

10

Field Book

BARRETT DAM

FIELD BOOK

W127

MICROFILMED

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300  
323  
1.10  
2.12



## Index

Conveyor trestle from Tunnel to Rock Bins	1-2
Elevation Top of Rock Bins	3
Reference Points Conveyor in Tunnel to Rock Bins	4-5
Layout of Bulkhead 0+00 to 0+72	6
Cement Conveyor. Cement House to Mixer Plant	7-10
Grades on footings Conveyor Stacks pile to Bins	11-12
Layout of Bulkhead for Crushed Rock Storage	13
Grades for School House	14
Road from Barrett To Lyons Valley	15-19
Road from Barrett To Salazar-	15-19
Sand Storage Site #2-Topog-	20-32
Grade Conveyor #3 Cement House to Mixer	33
Grades for Footings Conveyor #3	34-36
Sand Storage Site #2-Topog	37
Elev. 1461 - Sand Storage Site #2	(35)
<i>see page 34</i>	
Location Concrete Tower #1	39
Levels - Concrete Chute -	40-
Profile Concrete Chute - + Grades for Bents -	41
Grade for footings Concrete Chute	42-
Spoil Track Stiff leg derrick	44
Grade + Profile Spoil Track	45
Grades for footings Concrete Chute	46-47
Profile for Holes - Star Drill	48-49
Tie Present End Con. Chute To Tower #5/20	50



Elevation of Corners Concrete Tower #1	51
Grade of Track Sand Storage to Conroy #2	52
Elev for Profile w/ driver from pump	53
Location Concrete Tower #1	54
Upstream face - 38-24 - <sup>Transferred Est Book</sup> Bottom Sand Excav.	55
End of Concrete at Elev. 1477'	56
Elev footings Concrete Tower #1	56
Dist for Cable from End of concrete chute	57
Upstream Face for Excavation	58
Downstream face 26 - 38 -	
Landing Platform Cement House	60-61
Est. of Yardage -	62
Location of Star Drill Hole	
+ Topog for Est. of Yardage in shot	63-68
List of B.M.s.	69-70



3/9/20 Conveyor trestle from Tunnel  
to Rock Dips

Sta <sup>n</sup>	Grade Top 4x6 Stringers			
0+89 <sup>05</sup>		322	5322	165000
1+42	1648.84		751	45.71
1+37	1649.33		699	46.23
1+32	1649.81		644	46.78
1+31 <sup>50</sup>				
1+27	1650.29		596	47.26
1+22	1650.77		546	47.76
1+17	1651.26		498	48.24
1+12	1651.74		45	48.72
1+07	1652.22			
1+02	1652.70			
0+97	1653.18		301	50.21
0+89 <sup>05</sup>		684	5684	165000
0+92	1653.67		681	50.03
0+96 <sup>26</sup>	End of Tunnel on E. Plant			

0.964 ft = .0964 per ft

1742 1

Top Dips 1654.62

142	9.39
<hr/>	
	151.39

Center Line of Belt = 0.92 North of P<sup>n</sup> line  
Dist. between 6x6 Post inside = 2'-6" = 2.5'  
Base = 1'-2" = 1.17 on each side to Batter.

All stations = E of Bent section

1+12	51.74	1.92	1651.92	1650.00
			51.74	
		18	51.74	



3/11/20 See page 11 for Elev Footings

Sta P	Grade			
0+89.5	Top 4x6 Stringers	1656.84		
0+87			680	50.04
0+82			10.97	45.87
T.P. 15		119	453.5	12.68
0+67				28.67
0+42				28.23
0+32				27.83
0+12				17.92
0-207	1662.74 Top 4x6 str			06.10
	1661.97 Top Post			
	61.30			
0-6	1663.19 Top 4x6 str Produced			
0-979	2 Bins			
0-11	1662.64 Top 8x8 cap			00.49
	1661.97 Top of Post			
	61.30			
P.O.T.				1596.94

0.4760  
 9.4760  
 Level

0+82 = 1st Batter Bent



0-979

← 15' → 0+89.08

18.88  
12.28  
06.10

08.52  
.1158  
96.94

← 92' → 1432

0+6 24 L Pulley 1663.19

0-979 2 Bins

41 45.35  
 11.38 T.P.  
 33.97  
 1.41  
 35.38 H1  
 9.03  
 26.35  
 26.33  
 9.03  
 35.36 H2  
 6.13  
 29.23 T.P. H1  
 4.42  
 33.65 H1  
 582  
 27.83 T.P.  
 56  
 33.65 28.39 H1  
 582 10.47  
 4783 17.92 H1  
 96  
 18.88 H1  
 12.63  
 06.25 H1  
 2.27  
 08.52 H1  
 8.03



3/11/20

Elevation Top of Rock Bins

3

Bub  
Fisher

"PLinc"  
0.789.00      4.99    1654.79      1650.00

West      3.13    1651.86

±      3.11    1651.88

East      3.12    1651.87

Top of Bin      0.69    1654.30



Reference Points  
Conveyor to Bins

#

Station	6.71	1656.71	1650.00		
0+89 <sup>08</sup>					
5m Non/in 2x8"	North Side	Tunnel Entrance	5.74	1650.97	
0+92 Right			2.65	54.06	Bent 10 9.56 out
0+92 Left			6.65	50.06	7.12 "
0+87 Left			8.99	47.72	" 11 6.98 "
0+87 Right			4.27	52.44	9.17 "
0+82 Right			5.57	51.14	" 12 9.46 "
0+82 Left			12.59	44.12	10.55 "
0+67 Right				28.79	" 13 8.72 "
0+67 Left				28.29	8.82 "
0+42 Right				28.31	" 14 9.20
0+42 Left				28.18	9.25
0+27 Right				27.87	15 9.51
0+27 Left				28.79	" 9.60
0+12 Right				20.42	16 11.00
0+12 Left				17.43	" 14.50 "



Reference Point  
Conveyor To Rock Bins

5

0-2.07 Right

0-2.07 Left

Bent # 17

out

1608.75

16.12

0-11.74 Right

0-11.74 Left

Bent # 18

cc

1600.23

17.54



Layout of Bulkhead

P 0+89.25 for 9.23 1659.23 1650.00

Occupy Bulkhead 0+12 - Sight

0+70 for 25° -

chord

0+24 12' 5°-0

0+82

Occupy Bulkhead 0+24

Sight 0+70 for 20° -

0+24	1660	1.43	57.80	F 2.2
0+36	1660	8.03	51.20	F 8.8
0+48	1660	9.36	49.87	F 10.13
0+60	1660	10.46	48.77	F 11.23
0+72	1660			



3/13/20 South - Cement Conveyor from Cement  
Bub House to Concrete Mixers.  
Fisher

0.0 = South Edge of Cement House

Bent #1  
0+025 HUB

#2 HUB  
Bent 0+1525

P.O.T. HUB  
0+24.66

Bent #3  
0+30.25

Bent #4 P.O.R.  
0+45.25

P.O.T. Nail  
0+49.55

E. Mixing Plant  
0+57.06 HUB

5.09 Left to outside 12x12 Post  
West Line of Mixer Plant.



3/13/20

Profile Conveyor - South from Cement  
House to Mixing Plant.Bub  
Fisher

Conveyor - Stock pile to Rock Pile

0+27 Hub 2.50 1630.33 1627.83

Floor Cement House 9.32 21.01

Bent #1  
0+0.25 Hub 14.82 15.51

0+07 14.50 15.83

Bent #2 Hub  
0+15.25 9.57 20.76P.O.T. Hub  
0+24.68 8.90 21.43Hub #3  
0+30.25 8.62 21.710+15.25<sup>pp</sup> 0.31 1621.07 9.57 1620.76P.O.R. #4  
0+45.25 10.36 10.71Mixing Plant Hub  
0+57.06 12.41 08.66

Top Cement Floor 1.52 19.55

-17

19.21

3/14/20 Bents - Conveyor from Cement  
House to Bins

Sub  
Fisher

0+30.25

Gradetop  
Sta 4x6str

3.86 X 625.57

1621.71

00 = South  
Side C.H.

Bent #1  
0-6<sup>12</sup> pt. 23.07

Level Through  
Cement House X  
300 Vert Curve X

Bent #1 (23.07)  
0+25 pt. 23.17

2.40

B #2  
0+6<sup>67</sup> pt. 23.49

B #3  
0+21<sup>69</sup> 24.46

B #4  
0+36<sup>69</sup> 25.43

B #5  
0+55<sup>05</sup>

6.473%

0+58<sup>80</sup> E Polley 27.30 = T. Polley

0+59<sup>80</sup> chute

B #6  
0+63<sup>05</sup> 24.90 Top Post

See Paper  
for  
Stationing  
&  
Grading  
4/2/20

Rolls = 5" dia.



3/14/20

B.J.B.  
Fisher

0 + 30.25

Reference Points  
Conveyor Cement House to Bins

3.86 1625.57 1621.71

00 + 0.25 Right

6.06 19.51

Bent #1 1.78 out

Left

6.06 19.51

1.78

8.2

0 + 06.69

10.47 15.10

8.3  
0 + 21.69

Right

23.62

10' out

Left

12.89

10' out

4.45  
0 + 21.69

4.45 21.12

Bent #3

0 + 21.69 Left

10.08 15.49

2.66 out 10' out R.P.

0 + 21.69 Right

4.45 21.12

1.22 " 10' out R.P.

8.4  
0 + 36.69

8.47 17.10

Bent #4 2.50 out

Right

17.45

Left

T.P.

1.35 15.18 11.74 13.83

0 + 51.69

6.61 108.57

Bent #5

Right

0.74 14.44

2.99 out + on Rock

Left

8.31 062.87

4.25 out + on Rock

0 + 62.82

7.43 08.31

Bent #6 3.56 out + on Rock

Right



Cont. from page 2

3/16/20 Grades on Footings surveyed from  
Stout Pile to Sms.

Bub Grates Top  
Fisher 4x6 ST  
BM nail in 2x8

North side Tunnel	0.84	1651.81		1650.97
North (B11)				
0+87.0	1654.15		6.36	45.45
South				
0+87.0	1654.15		6.40	45.41
North (B12)				
0+82.0	54.63		7.95	43.86
South				
0+82	54.63		8.35	43.46
sw old Blackhawk exp. TP Nail	3.70	1632.93		1629.23
North (B13)				
0+67	1656.08		4.55	28.38
South				
0+67	1656.08		4.73	28.00
North (B14)				
0+42	58.49		5.41	27.52
South				
0+42	58.49		5.61	27.32
North (B15)				
0+27	59.93		5.58	27.35
South				
0+27	59.93		5.98	26.95
North (B16)				
0+12	61.38		12.54	20.39
TP	0.43	21.49	11.87	21.06
			3.56	17.93
South (B16)				
0+12	61.38		12.24	09.25

1.17 Base on all Bents except  
(17) & (18)

1.25 Base on (17) & (18)

Dist  
Vert height out  
Slope  
Dist

8.70	2.62	8.82	8'-9 <sup>3</sup> / <sub>4</sub> "
8.69	2.62	8.8099	8'-9 <sup>3</sup> / <sub>4</sub> "
10.77	2.97	10.92	10'-11"
11.17	3.03	11.324	11'-3 <sup>7</sup> / <sub>8</sub> "
27.70	5.79	28.082	28'-1"
28.08	5.85	28.467	28'-5 <sup>5</sup> / <sub>8</sub> "
30.97	6.33	31.398	31'-4 <sup>3</sup> / <sub>4</sub> "
31.17	6.37	31.600	31'-7 <sup>1</sup> / <sub>4</sub> "
32.58	6.60	33.030	33'-0 <sup>3</sup> / <sub>8</sub> "
32.98	6.67	33.435	33'-5 <sup>1</sup> / <sub>4</sub> "
40.99	8.00	41.555	41'-6 <sup>3</sup> / <sub>4</sub> "
52.13	9.86	52.829	52'-90"

✓



Footing Grades Conveyor.

Tunnel to Bins.

Tip of  
4x6 str

0-11.74 ~~818~~  
E

5.09 1605.58

1600.49

South B17

Top Post

0-2.07

61.97

3.84

0.74

60.73

11.79

61.061

61'-0<sup>3</sup>/<sub>4</sub>"

South ~~B18~~

Top Post

0-11.74

61.97

5.02

00.56

61.41

11.48

62.257

64'-3"

Vert. Dist. Slope  
Height. to Inside Post Dist

3/21/20  
Bob  
Fisher.

Layout of Bulkhead for  
Crushed Rock Storage.  
10' Chords

occupy 0-0      sight

10'	<sup>10'</sup> 4°-1667
20	<sup>20'</sup> 8°-333
30	<sup>30'</sup> 12°-500
40	<sup>40'</sup> 16-667
50	<sup>50'</sup> 20-834
60	<sup>10'</sup> 25-000
70	<sup>20'</sup> 29-167
80	<sup>30'</sup> 33-334
90	<sup>40'</sup> 37-500
100	<sup>50'</sup> 41-667
1+10	45-834
1+20	50-000

Grade Top of Bulkhead = 1660-



3/27/ Grades School House  
 Johnson's flag set on 175 Contour = E/1631

Johnson's Flag	35	1624.50		1621.00
	10.6	22.35	12.75	1611.75
	5.50	25.80	20.5	20.30
	3.1	24.1		1621.0

Points on Chute Q

00 = End Witter Spout

0-163 = Head of Nail in rock

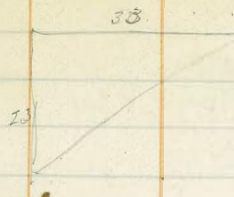
0+5  $\frac{61}{14.38}$  Hub.

0+19  $\frac{99}{13.16}$  Hub.

0+33  $\frac{15}{28.99}$  Hub.

0+6  $\frac{214}{14.50}$  Hub.

0+76  $\frac{64}{}$  Nail in Rock



14

33	
13	
99	
61	
1759	
379	
380	
15.20	156
35	
170	

224
163
561
19
9.99
28.99

3/19/20

Road from Barrett to Lyons  
Sub Cham. Valley & East to Salazar.  
Espir. Dist. 45 L A Rt.

#8 Δ R

#8 Δ L = 00 700 51° 27'

1

2

3

4

5

6

7

7+50

8

900 Δ Rt

13° 08'

10

11

11+80 ART

49° 53'

12+80

13+80 LLT

41° 35'

14+80 LRt

47° 0'

15+23 LRt.

60° 15'

16

17

17+33 LLT

31° 40'

18

18+40 RT RT to Road to Salazar.

18+80 LRt

27° 12'

15

Road

15 RT

10 "

20 "

2 Left

5 "

3 Right

2 Right

9 Left

8 "

E

50 Lt

57 Lt

7 Rt

3 Lt

55 Lt

5 Rt

8 Lt

2 Lt

30 Rt

45 Lt

E

E

5 Rt



Road Barnett-Leyons Valley  
3493 WS.

Sta Chain Dist. Ls Lt Ls Rt

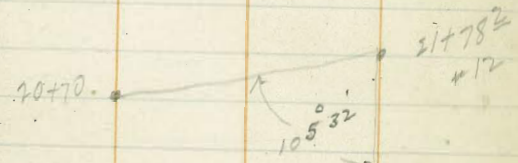
19+00		
19+50		
19+75		
20+00		
20+40		
20+70 LRT		20° 56'
21		
21+78 <sup>2</sup> L Lt = #12 on House Survey	95° 22'	
22		
23		
24 L RT		32° 48'
24+50		
25		
25+35 L RT		90° 49'
25+75		
26+35		
27+17 L Lt	53° 23'	
28		
29		
29+20 L Lt	58° 28'	
29+56 L Lt	50° 09'	
30		
31 L RT		28° 10'

15 Rt.  
2 Lt.  
2 Rt.  
100 R  
60 Lt  
E  
1 Rt.  
18 Lt  
12 Lt  
95 Lt  
E  
35 Lt  
8 Lt  
11 Rt.  
6 Lt  
4 Rt  
5 Lt  
2 Lt  
3 Rt  
5 Lt  
7 Lt  
15 Lt  
3 Rt

Average 11' Wide

21+25 4 Rt.

24+85 - 10 Lt



#11-06

Road Barrett Lyons Valley

17

Sta	Dist	LS	LT	LS Rt.	Dist to E Road
31+65					8 Lt.
32					35 Lt.
32+45 Lt.			24° 26'		⊘
33					7 Lt.
33+50					10.5 Lt.
34					1 Lt.
34+48 Lt.	End.				7 Lt.

---

18+40 Pt Lyons Valley R.					⊘
18+40 Δ Rt.			30° 24'		⊘
19+40					⊘
20+40					24.
20+50 Lt.			45° 39'		⊘
21					13 Lt.
21+50					11 Lt.
22					35 Lt.
22+50					4 Rt.
23					10 Rt.
23+50					9 Rt.
24					8 Rt.



3/29/20. Road to Salazar

18

Sta	Dist	Ls Lt	Ls Rt	Dist to E Road
24+50				9 Rt
25				9 Rt
25+50				7 Rt
26				9
26+50				4 Lt
27				5 Rt
27+26 Lt		78°-11'	✓	6 Lt
27+89 Lt		79° 30'		9 Lt
28				9
28+50				3 Rt.
29				25 Lt
29+50				2 Lt
30				9
30+20 L Rt.			59° 33'	7 Rt.
30+70				9 Lt
31 L Rt.			60° 32'	6 Rt.
31+50				9 Lt
32				7 Lt
32+50				7 Rt
33 L Lt		44° 33'		1 Lt
33+50				7 Rt
34				35 Lt
34+50				175 Lt
35				15 Lt
35+50				6 Lt.

Intersect Junction Road to Barns:  
8' Rd to Barns

3/29/20 Road Barnett - Salazar

Dist to  
E Road

19

Sta	Dist.	Ls Lt	Ls Rt	
36+00				40 Lt
36+50 =	W. side Conc Bridge			3' Lt
36+72 =	E Side " "			E
36+95				E
37+10	LLT.	41°54'		7 Lt
38				5' Rt
38+90	L Rt.			330 Rt
39				24' Rt
39+50				5 Rt.
40				E
40+50				E
41				E
41+32	Nail in Bridge	Wilson Creek		6' Lt



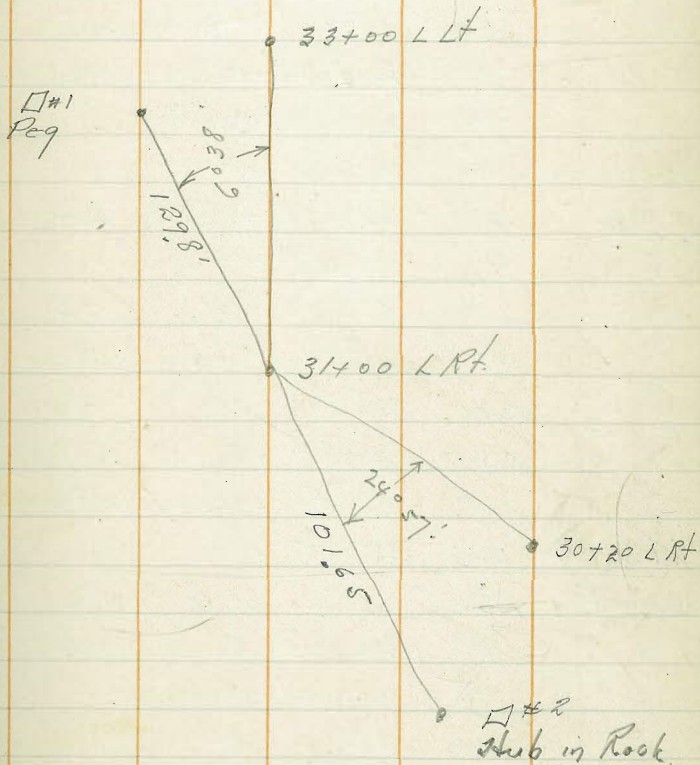
3/30/10

20

## Topog Sand Storage Site #2

Johnsons Flag	410	25.10	1621.00	
Peg	077	10.89	1498	1012
Rock	-05	9583	1501	9588
Peg	382	8451	1514	8069
30+20 LRT Road hub			840	7611
31 LRT			1100	1573.51
TP Nail	082	7033	1500	6951
□ #1			243	6790
Nail Edge Rd. P.	226	6050	1209	5824
33+00 LRT			913	5137

30+20 hub	1227	1588.38		157611
TP Point of Rock	1568	1602.99	107	8731
□ #2			4.45	98.54
27+89			2.67	1600.32





3/30/20 Topog Sand Storage #2.

	Sta	Stadia Dist	Az	Vert L	Rod	E/c	Corrected Dist	Diff in Elevation	
	AI-45	(7240)				1567.90 ✓			
			At	□ #1					
			Sight	Sta 31+00 L Rt	Salazar Road				
			for	Zero Az	Rt				
R.	660	189.30	00	160	56.4	66			✓
Rd Edge	680	192.30	-25.6	100	50.8	66	$\frac{116}{-17.1}$	✓	✓
R	800	156.0	+1030	45	70.0	80	+21	✓	✓
Ed. Rd.	71	200.30	-12.30	45	52.9	68	-15.0		
R	84	225.50	-17.50	45	43.5	80	-24.4		
R	90	232.35	-8.47	45	40.4	85	-27.5		
O. Draw.	105	237.55	-20.30	45	33.5	94	-34.4		
R	117	245.55	-14.0	45	40.4	110	-27.5		
R	142	253.45	00	17.7	54.7	142	-17.7		
R	172	258.20	00	5.9	66.5	172	-5.9		
R	210	269	+4.0	4.5	82.5	209	+14.6		
R	240	269.50	+5.30	10.0	85.2	237	+22.8		
R	177	274.45	+2.51	4.5	76.7	177	+8.8		
Rd.	140	283.55	-1.0	4.5	65.5	140	-2.4		
Main R	97	258.5	-17.18	4.5	40.4	88	-21.5		
" "	94	272.35	-12.10	100	43.4	88	-19.0		
" "	96	281.0	-12.0	4.5	48.4	92	-19.5	✓	
" "	104	294.15	-7.30	"	54.5	102	-13.4	✓	
" "	143	295	-5.0	"	57.3	142	-10.6	✓	
" "	120	316.30	-2.55	"	61.8	120	-6.1	✓	
" "	112	325.45	+0.15	10	62.8	114	+0.4	✓	

platted



7240

156720

At Δ #1 Sight 3140

Corrected Dist.

Diff in. Elev. +4.3

Bottom M. Draw	1280	341-10	+1°56'	700	66.7	128		
Edgt. "	150	348	+3°40'	140	68.1	150	+4.3	✓
" "	171	353-30	+1°30'	45	72.4	171	+4.5	✓
R. Ed Rd.	127	0°40'	00	+10	7340	127		
" " "	122	355-15	+2°55'	45	740	122	+6.1	✓
Rdg	115	351-30	+2-43'	"	73.3	115	+5.4	✓
" Rdg	86	344-30	00	37	68.7	86		
" "	84	314-40	00	89	63.5	84		
" "	112	301-10	00	114	61.0	112		
" "	90	282	-8-30	10.0	48.2	88	-13.2	✓
" "	85	285-20	-8-55	45	54.9	83	-13.0	✓
" "	77	305-	00	140	58.4	77		
" "	65	323-10	00	93	63.1	65		
" "	80	348:	00	40	68.4	80		
Ed R. "	95	5-15	00	1.1	71.3	95		
Eq R.	112	2°-40'	00	0.4	72.0	112		
Draw ER	55	13°20'	00	7.2	65.2	55		
" ER	53	7-50	00	6.1	66.3	53		
" ER	50	353-30	00	60	66.4	50		
Draw	51	341-45	00	10.2	62.2	51		
" "	38	316-45	00	14.3	58.1	38		
" "	48	287-10	-19-38	45	52.7	43	-15.2	✓
" "	60	263	-15-50	100	46.6	56	-15.8	✓
" "	85	250	-15-36	100	40.4	79	-22.0	✓

~~Stalled~~

✓



#145  
7240

At □ #1

156790

Point						Created D.H. in Dist	Elev
Point	88	256-25	-16°55'	45	43.5	81	-24.4 ✓
Rd.	58	250-35	-15°8'	100	47.8	54	-14.6 ✓
"	43	251-30	-19°27'	45	54.5	38	-13.4 ✓
" Eg Rd.	33	239-10	00	136	58.8	33	
N. Eg Rd.	25	272-30	00	142	58.2	25	
Rg	23	210-30	00	8.6	63.8	23	
"	35	153-40	+7°30'	45	74.4	34	+4.5 ✓
Rg.	53	145-15	+7°13'	45	74.5	52	+6.6 ✓
"	75	140-30	+11°24'	100	76.9	72	+14.5 ✓
Point Rg.	77	116-30	+13°55'	45	85.9	73	+18.0 ✓
"	46	105-	+15°30'	45	79.7	43	+11.8 ✓
"	28	86-50	+16°39'	45	75.5	26	+7.6 ✓
"	22	142-55	00	45	67.9	22	
" Eg Rd	28	72-20	00	8.8	63.6	28	
" "	40	349°	00	7.1	65.3	40	
Draw.	71	29°	+42°6'	100	67.5	71	+5.1 ✓
"	87	52°35'	+72°45'	100	73.0	85	+11.6 ✓
"	105	52-30	+72°5'	45	80.7	103	+12.8 ✓
"	125	50-15	+10°2'	10.0	83.9	121	+21.5 ✓
"	143	53-55	+8-30	45	88.7	139	+20.8 ✓
"	156	51-30	+9-10	45	82.4	152	+24.5 ✓
Junction "Draw	166	58-45	+10-12	45	96.7	161	+28.8 ✓
R Hand "	180	64-45	+13-20	10.0	1602.7	170	+40.3 ✓
" "	196	69°	+12°38'	45	1609.5	188	+41.6 ✓
" "	210	70-30	+18-8	45	1614.7	200	+46.8 ✓

23

Platted



Sta = 45  
72.40

Sta	Sta. Dist.	AZ.	Vert L		156790	Corrected Dist.	Diff Elev.
School Bldg	SE Cor. 222'	73-20	+14.0	45	1640.	409	+52
Ridge	724	82-55	+13-22	45	18.1	210	+502
"	184	84-15	+13-10	45	084	174	+40.5 ✓
"	157	88-45	+15-7	100	04.0	146	+39.6 ✓
"	120	95-30	+15-56	100	93.9	111	+31.5 ✓
"	85	111-15	+14.00	45	87.9	83	+20.0 ✓
	115	85-15	+16-15	10.0	93.2	110	+30.8 ✓
	100	74-45	+12-0	45	88.2	96	+20.3 ✓
	80	62-15	+13-15	45	85.7	78	+17.8 ✓
	70	49-45	+5-50	45	75.0	69	+7.1 ✓
Left Hand Draw	187	56-47	+13-26	10.0	04.4	177	+42.0 ✓
"	214	56-00	+13-07	10.0	10.0	203	+47.6 ✓
	232	56-55	+12-33	4.5	16.9	220	+49.0 ✓

P.M. Continued.

4.6 72.5

Sta	Sta. Dist.	AZ.	Vert L		1567.90	Corrected Dist.	Diff Elev.
Draw	253	56-29	+14-29	10.0	23.7	237	+61.2 ✓
Draw	272	55-25	+14-51	10.0	29.9	264	+67.4 ✓
Rg	265	48-28	+15-54	10.0	32.5	245	+70.0 ✓
Rg	237	49-23	+15-17	10.0	22.5	220	+60.0 ✓
"	204	51-00	+14-28	10.0	11.7	198	+49.2 ✓
"	194	49-04	+14-10	10.0	08.5	188	+46.0 ✓
"	171	48-08	+11-41	4.6	01.7	164	+33.8 ✓
"	151	43-09	+10-58	4.6	96.1	145	+28.2 ✓
"	130	38-10	+9-37	4.6	89.3	126	+21.4 ✓

Plotted



HI = 4.6

25

Station	Stadia Dist	Az	Vert L	Red	1567.90 Elev	Corrected Dist	Diff Elev.	
Ridge	113	41-28	+9-27	4.6	86.2	110	+18.3	✓
"	100	26-20	+6-42	4.6	79.7	99	+11.8	✓
"	89	9-24	+3-26	4.6	73.2	89	+5.3	✓
E of Road	87	7-21	0 0	2.9	69.6	87		
Ridge	124	5-00	+6-37	4.6	82.1	123	+14.2	✓
"	137	6-56	+8-03	4.6	86.9	134	+19.0	✓
	152	22-14	+9-30	4.6	92.6	148	+24.7	✓
	177	30-28	+13-06	10.0	01.5	168	+39.0	✓
	201	36-33	+14-19	10.0	10.3	189	+47.8	✓
	227	40-15	+13-37	4.6	19.7	215	+51.8	✓
	252	45-19	+ <del>14</del> 32	4.6	28.9	236	+61.0	✓
(?)	<sup>26.8</sup> +6.8	39-36	+15-46	10.0	<sup>32.5</sup> 06.5	<sup>2.50</sup> 156	+44.0	✓ +70.0
	240	35-44	+13-26	4.6	21.9	227	+54.0	✓
	223	30-41	+12-35	4.6	15.4	212	+47.5	✓
	210	25-13	+11-35	4.6	09.3	202	+41.4	✓
	201	21-31	+12-15	10.0	04.0	192	+41.5	✓
	188	17-24	+10-50	10.0	97.5	181	+35.0	✓
	175	12-06	+8-34	4.6	93.6	171	+25.7	✓
	173	7-57	+8-07	4.6	92.1	168	+24.2	✓
Draw	176	6-57	+8-37	10.0	88.5	172	+26.0	✓
Draw	168	8-54	+8-22	10.0	86.7	164	+24.2	✓
Draw-	167	12-48	+9-24	10.0	89.3	162	+26.8	✓
Pt of Ridge	183	7-32	+8-04	4.6	93.2	179	+25.3	✓
" " "	181	4-12	+6-58	4.6	89.6	179	+21.7	✓

Plotted.  
4/13/25



HE 46

A + D # /

Incom -

26

Station	Stadia Dist.	Az	Vert L	Ref	Elev.	Corrected Dist	Diff in Elev.
					1567.90		
Pl Ridge	180	3-40	+7- <del>48</del>	10.0	86.7	177	+27.2 ✓
Draw	168	2-37	+6-56	10.0	82.7	165	+20.2 ✓
Draw	149	3-11	+6-56	10.0	80.3	147	+17.8 ✓
Draw	167	345-22	+4-06	10.0	74.4	166	+11.9 ✓
Draw	153	340-51	+3-15	10.0	71.2	153	+8.7 ✓
Flat	146	333-09	+2-30	10.0	69.2	146	+6.7 ✓
Flat	142	320-22	-0.0	5.2	67.30	142	
Draw	<del>131</del> 131	294-21	0.0	1.8	60.7	131	
Draw	147	294-55	0.0	7.0	65.5	147	+6.5 ✓
"	160	291-22	+2-16	10.0	69.0	160	+10.6 ✓
"	176	287-08	+3-29	10.0	73.1	176	
"	192	285-44	+3-01	4.6	78.0	192	+10.1 ✓
"	214	281-30	+4-36	4.6	85.1	214	+17.2 ✓
Top of Ridge	243	278-38	+5-29	4.6	91.1	240	+23.2 ✓
Top of Ridge	264	283-34	+5-48	4.6	94.4	261	+26.5 ✓
Top of Ridge	295	287-04	+7-20	10.0	99.8	291	+37.3 ✓
Top of Ridge	264	287-54	+6-22	4.6	96.9	260	+29.0 ✓
Ridge	250	287.45	+5-37	4.6	92.2	247	+24.5 ✓
"	226	285-0	+6-16	10.0	87.0	223	+29.5 ✓
"	203	288-03	+3-20	4.6	79.7	203	+11.8 ✓
"	183	290-30	+1-56	4.6	74.1	183	+6.1 ✓
"	163	294-49	0.0	2.9	69.6	163	
"	184	297-07	+2-05	4.6	74.6	184	+6.1 ✓
"	208	295-55	+5-05	10.0	80.7	207	+18.2 ✓

Platted



HI 4.6		At #1			EL	Corrected	Diff in
72.50	Station	Stadia Dist.	AZ	Vert L	Red	Distance	Elev
	Ridge	230	294-21	+4-38	4.6	86.4	228 +18.5
N	Edge of Road	250	293-02	+6-01	4.6	93.9	246 +26.0
S	Edge of Road	270	293-09	+5-44	4.6	94.6	267 +26.7
	Pt - Ridge	280	293-41	+6-53	4.6	01.1	277 +33.2
	Point of Ridge	305	292-06	+7-36	4.6	07.9	301 +40.0
	Edge of Road	305	290- <del>37</del> <sup>39</sup>	+6-14	4.6	00.8	301 +32.9
	Ridge	302	298-20	+7-47	4.6	08.4	298 +40.5
	Ridge	287	299-20	+8-09	4.6	08.1	280 +40.2
	"	258	299-03	+6-14	4.6	95.7	255 +27.8
	Edge of Road	250	299-22	+5-04	4.6	89.9	247 +22.0
	"	228	301-11	+5-18	4.6	89.0	226 +21.1
	Ridge	212	301-53	+3-54	4.6	82.3	211 +14.4
	"	185	303-05	+2-24	4.6	75.5	185 +7.6
	"	164	304-45	+2-53	10.0	70.7	164 +8.2
	"	160	313-30	+1-00	4.6	70.7	160 +2.8
	"	183	312-15	+2-56	4.6	77.2	183 +9.3
	Ed - Road	205	311-03	+5-00	4.6	85.7	204 +17.8
	Edge Road	220	310-53	+4-34	4.6	85.3	219 +17.4
	Ridge	235	309-30	+5-59	4.6	92.2	233 +24.3
	"	267	307-16	+7-35	4.6	02.7	264 +34.8
	"	303	304-18	+8-50	4.6	13.9	295 +46.0
	"	305	304-02	+8-45	4.6	13.8 <sup>08.4</sup>	297 +45.9
	"	295	312-00	+9-02	4.6	13.6	287 +45.7
	"	277	312-19	+8-06	4.6	06.5	270 +38.6
	"	266	312-21	+8-10	4.6	05.3	260 +37.4

Platted



HI 4.6  
72.50  
station

At  $\square = 1$

Station	Stadia Dist	Az	Vert L	Red	Bl	Corrected Distance	Diff in Elev
	222	313-44	15-43	4.6	1567.90	220	+21.8
edge of Road	212	314-35	14-18	4.6	89.7	210	+15.8
"	193	319-43	14-13	4.6	83.7	192	+14.1
	180	321-0	14-10	10.0	82.0	179	+13.0
	167	322-52 352-	13-20	10.0	75.5	167	+9.7
	164	330-18	13-26	10.0	72.2	164	+9.8
edge of Road	190	326-30	15-16	10.0	72.3	158	+17.4
"	204	325-30	14-48	10.0	79.9	203	+17.4
"	200	333-33	14-18	10.0	79.9	199	+15.0
"	180	334-33	12-55	4.6	77.5	179	+9.1

Plotted  
4/13/20

HI 485  
160339

At  $\square = 2$  Sight Sta 31LRT for 9854  
Zero Az Rt.

Rg	105	84-30	-6°-32'	485	866	104	- 11.9
"	120	97-0	00	6.6	968		
"	140	104-30	+3°-12'	485	06.3	139	+ 7.5
"	143	106-35	+3°-8'	485	06.3	143	+ 7.5
"	152	107-40	+4°-15'	485	09.7	151	+ 11.2
Top Rg	162	110-15	+5°-32'	485	14.0	160	+ 15.5
	135	120-0'	+7-0	485	14.8	133	+ 16.3
	125	119-10	+4-49	485	09.0	124	+ 10.5
	120	118-45	+4-17	485	07.4	119	+ 8.9
	105	117-5	00	05	02.89		



#1. 485

1603.39

29

	At	□	#2	159854	Corrected Distance	Diff in Elev.
	82	108-15	00	98	936	
	70	92-10	00	165	869	
	72	80-0	-13-39	485	821	68 -16.4
Draw	52	64-10	-16-42	120	791	48 -14.3
"	63	90-30	-12-55	485	848	60 -13.7
"	65	101-05	00	146	888	
"	75	119-15	00	81	953	
"	96	131-35	+8-16	485	04.0	96 +5.5
"	104	142	+5-55	485	09.2	102 <sup>100</sup> +10.7
Top Draw	127	155-10	+9-13	485	18.5	124 +20.0
Rq. Sid. D.	112	160	+10-08	485	17.9	109 +19.4
	88	155-45	+7-40	485	10.1	87 +11.6
	70	146-15	00	15	019	
	42	134-30	00	86	94.8	
	27	102-5	00	14.9	8.85	
Base Rk.	36	53.0	-33-35	485	822	25 -16.5
" "	33	85-15	-24-40	485	862	27 -12.5
B. Rock	22	103-30	00	14.5	889	
" "	17	124-20	00	10.5	929	
" "	7	176-	00	70	964	
" "	12	276-50	00	69	965	

Plotted

4/13/20

✓



1/9/20

#14.8

Station	AT	□	↑	2	Sight	31	L	RT			
Station	Az	Int	L	Rod	El						
1603.34								98.54			
	25	229-30	00	53	98.0						
	49.0	202-30	00	22	01.1						
	58.0	190-15	+7-32	48	06.0	57	+7.5				
	81.0	182-34	+10-35	48	13.1	78	+14.6				
	103	205-34	+10-31	48	16.9	101	+18.4				
	82	215-0	+11-17	10.0	08.9	79	+15.6				
	59	231-0	+8-22	10.0	01.6	58	+8.3				
	51	252-35	00	66	96.7						
	66	282-47	0.0	13.3	90.0						
Pt of Rocks	41	292-15	00	7.8	95.5						
end R. Ridge	54	294-28	0.0	11.4	91.9						
Bot. Rock	47	313-37	-12-07	10.0	83.7	45	-9.6				
" "	33	350-15	-22-06	10.0	81.8	28	-11.5				
	38	350-15		Sm Elev	81.8						
Top of Boulder	42	351-09	-18-36	4.8	85.8	38	-12.7				
Bot. Main Draw	58	345-0	-17-05	10.0	77.0	53	-16.3				
Top Boulder	58	341-45	-15-16	4.8	83.8	54	-14.7				
Bot. Draw	55	332-39	-16-19	10.0	78.5	50	-14.8				
" "	60	325-10	-9-30	10.0	83.5	58	-9.5				
" "	63	313-09	-8-25	10.0	84.2	63	-9.1				
Top of Boulder	50	323-09	-4-20	10.0	89.5	50	-3.8				
Bot. Draw	67	303-30	-6-51	10.0	85.4	66	-7.9				

Platted

1/13/20



4.8

160.334

A + A 2

98.54

Corrected Dist. Diff in Elev.

Bottom Draw	73	284.54	0-0	15.8	87.5	73			
-	102	276.20	0-0	13.6	89.7	102			
"	108	270.20	0-0	10.8	92.5	108			
"	122	261.24	0-0	9.1	94.2	122			
"	137	256.06 + 2-32		10.0	99.4	137	+6.1	✓	
"	154	252.56 + 4-05		12-0	014.2	154 <sup>154</sup>	+10.9	✓	
"	184	248.45 + 4-48		14-0	04.5	183	+15.2	✓	
"	220	251.30 + 4-15		10.0	09.5	219	+16.2	✓	
side hill -	237	247.27 + 5-30		4.8	21.1	236 <sup>235</sup>	+22.6	✓	
"	253	243.10 + 7-46		4.8	32.4	250 <sup>249</sup>	+33.9	✓	
	235	238.08 + 8-12		4.8	31.6	230	+33.1	✓	
	215	243.12 + 7-04		10-0	19.5	211	+26.8	✓	
	206	245.45 + 6-26		14-0	12.1	204	+22.8	✓	
	176	243.39 + 7-10		14-0	11.0	174 <sup>173</sup>	+21.7	✓	
	141	245.15 + 4-58		10-0	05.4	140	+12.1	✓	
	144	<sup>238-30</sup> 245.30 + 2-16		10.0	16.1	139 <sup>140</sup>	+22.8	✓	
	150	229.15 + 12-09		10-0	24.1	143	+30.8	✓	
	14.2	220.47 + 11-16		4.8	25.6	136	+27.1	✓	
	121	226.30 + 12-25		10.0	18.7	116	+25.4	✓	
	112	235.45 + 8-39		4.8	15.1	109	+16.6	✓	
							+13.0	✓	
Ridge	102	245.45 + 7-23		10.0	06.3	100		✓	
"	97	251.45 + 2-07		4.8	02.1	97	+3.6	✓	
"	97	262.50 0-0		3.7	99.6	97		✓	
"	98	264.30 0-0		9.1	94.2	98		✓	

Platted  
4/13/20



				98.54	Corrected Distance	Diff in Elev.	
Top of Boulder	113	251-45	+4-50	4.8	08.0	112	+9.5
	115	252-0	+4-19	10.0	01.9	114	+8.6
	111	255-0	+3-37	10.0	00.4	111	+7.1
	76	313-20	00	13.9	89.4		
	100	315-10	00	7.1	96.2		
	120	311-40	+2-46	4.8	04.3	120	+5.8
	151	308-50	+5-29	4.8	12.8	130	+14.3
	157	307-04	+6-56	4.8	17.3	155	+18.8
	182	302.0	+8-20	4.8	24.6	178	+26.1
	178	298-55	+8-50	4.8	25.4	174	+26.9
	169	298-0	+8-12	4.8	21.5	160 <sup>115</sup>	+23.0
	144	297-0	+6-46	4.8	15.3	142	+16.8
	128	295-05	+4-51	4.8	09.3	127	+10.5
	111	294-30	+4-45	4.8	07.7	110	+9.2
	94	291-30	000	6.7	96.6	94	
	94	304-30	0-0	7.3	96.0	94	
Draw	126	276-40	00	6.7	96.6	126	
"	130	282 30	<del>12-39</del> 28	4.8	04.5	130	+6.0
"	144	284.45	+4-39	4.8	10.1	143	+11.6
"	160	285-30	+6-29	4.8	16.4	157	+17.9
	178	287-35	+8-14	4.8	23.7	174	+25.2
	190	281 33	+8-19	4.8	25.7	186	+27.2
	204	275-40	+8-28	4.8	28.3	199	+29.8

Continued on Page 37

Plotted 4/13/20

4/3/20.

Bob - Fisher  
Conveyor #3 - Cement Hoop  
to Mixer Plant.

33

Sta

Grades  
Top 4x6

00 = South Line Cement Hoop.

Level

Bent A1 23.82 Top Belt

0+6<sup>27</sup> 23.07 Top 4x6

PX

-6.44

#1 (2387-2392 Top Belt)

B 0+0.17 23.17 Top 4x6 P.I. X M.O. = 01

(6.44)

#2 0+6<sup>61</sup> 23.51 Top 4x6

PX

(15)

B#3 0+21<sup>61</sup> 24.55 Top 4x6

+

(15)

B#4 0+36<sup>61</sup> 25.59 Top 4x6

+

(9.22)

6.9087

B#5 0+45<sup>83</sup> 26.22 Top 4x6

(9.22)

B#6 0+55<sup>05</sup> (26.86)  
25.67 Top 6x6 Past \*

(8)

0+58<sup>80</sup> 27.87 Top Belt

Level

#7 0+63<sup>05</sup> 25.67 Top 6x6 Past \*



Grades for footings  
 Conveyor - from Cement House to Mixing Bin  
 Grade = Top of 4x6 Post.

at 57.06  
 E Plant 13.81 1622.47 16 05.66

Bolt-Brace (BM)  
 NW Cor. Mixing Plant 10.16 1612.31

Bolt in Brace  
 NW Cor. Mixing Plant 9.47 1621.78 1612.31

P.O.T.  
 0+26.61  
 Posts  
 0+36.61 25.59 7.44  
 Bent #4 West 7.26

Bolt in Brace  
 NW Cor. 8.10 1620.41 1612.31

Bent #3  
 East 0+21.61 24.55 2.96  
 West 2.94

Bolt in Brace  
 NW Cor. 8.79 1621.10 1612.31

Bent #2 East  
 0+6.61 23.51 9.98  
 0+6.61 5.42  
 Bent NW Cor. M. Plant 6.62 18.93 1612.31

Bent #5 East  
 0+45.83 26.22 8.09  
 Bent #5 West 5.57

#6  
 0+55.05 25.67  
 #6 West 25.67

Dist 1.17 Base on all Bents  
 6:1 Slope.  
 Dist 1.25 Last 2 bents - 4+7-  
 Slope

Vertical  
 Height

Distout

3.05

11.25 3.05  
 11.07 3.01

Set Hub 2.05  
 Set Nail 2.01

7.10 2.35  
 7.08 2.35

Set Hub 1.35  
 " " 1.35

12.39 3.23  
 7.83 2.47

Set nail in Plank 2.23  
 Nail in Ribs 1.47

15.38 3.73  
 12.76 3.31

HUB with nail 2.73  
 nail 2.31

8/16/20

Fisher

Mixer Elev- 1461 - at Sand  
Storage Site #2 Az R

At  $\square^* 1$  Sight  $\square^* 2$  fir 0.0

$\square^* V$  4.8 72.70 67.90

Stadia Dist

45.0	349-0	11.7	1461.0
88.0	318-25	11.7	
125.0	316-0	11.7	
123-0	297-10	11.7	
200.0	264-0	11.7	
24.5	295-15	11.7	
10.0	286-30	11.7	
73-0	185-30	11.7	



7/4/20

Bub  
Fisher.Grades on Footings Conveyor  
Cement House to Mixing Plant.

¢ Mixing Plant 0+57.06		13,22	1621.88		1608.66			
Bent # 3 East 0+21.61	Top 4x6 24.55			4.40	17.48	7.07	2.35	7'-2"
Bent # 3 West.				4.48	17.03 <sup>40</sup>	7.15	2.36	7'-3"
B#2 East 0+6.61	Top 4x6 23.51			10.76	11.12	12.39	3.23	12'-6 <sup>3</sup> / <sub>4</sub> "
B#2 West.				5.81	16.0 <sup>7</sup>	7.44	2.41	7'-6 <sup>1</sup> / <sub>2</sub> "
B#4 East 0+36.61	Top 4x6 25.59			7.43	14.45	11.14	3.03	11'-3 <sup>1</sup> / <sub>2</sub> "
B#4 West				6.82	15.06	10.53	2.98	10'-8 <sup>1</sup> / <sub>8</sub> "
B#5 East 0+45.83	26.22 Top 4x6			7.87	14.01	12.21	3.20	12'-4 <sup>1</sup> / <sub>2</sub> "
B#5 West				7.88	14.00	12.22	3.20	12'-4 <sup>9</sup> / <sub>8</sub> "
B#6 East 0+55.05	Top 6x6 Pst 25.67			2.47	19.41	6.26	2.29	6'-4 <sup>1</sup> / <sub>8</sub> "
B#6 West	25.67			2.49	19.39	6.28	2.29	6'-4 <sup>3</sup> / <sub>8</sub> "
B#7 East 0+63.05	Top 6x6 25.67			7.88	14.00	11.67	3.19	11'-10"
B#7 West 0+63.05								
¢ Mixing Plant 0+57.06		10.76	19.42		1608.66			
	25.67 Top 6x6			9.79	09.63	16.04	3.92	16'-3 <sup>3</sup> / <sub>8</sub> "

1.17 out = Base on all Bents except last 2 36

1.25 out = Base on #6 + 7 Bents. Batter 6:1

Vertical Height Out. Dist. Slope Dist.

4/9/20

HI 4.8  
1603.34

Topog - Sand Storage #2  
Continued from Page 32

98.54

					Corrected Distance	Diff in. Elev.	
185	270-0	+6-36	4.8	19.7	183	+21.2	✓
187	268-27	+6-32	4.8	19.6	185	+21.1	✓
176	258-15	+4-31	4.8	12.3	175	+13.8	✓
174	254-15	+3-30	4.8	09.1	174	+10.6	✓
158	262-40	+3-36	4.8	08.4	158	+9.9	✓
147	259-30	+2-17	4.8	04.3	147	+5.8	✓
134	264-30	00	3.0	00.3	134		
Pt of Rock	127	267-45	00	1.0	02.3	127	
148	273-15	+3-40	4.8	07.9	147	+9.4	✓
163	275-45	+5-43	4.8	14.6	162	+16.1	✓

✓

Platted 4/13/20



Reference Points

Occupy. 44-414-22 Sight B-44  
for 0:0 - Measured - 7.51 - Set Hvb  
44-422° — Set Reference  
Hvb about 654.5

4/21/19  
Sub  
Mitter

Location Concrete Tower #1  
See Page 54  
for Revised Location

18-R 303	9.05	38.45	1529.40
# Rock		10.79	27.66
Top Rock		5.07	33.38

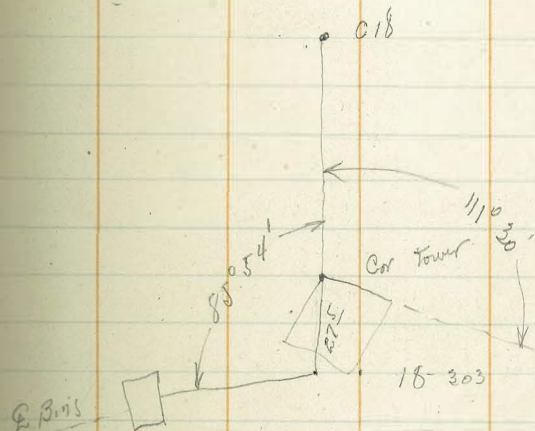
Overflow Section

1527 = 329.54	329.54	39
1528 = 330.31	.51	
14 = .077	330.06	R for E 27.66
.1 = .66		

46	4.00
46	49
.0508	351
	330.06
	10.94

Gravity

7528 = 333.96	333.21
1527 = 333.21	.50
.75	333.70 = R for E 27.66
.66	
450	
450	
.4950	



Tower Dimensions  
7'-6 1/2" x 10'-6 3/4"  
7.54' x 10.56'

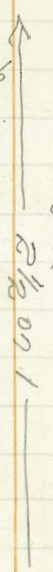


4/21/20

Sub  
Mixer

Levels Profile Conc. Chole

Hub. Pat. Conveyer #2	5.61	02.55		96.94
End Mixer Cpu. #2			0.21	02.34
0+5.61			4.81	97.74
0+12.22	97.46		5.37	97.18
0+19.99	94.26		11.17	91.38
0+33.15	89.00			
TP Peg	0.54	88.15	14.84	87.71
0+62.14 TP	7.00	81.45	13.80	74.45
0+76.64 Nad.			17.41	69.04
116.87			1.85	79.60
By Nail in Stamp				
Hub- 0+93.44				97.40
1+08.51				
1+20.28				
1+40.90				
1+45.27				



40

5.30  
 96.94  
 02.24  
 4.84

M

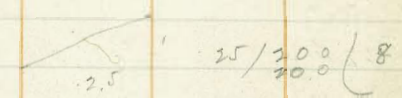
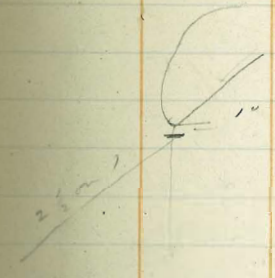
0+12- 97.40

02.34  
 .08

98.26  
 97.60

02.26 grade - 00  
 8.

94.26 grad 02.20



2.5 / 62.40 / 24.86  
 50  
 121  
 100  
 210  
 200  
 140  
 150

97.18  
 94.26  
 29.2

98.26

55 / 120 / 48  
 100  
 200

02.26  
 24.86  
 77.40  
 24.45  
 79.5

02.26  
 13.26  
 89.  
 91.58  
 80  
 2.0

2.5 / 33.50 / 13.26  
 35  
 81  
 75  
 65  
 50  
 150  
 150



4/22/20

Fisher  
Mixer

## Profile Concrete Chute

		1601.70		1600.00
Top 12x12 SE Mixing Plant conveyor # 2 POT - 14v6	1.72	1601.72		96.96
0+56L			4.76	96.94
0+19.99			3.96	97.74
0+33.15			4.52	97.18
T.P. peg 0+41.0	2.32	90.03	10.32	91.38
0+45	84.26		13.99	87.71
Bent # 5 0+56.0			6.72	93.31
0+62.14	0.66	25.13	13.70	76.33
BM Nail in Stump Bent # 6 0+70			15.56	74.47
0+76.64			10.40	79.63
Bent # 8 0+84	1.22	62.38	3.18	71.95
0+93.44			6.07	69.06
Bent # 8 0+98			13.97	61.16
1+08.51			5.26	57.12
Bent # 9 1+12			7.45	54.93
12-315			11.95	50.43
1+20.38			13.29	49.9
TP	0.79	48.00	0.58	61.50
14-319			10.74	156.74
1+26			15.17	51.64
1+40			10.46	1511.92
TP	5.00	41.17	2.69	45.31
1+45.27			7.19	40.21
			9.56	36.17
				31.61

## Bents - Concrete Chute

Station	Chute Grade	Top of Post
Bent # 1		
Bent # 2	1602.26	1603.59
0+14	1596.66	97.99
0+28	91.06	92.39
0+42	85.46	86.79
0+56	79.86	81.19
0+70	74.26	75.59
0+84	68.66	69.99
0+98	63.06	64.39
1+12	57.46	58.79
1+26	51.86	53.19
1+40	46.26	47.56
	44.66	

41  
Top of Post 1'-4" higher  
than grade of chute

25%





H.I  
4.9 104.9

30	2	5.2
48		4.2
60		3.3
86		4.3
100		3.0

Void



4/26/20

Bub  
Fisher.

Spoil Track for Stiff Leg derrick

49° Curve.

Δ 52° 54' - 48" 26 27 27

R 120.57

T 60

L 107.98

2430

Set 0-0 back 3' -

0+90 PC 49° Lt.

Occupy 0+90

1+05 15' 3'-40-30

1+20 30 7'-21-00

1+35 45 11'-01-30

1+50 60 14'-42-00

1+65 75 18'-22-30

1+80 90 22'-03-00

1+95 105 25'-43-30

1+97<sup>98</sup> P.T. 26'-27-18

Occupy 1+65 sight 0+90 in

18°-22-30 -

1+80 15' 3'-40-

1+95 30 7'-21

77 1+97.98 32.98 8'-04'

2-74298

44

.245
<u>298</u>
1960
2205
<u>490</u>
73010
<u>60</u>
438060
<u>60</u>
48360

7	21
<u>43</u>	45
8	00 45

56-250 □

60-250 □

39.525

90°-00

4/26/20

Sub  
Fisher  
Mixer.

Profile Spoil Tracks from 56-289-63

Grade = Bottom 8x8 - Bottom Ties.

45

56-300		8.91	1560.32	1551.41		
Hub 0+00	58.27		7.71	52.61	C	F. 6.7
Hub 0+15	57.97		8.22	52.10		5.9
0+30	57.67		7.93	52.39		5.3
0+45	57.37		7.53	52.79		4.6
0+60	57.07		5.64	54.68		2.4
0+75	56.77		4.54	55.78		1.0
Δ 49° L.P.C. 0+90	56.47		4.75	55.57		0.9
Nail 1+05	56.17		5.18	55.14		1.0
Nail 1+20	55.87		5.06	55.26		1.61
Nail 1+35	55.57		4.75	55.57	00	
Hub 1+50	55.27		3.15	57.17	1.9	
Hub 1+65	54.95		4.33	55.99	1.0	
Hub 1+80	54.67		8.33	51.99		2.7
Hub 1+95	54.37		10.03	50.29		4.1
Hub P.T. TP 1+97.95	54.31	2.14	52.58	9.85	1550.44	3.9
Hub P.O.T. 2+42.98				9.85	42.73	



4/28/20  
Fisher  
Mixer

Grades for footings Concrete Chute

2.13 Base on all bents - 6:1 slope

EYE TOP  
Footings:

Grade  
Top of Post

Vertical Height Dist. out. Slope Dist. Ft - inches

Location	Grade	Top of Post	Eye Top	Footings	Vertical Height	Dist. out.	Slope Dist.	Ft - inches
1+40	9.38	50.19	40.81					
North B#10 1+26	53.19 ✓		4.95	45.24	7.95	3.46	8.0596	8'-0 3/4" ✓
South B-10 1+26	53.19		8.86	41.33	11.86	4.11	8.60 12.0236	8'-7 1/4" 12'-0 1/4" ✓
cupage 41 TP	8.79	44.96		1536.17				
North 8-11 1+40	47.56		3.52	41.44	6.12	3.10 3.15 ✓	6.7044 6.20	6'-2 3/8" 6'-2 1/2" ✓
South 8-11 1+40	47.56		11.95	33.01	14.55	4.50 4.55 ✓	14.9507 14.75	14'-9" ✓
South 8-10 1+16	11.49	52.82		41.33 ✓				
North 8-9 1+12	58.79 ✓		1.49	51.38	7.41	3.31 3.36 ✓	7.512 ✓ 7.50	7'-6 4/8" ✓
South 8-9 1+12	58.79		4.14	48.68	10.11	3.52 ✓ 3.77	10.2495 10.24	10'-2 3/8" 10'-3" ✓
North 8-9 1+12	9.63	58.72		49.09 ✓				
North 8-8 0+98	64.39 ✓		3.40	55.32	9.07	3.59 ✓ 3.64	9.1951 9.20	9'-2 3/8" 9'-2 1/4" ✓
South 8-8 0+98	64.39		5.30	53.42	10.97	3.96 ✓ 3.91	11.1213 11.12	11'-1 1/2" ✓
North 8-7 0+84	69.99 ✓		3.71	62.61	7.38	3.31 3.36 ✓	7.4818 7.48	7'-5 3/4" ✓
South 8-7 0+84	69.99		8.66	60.66	9.33	3.68 ✓ 3.63	11.4587 7.46	9'-5 1/2" ✓
North 8-6 0+70	75.59 ✓		3.27	72.86	2.73	2.54 2.59 ✓	2.7677 2.77	2'-9 1/4" ✓
South 8-6 0+70	75.59 ✓		5.40	70.73	4.86	2.94 ✓ 2.88	4.9270 4.93	4'-11 1/4" 4'-11 1/8" ✓



Vert Height Dist out Ft + Inches

0+62.14

6.56 81.03 ✓

74.47 ✓

North B-5

0+56

81.19 ✓

4.07

76.96

4.23 ✓

279

284 ✓

4288 ✓

429

4-3 1/2" ✓

South

0+56

81.19

6.78

74.25

6.94 ✓

3.29 ✓

70357

7.04

7-0 1/2"

7'-0 3/8" ✓

322

✓



4/29/20

Fisher  
MixerElev.  
AssumedElevations for Star Drill  
Quarry-

11.40 1711.40 1700

~~0.73~~

11.68 22.35 0.73 10.67

12.83 34.75 0.43 21.92

11.41 44.70 1.46 33.29

12.82 56.37 1.15 43.55

Hole # 1

6.37 50.0

3.37 53.0

1.37 55.0

8.18 64.40 0.15 56.22

56.4

6.40 58.0

4.40 60.0

2.40 62.0

2.40 62.0

2.40 62.0

0.82 50.82 175.00

Profile

1756.37

9.4 47.0

7.5 48.9

6.2 50.2

4.8 51.6

2.7 53.7

0.07 56.4

8.18 64.40 0.15 56.22

5.9 58.5

5.0 59.4

4.5 59.9

3.7 60.7

3.0 61.4

2.6 61.8

48

4/29/30

Fisher  
Mixer-check Levels - for - Star Drill  
Elevations

49

0.82 1750.82 1750.00

check  
old - T.P.

7.26 43.56

0.59 38.48 12.93 37.89

check  
old T.P.

5.15 33.33

0.57 26.69 12.36 26.12

check  
old T.P.

4.80 22.89

2.57 17.44 11.82 14.87

check  
old T.P.

6.77 10.67

0.56 5.65 12.35 5.09

5.70 0.00

100-S-Drill

3.05 02.6



5/25/20

Bub  
Fisher  
Mixer

See Page 54

Location Concrete Tower #1

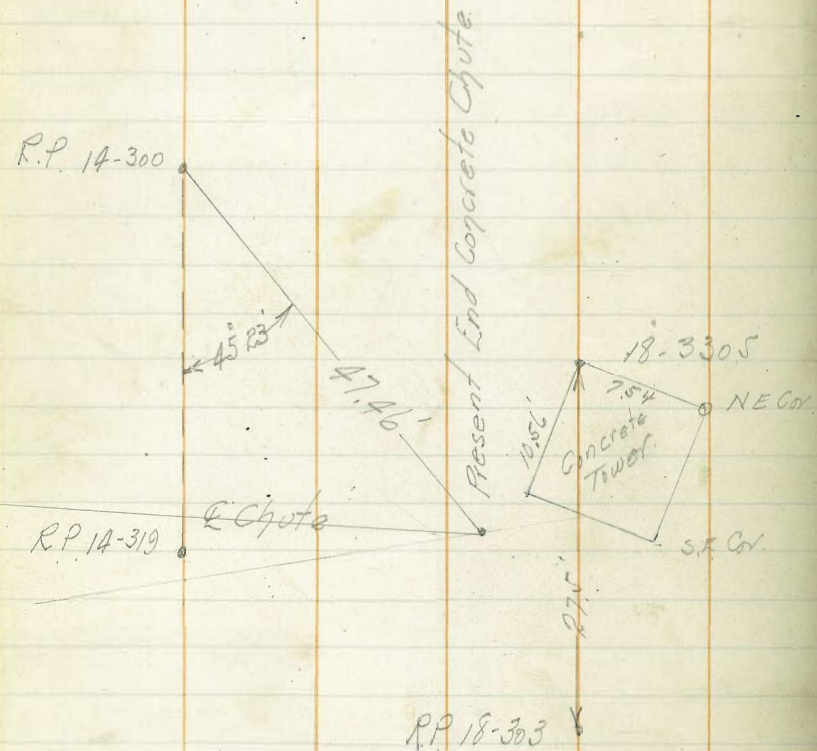
14-319

9.39 1561.23

1561.84

Flowline  
Concrete Chute

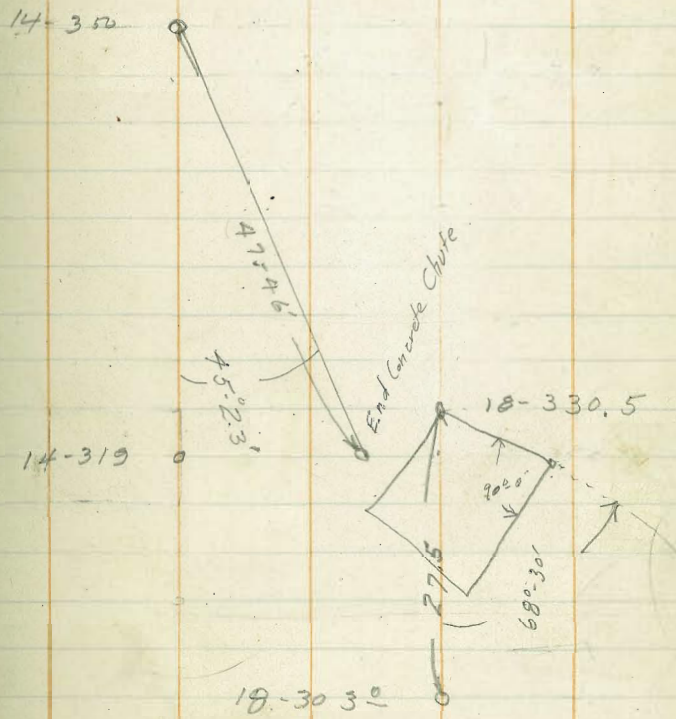
15.12 46.11



50

C18

$\frac{90-45}{45-22-30}$



Fiber Marker	Elevation of Corners		# Concrete Tower	
14-319.	0	78 1552.62	1551.84	
Southwest Corner.			12.64	39.99
TP on Rock.	0.99	40.57	13.04	39.58
TP on Rock.	3.69	32.22	12.04	28.53
NW Cor.			4.29	27.93
NE Cor			8.56	23.66
SE Cor.			6.73	25.47
18-303			2.82	29.40
South E			6.31	25.91
E North.			5.10	27.12



5/30/20

Fisher  
MixerGrade for Track - sand stockpile  
to Conveyor #2 -

B.M. Nail

North side Tunnel

11.82 1562.79 1659.97

0-0

2.39 60.40

0 + 5.6

2.20 60.59

TP <sup>on Rock</sup>

10.39 72.52 0.66 62.13

TP Break

0 + 62

12.67 82.77 2.42 70.10

T.P. Tap of stake

11.86 92.66 1.97 90.80

Water pipe

1 + 37

7.03 81.83

an pipe

1 + 60

5.36 87.30

T.P.

7.41 97.18 2.89 89.77

1 + 96

4.14 93.04

← 1232/22 Grade 15.47067

52

5/31/20  
Fisher  
Mixer

Profile for pipe Line  
from Well To 350 Up stream

	Grate				
Top of Well	3.93	71.57		1467.64	
0+25	67.6		5.7	65.9	F 1.7
0+16			4.4	67.1	F 0.5
0+50			4.0	67.6	0.0 ✓
0+97			4.2	67.4	F 0.2
0+97			5.5	66.1	F 1.5
1+0			5.5	66.1	F 1.5
1+50			5.0	66.6	F 1.0
2+00			4.5	67.1	F 0.5
2+50			4.1	67.4	F 0.2
3+00			3.9	67.7	C 0.1
3+50			3.6	68.0	C 0.4
Top of Stake	4.50	72.91	3.16	68.41	
4+00			4.65	68.2	C 0.6
4+50			4.2	68.7	C 1.1
5+00			3.7	69.2	C 1.6
5+50			3.5	69.4	C 1.8
6+00			2.8	70.1	C 2.5
B-38	3.38	1473.68		1470.30	
Top of Well			6.04	1467.64	

694  
676  
18

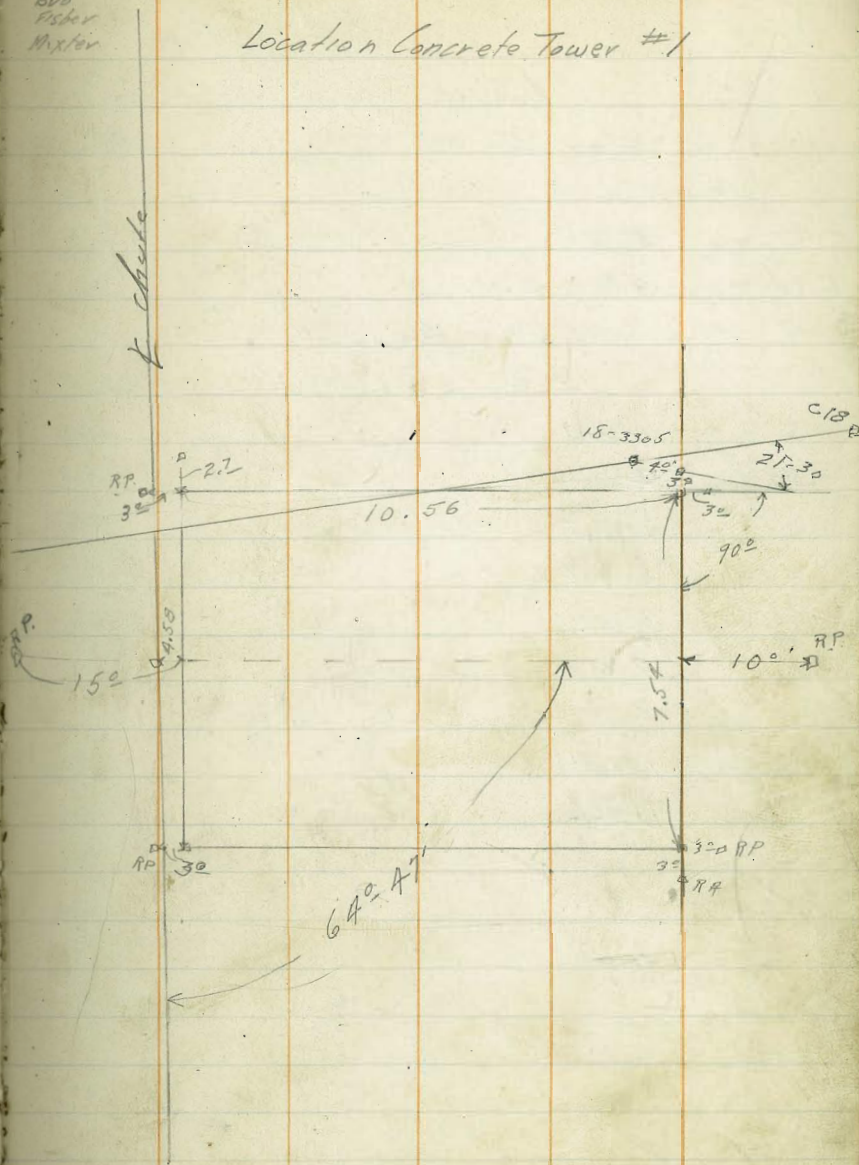
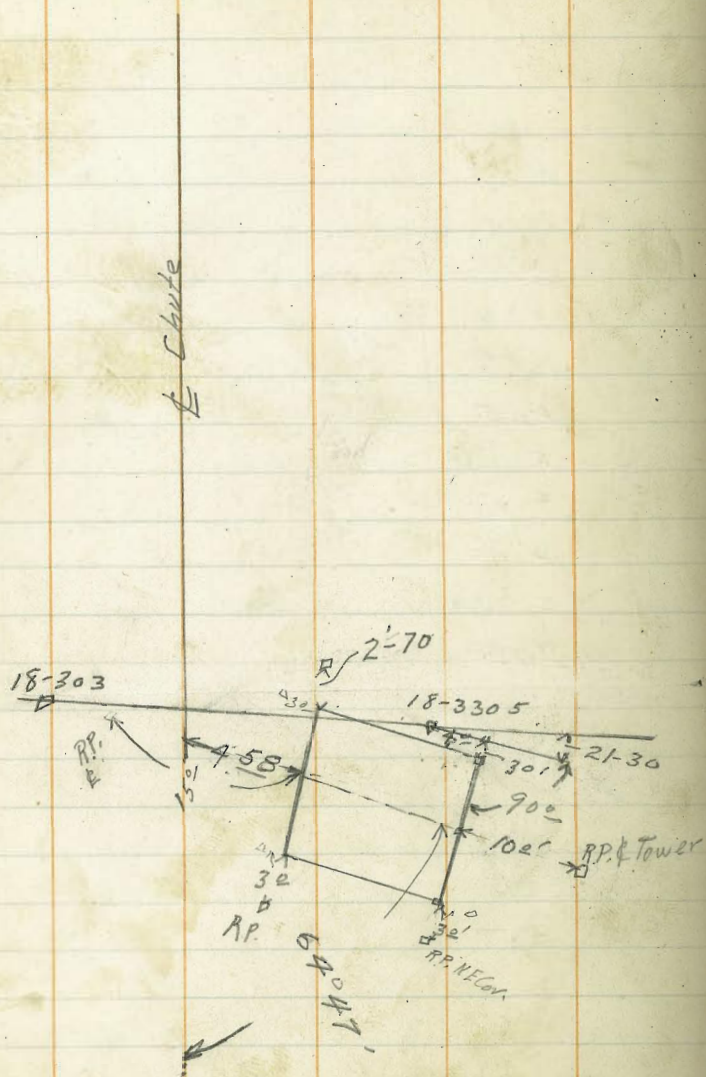


June 8. 1920

Bub  
Fisher  
Maxter

54

Location Concrete Tower #1





6/9/20

Bub  
Fisher  
Mixeroccupy C 46 sight C 41  
for 3-35'

C 41	50'	30-35'
C 40	60	4-18
	70	

occupy C 41 -

10	40	1-26
30	38	2-09
50	36	3-35'
70	34	5-01
90	32	6-27
110	30	7-53
130	28	9-19
150	26	10-44
155	-	11-06

55

Distout

Mar B-30		0.47	72.20		1471.73
B.M.					
T.P. on Rock		9.30	67.11	14.39	577.81
30	11.30			15.4	51.7
28	10.4			84	61.0
26	9.8			0.0	67.0
	10.0				
T.P. on Rock		0.0	57.8		5781
30	12.0		15	13.0	448
34	12.1			14.0	43.8
32	11.7			10.2	47.6
30	11.5			7.5	50.3
Low point in Excav				16.3	41.5

Elev. for Bottom of Sand

C-28		11.2	46.6
36		13.5	44.3
3A		14.0	43.8
32		14.0	43.8

Notes Transferred  
Book 9 - Page 31

B-28		4.18	9262		1488.44
				14.9	77.7
				89	83.7



6/10/20  
Fisher  
Mixer.

Location of End of Concrete at Elev 147

B.M. 6.17 77.90 1471.73 1530.3

TP on Rock 5.94 80.38 3.76 74.44

0.9 77.00  
3.38 77.0

E1- 1477 - On 400 Radius - at  
C 44 + 10 E -  
Need - 12 Excar - at C44 - 408 E

6/12/20  
Fisher  
Kirk

Difference of Elev - of Concrete  
Footings Concrete Tower #1

56

2.27 1531.67 2940

SE Cor 8.73 1522.94

NE Cor 10.03 1521.64

NW Cor 9.06 1522.61

SW Cor 8.04 1523.63

SW Cor 00

SE Cor 1.69 0-8 1/4"

NE Cor 1.99 2.10

NW Cor 1.02 1-0 1/4"

6/12/20  
Fisher  
Mixer.

### Dist for Cable.

End Concrete  
Chute H I

5.55 51.66 46.11

Guy Pin 278

-142.45 4.55

B-38-  
E of Point

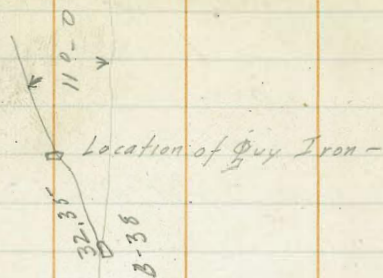
9.02 79.32 1470.30  
1.65 77.67

Dist  
Corrected. E/c  
Difference

260.5  
261

692

57





6/15/20

Bub  
Fisher  
Mixer

## Upstream Face - for Excavation

occupy C 46 - Sight 46-250  
for 90°

Turn 12°-53 for C-28-180'

C 28	
180	12° 53'
C-30	
160	11°-27'
31	
150	10°-45'
32	
140	10° 02'
33	
130	9-19'
<del>120</del>	8-36
100	7-09
80	5-44

On Rock near Flume  
BM

3.	57.81
3 97 1461 78	145781

12.7 48.0

T.P. 1-19 49.44 13.51 48.27

11.8 33.0 12.7

13.7 35.7 12.9

7.4 42.0

6.0 43.4

Lowest Elev -

16.0 33x5

TP 11.40 58.68 2.18 47.28

0.6 58 P 10.7

58

Location of  
Star Drill Holes

cut

D#6 24.3 D#14

10'  
D#13

D# 19.8 D#15

10'

D#14

D# 20.0 D#16

10.9

D 15

D1 18.7 D#17

10.7

C 16

D2 D#18

10.3

D#17

7/7/20

Bub  
FisherMixed At 34-274<sup>14</sup> chained 1.48 toward

Center for 34-272.76

Dist.

32 - 13.64 1°-26'

30 27.28 2°-52'

28 40.91 4°-18'

26 54.55 5°-44'

24 68.19 7°-10'

+3.41

23+50 71.60 7°-32'

+3.41

23+0 75.01 7°-54'

22 81.83 8°-36'

274<sup>14</sup> Radius = 1364 Chords - 20' on A00'R.

7/7/20

Bub  
Fisher  
Mixed

Radius Downstream face:

59

Radius

34-274<sup>14</sup> 8.98 1476.03 1467.0534- 277<sup>32</sup> 9.0 1467.0

32 12.29 1464.0

30 24.3<sup>00</sup> 33.6 40.426 24.3<sup>00</sup> 42.034-274<sup>14</sup> 7.03 74.08 1467.0538 274<sup>59</sup> 8.6 65.536 277<sup>32</sup> 7.3 66.8



4/3/20

## Landing Platform Cement Shed

60

Floor Cement House 11.21 1632.21 1621.0

21.0

9.6 22.6

C E

1.6

Landing Platform

6.3 25.9

C 4.9

NW Cor 22.57

0.4 31.5

C 9.2

5.7 26.5

2.9

At C 31 - Sight C 46 - for 10° 45'

C 32 ✓ 10.0 0-44'

C 33 ✓ 20.0 1°-26'

C 34 30.0 2°-09'

C 35 ✓ 40 2°-52'

C 36 ✓ 50 3-35

C 37 ✓ 60 4-18

C 38 ✓ 70 5.01

50 SE of Sump

B.M. x

0.19 1453.17 1452.98

4.56 4314 1459 38.58

About 32-41  
B.M. nail

798 35.16



7/23/20

Bub Grade  
Fisher Topot  
Mixer Floor.

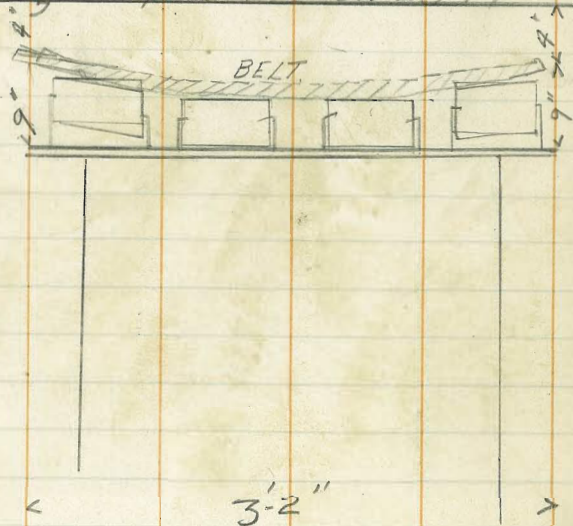
Floor Cement House 7.50 1628.50 1621.00

To/

1723.99

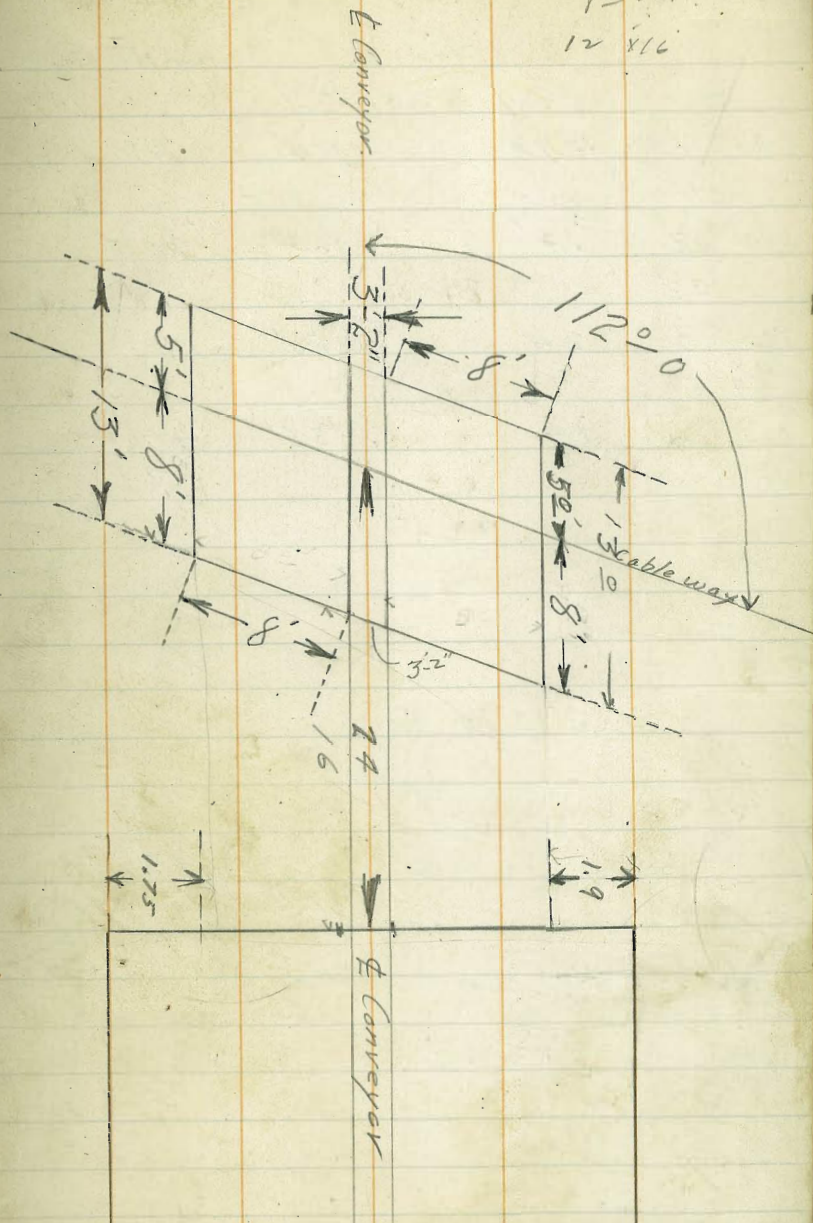
1.51 23.99

Landing Platform - Elev. 23.99



Cement Conveyor.

55 out 61  
12 x 16





7/22/20

## Sections for Estimate.

	cut.	Dist.	End Area
Sec #1	7 <sup>1</sup> / <sub>2</sub>	70'	490
42'			
Sec #2	16'	63'	1005
30'			
Sec #3	24'	50'	1200
54'			
Sec #4	14'	35'	490

Cu gds.

1150

1230

1750

4130

1000 - Sta 50 West.

~~4130~~  
3000 - Sta 57 East.

4000

5000

~~17130~~

14630

~~3500~~~~18130~~

Balance left July 15

Sand

80 x 20 x 15 = 800  
 40 x 27 x 30 = 1200  
 40 x 30 x 20 = 1000

Class 1 - 3000

Class 2 - 500

4000  
 3000  
 1000  
 5000  
 13000 Class 3+4  
 3000 Class 1  
 800  
 16800 Class - 2  
 Total.

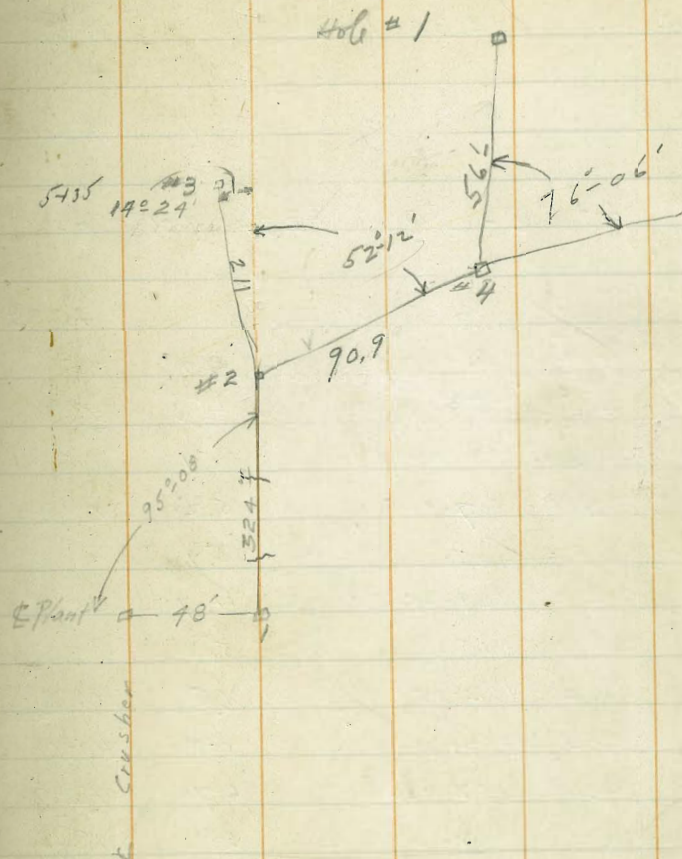
7/25/20  
Bob  
Fisher  
Mixer

Location of Star Drill Holes

63

#2 to #4 100' V.A. 24-38-

90.9





7/23/20  
 Sub  
 Fisher  
 Mixer  
 B.M. Pline  
 Above Crusher

Topog

Elev-

2.36 1754.03 1751.67

# 2

8.18 1745.85

At #3 - Sight #2 for 180° - Az Rt.

HI 80.3

	52.0	45	50.35		45.85
	4.7	70-45		47	45.7
Ver 10'	<del>4.5</del> 35.0	83-0	✓	43	46.1
Ver 8'	27.0	84-15	✓	51	45.3
Ver 5'	24.1	107-30	✓	5.2	45.2
Ver 20	31.6	128-15	✓	5.9	44.5
Ver 20	38.0	129-15	✓	4.9	45.5
	50.7	145-30	✓	5.9	44.5
Ver 12	60.2	152-35	✓	6.8	43.6
Ver -10	77.5	154-30	✓	6.8	43.6
Ver -10	84.6?	157-30	✓	6.7	43.7
9.0	92.5	157-0	✓	6.8	43.6
15	10.2	159-30	✓	6.6	43.8

Plotted  
7/24/20

✓

Topog

At #2 Sight #3 for Zero Az Rt.

HI 76.52

0.97 46.82 1745.85

106.0	17-15	37	43.1
95	18-30	41	42.7
100.0	24-30	0.0	46.8
85.0	26-45	1.0	45.8
68.0	27-30	1.0	45.8
58.5	23-45	3.4	43.4
47.3	20-0	2.7	44.1
30.0	58-15	4.0	42.8

Quarry Floor

3+25		5.1	41.7
4+25		4.2	42.6
5+25		1.8	45.0
Rock T.P.	13.53	57.29	1.06 45.76
Rock T.P.	14.52	71.66	2.15 57.14
Rock T.P.	15.25	86.27	0.64 71.02
" "	13.80	97.19	2.88 83.39
			95.89
		1.30	75.89

Plotted  
7/24/20

✓



7/23/20

## Elev of Star Drill Holes ✓

TP	130	97.19	1795.89	1795.89
		27.19	1725.89	
3 holes - North of #1 - old #12 - filled up.				
old #2 - filled up -				
#1 - old #12			6.2	91.0
#2 old #9			3.6	93.6
T.P.	11.30	7.19	1.30	1795.89
#3 old #8			6.7	00.5
Top of Plug old #4 #7			6.9	00.3
Top of Plug old #5 #3			5.3	01.9
Top of casing old #6 #4			3.1	04.1
#6 Top of Ground			4.4	02.8
#7 old #5			2.2	05.0
Top of Ground			3.2	04.0
55 =			9.65	97.54
TP.	12.55	7.17	0.57	06.62
TP.	15.31	31.80	2.68	16.49
Nail in Rock B.M.			1.66	1830 14

65

Topog

At Hole #1 Sight  $\square$  #3 for zero 39

T.P.	12.20	95.60	83.40
	13.2	45.0	10.5
	13.0	89.0	8.3
	13.9	117.30	7.3
	12.4	142.20	6.2
1/4 to 1 hr	17.51	144.15	6.0
16' with slope to bot.	26.8	158.30	5.2
" "	39.8	162.15	3.6
run - 5'	34.8	187.30	0.3
" 7	23.0	190.0	2.1
" 5'	7.8	212.15	3.9
	11.3	342.45	6.3
	22.6	338.30	5.8
run - 90	30.9	321.45	5.2
Top Hole #5	68.1	181.0	
#2	27.6	178.45	
#3	40.7	179.12	



7/3/20

Topog<sup>Hole</sup>

At Hole #5 Sight #1 for Zero Az R1

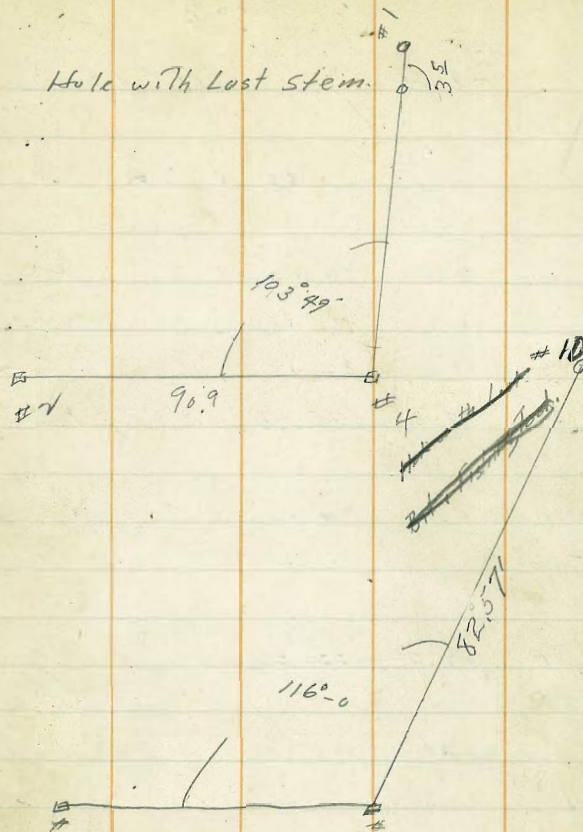
T.P. 06.44 - 89  
 10.55 1706.45 1775.70

√ 5	22.4	352-45	8.2	98.3
Hole #4	14.0	9-30 ✓	6.2	00.2
vert 50	6.0	327-45	4.6	01.8
v-5.0	11.5	210-30 ✓	4.1	02.3
1/4 Tol-6'	18.8	212-10	2.4	04.0 ✓
Hole #6	15.6	184-15 ✓		
Hole #7	29.6	187-50 ✓		
1/4 Tol-7'	39.5	195-20	2.6	03.8
1/2 Tol-8'	48.4	192-20	2.7	03.7
Top of cliff →	58.9	193-0	5.8	00.6
	53.4	193-0	2.8	03.6
	52.9	185-15	2.7	03.7
Top of cliff	59.0	185-15	10.7	95.7
T.C.	42.6	182-40	2.9	93.5
T.C.	31.0	178-0	2.6	93.8
edge of <del>cliff</del>	18.0	167-0	3.5	92.9
T.C.	24.8	135-0	10.7	95.7
	9.9	128-15	4.4	02.0
	18.5	116-20	7.8	98.6

✓

66

Hole with Lost stem.



don't  
 3/4 Tol down



1/23/20  
P.M.

Topo

At Hole #5 Sight #1 for Zero Az Pt

HI 1806.54

10.64 06.53 1795.89

7.8	68-30	4.2	02.3
15.3	84-30	8.0	98.5
13.7	34-15	5.5	01.0
18.0	43-30	7.5	99.0

1/4 Tol for 15'

1/4 Tol for 30'

Hole # 8

65.0 347-08 6.3 1800.2

T.P.

1.70 04.83

Aux/ Pt 39.7 330° 50'

At Aux/ Pt from Hole #5 Sight #5 for 00 Az Pt top Platform

HI 11.29

T.P.

6.45 11.28 04.83

11.6 325-20 7.7 03.6

10.3 325-20 5.0 06.3

Vert. 4.0

5.5 60-15 4.9 06.4

11.9 268-30 9.2 02.1

6 11.3 267.0 6.6 04.7

7.8 190-0 5.9 05.4

8.3 177-30 2.5 08.8

22.4 201-15 9.0 02.3

22.9 194-0 4.6 06.7

Hole # 4

21.1

17

Hole # 12

13.00 1813.3

1800.3

2.3 1811-0

4.3 1809.0

Hole # 0 21.5 # 13

0 8.1 7.6

# 5

12.5 14.4

01.9

2.0 12.4

3.4 11.0

Elev Hole # 13

See Page 58 for #14 to #18



Topo

At Auxil Pt from Hole #5 - Sight #5

HI 1811.29

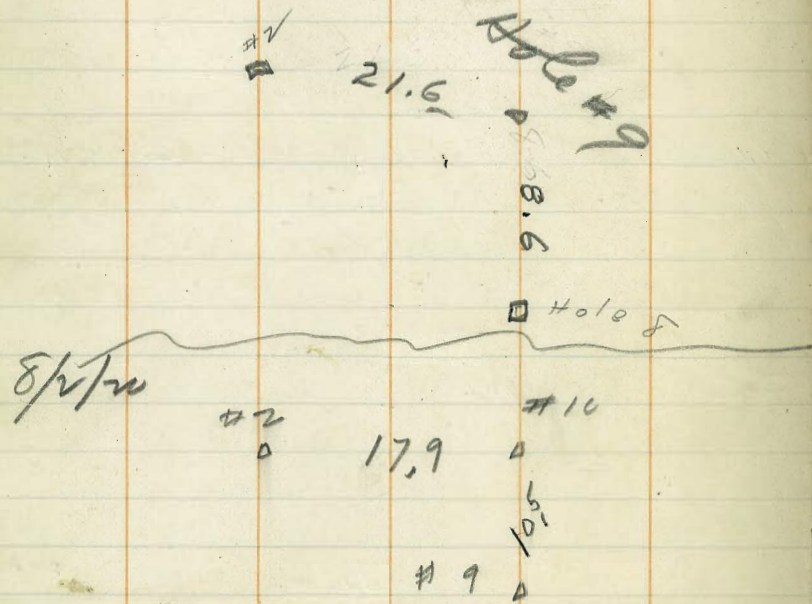
11.78

36.4	206-30	11.5	99.8
36.1	202-30	7.1	04.2
22.0	239.0	13.6	97.7
21.8	237-30	9.0	02.3

60' East of Hole #8 = Same Elev.

Blatted 7/15/30

Location Hole #9



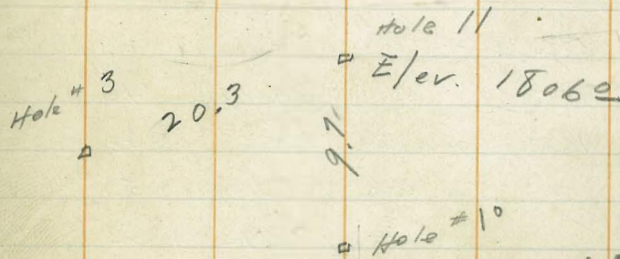
7/16/30

Fisher  
Marked

68

— Check Elevation on Holes —

TP	9.80	05.69	1795.89
11			<del>9.0</del>
Hole #1		14.5	91.2 ✓
Hole #2		12.0	93.7 ✓
Hole #3		9.0	96.7
Hole #4		5.6	00.1 ✓
Hole #5		3.8	01.9 ✓
Hole #6		2.8-9	02.9 ✓
Hole #7		1.4	04.3 ✓
Hole #8 (TP)	7.2	07.7	5.2 00.5 ✓
8/2/w		5.2	02.5
TP	12.5	08.4	95.89
		4.4	04.0
		1.6	06.8



See Page 67 for other Holes



## Reference Points

Coordinate Points	Elevation	Coordinate Point	Elevation	Coordinate Points	Elevation	Coordinate Points	Elevation	Coordinate Points	Elevation	Coordinate Points	Elevation		
"B" Line	455.79	B-450	East Tangent	300' Line		250 Line		Miscellaneous		"P" Line			
Tangent 14		60	1568.41	38	1474.66	58		21		(00-301) =0+00	1618.65		
Tangent 16		62	1579.43	40	1480.30	60	1568.21	22-321.39	1511.09	0+32	1627.85		
18	1557.81	64	1588.64	42	1488.29			24-321.2	1502.77	0+89.08	1650.00		
20	1545.11	66	1603.56	44	1496.84			Miscellaneous 26-	1510.42	2+00	1686.21		
22	1534.73	68	1617.48	46	1507.33	00-300	<del>1525.16</del>	27-357	1479.60	Iron pin - 5' S	2+08	1696.61	
24	1525.20	70	1624.03	48	1516.37	00-429	<del>1630.36</del>	28-352	1462.90	stump on line	1+85	1679.42	
26	1503.85	74	1650.44	50	1524.46	2-		28-325		2+33.6		1703.13	
28	1488.45			52	1536.34	2-		28-350	1479.60	Nail in 2x8		1650.97	
30	1472.35	East Tangent.		54	1540.42	4-350	1603.26	28-485	1503.57	North side of road		West	
32		60	1571.25	56	1551.41	4-455	1615.92	28-520		Cableway Line			
34		62	1582.59	58	1560.76	6		28-520	R.P.	(0.0-4466)	0+00	1631.70	
36		64	1591.57	60	1571.50	6-450	1615.35	28-600		1+00	1675.60		
38	1470.30	66	1602.58			8-		TOP of Wall	1467.41	1+75	1707.05		
40	1473.85	68	1612.52	250 Line		8-450	1601.85	34-274.14	1467.05	2+00	1715.89		
42	1480.64	70	1623.02	38	1491.47	10-315	1573.77	38-229.5	1509.45	2+50	1739.25		
44	1490.41	72	1633.50	40	1496.25	10-442	1596.58	38-480	1477.56	3+00	1760.48		
46	1502.68			42	1507.15	10-442	1596.58	40-413.53	1482.94	30' N-3+00		1764.33	
48	1512.78	East Tangent.		44	1513.11	12-315	1561.72	42-217.1	1514.56	Nail in Rock			
50	1522.67	60	1567.79	46	1519.99	12-437	1588.34	42-412.57	1486.04	East		Cableway Line	
52	1532.89	62	1579.68	48	1526.28	12-502.09	1600.80	42-434.02	1496.70	50-380.3	0+00	1524.51	
54	1545.20	64	1588.49	50	out.	14-319	1551.84	44-640	Ref. point	1+00	1561.51		
Tangent B Line 450		66	1600.42	52		14-350.42	1556.70	44-640		2+00	1618.81		
56	1550.34	68	1614.82	54		14-417.72	1574.98	44-414.49	1491.53	2+38.43	1649.52		
58	1559.53	70	1622.85	56		16-446.17	1567.78	46-432.22	1509.72	3+00	1685.42		
		72	1633.30			18-303	1529.40	46-414.04	1503.70	3+29.72	1704.52		
						20-312	1515.59			3+76.33	1739.82		
						16-309-	1539.58			4+25	1766.43		



Concrete  
Nail in Sewer Joint

10-446<sup>58</sup> (447<sup>9</sup>)

12-340<sup>13</sup> 1569<sup>42</sup>

12-426<sup>32</sup> 1587<sup>32</sup>

12-502<sup>09</sup> 1600<sup>80</sup>

12-

14-436<sup>28</sup> 1574<sup>96</sup>

14-495<sup>10</sup> 1588<sup>87</sup>

16-333<sup>20</sup> 1569<sup>42</sup>

16-490<sup>09</sup>

18-488<sup>02</sup> 1561<sup>08</sup>

18

20-421<sup>21</sup> ✓

20-505 ✓

22-497<sup>40</sup> ✓

22-409<sup>24</sup> ✓

24-

24-505<sup>0</sup> ✓

24

26

26-471<sup>20</sup> 1510<sup>42</sup>

26

28

28-481<sup>72</sup> 1503<sup>57</sup>

38-480<sup>4</sup> 1477<sup>56</sup>

40-219<sup>0</sup> 1513<sup>09</sup>

16-464<sup>44</sup>



List of B.Ms

Harris B.M. Iron Pin Set in top of Boulder 60' vs. G.S. South of Old Blacksmith Shop. Barrett Date. 1626.33	
Top of Wall	1467.41
Nail in Stump C-52-C54-15' North	1534.73
Hub about C-7+60 with Witt.	1649.50
Iron Pin Set in Boulder 2+08" P Line 5'-5"	1696.61
Nail in Rock 30' N-3+00 West Cableway	1764.35
On Old Engine Base N.S. Canyon	1461.38
Nail in 2'x8" Northside Tunnel "P" Line	1650.97
Nail in Stump about 52-468"	1537.77
Nail in Stump 10-340	1579.55
10-491 Nail Top of Concrete Joint End Iron Pipe sewer line	1597.75
Nail in Stump about 12-330	1570.88
Nail in Stump about 16-468	1573.90
Nail in Stump about 17-410	1550.96
Nail in Rock 4' West of SW Coy. Concrete Tower #1	1546.24
Nail in Rock 24-432	1525.75
Nail in Stump near B 30	1471.73

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in

IMPROVED TABLES

AND

INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree divide by degree of curve and add correction found in column of corrections.

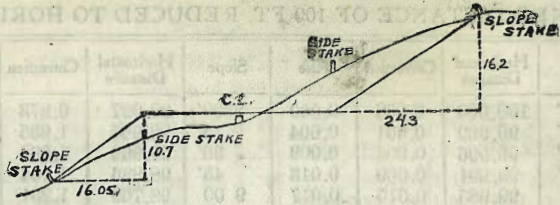
Degree of curve with a given  $L$  may be found by dividing tangent (or external) opposite  $L$  by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

1667  
 $\frac{160}{10.00220}$



TABLE XII  
 INCL. OF 100 FT. REDUCED TO HORIZONTAL



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

1750 El. Quarry



$\frac{74.8}{2.3}$

$\frac{15}{25}$   
 $\frac{17.5}{37.5}$

$\frac{25}{5}$   
 $12.5$

10.5

17.9

3.58

12.2  
5.9

400

216

4 with -

$\frac{1}{4}$  mt - was to down

say now.

$\frac{17}{3}$  3. 164  
 $\frac{164}{83}$  6