

Mean High Tide
Redin Dam Survey

W 166

LEVEL BOOK

380

J.W. Williams Const. Eng
City Hall

MICROFILMED

JAN 8 1965

Harstinau - Regr.

Index

| | |
|---|-------|
| Levels from Quarantine Sta. to La Playa | 1-12 |
| Levels from U.S.G.S. Bench to Axis of Roden Dam site - - - - - | 13 |
| Levels from beginning of Siphon #2 along Conduit - - - - - | 14-64 |
| Profile thru cut 334+50 to Proposed Flume from Roden Dam | 73 |
| Profile thru cut Sta. 238+00. to 240+50. | |
| P, Proposed Flume from Roden | 74 |
| Middle town B.M.s: | 75 |

July 28-1921

1. View South toward J. H. W. Steels (Hermitage ranch) on Spritt ranch showing character of soil
2. View south on N. ranch showing cultivated field
3. View of iron pipe on N. side of N. ranch 2 inch pipe disch. to surface.
4. Lower Darrin - 4" pipe painted Capac Res road level 18 m. S.
400 ft. or below

5. Row of 8 wells 10 to 15' deep
Water within 3' of surface and
surging in today - 2 gal
required

1 Well east of N.P. coupled to
(belt drive) Gould 5x5 size
pump & one to H.P.W. east
of E. coupled (belt drive)
to Byron Jackson centrif
Pump 3 stage

6. Near Dam above House

7. View N. from mine guffel

River, all ground in foreground
irrig

8. House

9. West from cow yard - canal
tank - see fence

Levels from Tidal 1" Quarantine
Station La Playa.

B.M.

8.721

| Sta | + | ⊖ | - | Elev. |
|---|-------|--------|------------|--------|
| | 5.440 | 14.161 | | |
| On Tidal B.M. Con. Block 12" square Marked 1906 on top square Top 1/50 N.W. U.S.G.S. map of Store Room U.S.G. Station U.S.G.S.T.P. | 0.950 | 13.462 | T.P. 1.649 | 12.512 |
| | | | T.P. 6.860 | 6.602 |
| | 3.930 | 10.532 | | |
| On Tidal B.M. Con. Block 12" square 30' N.W. of Marked U.S.G.S. La Playa Wharf 1906 | | | 4.330 | 6.202 |
| | 4.340 | 13.061 | | |
| T.P. | | | 6.750 | 6.311 |
| | 3.738 | 10.049 | | |
| T.P. | | | 6.220 | 3.829 |
| | 4.655 | 8.484 | | |
| T.P. | | | 5.175 | 3.309 |
| | 4.510 | 7.819 | | |
| T.P. | | | 3.800 | 4.019 |
| | 6.055 | 10.074 | | |
| T.P. | | | 6.330 | 3.744 |

B.M. Tidal 1" La Playa

8.721

J. W. Williams Level
Jack Sights Rod

June 15 - 1922

Quarantine Station north of Point Loma U.S. Coast
and Geodetic Survey benchmark "Tidal 1" granite
Block 10 inches square on top marked U.S. (north side
marked "Ref. mark" east side marked "Coast Survey
south side (Marked "1853-54-55") North side (Marked
"for tide, latest value

8.721

2.02 is 10 ft toward bay from point

on top of lead in center of Con. Mass 10" sq. located
on Military Reservation line 59' SE. of U.S. M.R. Stone

sta + π - Elev. B.M.
3.744

3.400 7.144

558

2.02 1.44 to bay from Hub.

557 on Highest point of granite Mon. 2.935 4.209 4.209

2.02 2.2 to " from point 1.0 Left of Hub. of Owen St.

556 5.124

2.02 1.3 to Rt of Hub. Record 1.0.9.14 of 0.9.14

555 5.124

2.02 1.5 to Lt of Hub (OK.)

T.P. T.P. 0.920 6.224 6.224

Set Nail in Cor. Wood Retaining wall N. Side Owen St.

11.938 18.162 0.625 17.537

12.025 29.562 0.205 29.357

11.815 41.172 0.452 40.720

11.975 52.695 0.374 52.321

6.090 58.411 4.305 54.106

U.S.G.S = 54.106
Brass Plug in Carb S.E. Owen St City Elev = 48.069
Difference 6.037

Starting from B.M. Owen St 6.224

0.350 6.574 2.940 3.634

6.220 9.854 6.550 3.304

4.410 7.714 5.694

543+00

542+56.62

2.02 3.0 to Rt of Hub. instead of 0.2 Rt

2.02 8.5 to Lt of Mon (OK Record)

542+56.62 on Gr. Mon High Point 4.110 3.604 3.604

7.144
2.020
5.124

7.714
2.020
5.694

2

U.S.G.S Elev of
M.H.W.

J.W. Williams
Jack Sites

6.839
2.020
4.819

7.254
2.020
5.234

8.841
2.020
6.821

3

| Sta | + | - | Elev. | B.M. | U.S.G.S. Elev | M.H. Water |
|------------------|-------|--------|-------|-------|---------------|--|
| | | 7.714 | | | | 2.02 |
| 542+00 | | | 5.694 | | | 2.02 Hit on Hub. (0.0 OK Record) |
| | T.P. | 5.850 | 1.864 | | | |
| | 4.800 | 6.664 | | | | |
| T.P. | | 4.010 | 2.654 | 2.654 | | on lead in com. mon. South line of Gay Place + Shoreline |
| | 4.600 | 7.254 | | | | |
| | | | 4.530 | 2.724 | | on lead in Com. Mon. North Line of Gay Place + Shoreline |
| 534+00 | | | 5.234 | | | 2.02 checks 1.0 to Rt of Hub. (OK) |
| 533+00 | | | 5.234 | | | 2.02 " 21.6 to Lt of Hub (OK) |
| 532+01.51 | | | 5.234 | | | 2.02 " 55.9 to Lt of Mon. (Record 53.9) |
| | T.P. | 4.515 | 2.739 | | | |
| | 4.100 | 6.839 | | | | |
| | 4.534 | 6.961 | | | | |
| | | | 4.410 | 2.429 | | |
| | | | 2.030 | 4.931 | 4.931 | B.M. on S.E. Cor. of Con. Shore Wall Jennings Place |
| | | | | | | End of June 15-1922 |
| Begin June 16 | 4.815 | 9.746 | | | | B.M. on N.E. Cor of Con Shore Wall Jennings Place |
| | | | 4.285 | 5.461 | 5.461 | |
| | 7.310 | 12.771 | | | | |
| | | | 4.350 | 8.421 | | |
| | 3.325 | 11.746 | | | | |
| | | | 4.160 | 7.586 | | |
| | 4.530 | 12.116 | | | | |
| | | | 4.045 | 8.071 | | |
| | 3.045 | 11.116 | | | | |
| | | | 6.020 | 5.096 | | |
| on Top | 3.745 | 8.841 | | | | B.M. |
| Gr. Mon 493+92.7 | | | 6.285 | 2.556 | 2.556 | |
| 493+92.7 | | | 6.821 | | | 2.02 1.5 Rt of Mon OK Record |

| Sta | + | π | - | Elev. | BM | Elev USGS. M.H. Water | |
|----------------------------|-------|---------------------|-------|--------|--------|-------------------------------------|---|
| | | 8.841 | | | | | |
| 493+00 | | | 6.821 | 6.821 | | 2.02 | (29.6 Rt of Hub. Schuyler) 34.2 Rt checked |
| 492 | | | 6.821 | 6.821 | | 2.02 | 44.8 Rt of Hub ") 45.8 Rt checked |
| | | T.P | 6.375 | 7.466 | | | |
| | 3.970 | 6.436 | | | | | |
| 490 | | | 4.416 | | | 2.02 | 48.4 Rt of Hub ") 52.1 Rt checked |
| 489 | | | 4.416 | | | 2.02 | 41.3 Rt of Hub ") 49.4 Rt checked |
| 488 | | | 4.416 | | | 2.02 | 30.5 Rt of Hub ") 42.3 Rt checked |
| 487 | | | 4.416 | | | 2.02 | 24.0 Rt of Hub ") 28.8 Rt checked |
| 486 | | | 4.416 | | | 2.02 | 7.8 Rt of Hub ") 14.7 Rt checked |
| | | T.P | 4.650 | 7.786 | | | |
| | 6.615 | 8.401 | | | | | |
| 485+00 | | | 6.381 | | | 2.02 | 7.2 Lt of Hub ") 1.6 Lt checked |
| 484 | | | 6.381 | | | 2.02 | 3.0 Rt of Hub ") 6.6 Rt ^{storm} _{main} checked |
| 483 | | | 6.381 | | | 2.02 | 14.9 Lt of Hub ") 38 Lt checked |
| 482 | | | 6.381 | | | 2.02 | 20.9 Lt of Hub ") on Schuyler Hub 0.0 |
| 481 | | | 6.381 | | | 2.02 | 44.6 Lt of Hub ") 21.4 to Lt checked |
| Gr. Man Elev. on High Cor. | | | | | | | |
| 480+56.46 | | T.P | 2.301 | 6.100 | 6.100 | | |
| | 4.370 | 10.470 | | | | | |
| | | | 2.990 | 7.480 | | | |
| | 8.180 | 15.660 | | | | | |
| | | | 1.400 | 14.260 | | | |
| Check on | 5.245 | 19.505 | | | | | |
| CITY B.M. SW Carb | | Lowell Rosecrans | 5.375 | 14.130 | 14.130 | US.G.S. = 8.063 City B.M. | |
| | | | | | | 14.130 8.063 Difference 6.067 | Finished June 16-22 11.45 A.M. |

6.426
2.02
4.416

8.401
2.02
6.381

7.100
2.020
7.080

San Diego Quadrangle
June 16. 22 P.M.

J.W. Williams
Jack Sights

5

| Sta | + | - | Elev | B.M. |
|--------|-------|--------|------------|--------|
| | | | | 20.622 |
| | 0.570 | 21.192 | | |
| | 0.558 | 9.100 | 12.650 | 8.542 |
| | 4.650 | 6.670 | 7.080 | 7.020 |
| | | | 4.650 | |
| 296+00 | | | 4.650 | |
| 295 | | | 4.650 | |
| 296 | | | 4.650 | |
| 293 | | | 4.650 | |
| 292 | | | 4.650 | |
| 291 | | | 4.650 | |
| | | | T.P. 4.600 | 7.070 |
| 290 | | | | |
| 289 | | | | |
| 288 | | | | |
| 287 | | | | |

B. About 1 1/2 miles north of San Diego on the Alchison
Tapeka and Santa Fe Railway right of way about 50
Meters north of Milepost 266 on West end of Concrete
Culvert "C 266" in the corner of the horizontal
Surface 2 1/2 meters below rail; Coast Survey B.M.
Tablet (20.622 Elev.)

Elev.
U.S.G.S.
M.H.W.
2.02

| | | |
|------|------------------|-----------------|
| 2.02 | 15.3 Lt Schuyler | 15.3 Lt checked |
| | 13.9 Lt | 17.4 Lt checked |
| 2.02 | 10.5 Lt | 11.9 Lt " |
| 2.02 | 4.5 Lt | 4.5 Lt " |
| | 9.0 Lt | 0.5 Lt " |
| 2.02 | 7.4 Lt | 2.2 Lt " |
| 2.02 | 6.5 Lt | 2.5 Lt " |
| 2.02 | 6.7 Lt | 1.0 Lt " |
| 2.02 | 4.6 Lt | 5.3 Rt " |
| 2.02 | 6.0 Rt | 11.2 Rt " |

+63.4 Foot of Thorn St

foot of spruce

J.W. Williams
 J. Sights June 19 1922
 6

Sta + π - Elev B.M.

| | | | | |
|-----------------------|--------|--------|--------|--|
| | | | 28.109 | |
| 0.430 | 28.539 | | | |
| | | 12.122 | 16.417 | |
| 4.500 | 20.917 | | | |
| | | 12.922 | 7.995 | |
| 1.383 | 9.378 | | | |
| | | 11.662 | -2.284 | |
| 2.820 | 0.536 | 4.636 | -4.10 | |
| 74+00 | | 4.626 | | |
| 75+00 = 0+00 "A" Line | | 4.626 | | |
| 1+00 "A" Line | | 4.626 | | |
| 2+00 " " | | 4.626 | | |
| 2+50 " " | | 4.626 | | |
| 3+00 " " | | 4.626 | | |
| 4+00 " " | | 4.626 | | |
| 5+00 " " | | 4.626 | | |
| | T.P. | 5.130 | -4.594 | |
| 6.315 | | | | |
| | 1.721 | | | |
| 6+00 " " | | 5.821 | -4.10 | |
| 7+00 " " | | 5.821 | -4.10 | |
| | T.P. | 0.385 | 1.336 | |
| 10.745 | 17.081 | | | |
| | | 3.970 | 8.111 | |
| 9.010 | 17.121 | | | |

City B.M North bolt of Fire Hydrant N.E. Cor 26th
 and Main St. Elev. 28.109

City Elev Mean High Water - 4.10
 -4.10

-4.10 checked 44 Lt Record 42 Lt
 -4.10 checked 48 Lt Record 52 Lt
 -4.10 checked 7.2 Lt Record 10.2 Lt
 -4.10 checked 7.5 Rt Record 3.1 Lt
 -4.10 checked 8.5 Lt Record 8.5 Lt
 -4.10 " 3.0 Lt " 9.3 Lt
 -4.10 " 4.0 Rt " 5.5 Lt
 -4.10 " 5.0 Rt " 4.1 Lt

10.7
 3.1
 7.6
 52
~~44.5~~
 47.5

From foot of 26th St

| Sta | + | π | - | Elev | B.M. |
|-------|--------|--------|-------|--------|--------|
| | | 17.121 | 0.560 | 16.561 | |
| 9.460 | 26.021 | | 0.485 | 25.536 | |
| 7.240 | 32.776 | | 5.145 | 27.631 | |
| 3.320 | 30.951 | | 5.780 | 25.171 | |
| 3.370 | 28.541 | | 5.650 | 22.891 | |
| 3.720 | 26.611 | | 5.230 | 21.381 | |
| 2.460 | 23.821 | | 8.020 | 15.801 | |
| 2.880 | 18.681 | | 3.960 | 14.721 | 14.721 |

N. Bolt of Fire Hydr Maint Sigsby City B.M.

J.W. Williams
J. Sigsby June 19 1922

7

June 20 - 1922

J.W. Williams
Jack Sights

8

| Sta | + | ∓ | - | Elev | B.M |
|------|--------------|--------|--------|--------|--------|
| | 1.280 | 16.001 | | | 14.721 |
| | | | 9.770 | 6.231 | |
| | 3564 | 9.793 | | | |
| | | | 12.045 | -2.252 | |
| | 4.740 | 2.488 | | | |
| 3+00 | Hartupce Tr. | | 6.588 | | |
| 2+00 | Hartupce Tr. | | 6.588 | | |
| 1+00 | Hartupce Tr. | | 6.588 | -4.10 | |
| | | T.P. | 1.675 | 0.813 | |
| | 8.860 | 9.673 | | | |
| | | | 2.465 | 7.208 | |
| | 8.680 | 15.288 | | | |
| | | | 1.160 | 14.728 | |

North Bolt of Fire Hydr. S.E. Cor Main + Sigby St.

4.10
-2.488
6.588

City Datum for line of Mean High Water = -4.10

-4.10 checked 81.3 ft Record 77.3 ft

-4.10 checked 51.0 ft Record 47.0 ft

-4.10 checked 31.1 ft Record 25.1 ft

14.721 Check on City B.M. N. Bolt in Fire Hydr
Cor. Main St + Sigby

Levels to establish height of
Tides at Hartapeet Trect.

| Sta | + | - | Elev | B.M. |
|------|-------|--------|-------|--------------------|
| | | | | 14.721 |
| T.P. | 1.015 | 15.736 | 8.888 | 6.848 |
| | 2.190 | 9.038 | | |
| T.P. | 3.230 | 6.658 | 5.610 | 3.428 |
| | 4.221 | 6.814 | 4.065 | 2.593 |
| | | | 5.530 | 1.284 B.M. in Pile |
| T.P. | 4.080 | 6.664 | 4.230 | 2.584 |
| | 5.605 | 9.019 | 3.250 | 3.414 |
| | 6.370 | 13.209 | 2.180 | 6.839 |
| | 4.765 | 16.974 | 1.100 | 14.109 |
| | | | 2.280 | 14.694 14.721 |

J.W. Williams Level
Johnny West Rod

9

N. Poll for Hight Con Man & Reg steel

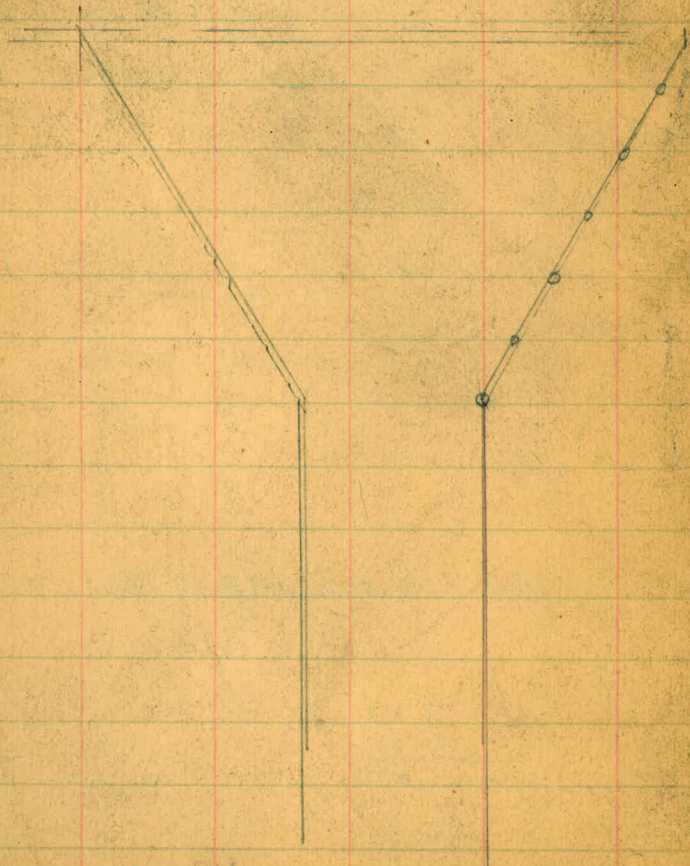
check

Elevation Mud 7.33 below (B.M. Elev 1.286)

7.33
 1.28
 -6.05
 -4.10
 1.95

Rod Readings from City B.M.
Bay of San Diego at Horner Tract

City Datum B.M. 1.284 nail in edge
of 12" x 12" Wing Cap Rod readings are shown
— or below bench.



on End of Bulkhead 10 1.284

J.W. Williams Old Winningsdal
J. West July 11-22

5.8
1.3
-4.5 10

11-17 AM. - 5.8 Rod.

11-20 am - 5.75 "

11-25 am - 5.80 "

11-30 am - 5.80 "

11-35 am - 5.80 "

11-40 am - 5.82 "

11-45 am - 5.83 "

11-50 am - 5.85 "

11-55 am - 5.87 "

12 noon - 5.94 "

12-05 P.M. - 5.99 "

12-10 P.M. - 6.01 "

12-15 P.M. - 6.05 "

12-20 P.M. - 6.10 "

12-25 P.M. - 6.15 "

12-30 P.M. - 6.22 "

12-35 P.M. - 6.25 "

Rod Readings to Determine
Height of Tide in Bay of San
Diego at Hartupel tract

B.M.

All rods measured down from City B.M. 1284-

J. W. Williams
J. R. West. "
July 11 - 22 P.M. "

| Time | Rod |
|---------|-------|
| 9-45 PM | -4.64 |
| 9-50 " | -4.63 |
| 9-55 " | -4.62 |
| 10-00 " | -4.56 |
| 10-05 " | -4.48 |
| 10-10 " | -4.46 |
| 10-15 " | -4.48 |
| 10-20 " | -4.45 |
| 10-25 " | -4.51 |
| 10-30 " | -4.49 |
| 10-35 " | -4.48 |
| 10-40 " | -4.54 |
| 10-45 " | -4.62 |
| 10-50 " | -4.63 |
| 10-55 " | -4.66 |
| 11.00 " | -4.67 |
| 11.05 " | -4.72 |

levels From U.S.G.S Bench to Axis of

Dam Site

Van Horn 13
Mansfield
1/9-24
Clear

Same Gr. U.S.G.S 0.2 m. S. Forks of Rd.

| | | | | |
|--------|--------|--------|--------|--------|
| B.M. | +2.45 | 792.07 | -0.31 | 792.24 |
| TP | +1.77 | 793.53 | -1.67 | 798.6 |
| TP | +12.00 | 803.86 | -1.67 | 791.86 |
| TP | +5.62 | 805.52 | -3.96 | 99.90- |
| | +11.37 | 815.30 | -1.59 | 03.93 |
| TP | +12.63 | 825.12 | -2.81 | 12.49 |
| | +0.52 | 813.01 | | 12.49 |
| TP | +0.59 | 80.98 | -12.62 | 00.39 |
| Trans. | +6.95 | | 24.63 | 6.72 |
| TP | +0.27 | 788.37 | -12.88 | 788.10 |
| | +0.23 | 775.88 | -12.72 | 75.65 |
| | +1.24 | 764.08 | -13.04 | 62.84 |
| | +0.02 | 751.66 | -12.44 | 51.14 |
| | +1.18 | 740.39 | -12.45 | 39.21 |
| | +0.27 | 738.04 | -12.62 | 37.77 |
| TP | +1.59 | 727.24 | -12.39 | 25.65 |
| | +0.69 | 715.06 | -12.87 | 14.37 |
| | | | -7.74 | 07.32 |

on large Rock E Side Stream below Axis

on Rock on E Bank

Grades from Proposed Dam

Grade Gr. Rod

| | | | | |
|----------------------|-------|-------|--------|------------|
| 2+40 | +9.77 | 08.82 | 799.05 | 99.76 |
| 3+00 | | | | 99.70 9.12 |
| 4+00 | | | | 99.60 9.22 |
| 5+00 | | | | 99.50 9.32 |
| 6+00 | | | | 99.40 9.42 |
| 7+00 | | | | 99.30 9.52 |
| 8+00 | | | | 99.20 9.62 |
| +50 | +0.35 | 04.28 | 99.15 | 803.93 |
| Stadia across Siphon | | | 437.00 | |
| Siphon Point B | | | 98.50 | |
| TP | +5.10 | 03.00 | | |
| 14+00 | | | 98.39 | 6.61 |
| 15+00 | | | 98.29 | 6.71 |
| | +3.50 | 03.40 | | |
| 16+00 | | | 98.19 | 5.21 |
| 17+00 | | | 98.09 | 5.31 |
| 18+00 | | | 97.99 | 5.41 |
| 19+00 | | | 97.89 | 5.51 |

Abandoned
 Transit Book
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799.32
 99.05
 27
 99.32
 27
 99.05

Van Horn
 Thompson II
 Stout
 Mansfield

Elev 799.05 Established by Transit

note Siphon Point B change
 note new stadia dist 400' or

Transit Book
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TP on Rock - Siphon Point A

level shot

Abandoned

800.26
 24
 99.76

802.25
 99.99
 438

| | T | Gr. | Elev. |
|---------|--------|--------|-------|
| 20+00 | 03.40 | 97.79 | 5.61 |
| 21+00 | | 97.69 | 5.71 |
| 22+00 | | 97.59 | 5.81 |
| +8.40 | 98.26 | | |
| 23+00 | | 97.49 | 2.77 |
| 24+00 | | 97.39 | |
| 25+00 | | 97.29 | |
| TP | +12.73 | 804.49 | 97.19 |
| 26+00 = | -0.52 | 97.18 | 98.18 |
| 24+56 | | | |

Abandoned
see Transit Book
Page 52

91.86

91.76

CI^o

Abandoned
see Transit Book
Page 53

11-23 16
 Party some
 clear.

Begin of
 Levels from 1 Syphon #2 along Conduit

| | | | | | |
|----------|--------|--------|-------|--------|-----------------------------|
| | +5.09 | 803.26 | Elev. | 198.17 | Sta 24+56 |
| 33+96 | -7.37 | | 75.89 | 95.78 | |
| TP | +8.43 | 804.32 | | | |
| 37+50 TP | -8.81 | | 95.45 | | |
| | +5.90 | 801.35 | | | |
| 44+00 TP | -6.55 | | 94.80 | | |
| | +10.75 | 805.55 | | | |
| TP | -0.57 | | 04.98 | | 20' S. of Sta 52+00 on Rock |
| | +4.09 | 809.07 | | | |
| TP | -11.53 | | 97.54 | | |
| | +2.34 | 799.88 | | | 5' West of Sta 53+75 |
| 56+00 TP | -6.30 | | 93.58 | | |
| | +7.25 | 800.83 | | | |
| 63+00 TP | -7.93 | | 92.90 | | |
| | +13.00 | 805.90 | | | |
| 77+50 TP | -13.00 | | 92.90 | | |
| | +9.37 | 802.27 | | | |
| 79+50 | -11.04 | | 91.23 | | |
| | +10.72 | 801.95 | | | |

81.65
88.83
12.87
30.90

TP 91+00 -11.87 801.95 790.08

+11.57 801.65

TP 103+50 -12.82 88.83

+12.06 800.89

TP 111+00 -12.81 88.08

+9.72 797.80

TP 113+50 -7.02 790.75 on Rock above grade.

+9.41 800.19

TP 126+25 -13.00 787.19 stone 06 above grade

+10.30 797.49

TP 133+50 -11.66 -11.66 785.83

+12.03 797.86

TP 143+00 -12.98 84.28

+11.92 796.80

-12.82 83.98

TP 152 + 7.31 791.29

TP 163 -8.41 82.88

+11.10 793.98

92.36 A 21

| | | | |
|-----------|--------|--------|-------|
| TP 169+00 | -11.71 | 793.98 | 82.27 |
| | +11.45 | 793.72 | |
| TP 171+00 | -11.63 | 793.02 | 82.09 |
| | +10.93 | 793.02 | |
| TP 176+00 | -11.44 | 791.44 | 81.58 |
| | +9.86 | 791.44 | |
| TP 179+00 | -10.16 | 791.00 | 81.28 |
| | +9.72 | 791.00 | |
| TP 183+00 | -10.14 | 791.27 | 80.86 |
| | +10.43 | 791.27 | |
| TP 192+00 | -11.21 | 789.67 | 80.08 |
| | +9.59 | 789.67 | |
| TP 196+00 | -10.06 | 792.44 | 79.61 |
| | +12.83 | 792.44 | |
| TP 198+90 | -12.82 | 787.25 | 79.62 |
| | +7.63 | 787.25 | |
| TP 201+50 | -8.89 | 788.79 | 78.36 |
| | +10.43 | 788.79 | |
| | 92.89 | 788.06 | |

788.09
87.27
1.54

52

TP 226+00 77.52 -11.27

TP 236+00 +8.76 786.28 -6.95 79.33

+6.00 785.33

TP 242+25 -10.37 74.96

+5.77 780.73

TP 256+00 -7.15 73.58

+5.98 779.56

TP 258+00 -6.18 73.38

+10.57 783.95

TP 268+00 -11.57 72.38

+8.22 780.60

TP 279+00 -9.32 71.28

+6.74 773.02

TP 290+00 -7.84 70.18

+9.66 779.84

-9.91 69.93

TP 292+50 +10.15 780.08

TP 299+00 -10.80 69.28

71.85 779.36

| | + | - | |
|------------|------------------------|-------------------------|-------|
| | ⁴ +10.49 | ⁵ 779.77 | 69.23 |
| TP306+50 | | ²³ -11.24 | 68.53 |
| | +9.38 | 777.91 | |
| TP313+25 | | -10.05 | 67.86 |
| | +11.45 | 779.31 | |
| TP315+75 | | -13.04 | 66.27 |
| | +9.11 | 775.38 | |
| TP318+52 | | -8.03 | 67.35 |
| | +7.57 | 774.92 | |
| TP327+00 | | -8.44 | 66.48 |
| | +11.77 | 778.25 | |
| TP332+50 | | -12.33 | 65.92 |
| | +12.17 | 778.09 | |
| TP | | -4.83 | 73.76 |
| | +2.57 | 775.83 | |
| TP340+32 | | -10.74 | 65.09 |
| | +9.64 | 774.73 | |
| TP on Rock | | -4.28 | 70.45 |
| | +2.70 | 773.23 | |

✓ 1/10-23

✓ 1/17-23
Party same
clean

65.09
64.93
14

TP 483 on Rock

Siphon #3 Point

30' h. of TP 347+50

| | | | |
|-----------|--------|--------|-------|
| | | 773.23 | |
| TP 352+60 | | -9.52 | 63.71 |
| | +11.76 | 775.47 | |
| TP 355+50 | | -12.04 | 63.43 |
| | +8.59 | 772.02 | |
| TP 357+50 | | -8.79 | 63.23 |
| | +11.30 | 774.53 | |
| TP 370+50 | | -12.60 | 61.93 |
| | +3.53 | 765.46 | |
| TP 2 | | -0.50 | 64.96 |
| | +0.84 | 765.80 | |
| TP 398+50 | | -6.55 | 59.25 |
| | +11.60 | 770.85 | |
| TP 2 | | -8.21 | 62.64 |
| | +5.75 | 768.39 | |
| TP 2 | | -8.92 | 59.67 |
| TP 414+00 | 17.76 | 769.43 | |
| | | -11.25 | 56.18 |
| | +12.16 | 768.34 | |

1/17-24

Siphon Point "B"

on top of large Rock near Siphon Point B ^{#A}

Siphon Point "B" 1/17-24

on Rock 10' E Sta 405+00

on Sta 407+66

| Sta | + | x | - | Elev. |
|-----------|--------|--------|--------|--------|
| | | 768.34 | | Elev. |
| A19+50 TP | | | -12.71 | 55.63 |
| | +12.17 | 767.80 | | |
| TR 420+50 | | | -12.27 | 55.53 |
| | +12.48 | 768.01 | | |
| 423+50 | | | -12.79 | 55.22 |
| | +10.60 | 765.82 | | |
| 428+00 | | | -11.04 | 54.78 |
| | +5.77 | 760.55 | | |
| 434+00 | | | -6.37 | 54.18 |
| | +11.36 | 765.54 | | |
| 441+75 | | | -12.15 | 53.39 |
| | +9.89 | 763.28 | | |
| 446+75 | | | -10.37 | 52.91 |
| | +9.68 | 762.59 | | |
| 449+50 | | | -9.95 | 52.64 |
| | 10.41 | 763.05 | | |
| 452+00 | | | -7.36 | 755.69 |
| | 7.02 | 762.71 | | |
| 457+50 | 49.38 | | -10.88 | 751.83 |
| | | | 1055.9 | |

J.W.V. Begins Jan 24. cracks level starting today

Gr. 752.39 Cat 3.2

✓ 11/18-24

8905

10443
LTC

| Sta | + | - | | File |
|------------------|--------|--------|--------|------------------------|
| | +9.01 | 760.84 | | 751.83 |
| | | | -9.86 | 750.98 |
| 465+95 | +6.55 | 757.53 | | |
| 467+40 | +12.39 | 763.18 | 6.69 | 750.84 |
| 468+40 | | | | 12.71 750.79 |
| 469+00 | | | | 12.50 750.68 |
| 471+00 | | | | 12.70 750.48 |
| | | | 6.14 | |
| | +1.90 | 758.94 | T.P. | 6.14 757.04 |
| | | | T.P. | 7.66 |
| | +2.67 | 753.95 | | 751.28 |
| 487+50 | | | T.P. | 5.12 |
| | +9.84 | 758.65 | | 748.83 |
| 491+70 | | | T.P. | 10.26 |
| | +9.25 | 757.66 | | 748.41 |
| 497+00 | | | T.P. | 9.78 |
| | +3.12 | 751.00 | | 747.88 |
| 498+50 | | | T.P. | 3.27 |
| | +11.07 | 758.80 | | 747.73 |
| 507+00 | | | T.P. | 11.92 |
| | +8.19 | 755.07 | | 746.88 |
| | | | T.P. | 0.60 |
| | +10.88 | 765.35 | | 754.47 |
| on Hub 521+50 | | | | 12.76 |
| | +0.42 | 753.01 | | 752.59 |
| 523+50 | | | | 8.35 |
| | +1.80 | 746.46 | | 744.66 |
| 526+60 | | | | 12.52 |
| | +0.96 | 734.90 | | 733.94 |
| 532 | | | | 2.96 |
| | +1.07 | 733.01 | | 731.94 |
| 536+40 | 89.05 | | 0.84 | 734.19 |
| | | | 122.55 | |

20' Rt of Sta 478+00 on Rock
 7' ahead of 483+50 on Rock

End of Jan 21 1924 Begin Jan 22

7' Lt of 516+75 on Hub

9.24

| Sta | + | x | - | Elev. |
|-----------------------------|--------|--------|-------|---------------|
| | | | | 732.19 |
| | +11.10 | 743.29 | | |
| 540 | | T.P. | 1.11 | 742.18 |
| | 6.18 | 748.36 | | |
| 546+80 | | | 3.60 | 744.76 |
| | 1.88 | 746.64 | | |
| Top 547+50 | | | 10.30 | 736.34 |
| Top Rock | 0.96 | 737.30 | | |
| 3' Lt of 548+05 | | | 12.78 | 724.52 |
| | 0.79 | 725.31 | | |
| Top of 549+00 | | | 12.20 | 713.11 |
| | 0.57 | 713.68 | | |
| Hub at about 551+50 | | | 1.09 | 712.59 |
| about 8' Rt of 552 | 12.36 | 724.95 | | |
| | | | 0.35 | 724.60 |
| at about 8' Rt of 552+00 | 12.36 | 736.96 | | |
| | | | 0.61 | 736.35 |
| On Rock at 554+48 | 11.91 | 748.26 | | |
| | 10.84 | 753.78 | 5.32 | 742.94 |
| 556+20 | | | 11.82 | 741.96 |
| | 9.02 | 750.98 | | |
| 559 - | | | 9.30 | 741.68 |
| | 9.39 | 751.07 | | |
| 562 - | | | 9.69 | 741.38 |
| | 11.97 | 753.35 | | |
| 563+80 | | | 12.15 | 741.20 |
| | 12.09 | 753.29 | | |
| 564+60 | | | 12.17 | 741.12 -12.17 |
| 566+60 | | | 12.37 | -12.37 |
| 568+40 | | | 12.55 | 740.77 |
| | +12.22 | 752.96 | | |
| | 113.62 | | 8' | 102.97 |

✓ 2/24

End of year 22 - 1924

Jan 23 - 1924

| | | | | | | |
|----------------------|-------|--------|---|-------|--------|-------|
| Sta | | H.I | ✓ | - | Elev | |
| | | 752.96 | | | | |
| 570+70 | 12.78 | 757.02 | ✓ | 8.72 | 744.29 | ✓ |
| | | | | 0.12 | | |
| T.P. | 11.03 | 767.81 | ✓ | 0.24 | 756.78 | ✓ |
| T.P. | 11.06 | 778.86 | ✓ | 0.01 | 767.80 | |
| 572+68 ³⁰ | 11.24 | 777.52 | ✓ | 8.58 | 770.20 | -8.58 |
| T.P. | 12.87 | 790.49 | ✓ | 1.24 | 777.62 | ✓ |
| T.P. | 11.50 | 799.94 | ✓ | 2.05 | 788.44 | ✓ |
| T.P. | 12.43 | 810.71 | ✓ | 1.66 | 798.28 | |
| | | 809.71 | | | 797.28 | |
| T.P. | 12.01 | 821.88 | ✓ | 0.84 | 809.87 | |
| | | 820.88 | | | 808.87 | |
| T.P. | 12.84 | 833.75 | ✓ | 0.97 | 820.91 | |
| | | 832.75 | | | 819.94 | |
| | 96.52 | | | 18.72 | | |

2/7-24

Rock 580+10±

Rock 571+30±

Line Stake

Rock ✓

Rock.

Set 10th.

$$\begin{array}{r} 770.30 \\ 235.24 \\ \hline 535.06 \end{array}$$

| | | | | | |
|-----------|--------------|-------------------------------------|-----------|-----------------------------|-------------------------|
| Sta | + | 833.75 H.I. 832.75 | - | Elev | |
| T.P. | 1203 | 844.86 843.86 | 0.92 | 832.83 831.83 | Set stake. |
| T.P. | 12.76 | 856.38 855.38 | 1.24 | 843.62 842.62 | Rock |
| T.P. | 11.66 | 865.67 864.67 | 2.37 | 854.01 853.01 | Set Stake |
| T.P. | 10.03 | 874.20 873.20 | 1.50 | 864.17 863.17 | Rock |
| Point No. | 12.20 | 885.92 884.92 | 0.48 | 873.72 872.72 | Point on Boulder (P.M.) |
| T.P. | 11.94 | 897.63 896.63 | 0.23 | 885.69 884.69 | Set Stake |
| T.P. | 11.86 | 909.41 908.41 | 0.08 | 897.53 896.53 | Set Stake. |
| T.P. | 11.93 | 921.34 920.34 | 0.00 | 909.41 908.41 | Set Stake |
| T.P. | 1263 | 933.97 932.97 | 0.00 | 921.34 920.34 | Set Stake |
| | 10904 153 | | 2.92 3 | | |

| Sta. | + | H.I. | - | Elev. |
|------|------|--------------------|------|-------------------|
| | | 933.97 | | |
| | | 932.97 | | 933.97 |
| T.P. | 1231 | 946.28 | 0.00 | 932.97 |
| | | 945.28 | | |
| T.P. | 1286 | 959.14 | 0.00 | 946.28 |
| | | 958.14 | | 945.28 |
| T.P. | 1194 | 971.08 | 0.00 | 959.14 |
| | | 970.08 | | 958.14 |
| T.P. | 1306 | 984.14 | 0.00 | 971.08 |
| | | 983.14 | | 970.08 |
| T.P. | 1300 | 997.14 | 0.00 | 984.14 |
| | | 996.14 | | 983.14 |
| T.P. | 1211 | 1009.25 | 0.00 | 997.14 |
| | | 1008.25 | | 996.14 |

Set Stake

Set Stake.

Set Stake.

Set Stake.

Set Stake

Set Stake.

Point No 5 366 ^{1005.57} ~~1004.59~~

Hub on Ridge = 583+783

T.P.
Point No 6 0.94 ^{07.31} ~~1007.19~~

Hub on Ridge = 584+04

Point No 5 4.91 ^{1010.50} ~~1009.50~~ ^{1005.57} ~~1004.59~~
 0.99 0.94

| Sta | + | 1010.50 H.I. 1009.50 | - | Elev. | |
|------------|---------|-----------------------------|-------------|------------------|------------------|
| T.P. | 0.70 | 999.24 998.24 | 11.96 | 998.54 997.54 | set Stake |
| T.P. | 1.00 | 987.46 986.46 | 12.78 | 986.46 985.46 | set Stake |
| T.P. | 0.68 | 975.29 974.29 | 12.85 | 974.61 973.61 | set Stake. |
| T.P. | 0.21 | 962.68 961.68 | 12.82 | 962.47 961.47 | set Stake |
| T.P. | (-0.10) | 950.05 949.05 | 12.53 | 950.15 949.15 | set Stake. |
| T.P. | 0.86 | 937.99 936.99 | 12.92 | 937.13 936.13 | set Stake |
| Point No 7 | | | 6.15 | 931.83 930.83 | Lath Hub on Line |
| T.P. | 2.27 | 927.26 925.26 | 13.00 | 924.99 923.99 | set Stake |
| Point No 8 | 8.62 | | 8.86 " " | | |
| " " 9 | 2.2 | | 0.90 | | Lath Hub on Line |
| | | | 10.77 | | " " " " |

| | | | | | |
|--------|-------|-------------------|-------|-------------------|---------------|
| Sta | + | 927.26 | - | Elev. | |
| | | 425.26 | | | |
| T.P. | 0.12 | 914.88 | 1250 | 914.76 | |
| | | 912.88 | | 912.76 | Set Stake. |
| T.P. | 4.45 | 906.33 | 13.00 | 901.88 | |
| | | 904.33 | | 899.88 | Set Stake |
| Point | | | | 895.63 | |
| No. 10 | | | | 893.63 | Point on Line |
| | | | | -10.76 | |
| T.P. | 7.08 | 900.73 | 12.68 | 893.65 | |
| | | 898.73 | | 891.65 | Set Stake. |
| T.P. | 1.02 | 889.64 | 12.11 | 888.62 | |
| | | 887.64 | | 886.62 | Set Stake |
| T.P. | 0.69 | 877.53 | 12.80 | 876.84 | |
| | | 875.53 | | 874.84 | Set Stake. |
| T.P. | | | 12.63 | 864.90 | |
| | | | | 862.90 | |
| | | 870.44 | | | |
| | 5.54 | 868.44 | | | |
| T.P. | 12.05 | 881.05 | 1.99 | 869.00 | |
| | | 879.05 | | 867.00 | Set Stake. |
| | 30.95 | | 77.16 | | |
| | | | | | |

Jan 25-1924

Brochitt
Thomason
Red
Manfield

| | | | | |
|-----------|-------|-------------------|-------|--------------------------|
| | | 881.05 | | |
| Sta | + | H.I. | - | Elev. |
| | | 877.05 | | 876.16 |
| T.P. | 2.36 | 878.52 | 4.89 | 874.16 |
| | | 876.52 | | |
| Point #13 | 1.76 | 869.86 | 10.42 | 868.10 |
| | | 867.86 | | 866.10 |
| T.P. | 0.96 | 857.56 | 12.76 | 857.10 |
| | | 855.56 | | 855.10 |
| T.P. | 1.24 | 846.08 | 12.72 | 844.80 |
| | | 844.08 | | 842.84 |
| T.P. | 0.00 | 833.81 | 12.27 | 833.81 |
| | | 831.81 | | 831.81 |
| T.P. | 1.66 | 823.47 | 12.00 | 821.81 |
| | | 821.47 | | 819.81 |
| Point #15 | 12.83 | | | 819.83 |
| | | | | 817.83 - 3.64 |
| T.P. | 4.69 | 815.33 | 12.83 | 810.64 |
| | | 813.33 | | 808.64 |
| Point #18 | 12.17 | | | 810.47 |
| | 3.3 | | | 808.47 - 4.86 |
| | | 77.89 | | |

Set Stake

Hub on E

Set Stake

Set Stake

Set Stake

Set Stake

Set Stake

Set Stake

Sta +
 815.33
~~813.33~~
 802.86
 800.84 1278 800.55
 Elev
 802.55

Set Stake

T.P. 0.41
 790.43
~~788.43~~ 12.88 787.96
 789.96

Set Stake

T.P. 0.03
 777.40
~~775.40~~ 13.06 775.37
 777.37

Set Stake

T.P. 0.22
 765.17
~~763.17~~ 12.95 762.95
 764.95

Set Stake

T.P. 0.53
 752.96
~~750.96~~ 12.74 750.43
 752.43

Set Stake

T.P. 0.62
 740.62
~~738.62~~ 12.99 738.07
 740.02

Set Stake

296 737.68
 735.68

Set Lath Hub Approximate Grade Point

79.81

Jan 26-1924.

~~17.97~~ 18+65
 10.99 746.65 ✓

1313
 53

626+920

11.76 736.89
 734.89
 734.76

grade at adjusted Sou. Portal of Tunnel.

| Sta | + | H.I. | - | Elev |
|----------|-------------|-------------------|--------|-----------------------------|
| | | 748.65 | | |
| 628 | | 746.65 | 11.87 | 736.78 734.78 |
| 630 | | | 12.07 | |
| TP | | 746.97 | | 736.48 |
| 631 | 10.29 | 744.71 | 12.17 | 734.48 |
| 632+25 | | | 10.91 | |
| 633+50 | | | 10.54 | |
| 634+50 | | | 10.64 | |
| 636+50 | | | 10.84 | 735.93 733.93 |
| TP | | 747.02 | | 735.88 |
| 637 | 11.14 | 745.02 | 10.89 | 733.88 |
| 638 | | | 11.24 | |
| 640 | | | 11.44 | |
| 642 | | | 11.64 | |
| 654 | | 742.02 | | 732.18 |
| TP | 7.84 | 740.02 | 12.34 | 732.18 |
| 674+20 | | | 8.14 | 733.88 731.88 |
| | +9.22 | 743.10 | | |
| TP682+50 | | | -12.62 | 730.48 728.48 |
| | | 740.91 | | 729.53 |
| TP692+00 | +10.43 | 738.91 | -11.38 | 727.53 |
| | +12.70 | | | |
| | | 742.73 | | |
| | 61.62 22 | 740.73 | 68.04 | |

1/29-24
 Williams
 Brackett
 Van Horn
 Thompson
 Mansfield
 Stout
 Clear

| | | | |
|-----------|-------------------|--------|------------------|
| | 742.23 | | 29.23 |
| TP 695+00 | 740.23 | -13.00 | 27.23 |
| +10.70 | 739.93 | | 28.23 |
| TP 705+00 | 737.93 | -11.70 | 26.23 |
| | 738.38 | | |
| +10.15 | 736.38 | | |
| TP 721+00 | | -11.75 | 26.63 |
| | 737.65 | | 24.63 |
| +11.02 | 732.65 | | |
| TP 722+15 | | -11.23 | 26.42 |
| | 735.51 | | 24.42 |
| +9.09 | 733.51 | | |
| TP 732+75 | | -10.80 | 25.31 |
| | 736.86 | | 23.31 |
| +11.55 | 734.86 | | |
| TP 738+00 | | -12.21 | 24.65 |
| | 732.79 | | 22.65 |
| +10.14 | 732.79 | | |
| TP 745+50 | | -10.59 | 23.90 |
| | | | 21.90 |
| +8.25 | 732.15 | | 23.43 |
| TP 750+00 | 730.15 | -8.72 | 21.43 |
| +11.17 | | | |
| | 734.60 | | 22.86 |
| TP 756+00 | 732.60 | -11.74 | 20.86 |
| | 730.81 | | |
| +7.95 | 728.81 | | |

on Rock Siphon Point "A" Siphon "B"

732 + 75
 22 15

 10 40

9002

10 1AA

21.75
10.57
32.32

730.81

TP 758+25 ~~25.81~~ -1.20

TP 767+00 +3.91 ~~733.52~~ 731.52 11.77
3.91 ~~731.52~~ 731.52 -7.77

767+00 732.32

TP 769+50 10.57 730.32

769+50 (note: not used as turn 221.50) 10.82 719.59

TP 780+00 6.70 ~~728.04~~ 728.04 10.98 719.34

787+63 -8.12 719.92 717.92

795+00 10.00 713.04

787+63 719.92 717.92

+8.96 728.88 726.88

TP 803+00 -11.64 17.24 15.24

+10.60 727.84 725.84

TP 811+00 -11.40 16.44 14.44

+10.18 726.62 724.62 -10.78

TP 817+00 15.84 13.84

+9.67 723.57

abandoned

-12.94 10.57

10.66 721.23

29.61

~~27.61~~

21.75

19.75

23.75

1.29.24

21.75

Beginning of Syphon.

Downstream End of Syphon. (Gr. 719.9 ^{719.9} ~~717.92~~)

Lower end of Syphon

TP on Concrete Base near Bee Hives

| | | | | |
|-----------|-------------------|------------|-------------------|------------------------------|
| TP 823+00 | 721.23 | -8.00 | 13.23 | |
| +3.86 | 717.09 | Abandoned. | | |
| TP 825+00 | | -4.05 | 13.04 | ✓ 11/31-24 |
| TP 817+00 | | | 15.84 | |
| | 727.39 | | 13.84 | |
| +11.55 | 725.39 | | | |
| TP 27 | | -0.39 | 727.00 | |
| | 739.10 | | 725.00 | 30' w. of 823+50 |
| +12.10 | 737.10 | | | |
| TP 27 | | -0.29 | 738.81 | |
| | 751.45 | | 736.81 | Sta 826+50 |
| +12.64 | 749.45 | | | |
| TP 27 | | -0.48 | 750.97 | |
| | 761.23 | | 748.97 | 30' w. 830+ ²⁵ 50 |
| +10.26 | 759.23 | | | |
| TP 27 | | -0.33 | 760.90 | |
| | 773.07 | | 759.90 | Sta 834+15 |
| +12.17 | 771.07 | | | |
| TP 839+00 | | -0.02 | 773.05 | |
| | 786.10 | | 771.05 | |
| +11.05 | 782.10 | | | |
| TP 849+00 | | -1.22 | 782.88 | |
| | 795.99 | | 780.88 | |
| +13.11 | 793.99 | | | |

| | | | |
|------------|-------------------|--------|-------------------|
| | 795.99 ✓ | | 795.81 |
| TP 7855+50 | 793.99 | -0.14 | 793.85 |
| | 807.53 | | |
| | +11.68 | | |
| | 795.85 | | |
| TP | 795.36 | -13.01 | 794.52 |
| | +10.84 | | 792.56 |
| | 793.36 | | |
| TP | 783.03 | -12.89 | 782.47 |
| | +10.56 | | 780.47 |
| | 781.03 | | |
| TP | 770.31 | -13.00 | 770.03 |
| | +10.28 | | 768.03 |
| | 768.31 | | |
| TP | 757.55 | -13.00 | 757.31 |
| | +10.24 | | 755.31 |
| | 755.55 | | |
| TP | 744.89 | -12.96 | 744.59 |
| | +10.30 | | 742.59 |
| | 742.89 | | |
| TP | 732.46 | -12.90 | 731.99 |
| | +10.47 | | 729.99 |
| | 730.46 | | |
| | 722.33 | -13.00 | 719.46 |
| | +12.87 | | 717.46 |
| | 720.33 | | |
| TP 883+00 | 719.02 | -10.35 | 711.98 |
| | +7.04 | | 709.98 |
| | 717.02 | | |
| TP 893+00 | | -8.02 | 711.00 ✓ |
| | | | 709.00 |

Levels to S. Portal

| | | | |
|-----------|--------|-------------------|-------------------|
| | | | 711.00 |
| | | | 709.00 |
| | | 720.99 | |
| | +9.99 | 718.99 | |
| TP 900+00 | | | 710.30 |
| | | | 708.30 |
| | | 720.70 | |
| | +10.40 | 718.70 | |
| TP 910+00 | | | 709.30 |
| | | | 707.30 |
| | | 719.66 | |
| | +10.36 | 717.66 | |
| TP 921+00 | | | 708.70 |
| | | | 706.70 |
| | | 11.46 | |
| | | -7.46 | 710.20 |
| | | 720.02 | |
| | +11.82 | 718.02 | |
| TP 933+00 | | | 707.00 |
| | | | 705.00 |
| | | 718.00 | |
| | +11.00 | 716.00 | |
| TP 940+00 | | | 706.30 |
| | | | 704.30 |
| | | 717.44 | |
| | +11.14 | 715.44 | |
| TP 946+00 | | | 705.67 |
| | | | 703.67 |
| | | 713.60 | |
| | +7.93 | 711.60 | |
| TP 957+00 | | | 705.20 |
| | | | 703.20 |
| | | 715.97 | |
| | +10.77 | 713.97 | |
| TP 961+00 | | | 706.63 |
| | | | 704.63 |
| | | 712.76 | |
| | +6.13 | 710.76 | |
| TP 971+00 | | | 704.05 |
| | | | 702.05 |
| | | 711.78 | |
| | +7.73 | 709.78 | |

an. 27

ac. 49

✓
11-24

| | | | | |
|-----------|--------|-------------------------------|--------|-----------------------------|
| | | 711.78 ✓ 709.78 | | 702.48 700.48 |
| TP 973+50 | | | -9.30 | |
| | +10.86 | 713.34 711.34 | | |
| TP 975+50 | | | -11.06 | 702.28 700.28 |
| | +10.57 | 712.85 710.85 | -10.89 | |
| TP 978+50 | | | -10.87 | 701.98 699.18 |
| | +10.60 | 712.58 710.58 | | |
| TP 978+50 | | | -11.00 | 701.58 699.58 |
| | +11.25 | 712.83 710.83 | | |
| TP 986+50 | | | -11.65 | 707.18 699.18 |
| | +11.31 | 712.49 710.49 | | |
| TP 986+70 | | | -1.14 | 711.35 709.35 |
| | +12.07 | 723.42 721.42 | | |
| TP | | | -0.46 | 722.96 720.96 |
| | +12.23 | 735.19 733.19 | | |
| TP | | | -0.34 | 734.85 732.85 |
| | +12.36 | 747.21 745.21 | | |
| TP | | | -0.08 | 747.13 745.13 |
| | +12.30 | 759.43 757.43 | | |
| TP | | | -0.69 | 758.74 756.74 |
| | 109.55 | | 46.96 | |

Tunnel Portal

$$\sqrt{\frac{n}{2} - 24}$$

| | | | | |
|------------|--------|-------------------|--------|-------------------|
| | | 771.45 | | 758.74 |
| | +12.71 | 769.45 | | 756.74 |
| TP | | | -0.94 | 770.51 |
| | | | | 768.51 |
| | +8.54 | 779.05 | | |
| | | 777.05 | | |
| 850+00 | | | -10.77 | 768.28 |
| | | | | 766.28 |
| | +0.46 | 768.74 | | |
| | | 766.74 | | |
| TP | | | -13.02 | 755.72 |
| | | | | 753.72 |
| | +1.06 | 756.78 | | |
| | | 754.78 | | |
| TP | | | -12.99 | 743.79 |
| | | | | 741.79 |
| | +0.47 | 744.26 | | |
| | | 742.26 | | |
| TP | | | -12.63 | 731.63 |
| | | | | 729.63 |
| | +0.07 | 731.70 | | |
| | | 729.70 | | |
| TP | | | -13.03 | 718.67 |
| | | | | 716.67 |
| | +0.48 | 719.15 | | |
| | | 717.15 | | |
| TP | | | -12.51 | 706.64 |
| | | | | 704.64 |
| | +4.32 | 710.96 | | |
| | | 708.96 | | |
| TP 1010+00 | | | -11.30 | 699.66 |
| | | | | 697.66 |
| | +11.77 | 711.43 | | |
| | | 709.43 | | |
| P 1013+00 | | | -12.06 | 699.37 |
| | | | | 697.37 |
| | +11.57 | 710.94 | | |
| | | 708.94 | | |
| 99.45 | | | 51.45 | |

on Fletcher Bench 769.48

✓ 2
3-24

| | | | |
|---------|-------------------------------|-------------------------------|-----------------------------|
| | 710.94 ✓ 708.94 | | |
| TP 1016 | | -11.87 | 699.07 697.07 |
| | +12.27 | 711.34 709.34 | |
| TP | | -0.04 | 711.30 709.30 |
| | +11.96 | 723.26 721.26 | |
| TP | | -0.02 | 723.24 721.24 |
| | +12.29 | 735.53 733.53 | |
| TP | | -12.99 | 722.54 720.54 |
| | +0.47 | 723.01 721.01 | |
| TP | | -13.01 | 710.00 708.00 |
| | +1.04 | 711.04 709.04 | |
| | | -13.00 | 698.04 696.04 |
| | +4.66 | 702.70 700.70 | |
| TP 1031 | | -5.13 | 697.57 695.57 |
| | +8.55 | 706.12 704.12 | |
| 1040 TP | | -9.45 | 696.67 694.67 |
| | +11.33 | 708.00 706.00 | |
| 1040+50 | | -11.59 | 696.41 694.41 |
| | +5.29 | 701.70 ✓ 699.70 | |
| | 67.86 | 47.10 | |

$$\frac{2}{3.24}$$

2/5-24 40
 Van Horn
 Thompson
 Clear

701.70 ✓
 TP 1052 TP ~~699.70~~ - 6.28 695.42
 693.42
 706.77
 +11.35 704.79

Levels Down Siphon T same

TP -13.01 692.76
 691.76
 1185

+0.21 691.97
 TP ~~Abandoned~~ -13.00 678.97

+1.56 680.53
 TP -12.87 667.66

705.31
 TP +11.55 703.31 692.76
 691.76

TP 1058+40 -10.40 694.91
 692.91

705.04
 +10.13 703.04
 -10.26 694.78
 692.78

TP +5.85 700.63 ✓
 698.63 694.78

TP -5.85 698.63 692.78
 +3.85 696.63

1096+50 TP -9.140 689.23
 687.23
 +8.37 697.60 ✓
 695.60

2/4-24

on sugar loaf

697.60 ✓
~~695.60~~

~~2/4-24~~

| | | | |
|------------|-----------------------------|--------|--|
| TP 1099+50 | | -8.64 | 688.96 686.96 |
| +9.78 | 698.74 696.74 | | |
| TP 1104+50 | | -10.33 | 688.41 686.41 |
| +8.88 | 697.29 695.29 | | |
| TP | | -0.48 | 696.81 694.81 |
| +11.81 | 708.62 706.62 | | |
| TP | | -0.01 | 708.61 706.61 |
| +12.04 | 720.65 718.65 | | |
| TP | | -0.19 | 720.46 718.46 |
| +12.95 | 733.41 731.41 | | |
| TP | | -0.00 | 733.41 731.41 |
| +12.43 | 745.84 743.84 | | 745.32 743.32 |
| TP | | -0.52 | 45.72 12.42 58.28 744.36 |
| +12.96 | 758.28 757.32 | | |
| TP | | -0.00 | 758.28 757.32 |
| +12.39 | 770.57 769.61 | | |
| TP | | -0.00 | 770.57 769.61 |
| +11.86 | 782.43 781.47 | | |
| TP | 105.00 3.5 | -0.00 | 782.43 781.47 |
| | | 25.17 | 780.43 |

on Rock in Creek 20' N. line 705+80

~~2/5-24~~

| | | | |
|------|-------------------|-------|-------------------|
| | 795.30 | | 780.43 |
| | 493.30 | | 781.49 |
| | +12.87 | | |
| | 794.34 | | |
| TP | | -0.00 | 795.30 |
| | | | 794.34 |
| | 807.92 | | |
| | +12.62 | | |
| | 806.96 | | |
| TP | | -0.03 | 807.89 |
| | | | 806.93 |
| | 818.78 | | |
| | +10.89 | | |
| | 817.88 | | |
| 5+38 | | -3.10 | |
| TP | | -0.00 | 818.78 |
| | | | 817.88 |
| | 831.16 | | |
| | +12.38 | | |
| | 830.20 | | |
| TP | | -0.00 | 831.16 |
| | | | 830.20 |
| | 843.41 | | |
| | +12.25 | | |
| | 842.45 | | |
| TP | | -0.00 | 843.41 |
| | | | 842.45 |
| | 856.51 | | |
| | +13.10 | | |
| | 855.55 | | |
| R | | -0.00 | 856.51 |
| | | | 855.55 |
| | 869.53 | | |
| | +13.02 | | |
| | 868.59 | | |
| TP | | -0.00 | 869.53 |
| | | | 868.59 |
| | 882.39 | | |
| | +12.86 | | |
| | 881.43 | | |
| TP | | -0.00 | 882.39 |
| | | | 881.43 |
| | 893.22 | | |
| | +10.83 | | |
| | 892.22 | | |
| | 892.24 | | |
| | 110.54 | | |
| | 44 | | |

on sm. Rock in Rd.

893.22 ✓
~~891.22~~
~~892.26~~

4/6-24 Van Hook
Thomas
Clear. 43

TP -0.00 893.22
~~892.26~~

+12.81 906.03 ✓
~~905.07~~

TP -0.00 906.03 ✓
~~905.07~~

+12.15 918.18 ✓
~~917.22~~

TP -0.31 917.87 ✓
~~916.94~~

+12.96 930.83
~~929.87~~

TP -0.00 930.83
~~929.87~~

+11.75 942.58
~~941.62~~

TP -0.00 942.58
~~941.62~~

+12.21 954.79
~~953.83~~

TP -0.00 954.79
~~953.83~~

+13.02 967.81
~~966.85~~

TP -0.06 967.75
~~966.79~~

+12.78 980.53
~~979.57~~

Rock on Right edge of Road

TP -0.03 980.50
~~979.54~~

+13.05 993.58
~~992.62~~

TP -0.08 993.50
~~992.54~~

+12.86 1006.36 ✓
~~1005.40~~

113.62

58

1006.36 ✓
~~1004.86~~ ✓
1005.40

78.50
24.26
54.24

1004.36
54.24
50.12

44

TP -0.22

1006.14
~~1005.78~~

+12.52 1018.66
~~1017.70~~

TP -0.00

1018.66
~~1017.70~~

+7.57 1026.23
~~1025.27~~

Peg on Rt Side Rd.

TP -0.41

1025.82
~~1024.86~~

+1.33 1027.15
~~1026.19~~

TP -13.05

1014.10
~~1013.14~~

+0.10 1014.20
~~1013.24~~

TP -12.93

1001.27
~~1000.31~~

+0.25 1001.52
~~1000.56~~

h. w. Rd

88.59
19
88.78

82
28
4

TP -12.93

988.59
~~987.63~~

+0.19 988.78
~~987.82~~
~~985.82~~

951.09
1002

TP -13.01

975.77
~~975.81~~

+0.48 976.25
~~976.29~~

TP -12.94

963.31
~~963.35~~

+0.79 964.10
~~964.14~~

TP -13.01

951.09
~~951.13~~

+1.03 952.12 ✓
~~950.12~~
~~952.11~~

NH. 26

78.50

952.12
~~950.12~~ ✓
~~952.16~~

TP +12.98 -12.98

939.31
~~939.55~~

TP +0.17 -13.10

926.34
~~926.35~~

TP +0.10 -12.63

913.78
~~913.82~~

TP +0.10 -12.97

901.15
~~901.19~~

TP +0.34 -12.86

888.33
~~888.37~~

TP +0.04 -12.91

875.76
~~875.80~~

TP +0.34 -12.89

863.67
~~863.91~~

TP +0.80 -10.29

853.46
~~853.50~~

TP +0.08 -13.06

840.85 ✓
~~838.85~~
~~840.89~~

2.42 113.69

939.14
~~939.28~~

926.24
~~926.25~~

913.68
~~913.72~~

900.81
~~900.85~~

888.29
~~888.33~~

875.42
~~875.46~~

862.89
~~862.91~~

853.38
~~853.42~~

840.40
~~840.44~~

113.69
 2.42
~~111.27~~

950.12
 111.27
~~838.85~~

45
 52.12
 12.98
~~39.14~~

840.85
~~838.85~~
840.89

TP -13.02

827.94
+0.11 ~~827.98~~

TP -12.66

815.44
+0.16 ~~815.48~~

TP -13.06

802.84
+0.46 ~~802.88~~

TP -6.03

799.09
+2.28 ~~799.13~~

TP -5.93

793.72
+0.56 ~~793.76~~
1302

TP -13.02

784.76
+4.06 ~~784.80~~

TP -12.88

772.15
+0.27 ~~772.19~~

TP -8.61

767.48
+3.94 ~~767.52~~
8021
309

51823 11.82 -3.95

" 21 ³/₄ -11.55

827.83
~~827.89~~

815.28
~~815.32~~

802.38
~~802.42~~

796.81
~~796.85~~

793.16
~~793.20~~

780.70
~~780.74~~

771.88
~~771.92~~

763.54
~~761.54~~
~~763.54~~

755.93
~~753.93~~
455.99

Tunnel Portal

26

| | | | | | |
|------|-------|-------------------|--------|-------------------|--|
| H | | 765.04 ✓ | | 763.54 | |
| | +1.50 | 763.04 | | 761.54 | |
| H | | | -12.91 | 752.13 | |
| | +0.12 | 752.25 | | 750.13 | |
| | | 750.25 | | | |
| TP | | | -12.48 | 739.77 | |
| | +2.11 | 741.88 | | 737.77 | |
| | | 739.88 | | | |
| TP | | | -9.68 | 732.20 | |
| | +0.52 | 732.72 | | 730.20 | |
| | | 730.72 | | | |
| TP | | | -8.48 | 724.24 | |
| | +0.92 | 725.16 | | 722.24 | |
| | | 723.16 | | | |
| TP | | | -12.95 | 712.21 | |
| | +0.46 | 712.67 | | 710.21 | |
| | | 710.67 | | | |
| TP | | | -9.00 | 703.67 | |
| | +0.41 | 704.08 | | 701.67 | |
| | | 702.08 | | | |
| TP | | | -11.55 | 692.53 | |
| | +0.30 | 690.83 | | 690.53 | |
| | | | | | |
| △ | | | -8.07 | 84.76 | |
| | | | | 82.76 | |
| B.M. | | | -7.91 | 684.92 | |
| | | | | 682.92 | |
| | 6.34 | | -84.96 | | |

Abandoned

✓
2/6-24✓
2/6-24

Van Horn
Thomps.
Clear.

TP 682.92
+7.87 ~~690.79~~
692.79

1200+85²

~~693.57~~
~~691.57~~ 93
Cut ~~113~~

TP 1205+80
+10.87 ~~701.40~~
703.40
-0.59
702.81
~~700.81~~

+12.58 ~~713.39~~
715.39

TP -0.00
715.39
~~713.39~~

+12.82 ~~726.21~~
728.21

TP -0.00
728.21
~~726.21~~

+13.08 ~~739.29~~
741.29

TP -0.06
741.23
739.23

+12.99 ~~752.22~~
754.22

TP -0.00
754.22
~~752.22~~

+12.50 ~~764.72~~
766.72

TP -0.00
766.72
~~764.72~~

+12.84 ~~777.56~~
779.56

TP -0.11
779.45
~~777.45~~

+12.92 ~~790.37~~
792.37

TP -0.00
792.37
~~790.37~~

| | | | | Elev. |
|----|--|--|-------|-------------------|
| | | | 8.03 | |
| | | | | 792.37 |
| | | | | 790.37 |
| | | | | 804.86 |
| | | | | 802.86 |
| TP | | | -0.02 | |
| | | | | 817.93 |
| | | | | 815.93 |
| TP | | | -0.07 | |
| | | | | 817.86 |
| | | | | 815.86 |
| | | | | 830.73 |
| | | | | 828.73 |
| TP | | | -0.05 | |
| | | | | 830.68 |
| | | | | 828.68 |
| | | | | 843.64 |
| | | | | 841.64 |
| TP | | | -0.01 | |
| | | | | 843.63 |
| | | | | 841.63 |
| | | | | 851.94 |
| | | | | 849.94 |
| TP | | | -1.88 | |
| | | | | 844.06 |
| | | | | 842.06 |
| | | | | 856.26 |
| | | | | 854.26 |
| TP | | | -0.00 | |
| | | | | 856.26 |
| | | | | 854.26 |
| | | | | 868.86 |
| | | | | 866.86 |
| TP | | | -0.00 | |
| | | | | 868.86 |
| | | | | 866.86 |
| | | | | 880.92 |
| | | | | 878.92 |
| TP | | | -0.00 | |
| | | | | 880.92 |
| | | | | 878.92 |
| | | | | 893.31 |
| | | | | 891.31 |
| TP | | | -0.00 | |
| | | | | 893.31 |
| | | | | 891.31 |
| | | | | 906.03 |
| | | | | 904.03 |

EL

2/8-24

| | | | |
|----|--------------------|-------|-------------------|
| | 906.03 | | 906.00 |
| | 914.03 | | 904.00 |
| TP | | -0.03 | |
| | 918.96 | | 918.96 |
| | +12.96 | | 916.96 |
| TP | | -0.00 | |
| | 931.94 | | 916.96 |
| | +12.98 | | 931.89 |
| | 929.94 | | 929.89 |
| TP | | -0.05 | |
| | 944.44 | | 944.44 |
| | +12.55 | | 942.44 |
| TP | | -0.00 | |
| | 957.43 | | 942.44 |
| | +12.99 | | 957.43 |
| | 955.43 | | 955.43 |
| TP | | -0.00 | |
| | 970.35 | | 970.30 |
| | +12.92 | | 968.30 |
| | 968.35 | | 968.30 |
| TP | | -0.05 | |
| | 983.30 | | 983.30 |
| | +13.00 | | 981.30 |
| TP | | -0.00 | |
| | 995.90 | | 983.30 |
| | +12.60 | | 981.30 |
| | 993.90 | | 995.90 |
| TP | | -0.00 | |
| | 1008.64 | | 993.90 |
| | +12.74 | | 1008.64 |
| | 1006.64 | | 1008.64 |
| TP | | -0.01 | |
| | 1020.37 | | 1006.63 |
| | +11.74 | | 1020.37 |
| | 1018.37 | | |

11448
263

0.14

2/8-24

| | | | |
|--------|--------------------|--------|--------------------|
| | 1020.37 | | 1020.37 |
| | 1018.37 | | 1018.37 |
| TP | | -0.00 | |
| | 1033.12 | | 1033.12 |
| +12.75 | 1031.12 | -0.00 | 1031.12 |
| TP | | -0.00 | |
| | 1045.71 | | 1045.71 |
| +12.59 | 1043.71 | | 1043.71 |
| TP | | -0.00 | |
| | 1058.38 | | 1058.38 |
| +12.67 | 1056.38 | | 1056.38 |
| TP | | -0.00 | |
| | 1070.66 | | 1070.66 |
| +12.28 | 1068.66 | | 1068.66 |
| TP | | -0.04 | |
| | 1082.47 | | 1082.47 |
| +11.85 | 1080.47 | | 1080.47 |
| TP | | -0.18 | |
| | 1090.36 | | 1090.36 |
| +8.07 | 1088.36 | | 1088.36 |
| TP | | -12.88 | |
| | 1090.04 | | 1077.48 |
| +12.56 | 1088.04 | | 1075.48 |
| TP | | -2.93 | |
| | 1088.82 | | 1087.11 |
| +1.71 | 1086.82 | | 1085.11 |
| TP | | -12.88 | |
| | 1076.15 | | 1073.94 |
| +0.21 | 1074.15 | | |
| 84169 | | 2891 | |
| 244 | | 23 | |

✓
2/8-24

| | | | |
|-------|--------------------|----------|--------------------|
| | 1076.15 | | 1063.13 |
| | 1074.15 | | 1061.13 |
| | | -13.02 | |
| | 1063.65 | | |
| +0.52 | 1061.65 | | |
| TP | | -12.61 | 1057.04 |
| | 1051.80 | | 1049.04 |
| +0.76 | 1049.80 | | |
| TP | | -12.78 | 1039.02 |
| | 1037.98 | | 1037.02 |
| +0.96 | 1037.98 | | |
| TP | | -12.82 | 1027.16 |
| | 1027.32 | | 1025.16 |
| +0.16 | 1025.32 | | |
| TP | | -12.46 | 1014.86 |
| | 1014.92 | | 1012.86 |
| +0.06 | 1012.92 | | |
| TP | | -12.54 | 1002.38 |
| | 1002.70 | | 1000.38 |
| +0.32 | 1000.70 | | |
| TP | | +12.83 | 989.87 |
| | 990.32 | | 987.87 |
| +0.45 | 988.32 | | |
| TP | | -12.22 | 978.10 |
| | 978.30 | | 976.10 |
| +0.20 | 976.30 | | |
| TP | | -13.00 | 963.30 |
| | 965.62 | | |
| +0.32 | 963.62 | | |
| 9.75 | | 11 ↓ 0.8 | |
| 2.3 | | 2.42 | |

| | | | |
|----|--------------------------------------|---------------|-----------------------------|
| | 965.62 ✓ 963.62 | | 952.70 950.70 |
| TP | | -12.92 | |
| | +0.58 953.28 ✓ 951.28 | | |
| TP | | -12.75 | 940.53 938.53 |
| | +0.46 940.99 938.99 | | |
| TP | | -12.92 | 928.07 926.07 |
| | +0.64 928.71 926.71 | | |
| TP | | -12.77 | 915.94 913.94 |
| | +0.68 916.62 914.62 | | |
| TP | | -12.89 | 903.72 901.73 |
| | +0.18 903.71 901.91 | | |
| TP | | -13.06 | 890.85 888.85 |
| | +0.35 891.20 889.20 | | |
| TP | | -12.98 | 878.22 876.22 |
| | +0.0 878.22 876.22 | | |
| TP | | -12.53 | 865.69 863.69 |
| | +0.12 865.81 863.81 | | |
| TP | | -12.59 | 853.22 851.22 |
| | +0.13 853.35 ✓ 851.35 | | |
| | 3.14 34 | 115.48 265 | |

2/9-24

2/9-24 53
Williams
Van Horn
Thompson
Rain, P.M.

835.98
676.8
158.18

748
680
54

15.34
27
15.61

✓ 7/24

853.35

~~851.35~~

840.47

~~838.47~~

TP

840.56

-12.88

+0.09

~~839.56~~

827.98

~~825.98~~

TP

828.03

-12.58

+0.05

~~826.03~~

815.34

~~813.34~~

TP

815.67

-12.67

+0.27

~~813.59~~

802.77

~~800.77~~

TP

803.41

-12.86

+0.36

~~801.09~~

790.35

~~788.35~~

TP

790.65

-12.76

+0.30

~~788.65~~

778.00

~~776.00~~

TP

778.36

-12.65

+0.36

~~776.34~~

765.42

~~763.40~~

TP

765.80

-12.94

+0.38

~~763.78~~

752.86

~~750.86~~

TP

752.94

-12.94

+0.08

~~750.92~~

737.99

~~737.99~~

TP

740.41

-12.95

+0.42

~~739.41~~
~~738.39~~

2.31

115.25
75

Grade 77.30

2/9-24 55

2/9-24

740.41
738.41
~~738.39~~

TP

-12.70

727.71
~~725.71~~

+0.40
728.11
~~726.11~~

TP

-12.80

715.31
~~713.31~~

+0.34
715.65
~~713.65~~

TP

-12.42

703.23
~~701.23~~

+1.34
704.57
~~703.57~~

TP

-12.74

691.83
~~689.83~~

+1.52
691.35

TP

-12.84

678.51

2.60

2/9-24

+2.20
694.03
~~692.03~~

TP

-13.00

691.83
~~689.83~~
681.03
~~679.03~~

+1.14
682.17
~~680.17~~

TP

-2.87

679.30
~~677.30~~

+11.12
690.42
~~682.42~~

Begin flame sta 1280+78.5

1291 TP

-12.20

678.22
~~676.22~~

+9.03
687.25
~~685.25~~

TP

-9.37

697.88
~~695.88~~

+10.56
688.44
~~686.44~~
3405

3744

2/11-24
Van Horn
Thompson
Stout
Clear
Windy in P.M.

✓ 2-11-24

| | | | | |
|---------|-------------------|-------------------|------|-------------------|
| | 688.44 | | | 677.12 |
| | 686.44 | | | 675.12 |
| 1302 TP | | -11.32 | | |
| | 688.32 | | | 676.82 |
| | +11.20 | 686.32 | | 674.82 |
| TP 1305 | | ✓ -11.50 | | |
| | 689.78 | | | |
| | +12.96 | 687.78 | | |
| | | (-2.81) | 2.81 | 684.97 |
| TP | | -0.00 | | 689.78 |
| | | | | 687.78 |
| | 702.36 | | | |
| | +12.58 | | | |
| | 700.36 | | | |
| TP | | -0.00 | | 702.36 |
| | | | | 700.36 |
| | 714.92 | | | |
| | +12.56 | | | |
| | 712.92 | | | |
| TP | | -0.00 | | 714.92 |
| | | | | 712.92 |
| | 727.73 | | | |
| | +12.81 | | | |
| | 725.73 | | | |
| TP | | -0.02 | | 727.71 |
| | | | | 725.71 |
| | 735.42 | | | |
| | +7.71 | | | |
| | 733.42 | | | |
| | | | | |
| TP | | -12.94 | | 722.48 |
| | | | | 720.48 |
| | 722.53 | | | |
| | +0.05 | | | |
| | 720.53 | | | |
| TP | | -13.02 | | 709.51 |
| | | | | 707.51 |
| | 709.66 | | | |
| | +0.15 | | | |
| | 707.66 | | | |
| TP | | -13.00 | | 696.66 |
| | | | | 694.66 |
| | 696.77 | | | |
| | +0.11 | | | |
| | 694.77 | 61.80 | | |

Tunnel Portal 1309+25

696.77
~~694.77~~

TP

-12.96

~~683.81~~
~~681.87~~

+0.57
684.38
~~682.38~~

TP

-8.38

676.00
~~674.00~~

+10.75
686.75
~~684.75~~

1323 TP

-11.43

675.32
~~673.32~~

+12.48
687.80
~~675.80~~

-8.28

77.52

TP 1327

-5.37

682.43
~~680.43~~

+12.23
694.66
~~692.66~~

Tunnel

TP

-0.20

694.46
~~692.46~~

+12.96
707.42
~~705.42~~

TP

-0.01

707.42
~~705.41~~

+12.82
720.23
~~718.23~~

TP

-0.28

719.95
~~717.95~~

+11.97
731.92
~~729.92~~

TP

-0.00

731.92
~~729.92~~

+12.73
744.65
~~742.65~~

TP

-0.00

744.65
~~742.65~~

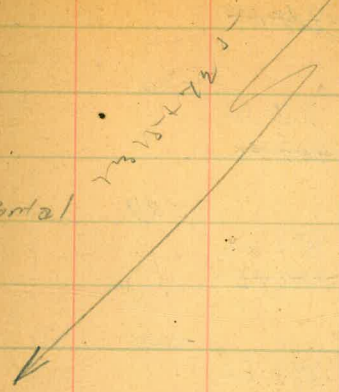
+12.72
757.37
~~755.37~~

4923
64

38.63

11-24

1/12-24 Jan Horn 57
Thompson
Windy in P.M.



| | | | | | |
|----|--------|-------------------|-------|-------------------|--|
| | | 757.37 | | | |
| | | 755.37 | | | |
| TP | | | -0.0 | 757.37 | |
| | | 769.50 | | 755.37 | |
| | +12.13 | 767.50 | | | |
| TP | | | -0.09 | 769.41 | |
| | | 782.42 | | 767.41 | |
| | +13.01 | 780.42 | | | |
| TP | | | -0.0 | 782.42 | |
| | | 795.52 | | 780.42 | |
| | +13.10 | 793.52 | | | |
| TP | | | -0.0 | 795.52 | |
| | | 808.62 | | 793.52 | |
| | +13.10 | 806.62 | | | |
| TP | | | -0.01 | 808.61 | |
| | | 821.53 | | 806.61 | |
| | +12.92 | 819.53 | | | |
| TP | | | -0.0 | 821.53 | |
| | | 834.36 | | 819.53 | |
| | +12.83 | 832.36 | | | |
| TP | | | -0.0 | 834.36 | |
| | | 847.39 | | 832.36 | |
| | +13.03 | 845.39 | | | |
| TP | | | -0.01 | 847.38 | |
| | | 860.31 | | 845.38 | |
| | +12.93 | 858.31 | | | |
| TP | | | -0.0 | 860.31 | |
| | | 872.99 | | 858.31 | |
| | +12.68 | 870.99 | | | |
| | | 875.63 | | | |
| | | 115.73 | | | |
| | | 232 | | | |

12-24

40.3
12.0
~~72.9~~

872.99
~~870.99~~
~~845.63~~

72.99
45.63 59
27.36

TP 872.99
-0.0
~~845.63~~

886.08
+13.09 ~~858.72~~
27.36

TP 885.98
-0.10
~~858.62~~

898.99
+13.01 ~~871.63~~

TP 898.99
-0.0
~~871.63~~

912.04
+13.05 ~~884.68~~

TP 912.00
-0.04
~~884.64~~

924.99
+12.99 ~~897.63~~

TP 924.99
-0.0
~~897.63~~

938.00
+13.01 ~~910.64~~

TP 938.00
-0.0
~~910.64~~

950.86
+12.86 ~~929.50~~

TP 950.85
-0.01
~~929.49~~

963.66
+12.81 ~~936.30~~

TP 963.65
-0.01
~~936.29~~

12.38 976.03
948.67

TP 975.91
-0.12
~~948.55~~

988.93
+13.02 ~~986.93~~
961.57

116.22
234 28

988.93
~~986.93~~
~~961.57~~

TP -0.10

1001.70
+12.87 ~~974.34~~

TP -0.03

1014.58
+12.91 ~~987.22~~

TP -0.12

1027.37
TP +12.91 ~~1000.02~~ $\frac{1}{2}$ $\frac{1}{2}$ -0.01

1039.30
+11.92 ~~1011.94~~

TP -4.87

1040.00
+6.01 ~~1013.08~~

TP -11.90

1029.17
+0.63 ~~1027.17~~

TP -12.98

1017.25
+1.06 ~~1015.25~~

TP -13.09

1005.62
+1.46 ~~1003.62~~

TP -12.81

993.15
+0.34 ~~991.15~~

-12.95

980.43
+0.23 ~~978.43~~

988.83

~~961.47~~

1001.67

~~974.31~~

1014.46

~~987.10~~

1027.38

~~1000.02~~

1034.43

~~1007.07~~

1028.54

~~1026.54~~

~~1000.18~~

1016.19

~~1014.19~~

1000.16

~~1002.16~~

992.81

~~990.81~~

980.20

~~978.20~~

27.36

12-24

Williams
Van Horn
Thompson
clear

| | | | |
|-------|---------------------|--------|-------------------|
| | 980.43 | | |
| | + 978.43 | | |
| TP | | -12.83 | 967.60 |
| | 967.68 | | 965.68 |
| +0.08 | 965.68 | | |
| TP | | -13.02 | 954.66 |
| | 956.11 | | 952.66 |
| +1.45 | 954.11 | | |
| TP | | -12.98 | 943.14 |
| | 944.27 | | 941.14 |
| +1.13 | 942.27 | | |
| TP | | -13.01 | 931.26 |
| | 931.78 | | 929.26 |
| +0.52 | 929.78 | | |
| TP | | -12.97 | 918.81 |
| | 919.54 | | 916.81 |
| +0.73 | 917.54 | | |
| TP | | -12.76 | 906.78 |
| | 907.05 | | 904.78 |
| +0.27 | 905.05 | | |
| TP | | -12.85 | 894.20 |
| | 894.73 | | 892.20 |
| +0.53 | 892.73 | | |
| TP | | -12.95 | 881.78 |
| | 881.97 | | 879.78 |
| +0.19 | 879.97 | | |
| TP | | -12.96 | 869.01 |
| | 870.05 | | 867.01 |
| +1.04 | 868.05 | | |

870.05
~~868.05~~

TP -12.97

+0.79
857.87
~~855.87~~

857.08
~~855.08~~

TP -12.85

+0.22
845.24
~~843.24~~

845.02
~~843.02~~

TP -12.96

+1.02
833.30
~~831.30~~

832.28
~~830.28~~

TP -12.93

+0.60
820.97
~~818.97~~

820.37
~~818.37~~

TP -12.97

+0.27
808.27
~~806.27~~

808.00
~~806.00~~

TP -12.43

+0.31
796.15
~~794.15~~

795.84
~~793.84~~

TP -13.04

+0.29
783.40
~~781.40~~

783.11
~~781.11~~

TP -13.09

+0.23
770.54
~~768.54~~

770.31
~~768.31~~

TP -13.00

+0.13
757.67
~~755.67~~

757.54
~~755.54~~

5/2 17

830.90
784.11

46.79

832.24
830.90

1.34
62

| | | | |
|----|-----------------------------------|--------|-----------------------------|
| | 757.67 755.67 | | 745.00 743.4 |
| TP | 745.43 +0.39 743.43 | -12.63 | |
| | 732.79 +0.10 730.79 | -12.74 | 732.69 730.64 |
| TP | 720.54 +0.47 718.54 | -12.72 | 720.07 718.07 |
| TP | 708.85 +0.84 706.85 | -12.53 | 708.01 706.01 |
| TP | 696.22 +0.48 694.22 | -13.11 | 695.70 693.74 |
| TP | 683.55 +0.41 681.55 | -13.08 | 683.10 681.14 |
| TP | 671.20 +0.50 669.20 | -12.85 | 670.70 668.70 |
| TP | 663.49 +1.01 661.49 | -18.72 | 662.58 660.48 |
| TP | 650.94 +0.37 648.94 | -12.92 | 650.57 648.57 |

650.94
~~648.94~~

TP

-12.53

638.41
~~636.41~~

+0.24
638.65
~~636.65~~

TP

-12.92

625.73
~~623.73~~

+0.35
626.08
~~624.08~~

TP

-12.86

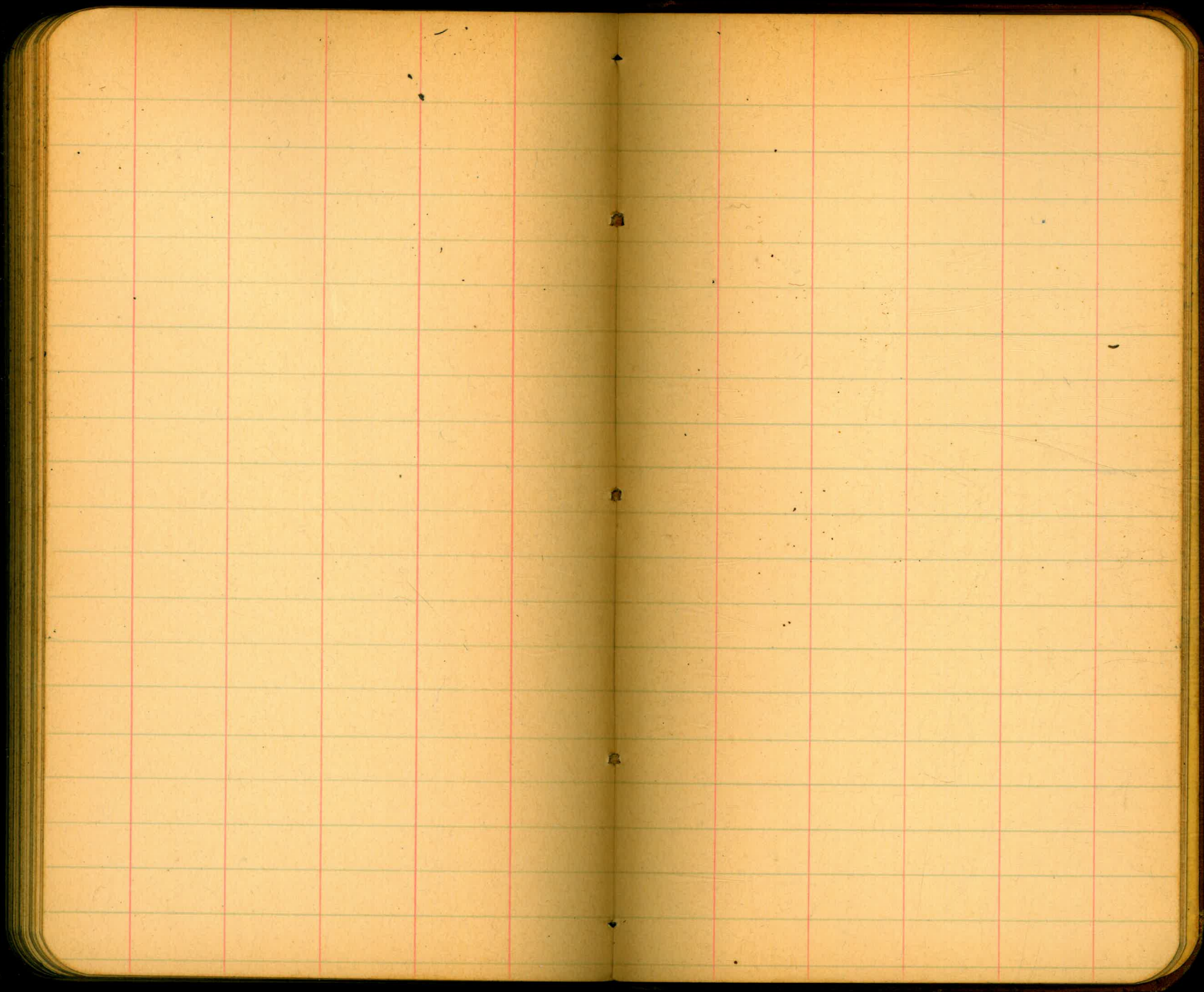
613.32
~~611.22~~

+0.59
613.81
~~611.81~~

-4.68

609.13
~~607.13~~

69.



Profile thru Throat 334+50 to

Proposed Plume from Reda Canyon Dam

334+50 765.73

+13.7

335+00 779.43

+ .9

335+50 780.33

-15.2

336+35 765.33

Profile thru Thru cut sta 238+00 to 240+50

P, Proposed Flume from Roden Canyon Dam site

| | | |
|--------|-------|--------|
| 238+00 | +11.8 | 775.38 |
| | +11.8 | |
| 238+50 | | 787.18 |
| | +12.7 | |
| 239+00 | | 799.88 |
| | +2.2 | |
| 239+30 | | 802.08 |
| | -2.2 | |
| 239+50 | | 799.88 |
| | -18.8 | |
| 240+00 | | 781.08 |
| | -6.3 | |
| 240+50 | | 774.78 |

563 34.20 W
N 81° 25' 40" W
145 00 00
35° Lt 250'

51° 09 Rt 55.43

190
125
35°

N 65° 16' 40" W
563 34 20 W
128 51 00
51° 09 Rt 74

15-24

Middletown

Harasity SE. Cor Hd spk. Pole grd 57,736

(Brewery)

E of Malt House - Inside Santa Fe

Right of Way 6' SE, Pole Witness

brass Plug Concrete monument 10.151

(26 + main st)

about 20' East of NE. Cor flush with

walk near prop Brass Plug Con Mon. 25.725

(26 main st)

North Bolt of fire Hydr 28.109

(Engsbee) + main

SE Cor north bolt of fire Hydr 14.721

(Main st) national city dyke 1st City Limits

N.W. Men 13.065

788.79
12.27

776.52
8.76

885.28

77.57
8.76

86.28

LA Playa B. M. ²

Bessmer Street + Rosecrans - N.W. Plug Curb 28.051
 Ha. Rogers Street + " N.E. Plug Curb 45.135
 Qual Trough St + " S.E. Plug Curb 64.074
 E. Perry St. + " N.E. Plug Curb 64.154
 Ft. Owens St + " S.E. Plug Curb 48.064
 br. Nichols St + " N.E. Plug Curb 41.645
 McCall St + " N.W. Plug Curb 38.135
 ab. Lawrence + " N.E. Plug Curb 35.094

W.

Roseville

Dewell + Rosecrans S.W. Plug Curb 8063
 S. Jarvis + " S.W. R.R. Spk Pole 4.643
 (M) Hugo + " " " " 2.163
 N. Goethe (Garrison) ^{New} " S.W. Plug Curb 1.145
 Emerson S.W. R.R. Spk Pole 5.741
 Carleton S.W. Plug Curb 14.554
 Addison S.W. R.R. Spk Pole 20.378

5.218
4600
0.615

7.888
3.005
4.883
4.876

9.823
5.007
4.816

4.1721
815
~~5.986~~
4.106

3.309
2.020
1.289
4.060
5.349

00.96
16
99.4

10007
670
483

000 0.07

390. - 89° 24'

42.77
2873
12831
34716
3408554
121.2391

14.130
8.063
6.067
8912
293
6

11.975

825
121.24
03.76

491
293
1473
4419
982
14386

8.721
3.309
5.412

102.64
96.15
6.490
5.412
6.082

6.112
6037.
082

8.455
266
8721
~~8721~~
~~8721~~
~~8721~~

40.96
24
16.354
11.77
78.240
200
10.8

54.106
48.064
6.037

8.441
2640
5.811

8721
266
8721
266
8721

825
16650
29.70

42.77
3.9
38473
12831
166.803

42.775
2.93
14832
38493
8854
125.2161 W

825
125.32
99.62

" Trade 1" = 8.45

1494
102.636
6.49
96.15
5-7

3.45

4565.845 =
649
1.96
202
06