

3

400

LEVEL

WIS

Table showing the difference of latitude and departure in running a course at any angle from 1 to 60 minutes.

**MICROFILMED**

MINUTES	LKS.	MINUTES	LKS.	MINUTES	LKS.
1.....	2 $\frac{1}{3}$	21.....	49	41.....	95 $\frac{2}{3}$
2.....	4 $\frac{2}{3}$	22.....	51 $\frac{1}{3}$	42.....	98
3.....	7	23.....	53 $\frac{2}{3}$	43.....	100 $\frac{1}{3}$
4.....	9 $\frac{1}{3}$	24.....	56	44.....	102 $\frac{2}{3}$
5.....	11 $\frac{2}{3}$	25.....	58 $\frac{1}{3}$	45.....	105
6.....	14	26.....	60 $\frac{2}{3}$	46.....	107 $\frac{1}{3}$
7.....	16 $\frac{1}{3}$	27.....	63	47.....	109 $\frac{2}{3}$
8.....	18 $\frac{2}{3}$	28.....	65 $\frac{1}{3}$	48.....	112
9.....	21	29.....	67 $\frac{2}{3}$	49.....	114 $\frac{1}{3}$
10.....	23 $\frac{1}{3}$	30.....	70	50.....	116 $\frac{2}{3}$
11.....	25 $\frac{2}{3}$	31.....	72 $\frac{1}{3}$	51.....	119
12.....	28	32.....	74 $\frac{2}{3}$	52.....	121 $\frac{1}{3}$
13.....	30 $\frac{1}{3}$	33.....	77	53.....	123 $\frac{2}{3}$
14.....	32 $\frac{2}{3}$	34.....	79 $\frac{1}{3}$	54.....	126
15.....	35	35.....	81 $\frac{2}{3}$	55.....	128 $\frac{1}{3}$
16.....	37 $\frac{1}{3}$	36.....	84	56.....	130 $\frac{2}{3}$
17.....	39 $\frac{2}{3}$	37.....	86 $\frac{1}{3}$	57.....	133
18.....	42	38.....	88 $\frac{2}{3}$	58.....	135 $\frac{1}{3}$
19.....	44 $\frac{1}{3}$	39.....	91	59.....	137 $\frac{2}{3}$
20.....	46 $\frac{2}{3}$	40.....	93 $\frac{1}{3}$	60.....	140

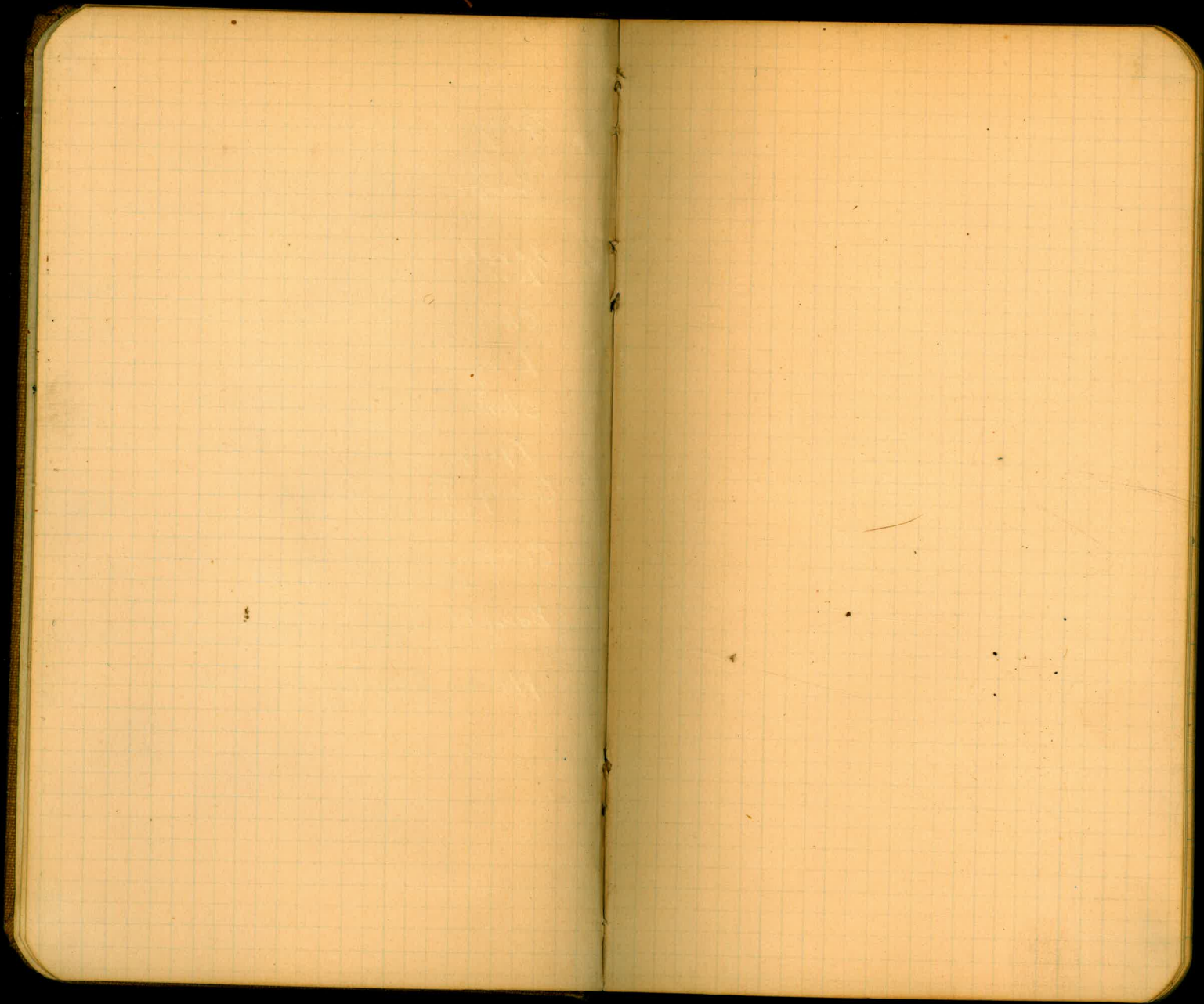
### TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

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i. Tying Dulzyna Pass - Shecken Valley

T.P. at D 131+50				748.26
	+94	753.20		
o	575	758.97	308	750.12
U.S.G.S B.M.		0.78		755.09

~~~~~ # ~~~~~

|                  |     |        |       |        |
|------------------|-----|--------|-------|--------|
| T.P. at V 113+30 |     |        |       | 793.35 |
|                  | 103 | 794.38 |       |        |
| o                | 050 | 789.35 | 12.53 | 781.35 |
| o                | 040 | 770.19 | 17.56 | 769.79 |
| o                | 349 | 760.78 | 17.90 | 757.29 |
| U.S.G.S B.M.     |     | 5.53   |       | 758.25 |

Road Levels to U.S.G.S B.M.

West of Shecken Avenue

4-30-07  
P.M.

R. Watson

Government Elev. 875.0

Max Watson

CO = 200

Government Elev. 875.0

2. Change of Sine in Rocky Gorge

(V. wire)

5-1-06

R. Wueste  
Max Watson  
Ford Beebe  
Geo. Lane  
R. Hutchins

|               |      |        |      |        |       |
|---------------|------|--------|------|--------|-------|
|               | 7.89 | 971.03 |      | 963.4  |       |
| 80+75         |      |        | 3.8  | 967.2  | 959.9 |
| 81            |      |        | 6.8  | 962.2  | 959.8 |
| +25           |      |        | 13.5 | 957.5  |       |
| +36           |      |        | 6.9  | 964.1  |       |
| +48           |      |        |      | 946.1  |       |
| +66           |      |        | 12.7 | 958.3  |       |
| +66           |      |        |      | 941.3  |       |
| 0             | 0.19 | 961.34 | 9.88 | 961.15 |       |
| +99           |      |        | 5.7  | 955.6  | 955.3 |
| 82+49 = 82+15 |      |        | 7.7  | 953.6  | 953.5 |

= T.P. on Rock 4' to 81+00

7.3  
3.4  
x

1  
2  
4

on Rock

x

3. Change in Sine across  
From Sta. V 85+04 to V 92

|       | 1225 | 945.24    |       | 937.99 | 588<br>11 |
|-------|------|-----------|-------|--------|-----------|
| 85+04 |      |           |       |        | 931.3     |
| +50   |      |           | 7.1   | 938.1  | 938.1     |
| 86    |      |           | 6.3   | 938.9  | 936.8     |
| 0     | 853  | 953.52    | 17.6  | 943.99 |           |
| +50   |      |           | 8.7   | 944.3  | 936.6     |
| +90   |      | by Ramsey |       | 943.1  | 934.5     |
| 87+34 |      |           | 3.1   | 949.4  | 933.3     |
| +49   |      |           |       | 935.4  | 936.1     |
| +70   |      |           | 7.1   | 945.4  | 937.4     |
| +92   |      |           |       | 930.3  | 936.3     |
| 88+20 |      |           | 13.2  | 939.2  | 931.1     |
| +50   |      |           | 13.6  | 938.9  | 930.3     |
| +75   |      |           | 13.3  | 937.7  | 929.6     |
| 89    |      |           |       | 917.9  | 931.0     |
| 0     | 236  | 942.59    | 11.99 | 940.53 | 930.0     |
| 89+30 |      |           | 9.9   | 933.0  | 928.2     |
| +50   |      |           | 8.8   | 934.1  | 927.7     |
| +70   |      |           | 7.6   | 935.3  | 927.2     |

Sine washes.

|       | Final sine<br>across gulches | 5-1-07                                                              |
|-------|------------------------------|---------------------------------------------------------------------|
| = T.P | 86+03 peg<br>flagged white.  | P. W. White<br>Max Watson<br>Ford Beale<br>Geo. Sam<br>H. Hutchins. |
|       | +2.1                         |                                                                     |
|       | +8.8                         | peg 86+38                                                           |
|       | -11.4                        | -13.1<br>Bottom of gulch no 1                                       |
|       | +16.1                        | 13.1                                                                |
|       |                              | -0.7<br>Bottom of gulch no 2                                        |
|       | +12.0                        | +10.2                                                               |
|       |                              | -4.9<br>Bottom of gulch no 3                                        |
|       | +8.1                         | +6.0                                                                |
|       | +8.6                         | +6.9                                                                |
|       | +8.6                         | +7.2                                                                |
|       | -11.1                        | Bottom of gulch 4<br>peg 87+75                                      |
|       | +5.2                         | +4.2                                                                |
|       | +6.4                         |                                                                     |
|       | +8.1                         | *                                                                   |



4.

90

942.89

10.1

932.8 925.4

+74

0

0.71

930.90

12.70

930.19

peg

90+28

90+35

3.2

927.7 923.4

+43

$\frac{1}{5}$   
0

+62

15.5

915.4 921.8

-6.4

91

12.5

918.4 919.4

-1.0

0

5.14

925.64

10.40

920.50

peg

91+70

+50

8.7

916.9 916.4

+0.5

92+04 = 192

9.9

915.7 913.1

+26

See Book 1

Page 43 for continuation

5. Change of Sign  $\sqrt{47+50}$  to  $52+50$

268

1173.61

1170.93

= T.P. page 54 Book 1.

42+50

1169.1

4.5

+90

1166.2

7.4

43

1154.2

+25

1167.9

5.7

+50

1166.8

6.8

x

44

1163.9

9.7

+50

1161.0

12.6

o

1.83

1162.98

12.56

1161.05

peg

44+63

45

1158.1

4.8

+50

1155.2

7.7

-5.8

46

1152.3

10.6

o

1.32

1151.67

12.53

1150.35

6<sup>th</sup> R

peg

45+90

+50

1149.4

2.3

47

1146.5

5.2

+50

1143.6

8.1

48

1140.7

11.0

o

0.72

1160.15

12.24

1139.43

peg

48+144

6.

1140.5

48+50

1137.5

2.4

0

56.8

1135.23

10.60

1179.55

peg

10' P

49+00

49

1134.9

0.3

+50

1132.0

3.2

50

1129.1

6.1

1  
1  
2

+50

1126.2

9.0

51

1123.3

1.9

0

0.54

1125.41

10.34

1124.89

on Rock

51+20

+50

1120.4

5.0

52

1117.5

7.9

+50

1114.6

10.8 ✓

x

7

Levels over "N" line

May 3<sup>rd</sup> 1907

|                     |       |        |       |        |
|---------------------|-------|--------|-------|--------|
|                     | 11.08 | 804.43 |       | 793.35 |
| N 111 + 53          |       |        | 6.1   | 798.3  |
| 112                 |       |        | 1.8   | 802.6  |
| +09                 |       |        | 1.8   | 802.6  |
| 113                 |       |        | 6.5   | 797.9  |
| 114                 |       |        | 10.2  | 794.2  |
| 115                 |       |        | 11.1  | 793.3  |
| 116                 |       |        | 10.8  | 793.6  |
| 117                 |       |        | 9.8   | 794.6  |
| +10                 |       |        | 9.9   | 794.5  |
| 118                 |       |        | 12.1  | 792.3  |
| 0                   | 7.16  | 795.35 | 11.74 | 793.19 |
| 119                 |       |        | 7.7   | 787.7  |
| 120                 |       |        | 11.6  | 783.8  |
| 121                 |       |        | 11.6  | 783.8  |
| 122 <sup>+</sup> 75 |       |        |       | 781.0  |
|                     |       |        | 12.1  | 783.3  |
| +17                 |       |        | 10.3  | 785.1  |
| 0                   | 5.53  | 790.60 | 10.78 | 785.07 |

= T.P. page 47 Book I

R.W. West  
Ford Bank

= Transit Hub

= Transit Hub

pg 5' h 118 + 00

pg 13' h 100 + 17

79060

123 4.8 785.8

+50 7.7 782.9

124 10.76 779.84

45 780.99

+50 3.8 777.14

125 5.4 775.6

126 7.7 773.3

127 10.3 770.7

128 11.7 769.3

+0.8 = D 127 + 50 11.63 769.36

128 + 32 = 127 + 50

= Transit Sub

= Transit Sub

= Transit Sub

< 85 > Check no. 127

Wagon Room

Elev. on D line 769.0 ✓ = Transit Sub

9. Seeds to Profile of Ward Sun

from 38+70 to 50+00

643 1215.43 1209.0

= Elev of 35+50

May 3<sup>rd</sup> 1907

38+70 5.2 1210.2

R. W. West

+50 4.1 1211.3

Max Watson

39 9.6 1205.8

Ford Beebe

0 343 1208.73 10.13 1205.30

Geo. S. Sam

+25 6.0 1202.7

R. H. Huleth

+40 14.2 1194.5

W. M. Moss

+50 11.0 1197.7

+75 4.6 1204.1

40 6.4 1202.3

+50 9.2 1199.5

+60 12.0 1196.7

+75 18.0 1190.7

41 12.0 1196.7

+33 12.3 1196.4

= 42 Ward's Sun

0 201 1199.70 11.04 1197.69

+50 5.7 1194.0

+75 3.1 1196.6

1199.70

|    |      |         |       |         |
|----|------|---------|-------|---------|
| 3  | 42   |         | 5.8   | 1193.9  |
|    | +32  |         | 8.9   | 1190.8  |
| 3  | +50  |         | 9.0   | 1190.7  |
|    | +70  |         | 9.1   | 1190.6  |
| 0  | 120  | 1189.66 | 11.24 | 1188.46 |
| 43 |      |         | 14.0  | 1175.7  |
|    | +20  |         | 5.6   | 1184.1  |
|    | +35  |         | 3.8   | 1185.9  |
| 4  | +50  |         | 3.9   | 1185.8  |
|    | +85  |         | 6.7   | 1183.0  |
| 44 |      |         | 3.5   | 1186.2  |
|    | +35  |         | 8.4   | 1181.3  |
| 4  | +50  |         | 6.7   | 1183.0  |
| 45 |      |         | 13.3  | 1176.4  |
| 0  | 7.33 | 1180.12 | 11.87 | 1177.9  |
|    | +45  |         | 6.0   | 1174.1  |
|    | +50  |         | 3.0   | 1177.1  |

= 43 Wards

on Shaped Rock

= 44 of Wards Sim

118012

|       |      |         |        |
|-------|------|---------|--------|
| 45+85 |      | 5.9     | 1174.2 |
| 46    |      | 6.2     | 1173.9 |
| +50   |      | 10.1    | 1170.0 |
| 47    |      | 11.7    | 1168.4 |
| +50   |      | 14.0    | 1166.1 |
| ⊙     | 0.65 | 1169.24 | 11.53  |
| 48    |      | 4.2     | 1165.0 |
| +50   |      | 6.0     | 1163.2 |
| 49    |      | 6.7     | 1162.5 |
| +15   |      | 0.6     | 1168.6 |
| +50   |      | 11.1    | 1158.1 |
| ⊙     | 4.21 | 1161.30 | 13.45  |
| 50    |      | 7.4     | 1153.8 |

Big cluster of rocks at 45+60

= Ward's stake

Through bad run of rocks.

Showing signs of Boulder.

= c 50 = 1151.7

Starting point 1.2  
above grade.



12.

Change in King Sine.

Apr 23 1907

R. Wiest  
Max Weber  
Fred Beck  
Geo. S. Lane

|        | 1240.0 | 138.82 |      | 126.42 | =                           |
|--------|--------|--------|------|--------|-----------------------------|
| 178    |        |        | 10.7 | 128.1  |                             |
| 177+50 |        |        | 10.8 | 128.0  |                             |
| 177    |        |        | 10.9 | 127.9  |                             |
| 177    |        |        | 15.6 | 123.2  | = Sewell Creek Apr 23, 1907 |
| 176+88 |        |        | 10.8 | 128.0  |                             |
| +85    |        |        |      |        | = Fence                     |
| +80    |        |        | 4.4  | 134.4  |                             |
| +70    |        |        | 7.7  | 136.1  |                             |
| +58    |        |        | 5.0  | 133.8  |                             |
| +50    |        |        | 9.1  | 129.7  |                             |
| 176    |        |        | 8.7  | 130.1  |                             |
| 175+87 |        |        | 7.3  | 131.5  |                             |
| +50    |        |        | 10.0 | 128.9  |                             |
| 0      | 546    | 140.28 | 4.00 | 134.82 |                             |
| 175    |        |        | 11.1 | 129.2  |                             |
| 174+50 |        |        | 8.8  | 131.5  |                             |
| +18    |        |        | 5.4  | 134.9  | on Solid Rock               |

Along Solid Rock face

13.

140.78

|        |      |        |       |        |
|--------|------|--------|-------|--------|
| 174    |      |        | 5.6   | 134.7  |
| 173+50 |      |        | 8.3   | 137.0  |
| 173    |      |        | 7.0   | 133.3  |
| 0      | 148  | 138.19 | 3.57  | 136.71 |
| 172+50 |      |        | 7.0   | 131.2  |
| +03    |      |        | 7.2   | 131.0  |
| 172    |      |        | 6.6   | 131.6  |
| 0      | 7.52 | 139.22 | 6.49  | 131.70 |
| 171    |      |        | 5.2   | 134.0  |
| 0      | 107  | 134.24 | 5.85  | 133.37 |
| 170    |      |        | 2.6   | 130.8  |
| 0      | 529  | 135.70 | 4.03  | 130.41 |
| 169    |      |        | 1.9   | 133.8  |
| 0      | 1222 | 145.59 | 2.33  | 133.37 |
| 168    |      |        | 11.1  | 134.5  |
| 167    |      |        | 13.0  | 132.6  |
| 0      |      |        | 11.40 | 134.19 |

change of  
Kings sin= 173 Kings sin  
(of Kings sin)

peg 172+00

peg 170+00

peg 4' L 170+00

peg 2' E 169+00

peg 15' R 167+00

|        |       |        |      |        |
|--------|-------|--------|------|--------|
|        | 7.19  | 138.89 |      | 131.70 |
| 172+50 |       |        | 7.9  | 131.0  |
| 172    |       |        | 7.4  | 131.5  |
| 171+50 |       |        | 4.2  | 134.7  |
| 171    |       |        | 5.0  | 133.9  |
| 170+50 |       |        | 7.3  | 131.6  |
| 0      |       |        | 7.31 | 131.58 |
|        | 4.82  | 136.40 |      |        |
| 170    |       |        | 6.1  | 130.3  |
| 169+50 |       |        | 4.8  | 131.6  |
| 169    |       |        | 3.5  | 132.9  |
| 168+50 |       |        | 1.8  | 134.6  |
| 0      | 8.45  | 142.65 | 2.70 | 134.20 |
| 168    |       |        | 8.9  | 133.9  |
| 167+50 |       |        | 9.5  | 133.2  |
| 167    |       |        | 8.8  | 133.9  |
| 0      | 11.12 | 147.28 | 6.49 | 136.16 |
| 166+50 |       |        | 13.4 | 133.9  |

changed  
King's Sin

May 9<sup>th</sup> 1907.

= T.P. at Kingo 172 (see page 13)  
(King's numbering)

J. P. Harris

R. W. W. W.  
Max Watson  
Ford Beebe  
Geo. S. Sam  
Michael Petchin  
Ewan Moss,

on pag 5' 170+35

on pag 168+65

on pag 4' P 166+75

147.28

|          |      |        |       |        |
|----------|------|--------|-------|--------|
| 166      |      |        | 139   | 133.1  |
| 165 + 50 |      |        | 12.7  | 135.1  |
| 165      |      |        | 8.2   | 139.1  |
| 164 + 50 |      |        | 7.1   | 140.2  |
| 0        | 8.00 | 150.81 | 44.7  | 142.81 |
| 164      |      |        | 10.9  | 139.9  |
| 163 + 50 |      |        | 10.2  | 140.6  |
| 163      |      |        | 10.2  | 140.6  |
| 162 + 50 |      |        | 12.4  | 138.4  |
| 162      |      |        | 13.1  | 137.7  |
| 0        | 8.33 | 148.21 | 10.93 | 139.38 |
| 161 + 50 |      |        | 12.7  | 135.5  |
| 161      |      |        | 16.0  | 132.7  |
| 160 + 50 |      |        | 14.2  | 134.0  |
| 160      |      |        | 11.9  | 136.3  |
| 0        | 8.95 | 145.31 | 11.85 | 136.36 |
| 159 + 50 |      |        | 5.7   | 139.6  |

on Jump 5' P 164 + 50

on Rock 70' P 161 + 50

on peg 15' L 159 + 50

change of Kingo  
Sun

16.

145.31

159 4.9 140.4

158+50 5.2 140.1

o 4.89 145.79 4.91 140.40

in per on line 158+35

158 4.7 140.6

157+50 5.4 139.9

157 5.1 140.2

156+50 4.4 140.9

156 4.0 141.3

o 10.57 152.01 3.85 141.44

in per 3.9 156+08

155+50 10.1 141.9

continued from 155+50 May 10, 1907

155 9.6 142.4

S.B. Harris

154+50 8.4 143.6

P. Wuest

154 8.3 143.7

Max Watson

153+50 8.1 143.9

Ford Beebe

E.W.M. Moss

R. Mitchell (driver)

o 3.70 153.48 2.23 149.78

in per on per 4.0 153+00

153 9.9 143.6

152+50 9.0 144.5

17.

15348

|          |       |        |     |        |       |  |
|----------|-------|--------|-----|--------|-------|--|
| 152      |       |        | 88  | 144.7  |       |  |
| 151 + 50 |       |        | 82  | 145.3  |       |  |
| 151      |       |        | 76  | 145.9  |       |  |
| 150 + 55 |       |        | 77  | 146.3  |       |  |
| + 05     |       |        | 56  | 147.9  |       |  |
| 0        | 12.33 | 162.07 | 374 | 149.74 |       |  |
| 149 + 55 |       |        | 121 | 150.0  |       |  |
| + 05     |       |        | 93  | 152.8  |       |  |
| 148 + 55 |       |        | 61  | 156.0  |       |  |
| + 31     |       |        | 74  | 159.7  |       |  |
| 0        | 12.73 | 173.25 | 155 | 160.52 |       |  |
| 149 + 05 |       |        | 144 | 158.9  |       |  |
| 147 + 50 |       |        | 111 | 162.2  | 162.2 |  |
| 147      |       |        |     | 165.7  | 7.6   |  |
| 146 + 50 |       |        |     | 169.2  | 4.1   |  |
| 0        | 12.65 | 182.87 | 303 | 170.22 |       |  |
| 146      |       |        |     | 172.7  | 10.2  |  |

change of  
ridge line

on Peak 6' W 149 + 70

on Peak on high 148 + 31

on Peak 10' P 146 + 70

18.

Change of King's line

182.87

145+50

176.2

6.7

145

179.7

3.2

0

12.10

192.93

204

180.83

on Rock 9' P

145+00

144+50

99

183.0

183.2

9.7

-0.2

144

7.1

185.8

143+50

43

188.6

0

10.17

201.62

148

191.45

on pag

10' L

143+18

143

9.7

191.9

142+63

73

194.3

142

54

196.2

141+50

39

197.7

141

35

198.1

140+50

40

197.6

0

6.98

204.67

393

197.69

on pag

line

140+30

140

73

197.4

134+50

60

198.7

139

50

199.7

19.

Change King's Sim

204.67

|        |      |        |       |        |       |      |         |             |
|--------|------|--------|-------|--------|-------|------|---------|-------------|
| 138+50 |      |        | 47    | 200.0  |       |      |         |             |
| 138    |      |        | 6.0   | 198.7  |       |      |         |             |
| 137+50 |      |        | 57    | 199.0  | 199.0 |      |         |             |
| 137    |      |        |       |        | 197.0 | 7.7  |         |             |
| 136+50 |      |        |       |        | 195.0 | 9.7  |         |             |
| 136    |      |        |       |        | 193.0 | 11.7 |         |             |
| 0      | 3.87 | 196.60 | 1194  | 192.73 |       |      | on peg  | line 135+85 |
| 135+50 |      |        |       |        | 191.0 | 5.6  |         |             |
| 135    |      |        |       |        | 189.0 | 7.6  |         |             |
| 134+50 |      |        |       |        | 187.0 | 9.6  |         |             |
| 134+41 |      |        | 108   |        |       |      | fence   |             |
| 134    |      |        |       |        | 185.0 | 11.6 |         |             |
| 133+50 |      |        |       |        | 183.0 | 13.6 |         |             |
| 0      | 3.84 | 188.09 | 12.35 | 184.25 |       |      | on Rock | line 133+60 |
| 133    |      |        |       |        | 181.0 | 7.1  |         |             |
| 132+50 |      |        |       |        | 179.0 | 9.1  |         |             |
| 132.0  |      |        | 126   | 175.5  | 177.0 | 11.1 | -1.5    |             |



18809

|        |       |        |       |         |   |         |             |
|--------|-------|--------|-------|---------|---|---------|-------------|
| 131+50 |       |        | 175.0 | 131     | + |         |             |
| 131    | 0.66  | 176.52 | 172.3 | 175.86  | 0 | on Rock | 6' R 131+23 |
| 131    |       |        | 173.0 | 36      | x |         |             |
| 130+50 |       |        | 7.5   | 16.90   |   |         |             |
| 130+27 |       |        |       |         |   | face    |             |
| 130    |       |        | 8.4   | 16.8.1  |   |         |             |
| 129+55 |       |        | 10.7  | 16.58   |   | crack   |             |
| +50    |       |        | 9.7   | 16.6.8  |   |         |             |
| 129    |       |        | 8.1   | 16.8.4  |   |         |             |
| 129    | 0.155 | 172.15 | 6.20  | 170.32  |   | on Rock | 2' L 129+08 |
| 128+50 |       |        | 4.7   | 16.7.5  |   |         |             |
| 128    |       |        | 5.4   | 16.6.8  |   |         |             |
| 127+50 |       |        | 5.9   | 16.6.3  |   |         |             |
| 127    |       |        | 5.8   | 16.6.4  |   |         |             |
| 127    | 0.588 | 172.34 | 5.69  | 16.6.46 |   | peg     | 127+00      |
| 126+50 |       |        | 5.6   | 16.6.7  |   |         |             |
| 126    |       |        | 5.4   | 16.6.9  |   |         |             |

17234

|        |      |        |      |        |
|--------|------|--------|------|--------|
| 125+50 |      |        | 5.1  | 167.2  |
| 125    |      |        | 4.6  | 167.7  |
| 124+50 |      |        | 3.5  | 168.8  |
| 0      | 8.30 | 177.88 | 2.76 | 169.58 |
| 124    |      |        | 8.4  | 169.5  |
| 123+50 |      |        | 7.0  | 170.9  |
| 123    |      |        | 6.4  | 171.5  |
| 122+50 |      |        | 5.6  | 172.3  |
| 122    |      |        | 3.5  | 174.4  |
| 121+50 |      |        | 2.9  | 175.0  |
| 121    |      |        | 1.7  | 176.2  |
| 0      | 12.7 | 189.41 | 0.64 | 177.24 |
| 120+50 |      |        | 1.9  | 176.5  |
| 120    |      |        | 12.6 | 176.8  |
| 119+50 |      |        | 10.4 | 179.0  |
| 119    |      |        | 11.3 | 178.1  |
| 118+50 |      |        | 10.7 | 178.7  |

Bottom of Basin of side hill  
 shows against rocks scattered about

on Rock line 124+50

on peak R.P. 120+50

189.41

|         |      |        |
|---------|------|--------|
| 118     | 10.1 | 179.2  |
| 117 +50 | 13.5 | 175.9  |
| 117     | 12.8 | 176.6  |
| 116 +50 | 11.1 | 178.3  |
| 116     | 9.4  | 180.0  |
| 115 +50 | 8.5  | 180.9  |
| 115     | 10.3 | 179.1  |
| 114 +50 | 9.0  | 180.4  |
| 114     | 8.5  | 180.9  |
| 0       | 8.47 | 180.94 |

on 7th 1' h 114+00

13.00 945.99 932.99

-T.R. page 3

85+04

939.3

x

+50

938.7

20  
2.50

86

938.9 938.1

+ 8.8  
- 0.5

+50

944.3 937.4

1.5

+69

+70

937.3

89

0.0

87 +15

936.6

94

0.0

8" paper

+25

1.8 944.2 936.4

+7.8 + 12.0  
4.0

12.0  
+4.0

+38

936.2

98

0.0

+50

936.0

x

8" paper

+70

935.2

109

88 +20

933.2

128

1  
F  
0

8" paper

0

1.21 934.93 12.27 933.72

page in grade 85+25

+50

932.0

29

+75

931.0

39

89

+30

929.8

6.1

934.93

89+50

934.1 928.0

69 + 6.1

632 934.61

927.7

= T.P. page 4

90+35

90

89+70

89+50

$$+ \frac{14.2}{6.2} + 4.3 + \frac{14.6}{3.6}$$

$$+ \frac{15.7}{10.7} + 7.4 + \frac{18.6}{5.4}$$

$$+ \frac{21}{13} + 8.1 + \frac{13.2}{5.2}$$

$$+ \frac{19.0}{11.3} + 2.1 + \frac{10.6}{2.9}$$

69

70

73

75

8.907

5.4

11.8

8.1

1.1

✓

6.3

1.9

0.3

6.2

93.4

93.3

10

963.21

490 972.11

80+50

1.3 970.8 9597

+75

53 966.8 9582

0

10.4 961.97

0.88 962.85

91

53 957.6 9567

+25

9552

7.7

82

131 49.8 9507

122

-09

+25

92 962.7 9501

+126

0

1.81 961.04

7.75 968.79

+50

33 9655 9495

+160

+75

57 963.1 9489

+142

93

10.1 9587 9481

+10.6

0

12.79 956.50

0.96 957.46

0

9.96 947.50

6-28-07.

R. W. West  
Mar Watson  
= BM 7 CVND line (north of big bench  
east of cut)

+ 11.11 grade for this station is 0.7'

+ 86.0' lower than in location by

reason of change of line

west of here

+09

N  
5'

0.1 947.61

947.50

7.3

940.4

= Sta 95+90 on finished road

95+50

941.4

6.2

95

6.3

940.9

942.7

4.9

94+50

5.1

942.5

944.0

3.6

-1.5

+25

944.6

3.0

94

6.1

947.5

945.3

2.3

+22

2

93+50

946.6

1.0

0

10.7

946.84

10.3

956.67

93

949.3

8.8

92+50

949.2

7.5

+25

949.8

6.9

92

950.5

6.2

| 27.  | Levels up | Contents of Cist |         |
|------|-----------|------------------|---------|
|      |           |                  | 1518.06 |
| 8.74 | 1526.80   |                  |         |
| 0    |           | 3.47             | 1523.33 |
| 9.62 | 1532.96   |                  |         |
| 0    |           | 11.20            | 1521.76 |
| 2.20 | 1523.96   |                  |         |
| 0    |           | 5.60             | 1518.36 |
| 5.49 | 1524.05   |                  |         |
| 0    |           | 0.51             | 1523.54 |
| 5.38 | 1528.92   |                  |         |
| 0    |           | 4.87             | 1524.05 |
| 3.68 | 1527.73   |                  |         |
| 0    |           | 10.83            | 1516.90 |
| 5.11 | 1522.08   |                  |         |
| 0    |           | 3.24             | 1518.84 |
| 0.70 | 1519.24   |                  |         |
| 0    |           | 11.29            | 1507.95 |
| 0.96 | 1508.81   |                  |         |

7-13-07

= B.M. at SW. cor Blacksmith Shop

P. Wilcox Sevelman  
Cassius Curtis Palmer

= Pl on Bldg opp Foreman's Stand

= peg on pt opp Indian Village

42.06  
51.31  
9.25

C 05



1508.51

561 1503.20

0.73 1502.93

125 1502.68

9.55 1512.23

0.55 1511.64

10.71 1522.44

160 1520.84

9.15 1529.99

0.50 1529.49

2.50 1527.49

10.49 1537.98

145 1536.53

5.70 1542.23

5.86 1536.37

6.45 1542.82

1.03 1541.79

0.15 1541.94

= 0.11 on Round Blt/ on Blt/indg  
 east / upper Indian camp

$$\begin{array}{r} 52.98 \\ 14.85 \\ \hline 33.13 \end{array}$$

29.

154.94

334 1538.60

7.62 1546.22

1129 1534.93

3.11 1528.04

8.04 1530.00

6.42 1536.42

4.72 1531.69

Branch up Pine Creek

9.46 1526.98

0.50 1527.48

14.11 1516.37

0.72 1517.09

11.59 1505.50

0.83 1506.33

7.60 1498.73

8.23 1506.96

2.07 1504.89

= Bill on round topped Bldg.

25' E, telephone post

27.43

64.48

87.65

CSD

49 1509.76

1504.89

O

0.62 1509.14

1.21 1510.35

D

7.62 1502.73

8.25 1510.98

2.51 1508.47

5.74 1505.24

= U.S.G.S. BM west of Pine Creek  
 gauge - marked "100"

= 10 feet mark on gauge itself  
 (atod 3.40 - 7-13-07)

6.60

1598.64 = w.s.

21.

Up letters of 10 Salazar's Ranch

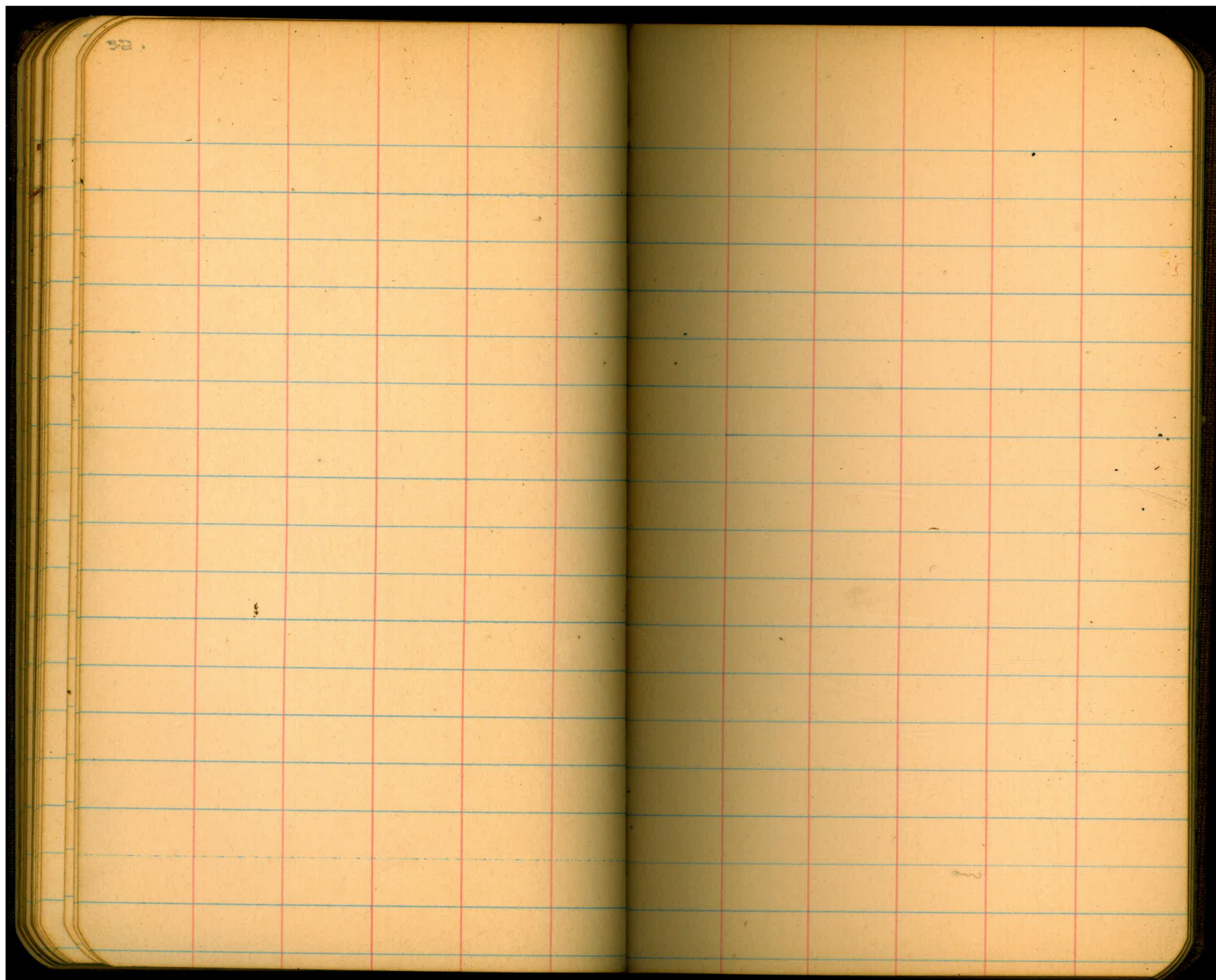
0.11 1531.80 1531.69

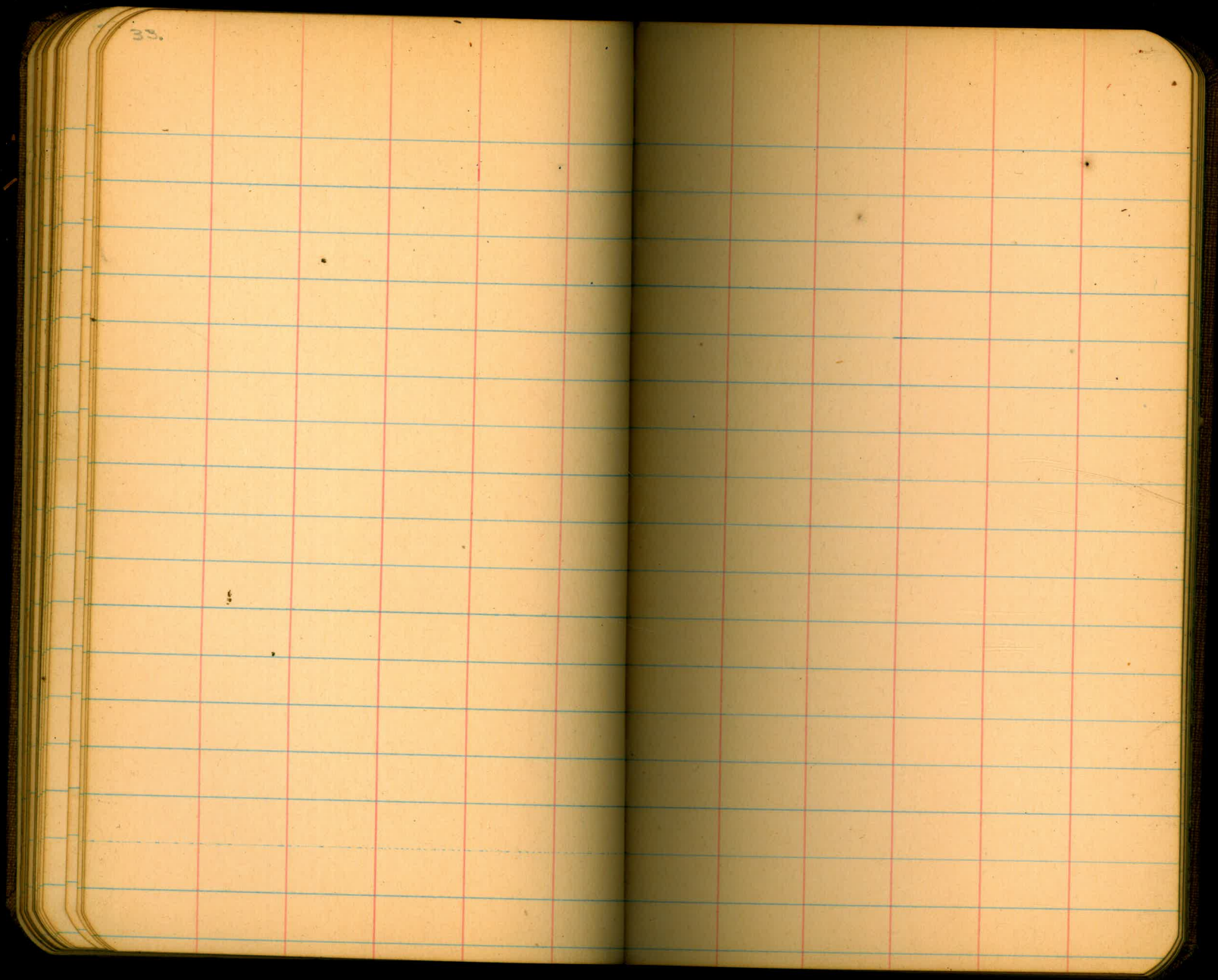
0 1150 1520.30

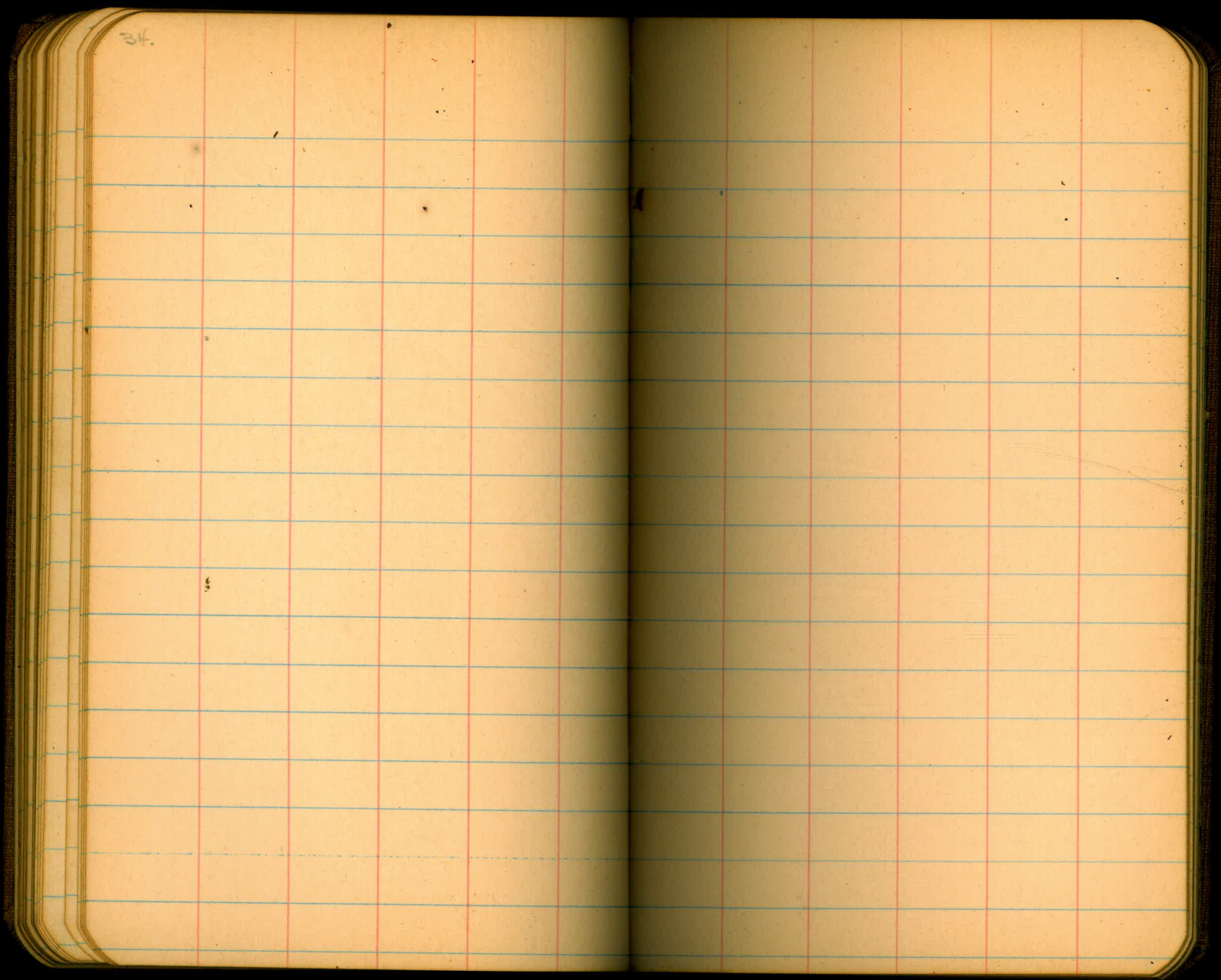
260 152290

0 1148 1511.42

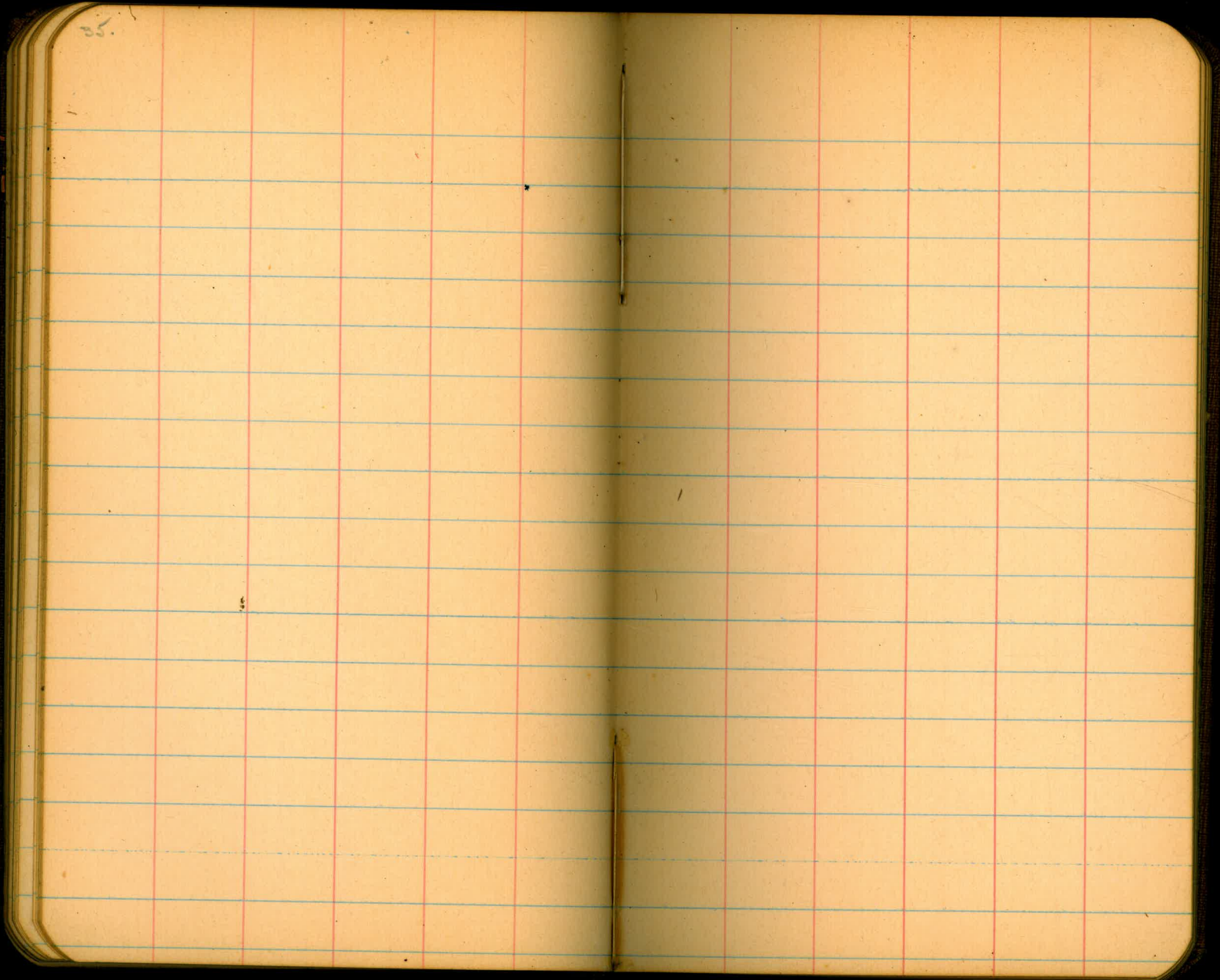
= PM Page 29.







24.

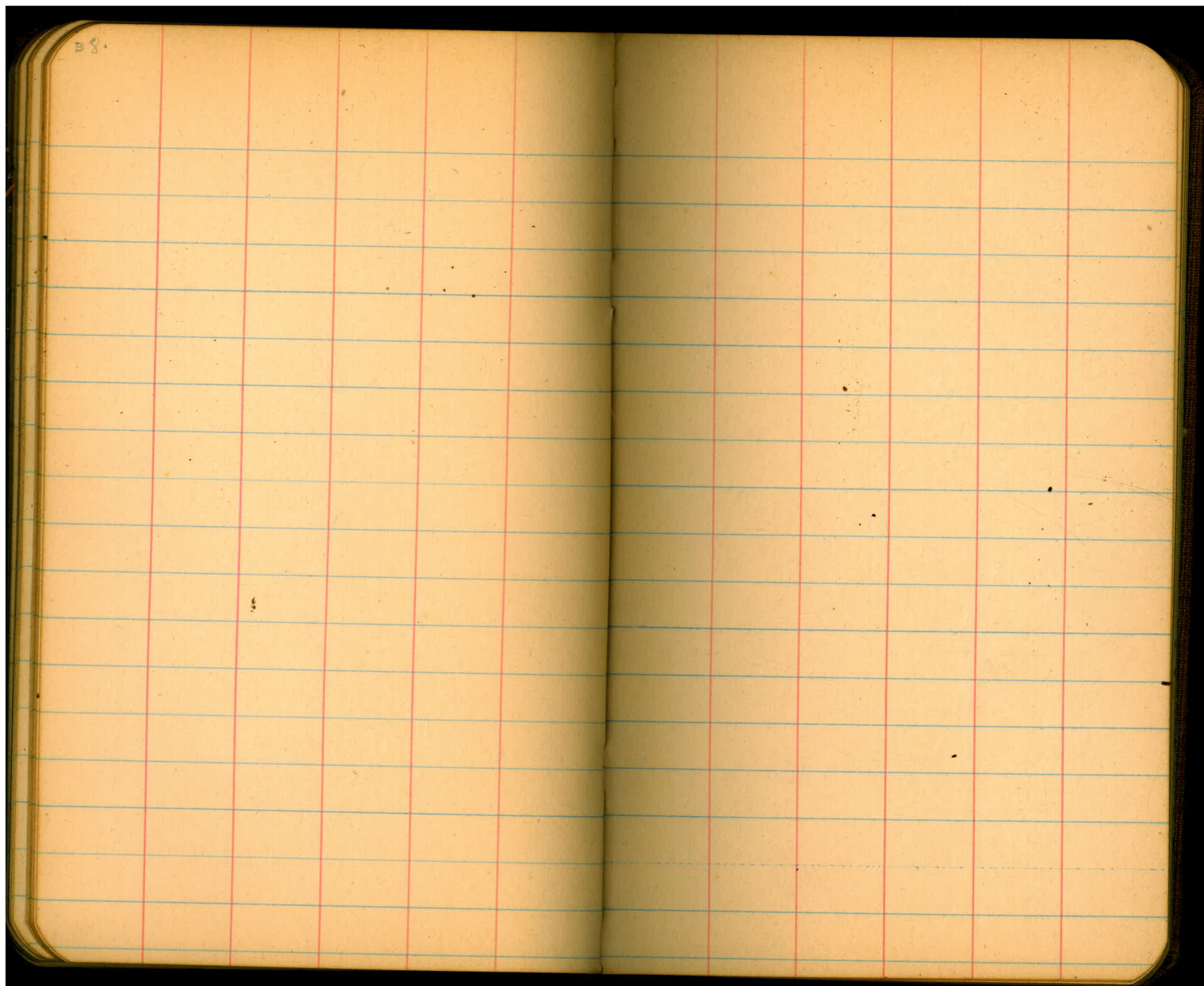




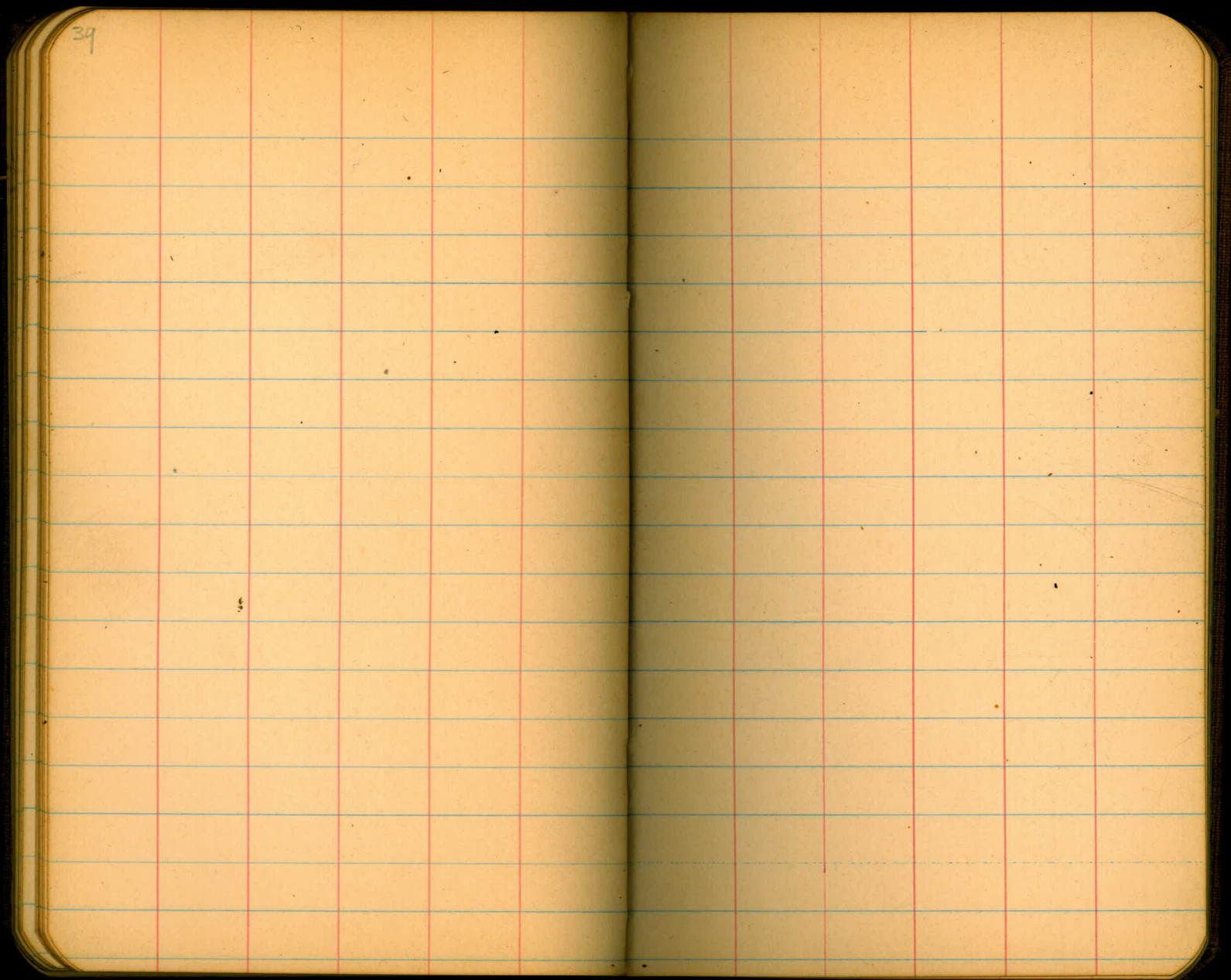
26.

27.

88.



39



740 change of value 42+00 to 45+00

|         |     |         |      |         |        |
|---------|-----|---------|------|---------|--------|
|         | 164 | 1172.57 |      | 117093  |        |
| √ 42+00 |     |         |      | 1170.0  |        |
| +50     |     |         | 3.3  | 1169.3  | 1168.0 |
| +79     |     |         | 7.2  | 1165.4  | 1166.8 |
|         | 188 | 1172.81 |      | 117093  |        |
| 43+33   |     |         | 8.1  | 1164.7  | 1164.7 |
| +50     |     |         | 8.8  | 1164.0  | 1164.0 |
| 0       | 488 | 1167.61 | 10.0 | 1162.73 |        |
|         |     |         | 56.5 | 1161.96 |        |
| 44      |     |         |      |         | 1162.0 |
| +50     |     |         |      |         | 1160.0 |
| 45      |     |         | 9.2  | 1158.4  | 1158.1 |

May 3<sup>rd</sup> 1907

= T.P. 42+10 'e' sin

|  |      |
|--|------|
|  | x    |
|  | +1.3 |
|  | -14  |

1170

= T.P. on √ sin

|  |     |
|--|-----|
|  | 5.6 |
|  | 7.6 |
|  | 9.5 |

R. W. W. W.  
 Max Watson  
 Ford Becke  
 Geo. Lane  
 P. Antoin  
 E. W. M. Moore

Th. Tying v "Line to N" wire

May 4<sup>th</sup> 1907

12.60 805.95

793.35

= T.P. page 47 Book I

V III

68

799.2

799.1

x

✓

P. Weston

+50

800.3

58

Max Watson

112

?

801.8

42

+

+

+

Ford Beebe

+33

3.3

802.7

802.6

3.4

= N 112 + 09

✓

Geo Sam.

R. Hutchins

E.W.M. Moss

42.

0 165 101.65 100

+50 36 98.1

1 49 96.8

+50 76

2 3

+50 106 91.1

0 159 91.96 115.8 90.07

3 88.1 39

+50 85.1 69

4 96 82.1 99 403

+50 79.1 129

0 226 81.29 129.3 79.03

5 76.1 5.2

+50 73.1 8.2

6 70.1 11.2

0 307 70.43 129.3 68.36

+50 67.1 3.3 63.1 y

61.1 9.3

91.1

626

23.5

7

91.1  
671  
240706  
8  
626706  
22.1  
73

43.

70.6

6+60

601

105

7

57.1

135

0

183

60 43

120

58.6

+50

54.0

64

8

51.0

94

+50

113

49.1

113

0

050

5206

893

51.50

9

45

46.1

59

202

3.14

1.58

202

1055

141.44

10.57

3.70

17.23

17.73

12.65

193.42

10.51

18287

12.10

10.17

6.98

212.12

19.39

192.73

204

3.14

1.58

202

1055

141.44

10.57

3.70

17.23

17.73

12.65

193.42

10.51

18287

12.10

10.17

6.98

212.12

19.39

192.73



2

3

15.

7

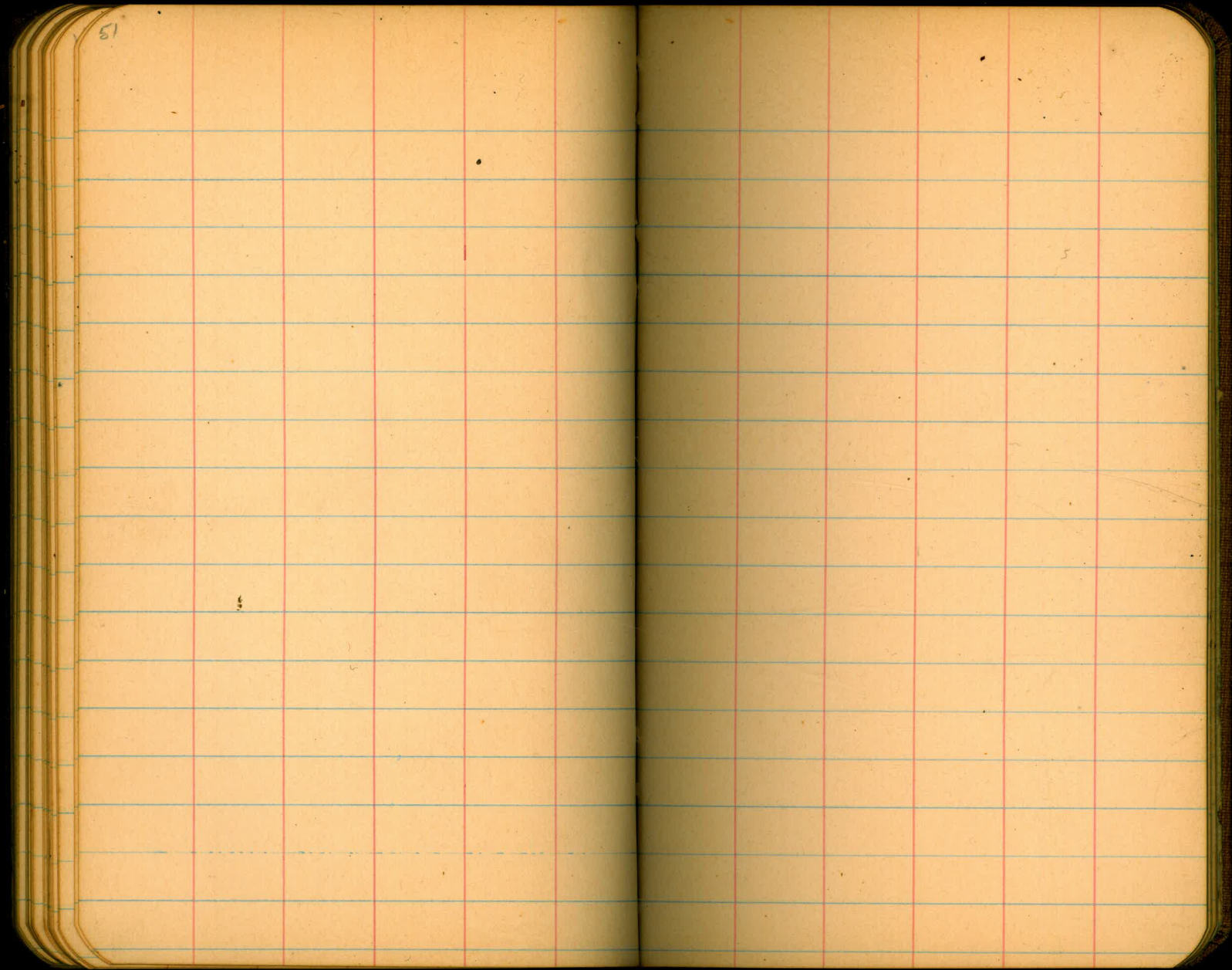
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47

48.

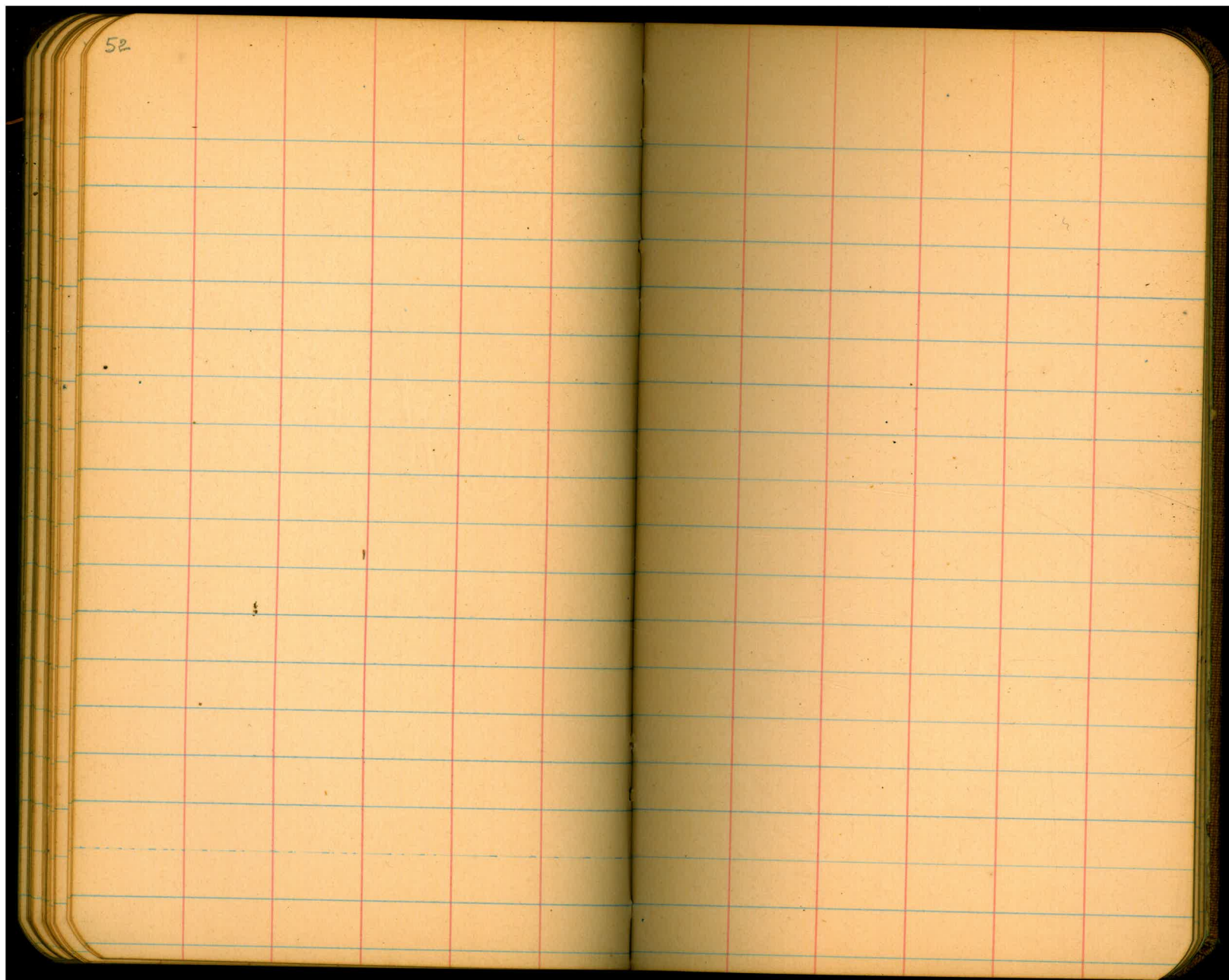
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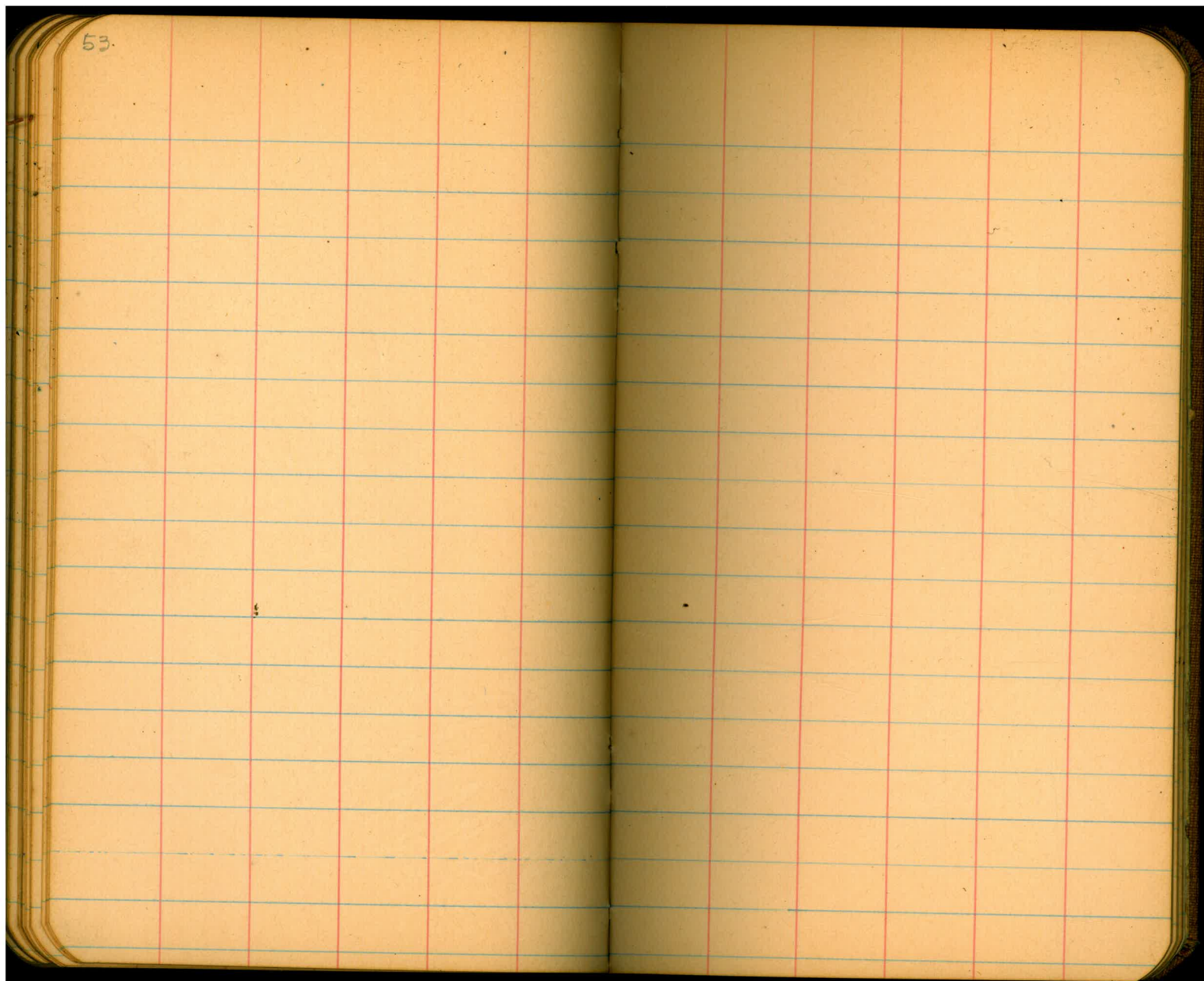
4 50.

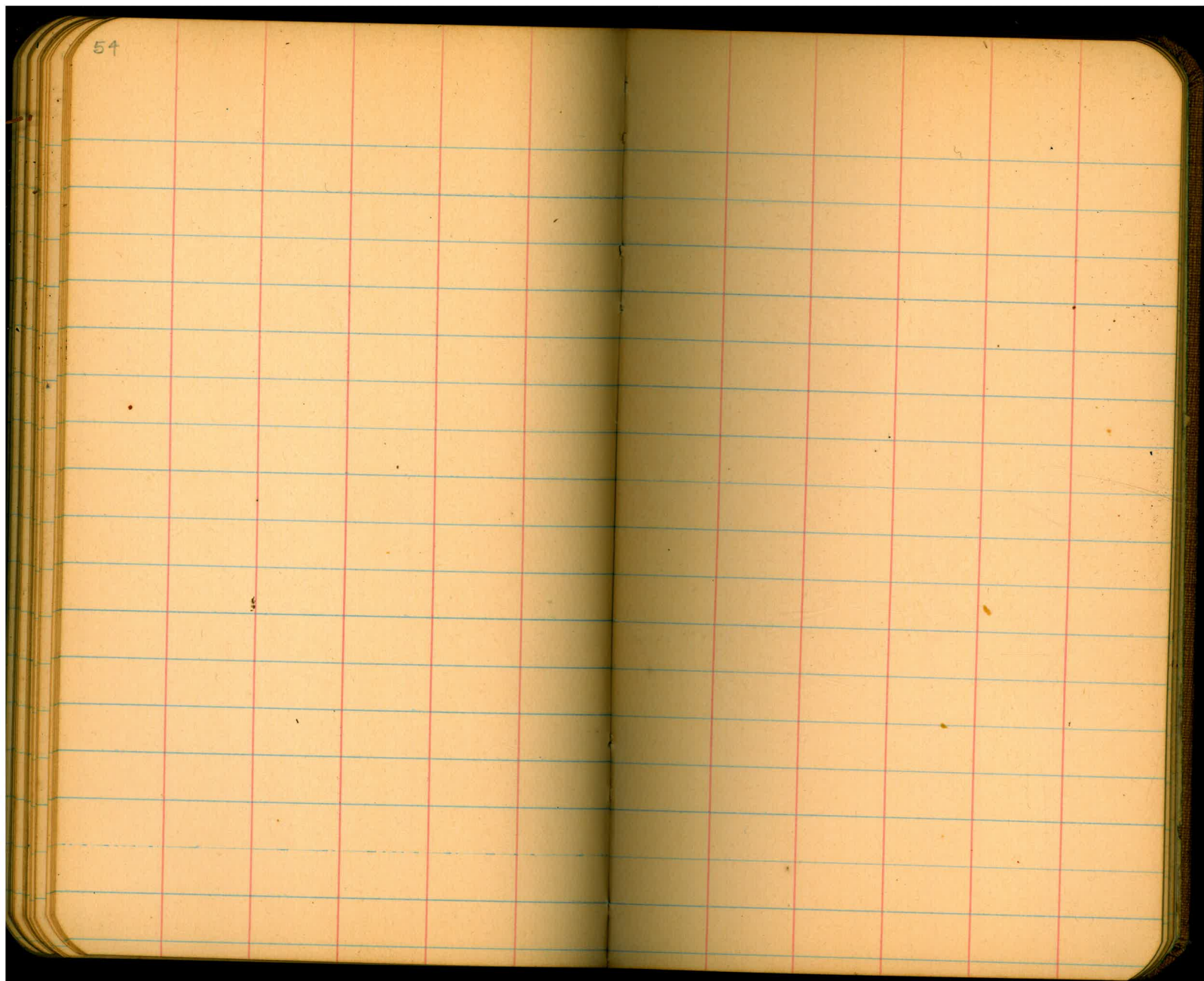


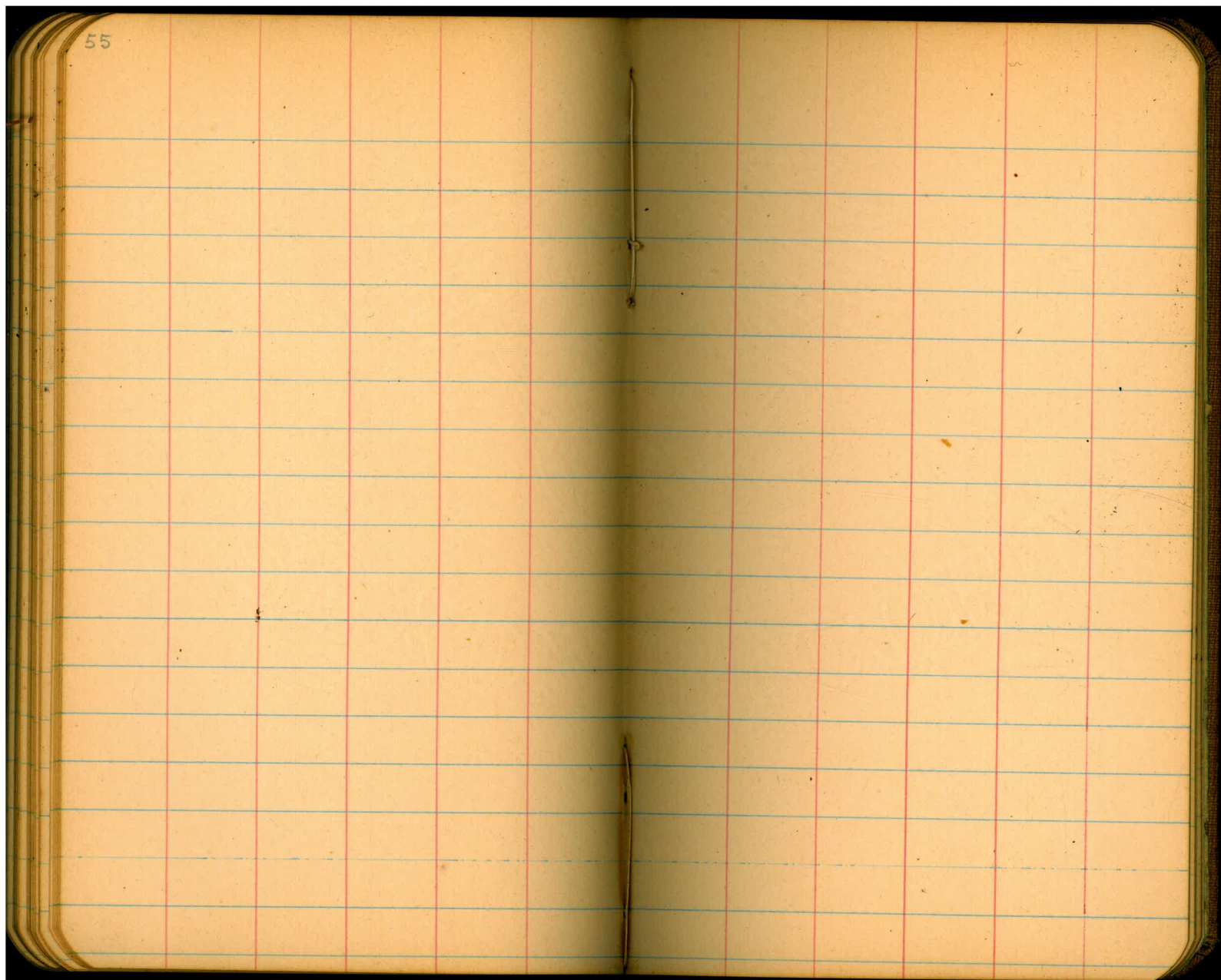
51

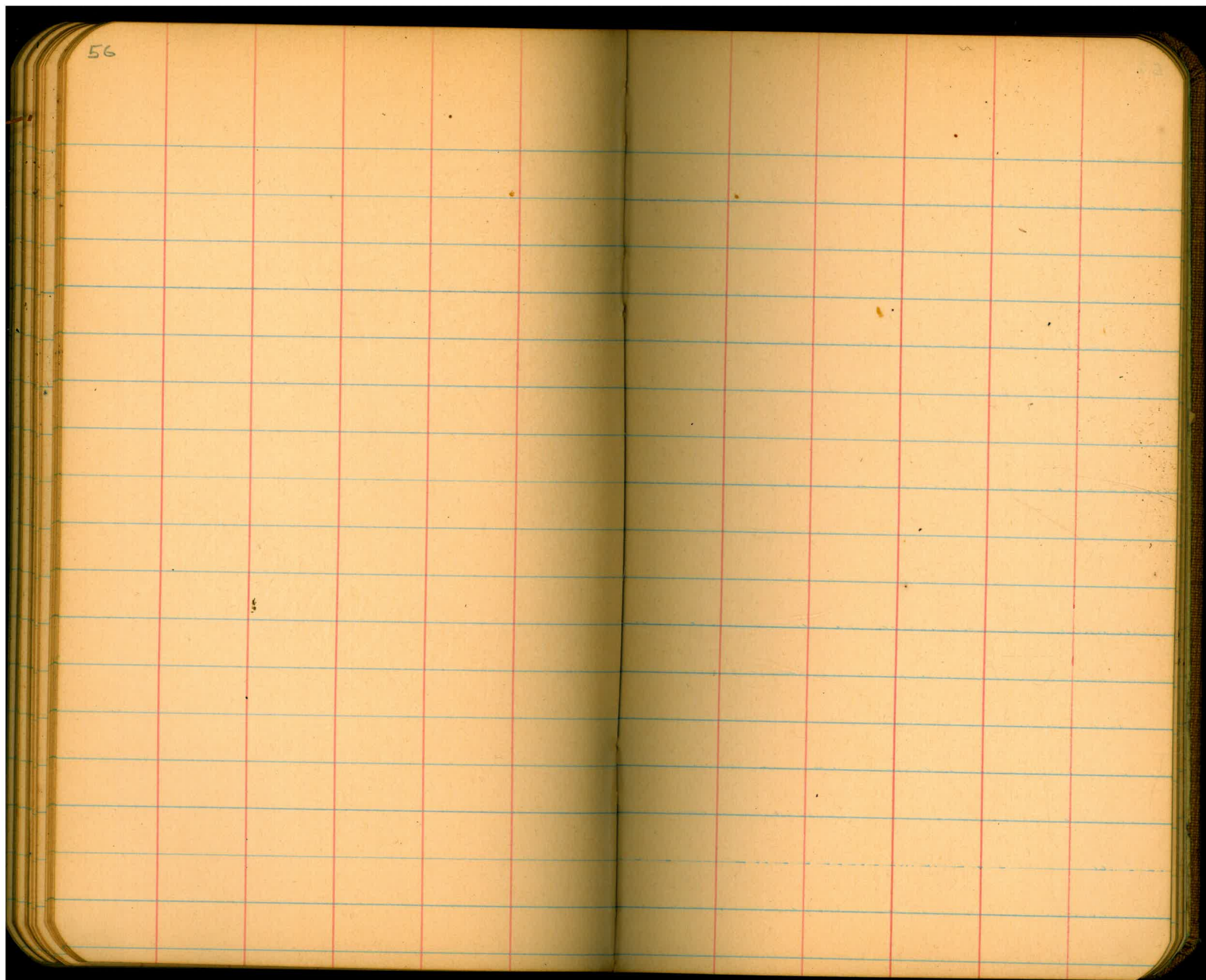


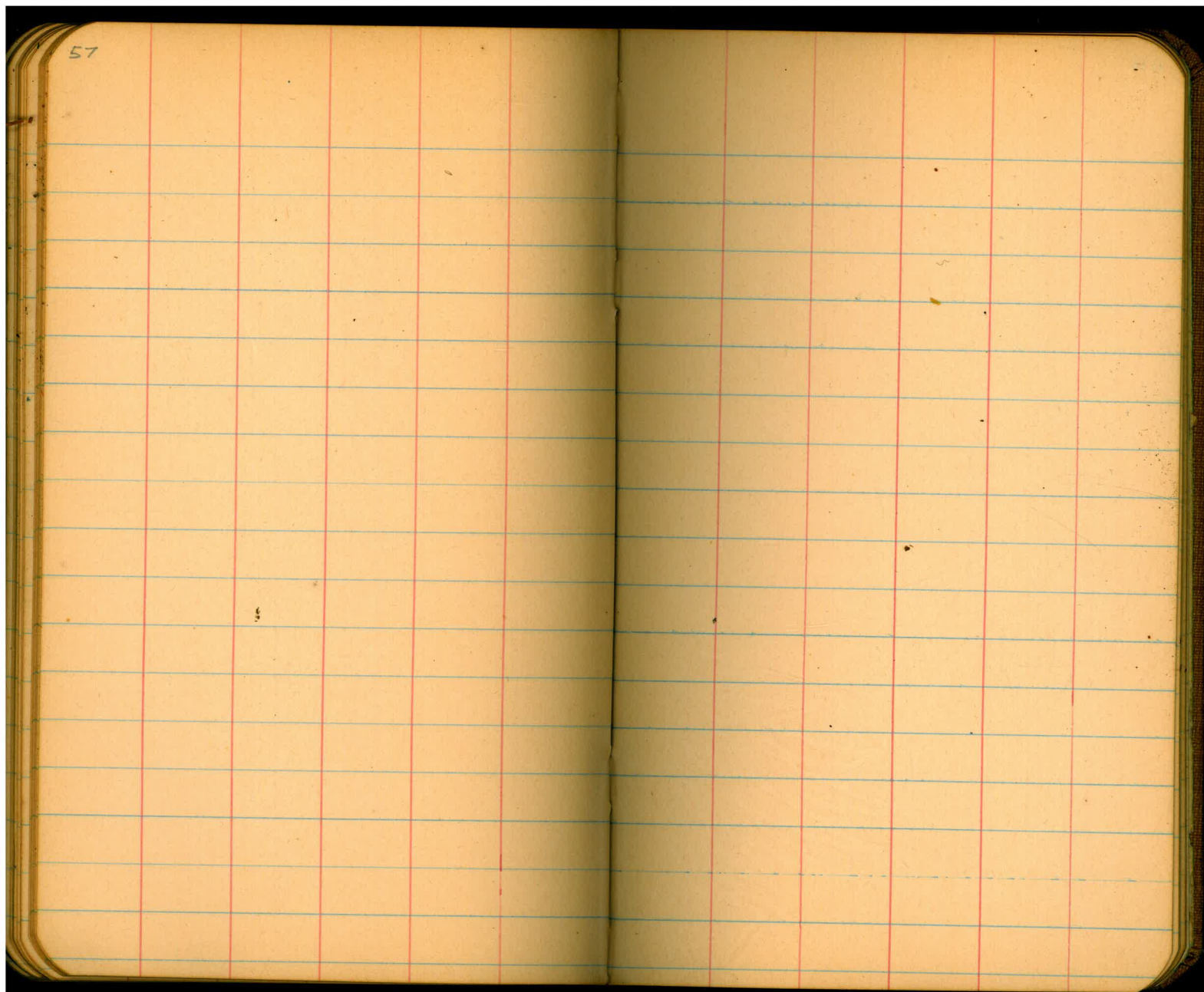




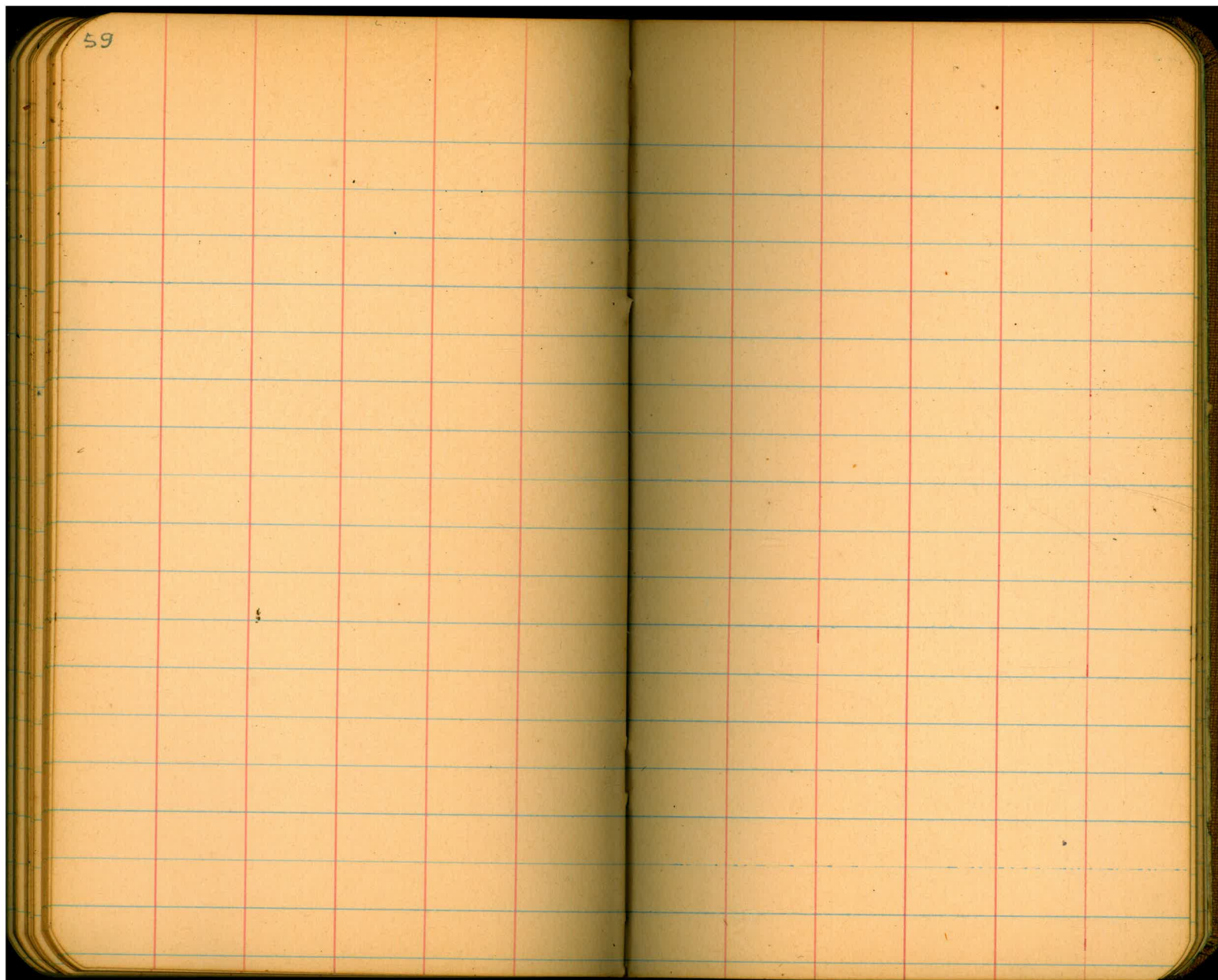






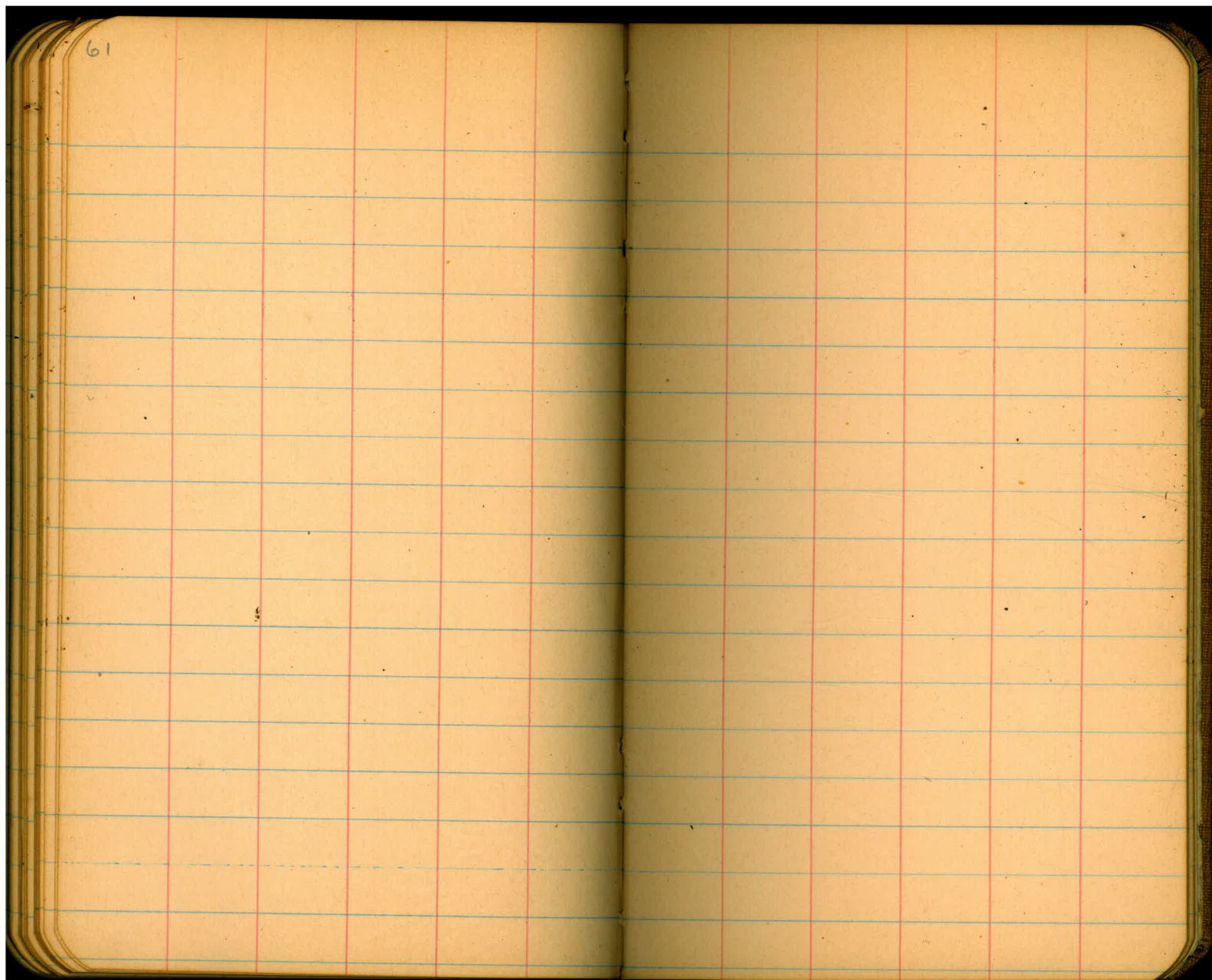








F 60



62

County Road -  
Audjuna Pass - Sheekles Valley

|       |     |      |             |
|-------|-----|------|-------------|
| 44+50 | 0.0 | 0.0  | E           |
| 45+50 | 4.5 | 15.0 | E-4.5, 10.0 |
| 46+50 | 6.0 | 11.0 | E           |

| Sta   | H    | B    |                 |
|-------|------|------|-----------------|
| 47+50 | 9.0  | 8.0  | E-30° Beds      |
| 48+50 | 9.0  | 12.0 | E-30° Beds      |
| 49+50 | 7.0  | 10.0 | E-30° Beds      |
| 50+50 | 6.0  | 9.0  | E-40° Beds      |
| 51+50 | 7.0  | 9.0  | 20° E+ Beds     |
| 52+50 | 11.0 | 10.0 | 40° Bed E       |
| 53+50 | 9.0  | 16.0 | Dis-gra         |
| 54+50 | 12.0 | 10.0 | Dis-gra         |
| 55+50 | 13.0 | 10.0 | 50° R (Dis-gra) |
| 56+50 | 8.0  | 9.0  | Q               |
| 57+50 | 8.0  | 11.0 | Q               |
| 58+50 | 7.0  | 10.0 | Dis-gra         |
| 59+50 | 11.0 | 12.0 | Dis-gra         |
| 60+50 | 4.0  | 8.0  | Dis-gra         |
| 61+50 | 6.0  | 10.0 | Dis-gra         |
| 62+50 | 7.0  | 11.0 | Dis-gra         |
| 63+50 | 11.0 | 8.0  | Dis-gra         |
| 64+50 | 7.0  | 10.0 | Dis-gra         |

| Sta   | H    | B    |                         |
|-------|------|------|-------------------------|
| 65+50 | 10.0 | 16.0 | 10° Beds Dis-gra Gulch  |
| 66+50 | 10.0 | 14.0 | 50° Beds (Dis-gra) R.R. |
| 67+50 | 4.0  | 9.0  | 50° Beds Dis-gra        |
| 68+50 | 6.0  | 10.0 | 10° Beds                |
| 69+50 | 4.5  | 10.0 | 20° Beds                |
| 70+50 | 7.0  | 11.0 | 20° Beds                |
| 71+50 | 3.0  | 8.0  | E                       |
| 72+50 | 3.0  | 10.0 | E                       |
| 73+50 | 2.6  | 10.0 | 20° Beds (Fault)        |
| 74+50 | 5.0  | 12.0 | 30° Beds (Dis-gra)      |
| +50   | 11.0 | 13.0 | Dis-gra                 |
| 75    | 9.0  | 10.0 | "                       |
| +50   | 17.0 | 8.0  | "                       |
| 76    | 13.0 | 13.0 | "                       |
| +50   | 20.0 | 14.0 | "                       |
| 77    | 16.0 | 15.0 | "                       |
| +50   | 14.0 | 11.0 | "                       |
| 78    | 13.0 | 10.0 | Dis-gra                 |

| 65           | County Road                  |      |                      | Sta | M         | B    |                 |
|--------------|------------------------------|------|----------------------|-----|-----------|------|-----------------|
|              | Dalyana Pass - Shukla Valley |      |                      |     |           |      | 65 1/2          |
| +50          | 8.0                          | 10.0 |                      |     |           |      |                 |
| 79           | 8.0                          | 12.0 | Dis Gra              |     |           |      |                 |
| +50          | 9.0                          | 8.0  | Dis Gra              |     |           |      |                 |
| +75          | 9.0                          | 11.0 |                      |     |           |      |                 |
| 80           | 8.0                          | 10.0 |                      |     |           |      |                 |
| +25          | 5.0                          | 11.0 |                      | 95  | 5.0       | 12.0 | R               |
| +29          | 8.0                          | 14.0 | Dis Gra              | 97  | 12.0      | 13.0 | R               |
| 80+50        | 0.0                          | 0.0  | R                    | 96  | 14.0      | 16.0 | R               |
|              |                              |      | 60 yds at this pt    | 95  | 8.0       | 11.0 | R               |
| at Sta 80+75 |                              |      | E Dis Gra 160 cu yds | 94  | 9.0       | 13.0 | R               |
| 3 +05        | 0.0                          | 5.0  |                      | 93  | 6.0       | 14.0 | Dis Gra         |
| +40          | 12.0                         | 19.0 | Dis Gra              | 92  | 0.0       | 0.0  |                 |
| +40          | 8.0                          | 11.0 | Dis Gra              | 91  | 22.0-12.0 | 20.0 | R (through cut) |
| 2            | 4.0                          | 9.0  | E                    | 90  | 6.0       | 8.0  | R               |
| +50          | 3.0                          | 6.0  | E                    | 89  | 12.0-5.0  | 20.0 | R (through cut) |
| 1            | 4.0                          | 6.0  | E                    | 88  | 6.0       | 10.0 | Dis Gra         |
| 0            | 0.0                          | 0.0  |                      | 87  | 6.0       | 12.0 | Dis Gra         |
| at Sta 84+50 |                              |      | R 30 cu yds          | 86  | 4.0       | 8.0  | Dis Gra         |

| Sta | H   | B    |                                |
|-----|-----|------|--------------------------------|
| 85  | 4.5 | 10.0 | R                              |
| 84  | 5.5 | 18.0 | Dis Gra                        |
| 83  | 5.6 | 10.0 | 70% R                          |
| 82  | 7.0 | 13.0 | 50% R 50% Dis Gra              |
| 81  | 4.0 | 7.0  | E                              |
| 80  | 4.0 | 9.0  | E                              |
| 79  | 6.0 | 8.0  | Dis Gra                        |
| 78  | 7.0 | 12.0 | Dis Gra                        |
| 77  | 7.4 | 16.0 | Dis Gra                        |
| 76  | 3.7 | 9.0  | E                              |
| 75  | 4.0 | 12.0 | E                              |
| 74  | 2.4 | 8.0  | 30% R                          |
| 73  | 3.0 | 9.0  | 30% R                          |
| 72  | 4.0 | 9.0  | E                              |
| 71  | 6.5 | 12.0 | Dis Gra                        |
| 70  | 7.5 | 12.0 | Dis Gra                        |
| +80 |     |      | = 106 + 5                      |
| 69  | 7.0 | 11.0 | Dis Gra (Finished to this Sta) |

| Sta | H   | B    |         |
|-----|-----|------|---------|
| 68  | 7.0 | 17.0 | Dis Gra |
| 67  | 0.0 | 0.0  |         |
| 66  | 8.0 | 16.0 | R       |
| 65  | 6.0 | 10.0 | Dis Gra |
| 64  | 8.0 | 12.0 | Dis Gra |
| 63  | 6.0 | 11.0 | Dis Gra |
| 62  | 2.6 | 10.0 | 50% R   |
| 61  | 2.0 | 8.0  | 40% R   |
| 60  | 2.0 | 6.0  | 40% R   |
| 59  | 2.4 | 9.0  | 10% R   |
| 58  | 2.0 | 9.0  | 20% R   |
| 57  | 2.0 | 8.0  | 50% R   |
| 56  | 3.0 | 10.0 | 50% R   |
| 55  | 4.2 | 11.0 | 50% R   |
| +50 | 0.0 | 0.0  |         |
| 54  | 1.8 | 7.0  | E       |
| +50 | 2.7 | 8.0  | E       |
| 53  | 0.0 | 0.0  |         |

67

| Sta | H   | B    |                         |
|-----|-----|------|-------------------------|
| 52  | 0.2 | 0.0  |                         |
| 51  | 0.0 | 0.0  |                         |
| 50  | 4.0 | 10.0 | L.P.                    |
| 49  | 0.0 | 0.0  |                         |
| 48  | 0.0 | 0.0  |                         |
| 47  | 0.0 | 0.0  |                         |
| 46  | 0.0 | 0.0  |                         |
| 45  | 0.0 | 0.0  |                         |
| 44  | 2.0 | 12.0 | L.P. W. antebach tunnel |
| 43  | 2.0 | 9.0  | E                       |
| 42  | 2.4 | 12.0 | E                       |
| 41  | 2.5 | 6.0  | E                       |
| 40  | 4.5 | 10.0 | E                       |
| 39  | 5.5 | 10.0 | Di-gra                  |
| 38  | 4.5 | 8.0  | Di-gra                  |
| 37  | 4.5 | 8.0  | Di-gra                  |
| 36  | 4.0 | 11.0 | L.P.                    |
| 35  | 1.8 | 10.0 | E                       |

| Sta | H   | B    |            |
|-----|-----|------|------------|
| 34  | 1.8 | 11.0 | E          |
| 33  | 1.5 | 8.0  | E          |
| 32  | 0.0 | 0.0  | E          |
|     | +75 |      | = 241 + 50 |
| 31  | 1.5 | 8.0  | E          |
| 30  | 2.0 | 9.0  | E          |
| 29  | 0.0 | 0.0  | E          |
| 28  | 2.0 | 8.0  | E          |
| 27  | 2.7 | 10.0 | 20% h.P.   |
| 26  | 2.0 | 7.0  | 30% h.P.   |
| 25  | 3.0 | 11.0 | 20% h.P.   |
| 24  | 3.0 | 11.0 | 30% h.P.   |
| 23  | 4.5 | 12.0 | 50% h.P.   |
| 22  | 1.0 | 6.0  | 30% h.P.   |
| 21  | 1.0 | 6.0  | E          |
| 20  | 2.5 | 6.0  | E          |
|     | +50 | 0.0  | 0.0 E      |
| 19  | 0.0 | 0.0  | E          |



| Sta | H   | B    |                   |
|-----|-----|------|-------------------|
| 18  | 0.0 | 0.0  | E                 |
| 17  | 0.0 | 0.0  | E                 |
| 16  | 0.0 | 0.0  | E                 |
| 15  | 1.5 | 6.0  | E                 |
| 14  | 1.5 | 10.0 | E (annular at 13) |
| 13  | 3.0 | 10.0 | WR                |
| +50 | 2.0 | 10.0 | LR                |
| 12  | 0.0 | 0.0  | E                 |
| 11  | 1.5 | 6.0  | E                 |
| 10  | 0.0 | 0.0  | E                 |
| 9   | 1.0 | 18.0 | E                 |
| 8   | 0.0 | 0.0  | E                 |
| 7   | 2.0 | 6.0  | E                 |
| 6   | 5.0 | 8.0  | E                 |
| 5   | 1.5 | 8.0  | E                 |
| 4   | 1.5 | 6.0  | E                 |
| 3   | 3.5 | 7.0  | E                 |
| 2   | 3.5 | 8.0  | E                 |

| Sta | H    | B    |   |
|-----|------|------|---|
| 1   | 1.25 | 9.0  | E |
| 0   | 0.0  | 0.0  | E |
| +16 | 0.0  | 0.0  | R |
| +50 | 3.0  | 13.0 | R |
| 5   | 8.0  | 14.0 | R |
| +50 | 24.0 | 28.0 | R |
| 4   | 10.0 | 18.0 | R |
| +50 | 10.0 | 15.0 | R |
| 3   | 1.5  | 12.0 | R |
| +50 | 2.5  | 9.0  | R |
| 2   | 7.0  | 12.0 | R |
| +50 | 10.0 | 14.0 | R |
| 1   | 7.0  | 12.0 | R |
| +75 | 2.5  | 11.0 | R |
| +50 | 4.0  | 9.0  | R |
| +25 | 3.5  | 8.0  | R |
| 0   | 0.0  | 0.0  | R |

= 174 + 50

Cottonwood  
April & May 1907.

|        |     |     |     |          |   |
|--------|-----|-----|-----|----------|---|
|        | 32  | 0   | 0   |          | R |
| 178+50 | 16  | 8.3 | 5   |          | R |
|        | 0   | 0   | 0   |          | R |
| 198+50 |     | 0   | 0   |          |   |
| 199    | 50  | 8   | 1.5 |          |   |
| 199+65 | 65  | 7   | 3.5 |          |   |
| 200    | 35  | 0   | 0   |          |   |
| +50    | 50  | 8   | 4.3 |          |   |
| 201    | 50  | 8   | 2   |          |   |
| 1+50   | 50  | 5.5 | 5.5 |          |   |
| 202    | 50  | 0   | 0   |          | E |
|        |     |     |     |          |   |
| 117    |     | 0   | 0   | = 204+70 |   |
| 115    | 200 | 0   | 0   |          |   |
| +30    | 70  | 0   | 0   |          | B |
| +20    | 10  | 11  | 2   |          | C |
| 114    | 20  |     |     |          |   |

|        |     |     |     |     |          |
|--------|-----|-----|-----|-----|----------|
| 113+35 | 65  | 18  | 1.5 | 1.5 |          |
| 113    | 35  |     |     |     |          |
| 112    | 100 |     |     |     |          |
| 111+50 | 50  |     |     |     |          |
| 111    | 50  |     |     |     |          |
| 110    | 100 | 0   | 0   |     |          |
| +75    |     |     |     |     | = 211+50 |
| +55    |     | 0   | 0   |     |          |
| 109    | 55  | 34  | 8   |     | E        |
| +50    | 50  | 8   | 3.5 |     |          |
| 108    | 50  | 8   | 3.5 |     | E        |
| 107    | 100 | 7   | 2   |     | C        |
| 106    | 100 | 5   | 1   |     | E        |
| 105    | 100 | 7.8 | 3.8 |     | R        |
| 104    | 100 | 8   | 7   |     | R        |
| 103    | 100 | 5   | 6   |     | R        |
| 102    | 100 | 9   | 4   |     | Dis      |

Road completed to 212+50

670

|        | sta   | Dist' | Width | Height   |   |
|--------|-------|-------|-------|----------|---|
| 178+50 | 101   | 100   | 12    | 5.3      |   |
|        | 100   | 100   | 14    | 5.5      |   |
|        | 99    | 100   | 11    | 6        |   |
| 19     | 98+60 |       | 0     | 0        |   |
| 19     | +80   | 80    | 0     | 0        |   |
| 19     | +50   | 30    | 19    | 4.8 1.5  |   |
| 2      | 97    | 50    | 15.5  | 8        |   |
|        |       |       | 8     | 5        |   |
|        | 96    | 100   | 11.5  | 2.7 36.5 |   |
|        |       |       | 8     | 6        |   |
| 26     | 95    | 100   | 10.5  | 30 38.5  |   |
|        |       |       | 5     | 5        |   |
|        | 94    | 100   | 13    | 15       |   |
| 21     | 93    | 100   | 11    | 8        |   |
|        | +30   | 70    | 8     | 5        |   |
|        | 92    | 30    | 10    | 7.5      |   |
|        | 91    | 100   | 9.5   | 5        |   |
|        | 90    | 100   | 7     | 1        |   |
|        | 89    | 100   | 7     | 1        | c |
| 11     | 88    | 100   | 9.5   | 1.5      | c |

|       |     |      |     |     |
|-------|-----|------|-----|-----|
| +35   | 65  | 9    | 5.5 | Dis |
| 87    | 35  | 10.5 | 8   | Dis |
| +30   | 70  | 13   | 12  | Dis |
| 86    | 30  | 8.5  | 2   | c   |
| 85    | 100 | 9    | 6.5 | Dis |
| 84    | 100 | 11   | 7   | Dis |
|       |     |      | 1.5 |     |
| 83    | 100 | 13   | 5   |     |
| 82+50 | 50  | 0    | 0   |     |
| 80    | 70  | 10   | 4   |     |
| 81+15 | 65  | 0    | 0   |     |
| +75   | 40  | 13   | 5   |     |
| 80    | 75  | 10   | 7.5 |     |
| +55   | 45  | 9.5  | 2.5 |     |
| +30   | 45  | 10.5 | 4.5 |     |
| 77    | 30  | 14.5 | 3   |     |
| +80   | 20  | 0    | 0   |     |
| 73+70 | 10  | 0    | 0   |     |

|       |     |      |     |
|-------|-----|------|-----|
| +50   | 20  | 10   | 2.5 |
| 78    | 50  | 8    | 1   |
| +80   | 20  | 12   | 2.5 |
| +65   | 75  | 0    | 0   |
| +45   | 20  | 0    | 0   |
| 77+40 | 5   | 9    | 2.5 |
| 76    | 140 | 8    | 2.2 |
| +65   | 35  | 11   | 2.5 |
| 75+30 | 35  | 0    | 0   |
| +50   | 80  | 0    | 0   |
| +20   | 30  | 13   | 2.7 |
| 74    | 20  | 11   | 1   |
| +50   | 50  | 6    | 1.5 |
| 73    | 50  | 11.5 | 6   |
| 72+25 | 75  | 9    | 4.5 |
| 71    | 125 | 11   | 5   |
| 70+40 | 60  | 12   | 9   |

|       |     |      |     |      |
|-------|-----|------|-----|------|
| 70    | 40  | 10   | 4.5 |      |
| +35   | 115 | 7    | 1.5 | =253 |
| 68    | 85  | 8    | 3   |      |
| 67+40 | 60  | 7    | 2.5 |      |
| +75   | 65  | 14   | 4   |      |
| +35   | 40  | 0    | 0   |      |
| 66    | 95  | 0    | 0   |      |
| +60   | 40  | 18   | 7   |      |
| +35   | 25  | 0    | 0   |      |
| 65    | 35  | 8.5  | 3   |      |
| +75   | 25  | 0    | 0   |      |
| 64+50 | 25  | 10.5 | 2   |      |
| +65   | 85  | 10.7 | 2.5 |      |
| +35   | 30  | 0    | 0   |      |
| 63    | 35  | 0    | 0   |      |
| +50   | 50  | 12   | 2.5 |      |
| 62    | 50  | 11   | 1.5 |      |

|       |     |     |     |
|-------|-----|-----|-----|
| 61+15 | 85  | 14  | 2.3 |
|       |     |     | 1.3 |
| +75   | 40  | 17  | 2.5 |
| +40   | 35  | 0   | 0   |
| 60    | 40  |     |     |
| +80   |     | 0   | 0   |
| +50   | 30  | 9   | 2   |
| 59    | 50  | 8.5 | 2   |
| 58    | 100 | 11  | 1.5 |
| 57    | 100 | 8   | .5  |
| 56    | 100 | 8   | .75 |
| 55    | 100 | 8   | 1   |
| 54    | 100 | 9   | 3.5 |
| 53+50 | 50  | 8.5 | 1.2 |
| 52    | 150 | 9   | 1.5 |
| 51    | 100 | 12  | 1.5 |
| +50   | 150 | 12  | 2   |
| 49    | 50  | 4   | 1   |

|       |     |      |     |
|-------|-----|------|-----|
| 48    | 100 | 11   | 2   |
| +50   | 50  | 18   | 2   |
| 47    | 50  | 10   | 2   |
| 46    | 100 | 10   | 4   |
| 45    | 100 | 6    | 3   |
| +60   | 40  | 7.5  | 3.5 |
| +30   | 40  | 0    | 0   |
| 44    | 20  | 11   | 5   |
| +50   | 50  | 12   | 4.5 |
| 43    | 50  | 7.5  | 3   |
| +60   | 40  | 10   | 4.5 |
| 42    | 20  | 6.5  | 4   |
| 41    | 100 | 10   | 3   |
| +60   | 40  | 11.8 | 3.2 |
| 40+35 | 25  | 0    | 0   |
| +65   | 50  | 0    | 0   |
| 39+50 | 35  | 27   | 5.5 |

Cont'd 15% S.F.

|       |     |      |      |
|-------|-----|------|------|
| +65   | 85  | 14   | 5    |
| 38    | 65  | 12.5 | 3.5  |
| +70   | 30  | 0    | 0    |
| +50   | 20  | 0    | 0    |
| +25   | 25  | 11   | 5    |
| 37    | 25  | 8    | 3.8  |
| +90   | 10  | 0    | 0    |
| +75   | 15  | 0    | 0    |
| 36+50 | 25  | 10.5 | 3.5  |
| +50   | 100 | 9    | 2.5  |
| 35    | 50  | 0    | 0    |
| +90   | 10  | 0    | 0    |
| +35   | 55  | 11   | 3.5  |
| 34    | 35  | 9    | 3.75 |
| 33    | 100 | 13   | 3.5  |
| +50   | 50  | 9    | 2    |
| 32    | 50  | 10   | 2.2  |

5%  
5%

|       |     |      |     |
|-------|-----|------|-----|
| +75   | 35  | 10   | 2.5 |
| +35   | 40  | 3    | 1   |
| 31    | 35  | 18   | 4.5 |
| +70   | 30  | 0    | 0   |
| +50   | 20  | 0    | 0   |
| 30    | 50  | 25   | 3.5 |
| +60   | 40  | 7    | 1.5 |
| 29    | 10  | 8    | 1   |
| +35   | 15  | 10   | 2.8 |
| 28    | 35  | 12   | 3.5 |
| 27+45 | 55  | 16   | 5.2 |
| 27    | 45  | 15.5 | 2.5 |
| 26+75 | 25  | 0    | 0   |
| 26+40 |     | 0    | 0   |
| +40   |     | 11   | 2   |
| 26    | 40  | 11   | 2   |
| 25    | 100 | 9    | 1.5 |

|       |     |      |      |
|-------|-----|------|------|
| 24    | 100 | 7.5  | 1    |
| +50   | 50  | 10.5 | 1.4  |
| 23    | 50  | 9.5  | 1.3  |
| +50   | 50  | 10   | 1.5  |
| 22    | 50  | 8.5  | 1.2  |
| 21    | 100 | 11   | 1.5  |
| 20    | 100 | 9.5  | 1.3  |
| 19    | 100 | 8.5  | 1    |
| 18    | 100 | 6    | 1    |
| 17    | 100 | 6    | 1    |
| +50   | 50  | 7    | 1.7  |
| 16    | 50  | 9    | 2    |
| +50   | 50  | 11   | 2.4  |
| 15    | 50  | 8    | 1.5  |
| 14    | 100 | 10   | 2.25 |
| 13    | 100 | 9.5  | 2    |
| 12+25 | 75  | 14   | 1.50 |

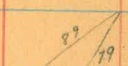
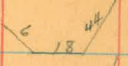
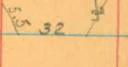

Cottonwood Camp  
Barrett Road  
Job #42  
June 3 1907

|       |     |      |      |
|-------|-----|------|------|
| 12    | 25  | 9    | 1.5  |
| 11+45 | 55  | 5    | .75  |
| 11    | 45  | 9    | 1.5  |
| 10    | 100 | 6.75 | 1.75 |
| 9     | 100 | 5    | .75  |
| 8     | 100 | 8    | 2    |
| 7+75  | 35  | 11.5 | 3    |
| 7     | 75  | 9.5  | 2.5  |
| 6     | 100 | 7    | 1.5  |
| 5     | 100 | 7    | 1.5  |
| +50   | 50  | 8.5  | 2.4  |
| 4+60  | 50  | 10.5 | 2    |
| 3+45  | 55  | 11   | 1.5  |
| 300   | 45  | 8    | 1    |
| 200   | 100 | 7    | 1    |
| 100   | 100 | 8    | 1.1  |
| 0     | 100 |      |      |

Junction with County Rd.

BARRETT CAMP  
May 1907.

## Cottonwood Canon Road Measurement.

| Sta.    | Dist. | Width | Height<br>(ft) |                                                                                     |
|---------|-------|-------|----------------|-------------------------------------------------------------------------------------|
| 52 + 05 | 30    | 17    | 39             |  |
| + 15    | 10    |       |                |  |
| 52 + 55 | 40    |       |                |  |
| 53 + 10 | 55    | 16    | 21             |                                                                                     |
| 54 + 10 | 100   | 15    |                |  |
| 54 + 80 | 70    | 12    | 20             | R.                                                                                  |
| 55 + 80 | 100   | 12    | 18             | R                                                                                   |
| 56 + 80 | 100   | 15    | 28             | R                                                                                   |
| 57 + 80 | 100   | 19    | 18             | R                                                                                   |
| 58 + 45 | 65    | 22    | 11             | Dis                                                                                 |
| 58 + 75 | 30    | 0     | 0              |                                                                                     |
| + 90    | 15    | 0     | 0              |                                                                                     |
| 59 + 35 | 45    | 12    | 28             | Dis                                                                                 |
| 59 + 95 | 60    | 10    | 7              | Sig                                                                                 |
| + 30    | 35    | 15    | 22             | Sig                                                                                 |
| 60 + 65 | 35    | 19    | 13             | Sig                                                                                 |
| 61 + 65 | 100   | 7     | 18             | L. R.                                                                               |

51 + 38

0

0

(57)

90

78

51 + 75

37

16



|       |     |      |                            |                            |      |
|-------|-----|------|----------------------------|----------------------------|------|
| 62+30 | 65  | 16   | 16.5                       | $\frac{11.5}{16} \cdot 19$ | Dis  |
| 62+55 | 35  | 14   | 21                         |                            | L.R. |
| 63    | 45  | 7    | 7                          |                            | L.R. |
| 63+20 | 20  | 0    | 0                          |                            |      |
| 64    | 30  | 0    | 0                          |                            |      |
| 63+40 |     | 0    | 0                          |                            |      |
| 63+60 | 20  | 7    | $\frac{(37)}{41} \cdot 45$ |                            | L.R. |
| 64    | 40  | 15   | 16                         |                            | L.R. |
| 65    | 100 | 8    | 5                          |                            | E.   |
| 66    | 100 | 10   | 10                         |                            | E.   |
| 67+55 | 55  | 16.6 | 16                         |                            | Ley  |
| 67+90 | 35  | 0    | 0                          |                            |      |
| 67+40 | 50  | 0    | 0                          |                            | E.   |
| 68+15 | 75  | 11   | 11                         |                            | E.   |
| 69+15 | 100 | 13   | 11                         |                            | Ley  |
| 70+15 | 100 | 12.5 | 18                         |                            | Dis  |

|       |     |      |      |  |      |
|-------|-----|------|------|--|------|
| 70+45 | 30  | 7    | 9    |  | Dis  |
| 71+00 | 55  | 16.7 | 14   |  | Ley  |
| 71+45 | 45  | 0    | 0    |  | L.R. |
| 71+90 | 45  | 13.5 | 16   |  | L.R. |
| 72+30 | 40  | 10   | 13   |  | R.   |
| 72+75 | 45  | 0    | 0    |  | R.   |
| 73    | 25  | 13   | 18   |  | R.   |
| 73+60 | 60  | 12   | 18   |  | R.   |
| 74+60 | 100 | 10.5 | 14   |  | R.   |
| 75+35 | 75  | 11   | 17   |  | R.   |
| 75+90 | 55  | 9    | 12.5 |  | E.   |
| 76+35 | 45  | 8    | 3.5  |  |      |
| 76+80 | 45  | 13   | 10   |  |      |
| 35    | 55  | 14   | 12   |  | Dis  |
| 77+75 | 40  | 9.5  | 7    |  | R.   |
| 78+05 | 30  | 16   | 15   |  | R.   |
| 78+30 | 25  | 14   | 16   |  | Dis  |

3

|         |    |      |                      |      |          |    |                      |                                            |
|---------|----|------|----------------------|------|----------|----|----------------------|--------------------------------------------|
| 77      | 70 | 12   | 15                   | L.R. | 86 + 06  | 0  | 0                    | Dis                                        |
| 79 + 50 | 50 | 11.7 | 8.4                  | Dis  | + 23     | 0  | 0                    |                                            |
| 80 + 15 | 65 | 12   | 9                    | Dis  | 86 + 58  | 35 | 3.5                  | $\frac{21}{2} \frac{16}{1} \frac{4}{10.5}$ |
| 80 + 65 | 50 | 13   | 8                    | Dis  | 86 + 58  | 0  | 0                    |                                            |
| 81 + 15 | 50 | 7    | 3.5                  | Dis  | 86 + 85  | 15 | 21.8 <sup>(10)</sup> | 34                                         |
| 81 + 75 | 60 | 21.7 | 6.7                  | Dis  | 87 + 05  | 20 | 10.3                 | 5                                          |
| 82 + 30 | 55 | 0    | 0                    |      | 87 + 0.5 | 0  | 0                    |                                            |
|         |    |      |                      |      | + 25     | 15 | 16 <sup>(9.5)</sup>  | 27.5                                       |
| 82 + 95 |    | 0    | 0                    | Dis  | + 60     | 35 | 0                    | 0                                          |
| 50      | 35 | 5.5  | <sup>(13)</sup> 13.4 |      | + 55     | 0  | 0                    | 30.7                                       |
| 83 + 61 | 11 | 12   | 8                    | Dis  | + 75     | 20 | 9.0                  | 6.8                                        |
| 83 + 61 |    | 0    | 0                    |      | 88       | 25 | 9.0                  | 3.7                                        |
| + 33    |    | 0    | 0                    | Dis  | + 50     | 50 | 10.6                 | 3.5                                        |
| + 58    | 25 | 18   | 10                   | Dis  | 89 + 00  | 50 | 7.4                  | 3.4                                        |
| + 90    | 32 | 12   | 15.4                 | Dis  | + 50     | 50 | 7                    | 3.5                                        |
| 85 + 50 | 60 | 9.1  | 3.3                  | Dis  | 90 + 00  | 50 | 7                    | 3.2                                        |
| 85 + 80 |    | 6    | 3                    |      | 90 + 35  | 35 | 0                    | 0                                          |



Illustration of Sta 87+25

75

Placing Bunches on C-V-N-D line

May 11, 1907.

Bms undulating on QR

0.50 1234.92 1234.42

= T.P. at 32+35 C him page 53

BM 1

294 1231.98

opp. 33+25 on Rock bottom of rock face

Rock I

0 0.50 1222.57 1222.07

R. West

0 1.14 1211.25 1210.11

Ford Beebe

0 0.06 1199.76 1199.70

Geo. Lane

BM 2

4.17 1195.64

on Boulder in water gulch - painted

(Pinned)

0 0.69 1187.52 1186.83

0 0.35 1174.99 1174.64

BM 3

8.89 1166.10

on Boulder north of other boulders

0 2.45 1165.28 1162.83

3.55 1161.73

= T.P. on V him #3+94 on Rock 1161.74

0 1.31 1154.51 1153.20

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Rock I

0 2.40 1144.45 1142.05

BM 4

4.84 1139.61

on Boulder (Rocky Point) 48+78

continued June 29-07

R. West, Max Weber, and man

0.31 1139.92 1139.61

0.47 1128.09 1127.62

0.57 1116.24 1115.67

1116.24

1.15 1105.76 1263 1103.61

0.87 1098.63 1200 1092.76

Bm 5 1.71 1084.42 1092 1082.71 on Rock

1.01 1072.44 1199 1072.43

0.91 1063.20 1115 1062.29

0.47 1051.50 1217 1051.03

1.79 1040.91 1188 1039.62

Bm 6 9.17 1031.73 on Bed in Chapter

0.74 1028.89 1276 1028.15

0.69 1017.41 1217 1016.72

1.30 1007.25 1146 1005.95

0.98 996.67 1236 994.69

1.55 984.77 1245 983.22

2.65 976.99 1043 974.24

Bm 7 1.20 965.15 1278 963.21  
1304 963.95

1.15 953.99 1231 952.84

0.99 942.39 1209 941.40

Bm 8 9.47 932.92 ✓  
1194 930.45on Rock north of boulder  
at Boulder gate

(932.99 on summit of Road) - T.P. at 96+03 - Trial Run

1.15

1116

11

0.87

10

Bm 5

171

1.01

0.91

0.47

17

Bm 6

Bm 7

0.99

942

Bm 8

947

1197 930.45



