+00 12.7

STA	H.I.	-	ELEV
N/ +50		0.8	10.5
N/ +25	<i>R+</i>	1.8	9.5
0+00	11.32	3.4	7.9
S +22		5.3	6.0
S +42		7.3	4.0

SECTION AT 135° To 1/2 (NORTH)

8+00

STA	H.I.	-	ELEV
N/ 0+75		+0.4 (0.8)	11.7
N/ 0+58	11.32	+0.1 (0.3)	11.4
N/ +51		1.0	10.3
+25	<i>R+</i>	2.1	9.2
0+00		3.1	7.9
S +27		4.9	6.4
S +57		7.2	4.1

8+00

SECTION AT 90° To 1/2 (WEST)

STA	H.I.	-	ELEV
N/ 0+50		3.8	7.5
0+00	<i>R+</i> 11.32	3.4	7.9
S +25		3.7	7.6
S +50		7.7	6.6
S +73		7.3	4.0
T.P.		3.35	7.97

8+50

SECTION @ 90° To 1/2 (WEST) SOUND SOUTH

STA	H.I.	-	ELEV
0+00		5.78	13.75
+50			2.0 11.8
+32			2.7 11.4
+20	<i>R+</i>		2.9 10.9
+80			3.3 10.5
+75			3.5 10.7
+47			3.9 9.9
+67			5.2 8.6
+82			6.3 7.5
+10			8.9 4.9

7-3-50

9+00

SECTION @ 90° To 3/4 (W)

DIST	+	H.I.	-	ELEV
N/0	+50	13.75	1.9	12.3
N/	+20		1.7	12.1
N/	+15		2.2	11.6
	0+00		2.5	11.3
S-	+50		3.9	9.9
S-	+00		6.1	7.7
S-	+16		8.9	4.9

R+

7-3-50

(60)

9+50

SECTION AT 90° To 3/4 (WEST)

STA	+	H.I.	-	ELEV
9+50		13.75	2.1	11.7
9+00			2.6	11.2
8+99			3.7	10.1
8+50			4.3	9.5
8+96			6.1	7.7
8+50			6.1	7.7
8+39			6.5	7.3
8+92			8.8	5.0

R+

10+00

SECTION AT 90° To 3/4 (WEST)

STA	+	H.I.	-	ELEV
9+50		13.75	4.5	9.3
9+00			4.1	9.7
8+13			7.9	8.5
8+39			6.1	7.7
8+50			7.6	6.2
8+15			8.9	4.9

R+

SHORE SECTIONS, QUINERA 7-3-50

10+00

SECT. A. T. 135° To B/L (EAST.)

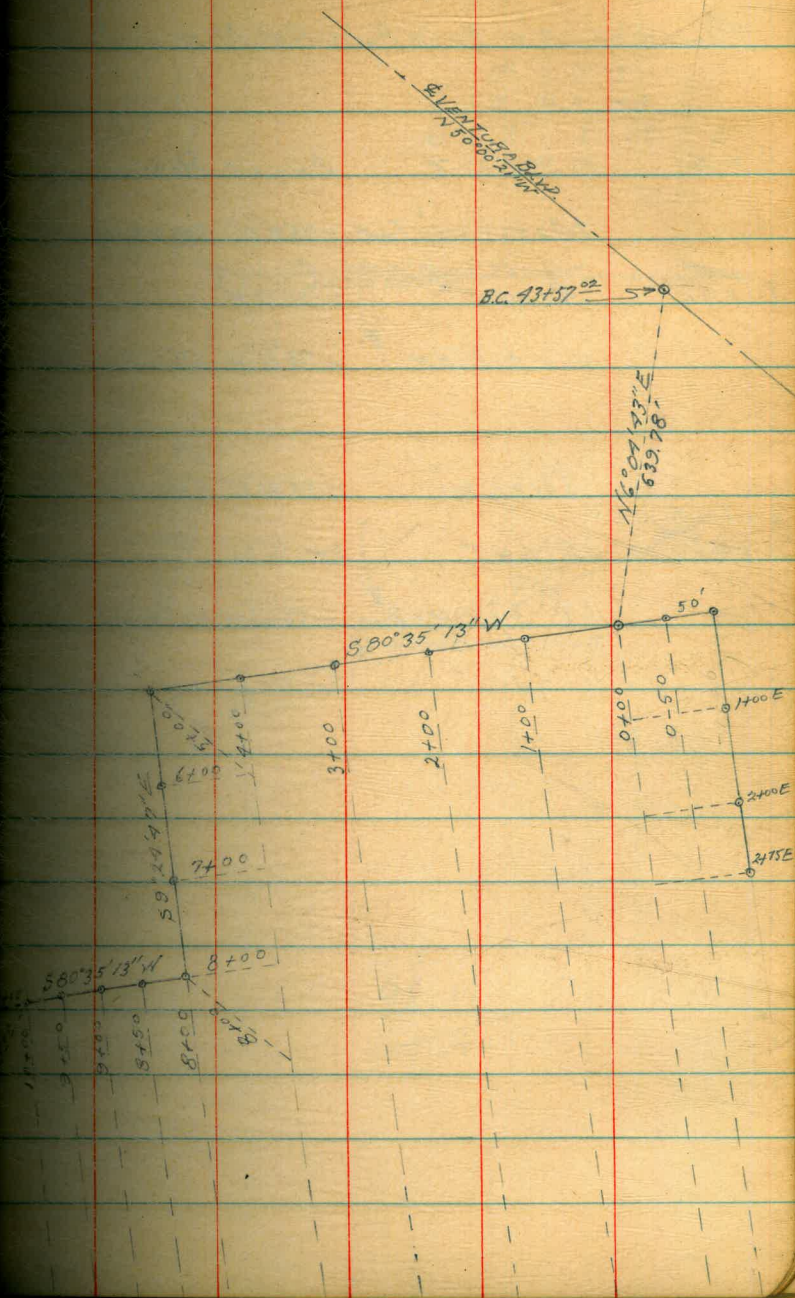
STA	H.L.	ELEV
N/E 0+50	13.75	2.4 11.4
0+00	9.1	9.7
S/W +24	6.2	7.6
S/W +44	8.9	4.9

10+00

SECTION ALONG B/L (WEST)

STA	H.L.	ELEV
E-0+50	13.75	2.6 11.2
0+00	9.1	9.7
W/ +28	5.8	8.0
W/ +31	6.4	7.4
W/ +50	8.9	4.9

BASE LINES FOR X-SECTIONS QUINERA BASIN



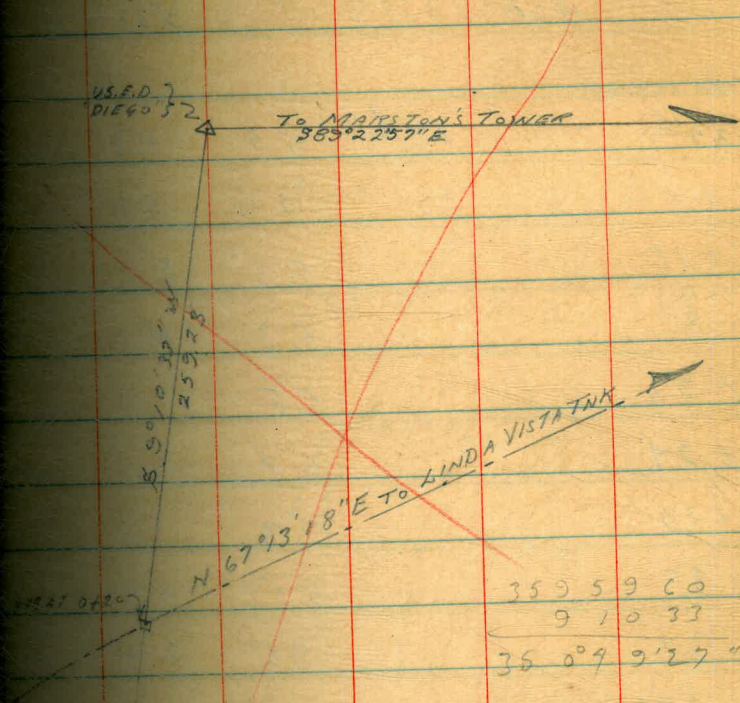
LOCATION OF PIER NEAR LIFE GUARD
TOWER AT EAST END OF NORTH JETTY

STA	OBJECT	ANGLE	BEARING	DIST
	MARSTON'S TWR.	① 28° 33' 30"	S 89° 22' 57" E	?
"DIEGO"	RIGHT	② 197° 07' 00"		
	HUB & PIER	AV. 98° 33' 30"	S 9° 10' 33" W	259.23'
(0+20 ft)	"DIEGO"	① 58° 02' 30"	N 9° 10' 33" W	259.23'
HUB @ PIER	RIGHT	② 116° 05' 30"		
	LINE TO PIER =	AV. 58° 02' 45"	N 67° 13' 18" E	
	TOWARD LINDA VISTA TANK			

REVISED

175.83
83.40
259.23'

98 33 30
MARI - S 89° 22' 57" E
S 9° 10' 33" W
58 02 45
N 67° 13' 18" E



359 59 60
9 10 33
35 09 9' 27"

100.55
98.33
6.22

PROFILE ALONG & OF PROPOSED
PIER

STA	H.I.	ELEV
B.M. 406	13.39	9.33
GUTTER AT CURB)		
0-25 ¹⁵	13.4	4.5
0+00		4.9
0+10		5.3
(HOB) 0+20		5.3
+23		5.5
+24		6.7
+29		7.3
+33		8.5
+37		9.5
+38		9.0
+39 ²		9.5
+41		9.7
+50		10.3

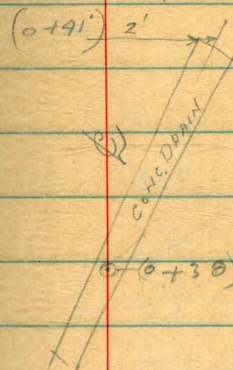
SEE NEXT PAGE

C. BARRAGAN OCT-17-50
A. SHERRY
H. BROWN
W. CARVER

8.1
+5.3
13.4
5.3
4.9
4.5 cb

1.8
8.1
12.9

"S.E.D. DIEGO"



TOP CONC DRAIN PIPE (P.I. WITH & PIERS)

OPPOSITE END DRAIN (WHICH IS 2' SOUTH OF & AT STA-0+41)

SOUNDINGS ALONG E OF PROPOSED
PIER

DIST	SOUND	DIST	SOUND
(4.2) (1:20 P.M.)		2+10	16.8 -12.6
0+60	3.1 +1.1		18.3 -14.1
	4.0 +0.2	(4.2)	19.0 -14.8
	6.1 -1.9		17.9 -13.7
	7.7 -3.5	+50	18.2 -14.0
1+00	9.3 -5.1		18.2 -14.0
	12.1 -7.9		19.0 -14.8
	15.2 -11.0		
	15.7 -11.5		
	15.7 -11.5		
+50	16.3 -12.1		
	16.6 -12.4		
	15.8 -11.6		
	15.4 -11.2		
	14.8 -10.6		
2+00	15.1 -10.9		

SEID

4.2

10-17-50

(64)

LOCATION OF SHOUFF LINE

AT EAST END OF NORTH JETTY

(N 67° 13' 18" E)

X @ 0+20 ; 0° 00' 00" = LINDA VISTA TANK

STA	OBJECT	ANGLE LEFT	ANGLE RIGHT	DIST
0+20	①		114° 45'	76'
"	②		99° 10'	75'
"	③		79° 04'	70'
"	④		71° 0'	48'
"	⑤		26° 35'	16'
"	⑥	28° 30'		30'
"	⑦	60° 30'		65'
"	⑧	62° 25'		107'
"	⑨	49° 45'		200'
"	⑩	38° 55'		237'
"	⑪	42° 10'		270'
"	⑫	45° 35'		305'
"	⑬	49° 25'		312'

H.I. = 12.9
8.7
4.6

C. BARRY M. 10-18-50
SHEPARD
BROWN X
CARVER

(65)

Existing Pier & Ramp - Ventura Cove

Float 14x24 On Drums. 

Ramp 2x30

Pier 5x52 (Old Ramp 2 Pile Bents)

ALL SHOTS APPROX. 4.6 EL.

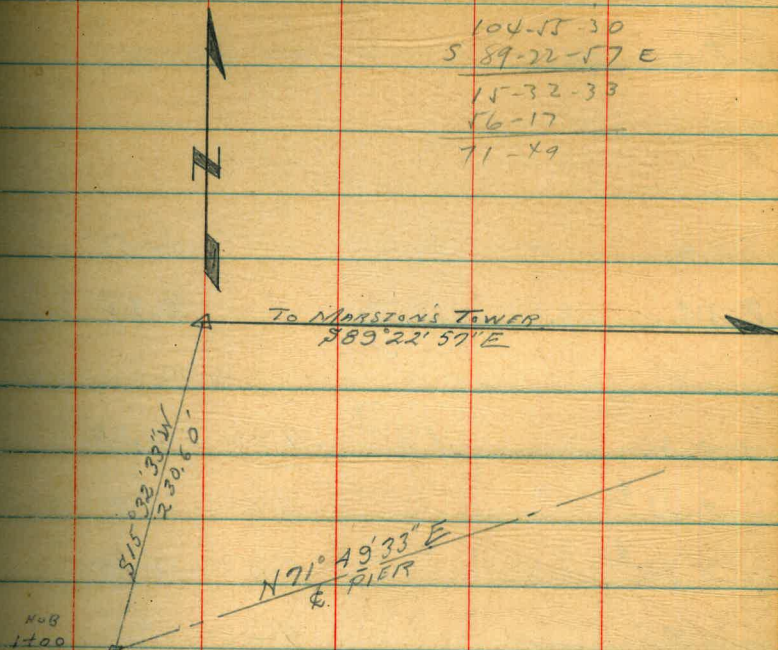
LOCATION OF PIER AT EAST END OF NORTH JETTY

STA	OBJECT	ANGLE	BEARING	DIST
	MARSTON'S TOWER	$\odot 109^{\circ}55'15''$	$S 89^{\circ}22'57'' E$?
	U.S.E.D. DIEGO RIGHT	$\odot 209^{\circ}51'00''$		
	HUB & PIER STA-1400	$N 109^{\circ}55'30''$	$S 15^{\circ}32'33'' W$	230.60
	U.S.E.D. DIEGO	$\odot 56^{\circ}17'$		
	HUB & PIER STA-1400 RIGHT	$\odot 112^{\circ}39'0''$		
	Q OF PIER	$N 56^{\circ}17'00''$	$N 71^{\circ}49'33'' E$	

C. BARRAGAN 10-19-50
A. SHERRY
H. BROWN
W. CARVER

(66)

104-15-30
S 89-22-57 E
15-32-33
56-17
71-49



PROFILE ALONG E. OF PROPOSED PIER
EAST END OF NORTH JETTY

STA	+ H.I.	-	ELEV
B.M.	3.39	12.72	9.33
0+30	12 ²	4.95	7.77
+32 ⁴		5.0	7.7
+32 ⁴ ₁₃		4.3	8.4
+45		4.2	8.5
+62		5.6	7.1
+75		5.3	7.4
HJB 1+00		5.0	7.7
1+17		5.1	7.6
17 ⁵		5.7	7.0
30		7.5	5.2
40		8.7	4.0

SEE NEXT PAGE

1-40 10-19-50

3-33
3.39
12.72

(67)

U.S.E.D. "DIEGO"

PAVEMENT

GUTTER

TOP CURB

SOUNDINGS OF PROPOSED PIERS

EAST END OF NORTH JETTY

DIST	SOUND		DIST	SOUND	
1+50	1.8	+1.2	3+20	16.8	-13.8
+60	5.3	-2.3		15.5	-12.5
(3.0)	9.8	-6.8	(3.0)	16.2	-13.2
	11.3	-8.3	3+50	16.5	-13.5
	11.9	-8.9			
2+00	12.2	-9.2			
	12.8	-9.8			
	13.3	-10.3			
	12.0	-9.0			
	11.3	-8.3			
50	10.2	-7.2			
	8.5	-5.5			
+70	6.8	-3.8			
	8.1	-5.1			
	10.8	-7.8			
3+00	14.0	-11.0			
+10	16.2	-13.2			

9.7

12.7

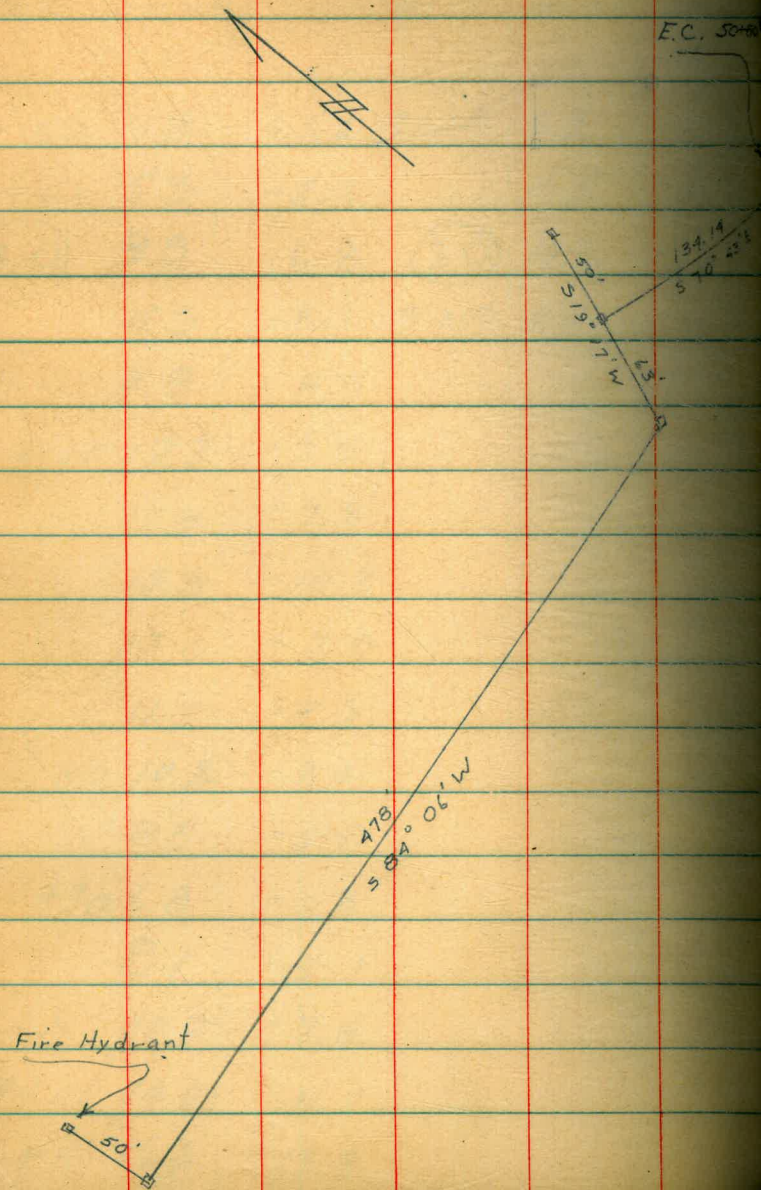
3.0

10-19-50

(6)

LAYOUT OF 8" WATER LINE QUIVER

AREA FROM VENTURA BLVD



INVESTIGATION OF 12"
 FLEXIBLE C.I. SUBMARINE PRESSURE
 SEWER FROM MISSION BEACH
 TO OCEAN BEACH PROJ. NO. 64340

9-21-51

T. Stamper
 E. Watson
 A. Sherry
 R. Shorey

0+00 = PT. OPPOSITE MON. DIEGO				DIST.	SOUND			DIST.	SOUND
SOUND S.E.				3+30	21.0				-16.9
DIST.	SOUND			3+45	22.6			5+00	-18.5
0+50		5.4		50	24.3				-20.2
60		2+00 6.0			25.7				-21.6
70		6.0			27.0				-22.9
9:35	80	1.0	+3.1		27.0				-22.9
	90	1.0	+3.1	(4.1)	26.4			50	-22.3
	1+00	1.2	+2.9		26.7	4+00			-22.6
		1.4	+2.7	50	28.2				-24.1
(4.1)		2.0	+2.1		28.5				-24.4
		2.3	+1.8		28.5				-24.4
		2.7	+1.4		28.0			6+00	-23.9
	50	3.5	+0.6		28.5	50			-24.4
		4.4	-0.3	3+00	29.0				-24.9
		5.0	-0.9		28.8				-24.7
		5.3	-1.2		20.3				-16.2

SEWER INVESTIGATION CONTD.

9-21-51

(1)

DIST SOUND

DIST SOUND

6+50

5

50

7+00

9+00

50

50

8+00

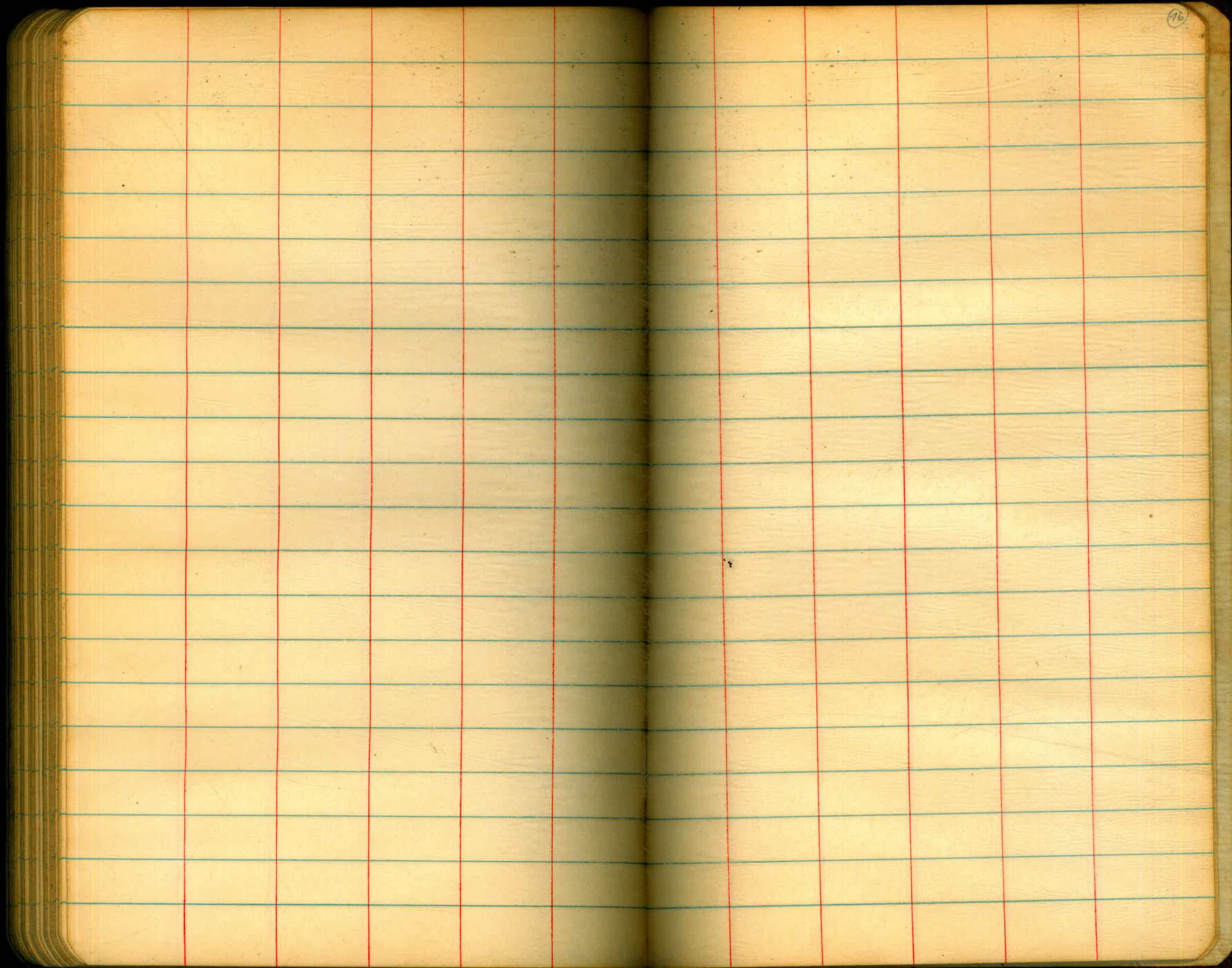
10+00

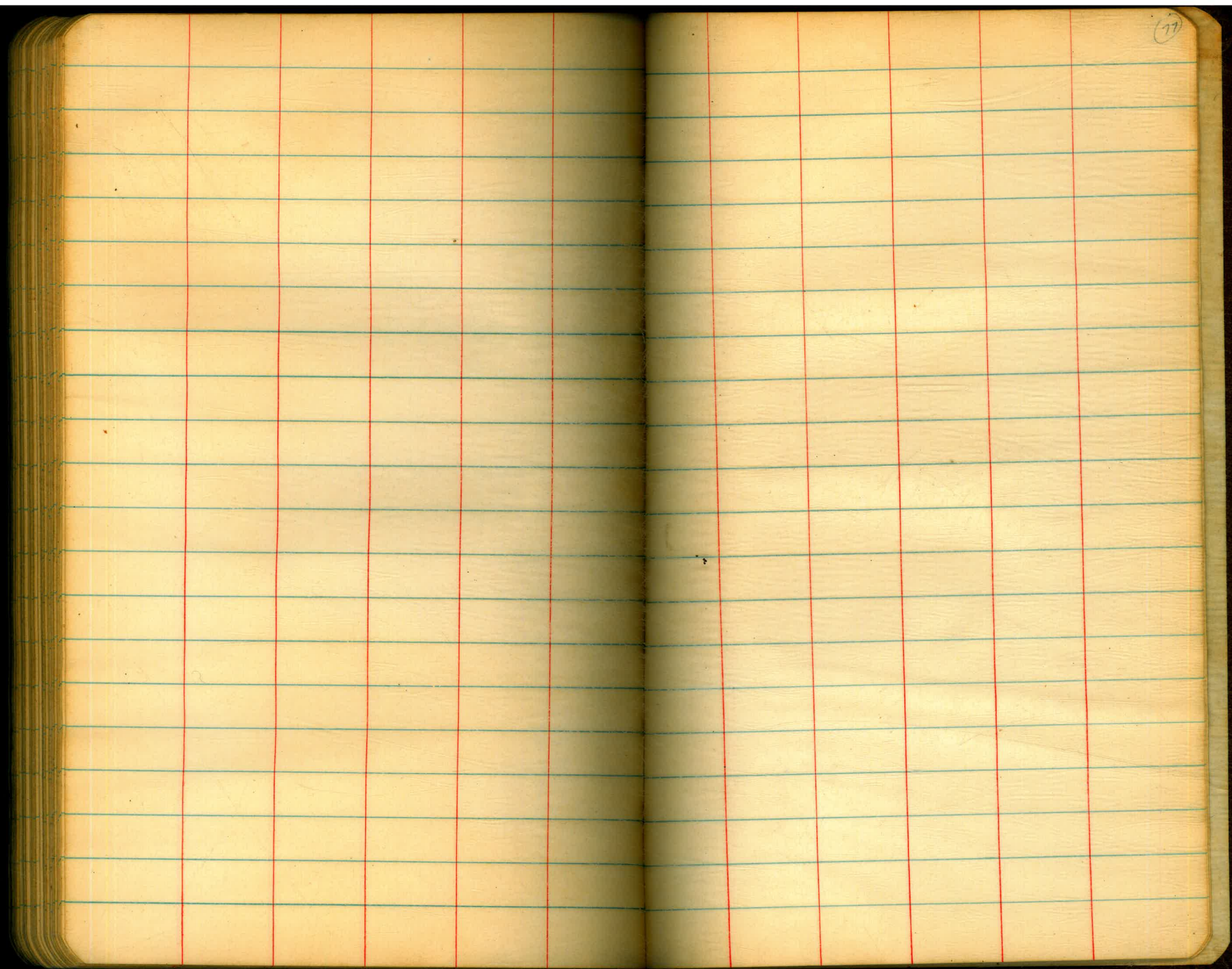
The image shows an open notebook with two facing pages. The pages are cream-colored and feature light blue horizontal ruling. Each page has two vertical red margin lines, one on each side of the central gutter. The notebook has rounded corners and a dark, possibly black, cover. The pages are blank, with no writing or markings, except for a small handwritten number '22' in the top right corner of the right page. The lighting is even, highlighting the texture of the paper and the color of the lines.

The image shows an open notebook with two facing pages. The pages are cream-colored and feature light blue horizontal ruling. Each page has four vertical red margin lines, creating five columns of varying widths. The notebook is bound in the center, and the dark cover is visible at the edges. The pages are blank, with no writing or markings other than the page number '73' in the top right corner of the right page.

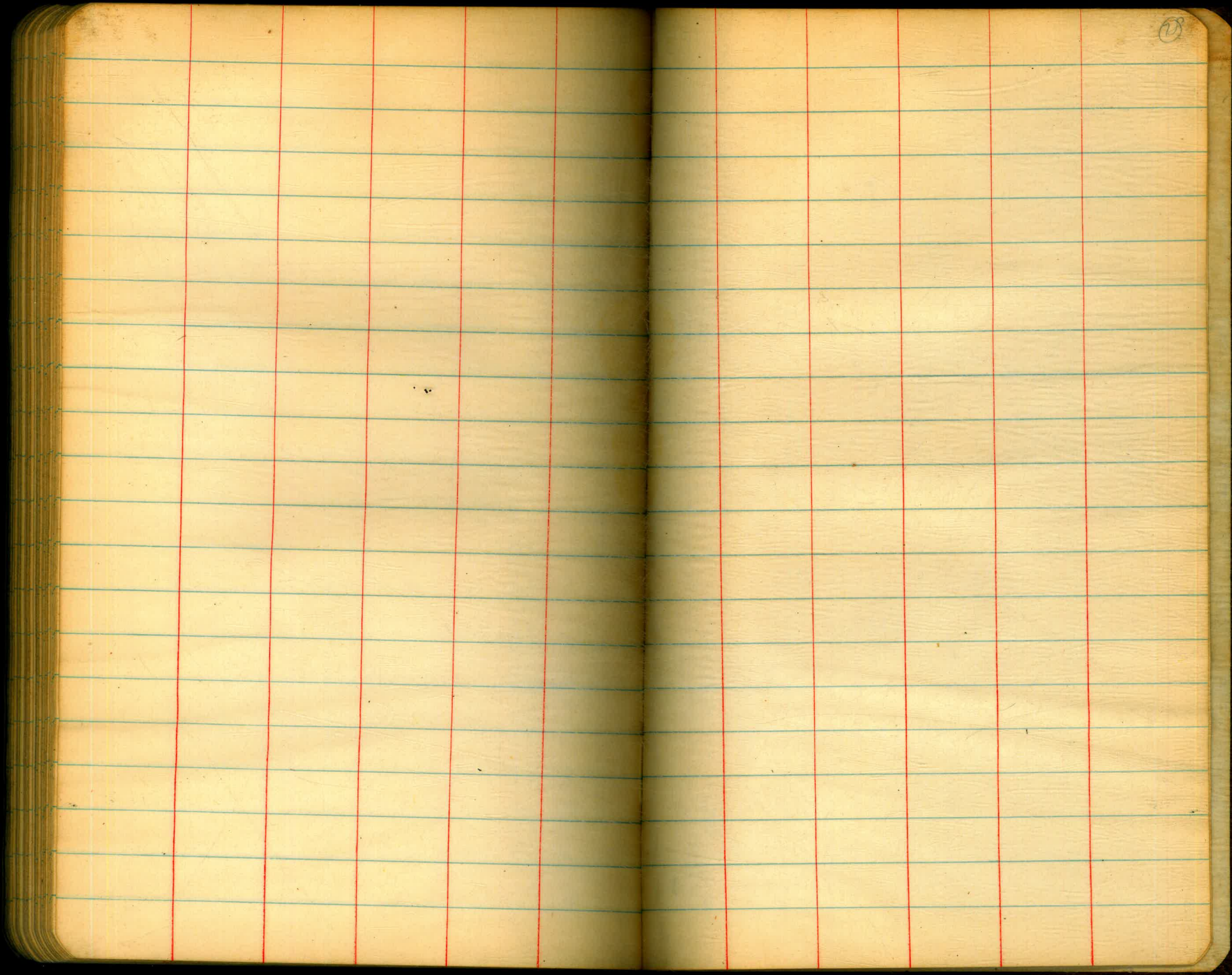
The image shows an open notebook with two facing pages. The pages are cream-colored and feature horizontal light blue lines for writing. Vertical red lines create margins on both sides of each page. The notebook is bound in the center, and the dark cover is visible at the edges. The pages are completely blank, with no handwriting or printed text.

The image shows an open notebook with two facing pages. The pages are cream-colored and feature horizontal light blue lines for writing. Vertical red lines create margins on both sides of each page. The notebook is bound in the center, and the dark cover is visible at the edges. The pages are completely blank, with no handwriting or printed text.





17



2

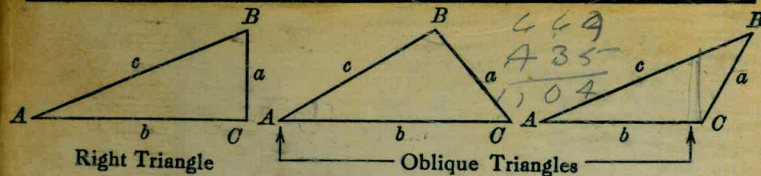
11.14
22.35
137
153
1001
S 50° 00' 21" E
43+57.02

101° 08' ①
②

MARS ①-55° 44'
M.H.N. ② 97
M.H.N. ③-111° 28'
AU 55° 44' 00"
M.H. ④
AT ⑤ 19° 22' 30" } 25.33'
90+00 38° 45' 00" }

(0° 11' 0" 22' 00")
(2° 35' 5° 10' 00")
(4° 19' 8° 38' 00")
MARS (104° 50' 30" 209 21)

TRIGONOMETRIC FORMULÆ



Solution of Right Triangles

For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{a}$, $\operatorname{cosec} = \frac{c}{a}$

Given	Required	Formulas
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B$, $c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$, $b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$, $b = a \cot A$, $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$, $a = b \tan A$, $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$, $a = c \sin A$, $b = c \cos A$

Solution of Oblique Triangles

Given	Required	Formulas
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$, $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$, $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$, $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$, $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$, $C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}$, $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = 5° 10'. From Table, Page IX. $\cos 5^\circ 10' = .9959$. Horizontal distance = $319.4 \times .9959 = 318.09$ ft. Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\cos 5^\circ 10' = .9959$. $1 - .9959 = .0041$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.09$ ft.

When the rise is known, the horizontal distance is approximately:—the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft. slope distance = 302.6 ft. Horizontal distance = $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.