

Barrett

LAM



CONSTRUCTION

Notes

Sep - Dec

1906

404

LEVEL



W13

MICROFILMED

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.7	
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.4	
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.2	
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.92	
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	78
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	77
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	76
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	75
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	74
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	73
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	72
19	94.55	32.56	94.41	32.97	94.26	33.35	94.12	33.79	71
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	70
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	69
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	68
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	67
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	66
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	65
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	64
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	63
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	62
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	61
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	60
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	59
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	58
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	57
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	56
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	55
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	54
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	53
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	52
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	51
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	50
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.5	49
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.7	
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.0	
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	
45	70.71	70.71							

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Delgura

Sept 17th 1906

			152.05
	1.67	153.67	
			4.12
0			149.55
			2.2
5+11 ²			151.9
			0.8
			152.9

B.M. on iron bolt east side Barrett Dam

original B.C. east side Barrett dam

B.C. east side Barrett dam } relocated by L.B.H.

E.C. west " " "

Levels for profile of excavation on Barrett dam site

			152.05
	1.73	153.78	
0			12.50
	1.40	142.72	
0+10			99
0			12.89
	1.09	130.92	
0+28			11.0
0			12.73
	1.21	119.49	
0+32			97
0			12.88
	0.05	102.57	
0			12.56
	1.51	95.55	
0			12.66
	0.06	82.95	

Sept 18th 1906

		82.95		
0			5.8	79.1
1			6.0	74.9
			12.5	70.4
0			13.00	69.95
	1.57	71.52		
1			2.6	68.9
			11.0	60.5
			12.8	58.7
0			12.82	58.70
	1.31	60.01		
			8.5	51.5
			10.7	49.3
2			13.7	46.3
			14.8	45.2
			12.7	47.3
0			12.70	47.31
	0.96	48.27		
			5.2	43.1
0			12.85	35.42
	1.58	37.00		
			4.3	32.7
			6.8	30.2
			10.7	26.3
			11.0	26.0
0			12.88	24.02

			24.02
	2.16	20.18	
3420		15.0	11.2
415		15.0	14.2
4		0.0	26.2
		16.4	9.8
		6.23	19.95
	10.27	30.22	
		9.66	21.56
	4.62	20.18	
		5.0	21.2
		7.5	18.7
B.M.		0.65	25.53

bed of Cottonwood creek east side }
 " " " " west " } same site

top of lower wall

top of upper wall

bottom of hole in upper wall

B.M. On Boulder at east end of upper wall

Distance from lower edge of lower wall to upper edge of upper wall = 900 feet

Barnett Dam

Sept 21st 1906

6.01

300.73

294.72

B.M. on white knob near south end head tower bench

8.91

291.82

top of nail movable head tower

9.33

291.40

top " sill fixed " "

0.07

300.66

top of nail movable tail "

0.40

300.33

top of sill fixed " "

Distance from top of head block to top of sill
of fixed head tower 50.4

Distance from top of head block to top of sill
of fixed tail tower 28.3

Contours for proposed new tail tower and

Sep 22nd 1906

Quarry west side Barnett dam site

			300.33
2.42	302.75	275	300.00
		12.75	290.00
°		12.57	290.18
2.43	292.61	12.61	280.00
°		12.69	279.92
2.65	282.57	12.57	270.00
°		12.70	269.87
2.21	272.08	12.08	260.00
°		12.13	259.95
2.30	262.25	12.25	250.00
°		12.63	249.62
3.21	252.83	12.83	240.00
°		12.90	239.93
2.42	242.95	12.35	230.00
°		12.30	230.05
2.70	232.75		

top of sill present fixed tail tower

Sep 24th 1906

232.75

12.75

220.00

o

12.26

220.49

167

222.11

12.11

210.00

o

12.08

210.03

2.20

212.23

12.23

200.00

o

12.14

200.07

2.61

202.70

12.70

190.00

o

12.49

190.21

2.44

192.65

12.65

180.00

o

12.53

180.12

12.50

192.62

12.62

180.00

o

2.91

182.91

12.91

170.00

o

Levels to reestablish contours on east side Barnett Dam

Sep 25th 1906

			294.72	B.M. on bank south end head tower bench
8.00	302.72			
		12.72	290.00	
		12.52	290.20	
11.89	302.09			
		12.09	290.00	
		11.81	290.28	
1.87	292.15			
		12.15	280.00	
		12.17	279.99	
2.62	282.60			
		12.60	270.00	
		12.80	269.80	
12.50	282.30			
		12.30	270.00	
		11.93	270.37	
2.51	272.88			
		12.88	260.00	
		12.39	260.49	
12.15	272.64			
		12.46	260.18	
2.24	262.42			
		12.42	250.00	
		12.35	250.07	
11.78	261.85			
		11.85	250.00	

	261.85		
0		11.91	249.94
	2.38	252.32	
		12.32	240.00
0		12.55	239.77
	2.29	242.00	
		2.06	240.00
		12.00	230.00
0		12.28	229.78
	12.10	241.98	
		11.88	230.00
0		11.95	229.93
	2.46	232.39	
		12.39	220.00
0		12.84	219.55
	1.47	221.02	
		11.02	210.00
0		11.22	209.80
	2.44	212.24	
		12.24	200.00
0		11.94	200.30
	12.67	212.97	
		12.97	200.00
0		12.72	200.25
	1.68	201.93	

Sept 26th 1906

	201.93	11.93	190.00
o		11.98	189.95
	12.57 202.52	12.52	190.00
o		12.71	189.81
	2.12 191.93	11.93	180.00
o		12.04	179.89
	2.53 182.42	2.42	180.00
o		12.42	170.00
		12.20	170.22
o	12.66 182.88	12.88	170.00
		12.65	170.23
o	1.93 172.16	12.16	160.00
		12.10	160.00
o	11.30 171.36	11.36	160.00
		10.96	160.40

Profile of tunnel line for wasteway

east side of Barnett dam

			152.05	
	10.55	162.50		
0	△		12.5	150.0
°			0.59	161.91
	12.91	174.82		
+25			16.5	158.3
+50			6.0	68.8
°			0.71	174.11
	12.36	186.47		
+75			9.5	77.0
1			2.1	84.4
°			0.11	186.36
	12.78	199.14		
+25			4.6	94.5
°			0.13	199.01
	12.81	211.82		
+50			6.5	205.3
°			0.14	211.68
	12.78	224.40		
+75			9.0	15.5
2			2.8	21.7
+25			1.3	23.2
+50			1.0	23.5
+75			3.3	21.2

Sep 26th 1906

B.M. On iron bolt east side dam site

North end tunnel line

		224.46		
3			2.8	221.7
0			0.92	223.54
	5.31	228.85		
+25			3.0	25.8
+50			0.8	28.0
+65			0.4	28.4
0			12.93	215.92
	0.87	216.79		
4+10			2.2	14.6
+25			12.2	04.6
0			12.90	203.89
	0.85	204.74		
0			12.88	191.86
	0.14	192.00		
+50			4.0	88.0
0			12.93	179.07
	0.16	179.23		
+75			5.2	74.0
0			12.73	166.50
	0.43	166.93		
0			11.28	155.65
	2.73	158.38		
5			5.2	153.2
+07			11.0	47.4
+15.8 Δ			9.1	149.3

Bottom of gulch
South end tunnel line

Levels for elev. of reservoir above head town

				294.72
o	12.93	307.05		
			0.22	307.43
o	12.93	320.36		
			0.31	320.05
o	12.91	332.90		
			0.14	332.82
o	12.74	345.56		
			0.05	345.51
o	12.89	358.40		
			0.16	358.24
o	12.90	371.14		
			0.15	370.99
o	12.64	383.63		
			0.21	383.42
o	12.89	396.31		
			0.05	396.26
o	11.46	407.72		
			4.05	403.67
			10.52	397.20

Distance from top of reservoir to toe of slope
on head town bench = 190 feet

Distance from toe of slope to first rail = 30 ft.
measurements made on slope of ground

Sep 26th 1906

B.M. on back south end head town bench

top of reservoir wall
bottom " "

top of reservoir 27.0 x 11.7 } 6.47 deep
bottom " " 24.0 x 11.3 }

Levels for elev. of camp reservoir and spring

in head of Durham cañon

			239.93
0	0.29	240.22	
			12.92 227.30
0	2.94	230.24	
			4.28 225.96
0			12.08 218.16
			12.77 217.47
0	0.76	218.23	
			12.94 205.29
0	5.00	210.29	
			10.18 200.11
0	6.04	206.15	
			5.53 200.62
0	12.68	213.30	
			0.51 212.79
0	12.18	224.97	
			3.24 221.73
0	4.89	226.62	
			6.57 220.05
0			1.01 225.61
	12.48	238.09	
0			0.20 237.89
	12.90	250.79	
0			0.16 250.63

Sep 27th 1906

T. P. on trail to tail tower

inlet pipe in top of wall

bottom of reservoir

top of reservoir 9 x 12.5	} 7.80 deep
bottom 5 x 12	

Distance measured along road from camp res-
t. water trough = 2400 ft.
top of water trough

12.61

263.24

250.63

2.44

260.80

5.17

265.97

8.0

258.0

Top of inlet pipe at Spring

Distance from water trough to barn = 1200 feet
 Time required to fill 5 Gal tin at water
 trough = 4 min 10 seconds. 7.30 A.M. Sep 27th '06

$$\begin{array}{r} 258 \\ 226 \\ \hline 32 \end{array}$$

Levels to large boulder below wall

			+ 9.8
5.2	15.0		
		9.7	+ 5.3
6.3	11.2		
		0.0	+ 11.6
		12.2	
			- 0.6
0.2	- 0.8		
		12.1	- 17.9
3.4	- 9.5		
		10.0	- 19.5
2.5	- 17.0		
		19.0	- 36.0

Sept 27th 1906

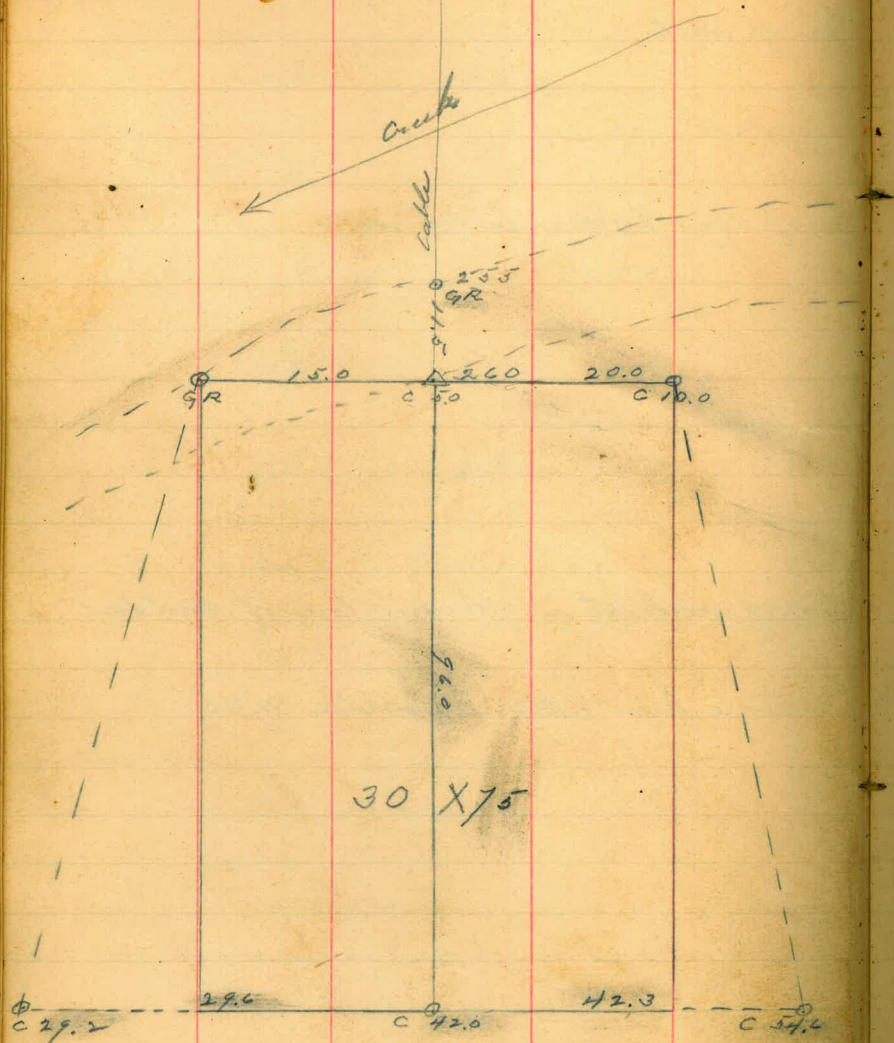
top of wall

top of large boulder below wall

bed of creek at up stream face of boulder

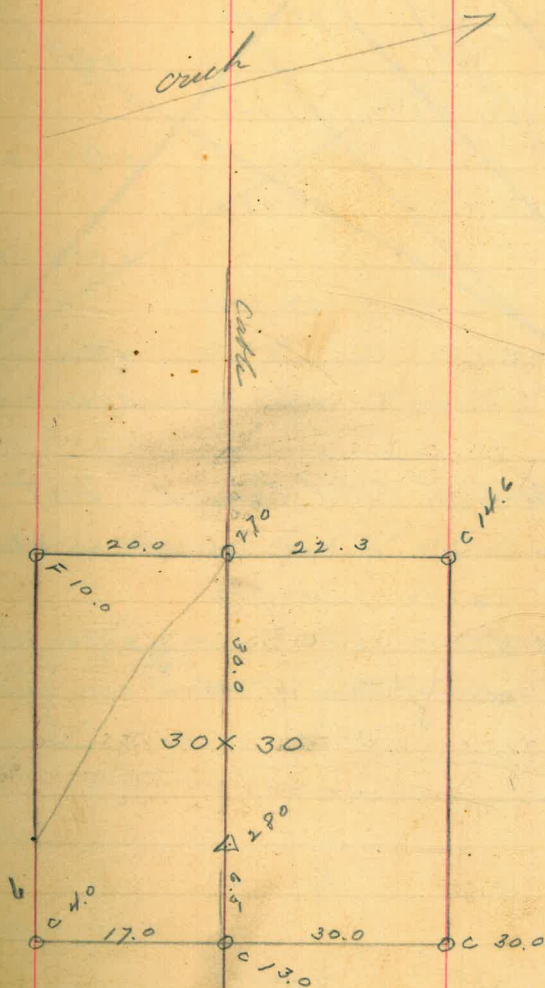
Distance from wall to boulder 440'

New fire head tower bench



Slopes 1/2 to 1

New fire tail tower bench Sep 28th 1906



Slopes 1/2 to 1

Levels to Outlet tunnel, working elev -

			71.737
6.077	78.610	1.747	76.863
6.877	87.740	1.270	86.467
6.813	73.080	12.190	80.890
2.092	82.982	4.982	78.000
B.M.		3.402	79.580

Check levels to Outlet tunnel. Govt elev -

			1518.060
12.842	1530.902		
Same B.M. No 1		2.190	1528.712
corrected elev of this B.M. =			1528.715
			82.592

			1528.714
2.660	1531.374		
		8.267	1523.107
2.378	1525.483		
		7.417	1518.066

Sep 29th 1906

B.M. on boulder near Blacksmith shop

floor of mouth of outlet tunnel (approx)
B.M. knob on granite ledge at mouth of outlet tunnel

Nov 6th 1906

B.M. disk on boulder back of Blacksmith shop

1" iron bolt on top of granite ledge 100 ft. of Station 0 of
same line near mouth of outlet tunnel
= working elev of same B.M.

1518.060 Edwards }
1518.066 King }

10/21/06.
18

6% grade line for road from Barrett Dam, down

				1598.173
	3.35	1601.52		
0				1596.0 =
+50				
1				
0			12.75	1588.77
	0.13	1588.90		
+50				1587.0
2				
+50				
3				
0	2.83	1579.00	12.43	1576.47
+50				
4				
+50				
5			12.00	1566.00
0	0.31	1566.68	12.60	1566.37
+50				
6				
+50				
0	1.44	1555.52	12.60	1554.08
7				
+50				
8				
0	1.12	1543.97	12.67	1542.15

bottom of creek on West side of canal

B.N. on toulder near E end of Barrett Dam Site

Grade at end of constructed road on West side of Barrett Dam Site

* From Sta 5 to Sta 5+60 edge of toulder.

From Sta 6+60 to 7+40 solid rock.

10/31/06

19

		1542.97		1542.00
9				15
	+50			27
10				
	+50			
0	0.31	1532.11	12.17	1531.80
11				
	+50			
12				
0	1.02	1520.54	12.59	1519.52
	+50			1521.00
13				
	+50			
0	2.03	1513.29	9.28	1511.26
15				
	+50			
0	1.57	1502.21	12.55	1500.74
16	+50			1499.0
17				
	+50			
0	0.29	1490.10	12.60	1489.71
18			2.1	1488.
	+50			
	+80			

10/3/06

20

19+50		1490.10	11.1	1479.0
0	5.00	1485.10	9.37	1480.73
20				
+50				
	1.23	1474.09	12.87	1472.86
22			10.1	1464.0
0	2.33	1464.09	12.33	1461.76
23			6.1	58.0
0	0.43	1452.19	12.33	1457.76
0	1.18	1440.66	12.71	1439.48
26+50				
26+70				
27				
0	1.88	1429.59	12.95	1427.71
28			1.6	1428.0
0	9.94	1437.10	2.23	1427.16
0	6.34	1441.94	1.52	1438.58
0	4.80	1436.44	10.20	1431.62
0	1.56	1428.45	14.53	1423.59
30			9.2	1416.0
0	0.15	1413.09	12.51	1414.94
0	7.20	1410.47	9.72	1403.27
32			6.5	1404.0
+50			9.5	1401.0

From Sta. 18.5 to Sta. 22 Solid rock cut.

From Sta. 23 line changed to 4% to Sta. 36.

Edge of Perpendicular Wall.

10/31/06
21

		1410.27		
0	12.24	1424.93	0.78	1409.69
0	0.40	1420.13	2.20	1419.73
34+50			4.9	1415.20
0	3.70	1414.38	9.45	1410.68
0	0.75	1402.96	12.17	1402.24
0	2.96	1393.78	12.14	1390.82
0	0.40	1381.29	12.89	1380.89
36+50			4.3	1377.0
37				
+50				
0	2.22	1371.24	12.29	1369.00
0			8.90	1362.51
0	12.62	1393.53		1380.89
	11.78	1404.46	0.85	1392.68
36				1405.0 =
0	2.62	1382.51		1380.89
38			+10.5	1393.0
39			+4.5	1387.0
	12.25	1382.78	12.18	1370.33
41			1.8	1381.00
0	5.90	1385.88	2.80	1379.98
45			4.9	1381.0

cut 4 26.2

Sta 36. Leave cut.

Nov. 1, '06

Pig man Sta 36.

Grade at Sta 36.

1405
1380.9
24.1

36 to 42 4%

It advisable from Sta 36 to 45
The grade may be 2.6%

42 to 48 level

From Sta 45 - 6%

21/1/06

22

		1385.88		
0	0.93	1374.61	12.20	1373.68
46+80			4.4	1370.2
48			11.6	
	1.82	1364.77	11.66	1362.95
49			7.8	1357.0
50			13.8	51.0
0	1.31	1357.51	8.57	1356.20
51			12.5	1345.0
0	0.32	1345.43	12.20	1345.11
52			6.4	1339.0
0	0.97	1334.04	12.36	1333.07
0	0.78	1328.57	6.25	1327.79
54			1.6	1327.0
55				
0	1.71	1318.22	12.06	1316.51
56			3.2	15.0
0	4.38	1309.79	12.61	1305.61
0	0.23	1296.56	13.66	1296.33
60			5.6	1291.0
0	4.65	1289.15	12.06	1284.50
61+75				
62+28			11.6	
0	0.22	1277.61	12.26	1276.89

52+50. narrow of rock.

From Sta 53 side hill Earth + Rock

Left bank of Gulch at crossing

Middle of "

63. Right 136.

11/1/06

23

		1277.61		
63			4.6	1279.0
64				
0	1.81	1266.62	12.82	1264.81
65			5.6	
0	0.97	1255.78	12.81	1254.81
66+50			2.8	1252.0
67			6.8	
0	2.34	1246.61	12.51	1240.27
69			8.6	1237.0
0	2.29	1236.11	12.79	1232.82
70			5.1	31.0
0	1.40	1227.94	9.57	1226.54
71			2.9	25.0
0	0.24	1215.24	12.92	1215.02
73			2.2	1213.0
0	2.73	1205.85	12.12	1205.12
0	5.46	1208.86	2.45	1203.40
75			7.6	1201.0
0	2.30	1198.66	12.50	1196.36
77			9.7	1189.0
0	2.20	1187.91	12.95	1185.71
79			10.9	1177.0
0	5.60	1180.88	12.62	1175.28
80			9.9	1171.0

Left tank Q. Wash.

Right " " "

11/2/06.

24

0		1180.88	12.54	1168.34
-	2.46	1170.80		
81			5.8	1165.0
+50			8.8	
82			11.8	59.0
0	0.16	1158.36	12.60	(1158.20)
83			5.4	1153.0
	1302	1171.22		
0	13.20	1184.20	0.22	1171.00
83			1.2	1173.0
0	0.69	1179.86	5.00	1172.17
88			2.9	1172.0
0	-0.08	1167.53	2.25	1167.61
90			2.5	1165.0
0	1.37	1155.76	13.14	1154.39
92			2.8	1153.0
0	(0.02)	1143.06	12.72	1143.04
	3.96	1146.20		
94			3.0	1141.0
0	1.29	1142.69	4.60	1141.40
98			7.7	1135.0
0	0.38	1131.71	11.26	1131.83
100			2.9	1123.0
0	-0.15	1119.04	12.52	1119.19
101			2.0	1117.0

L. Bk. of Wash

Wash

at Sta 83 same. Lmi. 30. to avoid heavy work
in gulches.

From Sta 83 to Sta 87 Lmi.

87 - 6% grade

grade at Sta 88

From Sta 88 - 6%

From Sta 94 Lmi. (to pass thro. Saddle)
to Sta 97

11/2/06

25

		1119.02		
0	0.03	1107.79	12.28	1107.76
103			2.8	1105.0
0	0.12	1095.64	12.27	1095.52
105			2.6	1093.0
0	0.28	1084.15	11.77	1083.87
107			3.1	1081.0
0	0.75	1072.17	12.73	1071.42
109			3.2	1069.0
0	-0.01	1059.81	12.55	1059.82
111			2.8	1057.0
0	1.26	1048.88	12.22	1047.59
113			3.2	1045.0
0	12.61	1028.98	2.48	1036.37
0	11.05	1059.92	0.2	1048.87
	12.94	1071.24	1.62	1058.30
114			1.2	1070.0 =
0			3.04	1068.20

106 L. Bank

106+70 Wash. 25' dep.

107 R. Bank

112+75 L. Bank

Lulsh. 15' dep. } Can be lightened a little by

113+50 R. Bank } raising line 25 ft. and

will get country ahead better.

Grade. raise line of Sta. 114. 31 ft.

11/3/06

26

Back up to Sta 83. and project 6% - grade.

83.	
+ 50	
84 + 40	
85 + 10	
+ 60.	
86 + 50.	
87	
+ 50	
88	
89	
89 + 50	
91 + 50	
91 + 70	
92 + 55	
93	
100	
101 + 50	
108	
113.	
132	
175	

ang of incline - 3° 10'

Edge of Wash
in Wash. 30' deep.

Edge of Wash

In Wash.

Rx Bank

Pt. of ledge

Edge of Wash

" "

" "

" "

" "

" "

Trench.

Trench. 4' wide 12' deep

End of 6% grade in river bottom above high water.

Up Lander tracks Sta.

From Sta. 133 + 4% to Sta 138.

" " 144 - 6% " " 151

Enter creek bed to avoid granite reef on right.

11/3/06.

27

181+70

191

200

203

217

221

223+90

224+50

300

- 4%

305+50

Level to

317+00

Sta. 114 of County road = 0 of line tested, in to Sta. 317+00

From Sta 0 - 2% to Sta 10

" " 10 + 3% " " 18 = 317+00

15
336.

7+80 Flame

1528
228
152727

1528
15204
152727
22

1596
69
1527
1531.

Leave truck and enter old road.

on old road opp. Matchum cabin

From Sta 200 - 6% down off bench to creek
Creek bottom

Rock point

Leave Rock Point

Wash. Bridge or Culvert.

From 224+50 along precipitous bank, ^{is} to 229
high to 229.

Sandhill

Saddle.

Saddle

5280 / 33400 (6.3)
31680
18200
15840

Profile of Dam excavation Nov 1st 1906

				152.0	B.M. east side Barrett Dam		
	9.7	161.7					
0			0.3	161.4			
	8.9	170.3				LT	RT
-47			17	168.6	top of bank	7	17
-40			9.6	160.7		10	17
0			10.0	160.3			
	1.0	161.3					
-30			8.8	152.5		16	16
0			9.7	151.6			
	1.0	152.2					
-20			9.0	143.6		18	20
0			10.1	142.5			
	1.2	143.7					
-10			3.2	140.5		23	20
0+4			3.5	140.2			
0			9.4	134.3			
	0.4	134.7					
+10			5.4	129.3		18	12
0			9.8	124.9			
	0.4	125.3					
+20			7.5	117.8		12	18
0			7.7	115.6			
	0.1	115.7					
+30			4.8	110.9		25	10

		115.7			LT	RT
0			10.0	105.7		
	0.0	105.7				
+40			3.2	102.5		25.11
0			9.6	96.1		
	0.0	96.1				
+50			0.7	95.4		23.7
+60			7.5	89.6		21.7
0			9.8	86.3		
	1.2	87.5				
+70			3.7	83.8		18.6
+80			8.8	77.7		17.8
+90			9.6	77.9		18.7
1			9.3	78.2		18.7
+10			10.0	77.5		18.6
+20			10.1	77.4		23.6
+30			10.3	77.2		23.5
+40			10.0	77.5		23.5
+50			10.0	77.5		30.3
+60			10.7	76.8		31.4
+65			10.7	76.8		
0			10.0	77.5		
	0.9	78.4				
+70			4.0	74.4		32.4
0			9.8	68.6		

				28.6	L ⁺ R ⁺
	0.1	68.7			
1 + 80			0.8	67.9	22.5
+ 90			8.2	60.5	32.8
2			9.8	58.9	
	1.8	60.7			
2			7.2	53.5	42.7
0			10.3	50.4	
	1.01	50.5			
+ 10			2.8	47.7	43.7
+ 20			4.6	45.9	45.7
+ 30			3.8	46.7	47.7
+ 40			3.2	47.3	50.7
+ 45			4.5	46.0	
+ 47			9.0	41.5	
+ 50			9.0	41.6	52.4
0			10.1	40.4	
	1.0	41.4			
+ 60			6.0	35.4	57.5
0			9.9	31.5	
	0.8	32.3			
+ 70			3.7	29.6	58.6
+ 80			3.3	29.0	60.10
+ 90			6.0	26.3	
3			6.8	25.5	

working elev of this B.M. = 82.592
 Preliminary grades for flume line from Barrette towards Dulzura Nov 7th 1906

B.M. 1			1528.715	1" iron bolt on granite ledge 120' L Sta 0 near mouth of outlet tunnel
	3.870	1532.585		
0			8.6 1524.0	1524.0 = Grade Sta 0. changed to 1524.2
1			8.7 23.9	
2			8.8 23.8	
0			6.902 1525.683	
	8.830	1534.513		
3			10.8 23.7	
4			10.9 23.6	
0			7.076 1527.437	
	2.608	1530.045		
5			6.5 23.5	
6			6.6 23.4	
7			6.7 23.3	
B.M. 2			1.974 1528.071	
	6.629	1534.700		
7			11.2 23.5	Grade raised 0.20 at Sta 7
8			11.3 23.4	
9			11.4 23.3	
10			11.5 23.2	
B.M. 3			4.264 1530.036	
	3.912	1533.948		
11			10.8 23.1	
12			10.9 23.0	
13			11.0 22.9	

Preliminary Grades *Sturms Line*

1		1533.948		
0			8.017	1525.931
	5.854	1531.785		
14			9.0	22.8
15			9.1	22.7
B.M. 4			13.181	1518.604
	11.416	1530.020		
16			7.4	22.6
			8.008	1522.012
	12.782	1534.794		
17			12.3	22.5
0			10.932	1523.862
	5.325	1529.187		
18			6.8	22.4
19			6.9	22.3
B.M. 5			17.74	1527.413
20			7.0	22.2
21			7.1	22.1
0			7.96	1521.491
	9.185	1530.676		
22			8.7	22.0
23			8.8	21.9
B.M. 6			4.369	1526.307
	2.351	1528.658		
24			6.9	21.8

Nov 8th 1906

Preliminary Grades Same line

	1528.658		
25		7.0	1521.7
26		7.1	21.6
27		7.2	21.5
28		7.3	21.4
29		7.4	21.3
30		7.5	21.2
B.M.7		9.164	1519.494
	6.942	1526.436	
31		5.3	21.1
32		5.4	21.0
0		6.183	1520.253
	6.785	1527.038	
33		6.1	20.9
34		6.2	20.8
35		6.3	20.7
36		6.4	20.6
37		6.5	20.5
0		12.830	1514.208
	11.104	1525.312	
38		4.9	20.4
39		5.0	20.3
40		5.1	20.2
B.M.9		11.536	1513.776
	12.786	1526.562	

Rail Grades Flume line

Nov 9th 1906

	1526.522		
41		6.5	1520.1
42		6.6	20.0
43		6.7	19.9
o		0.950	1525.612
	0.708		1526.320
44		6.5	19.8
45		6.6	19.7
B.M. 10		0.820	1525.500
46		6.7	19.6
47		6.8	19.5
48		6.9	19.4
o		5.562	1520.758
	8.975		1529.733
49		10.4	19.3
50		10.5	19.2
51		10.6	19.1
B.M. 11		2.641	1527.092
52		10.7	19.0
53		10.8	18.9
o		6.735	1522.798
	5.774		1528.570
54		9.8	18.8
55		9.9	18.7
56		10.0	18.6

42 + 20 = 45 EATONS LINE

Very windy !!

Pub. Grads. Home line

	1528.570		
B.M. 12		2.718	1525.852
	2.393		1528.245
57		9.7	18.5
58		9.8	18.4
o		5.341	1522.904
	6.954		1529.858
59		11.5	18.3
60		11.6	18.2
B.M. 13		0.365	1529.493
61		11.7	18.1
62		11.8	18.0
63		11.9	17.9
o		6.615	1523.243
	1.040		1524.283
64		6.5	17.8
65		6.6	17.7
B.M. 14		0.587	1523.696
66		6.7	17.6
67		6.8	17.5
68		6.9	17.4
o		3.638	1520.645
	5.645		1526.290
69		9.0	17.3
70		9.1	17.2

Paul Grader Home Lane

		1526.290		
71			9.2	1517.1
o			12.564	1513.726
	9.640	1523.366		
72			6.4	17.0
B.M. 15			1.323	1522.043
	2767	1524.810		
73			7.9	16.9
74			8.0	16.8
75			8.1	16.7
o			2.720	1522.090
	2.277	1524.717		
B.M. 16			0.937	1523.830
76			8.2	16.6
77			8.3	16.5
78			8.4	16.4
o			1.240	1523.527
	2727	1526.254		
79			10.0	16.3
80			10.1	16.2
B.M. 17			2.386	1523.868
81			10.2	16.1
82			10.3	16.0
o			8.872	1517.382
	4.905	1522.287		

Nov 10th 1906

Trail Grade Level line

	1522.287		
83		6.4	1515.9
84		6.5	15.8
B.M. 18		1977	1520.510
85		6.6	15.7
86		6.7	15.6
87		6.8	15.5
88		6.9	15.4
89		7.0	15.3
B.M. 19		4.179	1519.109
	2.707	1520.815	
90		5.6	15.2
91		5.7	15.1
0		4.269	1516.546

Sta 84 = Sta 82 EATONS LINE

11/12/06.

Slopes on road line

				End Area	Rock	Loose Rock	Earth
14	Superm.	Solid rock	average of $8' \frac{\text{cut}}{\lambda}$ to Sta 15	120	120	192	946
13+50	36°	Loose Rock	14	87.5		284	
12+50	30°	(average size of 6' to 13+50 around Superm. Rock bluff. 40' long to		65.8	65.8	610	
10	30°			65.8	65.8	464	
8	28°	Loose rock to 12+50		59.5	59.5	256	
7	34°	Solid rock. to 8.		79.1	79.1	292	
6	34°	Earth + Rock. to 6+60		79.1	79.1	181	81
		from 5 to 5+70 Solid rock average	10ft. cut		181		
5	29°	Earth + Rock.		63	63	86	128
4	25°	from 4 to 4+40 Solid Rock		52.5	52.5		158
+50	42°			119	119		149
3	21°			42	42		87
2+50	25°	Earth + Boulders to 4		52.5	52.5		242
1							
+50							
0							

			End Area.	Rock	Loose Rock	Earth
				52.3		2687
30	36°		87.5	313		353
29	40°	Loose rock to Sta 30+50	104.3	207		
28+50	Broken	Rock cut of 8' to Sta 29	120			163
28	27°		57.4			327
26+50	28°		59.5	220		220
25+50	28°		59.5			250
24+50	33°		75.6			420
23	33°	Loose rock to Sta. 28+50	75.6	1275		
20	Broken.	From 20 to 23 average cut of 20'	166.6	172		
19+50	25°	Solid Rock to Sta 23	52.5	578		
17+50	40°		104.3	308		
16+50	29°	Solid Rock to 19+50 ^{disintegrated & Loose Rock}	63			339
15	28°	Earth + Rock. to 16+50	59.5	332		
				3395		4759

End Area Rock Loose Rock Earth

					3395	4759
28	45°			104.3		292
47	26°			53.9		194
46	25°	Loose rock to Sta.	49+50	52.5	194	
45	26°			53.9	210	
44	28°			59.5	136	
+50	36°			87.5	162	
43	36°			87.5	338	
42	38°			95.2	286	
41	28°			59.5	202	
40	24°			49	283	
39	40°	Solid rock to Sta	46	104.3		736
37	38°	Loose rock to Sta.	39	95.2	242	
+50	50°			166.6	326	
36	52°			184.8	650	
35	50°			166.6	260	
34 + 50	42°			114.1	178	
34	34°			79.1	152	
33+50	26°			87.5	212	
32+90	40°			104.3	353	
32	41°			108.5	361	
31	36°			87.5	141	
30+65	45°			131	262	

30+50

Solid rock to Sta 37

			End Area	Rock	Loose Rock	Earth
	72	34°		79.1		280
	71	32°		72.1		260
	70	31°	Loose Rock to Sta 79	68.6		286
	69	28°		86.		318
	68	28°		86		405
	67	30°		133		518
	66	31°		147.		476
	65	28°		110.		314
	64	28°	Earth to Sta 70	59.5		232
	63	30°		65.8		221
	62	26°		53.3		185
	61	23°	Earth + Rocks to Sta. 64	46.2		231
	60	24°		78.7		227
	59	22°	Earth to Sta 61	44.1		178
	58	25°		52.5		224
	57	31°		68.6		213
	56	23°		46.2		196
	55	28°	Earth + Rocks to Sta 59	59.5		232
	54	30°		65.8		244
	53	30°		65.8	8343	244
	52	30°		65.8		244
	51	40°	Loose rock to Sta. 55	104.3	178	
	+ 50	36°		87.5	314	
	50	disputed				
	49+50	35°	Solid rock to Sta. 51	81.9		516
				8835	7057	Mile No. 1

 No. 2
 Mile No. 1

			End Area	Rock	Loose Rock	Earth
				0	2465	2775
90	22°		44.1		58	
+50	10°		18.2		50	
89	19°		37.1		166	
88	26°		52.5		89	
+50	22°		44.1		77	
87	20°		39.2		170	
86	25°		52.5		59	
85+60	11°		19.6		82	
85+10	31°	Edge of Bank	68.6			
84+70		Each 15' Deep.				
84+40	37°	Edge of Bank	32.4		138	
84	38°		35.2		137	
+50	26°		53.9		113	
83	31°		68.6		152	
82+50	38°		35.2		105	
82	10°		18.2		152	
81	23°	Loose Rocks to Sta 91+70.	46.2			138
80	21°		60.9			246
79	32°	Earth to Sta 81.	72.1		235	
78	25°		52.5		197	
77	26°		53.9		233	
76	32°		72.1		285	
75	35°		81.9		335	
74	39°		99.4		311	
73	31°		68.6		276	
				0	5879	3219

				End Area	Rock	Loose Rock	Earth
	13	0	In Creek bottom.			110	
	12	28°		59.5		220	
	11	28°		59.5		210	
	110	26°		53.9		200	
	9	26°		53.9		185	
	8	24°		49.0		155	
	7	18°		35.0		187	
	6	30°		65.8		232	0
	5	28°		59.5		149.9	321.9
	4	27°		57.4		58.79	
	3	18°		35.0		216	
	2	12°		22.4		172	
	1	9°	Loose Rocks Sta 113	16.1		106	73
	100	0°					29
	99	19°		51.1			95
	98	26°		93.1			267
	97	32°		163.8			475
	96	25°		86.1			462
	95	23°		72.1			232.
	94	26°		93.1			306.
	93	26°		93.1			344.
	92	35°		86.1			332.
	+70	21°	Earth to Sta 101	39.2		102	70.
	91	20°		39.2			58.91
					Mile N ^o 2.	67.54	

Mile No. 3

			End Area	Rock	Loose Rock	Earth
165	0°	In Creek bottom.		3		35
164	9°		18.9			35
163	0°	Earth to 165.			1499	(70)
52	0°	In creek bottom.				19
51	6°		10.5			45
150	8°	Earth + boulders to Sta 152	14.0			86
49	14°		32.9			89
48	8°		15.4			77
47	12°		26.6			77
46	8°		15.4			28
145	0°	Earth to Sta 149				
140	0°					81
39	17°		43.4			203
38	22°		66.5			310
37	27°		100.8			290
36	20°		56.			194
35	19°		51.1			189
34	19°		51.1			133
33	10°		21.			34
132	0°	Earth to Sta. 140				
				Mile No 3	1499	1835

	218	22°		44.1	69.	
	+60	24°		43.	88	
	+10	23°	Beginning of limestone reef.	46.2		extending to river
	17	0°				
	216					
MP Mile No. 5	3	0°	In creek bottom.			62
	+50	22°		66.5		101
	4	17°		43.4		152
	1	16°		38.5	157	(37.5) 71
	200	0°	Leave old road. South to Sta. 203			
	182					
	+70	0°	End of reef and enter old road		20	
	+50	26°		53.9	100	
	181	0°				
	+50	0°			55	
	180	28°		59.5	220	
	179	28°		59.5	192	
	178	22°		44.1	375	
	+80	40°		104.3	485	
	177	49°		158.9	415	
	176	30°		65.8	190	
	175	19°	Beginning of limestone reef.	37.1		
			extending into River			
				Mile No. 4	(2052)	(141)

	12	17°		32.2		112
	11	15°		28.0		107
	10	16°		30.1		104
	9	14°		26.6		94
	8	13°		24.5		86
	7	12°		22.4		75
	6	10°		18.2		17 (595)
	505250	0°				
	<hr/>					
	232	0°	Enter old pond		(157)	(315)
	231	22°	↑	66.5		123
	230	25°	↓	85.1		282
	229	22°	Earth	66.5		162
	228	10°		21.		29
	227	0°				
	226	0°				
	+50	0°				13
	225	7°		14.0		45
	224+50	6°	Earth	11.2		20
	223+50	0°	↓			
	+10	0°	in creek bottom			
	221	24°	End of reef	49.	207	
	220	29°		63.0	216	
	219	26°		53.9	181	
				Mile No. 5	(761)	(1271)

320	0°
19	18°
18	20°
17	0°
16	10°
15	15°
14	17°
313	12°

	Rock	Loose Rock	Earth
--	------	------------	-------

Mile No 1	8835	7057	
2		6702	5891
3		1499	1855
4	2052		141
5	761		300 1271
6			600 1314
	11648	15258	11372

from 320 to 335 (connect with Co. Survey)
35 light work - Earth

33.2	535
18.2	137
28.0	72
32.2	32
26.6	85
	111
	109
	109

Mile No 6

1314

Cable for Monmouth trolley

4.07

295.47

1.97

291.40

293.50

1.97

293.50

Cable set at =

291.0

Levels for setting water gage

9.12

9.16

9.08

9.12

(average)

9.12

0

1

8.12

2

7.12

3

6.12

4

5.12

5

4.12

6

3.12

7

2.12

8

1.12

9

0.12

10

+0.88

79.88

79.69

60.14

Dec 13th 1906

Top of sill fixed head tower

Set red and white flag on east side canon } middle
 " " " " " west " " } ordinate

P.M. Dec 15th 1906

Prod at west end old wall

Dec 13th 1906

" " center " "

" " east " " "

" for water gage 1 up stream on east side

Distance across stream at water level 66.6

" " " " 67.0

" " " " 66.6

" " " " 64.2

" " " " 64.1

" " " " 65.3

" " " " 67.7

" " " " 70.0

" " " " 71.8

" " " " 75.0

" " " " 78.8

Prod at front of box

See Page 58

near

ceiling

Levels to establish 175' contours on original

site at Barnett

			152.05
10.35	162.40		
0		0.33	162.07
12.59	174.66		
0		5.86	168.80
12.09	180.89		
0		5.89	175.00
9.10	184.10		
		9.10	175.00

Dec 14th 1906

B.M. iron bolt on east side of present site

8 penny nail in 2" x 2" post east side

8 " " " " " east "

Rock in place on platform visible tail tower

Dec 15th 1906

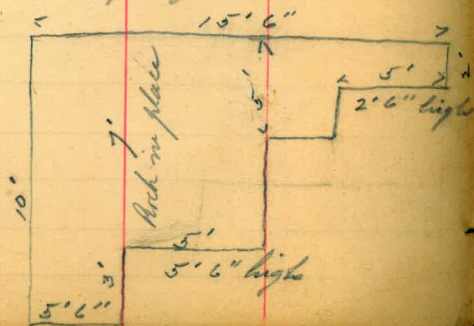
base - 22' 4" x 21' 4"

top 20' 8" x 19' 4"

4' 8" high

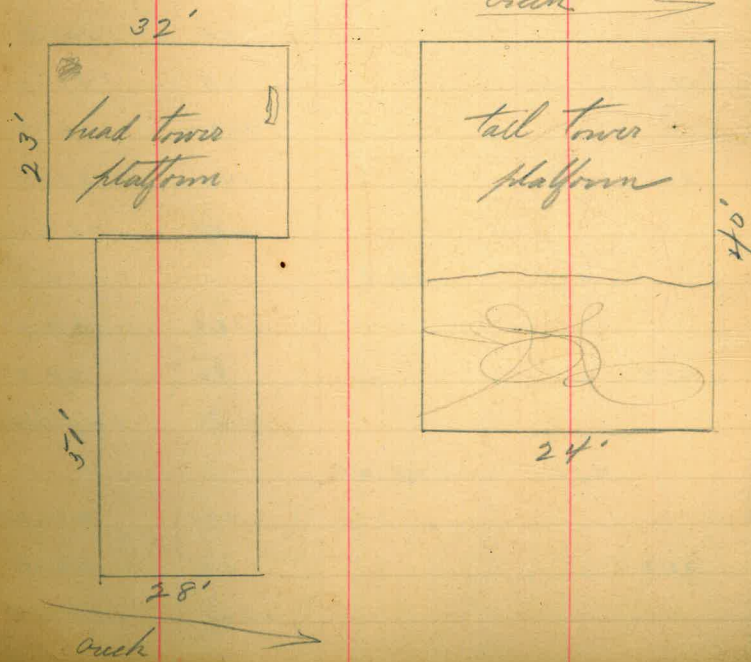
Available space for rock on platform head tower

Vacant



Bolt

Creek →



Connection of the original Bennett Dam site

Dec 17th 1896

			175.00	Hub at Sta 0 B.C. east side
	0.34	175.34		
O.B.C.			0.34	175.00
17 L			6.5	28.8
+20			6.5	28.8
17 L			11.1	44.2
0			12.54	162.80
	0.77	163.57		
+460			3.2	60.3
17 L			6.1	57.5
0			12.63	150.94
	0.56	151.50		
+600			1.5	150.0
19 L			2.5	49.0
+80			11.9	39.0
22 L			14.1	37.4
0			12.87	138.63
	0.19	138.82		
1			8.8	30.0
27 L			9.0	29.8
0			12.56	120.26
	0.95	127.21		
+2000			6.2	21.0
32 L			6.8	20.4
0			12.67	114.54

Correction of the original Barrett data

				114.54
	0.10	114.64		
+40			1.1	113.0
	38 L		2.2	12.4
+60			9.6	05.0
	41 L		6.6	08.0
0			12.89	101.75
	1.72	103.47		
+80			6.5	97.0
2			12.3	91.2
	51 L		9.7	93.8
	1 R		12.3	91.2
0			11.74	91.73
	0.42	92.15		
+20			12.1	80.0
	58 L		6.9	85.2
	2 R		12.1	80.0
0			12.50	79.65
	3.32	82.97		
+40			12.7	70.3
	65 R		5.5	77.5
0			12.72	70.25
	3.44	73.69		
+60			11.7	62.0
	72 R		5.7	69.0
	3 L		12.9	60.8

Connection of the original Barrett dam site

		73.69		
0			12.47	61.22
	0.45	61.67		
2+80			16.3	45.4
	56L -90°		0.7	61.0
	5R		17.3	44.4
0			12.57	49.10
	1.93	51.03		
0			12.21	38.82
	0.58	39.40		
3			7.9	31.5
	55L -90°		+19.6	59.0
	7R		7.9	31.5
0			11.68	27.72
	0.72	28.44		
+20			6.9	
	102L		14.4	14.0
	12R		7.4	21.0
+40			8.4	20.0
	102L		14.4	14.0
	12R		8.4	20.0
+80			9.9	18.5
	102L		14.4	14.0
	12R		8.6	19.8
+88			7.2	21.2
0			1.39	27.05

Bottom of spillway

top of wall west side

Correctors of original Barrett datasets

				27.05
	12.00	39.05		
4			90	30.0
	94 L		25.0	14.0
	7 R		12.4	26.6
0			0.72	38.33
	12.87	51.20		
0			0.15	51.05
	11.90	62.95		
+20			10.9	52.0
	79 R		44.9	18.0
	4 L		9.3	53.6
0			0.47	62.48
	12.76	75.24		
+40			0.2	75.0
	82 R		33.2	42.0
	13		0.2	75.0
0			0.39	74.85
	12.90	87.75		
+60			0.8	87.0
	60 R		25.5	62.2
	2 L		0.8	87.0
0			1.01	86.74
	12.21	98.95		
+80			1.2	97.7
	44 R		8.5	90.4

Construction of original Bennett dam site

		98.95		
0			1.19	97.76
	12.92	110.68		
5			3.7	107.0
	38L		18.0	92.7
0			0.41	110.27
	12.50	123.07		
+20			2.5	120.6
	32L		14.6	98.5
0			1.37	121.70
	12.91	134.61		
+40			5.0	29.6
	27L		14.3	20.3
0			0.22	134.39
	12.50	146.89		
+60			9.9	37.0
	22L		20.9	26.0
+80			0.5	46.4
	20L		10.9	36.0
0			1.17	145.72
	12.50	158.22		
6			1.6	56.6
	19L		6.7	51.5
0			1.54	156.68
	11.9	167.87		

Connection of original Bennett dam site

	167.57		
o		0.17	167.70
9.57	177.27		
6 + 26.65 E.C.		2.27	175.00
17 R		11.1	66.2

Distances across stream from bulkhead to ledge
at cutoff wall

	distance across
0	61'
1	62'
2	62.5'
3	63'
4	65'
5	65'
6	65'
7	67'
8	70'
9	81'

See page 49 for distances across at water gage

BOULDER

STAKE

STAKE

LEDGE

GAGE

STAKE

STAKE

BULKHEAD
WALL

50'

50'

98.5'

61'

50'

50'

107.2'

Levels for Gage Rod at Barrett Dam

	6.078
	6.072
	4.030
	4.040
	3.110
(New reading)	5.958
	5.868
	938
	989
	986
	918
	943
	Average.

Upper Site.

2/1/07

Bottom of box	W side
"	" " E "
Top	" " W "
"	" " E "
3' mark on box	gage
Crest of Dam	E of box.
"	" " Center of channel.
"	" " "
"	" " E bulkhead.
"	" " " "
"	" " W "

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MINUTES	LKS.	MINUTES	LKS.	MINUTES	LKS.
1	2 $\frac{1}{3}$	21	49	41	95 $\frac{2}{3}$
2	4 $\frac{2}{3}$	22	51 $\frac{1}{3}$	42	98
3	7	23	53 $\frac{2}{3}$	43	100 $\frac{1}{3}$
4	9 $\frac{1}{3}$	24	56	44	102 $\frac{2}{3}$
5	11 $\frac{2}{3}$	25	58 $\frac{1}{3}$	45	105
6	14	26	60 $\frac{2}{3}$	46	107 $\frac{1}{3}$
7	16 $\frac{1}{3}$	27	63	47	109 $\frac{2}{3}$
8	18 $\frac{2}{3}$	28	65 $\frac{1}{3}$	48	112
9	21	29	67 $\frac{2}{3}$	49	114 $\frac{1}{3}$
10	23 $\frac{1}{3}$	30	70	50	116 $\frac{2}{3}$
11	25 $\frac{2}{3}$	31	72 $\frac{1}{3}$	51	119
12	28	32	74 $\frac{2}{3}$	52	121 $\frac{1}{3}$
13	30 $\frac{1}{3}$	33	77	53	123 $\frac{2}{3}$
14	32 $\frac{2}{3}$	34	79 $\frac{1}{3}$	54	126
15	35	35	81 $\frac{2}{3}$	55	128 $\frac{1}{3}$
16	37 $\frac{1}{3}$	36	84	56	130 $\frac{1}{3}$
17	39 $\frac{2}{3}$	37	86 $\frac{1}{3}$	57	133
18	42	38	88 $\frac{2}{3}$	58	135 $\frac{1}{3}$
19	44 $\frac{1}{3}$	39	91	59	137 $\frac{2}{3}$
20	46 $\frac{2}{3}$	40	93 $\frac{1}{3}$	60	140

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

Angle	COR. IN LINKS	Angle	COR. IN LINKS	Angle	COR. IN LINKS	Angle	COR. IN LINKS
0		0		0		0	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

Handwritten calculations on the left page, including a vertical sum of 24-3 and other numbers like 300.66, 18.46, 28.91, 335.40, 328.91, 311.90, 291.82, 30.08, 290.4.