

W 144

FIELD BOOK

361

CITY OF
SAN DIEGO - CALIFORNIA
ADDITIONAL WATER SUPPLY
MISSION GORGE DAMSITES 1 & 2

3

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

MICROFILMED
NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

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	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

FOR KEITH'S RAILROAD CURVE TABLES SEE END OF BOOK.

2.7.3 - 4-55

CITY OF SAN DIEGO
California

Additional Water Supply

Water Commission Office
320 McVeece Bldg
Cor 5th & F Sts
H. N. Savage C. E.

IBK #3

129

1305

2575

1.29.75 Cor Ret Wall Cath Ch Highwellington Curb

Ref A2

Sta A2

68 to Top of Old Mission Dam Δ 354-54

Riv Bed " " " Line Δ 3-4 = 230-56

" " " 2 to 3 180-53^{10/10}

67 to 68 - 81-47

66 to 67 66-14

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Original Index in back of book

Sta	Az	Rdg	H. Dist	Vert L	
64 to 65	36-37	2.18	818		
π @ #64			MI 364.78		
*64 to 233	338-01	8.50	846	0	
			Cor. Dist		
"64 to "	326-2430	9.04	900'	+4-38	+930 433
	Shots across Gorge for Topog.				
π @ #64	321-10	8.08	800'	+5-33	+778 437.8
	307-13	8.00	792	+5-55	+82 442.0
	299-0	7.58	750	+6-16	+82.2 442.2
	297-30	7.20	718	+3-41	+46 406.0
	287-50	7.50	746	+4-21	+56.7 416.7
	287-31	8.78	859	+8-04	+122 482
Exposed Rock	278-51	7.73	762	+7-0	+93.3 453.3
Earth	267-20	8.00	790	+6-18	+87 442.3
"	257-42	8.50	840	+5-45	+84.5 444.5
"	251-19	8.75	870	+4-56	+75 435
"	245-50	9.70	965	+4-22	+73.5 433.5
"	240-04	9.90	988	+4-27	+76.5 436.5
"	230-03	10.80	1075	+3-30	+68.8 425.8
Exposed Earth	244-11	9.25	920	+2-28	+40 400
	249-28	8.14	810	+2-50	+40.4 400.4
	262-51	7.25	745	+1-42	+21.5 381.5
#64 to AX point No side set to shoot so side	260-34	7.00	700	0	360

Additional Topography Mission Damisito

Hayler Loe
Franklin X
Williams

Sept 22/21

3

FS on #65 Bk #2 p13

360 Bk #1 p?

Hub uphill from "233A" for Topog. in gully North

On rock hog back S.R. @ Surf

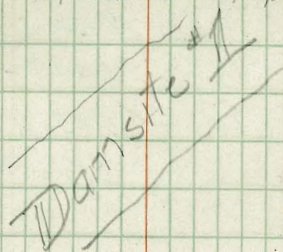
" " " Exposed

" Toe sheer Cliff " Main outcrop side below

" Top " on bench

@ a bath not marked * see next page

Something Rotten in Az and E1



Gully washed bar up + also down hillside - 100 each way

360 Hub set on No side

Plotted 10/25/21
HRS

Sta	Az	Rod	H. Dist	Vert	
$\pi @$ 233	5.0				
Earth	✓ 131-08	9.70	965	+4-30	436
"	✓ 139-35	9.80	970	+4-54	443
"	✓ 147-53	9.75	970	+4-34	437
Rock Exposed	153-11	10.05	1000	+4-23	436.8
	✓ 155-35	10.60	1055	+4-25	441.5
		11.20	1110	+5-18	463

Sta	Az	Rod	H. Dist	Vert	
$\pi @$ ΔX	P+3 5.00				360
	✓ 85-08	7.60	758	+2-51	437.6
	✓ 104-35	7.25	744	+4-02	411
	✓ 109-11	7.35	732	+3-48	407.6
	✓ 105-30	8.05	798	+5-52	442
	112-53	8.60	850	+5-29	439.3
	✓ 116-23	9.05	899	+5-03	439.2
	✓ 122-24	10.60	1045	+4-02	434.2
	✓ 119-23	8.20	818	+2-54	401.5

See also pages 52+53

Plotted 10/25/41
MRS

Shots So across R same stn p 3
on No side S.D.P B.S. #64

lath unmarked * see p 3

STATSITE #1
Additional Topog
above 260 Eley

End

Sta	Az	Rod	H. Dist	Vert	
⊙ #4 } B#2 p 53 }	465				
#4 to 236	320-01	3.07	262	+22-40	+109 469
⊙ #236	+26				
#236 to #51	203-12	10.50	1050	0	360
" to #237	226-46	1.23	123	"	360
foot of Cliff	198-16	10.80	1075	+3-30	+66 426
"	195-17	9.84	980	+2-36	+455 4055
"	192-36	9.50	945	+3-08	+58 412
"	188-49	8.90	888	+2-50	+44 404
Earth	181-42	8.40	835	+3-36	+528 412.8
Rock Exposed	179-41	8.20	815	+4-36	+65.7 425.7
Earth	177-50	8.10	805	+4-0	+56.3 416.3
"	174-10	8.00	793	+4-25	+61.5 421.5
Rock Exposed	172-06	8.00	790	+5-56	+82 442
Earth	165-05	7.88	780	+6-57	+94.3 454.2
"	166-37	7.60	755	+5-07	+67.8 427.8
"	163-45	7.45	742	+4-51	+62.8 422.8
"	161-30	7.25	720	+5-07	+62.2 424.2
"	161-32	7.80	770	+6-54	+93.0 453.0
"	157-02	7.05	695	+6-28	+79 439
"	156-27	6.74	670	+4-23	+51.2 411.2
"	152-33	6.97	690	+5-54	+71 431
"	144-02	6.98	690	+6-03	+73 433
Rock Exposed	138-54	7.10	700	+6-15	+76.8 436.8

Additional Topog above 360 Dam site #2
BS on #3 stub line down R from Old Mission Dam
Sec BK #2 p 53 Az 3 to 4-230-56

BS #4 in River Bed

Book #1 15 in
Office not available
Az of Original line

Beginning shots for additional Contours

Cliff goes up Vert 40ft +10ft back 960'

Toe Vert Cliff E end

DAM SITE #2
Add. Topog above 360

Plotted
out with
diff.

Sta	Az	Rod	H	Dist	Vert	L
X@236						
Rock Exposed	132-27	7.15	705	+6-31	4805	4405
"	124-27	7.48	738	+6-26	+83	443
"	120-48	8.05	799	+5-41	+79.4	439.2
<hr/>						
*236 to #55	161-53	6.22		0		360
<hr/>						
54 to 55	52-27	1.52				
X@ #55	6.97					
#55 to #236	341-36	6.30		0		
<hr/>						
Earth	337-25	6.00	688	+3-08	+377	397.7
Rock Exp	340-51	7.50	748	+3-27	+45	405
Earth	349-17	8.70	868	+3-32	+533	413.3
"	346-29	9.25	919	+5-02	+81	441
Rock Exp	338-42	8.10	802	+6-01	+845	444.5
"	331-56	7.28	718	+6-52	+865	446.5
"	326-26	7.20	712	+6-39	+828	442.8
"	325-26	7.10	700	+6-40	+818	441.8
"	321-43	6.32	630	+3-60	+422	402.2
"	322-08	"	630	+2-54	+32	392
Earth ^{not much}	312-36	6.70	668	+4-0	+465	406.5
Rock Exp	311-0	7.60	750	+6-41	+878	447.8
Earth	304-27	8.30	870	+6-34	+94	454
"	300-12	8.95	885	+5-50	+902	450.2

End shots to So Side

Began shots to No Side

BR #2 - P11
BS #54

Sept 23/21

1st Add Topog Shot to No Side

Dam site #2
 Add Topog above 360

Small cliff outcrop Top
" " " " " " " " " " " " " " " " " " " " " " " "

Plotted Oct 25-21
2/28

Sta	Az	Rod	H. Dist	Vert L	
					4888
K@ 55	⁵⁰⁷ 295-30	1080	1075	+4-27	4438
					+82.5
Rock Exp	287-20	1060	1055	+4-28	4425
					-31.5
✓	335-15	540	538	-3-21	328.5
✓	336-32	518	514	-5-0.9	-46.3
					313.7

See also pages 52+53

Platted
10/25/21
JH/RS

Additional Topog above 360 Dam site #2 ⁷

17 @ Gulch Rock Washed bare

two shallow test pits in earth

End shot to No. 514

P Line

Hayler Loc
Franklin T
Williams Rod.

Transit #3

126

P Beg 175

Alibi } Vert Vernier
poor shape 8

Profile for Pipe Line Mission Dam to S.D. Sept 24/21

Sta A2 Rod H. Dist Vert L H_v
BS HI FS

π@ #67 H.I. = 364.47
447 360

#67 to 0+00 30°-22' 4.96 483.3 ✓ -9°-36' -81.71 ✓ 278.3 ✓
π@ 0+00 4.93 283.23

BM 341-36 0.66 67 ✓ 0 126 281.07 ✓

π@ 0+00 4.93
0 to 1+21 256°-43' 2.90 291 ✓ +0°-47' 1.50 ✓ 281.73 ✓

π@ 2+21 5.17 286.90

1 8.6 278.3 ✓

2 8.9 278.0 ✓

5+23 11.44 275.46 ✓

2+21 to 5+23 254°-51' 2.31 232 -1°-33' ✓

π@ 5+23 1.6 4.62 280.08

3 2.22 223 +1°-0' +38 279.3 ✓

4 3.8 276.3 ✓

5 4.7 275.4 ✓

to 9+43 220°-10' 4.19 420 -1°-50' 13.44 262.02 ✓

6 5.5 274.6 ✓

6+78 7.8 272.3 ✓

π@ 9+43 4.43 266.45

7 2.2 264.3 ✓

8 6.0 260.5 ✓

9 6.1 260.4 ✓

10 3.1 263.4 ✓

to 10+50 196°-37' 1.06 107 3.11 263.34 ✓

FS. #68 = A2-81-47

π H.I. = 278.3 4.93 283.23 281.97 } Iron Bolt in top of Abutment
of Old Mission Dam. Approx Axis also

35 07 262.02 @ 9+43

Sta	Az	Rod	H. Dist	Vert L	Elev
T @10+50			^{RS} 5.27	^{VHI} 268.61	^{FS} 263.34
to 13+91	192°-07'	340	341	4.89	263.72
11				8.2	260.4
12				7.6	261.0
13				7.4	261.2
T@13+21			4.61	268.33	
to 15+87	184°-38'	195	196	8.74	259.55
14				5.4	262.9
15				8.8	259.5
T@15+87			^{RS} 4.72	^{VHI} 264.38	
to 21+66	170°-57'	5.78	579	7.75	267.34
16				4.5	259.9
17				5.3	259.1
18				4.2	260.2
19				3.8	260.6
20				1.0	263.4
T@21+66			5.21	272.55	
to 25+16	200°-35'	342	350	0.93	271.62
21			5.21		4.5
22					4.8
23					3.4
24					2.0
25					0.8
T@25+16			^{RS} 5.23	^{VHI} 276.70	
to 30+90	224°-04'	5.73	574	11.03	260.59

15 91
1 96
15+87

1587
578
21+66
350

25+16
5-74
30+90

25+16

HI off 10+50 263.34

HI off 13+21

259.57

HI off 15+87

267.23

HI off 21+66 267.34

271.47

17 Co Highway Grade

" " " "

" " " "

" " " "

" " " "

" " " "

" " " "

260.61

267.6
4.8
22.1
9
71.5

BS F.I. F.S.

5.17

30+90
5 41
36 + 31
7 03

10

Sta A2 Rod H. Dist Vert L Elev

π@25+16	5.23	523	276.70		
26				5.5	271.2
27				6.6	270.1
28				9.1	267.6
29				12.0	264.7

π@30+20 5 5.35 265.94

to 36+31	31	237°-29'	5.40	541	9.98	255.96
30				3.1	262.8	
31				5.3	260.6	
32				8.5	257.4	
33				9.7	256.2	
34				9.9	256.0	
35				10.3	255.6	
36				9.9	256.0	

π@36+31 5.18 261.14

to 42+34	34	244°-07'	6.02	60.3	+0°-48'	+8.44	264.40	
37					4.8	256.3		
38					4.2	256.9		
39					5.3	255.8		
40					7.8	253.3		
41					4.9	256.2		
42				5.66	5.67	+0°-35'	+5.77	266.8

43 + 34
271.47 254.6

261.80
5.23
267.03

255.89

36+31

264.15 by levelling

43+34
4 71
48+08
2 25

11

Sta	As	Rod	Hor Dist	Vert L	Elev
π@42+34			5.17	269.57	
to 47+05	214-54	4.70	471	970	259.81
43				72	262.4
44				28	259.8
45				103	259.3
46				26	260.0
π a					
π@47+05			5.13	265.00	
to 49+50	196-23	2.44	244	-3°-48'	16.13 249.68
47				48	260.2
48				11.4	253.8
49		2.95	295	-3°-38'	18.7 241.2
π@49+50			5.10	248.78	
to 53+00	175-12	3.49	350	10.21	238.57
50				8.4	240.4
51				10.8	238.0
52				10.7	238.1
to 56+20	195-00	3.89	390	? (+4°-02')	? 249.58
π @53+00			5.29	243.86	
54				3.7	240.2
55				1.4	242.5
56		3.00		+1°-08'+60"	244.6

H.I. from 47+34 264.15
259.58

H.I. of 47+05
243.56

H.I. of 49+50
238.44

H.I. of 53+00
244.00

Stakes marked wrong for this page 100

50+50
8 51
54+00
8+90
57+90

Sta	BS	HI	FS	Dist	Vert L	Elev	
$\pi @ 56+90$	508	254.66				249.58	
to #44	93°-31'	2.96	249	+23'-40"	+109.24	358.84	
44 to 43	22-22						
$\pi @ 56+90$	500	254.58					
to 61+90	193-08	4.99	500	-0°-1'	5.75	248.83	
$\pi @ 61+90$	5.07	253.90				248.63	
No. of Highway	57+94	13-08	395	396	-1°-21'	-9.3	139.5
"	59+40	"	2.50	250	-5°-57'	-25.4	123.4
63+23	198-32	1.32	133	-0°-53'	7.1	146.8	
to 64+25	198-32	2.34	235	-0°-35'	7.49	246.41	
$\pi @ 64+25$	5.09	251.50				246.41	
63+65	18-32	0.61	60	-10-32	-11.0	235.4	
65+15	192-47	0.90	90	-6-38	-10.3	236.1	
66+30	"	2.05	205	-3-40	-13.3	233.1	
66+71	"	2.45	246	-0-40	-2.8	243.6	
to 68+43	192-47	4.17	418	+0°-56'	+6.81	253.22	
$\pi @ 68+43$	4.53	257.75				253.22	
67+51	12-47	0.91	92	-2°-28'	-3.9	249.3	
69+39	196-30	0.95	96		6.0	257.8	
71-12	198-20	2.68	269		3.5	254.3	
to 73+61	200-18	5.17	518	+0°-27'	+0.60	257.31	

Book #	p #
645	12
48	
59.7	
Mon 9/25/21	
4.30	+14°-21' to Sta 57 = 360.
Levels for Check	
HI. off 56+90 = 249.58	
263.72	264.49
59.7	48
TP 261.87	262
267.23	7.67
271.47	34.3
TP 272.09	2.81
TP 260.61	12.12
255.89	5.70
264.15	4.74
259.58	9.31
TP 247.79	12.29
243.56	5.92
238.44	11.04
242.58	1.65
57.54	43.40
62.72	14.14
47.58	14.14

Sta	Az	Rod	H Dist	Vert L	Diff	Elv
π @73+61		473	262.04			257.31
74+25	247-54	0.80	64	-27°-16'	-33.0	243.3
74+74	"	1.14	113	-6°-53'	-13.6	243.7
75+14	"	1.53	153	-7°-06'	-18.9	238.4
75+98	"	2.37	237	-4°-12'	-17.3	240.0
76+48	"	2.87	287	-3°-23'	-16.9	240.4
76+94	"	3.32	332	-1°-23'	-8.0	249.3
to 77+30	247-54	3.68 ✓	369		8.69	253.35
π @77+30		449	257.84			253.38
78+23	258-13	0.93	93	-3°-04'	-5.0	248.4 ✓
79+19	"	1.88	189		7.2	250.6 ✓
to 80+13	258-13	2.82 ✓	283	+0°-52'	0.13	257.71 ✓
π @80+13		513	262.84			257.91
to 81+42	223-38	1.28 ✓	129	+4°-05'	+9.7	266.88 ✓
π @81+42		513	272.01			266.88 ✓
to 83+12	248-12	3.69 ✓	170	-4°-01'	-11.89	254.99
π @83+12		5.27	260.26			-11.89 254.99
83+81	279-02	0.75	69	-18°-08'	-22.5	232.5 ✓
85+32	"	1.20	120	-4°-42'	-9.9	245.1 ✓
85+72	"	2.60	260	-4°-33'	-20.7	234.3 ✓
to 88+43	279-02	5.30 ✓	531	-0°-09'	6.70	253.56

13

75+61	3	69
77+30	2	83
80+13	1	27
81+42	1	42
83+12	5	31
88+43	1	43

Sta	Az	Rod	H. Dist	Vert L	Diff	Elev
K@88+43		457	258.13 257.97			253.56
to 89+13	254-26	0.69	70	-1°-0'	5.78	252.35 252.19
K@89+13		284	256.40 24			253.56
to 90+24	227-13	1.10	111	-1-10	6.37	249.87 250.03
K@90+24		442	254.45 29			250.03 249.87
90+45	237-11	0.21	21	-13°-15'	-4.9	245.1
91+09	"	0.90	85	-14-40	-22.3	247.7
91+75	"	1.52	151	-5°-45'	-15.2	234.8
to 93+00	237-11	2.75	276	-1°-0'	9.25	245.24
K@93+00		444	249.64 48			245.24
to 94+30	231-43	1.29	130	-0°-37'	5.89	243.54
K@94+30		440	248.15 277.99			243.54
95+28	225-09	0.98	98	-5°-10'	-8.9	234.9
95+95	"	1.65	165	-3°-44'	-10.8	233.0
to 98+52	225-09	4.21	422	+0-20	2.10	246.05 245.89
K@98+52		460	250.65 49			246.05 245.89
Backshot	45-09	1.25	19	-8°-08'	-27.5	218.6

14

88+43
70
89+13
1 11

284

225-09
1.50
45-09

90+24
2 76
93 00
1 30
99 1 30
4 22
28 1 52

H.I. of 88+43 253.40 by B.S.

Tues 9/27/21

Sta	Az	Rod	H. Dist	Vert. L	Diff	Elev.
π @98+52	4.6		250	⁶⁵ 49		246.05 245.60
Back Shot	45-09	0.81	80	-6-07	-8.7	137.4
to 100+68	237-21	1.21	118	-11-02	-23.0	223.1
π @100+68		4.27	240.19			236.08 235.02 236.08 235.22
101+87	263-34	1.46	119	-26-08	-58.2	177.9
102+41	"	1.86	183	-8-54	-28.6	207.5
103+19	"	2.50	251	+0-23	+1.7	137.8
103+89	"	3.20	321	+2-20	+13.10	149.2
to 104+28	263-34	3.59	360	+2-30	+15.19	251.77 251.11
π @104+28		4.30	256.07 255.97			"
105+59	238-24	1.30	131	-3-10	-7.2	244.6
to 106+61	238-24	2.32	233	-1-01	8.51	247.40
π @106+61		4.70	252.26 252.10			"
106+91	264-06	0.32	30	-18-45	-10.0	237.6
107+34	"	0.90	78	-26-40	-36.6	211.0
107+48	"	0.94	87	-16-54	-26.5	221.1
107+90	"	1.29	130	-2-30	-5.6	142.0
to 108+60	264-06	1.98	199	+0-7	4.30	247.82
π @108+60		4.56	252.57 252.36			"
to 110+03	235-34	1.42	143	-1-51	9.05	243.2

						98+52
						2 16
						100+68
						3 60
						104+28
						2 33
						106+61
						1 49
						108+60
						1 43
						110+03

BS put up gullies

Sta	Az	Rad	H. Dist	Vert	L. Off	Elev
π @110+03		4.27	247	⁷⁴ 58		¹⁴⁷ 243.27
111+15	216-32	1.11	112		100	237.7
111+76	"	1.72	173		76	240.1
112+12	"	2.08	209		48	241.9
to 112+62	\triangle 216°-32'	2.58 [✓]	259 [✓]	-0°-25'	5.90	¹³⁴ 241.80
π @112+62		4.81	246	⁶⁵ 49		"
* 112+97	198-50	0.29	30		+1.0	247.7
* 114+03	203 0	1.40	141		-6.5	240.2
* 114+88	187-56	3.04	277	+17-55	+89.5	331.3
114+88	214-40	2.25	226		3.6	243.0
to 115+54	\triangle 214°-40'	2.91	292	+0°-42'	1.31	¹³⁴ 245.12
π @115+54		5.02	250	³⁶ 20		"
116+35	217-36	0.82	81	-8°-55'	-12.5	232.8
to 117+00	\triangle 217°-36'	1.45 ^{Level}	146	-2-47	11.23	^{239.13} 238.97
π @117		4.30	243	⁴³ 27		"
to 117+96	\triangle 208°-01'	0.95 ^{Level}	96	-0°-01'	4.40	^{239.03} 238.87
π @117+96		4.55	243	⁵⁸ 42		"
118+87	202-43	0.90	91		8.4	235.2
119+52	"	1.60	161		12.0	231.6
to 120+52	\triangle 202°-43'	2.55 [✓]	256	-0°-10'	5.08	^{238.34} 238.5

110+03
2 59
112+62
2 92
115+54
1 46
117+00
96
117+96
2 56
120+52

N.B.
 about where pipe line would go. Deep Gulch to
 Affects Stas on Profile if used S.R. Box " 115+54 "

330 F/elder #11

Sta	Az	Rad	H. Dist	Vert	Dist	Elev
π @120+52			4.73	243.87		238.80 238.37
to 123+91	$199^{\circ}-52'$	3.38	339	$+0^{\circ}-28'$	2.18	241.05 240.89
π @123+91			4.27	245.16		
to 124+78	$186^{\circ}-18'$	0.86	87	$+2^{\circ}-13'$	0.80	244.36
π @124+78			4.69	249.95		
to 125+20	$154^{\circ}-29'$	0.41	42	$+1^{\circ}-01'$	3.75	245.32
π @125+20			4.50	249.80		
127+31	$122^{\circ}-34'$	"	2.10	211	9.8	240.2
to 128+80	$122^{\circ}-24'$	3.59	360	$-0^{\circ}-10'$	5.72	244.02
π @128+80			5.25	249.33		
131+19	$260^{\circ}-40'$	2.38	239		4.5	245.0
to 132+53	$260^{\circ}-40'$	3.72	373	$+0^{\circ}-26'$	2.41	247.68 246.32
π @132+53			5.12	252.04		
to 134+00	$213^{\circ}-48'$	1.46	147	$+0^{\circ}-53'$	2.94	249.72

120+52
3 39
123+91
0 87
124+78
0 42
125+20
3 60
128+80
3 73
132+53
1 47
134+00

So side Co. Highway } ^(over cut) E quick } sharp turn fill W side / bleed /

In Hwy on line.

(No Side Highway
is same point (diff elev -5±) as #12 Δ of Ramsite #3.

No side Hwy grade

Sta Az Rod H Dist Vert L DA Elev
 T@134 514 254.24 249.26
 249.10

to 136+66 Δ 205°-53' 2.65 ✓ 26' +0-58' 0.78 253.46 ✓

T@136+66 5.28 258.74 ✓ 190

to 141+35 Δ 229°-48' 4.68 469 +0°-51' +6.94 260.42 ✓

T@141+35 508
 134-24 1.21 97 +26-40 +48.98 309.54 ✓
 see below ✓

Az started
 anew from Dam #3 Δ

T@ Δ #13 FS Δ Dam 133-40 Az ?

141+35 }
 with Plumb bob 4.95 265.37 ✓
 133-40 = 1.225 +26-40 49.58 260.42 ✓

to 143+44 Δ 220°-09' 2.08 ✓ 209 -0-41 7.38 257.29 ✓

T@143+44 437 262.36 ✓

142+54 40-09 0.90 90 +3-08 +4.9 ✓ 262.9 ✓

144+94 220-34 1.50 150 -3-55 -10.3 ✓ 247.7 ✓

145+64 7 2.20 220 -3-40 -14.1 ✓ 243.9 ✓

to 147+87 Δ 220-34 4.42 ✓ 443 -1°-29' -11.48 246.51 ✓

Cont. on p 43

So side Hwy Grade

Level Calc's checked
 to 141+35

134	0.0
2	66
136	1.66
4	89
141	3.55
2	09
143	4.4
4	43
147	8.7

"TP" — Tie — "Damm #3"

on Δ Damsite #3 is same Δ as #13 Damsite #3 Δ

Vert L to Fitcher stake 310 Error 0.02 ✓

Az on Δ Damsite #3 133-40 Error 0.44 ✓

Wed 9/28/41

#13 Δ Damsite #3 Compass read N 1° E Var 14-30

Wed Oct 5 21

to Fitcher 310 Δ Dam

Blount Co Road 50' N.

Minus Slas

Survey for Tunnel near St Josephs Hospital

Sta Az Rod H. Dist Vert L Diff Elev

BS H.I. FS

0+00

5.83 295.82

T@

T@ 0+00 518

5.18 290.64

to 5+26 Δ 8°-27' 5.25 526.0 -2°-56' -26.87 263.77

T@ 5+26 4.21

to 8+22 Δ 37°-24' 2.95 296.0 -2°-40' -13.76 250.01

T@ 8-22 398 253.99

198-06 3.35 336.0 -1°-05' -6.3 443.7

188-08 1.87 185.6 -6°-29' -21.1 228.9

102-04 0.91 75.1 -25°-27' -35.7 244.3

44-08 1.38 121.9 -20°-33' -45.7 244.3

26-25 2.54 242.4 -12°-51' -55.3 194.7

29-14 4.12 402.4 -9°-12' -65.2 184.8

again T@ -8+22

393 253.94 250.01

to 6+78 Δ 18°-38' 8.55 852 -3°-50' -57.09 192.92

Continued p 23

"T" Begins

278-22-19

Compass reads N 10° W on 360-0

= 270 to West
BS on 7' Point S.E. Cor 5th + University Ave
= 7' Point S.W. Cor 6th + University Ave
Copper plug in curb N.W. Cor 6th + Univ
7' Point S.W. Cor 6th + Univ Ave = 0+00

5+26

2.96

8+22

8.66

16+88

W side graded road

E side graded road

In a gulch in W 1/2 St Joseph Hospital Lot

" " " " " " " " " " " "

" " " (North and below) " " " " " "

THURS 3/29/21

Tunnel Line South from ^{BS} 6th + Univ ⁴¹ Sta Az Rod H Dist Vert L DA Elev ^{FS}

π@0+00 523 295.87 296.64

23-12 2.81 284.0 -1°-39 -8.1 282.5

to 4+77 ^{180°-17} 4.76 477.0 ^{10°-6'} 4.20 291.67

π@4+77 523 296.90

to 11+98 ^{90°-10-30} 7.20 721.0 ^{0°-56'} -11.75 299.92

π@11+98 525

⁸⁶ to 14+98 ^{133°-48-30} 2.91 288.5 -6°-32 -32.99 286.93

⁸⁶ π@14+98 520 252.13

2-11 4.35 436. 71-40 +12.7 259.6

8-55 3.35 336 365 248.5

355-55 1.08 109 90 243.1

77-20 0.51 51.3 -6°-32 -5.9 41.0

171-05 0.70 69.1 -9°-31 -11.6 235.3

168-49 3.10 309.6 -3°-52 -20.9 286.0

173-30 5.48 547.7 -2°-50 -27.11 219.8

³⁷ to 22+71 ¹⁷⁵⁻³⁸ 7.50 751 -1°-26° -18.78 228.15

+ " T " Begins

So along r/side 6th St

Back shot Head of gulch W of St Jos Hospital Bldg

7' offset City Plug S W cor 6th & Robinson Ave

7' " " " S W cor 8th + Robinson Ave

4+77
7 21
11+98
2 92
14 90
7 51
22+41

E side of road So in gulch to Park

Head of gulch (near 8th + Univ)

Gulch or drainage wash

" "

" "

" "

" "

W 45' of road on hillside

Sta Az Rod H. Dist Vert L Diff Elev

³⁷
~~T@22+77~~ 4.59 232.74 228.15 ✓

43-0 0.49 45.2 -18°-11' -14.8' 213.4

122-50 1.08 106.6 -8-35 -16.1' 212.1

176-15 2.28 227.0 -5-22 -21.3' 206.9

176-0 3.90 389.5 -3-34 -24.3' 203.9

⁷³
 to 30+77 ~~A~~ 181-08 8.35 8.36 -1°-57' -28.42 199.73 ✓

⁷³
~~T@30+77~~ 5.08 204.81

350-0 3.15 316.0 +0-10 +0.9 100.6 ✓

7-35 1.65 166.0 9.0 195.8 ✓

25-45 0.42 42.2 -7°-40' -5.7 194.0 ✓

155-56 1.25 125.5 -3-45 -8.2 191.5 ✓

191-30 2.10 211.0 -2-42 -9.9 189.8 ✓

⁶⁸
 to 32+72 ~~A~~ 193-44 1.94 ✓ 195 -1°-40' -5.68 194.05 ✓

⁶⁸
~~T@32+72~~ ⁵¹⁴ 514

239-20 2.67 257.2 +11-37 +52.87 246.92

³⁶⁺⁸⁶
 to 37+03 ~~A~~ 113-00 4.30 ✓ 417.8 +10-05 +24.19 268.34

☒ Drainage flash
 " " "
 " " "
 " " "

E side road down into Park opp Mairstons Ho

Back shots ☒ drainage
 " " " @ road bridge East
 ☒ drainage
 " "
 " "

E side road

4x4 Post on N Line of Balboa Park

2x2 Stake " " " "

22+41
 8 80
 30+77
 1 95
 32+72
 4 31
 37+03

Sta A2 Rod H. Dist Vert L DH EI

36+86
 T@ 37+03

3.98

to 38+24⁰⁷ 90-40 1.20 ✓ 120.5 +3-33 +7.48 275.82 ✓

T@ 38+24⁰⁷

4.99

89+1-30 11.00 +0°-35' +11.23 287.05

~~~~~ X ~~~~~

|               |         |
|---------------|---------|
| 282.96        | 371.03  |
| 61.27         | 1.21    |
| <u>289.08</u> | 38 + 24 |

to Concrete Mon. on N line Balboa Park near Richmond  
 (Marked 79 + 21.20 BM 282.96 (city datum)  
 289.08 - 459.5  
 END + T Line

~~~~~ X ~~~~~


| Sta | Az | Rod | H. Dist | Vert | ∠ | Diff | El |
|-------------------|------|-------|---------|-------|---|-------|--------|
| 74
K @ 1/17/78 | | 5.00 | 197.92 | | | | 1929.2 |
| ✓ 139-35 | 1.04 | 91.0 | -21-27 | -35.8 | | 157.1 | |
| ✓ 180-03 | 2.30 | 228.8 | -5-40 | -22.7 | | 170.2 | |
| ✓ 186-44 | 4.10 | 411.0 | -1-36 | -71.5 | | 181.4 | |
| ✓ 184-42 | 4.50 | 451.0 | +0-36 | +4.7 | | 197.6 | |
| ✓ 174-27 | 3.10 | 311.0 | +1-43 | +9.30 | | 202.2 | |
| ✓ 167-15 | 3.14 | 312.1 | +5-33 | +30.3 | | 223.2 | |
| ✓ 151-04 | 2.38 | 234 | +8-20 | +34.3 | | 227.2 | |
| ✓ 142-15 | 3.18 | 318 | +5-50 | +32.3 | | 225.2 | |
| ✓ 118-16 | 3.75 | 374 | -4-27 | -29.2 | | 163.7 | |
| ✓ 111-15 | 3.78 | 378 | -4-15 | -28.1 | | 164.8 | |
| ✓ 116-52 | 2.45 | 242 | -8-02 | -34.2 | | 158.7 | |
| ✓ 112-54 | 2.06 | 200 | -10-26 | -36.9 | | 156.0 | |
| ✓ 114-08 | 1.45 | 135 | -15-27 | -32.8 | | 155.1 | |
| ✓ 59-25 | 1.26 | 105 | -22-06 | -44.4 | | 148.5 | |
| ✓ 63-66 | 1.68 | 163 | -10-55 | -31.5 | | 161.4 | |
| ✓ 93-23 | 3.43 | 339 | +6-23 | +38.1 | | 231.0 | |
| ✓ 72-41 | 2.60 | 258 | +7-28 | +33.6 | | 226.5 | |
| ✓ 58-11 | 2.70 | 268 | +6-56 | +32.4 | | 225.3 | |
| ✓ 49-50 | " | 268 | +6-58 | +32.8 | | 225.7 | |
| ✓ 34-50 | 3.50 | 346 | +6-37 | +40.1 | | 233.0 | |
| ✓ 23-12 | 3.45 | 346 | +0-02 | +0.2 | | 193.1 | |
| ✓ 11-0 | 2.90 | 281 | -10-37 | -52.7 | | 140.2 | |
| ✓ 359-0 | 2.55 | 246 | -11-33 | -50.2 | | 142.7 | |
| ✓ 9-26 | 1.48 | 132 | -19-24 | -46.7 | | 146.2 | |

E side Hwy grade opp junction of gulch from SE
 @ Bot drainage from St Jos Hospital

" " " " " " " " " "

On side hill above HOB " " "

" " " " " " " " " "

" " " " " " " " " "

" " " " " " " " " " " " " " " " " " " " " " " "

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drainage from E " " " " " " " " " " " " " " " " " " " " " " " "

W side bot " " " " " " " " " " " " " " " " " " " " " " " "

" " " " " " " " " " " " " " " " " " " " " " " "

drainage from E

Toe of hog back between gulches @ junction of

main drainage @ junct

on ridge to E of " "

" " " " " " " " " " " " " " " " " " " " " " " "

" " " " " " " " " " " " " " " " " " " " " " " "

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" " " " " " " " " " " " " " " " " " " " " " " " " " " " " " " " " " " " "

same as last lower

main drainage

W side " " " " " " " " " " " " " " " " " " " " " " " "

" " " " " " " " " " " " " " " " " " " " " " " "

| Sta | Az | Rod | H. Dist | Vert | ∠ | Diff | Elev |
|----------------------------|--------|------|---------|--------|-------|------|--------|
| ^{ov}
K @ 28+18 | | | 135.20 | | | | 1299.9 |
| | 135-30 | 2.00 | 201 | -2.52 | -100 | | 120.0 |
| | 112-27 | 1.60 | 161 | -1°-56 | -54 | | 124.6 |
| | 72-50 | 1.58 | 159 | -0-24 | -11 | | 128.9 |
| | 75-12 | 2.25 | 221 | +8-28 | +32.0 | | 162.9 |
| | 63-19 | 3.50 | 348 | +5-05 | +30.9 | | 160.9 |
| | 30-29 | 2.85 | 283 | +6-23 | +31.6 | | 161.6 |
| | 27-52 | 4.15 | 394 | +13-08 | +42.0 | | 220 |
| | 39-16 | 4.05 | 382 | +14-06 | +46.0 | | 226.0 |
| | 47-40 | 4.25 | 407 | +12-27 | +89.7 | | 219.7 |

50-30 measured .11.0 11.0

| | | | | | | | |
|--|-------|------|-----|-------|-------|--|-------|
| | 30-33 | 2.45 | 246 | +1-30 | +6.4 | | 136.4 |
| | 52-40 | 2.15 | 216 | -0-36 | -2.2 | | 127.8 |
| | 4-03 | 3.25 | 326 | -2-07 | -12.0 | | 118.0 |

⁶⁶
to 32+76 11-49 4.65 464.4 +3-20 +27.03 157.02

⁶⁶
K @ 32+76 4.30 16130 "

⁸⁹
to 37+82 39-22 5.22 523 +1-5.7 +17.8 174.80

⁸⁹
K @ 37+82 4.41 17919 "

Along top ridge E of drain age

" " " "

" " " " @ cor into gulch #3

Break at ridge Canyon to East

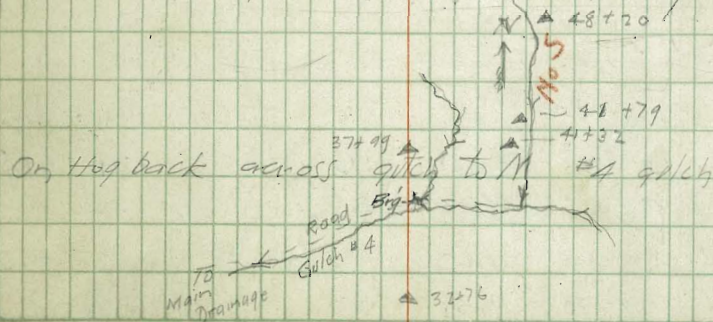
No side of " " "

Triangular Stake marked V.L. 364.

on hill top No side gulch to E

& Bot gulch to E

On Cor of hogback across from Highway



28+10

+66

32+76

523

37+99

| Sta | Az | Rod | H Dist | Vert | L | D.H. | El |
|----------------------|------|------|--------|-------|-------|------|--------|
| $\pi @ 48^{08} + 20$ | | 4.55 | 233.08 | | | | 228.55 |
| ✓ 247-0 | 1.53 | 146 | -13-15 | 34.4 | 192.2 | | |
| ✓ 254-06 | 1.85 | 186 | -0-34 | -1.8 | 226.8 | | |
| ✓ 288-34 | 1.59 | 160 | -0-27 | -1.8 | 227.3 | | |
| ✓ 313-56 | 1.36 | 137 | +0-25 | +1.0 | 229.6 | | |
| ✓ 347-13 | 1.71 | 171 | +2-50 | +8.5 | 237.1 | | |
| ✓ 345-34 | 1.03 | 96 | -16-0 | -27.6 | 201.0 | | |
| ✓ 7-30 | 1.50 | 148 | -7-54 | -20.5 | 208.1 | | |
| ✓ 18-54 | 2.38 | 239 | -2-33 | +0.4 | 218.2 | | |
| ✓ 25-50 | 3.00 | 301 | -0-53 | -4.6 | 224.0 | | |
| ✓ 26-56 | 3.45 | 346 | Seeds | 5.3 | 227.8 | | |

$\pi @ 52^{42} + 55$ 27-06 4.34 ✓ 433.68 +3-00 +2389 252.44 ✓

| | | | | | | | |
|----------------------|------|--------|--------|-------|-------|--|--|
| $\pi @ 52^{42} + 55$ | 4.29 | 256.71 | | | | | |
| 170-30 | 0.55 | 48 | -22-58 | -20.2 | 232.2 | | |
| 83-14 | 0.89 | 88 | -8-52 | -13.7 | 238.7 | | |
| 80-40 | 1.60 | 161 | Seeds | 10.1 | 246.6 | | |
| 80-28 | 2.90 | | +1-09 | +5.8 | 258.2 | | |

$\pi @ 57^{08} + 26$ 81-10 4.70 416.46 +5-39 +46.16 298.60 ✓

$\pi @ 57^{08} + 26$ 4.25 302.83

$\pi @ 57^{08} + 26$ 138-18 0.53 46 -23-12 +9.6 ✓ 279.0

$\pi @ 57^{08} + 26$ 81-10 2.71 264.32 +9-41 +45.10 343.70

Some hill same toe

" " higher up

" " " "

" " " "

☒ gulch #5

" " "

" " "

" " "

" " "

Hub is back in old stake sawbed } No side #228
is also on W side gulch #5 } So " #229

☒ gulch #5

" " "

" " "

" " "

is on W side of gulch #5 P.O.T.

☒ gulch

On hill W side Maryland SA

16+20
+ 35
52+55
+ 71
57+26
+ 72
59+98

| Sta | Az | Rod | H. Dist | Vert L. Diff | Elev |
|---------------------------|--------|-----------|---------|--------------|---------------|
| ^{7V}
π@59+75 | | | 518 | 348.86 | 343.70 |
| ⁴⁰
to 63+66 | 1°-00 | 3.67 | 268 | 1°-06 | 7.08 350.78 |
| ⁴⁰
π@63+66 | 0°-14' | (Az. Tie) | | | |
| ⁴⁰
π@63+66 | | 5.23 | 356.01 | | |
| ⁰⁶
to 68+32 | 310-16 | 4.65 | 466 | 0-29 | 9.16 346.85 |
| ⁰⁶
π@68+32 | | 4.43 | 351.26 | | |
| | 316-50 | 1.35 | 81 | -39-28 | -66.5 280.4 |
| | 317-12 | 2.85 | 213 | -30-33 | -125.3 221.6 |
| | 316-41 | 4.25 | 352 | -24-53 | -162.3 184.70 |

347.00
N side Maryland St fill

591.94
3 68
63+66
4 64
68 32

7' plug @ SW Cor Madison Ave & Maryland St
(Cor. Elev. should be 347.00 + 6.12 = 353.12)

to 7' plug N side @ end of Maryland St

Top steep bluff head of gulch near ^{No.} end of Delaware St

Head of gulch bottom of bluff

of bot. gulch

" " " "

| Sta | Az | Rod | H Dist | | | |
|--------------|------|------|--------|-------|--|--------|
| π @37+89 | | 4.32 | 179.10 | | | 174.80 |
| ✓ 94-20 | 2.67 | 261 | +9-38 | +44.2 | | 219.0 |
| ✓ 77-02 | 3.26 | 315 | +11-08 | +61.9 | | 236.7 |
| ✓ 65-30 | 3.76 | 360 | +11-55 | +76.1 | | 250.9 |
| ✓ 59-32 | 4.30 | 419 | +9-36 | +71.0 | | 245.8 |
| ✓ 55-50 | 4.55 | 441 | +10-06 | +78.6 | | 253.4 |
| ✓ 53-20 | 4.90 | 478 | +9-28 | +79.8 | | 254.6 |
| ✓ 47-53 | 5.15 | 499 | +10-38 | +94.4 | | 269.2 |
| ✓ 46-16 | 5.55 | 543 | +9-06 | +87.2 | | 262.0 |

to 43+85⁸⁹ 41-31 5.55 549.9 +6°-0' +57.83 232.63

| | | | | | | |
|----------------------------|--------|------|-----|----------|-------|-------|
| π @37+99 ⁸⁹ | 37-24 | 4.90 | 491 | +2-42 | +23.1 | 197.9 |
| ✓ | 38-50 | 4.15 | 416 | +1-18 | +9.4 | 184.2 |
| ✓ | 42-58 | 3.38 | 339 | curve 44 | | 174.7 |
| ✓ | 39-45 | 3.18 | 319 | -1-43 | -9.5 | 165.3 |
| ✓ | 48-50 | 2.53 | 254 | -3-30 | -15.2 | 159.6 |
| ✓ | 50-40 | 2.16 | 214 | -6-34 | -24.6 | 150.2 |
| ✓ | 69-20 | 1.84 | 183 | -8-0 | -25.5 | 149.3 |
| ✓ | 134-43 | 1.63 | 159 | -15-26 | -42.1 | 132.7 |
| ✓ | 136-02 | 1.32 | 104 | -26-35 | -53.3 | 121.5 |

| | | | | | | |
|----------------------------|--------|------|-----|--------|-------|--------|
| π @43+85 ⁸⁹ | | 4.80 | | | | 232.63 |
| | 274-35 | 1.25 | 102 | -26-10 | -50.0 | 182.6 |
| | 303-37 | 1.15 | 94 | -26-08 | -46.0 | 186.6 |

Gulch next W. of #5
" 7 2"

30

| Lure up gulch between 37+99 | | Mon Oct 3/21 | |
|------------------------------------------------|-------|--------------|--|
| E.S. on 41+32 | 41+32 | 371.99 | |
| on hillside North of Gulch next W. of Gulch #5 | | 5.56 | |
| " | | 43+55 | |
| " | | | |
| " | | | |
| " | | | |
| " | | | |
| " | | | |
| same hillside lower | | | |
| " " " | | | |
| " " " | | | |
| Q Bot gulch | | | |
| Toe E of Q | | | |
| Q gulch | | | |
| Toe of same hill Low down | | | |
| " " " " break @ Cor | | | |
| Q gulch @ out-let | | | |
| Q bot gulch | | | |
| Q " " @ junct of 3 drains | | | |

| Sta | Az | Rod | H Dist | Vert L | Diff | Elev |
|----------------------------------|----|------|--------|--------|-------|--------|
| π@43+55 ³⁹ | | 4.50 | 237.41 | | | 232.62 |
| ✓ 340-07 | | 1.27 | 124 | -11-06 | -24.2 | 208.4 |
| ✓ 352-24 | | 1.61 | 161 | -3-36 | -9.9 | 222.7 |
| ✓ 359-07 | | 2.20 | 221 | +2-08 | +8.2 | 240.8 |
| ✓ 3-23 | | 2.70 | 269 | +5-44 | +26.9 | 259.5 |
| ✓ 5-54 | | 3.25 | 315 | +8-24 | +47.2 | 279.8 |
| ✓ 7-10 | | 3.61 | 354 | +10-0 | +62.5 | 295.1 |
| ✓ 55-15 | | 3.85 | 375 | +9-40 | +64.0 | 296.6 |
| 54-38 | | 3.03 | 299 | +7-12 | +38.0 | 270.6 |
| 59-52 | | 2.15 | 214 | +6-06 | +22.8 | 255.4 |
| 55-30 | | 1.45 | 146 | +2-02 | +5.2 | 237.8 |
| 54-15 | | 1.17 | 118 | | 65 | 230.9 |
| 9-28 | | 0.71 | 65 | -18-06 | -21.3 | 211.3 |

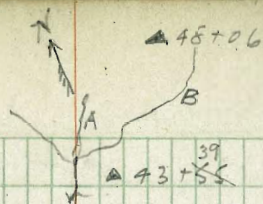
47+71
to ~~48+06~~ ⁴⁷⁺⁷¹ 452-49 4.50 432.4 +11-43 +89.68 322.31

47+71
π@~~48+06~~ 4.50

50+74
to ~~51+10~~ ⁵⁰⁺⁷⁴ 11-41 3.03 302.88 +30-28' +18.36 240.67

5.14

50+74
π@~~51+10~~ ⁵⁰⁺⁷⁴ 15 14-45 1.40 141.0 +0-26' +08 341.73



31

☒ of draw in ☒ of head of gulch or "A"

| | | |
|---|--|---|
| ✓ | | A |
| ✓ | | " |
| ✓ | | " |
| ✓ | | " |
| ✓ | | " |
| ✓ | | " |

43+55
4 54
48+06
3 04
51+10
1 - 41
52+51

☒ of " " " " " B

| | | |
|---|--|---|
| ✓ | | " |
| ✓ | | " |
| ✓ | | " |
| ✓ | | " |
| ✓ | | " |
| ✓ | | " |

On top @ head of gulch B

☒ Madison Ave @ Intersect with E Prop Line Rhode Island Ave

15
 T @ 52+5X 510 341.73

✓
 50-16 4.10 342.73

54+88
 to 55+24 41-47 2.72 273 -0°-29' 729 339.54
 +42

54+88
 T @ 55+24 T'

page #29
 to 68+32 T 83-00 4.92 493 +0°-47' +675 346.29

54+88
 T @ 55+24 31-57 2.75 200 -31°-36' -123 216.5
 " 42-17 2.40 167 -33°-52' -112 227.5
 " 20-23 4.00 315 -27°-42' -165.1 174.4

06
 T @ 68+32
 40
 to 63+66 130-17 OK-Az

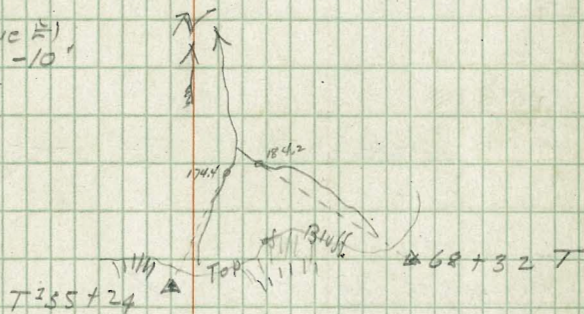
BM on Mon @ Sry Cor Madison + Rhode Is Ave's
 shot E on & Paving Madison Ave

@ Head (on top of bluff) deep gulch No of Madison Ave
 52+51
 273
 55+24

Tie to T' from T'' Error Level 0.5
 Az 0-01'

Bot of drain (True E)
 15'-10"

310-16
 180
 130-16



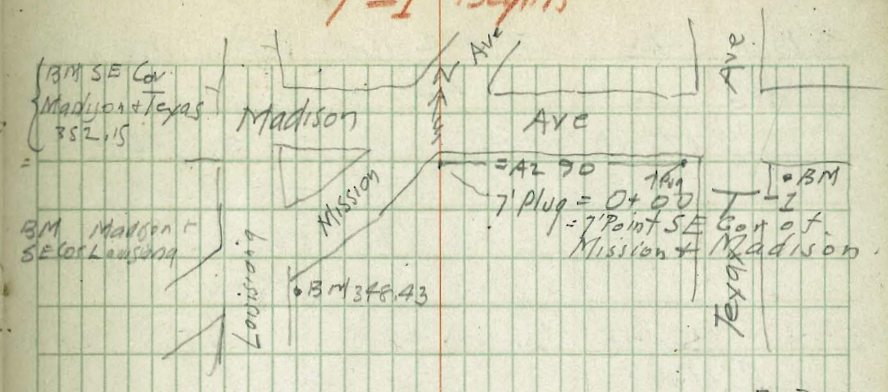
Tunnel Line - Sandrock Grade to Balboa Park.
North from Madison Ave.

| Sta | Az | Rod | H. Dist | Vert L | |
|---------------------------|--------|------|---------|---------|---------------|
| Az from E St Line 7' plug | | | 2.96 | 355.11 | 352.15 |
| K@ 0+00 | 523 | | | | 5.23 342.86 |
| | | | | | 6.71 348.40 |
| to 3+30 | 38-58 | 3.29 | 330 | 40°-29' | 265 352.46 |
| K@ 3+30 | | 4.36 | | | 356.82 |
| to 6+17 | 0-17° | 2.86 | 287 | -1°-54' | -9.5 342.96 |
| K@ 6+17 | | 4.26 | | | |
| | 66-45 | 1.10 | 91 | -25-10 | -42.3 300.7 |
| | 21-0 | 1.72 | 153 | -19-44 | -55.0 288.0 |
| to 11+68 | 356-09 | 5.50 | 538.64 | -8-37 | -81.63 261.33 |
| K@ 11+68 | | 4.51 | | | 265.84 |
| | 162-40 | 1.72 | 173 | | 7.3 258.5 |
| | 146-0 | 0.59 | 56 | -16-12 | -16.0 245.3 |
| | 9-27 | 2.00 | 193 | -11-32 | -39.4 221.9 |
| to 16+86 | 4-18 | 5.17 | 511.48 | -6°-26' | -57.65 203.63 |

352.15
246

T-1 Begins

33



13 m bank above road down gulch 150' + 9 boxes Ry Bldg

Bot Gulch above El Ry Bridge
" " " " " "

East edge of Road

Bot gulch
" " " "

3+30
287

6+17
551

11+68

11+68
515
16+86

| Sta | Az | Rod | H. Dist | Vert | L | Diff | Elev. |
|-------------|------|------|---------|-------|---|------|--------|
| $\pi@16+86$ | | 4.18 | 207.86 | | | | 203.68 |
| 177-10 | 0.96 | 96 | -3-36 | -60 | | | 197.7 |
| 168-20 | 0.39 | 36 | -16-02 | -10.7 | | | 193.0 |
| 68-40 | 0.42 | 35 | -25-26 | -16.7 | | | 187.0 |

End this Line North

same Line π again on 0+00 South

| | | | | | | | |
|------------|------|------|--------|--|--|--|--------|
| $\pi@0+00$ | 5.23 | 6.70 | 355.13 | | | | 348.43 |
|------------|------|------|--------|--|--|--|--------|

5.23 349.90

| | | | | | | | |
|----|--------|------|-----|-------|-------|--|--------|
| to | 242-58 | 5.92 | 593 | -0-39 | -6.73 | | 343.17 |
|----|--------|------|-----|-------|-------|--|--------|

| | | | | | | | |
|---------|-----------------|------|-----|-------|-------|--|--------|
| to 5+55 | $\Delta 236-35$ | 5.54 | 555 | -0-38 | -6.16 | | 343.74 |
|---------|-----------------|------|-----|-------|-------|--|--------|

| | | | | | | | |
|------------|--|------|--------|--|--|--|---|
| $\pi@5+55$ | | 5.29 | 349.03 | | | | " |
|------------|--|------|--------|--|--|--|---|

| | | | | | | | |
|----------|-----------------|------|-----|---------|--------|--|--------|
| to 10+56 | $\Delta 241-28$ | 5.00 | 501 | -1°-31' | -13.25 | | 330.49 |
|----------|-----------------|------|-----|---------|--------|--|--------|

| | | | | | | | |
|-------------|--|------|--------|--|--|--|---|
| $\pi@10+56$ | | 5.03 | 335.52 | | | | " |
|-------------|--|------|--------|--|--|--|---|

| | | | | | | | |
|----|--------|------|-----|--|--|--|--|
| to | 182-03 | 1.34 | 135 | | | | |
|----|--------|------|-----|--|--|--|--|

| | | | | | | | |
|----------|-----------------|------|-----|---------|-------|--|-------|
| to 18+71 | $\Delta 180-23$ | 8.14 | 815 | -0°-27' | -6.46 | | 340.9 |
|----------|-----------------|------|-----|---------|-------|--|-------|

| | | | | | | | |
|-------------|--|------|--|--|--|--|--|
| $\pi@18+71$ | | 5.17 | | | | | |
|-------------|--|------|--|--|--|--|--|

| | | | | | | | |
|----------|----------------|------|-----|---------|--------|--|--------|
| to 24+97 | $\Delta 180-0$ | 6.25 | 626 | -1°-10' | -12.78 | | 311.31 |
|----------|----------------|------|-----|---------|--------|--|--------|

| | | | | | | | |
|--|-------|------|--|--|--|--|--|
| | 10-56 | 8.15 | | | | | |
| | 18+71 | 6.26 | | | | | |
| | 24+97 | | | | | | |

from Madison **T+1**
 $0+00 = 7'$ Tie Point Plug SE Cor Mission + Madison
 S wly along So side Mission Ave

$0+00$
 7' Tie Point NW Cor Mission + Mississippi
 7' Tie Point SE Cor Mission + Mississippi

@ SW Cor + Mission + Alabama

(7' Tie Point) SW Cor Alabama + Monroe

@ SW Cor Alabama + Meade (no 7' Point + incl)

@ NW Cor " " El Cajon } 7' E of W prop line
 = 7' E of W. Line of Alabama + 55' N of N Curve of El Cajon.

| Sta | Az | Rod | H Dist | Vert | L | Diff | Elev |
|----------|--------|------|--------|---------|---------------------|--------|------|
| π@24197 | | | 4.18 | 315.45 | | 311.37 | |
| | | | | | 2.61 | 312.98 | |
| to 30+39 | 180-03 | 5.41 | 542 | -1°34' | -14.80 | 296.51 | |
| π@30+39 | | | 5.18 | 301.69 | | " | |
| to 36+54 | 180-02 | 6.14 | 615 | -0°6' | 6.20 | 295.49 | |
| π@36+54 | | | 5.13 | 300.69 | | " | |
| to 43+35 | 180-03 | 6.80 | 681 | -0°22' | 9.13 | 291.49 | |
| π@43+35 | | | | | | | |
| | 180-04 | | | | | | |
| | | | 5.24 | 297.47 | | 292.23 | |
| π@43+35 | | | | | | | |
| to 46+61 | 257-00 | 3.25 | 324.4 | -4°-02' | -2.90 | 269.33 | |
| π@46+61 | | | 5.18 | 274.51 | | | |
| to 49+57 | 180-05 | 2.95 | 296 | +0°-11' | 4.14 ⁺⁹⁵ | 270.28 | |

5.24
 42.23
 297.47
 5.15
 24+97
 5.42
 30.39
 6.15
 7' point SW Cor Alabama + Howard - No Plug in. 36+54
 6.81
 43.35
 6+79
 50+14

312.69 BM NE Cor Alabama + El Cajon
 7' point SW Cor Alabama + Howard - No Plug in. 36+54

7' point NW Cor Alabama + Polk

Alabama + Lincoln 7' point found

5.74 277.35 277.61
 7' point Alabama + Univ Ave 176 275.59

BM Alabama + Lincoln Curb NW Cor.

FS Alabama + Univ Ave Az of 180-04 43+35
 3-20
 46+61
 2.96
 49+57

Approx SE Prop Line Cor Florida + Lincoln

270.37

| Sta | Az | Rod | H. Dist | Vert L | Diff | Fl |
|----------|--------|-------------------|---------|--------|--------|--------|
| π@49+57 | | | 4.71 | 27508 | | 270.37 |
| | 145-12 | 0.38 | 36 | -17-48 | -11.5 | 258.9 |
| | 136-07 | 1.70 | 169 | -4-53 | -14.4 | 256.0 |
| | 137-0 | 2.72 | 272 | -3-20 | -15.9 | 254.5 |
| to 53+08 | 151-06 | 3.50 ^v | 351 | +1-42 | +10.43 | 280.80 |
| π@53+08 | | | 484 | 28564 | | " |
| | 352-48 | 0.63 | 44 | -34-40 | -29.5 | 251.3 |
| | 167-26 | 0.75 | 76 | | 7.21 | 278.7 |
| | | 2.22 | 223 | -2-09 | -8.37 | 272.43 |
| to 60+17 | 168-40 | 7.08 | 709 | -2-48 | -34.59 | 246.21 |
| π@60+17 | | | 450 | 25071 | | |
| | | 5.85 | 586 | +0-39 | +5.9 | 252.1 |
| | 351-29 | 3.50 | 351 | | 6.3 | 246.4 |
| | 353-25 | 1.25 | 126 | | 11.2 | 239.5 |
| | 338-35 | 0.26 | 24 | -20-44 | -9.0 | 237.2 |
| | 222-0 | 1.50 | 150 | -4-32 | -11.9 | 234.3 |
| | 202-10 | 4.20 | 421 | -2-18 | -16.8 | 229.4 |
| to 67+53 | 194-26 | 7.35 | 736 | -0-22 | 9.08 | 241.63 |
| π@67+53 | | | 449 | 24612 | | " |
| | 5-55 | 2.21 | 220 | -3-34 | -13.8 | 227.8 |

Outlet 36" Conc pipe bottom invert
 On surface in bottom wash 53+08
 " " " " " 7 09
 " " " " " 60+17
 " " " " " 7-36
 On Prop Line + No side fill Univ Ave 67-53
 * Tues 10/4/21

No side fill
 Invert 36" Culv Conc Pipe under Univ Ave
 So side Top fill Univ Ave over & wash
 On BM NE Cor Univ. + Algham Corner Mon
 271.61

So side toe Univ Ave fill in invert of Culvert 36"
 & of wash
 " " "
 " " "
 " " "
 " " "

| Sta | Az | Rod | H. Dist | Vert L | Dist | EI |
|---------|--------|------|---------|---------|------|--------|
| X@67+53 | | | 246.12 | | | 241.63 |
| | 26.55 | 1.55 | 154 | -6°-05' | 165 | 225.1 |
| | 137.50 | 0.86 | 83 | -13-14 | 194 | 222.2 |
| | 150.47 | 1.70 | 168 | -7-26 | 219 | 219.7 |
| | 185.54 | 2.95 | 294 | -5°-0' | 257 | 215.9 |
| | 193-14 | 5.50 | 550 | -2°-51' | 277 | 213.9 |
| | 191-10 | 7.38 | 738 | -2-37 | 337 | 207.9 |

576+64 190-47 9.10 911 -2-24 38.08 203.55

X@76+64

5.31 208.86

| | | | | | | |
|--|--------|------|-----|---------|----|-------|
| | 180.06 | 4.00 | 401 | -0°-32' | 89 | 200.0 |
| | 181-02 | 3.35 | 336 | | 97 | 199.2 |
| | 181-33 | 1.97 | 198 | | 79 | 201.0 |

Ends @ No side

67153

9+11

76+64

☉ of Wash

" " "

" " "

" " "

36" Culvert } Top Concr. top E side Florida St

☉ E gutter = ☉ Wash Guts wrecked by wash

13' part = 13' W + 13 S. of intersect of St Lines

Florida St @ Myrtle Ave Old RY Hvb out (spike but no

End. is at No Line + Balboa Park

13' line W of ☉ Florida St V for Az FS @ U past 13 Lines (AHHOY Both out)

Large gutter

" " "

of Balboa Park + Florida St

East San Diego Tunnel Line "T-2" ^{BS H.I. F.S. I.}

Sta Az Rod H. Dist Vert L Diff El

4.87 362.99 358.12

0+00 ⁵¹⁵

to 7+11 ³⁶⁰⁻⁰ 7.10 711 -0°-8' 6.98 356.21

κ@7+11 5.15 361.16 "

to 11+52 ³⁵⁴⁻⁴⁰ 4.40 441 +0°-17' 2.93 358.23

κ@11+52 5.01 363.24 "

to 12+89 ³⁵⁶⁻¹¹ 1.36 137 -1°-54' 2.55 353.63

κ@12+89 4.46 358.15 "

³⁸ to 14+76 ^{7°-32'} 1.56 149 -13°-06' -34.67 319.02

5.05 324.07

³⁸ κ@14+76

²¹⁺⁹³ to 22+03 ³⁵⁻⁰³ 7.56 755 -2°-53' -37.99 281.03

²¹⁺⁹³ κ@22+03 4.45 285.48

✓ 235-24 1.32 132 -4-32 -10.5 270.5

✓ 12-05 0.99 97 -10-35 -18.0 263.0

✓ 34-45 3.12 311 -5-01 -27.3 253.7

T-2 Begins

38

352.00

Tues 10/1/21

0+00: Point on S line El Cajon and 10' W. of C of Fairmount Ave

Brass Plug in Carb SW Cor El Cajon + Fairmount

(Az 360-0 Compass, reads N 6-30 W with Ver @ 140 30 E

F.S. to 10' W of C of Fairmount Ave @ Olive Ave

7+11

4 41

11+52

1 37

12+89

1+52

14+76

7+57

22+03

In field N. of Olive Ave

" " " " above road grade

On r/ edge graded road

☒ Gulch wash

|| " "

" " "

| Sta | Az | Rod | H. Dist | Vert L | DA | El |
|------------------------------|--------|------|---------|--------|--------|--------|
| ²¹⁺⁹³
K@22+03 | 445 | | 285.48 | | | 251.03 |
| | 35-16 | 445 | 444 | -4-06 | -31.9 | 249.1 |
| ⁵⁰
to 29+62 | 43-05 | 7.58 | 7.57 | -2-34 | -33.9 | 247.11 |
| ⁵⁰
K@29+62 | | 453 | 251.64 | | | |
| | 237-04 | 1.50 | 151 | -1-43 | -4.5 | 242.6 |
| | 320-30 | 0.52 | 51 | -11-36 | -10.4 | 236.7 |
| | 14-47 | 1.28 | 127 | -7-0 | -15.6 | 231.5 |
| | 33-22 | 2.35 | 234 | -4-59 | -20.4 | 226.7 |
| ³⁴⁺⁹⁶
to 35+08 | 22-11 | 5.45 | 546 | -1-42 | -16.2 | 230.89 |
| ³⁴⁺⁹⁶
K@35+08 | | 429 | 235.18 | | | |
| | 201-15 | 1.15 | 115 | -5-09 | -10.4 | 220.5 |
| | 266-27 | 0.54 | 51 | -15-50 | -14.5 | 216.4 |
| | 331-17 | 1.22 | 120 | -8-26 | -17.9 | 213.0 |
| | 342-24 | 3.90 | 389 | -3-30 | -23.8 | 207.1 |
| ²⁷
to 39+34 | 355-39 | 4.25 | 426 | -1-20 | -9.93 | 220.96 |
| ²⁷
K@39+34 | | 4.38 | 225.34 | | | |
| | 258-37 | 0.82 | 80 | -10-37 | -15.0 | 206.0 |
| | 354-47 | 2.18 | 218 | -5-48 | -22.0 | 199.0 |
| | 0-48 | 4.10 | 409 | -3-58 | -28.35 | 192.61 |

End of T-2 North

☒ gulch wash

☒ edge graded road

☒ gulch wash

" " "

" " "

" " "

☒ edge graded road

☒ wash

" " "

" " "

" " "

☒ edge graded road

☒ wash

" "

| |
|-------|
| 22+03 |
| 7 59 |
| 29+62 |
| 5 46 |
| 35+08 |
| 4 20 |
| 39+34 |

Sta Az Rod H. Dist Vert L Diff E

515
0+00 4.83 362.95 358.12

to 7+01 \triangle 180-06 7.00 701 +0°-18' +3.65 361.77

π @7+01 515 366.92

to 13+82 \triangle 269-35 6.80 681 +0°-12' 2.90 364.52

π @13+82 511 369.63

to 22+08 \triangle 269-55 8.25 826 +0°-07' 3.33 366.30

512 371.42 "

to 28+90 \triangle 269-56 6.81 682 +0°-2' 4.65 366.77

π @28+90 501 371.78 "

to 33+46 \triangle 269-57 4.55 456 +0°-5' 4.32 367.46

π @33+46 524 372.70 "

to 39+61 \triangle 180-02 6.14 615 -0°-34' -6.09 361.32

T+2

East San Diego

Wed Oct 5/21

Same 0+00 as on p 38 same B.M.

Point 10' W of E of Fairmeant Ave + 6.5' North of S Line Orange Ave

S. Line of Orange Ave + 10' W. of E. Line Van Dyke Ave.

S.W. Cor Stockton + Orange Aves

S.E. Cor Orange + Central Aves

S. Line Orange Ave and 5' East of West Line of Sisson Ave

Point 1.67' S. of S. Line of Anna St and 5' E. of W. Line of Sisson Ave

7+01
6.81
13+82
6.20
22+08
6.82
28+90
4.30
33+46
6.15
39+61

| Sta | Az | Rad | H. Dist | Vert L | Diff | EI |
|----------|--------|------|---------|---------|--------|--------|
| π@39+61 | | | 517 | 366.54 | | 261.37 |
| to 45+60 | 180-22 | 5.98 | 599 | -0°-53' | -9.22 | 352.15 |
| π@45+60 | | | 508 | 357.23 | | |
| to 53+21 | 179-59 | 7.60 | 761 | -0°-32' | -7.08 | 345.07 |
| π@53+21 | | | 515 | 350.22 | | |
| to 60+01 | 180-0 | 6.79 | 680 | -1°-05' | -12.86 | 332.21 |
| π@60+01 | | | 517 | 327.38 | | |
| | | | NEW | H.I. | 4.70 | 332.68 |
| | | | 4.70 | 341.34 | | 336.64 |
| to 62+98 | 236-57 | 2.96 | 297 | -2°-03' | -10.62 | 326.02 |
| π@62+98 | | | 4.47 | 330.49 | | |
| to 65+73 | 212-58 | 2.85 | 275.0 | -11-26 | -55.58 | 270.44 |
| π@65+73 | | | 4.50 | 274.94 | | |
| | 247-35 | 1.11 | 112 | | 10.2 | 264.7 |
| | 208-15 | 2.45 | 246 | -2-40 | -11.4 | 259.0 |
| to 70+48 | 194-32 | 4.74 | 475 | -1°-54' | -15.72 | 254.72 |

29+61
5 97
45+60
7 41
53+21

Point on N Line University Ave and 167 E. of W. Line of Sisson Ave.

53+21
6 80
60+01
2 47
Point on S Line of Klauber Ave and 167 E. of W. Line of Sisson Ave.

62+98
2 86
+
Point on S Line of Castel Ave and 167 E. of W. Line of Sisson Ave.

386.64 Brass Peg at N.W. Cor Sisson + Castle
Castle S. S. Line

@ top of ridge

@ junct of gullies

62+98
65+73
65+73
2 75
70+48

W side bot @ Toe of ridge to W
main wash below junct

Sta Az Rod H. Dist Vert L DB Elev

π@ 70+48

498 25970

✓ 317-30 0.88 89 4.5 255.2
 ✓ 218-10 2.14 215 -1-55 -7.2 247.5
 ✓ 205-22 3.35 336 -1-37 -9.5 245.2
 ✓ 207-34 5.60 561 -1-37 -15.8 238.9

⊕ wash

" "

" "

" " 3' Lower 15' Left

70+48
 6 71
 77+19
 7 99
 85 18

to 77+19 208-35 6.70 671 -1-36 -18.7 236.00

π@ 77+19

494 240.94

✓ 176-0 0.29 30 8.3 232.6
 ✓ 198-30 1.75 176 -1°-58 -6.0 230.0
 ✓ 218-05 4.00 401 -2°-0 -14.0 222.0

⊕ wash

" "

" " Xing Series Line down ⊕ gulch

to 85+18 217-26 7.98 799 -1°-31' -21.4 248.6

π@ 85+18

4.43 219 29

✓ 8-10 0.92 93 5.3 214.0
 ✓ 224-40 0.60 61 8.5 210.8
 ✓ 194-45 1.34 124 -2-48 -6.5 208.4
 ✓ 197-33 2.38 239 -2-19 -9.6 205.3
 197-39 4.72 473 -1-40 -13.6 201.1

⊕ wash

"

"

"

"

" Jct. with canyon from N.W. near City Boundary

End South T+2

Contd from p 18 BS H-1. P.S

Sta A2 Rod H. Dist Vert \angle Diff Elev
 T @ 147+87 4.28 250.79 246.51

to 148+90A 200-38 1.02 103 +1°-07' 2.21 248.58

T @ 148+90 4.35 252.93

149+20 221-57 0.33 30 -20-25 -11.2 237.4

149+59 " 0.78 69 -21-33 -17.0 221.6

149+71 " 0.86 81 -15-30 -20.0 228.6

150+31 " 1.40 141 -10-10' -29 248.7

to 151+25A 221-57 2.34 235 +0°-03' 4.00 248.93

T @ 151+25 4.74 253.67

152+96 232-29 1.73 171 -8-12 -24.4 245

153+16 " 1.90 191 \angle 45 249.2

153+74 " 2.48 249 11.7 242.0

154+01 " 2.75 276 +0-52' 44.2 253.1

to 154+34A 232-29 3.08 309 +0-47' 44.23 253.16

483 457.99

to 155+37A 217-26 1.02 103 -1°-05' 6.77 251.22

T @ 155+37 4.98 256.20

156+23 197-05 0.85 86 9.0 247.2

157+55 " 2.18 218 -4-36 -17.5 233.7

158+33 " 2.96 296 -2-44 -14.1 237.1

"IP" Contd from p 18 43

147+87
 1 03
 148+90
 2 35
 5.1 + 25
 3 09
 54 + 34
 1 03
 55 + 37

foot of Vert Cliff

Just out of mouth of Mission Gorge So Side

Thurs Oct 6/21

| Sta | Az | Rod | H. Dist | Vert | ∠ | Diff | Elev |
|-----------|--------|------|---------|---------|--------|------|--------|
| π@155+37 | 496 | | 256.20 | | | | 251.22 |
| 153+96 | 197-05 | 4.60 | 459 | -3-34 | -28.6 | | 222.6 |
| to 168+33 | 197-05 | 6.95 | 696 | -2°-14' | -27.08 | | 224.14 |
| π@168+33 | | 451 | 228.65 | | | | |
| 165+67 | 198-40 | 3.35 | 334 | -5-04 | -29.6 | | 194.5 |
| to 169+62 | 198-40 | 7.28 | 729 | -0-12' | 7.00 | | 221.65 |
| π@169+62 | | 443 | 226.08 | | | | |
| 166+76 | 18-40 | 2.95 | 286 | -10-33 | -53.3 | | 168.4 |
| to 172+24 | 210-56 | 4.61 | 462 | +0°-12' | 2.48 | | 223.60 |
| π@172+24 | | 441 | 228.01 | | | | |
| 175+27 | 201-31 | 1.02 | 103 | | 13.4 | | 214.6 |
| 179+31 | " | 5.20 | 513 | -6°-05' | -54.8 | | 168.8 |
| to 183+44 | 201-31 | 9.19 | 920 | -2°-07' | -33.95 | | 189.65 |
| π@183+44 | | 450 | 194.15 | | | | |
| 181+35 | 201-31 | 2.23 | 209 | -15°-0' | -56.2 | | 132.5 |
| 182+11 | " | 1.52 | 133 | -21-25 | 52.1 | | 137.6 |

155-37
29.07
183.44

155+37

6.96

160+33

7.29

167+62

4.62

174+24

9.20

183+44

Back shot & gulch below Auxiliary Spillway Dam #3

On hillside So. & leaving thence Co. Road of Gorge

P.O.T.

& of wash back shot
Toe ridge on bottom gulch

| Sta | Az | Rod | H. Dist | Vert | L | D.A | L) |
|-----------|--------|------|---------|--------|--------|--------|----|
| K@183+44 | | | 194.15 | | | 189.65 | |
| 184+41 | 201-31 | 1.02 | 97 | -14-15 | -24.6 | 165.1 | |
| 185+42 | " | 2.02 | 198 | +9-28 | +33.0 | 222.7 | |
| to 186+04 | 201-31 | 2.67 | 260.49 | +9-39 | +44.29 | 233.94 | |
| K@186+04 | | 4.53 | 238.47 | | | | |
| 187+74 | 207-13 | 1.70 | 170 | -3-08 | -9.3 | 224.6 | |
| to 190+35 | 207-13 | 4.30 | 421 | -1-43 | -12.91 | 221.03 | |
| K@190+35 | | 4.40 | 225.43 | | | | |
| 192+21 | 245-19 | 2.25 | 224 | -5-30 | -21.6 | 199.4 | |
| 192+21 | 251-24 | 1.90 | 186 | -9-38 | -31.5 | 189.5 | |
| 192+99 | " | 2.65 | 264 | -4-06 | -19.0 | 202.0 | |
| to 194+10 | " | 3.75 | 375 | -2-33 | -16.7 | 204.3 | |
| to 195+38 | 251-24 | 5.02 | 503 | -2-36 | -22.78 | 198.25 | |
| K@195+38 | | 4.56 | 202.81 | | | | |
| 196+37 | 258-10 | 1.20 | 99 | -25-40 | -47.2 | 151.0 | |
| 197+53 | " | 2.15 | 215 | -2-45 | -10.3 | 188.0 | |
| 198+04 | " | 2.65 | 266 | -0-25 | -1.9 | 196.4 | |
| 199+94 | " | 4.55 | 456 | +1-25 | +11.2 | 208.5 | |
| to 202+61 | 258-10 | 7.22 | 723 | +7-05 | +26.25 | 224.50 | |

Bot gulch

On hill side

Hub at Fence Cor (Fence runs North + West from Hub)

Bot gulch

| | |
|--------|----|
| 183+44 | |
| 2 | 80 |
| 186 | 04 |
| 4 | 31 |
| 190 | 35 |
| 5 | 03 |
| 195 | 38 |
| 7 | 23 |
| 202 | 61 |

Sta A2 Rod H. Dist Vert \angle Off El
 K@202+61 457 229.07 224.50

t@204+80 \blacktriangle 254-33 2.18 219 -2-58 -11.31 213.19

K@204+80 444 217.63

27-27 2.82 2.83 +2-10' +10.7 223.9

206+92 243-38 2.45 212 -22-0 -85.4 127.8

207+44 " 2.95 264 -18-55 -91.0 122.2

209+12 " 4.35 432 -5-58 -42.6 170.6

210+01 " 5.20 521 0-26' -40 209.2

t@211+51 \blacktriangle 243-38 6.70 671 +1-27 +16.98 230.17

K@211+51 454 234.71

212+32 247-28 0.13 14 16 233.1

214+25 " 2.73 274 88 225.9

216+22 " 4.70 471 14.7 220.0

t@219+42 \blacktriangle 247-28 7.90 791 -0-42' -9.65 220.52

K@219+42 437 224.89

217+38 67-29 2.04 204 -2-50 -10.1 210.4

218+23 " 1.19 119 -2-30 -5.2 215.3

211+81 234-31 2.38 239 71 217.8

t@222+68 \blacktriangle 234-31 3.25 326 -0-53' 9.25 215.64

202+61
 2.19
 204+80
 6.71
 211+51
 7.91
 219+42
 3.26
 222+68

W fence from hub @ Cor p 45

Bot gulch E side @ toe

" " " " " "

on Hill

" "

N+S Fence

Back shot ground

" " N+S fence

N+S fence

| Sta | Az | Rod | H | Dst | Vert | L | D# | El |
|---------------|--------|------|------|---------|-------|-----|----|--------|
| π @222+68 | | | 4.54 | 220 | 18 | | | 215.69 |
| | 164-48 | 3.05 | 204 | +4-52 | +25.8 | | | 241.4 |
| 224+74 | 214-04 | 2.05 | 206 | | | 68 | | 213.4 |
| 226+32 | " | 3.63 | 364 | | | 4.6 | | 215.6 |
| τ 229+89 | 214-04 | 7.20 | 721 | +0°-31' | +6.49 | | | 222.13 |
| π @229+89 | | 5.10 | 227 | | | | | 227.23 |
| τ 234+98 | 196-40 | 5.08 | 509 | +0°-5' | +4.03 | | | 223.20 |
| π @234+98 | | 5.0 | 228 | | | | | 228.20 |
| | 169-22 | 4.93 | 494 | | | | | |
| 236+93 | 177-40 | 1.95 | 195 | -4-07 | -4.0 | | | 209.2 |
| 237+84 | " | 2.85 | 286 | -2-05 | -10.1 | | | 213.1 |
| 239+09 | " | 4.10 | 411 | -2-17 | -16.4 | | | 206.8 |
| τ 241+23 | 177-40 | 6.24 | 625 | -0°-7' | +6.37 | | | 221.93 |
| π @241+23 | | 4.98 | 226 | | | | | 226.81 |
| | 203-89 | 5.80 | 581 | | | | | |
| | 201-53 | 5.70 | 571 | | | | | |
| 242+99 | 184+17 | 1.75 | 176 | | | 3.2 | | 223.6 |
| 246+04 | " | 4.80 | 481 | | | 6.0 | | 220.8 |
| τ 248+74 | 184+17 | 7.50 | 751 | +0°-39' | +8.52 | | | 230.35 |

Hub @ fence Cor E + N and N

E + N fence

fence Cor N + S + N

ground on line

Fence Cor #1 sketch

" " #2

222+68

7 21

229+89

5 09

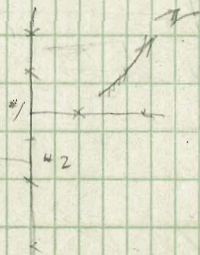
234+98

6 25

241+23

7 51

✓ 248+74



B.S. H.I. F.S.

| Sta | Az | Rod | H. Dist | Vert | L. Diff | EI |
|----------------|--------|------|---------|---------|---------|--------|
| $\pi @ 245+74$ | | | 4.93 | 235.28 | | 230.35 |
| 250+75 | 201-48 | 200 | 201 | | 76 | 222.7 |
| 253+30 | 1 | 4.55 | 456 | -1°-20' | -10.6 | 219.8 |
| $\pi @ 255+48$ | 201-48 | 6.73 | 674 | -0°-23' | 9.25 | 226.03 |

| | | | | | | |
|----------------|--------|------|------|--------|------|--------|
| $\pi @ 255+48$ | | | 4.95 | 230.88 | | |
| 257+14 | 207-27 | 1.65 | 166 | | 5.40 | 225.5 |
| 258+69 | " | 3.20 | 321 | | 12.4 | 218.5 |
| 259+44 | " | 3.95 | 396 | | 5.1 | 225.8 |
| $\pi @ 260+46$ | 207-27 | 4.97 | 498 | 0 | 4.55 | 226.33 |

| | | | | | | |
|----------------|--------|------|------|---------|-------|--------|
| $\pi @ 260+46$ | | | 4.85 | 231.18 | | |
| 261+43 | 204-41 | 0.97 | 97 | -5-10' | -8.7 | 217.6 |
| 262+24 | " | 1.80 | 178 | -7-28' | -23.2 | 203.9 |
| 263+22 | " | 2.75 | 276 | -1°-30' | -7.2 | 219.1 |
| 264+32 | " | 3.85 | 386 | | 7.8 | 223.4 |
| $\pi @ 266+27$ | 204-41 | 5.80 | 581 | -0°-4' | 5.58 | 228.60 |

"P"

48

245+74
 674
 255+48
 4+98
 260+46
 5.51
 266+27

| Sta | Az | Rad | H. Dist | Vert L | Dist | El. |
|----------|---------|------|---------|---------|--------|-------|
| T@ #54 | | | | | | 360.0 |
| B.S. #55 | 230°08' | 1.52 | | 0°00' | | |
| ✓ | 296°17' | 6.85 | 681 | +4°45' | +56.6 | 416.6 |
| ✓ | 290°19' | 5.80 | 581 | 0°00' | | 360 |
| ✓ | 293°35' | 5.20 | 519 | -3°17' | -29.8 | 330.2 |
| ✓ | 288°32' | 4.35 | 399 | -17°02' | -122.2 | 237.8 |
| ✓ | 289°24' | 3.60 | 316 | -20°40' | -119.3 | 240.7 |
| ✓ | 277°03' | 2.90 | 238 | -25°15' | -112.4 | 247.6 |
| ✓ | 270°34' | 2.20 | 140 | -32°34' | -100.5 | 259.5 |
| ✓ | 206°22' | .62 | 63 | 0°0' | | 360.0 |
| ✓ | 167°02' | .93 | 79 | +23°49' | +34.8 | 394.8 |
| ✓ | 248°07' | 1.00 | 82 | -25°50' | -39.7 | 320.3 |

See Book #4 page 29
for later notes.

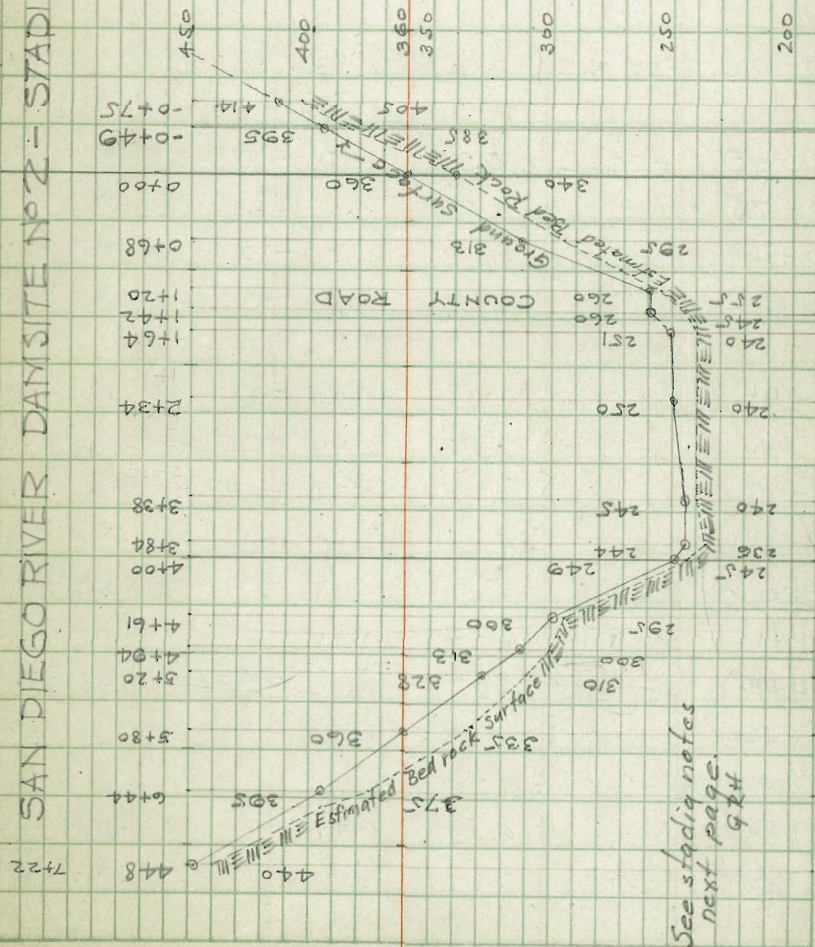
7-1-22

Sta #55 of 360' Contour
Test Pit Rock at 1'
Sta #238 of 360' Contour
Point #23 (Fletcher)
Toe of North Slope
Core Drill Hole #1 Now working
Core drill Hole #2 Casing in
In road
On hub at 360' Contour
Test Pit Rock 3' deep
On hillside on line

Sta. Az Rod H. Dist Vert L Dist El.

SAN DIEGO RIVER DAM SITE NO 2 - STADIA PROFILE

Note, Figures above ground line indicate
Ground surface elevations
Figures below ground line indicate
estimated bedrock surface



See stadia notes
next page.

Sta Az Rod H. Dist Vert L DA EI

| | | | | | | |
|------------|--------|------|--------|---------|--------|-------|
| BS on A 56 | 46°-31 | | | | | |
| K@Δ 57 | | 482 | 364.82 | | | 360 |
| to 0+00 | 230-51 | 0.50 | | | 0 | |
| K@0+0.0 | 320-22 | | 496 | 364.96 | | 360 |
| -0+49 | 140-22 | 0.73 | 48.5 | +35°-27 | +35.0 | 395.0 |
| -0+75 | " | 1.13 | 74.8 | +36-03 | +54.3 | 414.3 |
| +0+68 | 320-22 | 0.99 | 68.3 | -34-24 | -46.7 | 313.3 |
| +47 | " | 2.12 | 142 | -35-20 | -100.5 | 259.5 |
| +64 | " | 2.35 | 163.5 | -33-30 | -108.7 | 251.3 |
| 2+34 | " | 2.85 | 224.4 | -25-09 | -110.1 | 249.9 |
| 2+38 | " | 3.76 | 327.6 | -18-52 | -115.4 | 244.6 |
| 3+84 | " | 4.18 | 384.1 | -16°-48 | -115.9 | 244.1 |
| 4+00 | " | 4.30 | 400.1 | -15-32 | -111.5 | 248.5 |
| 4+61 | " | 4.68 | 461.1 | -7-28 | -60.4 | 299.6 |
| 4+94 | " | 4.97 | 493.6 | -5-25 | -46.8 | 313.2 |
| 5+20 | " | 5.21 | 520.0 | -3-32 | -32.1 | 327.9 |
| to 5+80 | ▲ | 5.79 | | | | 360 |
| 6+44 | " | 6.45 | 644.1 | +3-08 | +35.28 | 395.3 |
| 7+22 | " | 7.32 | 722.3 | +6-57 | +88.01 | 448.0 |

San Diego R. Dam Site No 2 51
Hayler Loc Franklin X Williams Rod - Stadia Profile Oct 21/21

46-31 (See profile on preceding page for estimated depth to bedrock GRH)
Compass on 0 Az = 0-30'E
Rod
0+00 to 57 = 0.50

Northly on Axis on Profile

| | | | | | | |
|-------|---|---|---|---|---|---------------------------------|
| Soly | " | " | " | " | " | on hillside |
| " | " | " | " | " | " | " |
| No ly | " | " | " | " | " | " |
| " | " | " | " | " | " | No edge to road |
| " | " | " | " | " | " | 17 R bcd |
| " | " | " | " | " | " | " " " |
| " | " | " | " | " | " | " " " |
| " | " | " | " | " | " | " " " Top No Slope |
| " | " | " | " | " | " | On No Slope (Old Mission Ditch) |
| " | " | " | " | " | " | " " " |
| " | " | " | " | " | " | In old test pit |
| " | " | " | " | " | " | On No Slope |
| " | " | " | " | " | " | " " " |
| " | " | " | " | " | " | @ 360 Contour |
| " | " | " | " | " | " | " " " |
| " | " | " | " | " | " | " " " |

Plotted Oct 21 1921

| Sta | Az | Rod H | Dist | Vert L |
|---------------------|--------|-------|--------|--------|
| π @5+80A | | 4.90 | | |
| to 237 | 227-39 | 0.382 | | 0 515 |
| to 236 | 45-54 | 0.82 | | 5.20 |
| | | 0.82 | | |
| π @235 | | 4.87 | | |
| 236 to 235 | 32-58 | 2.16 | | 0 4.80 |
| | | 2.16 | | |
| π @235 Δ | | 4.59 | 364.59 | 360 |
| 235 to 234 | 15-40 | 2.74 | | |
| | | | | +30 |
| ✓ 243-54 | 1.25 | 117 | +14-25 | 390 |
| | | | | +63 |
| ✓ 264-10 | 1.90 | 166 | +20-55 | 423 |
| | | | | +60.2 |
| ✓ 302-05 | 1.53 | 124 | +26-0 | 420.2 |
| | | | | +56 |
| ✓ 321-50 | 1.54 | 130 | +23-21 | 416 |
| | | | | +57.2 |
| ✓ 337-36 | 2.06 | 189 | +16-57 | 417.2 |
| | | | | +23 |
| ✓ 359-22 | 2.04 | 196 | +6-30 | 383 |
| | | | | +24.3 |
| ✓ 354-05 | 1.49 | 145 | +9-31 | 384.3 |
| | | | | +33.5 |
| ✓ 330-50 | 1.16 | 105 | +17-39 | 393.5 |
| | | | | +36.8 |
| ✓ 304-06 | 0.91 | 72 | +27-08 | 396.8 |
| | | | | +25.3 |
| ✓ 250-43 | 0.86 | 78 | +18-01 | 385.3 |
| π @234 | | 4.75 | 364.75 | 360 |
| | | | | +52.5 |
| ✓ 262-04 | 1.50 | 128 | +22-13 | 412.5 |

SDR Dam #2

52

5.15

Levels across R
0.30 Error

Hub 360 Contour Stake N.G.

" " " "

4+2.07 5+80 Rod ✓
236 to 5+80 0.82

214-07 1-09 Error in Az line on opp Side
212-58 Valley original 360 Survey

Az from Dam #2 Axis
Contour points for Dam site #2 Topog

plotted 10/25/11
2/12/18

| Sta | Az | Rod | H Dist | Vert L | |
|---------|--------|------|--------|--------|-------|
| ✓ T@234 | 297-15 | 1.60 | 139 | +21-34 | 414.8 |
| | | | | | +60.5 |
| | 331-52 | 2.98 | 285 | +12-0 | 420.5 |
| | | | | | +25.7 |
| | 345-02 | 2.55 | 253 | +5-51 | 385.7 |
| | | | | | +12.7 |
| | 245-33 | 0.60 | 57 | +12-33 | 372.7 |

Shots across S.D.R to Soly Side

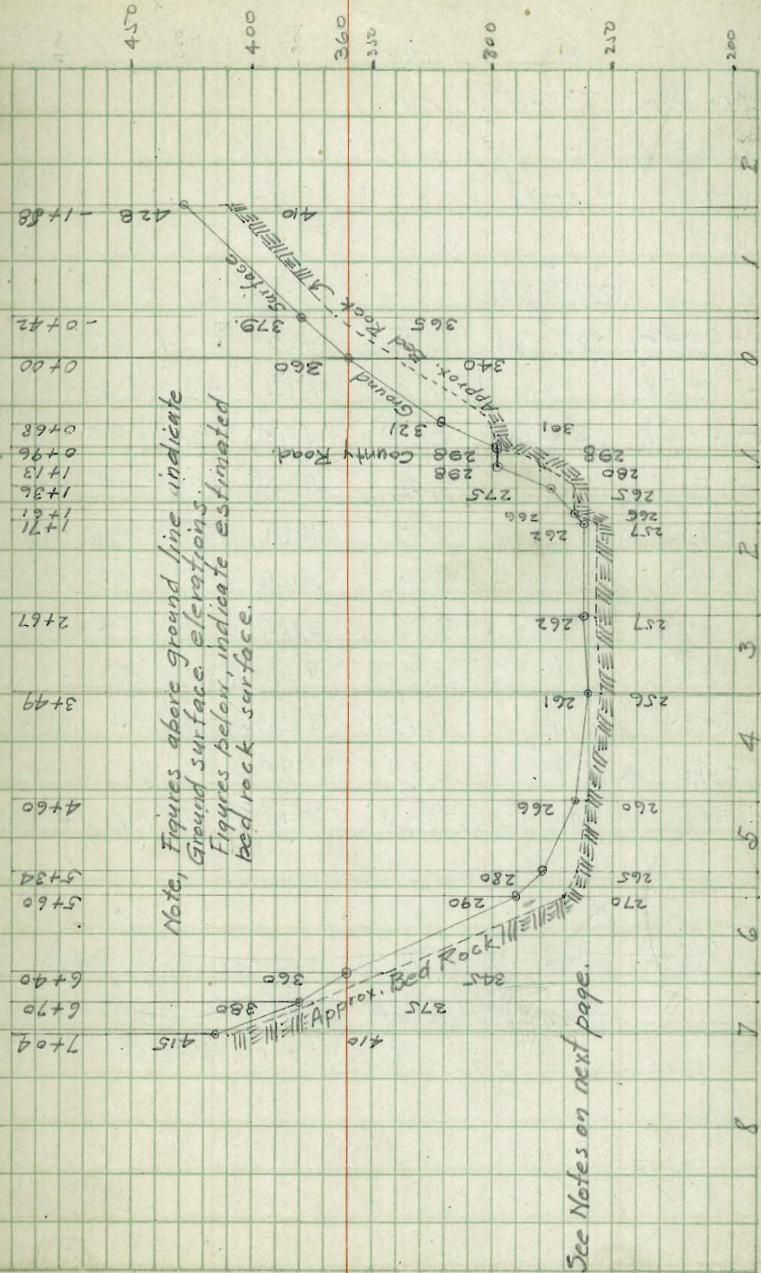
| | | | | | |
|--|--------|-------|------|-------|-------|
| | | | | | +35.5 |
| | 89-27 | 7.64 | 762 | +2-40 | 395.5 |
| | | | | | +27.5 |
| | 92-02 | 7.35 | 733 | +2-08 | 387.5 |
| | | | | | +42.7 |
| | 93-47 | 7.60 | 758 | +3-14 | 402.7 |
| | | | | | +47.0 |
| | 102-33 | 7.50 | 748 | +3-36 | 407.0 |
| | | | | | +51 |
| | 123-11 | 7.55 | 752 | +3-58 | 411 |
| | | | | | +47 |
| | 131-47 | 7.80 | 778 | +3-28 | 407 |
| | | | | | +54.8 |
| | 135-49 | 8.30 | 827 | +3-47 | 414.8 |
| | | | | | +60.7 |
| | 138-14 | 8.90 | 887 | +3-55 | 420.7 |
| | | | | | +68.2 |
| | 140-35 | 9.90 | 987 | +3-58 | 428.7 |
| | | | | | +60 |
| | 146-25 | 10.12 | 1008 | +3-23 | 420 |

End for Dam #2 Profile
+ Topog

A2 from Dam #2 AXIS

Sta. A2 Rod H. Dist Vert L Diff R

2A
SAN DIEGO RIVER DAMSITE NO. 1 STADIA PROFILE



See Notes on next page.

B.S.

H.I.

F.S.

E

| Sta | Az | Rod | H. Dist | Vert | L. D/H | Elev |
|----------|--------|------|---------|--------|--------|-------|
| 62 to 63 | 7-24 | 1.20 | | | | |
| X@63 A | | 479 | 364.79 | | | 360 |
| 63 to 64 | 24-48 | 1.22 | | | | |
| | 277-31 | | | | | |
| to -0+42 | 97-31 | 0.50 | 42.0 | +24-42 | +194 | 379.4 |
| - 1+58 | " | 1.86 | 158.1 | +23-10 | +67.7 | 427.7 |
| + 0+68 | 277-31 | 0.89 | 68.7 | -29-35 | -38.7 | 321.3 |
| 1+13 | " | 1.46 | 113.4 | -28-37 | -61.9 | 298.1 |
| 1+61 | " | 2.15 | 161.1 | -30-19 | -94.2 | 265.8 |
| 2+67 | " | 3.02 | 266.9 | -20-13 | -98.3 | 261.7 |
| 3+49 | " | 3.76 | 348.7 | -15-55 | -99.4 | 260.6 |
| 4+60 | " | 4.78 | 460.0 | -11-30 | -93.6 | 266.4 |
| 5+34 | " | 5.45 | 533.9 | -8-34 | -80.4 | 279.6 |
| to 6+40 | " | 6.39 | 640 | 0 | | 360.0 |
| 7+05 | " | 7.08 | 704.5 | +4-34 | +55.3 | 415.3 |

Note, See profile on preceding page
for estimated depth to bed rock
G.R.H.

S.D.R Dam No 1

55

Stadia Profile

24-48
7-20
20

63A is Original 360 Contour Line Station

Axis Dam #1 Profile

Compass 0 Az 360 SW

" " " S.

" " " "

" " " "

No edge Co road

S.D.R. bad, toe Soly slope (or near as rod may be read)

" " " "

" " " "

On Holy Slope toe.

360 Contour

Plotted
at 10:30
A.M.

Hayler
Franklin
Williams

(See sketch page 59)

Oct 27/27

| Sta | Az | Rod | H. Dist | Vert L | Diff | Elev |
|--------------------------|--------|------|---------|--------|------|------------------------|
| (BK [#] 2 b 53) | | | | | | 360
81.2
-786 |
| 68 to 0+00 | 354-54 | 5.48 | 538 | 8-38 | | |
| From 0+00 | | 4.90 | 284.61 | | | 279.71 |
| T.B.M | | | | 2.10 | | 282.51 |
| T.B.M | | | | 4.50 | | 282.11 |
| | 343-30 | | | | | |
| " | 1.17 | | | 0.97 | | 292.6
+335
313.2 |
| " | 1.54 | 146 | +12-55 | | | +415
321.2 |
| " | 1.82 | 172 | +13-35 | | | |
| " | 1.04 | | | 2.7 | | 281.9 |
| 165-10 | 0.67 | | | 3.7 | | 280.9 |
| " | " | | | 8.7 | | 275.9 |
| " | 0.80 | | | 8.9 | | 275.7 |
| " | " | | | 2.7 | | 281.9 |
| " | 0.97 | | | 2.15 | | 282.45 |
| " | 1.02 | | | 11.2 | | 273.4 |
| " | 1.35 | | | 10.4 | | 274.2
+67
286.4 |
| " | 1.80 | 178 | +2-07 | | | +19.1
298.81 |
| " | 2.50 | 248 | +4-24 | | | +23.3
303.01 |
| " | 2.83 | 281 | +4-31 | | | +33.8
313.51 |
| " | 3.43 | 340 | +5-42 | | | -5.95
273.76 |
| to "A" | 177-09 | 1.05 | 105 | -3-15 | | |

Dam is about 0+00

See sketch p 59

Rod 5+0 Vert L 8-38
Compass on 0-0 Az = N0-20E
468 is on So hillside original 360 contour survey
0+00 atack in corner top Old Mission Dam & Middle of dam
Top Bolt So end Old Mission Dam
" rock point top " " " No end
Called Axis of Dam which is cracked
No end of dam on hill same elev + as top of dam
" " top steep slope on hill side or knoll
" " " of knoll
No end top of dam's masonry
" " of Break in Soly end of Dam Top Masonry
" " " " " " " " Bot "
So " " " " " " " " " "
" " " " " " " " " " Top "
So end top Masonry where it breaks down
" " Bot " @ surf earth = extreme So end
Toe of hillside So of dam &
on hillside
fence No of Co road
" So " " "
on hillside So of " "
Toe of wing down stream So end dam (point "A")

plotted 10/26/27

| Sta | Az | Rod | H. Dist | Vert | Off | El |
|------|--------|------|-------------|------|-----|---------------------------|
| | | | | | | 284.61 |
| 0+00 | 253-30 | 0.06 | | 12.0 | | 271.7 |
| " | 73-30 | 0.04 | | 7.9 | | 276.7 |
| | 337-54 | 0.72 | | 14.3 | | 270.3 |
| | 345-36 | 0.72 | | 6.8 | | 277.8 |
| | 338-48 | 1.01 | | 6.1 | | 278.5 |
| | 281-53 | 1.41 | 141 - 3-43 | | | ^{-8.6}
271.1 |
| | 293-23 | 1.79 | | 6.6 | | 278.0 |
| | 307-02 | 1.49 | 148 + 4-31 | | | ^{+11.7}
291.4 |
| | 318-14 | 1.41 | 139 + 7-40 | | | ^{+18.6}
298.3 |
| | 324-20 | 1.21 | | 1.7 | | 282.0 |
| | 329-35 | 1.48 | 143 + 9-57 | | | ^{+25.8}
304.9 |
| | 325-35 | 1.82 | 177 + 9-03 | | | ^{+28.3}
308 |
| | 354-40 | 1.75 | 168 + 11-33 | | | ^{+34.3}
314 |
| | " | 2.31 | 223 + 10-48 | | | ^{+42.5}
322.2 |
| | 7-37 | 2.63 | 258 + 7-35 | | | ^{+34.4}
314.1 |
| | 19-12 | 2.30 | 237 + 6-10 | | | ^{+28.5}
305.2 |
| | 28-29 | 2.18 | 217 + 2-31 | | | ^{+9.6}
289.3 |
| | 38-32 | 1.92 | | 6.7 | | 277.9 |
| | 21-10 | 1.30 | | 6.5 | | ^{+11.6}
276.1 |
| | 6-03 | 1.55 | 154 + 4-20 | | | 291.3 |
| | 69-48 | 1.76 | | 8.4 | | 276.7 |
| | 85-53 | 1.38 | | 8.0 | | 276.6 |
| | " | 0.61 | | 4.9 | | ^{-4.6}
279.7 |
| | 106-33 | 0.86 | 86 - 3-03 | | | 275.1 |

| | | |
|--------------------------|-----------------------|----------------|
| lower toe of dam | River bottom | (point "B") |
| Upper face toe | " on silt | (" "C") |
| lower toe of dam | River bottom | (" "D") |
| Upper face " " | " on silt | (" "E") |
| (Elev. Top of dam 282.0) | | |
| lower junct with ledge | | |
| River bed | No side | |
| on slope | No side | |
| on hogback top | No side | |
| " | " | " |
| " | " | " |
| " | " | below |
| Hub on top hogback | No side | |
| On hogback top | So edge | |
| " | " | " |
| On Bench | | |
| " | " | So edge |
| On slope | | |
| " | No edge R top silt | |
| " | " | " |
| " | slope above last shot | |
| E of R | on silt | |
| 17 R | " | No edge stream |
| " | " | Silt |
| " | " | " |

Plotted
10/20/27
H.R.B.

| Sta | Az | Rod | H. Dist | Vert. L | Dist | El |
|----------|------|-----|---------|---------|------|--------|
| K@0+00 | | | 284 | 61 | | 279.71 |
| ✓ 117-0 | 1.55 | | | | 90 | 275.6 |
| ✓ 97-0 | 1.86 | | | | 89 | 275.7 |
| ✓ 115-45 | 1.91 | | | | 49 | 279.7 |
| ✓ 122-15 | 2.37 | 236 | +2-37 | | | 290.6 |
| ✓ 122-46 | 2.92 | 291 | +3-36 | | | 298 |
| ✓ 137-22 | 1.85 | 184 | +2-42 | | | 288.4 |
| ✓ 174-09 | 1.98 | 197 | +2-24 | | | 288 |
| ✓ 194-58 | 2.63 | 261 | +5-05 | | | 303 |
| ✓ 204-07 | 2.30 | 229 | +2-57 | | | 291.5 |
| ✓ 210-29 | 2.09 | | | | 50 | 279.6 |
| ✓ 187-57 | 1.71 | | | | 55 | 279.1 |
| ✓ 218-54 | 1.88 | | | | 106 | 274.0 |
| ✓ 237-10 | 1.70 | 170 | -2-03 | | | 273.6 |
| ✓ 215-05 | 1.00 | 100 | -3-19 | | | 273.9 |
| ✓ 247-15 | 0.57 | | | | 73 | 277.3 |
| ✓ " | 1.50 | | | | 86 | 276.0 |
| 266-45 | 1.50 | 150 | -3-50 | | | 269.7 |
| 286-20 | 0.63 | 61 | -8-42 | | | 270.2 |

End

Old Mission Dam Profile & Topog

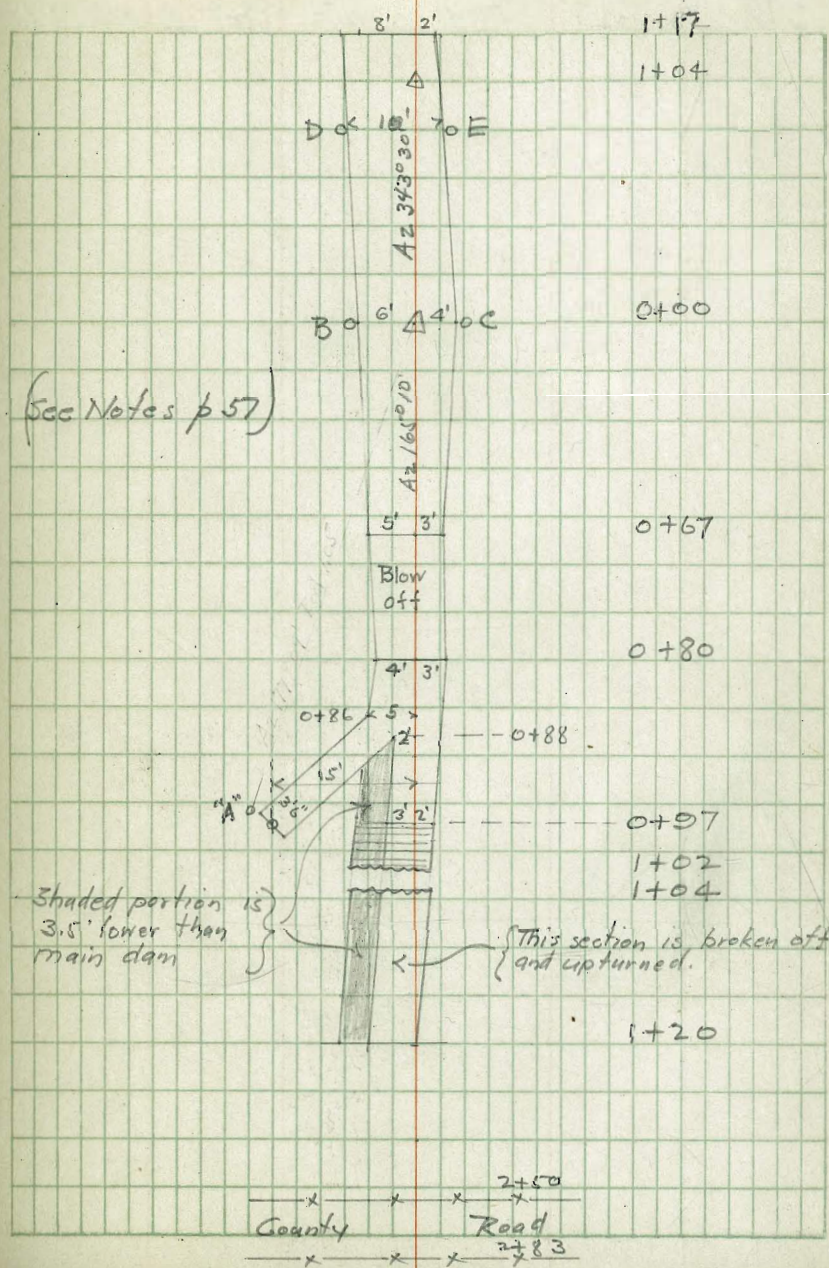
| | | |
|---------|---------|------------|
| in R | So edge | stream |
| in R | " | " |
| R | edge | Soly slope |
| On | Soly | slope |
| @ fence | No | side road |
| On | So | Slope |
| " | " | " |
| @ fence | No | side road |
| On | Soly | Slope |
| " | " | " |
| " | " | " |
| in R | So | edge |
| in R | bed | |
| " | " | " |
| " | " | on roof |
| " | " | " |
| " | " | " |
| " | " | No edge |
| " | " | " |

Plotted Oct 26 21
HCB

Sta Az Rod H. Dist Vert L. Diff El

Old Mission Dam

10-22-21
Hayler



Sta Az Rad. H. Dist Vert L Diff E/L

The right page of the notebook features a grid of 20 columns and 20 rows. The grid is formed by light green lines. The columns are defined by vertical lines, and the rows are defined by horizontal lines. The grid is empty and occupies the majority of the right page.

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KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P. = $23^{\circ} 20'$ to the R. at Station 542+72.

Ext. in Tab. IV opposite $23^{\circ} 20' = 120.87$
 $120.87 \div 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. IV opp. $23^{\circ} 20' = 1183.1$
 $1183.1 \div 10 = 118.31$.

Tab. V correction for A. $23^{\circ} 20'$ for a 10° Cur. = 0.16
 $118.31 + 0.16 = 118.47 =$ corrected Tangent.

(If corrected Ext. is required find in same way)
 Ang. $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333 =$ L. C.

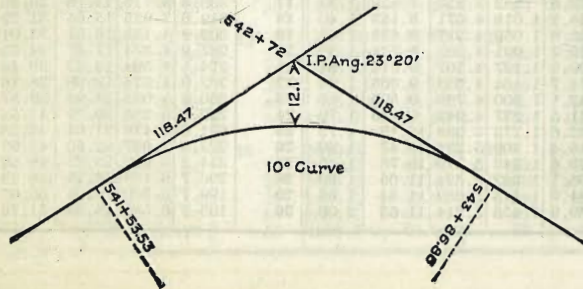
| | | | |
|--------------------------------------------|-------|--------------|-----------|
| $2^{\circ} 19\frac{1}{2}' =$ def. for sta. | 542 | I. P. = sta. | 542+72 |
| $4^{\circ} 49\frac{1}{2}' =$ " " " | +50 | Tan. = | 1.18.47 |
| $7^{\circ} 19\frac{1}{2}' =$ " " " | 543 | B. C. = sta. | 541+53.53 |
| $9^{\circ} 49\frac{1}{2}' =$ " " " | +50 | L. C. = | 2.33.33 |
| $11^{\circ} 40' =$ " " " | 543+ | E. C. = Sta. | 543+86.86 |
| | 86.86 | | |

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^{\circ} \text{ Cur.}) = 139.41' =$
 $2^{\circ} 19\frac{1}{2}' =$ def. for sta. 542.

Def. for 50 ft. = $2^{\circ} 30'$ for a 10° Curve.

Def. for 36.86 ft. = $1^{\circ} 50\frac{1}{2}'$ for a 10° Curve.

(These tables are published in Field Books of KEUFFEL & ESSER CO., New York, N. Y.)



CITY - BENCH MARKS

| | | City
Datum | U.S.G.S.
Datum | |
|------|------------------------|--------------------|-------------------|----------|
| SE | Cor Madison + Texas | Brass Plug in Curb | 346.03 | 352.15 |
| " | " " " Louisiana | " " " " | 342.31 | 348.43 |
| N.E. | " University + Alabama | " " " " " " " | 265.49 | 271.61 |
| S.W. | " " + Florida | " " " " " " " | 287.08 | 293.20 |
| NE | " Alabama + El Cajon | " " " " " " " | 306.57 | 312.69 |
| NW | " " + Lincoln | " " " " " " " | 286.11 | 292.23 |
| NW | " " + Cypress | " " " " " " " | 244.98 | 251.10 |
| NW | " " + Upas | " " " " " " " | 259.50 | 265.62 |
| N.W. | " 6th + University | " " " " " " " | 283.87 | = 289.99 |

East San Diego Bench Marks

Fairmount + El Cajon S.W. Cor B.P. 352.00 358.12
 Castel + Sisson. NW Cor B.P. 330.52 336.64
 78ks

330.52
 6.12
 336.64

62-63 7-24

67-64 24-48

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0 | 7.0 | 7.2 | 7.3 | 7.5 | 7.6 | 7.8 | 7.9 | 8.1 | 8.2 | 8.4 | 0 |
| 1 | 8.5 | 8.7 | 8.8 | 9.0 | 9.1 | 9.3 | 9.4 | 9.6 | 9.7 | 9.9 | 1 |
| 2 | 10.0 | 10.2 | 10.3 | 10.5 | 10.6 | 10.8 | 10.9 | 11.1 | 11.2 | 11.4 | 2 |
| 3 | 11.5 | 11.7 | 11.8 | 12.0 | 12.1 | 12.3 | 12.4 | 12.6 | 12.7 | 12.9 | 3 |
| 4 | 13.0 | 13.2 | 13.3 | 13.5 | 13.6 | 13.8 | 13.9 | 14.1 | 14.2 | 14.4 | 4 |
| 5 | 14.5 | 14.7 | 14.8 | 15.0 | 15.1 | 15.3 | 15.4 | 15.6 | 15.7 | 15.9 | 5 |
| 6 | 16.0 | 16.2 | 16.3 | 16.5 | 16.6 | 16.8 | 16.9 | 17.1 | 17.2 | 17.4 | 6 |
| 7 | 17.5 | 17.7 | 17.8 | 18.0 | 18.1 | 18.3 | 18.4 | 18.6 | 18.7 | 18.9 | 7 |
| 8 | 19.0 | 19.2 | 19.3 | 19.5 | 19.6 | 19.8 | 19.9 | 20.1 | 20.2 | 20.4 | 8 |
| 9 | 20.5 | 20.7 | 20.8 | 21.0 | 21.1 | 21.3 | 21.4 | 21.6 | 21.7 | 21.9 | 9 |
| 10 | 22.0 | 22.2 | 22.3 | 22.5 | 22.6 | 22.8 | 22.9 | 23.1 | 23.2 | 23.4 | 10 |
| 11 | 23.5 | 23.7 | 23.8 | 24.0 | 24.1 | 24.3 | 24.4 | 24.6 | 24.7 | 24.9 | 11 |
| 12 | 25.0 | 25.2 | 25.3 | 25.5 | 25.6 | 25.8 | 25.9 | 26.1 | 26.2 | 26.4 | 12 |
| 13 | 26.5 | 26.7 | 26.8 | 27.0 | 27.1 | 27.3 | 27.4 | 27.6 | 27.7 | 27.9 | 13 |
| 14 | 28.0 | 28.2 | 28.3 | 28.5 | 28.6 | 28.8 | 28.9 | 29.1 | 29.2 | 29.4 | 14 |
| 15 | 29.5 | 29.7 | 29.8 | 30.0 | 30.1 | 30.3 | 30.4 | 30.6 | 30.7 | 30.9 | 15 |
| 16 | 31.0 | 31.2 | 31.3 | 31.5 | 31.6 | 31.8 | 31.9 | 32.1 | 32.2 | 32.4 | 16 |
| 17 | 32.5 | 32.7 | 32.8 | 33.0 | 33.1 | 33.3 | 33.4 | 33.6 | 33.7 | 33.9 | 17 |
| 18 | 34.0 | 34.2 | 34.3 | 34.5 | 34.6 | 34.8 | 34.9 | 35.1 | 35.2 | 35.4 | 18 |
| 19 | 35.5 | 35.7 | 35.8 | 36.0 | 36.1 | 36.3 | 36.4 | 36.6 | 36.7 | 36.9 | 19 |
| 20 | 37.0 | 37.2 | 37.3 | 37.5 | 37.6 | 37.8 | 37.9 | 38.1 | 38.2 | 38.4 | 20 |
| 21 | 38.5 | 38.7 | 38.8 | 39.0 | 39.1 | 39.3 | 39.4 | 39.6 | 39.7 | 39.9 | 21 |
| 22 | 40.0 | 40.2 | 40.3 | 40.5 | 40.6 | 40.8 | 40.9 | 41.1 | 41.2 | 41.4 | 22 |
| 23 | 41.5 | 41.7 | 41.8 | 42.0 | 42.1 | 42.3 | 42.4 | 42.6 | 42.7 | 42.9 | 23 |
| 24 | 43.0 | 43.2 | 43.3 | 43.5 | 43.6 | 43.8 | 43.9 | 44.1 | 44.2 | 44.4 | 24 |
| 25 | 44.5 | 44.7 | 44.8 | 45.0 | 45.1 | 45.3 | 45.4 | 45.6 | 45.7 | 45.9 | 25 |
| 26 | 46.0 | 46.2 | 46.3 | 46.5 | 46.6 | 46.8 | 46.9 | 47.1 | 47.2 | 47.4 | 26 |
| 27 | 47.5 | 47.7 | 47.8 | 48.0 | 48.1 | 48.3 | 48.4 | 48.6 | 48.7 | 48.9 | 27 |
| 28 | 49.0 | 49.2 | 49.3 | 49.5 | 49.6 | 49.8 | 49.9 | 50.1 | 50.2 | 50.4 | 28 |
| 29 | 50.5 | 50.7 | 50.8 | 51.0 | 51.1 | 51.3 | 51.4 | 51.6 | 51.7 | 51.9 | 29 |
| 30 | 52.0 | 52.2 | 52.3 | 52.5 | 52.6 | 52.8 | 52.9 | 53.1 | 53.2 | 53.4 | 30 |
| 31 | 53.5 | 53.7 | 53.8 | 54.0 | 54.1 | 54.3 | 54.4 | 54.6 | 54.7 | 54.9 | 31 |
| 32 | 55.0 | 55.2 | 55.3 | 55.5 | 55.6 | 55.8 | 55.9 | 56.1 | 56.2 | 56.4 | 32 |
| 33 | 56.5 | 56.7 | 56.8 | 57.0 | 57.1 | 57.3 | 57.4 | 57.6 | 57.7 | 57.9 | 33 |
| 34 | 58.0 | 58.2 | 58.3 | 58.5 | 58.6 | 58.8 | 58.9 | 59.1 | 59.2 | 59.4 | 34 |
| 35 | 59.5 | 59.7 | 59.8 | 60.0 | 60.1 | 60.3 | 60.4 | 60.6 | 60.7 | 60.9 | 35 |
| 36 | 61.0 | 61.2 | 61.3 | 61.5 | 61.6 | 61.8 | 61.9 | 62.1 | 62.2 | 62.4 | 36 |

Calculated by Julien A. Hall, M. Am. Soc. C. E.