

W 170

FIELD BOOK

361

CITY OF
SAN DIEGO - CALIFORNIA
1710 FOOT BARRETT CONTOUR
TRAVERSE, LAND-LINE TIES.

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

FOR KEITH'S RAILROAD CURVE TABLES SEE END OF BOOK.

MICROFILMED

JAN 8 1965

Index.

Traverse Sta. 100 to 606 + 45.3 - - - - 1-57

Azimuth Checks - - - - - 58-59

MICROFILMED

JAN 8 1985

Traverse 1710 Barrett Res⁵ Contour

Sta	Dist	Lt	Rt	Az	Mag Co
π@Δ1					
FS on stake (500 pg. 59 for Polaris Ob.)				331-05	
to Δ2	150.3		✓	45-51	N45-40E
to sec. cor.			✓	38-28 $\frac{1}{2}$	N38-25E
π@Δ2-1450.7					
BS on Δ1					N46-30E
to Δ3	195.7		✓	27-27	N28-00E
π@Δ3-3446.0					
BS on Δ2					N27-20E
to Δ4	146.0		✓	61-46	N61-35E
π@Δ4-4920					
BS on Δ3					N61-50E
to Δ5	103.3		✓	80-26	N80-20E
π@Δ5-5795.3					
BS on Δ4					
to Δ6	123.0		+	358-40 $\frac{1}{2}$	N1-40W
π@Δ6-7418.3					
BS on Δ5					
to Δ7	182.9		✓	58-43	N58-30E
π@Δ7-9012					
BS on Δ6					N58-30E
to Δ8	153.6		✓	100-54	S79-05E
π@Δ8-10544.8					
BS on Δ7					
to Δ9	134.7		✓	324-45	N35-10W

Litz Transit #5223
Ded. Plate @ 14°30'E

R.C. Wugst
Ed. Ketchum
O.S. Palmer

PM 12-26-22 (fine)

= hub on 1710 contour on Lt Barrett Dam Tangent
13' Downstream from focal
pt on Lt tangent on 3' offset produced to Rt bank

N45-51E

¼ cor bet. sacs. 15 and 22 (1988.5 ft by triangulation)

N27-27E

N61-46E

+ on Rk.

N80-26E

N1-19W

N58-43E

+ on Rk.

12-27-22

R.C. Wugst
Ed. Ketchum
O.S. Palmer

S79-06E

N35-15W

Co.	Sta.	Dist.	Defl.	Az.	Mag Co
π@Δ9	11+89.5				
B.S. on Δ8					
to Δ10		75.1	-	349-59½	N10-10W
π@Δ10	12+646				
B.S. on Δ9					
to Δ11		68.2	/	30-31	N30-15E
π@11	13+328				
B.S. on Δ10					
to Δ12		75.1	/	65-55	N65-55E
π@Δ12	14+079				
B.S. on Δ11					
to Δ13		118.8	/	27-53	N27-50E
π@Δ13	15+267				
B.S. on Δ12					
to Δ14		81.3	/	33-17	N33-15E
to Sec. Cor.				34-54	N34-50E
π@Δ14	16+080				
B.S. on Δ13					
to Δ15		119.3	+ /	61-29½	N61-15E
π@Δ15	17+273				
B.S. on Δ14					
to Sec. Cor.				29-50½	N29-45E
to Δ16		161.1	/	97-47	582-10E
π@Δ16	18+884				
B.S. on Δ15					282-10E
to Δ17		180.3	/	47-36	N47-35E

					N10-00W
					N30-31E
to on Rk					
					N65-55E
					N27-53E
to on Rk					
					N33-17E
					N61-30E
to on Rk					
					582-13E
					N47-36E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @A25	28+206				
BS.07A24					
to A 26		108.1	✓	2-18	N2-15E
π @A26	29+28.7				
BS.07A25					
to A 27		73.0	+ ✓	12-00 $\frac{1}{2}$	N12-00E
π @A27	30+01.7				
BS.07A26					
to A 28		64.1	✓	47-50	N47-45E
π @A28	30+65.8				
BS.07A27					
to A 29		179.0	✓	355-15	N4-45W
π @A29	32+44.8				
BS.07A28					
to A 30		68.9	✓	319-04	N40-55W
π @A30	33+13.7				
BS.07A29					
to A 31		56.9	✓	358-54	N1-05W
π @A31	33+70.6				
BS.07A30					
to A 32		180.0	✓	34-39	N34-40E
π @A32	35+50.6				
BS.0731					
to A 33		104.7	- ✓	82-22 $\frac{1}{2}$	N82-30E

N2-18E

N12-01E

N47-50E

N4-45W

N40-56W

N1-06W

N34-39E

N82-22E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@ 41	47+37.35				
B.S. on 40					
to 42		180.05	✓	309-48	N49-55W
π@ 42	49+17.4				
B.S. on 41					
to 43		229.6	✓	274-46	N85-10W
π@ 43	51+47.0				
B.S. on 42					
to 44		83.35	✓	355-02	N5-05W
π@ 44	52+30.35				
B.S. on 43					
to 45		222.0	✓	30-37	N30-25E
π@ 45	54+52.35				
B.S. on 44					
to 46		146.85	✓	299-40	N59-50W
π@ 46	55+99.2				
B.S. on 45					
to 47		126.8	✓	319-38	N40-25W
π@ 47	57+26.0				
B.S. on 46					
to 48		75.2	-✓	253-38 ¹ / ₂	S73-50W
π@ 48	58+01.2				
B.S. on 47					
to 49		81.7	✓	317-34	N42-30W
	58+82.9				

1145.55 ✓

6

	N50-12W
tan rock	
	N85-14W
	N4-58W
	N30-37E
	N60-20W
	N40-22W
	S73-38W
	N42-26W

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 49	58+829				
B.S. on 48					
to $\Delta 1$	0+00			179-21 $\frac{1}{2}$	50-55E
to 50		138.5	+ ✓	354-58 $\frac{1}{2}$	N5-15W
π @ 50	60+21.4				
B.S. on 49					
to 51		6.4	- ✓	18-57 $\frac{1}{2}$	N18-45E
π @ 51	60+828				
B.S. on 50					
to 52		66.65	✓	61-26	N61-10E
π @ 52	61+49.45				
B.S. on 51					
to 53		110.1	+ ✓	14-57 $\frac{1}{2}$	N14-55E
π @ 53	62+59.55				
B.S. on 52					
to 54		124.1	✓	309-06	N51-00W
π @ 54	63+83.65				
B.S. on 53					
to 55		186.9	- ✓	28-00 $\frac{1}{2}$	N27-45E
π @ 55	65+70.55				
B.S. on 54					
to 56		108.35	+ ✓	59-17 $\frac{1}{2}$	N59-05E
π @ 56	66+78.9				
B.S. on 55					
to 57		218.5	✓	359-51	N0-15W
		1014.50 ✓			

For Az. Check see page

N5-01W

1230-22 (fine)

R.S. Muessta
Ed. Ketchum
O.G. Palmer
P. Horan

N18-52E

N61-26E

N14-58E

Note: This Co. over rocky point
+ on rock

41.15 @ - 21°39'
75.32 @ - 14°36'

N50-54W

N28-00E

N59-18E

N0-09W

Co.	Sta	Dist	Defl.	Az.	Mag. Co.
π@ 57	68+97.4				
B.S. on 56					
to 58		77.8	-	✓ 305-43½	N54-10W
π@ 58	69+75.2				
B.S. on 57					
to 59		45.2	+	✓ 355-03½	N5-05W
π@ 59	70+20.4				
B.S. on 58					
to 60		113.0	-	✓ 0-11½	North
π@ 60	71+33.4				
B.S. on 59					
to 61		133.55	✓	324-51	N35-05W
π@ 61	72+66.95				
B.S. on 60					
to 62		82.2	✓	75-33	N75-40E
π@ 62	73+49.15				
B.S. on 61					
to 63		110.9	+	✓ 104-27½	S75-25E
π@ 63	74+60.05				
B.S. on 62					
to 64		203.65	-	✓ 123-59½	S56-00E
π@ 64	76+63.7				
B.S. on 63					
to 65		212.3	✓	168-12	S11-30E
		978.60			

	N54-17W
	N4-56W
	N0-11E
	N35-09W
	N75-33E
= first Co. on Cottonwood arm of reservoir.	
	S75-32E
	S56-01E
	S11-48E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 65	78+760				
BS on 64					
to 66		105.6		\checkmark 93-20	586-10E
π @ 66	79+81.6				
BS on 65					
to 67		84.8		\checkmark 75-59	N76-10E
π @ 67	80+664				
BS on 66					
to 68		186.8		\checkmark 101-40	578-15E
π @ 68	82+532				
BS on 77					
to 69		1650		\checkmark 77-24	N77-30E
π @ 69	84+182				
BS on 68					
to 70		117.5		\checkmark 154-22	525-30E
π @ 70	85+357				
BS on 69					
to 71		96.75		+ \checkmark 103-24 $\frac{1}{2}$	576-20E
π @ 71	86+324.5				
BS on 70					
to 72		750		\checkmark 115-45	563-50E
π @ 72	87+07.45				
BS on 71					
to 73		140.3		- \checkmark 75-47 $\frac{1}{2}$	N75-55E
	88+47.75				
	971.75 \checkmark				

586-40E

N75-59E

578-20E

N77-24E

525-38E

576-35E

+ on rock

564-15E

N75-47E

1-1-23 (fine/muddy
in PM)
R.C. Wueste
Ed. Kitchum
O.E. Palmer
P. Horan

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 81	95+05.6				
BS. 0780					
to 82		221.85	-	\checkmark 168-58 $\frac{1}{2}$	510-55E
π @ 82	97+27.45				
BS. 0781					
to 83		119.7	+	\checkmark 96-29 $\frac{1}{2}$	583-15E
π @ 83	98+47.15				
BS. 0782					
to 84		146.4	-	\checkmark 151-49 $\frac{1}{2}$	528-05E
π @ 84	99+93.55				
BS. 0783					
to 85		77.45	+	\checkmark 181-32 $\frac{1}{2}$	51-35W
π @ 85	100+71.0				
BS. 0784					
to 86		123.25	-	\checkmark 108-53 $\frac{1}{2}$	570-50E
π @ 86	101+94.25				
BS. 0785					
to 87		159.25	\checkmark	96-34	583-30E
π @ 87	103+53.5				
BS. 0786					
to 88		45.75	\checkmark	147-17	532-50E
π @ 88	103+99.25				
BS. 0787					
to 89		133.25	\checkmark	196-42	517-05W
	105+32.5				
		1026.90			

511-02E

583-30E

528-11E

51-33W

571-07E

1-2-23 (East wind)

R.C. Wueste
 Ed. Ketchum
 O.C. Palmer
 F. Horan

583-26E

532-43E

516-42W

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@ 89	105+32.5				
BS on 88					
to 90		121.25		✓ 121-49	558-10E
π@ 90	106+53.75				
BS on 89					
to 91		163.05		✓ 103-00	576-50E
π@ 91	108+16.8				
BS on 90					
to 92		54.15		+ ✓ 9-40½	N9-35E
π@ 92	108+70.95				
BS on 91					
to 93		210.1		✓ 48-54	N48-45E
π@ 93	110+81.05				
BS on 92					
to 94		68.65		- ✓ 99-13½	580-40E
π@ 94	111+49.7				
BS on 93					
to 95		70.5		+ ✓ 138-51½	541-05E
π@ 95	112+202				
BS on 94					
to 96		878		✓ 148-41	531-20E
π@ 96	113+080				
BS on 95					
to 97		1960		✓ 102-02	578-05E
	115+040				
		971.50			

					558-11E
					577-00E
					Copper tack in disintegrated rock
					N9-41E
					N48-54E
					580-47E
					541-08E
					531-19E
					577°58E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@97	115+04.0				
B.S. on 96					
to 98		65.45	✓	137-41	542-40E
π@98	115+69.45				
B.S. on 97					
to 99		70.8	✓	75-19	N75-00E
π@99	116+40.25				
B.S. on 98					
to 100		103.05	✓	48-51	N48-10E
π@100	117+43.3				
B.S. on 99					
to 101		123.55	✓	1-41	N1-20E
π@101	118+66.85				
B.S. on 100					
to 102		54.4	✓	45-16	N45-05E
π@102	119+21.25				
B.S. on 101					
to 103		74.25	-	102-3 1/2	577-10E
π@103	119+95.5				
B.S. on 102					
to 104		135.9	+	115-43 1/2	563-05E
π@104	121+31.4				
B.S. on 103					
to 105		146.9	x	129-43	550-00E
	122+783				
		774.30	✓		

					542-19E
					N75-19E
					N48-51E
					N1-41E
					N45-16E
				Above rock dike	
					577-29E
					564-16E
					550-17E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@105	122+78.3				
BS. on 104					
to 106		144.3		X 142-42	536-05E
π@106	124+226				
BS. on 105					
to 107		89.0		X 111-52	567-15E
π@107	125+11.6				
BS. on 106					
to 108		79.8		X 123-42	555-15E
π@108	125+91.4				
BS. on 107					
to 109	✓1	120.6		X 157-11	522-10E
π@109	127+12.0				
BS. on 108					
to 110		81.15		-X 203-08 $\frac{1}{2}$	525-05W
π@110	127+93.15				
BS. on 109					
to 111		257.6		X 151-15	527-05E
π@111	130+50.75				
BS. on 110					
to 112		209.0		X 119-46	560-00E
π@112	132+59.75				
BS. on 111					
to 113		99.4		X 161-07	518-30E
	133+59.15				
	1080.85✓				

	+ on rock		
Ⓟ		537-18E	
	+ on rock		
Ⓟ		568-08E	
Ⓟ		556-18E	
Ⓟ		522-50E	
Ⓟ		523-07W	
Ⓟ		528-46E	
		560-15E	
	(Favorable for connection to island)		
		518-54E	1-3-23 (fine)
			R.C. Wueste Ed. Ketchum
			O.C. Palmer P. Horan

Either static or compass glass
 or local attraction

Co.	Sta.	Dist.	Defl.	Az	Mag. Co.
π @ 137	159+133.4				
BS on 136					
to 138		51.3	X	264-21	S84-10W
π @ 138	159+84.7				
BS on 137					
to 139	✓ 5	151.2	+ X	327-53 $\frac{1}{2}$	N32-30W
π @ 139	161+35.9				
BS on 138					
to 140		109.05	- X	195-14 $\frac{1}{2}$	S15-05W
π @ 140	162+44.95				
BS on 139					
to 141		42.6	+ X	236-31 $\frac{1}{2}$	S56-25W
π @ 141	162+87.55				
BS on 140					
to 142		229.7	X	304-39	N55-30W
π @ 142	165+17.25				
BS on 141					
to 143		199.15	X	146-05	S34-10E
π @ 143	167+16.4				
BS on 142					
to 144		84.65	- X	210-11 $\frac{1}{2}$	S30-00W
π @ 144	168+01.05				
BS on 143					
to 145	✓ 6	113.0	+ X	292-04 $\frac{1}{2}$	N68-05W
	169+14.05				
	480.65 ✓				

Head of wooded draw with spring

S84-17W

N32-11W

S15-09W

S56-27W

N55-26W

S34-00E

S30-06W

N68-01W

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@145	169+14.05				
BS on 144					
to 146		132.9		X 146-01	S34-05E
π@146	170+46.95				
BS on 145					
to 147		146.6		X 203-15	S23-05W
π@147	171+88.55				
BS on 146					
to 148		219.5		X 244-09	S64-05W
π@148	174+08.05				
BS on 147					
to 149		141.2		- X 94-13½	S85-53E
π@149	175+49.25				
BS on 148					
to 150		144.6		X 176-46	S3-20E
π@150	176+93.85				
BS on 149					
to 151	✓	78.55		X 103-10½	S76-45E
π@151	177+72.4				
BS on 149					
to 152		80.75		X 34-28½	N34-15E
π@152	178+53.15				
BS on 151					
to 153		140.7		X 78-02	N77-50E
	179+93.85				
	1079.803				

19

	S34-05E
	S23-09W
West side Cement Road	
	S64-03W
	S85-53E
	S3-20E
+ on rock	
	S76-56E
Copper tack in disintegrated boulder.	
	N34-21E
	N77-55E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@161	191+69.35				
BS. on 160					
to 162		56.3	X	93-23	S86-35E
π@162	192+25.65				
BS. on 161					
to 163	✓ ₉	110.1	- X	337-30½	N22-35W
π on 163	193+35.75				
BS. on 162					
to 164		127.4	+ X	356-48½	N3-35W
π@164	194+63.15				
BS. on 163					
to 165		56.65	- X	28-03½	N27-30E
π@165	195+19.8				
BS. on 164					
to 166		132.9	X	125-25	S54-40E
π@166	196+52.7				
BS. on 165					
to 167		184.7	X	26-53	N26-45E
π@167	198+37.4				
BS. on 166					
to 168		190.4	X	97-01	S83-00E
π@168	200+27.8				
BS. on 167					
to 169	✓ ₁₀	158.7	X	356-27	N3-50W
	201+86.5				
	1017.15 ✓				

along steep sloping rock face

S86-45E

In gulch with tanks

N22-39W

N3-20W

N27-54E

S54-44E

N26-44E

S83-08E

top rock

N3-43W

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @169	201+86.5				
BS on 168					
+o 170	76.9		+ X	47-48 $\frac{1}{2}$	N47-35E
π @170	202+63.4				
BS on 169					
+o 171	187.1		X	101-02	579-05E
π @171	204+50.5				
BS on 170					
+o 172	178.8		- X	109-25 $\frac{1}{2}$	570-45E
π @172	206+29.3				
BS on 171					
+o 173	191.9		X	97-36	582-30E
π @173	208+21.2				
BS on 172					
+o 174	86.5		+ X	101-07 $\frac{1}{2}$	579-00E
π @174	209+07.7				
BS on 173					
+o 175	89.8		- X	84-30 $\frac{1}{2}$	N84-25E
π @175	209+97.5				
BS on 174					
+o 176	82.1		+ X	108-54 $\frac{1}{2}$	571-10E
π @176	210+79.6				
BS on 175					
+o 177	300.5		- X	127-06 $\frac{1}{2}$	553-05E
	213+80.1				
	1193.6				

N47-39E

579-08E

570-45E

582-34E

579-02E

N84-19E

571-16E

553-05E

1-6-23 (Final)

R.C. Wueste
Ed. Katchum
O.C. Palmer
P. Moran

Co.	Sta.	Dist	Defl.	Az.	Mag. Co.
π @177	213+80.1				
B.S. on 176					
+o 178		953		+x 90-29 $\frac{1}{2}$	589-30E
π @178	214+75.4				
B.S. on 177					
+o 179		989		x 58-01	N57-50E
π @179	215+74.3				
B.S. on 178					
+o 180		523		-x 128-26 $\frac{1}{2}$	551-35E
π @180	216+26.6				
B.S. on 179					
+o 181	\checkmark_{12}	60.85		x 53-57	526-15E
π @181	216+87.45				
B.S. on 180					
+o 182		174.0		x 89-13	N89-01E
π @182	218+61.45				
B.S. on 181					
+o 183		762		+x 53-40 $\frac{1}{2}$	N53-29E
π @183	219+37.65				
B.S. on 182					
+o 184		993		-x 117-18 $\frac{1}{2}$	562-50E
π @184	220+36.95				
B.S. on 183					
+o 185	\checkmark_{13}	203.3		+x 115-24 $\frac{1}{2}$	564-30E
	222+40.25				
	860.15				

	589-41E
	N57-50E
	551-45E
	526-15E
	N89-01E
+ on rock	
	N53-29E
+ on rock (sloping rock face)	
	562-54E
+ on rock (sloping rock face)	
	564-48E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 185	222+40.25				
BS. on 184					
to 186		2585	-	33-42 $\frac{1}{2}$	N33-20E
π @ 186	224+98.75				
BS. on 185					
to 187		707	X	49-57	N49-20E
π @ 187	225+69.45				
BS. on 186					
to 188		1000	+ X	86-03 $\frac{1}{2}$	N85-35E
π @ 188	226+69.45				
BS. on 187					
to 189		1953	✓	111-14	568-25E
π @ 189	228+64.75				
BS. on 188					
to 190		1813	✓	94-07	585-15E
π @ 190	230+46.05				
BS. on 189					
to 191		293.8	- ✓	93-34 $\frac{1}{2}$	586-20E
π @ 191	233+39.85				
BS. on 190					
to 192		119.0	✓	70-03	N69-50E
π @ 192	234+58.85				
BS. on 191					
to 193		183.0	✓	82-30	N82-15E
	236+41.85				

1401.6 ✓

+ on rock

N33-29E

N49-44E 1-8-23 (find)

RC. Wueste - transit

P. Horan - front of rear flag

N85-51E OC. Palmer, Ed. Ketchum (motorboat)

568-59E

586-06E

Chaining beginning here by Ed. Ketchum & OC. Palmer

+ on rock

586-39E

N69-50E

N82-17E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 193	236+41.85				
B.S. on 192					
to 194	274.0	+ /	89-0 $\frac{1}{2}$	N89-00E	
π @ 194	239+15.85				
B.S. on 193					
to 195	126.0	- /	53-25 $\frac{1}{2}$	N53-05E	
π @ 195	240+41.85				
B.S. on 194					
to 196	423.7	+ /	98-30 $\frac{1}{2}$	S81-50E	
π @ 196	244+65.55				
B.S. on 195					
to 197	918	✓	79-21	N79-00E	
π @ 197	245+57.35				
B.S. on 196					
to 198	211.3	- /	97-58 $\frac{1}{2}$	S82-15E	
π @ 198	247+68.65				
B.S. on 197					
to 199	98.5	+ /	88-25 $\frac{1}{2}$	N88-15E	
π @ 199	248+67.15				
B.S. on 198					
to 200	70.6	✓	136-41	S43-35E	
π @ 200	249+37.75				
B.S. on 199					
to 201	163.0	✓	96-28	S83-50E	
	251+00.75				
	1458.9 ✓				

tan rock					
				N88-55E	
				N53-12E	
tan rock					
				S81-42E	
+ on rock					
				N79-08E	
+ on rock					
				S82-15E	1-9-23 (fine) ^{East wind in} _(afternoon)
					R.C. Woeste } Transit P. Horan }
				N88-13E	Ed. Ketchum } Chain O.G. Palmer }
+ on rock					
				S43-32E	
				S83-45E	

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 201	251+00.75				
BS on 200					
to 202		229.3	-	80-21 $\frac{1}{2}$	N80-00E
π @ 202	253+30.05				
BS on 201					
to 203		153.8		81-16	N80-50E
π @ 203	254+83.85				
BS on 202					
to 204		295.4		90-37	S89-50E
π @ 204	257+79.25				
BS on 203					
to 205		129.1	+ ✓	96-10 $\frac{1}{2}$	S84-15E
π @ 205	259+08.35				
BS on 204					
to 206		62.15		23-15	N22-35E
π @ 206	259+70.5				
BS on 205					
to 207		102.9		61-50	N61-15E
π @ 207	260+73.4				
BS on 206					
to 208		158.4	- ✓	64-49 $\frac{1}{2}$	N64-25E
π @ 208	262+31.8				
BS on 207					
to 209	✓ 12	206.3	+ ✓	37-22 $\frac{1}{2}$	N36-45E
	264+38.1				

1337.35 ✓

	N80-08E
+ on rock	
	N81-03E
+ on rock	
	S89-36E
	S84-02E
In gulch with a little water	
	N23-02E
	N61-37E
+ on rock	
	N64-36E
	N37-11E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @209	264+381				
B.S. on 208					
to 210		58.4	✓ 91-47	588-30E	
π @210	264+965				
B.S. on 209					
to 211		300.4	- ✓ 138-05½	542-15E	
π @211	267+969				
B.S. on 210					
to 212		172.3	✓ 87-15	N87-00E	
π @212	269+69.2				
B.S. on 211					
to 213		337.5	✓ 94-08	586-15E	
π @213	273+067				
B.S. on 212					
to 214		202.0	✓ 119-22	560-50E	
π @214	275+087				
B.S. on 213					
to 215		43.0	✓ 35-02	N34-00E	
π @215	275+51.7				
B.S. on 214					
to 216		150.4	+ ✓ 64-57½	N64-25E	
π @216	277+021				
B.S. on 215					
to 217		145.0	- ✓ 89-03½	N88-55E	
	278+47.1				

7409.0 ✓

	588-25E	(Az. on this Co. uncertain acct. wind)
	542-07E	Very windy hogs-back - oak tree on flat below
	N87-03E	
		+ on edge of rock cliff.
	586-04E	
		+ on rock
	560-50E	
	N34-50E	1-10-23 (fine)
		R.G. Waasta } Transit P. Horan }
	N64-46E	Ed. Ratchum } chain O.G. Palmer }
		+ on rock
	N88-51E	

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 217	278+471				
BS on 216					
+o 218		297.7	✓	102-09	578-05E
π @ 218	281+448				
BS on 217					
+o 219		164.1	✓	95-58	584-20E
π @ 219	283+08.9				
BS on 218					
+o 220		217.8	+ ✓	118-56 $\frac{1}{2}$	561-00E
π @ 220	285+26.7				
BS on 219					
+o 221		133.0	✓	154-07	525-50E
π @ 221	286+59.7				
BS on 220					
+o 222		159.7	✓	82-14	N82-15E
π @ 222	288+19.4				
BS on 221					
+o 223		94.4	✓	109-02	570-55E
π @ 223	289+13.8				
BS on 222					
+o 224		75.4	✓	60-55	N61-00E
π @ 224	289+89.2				
BS on 223					
+o 225		102.8	✓	94-42	585-10E
	290+920				
	1244.9 ✓				

578-03E
584-14E
561-15E
526-05E
rock slide gulch
N82-02E
+ on rock in boulder moraine below oak tree
571-10E
N60-43E
585-30E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@225	290+920				
B.S. on 224					
to 226		121.0	-	62-14½	N62-10E
π@226	292+130				
B.S. on 225					
to 227 ✓		128.0	+	83-47½	N83-30E
π@227	293+41.0				
B.S. on 226					
to 228		188.3	-	124-59½	S55-00E
π@228	295+29.3				
B.S. on 227					
to 229		102.2	✓	110-53	S69-00E
π@229	296+31.5				
B.S. on 228					
to 230		231.4	✓	128-36	S51-25E
π@230	298+62.9				
B.S. on 229					
to 231		289.7	✓	124-58	S55-00E
π@231	301+52.6				
B.S. on 230					
to 232		219.9	+	76-14½	N76-25E
π@232	303+72.5				
B.S. on 231					
to 233		145.9	✓	139-12	S40-55E
	305+18.4				
	1426.4				

					N62-02E
					N83-37E
					S55-12E
					S69-18E
					S51-35E
					S55-13E
					N76-04E
					S40-59E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @233	305+184				
B.S. on 232					
to 234		299.7		\checkmark 102-14	578-00E
π @234	308+181				
B.S. on 233					
to 235		419.1		\checkmark 93-50	596-15E
π @235	312+372				
B.S. on 234					
to 236		52.6		\checkmark 29-20	N29-05E
π @236	312+898				
B.S. on 235					
to 237		125.6		\checkmark 86-13	N86-00E
π @237	314+154				
B.S. on 236					
to 238		126.2		\checkmark 13-41	N13-30E
π @238	315+416				
B.S. on 237					
to 239	\checkmark 11	400.0		\checkmark 83-05	N83-00E
π @239	319+416				
B.S. on 238					
to 240		117.3		\checkmark 126-10 $\frac{1}{2}$	554-00E
π @240	320+589				
B.S. on 239					
to 241		90.2		\checkmark 146-00	534-05E
	321+491				
	4630.7				

	577-57E		
	this co. across gulch deviating about 50ft from line		
	586-21E		1-11-23 (fine)
			RC. Wueste } Transit
			P. Horan }
	N29-09E		Ed Ketchum } chain
			OC. Palmer }
	top rock		
	N86-02E		
	N13-30E		
	top rock		
	N82-54E		
	this co across rocks on front of Salazar Hill		
	top rock		
	554-01E		
	554-11E		

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @241	321+49.1				
B.S. on 240					
to 242		61.1		$\sqrt{101-11}$	579-00E
π @242	322+10.2				
B.S. on 241					
to 243	12	179.7		$+ \sqrt{137-53\frac{1}{2}}$	542-18E
π @243	323+89.9				
B.S. on 242					
to 244		176.8		$\sqrt{106-46}$	573-15E
π @244	325+66.7				
B.S. on 243					
to 245		279.3		$\sqrt{108-16}$	571-45E
π @245	328+46.0				
B.S. on 244					
to 246		241.6		$\sqrt{100-27}$	579-40E
π @246	330+87.6				
B.S. on 245					
to 247	13	236.5		$- \sqrt{96-07\frac{1}{2}}$	584-06E
π @247	333+24.1				
B.S. on 246					
to 248		99.4		$+ \sqrt{111-54\frac{1}{2}}$	568-00E
π @248	334+23.5				
B.S. on 247					
to 249		213.1		$\sqrt{100-38}$	579-30E
	336+36.6				
	1487.5				

	579-00E
	542-18E
+ on rock	573-26E
	571-56E
	579-45E
	584-06E
	568-18E
	579-35E

Co	Sta	Dist	Defl	Az	Mag Co
π @249	336+36.6				
BS on 248					
to 250		74.5		$\sqrt{125-49}$	554-NE
π @250	337+11.1				
BS on 249					
to 251	4	163.1		$\sqrt{83-32}$	N83-25 E
π @251	338+74.2				
BS on 250					
to 252		93.5		$\sqrt{90-13\frac{1}{2}}$	589-50E
π @252	339+67.7				
BS on 251					
to 253		144.3		$\sqrt{103-32\frac{1}{2}}$	576-35E
π @253	341+120				
BS on 252					
to 254		108.0		$\sqrt{141-12\frac{1}{2}}$	539-05E
π @254	342+200				
BS on 253					
to 255	15	720		$\sqrt{90-39}$	589-35E
π @255	342+920				
BS on 254					
to 256		299.6		$\sqrt{107-27}$	572-45E
π @256	345+916				
BS on 255					
to 257		83.8		$\sqrt{164-40\frac{1}{2}}$	515-30E
	346+754				
	1038.8				

+ on rock					
					554-24E
					N83-18 E
+ on rock					
					N89-59E
+ on rock					
					576-41E
+ on rock (copper lock in soft rock)					
					539-02E
					589-36E
					1-12-23 (fine)
					R.G. Woodgate
					P. Haron
					} Transit
					Ed. Ketchum
					O.C. Palmer
					} chain
+ on rock					
					572-48E
					515-34E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 257	346+754				
BS on 256					
to 258		111.7		- $\sqrt{108-41\frac{1}{2}}$	571-30E
π @ 258	347+871				
BS on 257					
to 259	16	255.6		+ $\sqrt{112-58\frac{1}{2}}$	567-15E
π @ 259	350+427				
BS on 258					
to 260		187.3		$\sqrt{121-49}$	558-10E
π @ 260	352+30.0				
BS on 259					
to 261		67.3		- $\sqrt{92-43\frac{1}{2}}$	587-20E
π @ 261	352+973				
BS on 260					
to 262		81.8		+ $\sqrt{127-05\frac{1}{2}}$	553-00E
π @ 262	353+791				
BS on 261					
to 263	17	126.4		- $\sqrt{91-46\frac{1}{2}}$	588-20E
π @ 263	355+05.5				
BS on 262					
to 264		118.8		$\sqrt{77-50}$	N77-45E
π @ 264	356+243				
BS on 263					
to 265		152.5		$\sqrt{112-44}$	567-15E
	357+76.8	1101.4			

	571-34E
top rock	
	567-17E
top rock	
	558-27E
top rock	
	587-33E
	553-10E
	588-31E
top rock	
	N77-33E
top rock	
	567-33E

Co.	Sta.	Dist.	Def.	Az.	Mag Co
π @265	357+768				
BS on 264					
to 266		134.3		✓ 89-21	N89-25E
π @266	359+111				
BS on 265					
to 267	18	123.5		✓ 110-30	S72-30E
π @267	360+346				
BS on 266					
to 268		105.3		✓ 87-02	N87-00E
π @268	361+399				
BS on 267					
to 269		202.9		✓ 67-15	N67-05E
π @269	363+428				
BS on 268					
to 270		90.5		+ ✓ 102-14 $\frac{1}{2}$	S77-50E
π @270	364+333				
BS on 269					
to 271	19	103.8		- ✓ 57-57 $\frac{1}{2}$	N57-55E
π @271	365+371				
BS on 270					
to 272		116.3		✓ 97-58	S82-05E
π @272	366+534				
BS on 271					
to 273		122.8		✓ 105-44	S74-25E
	367+762				
	999.4 ✓				

+ on rock	
	N89-04E
+ on rock	
	S72-48E
	N86-44E
	N66-57E
	S78-03E
	N57-38E
	S82-21E
	S74-35E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @273	367+762				
B.S. on 272					
to 274		1395	+ $78-31\frac{1}{2}$	N78-30E	
π @274	369+157				
B.S. on 273					
to 275	20	251.0	- $92-29\frac{1}{2}$	S87-35E	
π @275	371+667				
B.S. on 274					
to 276		935	\checkmark 114-52	S65-10E	
π @276	372+602				
B.S. on 275					
to 277		113.0	+ \checkmark 91-55 $\frac{1}{2}$	S88-00E	
π @277	373+732				
B.S. on 276					
to 278		1062	\checkmark 84-27	N84-30E	
π @278	374+794				
B.S. on 277					
to 279	21	2050	- \checkmark 95-40 $\frac{1}{2}$	S84-30E	
π @279	376+844				
B.S. on 278					
to 280		1584	+ \checkmark 60-53 $\frac{1}{2}$	N60-53E	
π @280	378+428				
B.S. on 279					
to 281		1578	\checkmark 70-14	N70-15E	
	380+006				

T224.4 \checkmark

+ on rock

N78-13E

S87-51E

S65-28E

S88-24E

+ on rock

N84-07E

1-13-23 (fine)

+ on rock

R. Moeste	} Transit
P. Horan	
E. Ketchum	} Chem.
O.C. Palmer	

S84-41E

N60-33E

N69-53E

Co.	Sta.	Dist.	Def.	Az.	Mag. Co.
T@281	380+006				
B.S. on 280					
to 282		1412	-	63-37½	N63-30E
T@282	381+41.8				
B.S. on 281					
to 283	22	676	+	55-01½	N55-00E
T@283	382+094				
B.S. on 282					
to 284		1304	✓	77-11	N77-05E
T@284	383+398				
B.S. on 283					
to 285		1892	✓	79-52	N79-45E
T@285	385+290				
B.S. on 284					
to 286	✓ 43 (45)	1028	✓	92-51	S87-10E
T@286	Δ 386+318				
B.S. on 285					
to 287		82.8	-	119-49½	S60-15E
T@287	387+146				
B.S. on 286					
to 288		1110	-	87-57	N87-55E
T@288	388+256				
B.S. on 287					
to 289		1607	×	81-48	N81-50E
	389+863				
	485.7 ✓				

N63-16E
N54-40E
N76-49E
N79-30E
alongside immense boulder with two oak trees on lower side
S87-32E
S60-34E
N87-34E
N81-25E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @289	389+86.3				
BS on 288					
to 290		121.8	+ X	110-44 $\frac{1}{2}$	569-25E
π @290	391+081				
BS on 289					
to 291	(20)	188.2	- X	82-25 $\frac{1}{2}$	N82-25E
π @291	392+96.3				
BS on 290					
to 292		284.0	X	103-13	577-05E
π @292	395+80.3				
BS on 191					
to 293		65.3	+ X	66-29 $\frac{1}{2}$	N66-25E
π @293	396+45.6				
BS on 292					
to 294		171.2	X	110-42	569-15E
π @294	398+16.8				
BS on 293					
to 295		180.7	X	82-55	N82-50E
π @295	399+97.5				
BS on 294					
to 296	(25)	210.4	X	118-01	562-05E
π @296	402+07.9				
BS on 295					
to 297		94.2	X	128-37	551-30E
	403+02.1				
		1315.8			

569-38E
+ on rock

N82-01E

577-11E

N66-26E

569-42E

N82-31E

+ on rock

562-24E

551-48E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 297	403+02.1				
B.S. on 296					
to 298		61.3	X	102-14+	577-55E
π @ 298	403+63.4				
B.S. on 297					
to 299		86.0	X	139-27	540-35E
π @ 299	404+49.4				
B.S. on 298					
to 300		85.8	X	99-47	580-25E
π @ 300	405+35.2				
B.S. on 299					
to 301	(26)	80.8	X	53-25	N53-10E
π @ 301	406+16.0				
B.S. on 300					
to 302		66.1	X	119-26	560-45E
π @ 302	406+82.1				
B.S. on 301					
to 303		128.0	X	84-34+	N84-15E
π @ 303	408+10.1				
B.S. on 302					
to 304		162.3	X	98-46	581-30E
π @ 304	409+72.4				
B.S. on 303					
to 305		60.9	+ X	92-54 $\frac{1}{2}$	587-25E
	410+33.3				

731.2 ✓

					578-11E
					540-58E
					N80-38E
				+ on rock	
					N57-59E
				+ on rock	
					561-00E
				+ on rock	
					N84-08E
					581-40E
					587-31E

Co.	Sta.	Dist.	Defl.	Az	Mag. Co.
π @305	410+333				
BS on 304					
to 306 (27)	1830		X 107-56	572-30E	
π @ 306	412 + 16.3				
BS on 305					
to 307	1722		X 86-25	N 86-15E	
π @ 307	413 + 885				
BS on 306					
to 308	1866		X 102-17	578-00E	
π @ 308	415 + 751				
BS on 307					
to 309	595		X 79-13	N 79-10E	
π @ 309	416 + 346				
BS on 308					
to 310	647		- X 114-51 $\frac{1}{2}$	565-10E	
π @ 310	416 + 993				
BS on 309					
to 311 (28)	854		X 136-08	544-00E	
π @ 311	417 + 847				
BS on 310					
to 312	1741		+ X 105-57 $\frac{1}{2}$	574-10E	
π @ 312	419 + 588				
BS on 311					
to 313	683		- X 112-11 $\frac{1}{2}$	568-00E	
	420 + 271				

993.8 ✓

1-15-23 (East Wind)
 RG Wasta } Transit
 P Moran }
 Ed. Ketchum }
 O.G. Palmer } chain

572-31E

N 85-58E

578-10E

N 78-46E

565-36E

544-20E

574-30E

568-17E

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 321	432+95.8				
B.S. on 320					
to 322		131.6	X 79-29	N 79-15E	
π @ 322	434+27.4				
B.S. on 321					
to 323		86.3	X 99-39	S 80-55E	
π @ 323	435+13.7				
B.S. on 322					
to 324		119.4	- X 110-25 $\frac{1}{2}$	S 69-30E	
π @ 324	436+33.1				
B.S. on 323					
to 325		145.5	X 118-19	S 62-00E	
π @ 325	437+78.6				
B.S. on 324					
to 326 (3)		151.0	+ X 112-35 $\frac{1}{2}$	S 67-55E	
π @ 326	439+29.6				
B.S. on 325					
to 327		234.5	- X 75-45 $\frac{1}{2}$	N 75-30E	
π @ 327	441+64.1				
B.S. on 326					
to 328		125.6	+ X 97-47 $\frac{1}{2}$	S 82-50E	
π @ 328	442+89.7				
B.S. on 327					
to 329		191.2	X 115-13	S 65-00E	
	444+80.9				

1185.1

N 78-59E	
opposite Drop in Flume at Road Xing	
S 80-51E	
+ on sloping rock	
S 70-05E	
S 62-11E	
1-16-23 (firing)	
R. G. Wueste } Transit	
P. Horan } chain	
S 67-55E	
Ed. Ketchum } chain	
O. Palmer } chain	
N 75-14E	
This Co. crosses Dulzura Conduit Extension	
On Conduit berm	
(barbwire fence) S 82-43E	
S 65-18E	
This Co. crosses Dulzura Conduit Extension	

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@329	444+809				
BS on 328					
to 330		201.9	+ 106-25	S73-45E	
π@330	446+828				
BS on 329					
to 331	(32)	118.0	- 86-30 $\frac{1}{2}$	N86-15E	
π@331	448+008				
BS on 330					
to 332		183.3	+ 315-42	N44-30W	
π@332	449+841				
BS on 331					
to 333		226.3	+ 302-10	N58-00W	
π@333	452+104				
BS on 332					
to 334		475.0 288.9	+ 303-19+	N57-00W	
π@334	454+993				
BS on 333					
to 335		100.7	+ 354-13 $\frac{1}{2}$	N6-10W	
π@335	456+000				
BS on 334					
to 336	(33)	100.9	- 220-56 $\frac{1}{2}$	S40.40W	
π@336	457+009				
BS on 335					
to 337		155.6	+ 269-34+	S89-25W	
	458+565				
		1375.6 ^v			

	S74-06E
	N85-58E
	top rock in creek bottom alongside flume
	N44-50W
	This co crosses Cottonwood Creek
	N58-22W
	@ outside edge of road
	N57-13W
	this co crosses road
	Note: this co assumed in error in plotting lengthened to 475±
	N6°18'W
	S40°23'W
	S89°01'W

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
T@337	458+56.5				
BS. on 336					
to 338		155.4	+ X	284-55 $\frac{1}{2}$	N75-15W
T@338	460+119				
BS. on 337					
to 339		105.0	- X	349-12 $\frac{1}{2}$	N11-10W
T@339	461+169				
BS. on 338					
to 340		167.0	X	247-13	S67-00W
T@340	462+839				
BS. on 339					
to 341	(34)	469.9	+ X	274-15 $\frac{1}{2}$	N86-10W
T@341	467+538				
BS. on 340					
to 342		369.0	- X	287-39 $\frac{1}{2}$	N72-30W
T@342	471+228				
BS. on 341					
to 343		274.0	+ X	277-04 $\frac{1}{2}$	N83-10W
T@343	473+968				
BS. on 342					
to 344		173.6	- X	284-02 $\frac{1}{2}$	N76-05W
T@344	475+70.4				
BS. on 343					
to 345		463.3	+ X	292-29 $\frac{1}{2}$	N67-50W
	480+33.7				
		2177.2			

+ on rock

N75-37W

+ on rock

N11-21W

S66-40W

+ on rock under oak tree

N86-18W

N72-55W

N83-29W

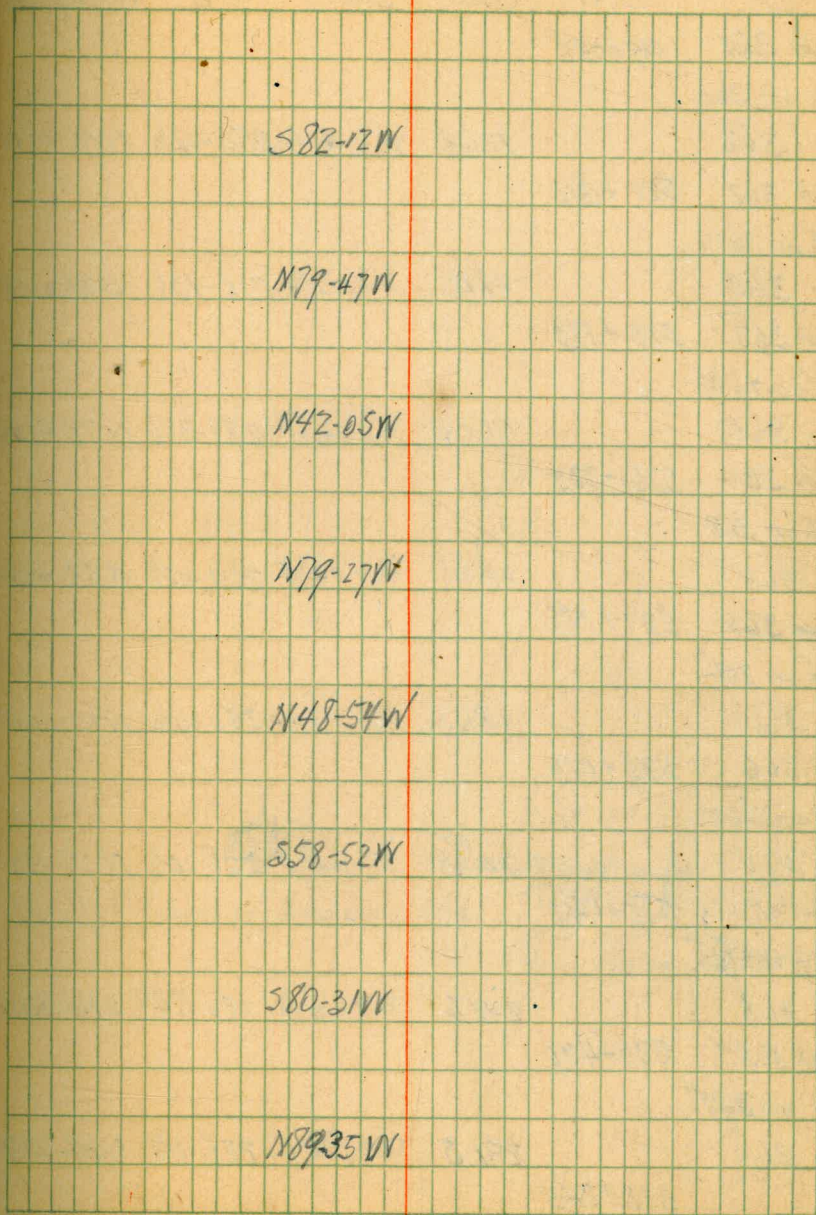
N76-32W

N68-04W

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π@ 345	480+337				
BS. on 344					
to 346 (35)	527.9		✓ 287-04	N73-05W	
π@ 346	485+61.6				
BS. on 345					
to 347	77.1		✓ 265-23	S85-00W	
π@ 347	486+387				
BS. on 346					
to 348	520.9		✓ 295-39	N64-30W	
π@ 348	491+596				
BS. on 347					
to 349	261.0		- ✓ 295-55½	N64-25W	
π@ 349	494+206				
BS. on 348					
to 350	257.3		✓ 350-13	N10-10W	
π@ 350	496+77.9				
BS. on 349					
to 351 (36)	540.8		✓ 292-12+	N68-00W	
π@ 351	502+18.7				
BS. on 350					
to 352	118.1		+ ✓ 251-16½	S71-00W	
π@ 352	503+368				
BS. on 351					
to 353	227.8		- ✓ 282-13½	N78-05W	
	508+64.6				
	2530.9 ✓				

					1-17-23 (final)
				N73-31W	RC. Wueste } Transit P. Heron }
				S84-48W	Ed Retchurn } chain OC. Palmer }
				N64-56W	
					fence running uphill @ 20 ft plus on this co.
				N64-40W	
				N10-22W	
				N68-24W	
				S70-41W	
				N78-23W	

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 353	505+646				
BS on 352					
+ to 354	150.9		+ \checkmark 262-47 $\frac{1}{2}$	S 82-30W	S 82-12W
π @ 354	507+155				
BS on 353					
+ to 355	144.0		\checkmark 280-49	N 79-25W	N 79-47W
π @ 355	508+595				
BS on 354					
+ to 356 (37)	195.4		- \checkmark 318-32 $\frac{1}{2}$	N 41-40W	N 42-05W
π @ 356	510+511.9				
BS on 355					
+ to 357	114.3		+ \checkmark 281-09 $\frac{1}{2}$	N 79-00W	N 79-27W
π @ 357	511+69.2				
BS on 356					
+ to 358	104.5		\checkmark 311-43	N 48-35W	N 48-54W
π @ 358	512+73.7				
BS on 357					
+ to 359	122.6		\checkmark 239-29	S 59-15W	S 58-52W
π @ 359	513+96.3				
BS on 358					
+ to 360 \checkmark 38	345.6		\checkmark 261-09	S 80-45W	S 80-31W
π @ 360	517+41.9				
BS on 359					
+ to 361	252.3		- \checkmark 271-03 $\frac{1}{2}$	N 89-10W	N 89-35W
	519+94.2				
	1429.6 \checkmark				



Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @369	538+34.5				
BS on 368					
+o 370		53.2	-	$\sqrt{251-20\frac{1}{2}}$	571-00W
π @370	543+65.7				
BS on 369					
+o 371		245.5	+	$\sqrt{277-44\frac{1}{2}}$	N 82-30W
π @371	546+112				
BS on 370					
+o 372		82.2	$\sqrt{}$	253-10	572-50W
π @372	546+93.4				
BS on 371					
+o 373		217.6	-	$\sqrt{275-56\frac{1}{2}}$	N 84-25W
π @373	549+110				
BS on 372					
+o 374		56.5	+	$\sqrt{233-24\frac{1}{2}}$	553-05W
π @374	549+67.5				
BS on 373					
+o 375		117.0	$\sqrt{}$	279-29	N 80-15W
π @375	550+84.5				
BS on 374					
+o 376		213.6	$\sqrt{}$	240-02	559-40W
π @376	552+98.1				
BS on 375					
+o 377		58.0	-	$\sqrt{308-33\frac{1}{2}}$	N 51-50W
	553+56.1				
	1521.6				

					570-42W
					N 82-53W
					572-32W
					N 84-42W
					552-47W
					N 81-09W
					559-24W
					N 52-05W

Co	Sta	Dist	Defl	Az	Mag. Co
π @401	598+778				
BS on 400					
to 402		142.8	-	\checkmark 309-10 $\frac{1}{2}$	N51-30W
π @402	600+206				
BS on 401					
to 403		159.0	+	\checkmark 226-28 $\frac{1}{2}$	S45-45W
π @403	601+796				
BS on 402					
to 404		1604	-	\checkmark 244-55 $\frac{1}{2}$	S64-30W
π @404	603+400				
BS on 403					
to 405		1992	+	\checkmark 280-38 $\frac{1}{2}$	N80-00W
π @405	605+392				
BS on 404					
to 406	\checkmark 610	106.1	\checkmark	216-58	S36-25W
π @406	606+453				
BS on 405					
to 407		518.6	\checkmark	302-37+	N57-55W
	611+639				
(to 239)		1286.1 \checkmark		195-17-	S14-50W
New Start with Corrected Azimuth					
π @406					
BS on Δ				283-13	
to 407	\checkmark 610	518.6	\checkmark	301-57	N57-50W
	611+639				

to on rock	
	N51-30W
	S45-50W
to on rock	
	S64-16W
to on rock	
	N80-00W
	1-20-23 (lightly clouded)
	RC. Wueste } Transit P. Heran } and chain
	S36-18-W
In quarry on Salazar Hill (Rt. side)	
	N58-03W
For Az. check see page 58	
	1-22-23 (cloudy)
See page 58	RC. Wueste } Transit P. Heran } Ed. Ketchum } Chain O.C. Palmer }
	N58-03W

Co	Sta	Dist	Decl.	Az	Mag. Co
π @ 415	623+767				
BS on 414					
to 416		545.7		$\sqrt{294-30\frac{1}{2}}$	N65-30W
π @ 416	629+224				
BS on 415					
to 417		488.9		$\sqrt{295-16}$	N64-30W
π @ 417	634+113				
BS on 416					
to 418		295.9		$\sqrt{305-51}$	N63-35W
π @ 418	637+07.2				
BS on 417					
to 419		600 -529.8		$\sqrt{325-17}$	N34-30W
π @ 419	642+370				
BS on 418					
to 420		1032		$\sqrt{219-11\frac{1}{2}}$	S39-35W
π @ 420	643+40.7				
BS on 419					
to 421		340.0		$\sqrt{240-28}$	S61-00W
π @ 421	646+80.2				
BS on 420					
to 422		324.6		$\sqrt{266-04}$	S86-10W
π @ 422	650+04.8				
BS on 421					
to 423		185.9		$\sqrt{247-34\frac{1}{2}}$	S67-45W
	651+907				
	2814.0				

+ on rock	
	N65-29W
	N64-44W
+ on rock	
②	N54-09W
	N34-43W this co. lengthened to 600' in plating
Head of gulch with water	
	S39-11W
+ on rock	
	S60-28W
+ on rock	
	S86-04W
	S67-35W

Co.	Sta.	Dist.	Defl.	Az	Mag. Co.
π@ 423	651-1907				
BS on 422					
to 424		131.6	✓	266-55	587-05W
π@ 424	653 + 223				
BS on 423					
to 425		518.5	✓	290-10	N69.50W
π@ 425	658 + 408				
BS on 424					
to 426		299.8	- ✓	296-29½	N.63-15W
π@ 426	661 + 406				
BS on 425					
to 427		298.6	✓	299-03	N60-30W
π@ 427	664 + 392				
BS on 426					
to 428		166.6	✓	317-12	N42-25W
π@ 428	666 + 068				
BS on 427					
to 429		178.7	✓	275-46	N83-30W
π@ 429	667 + 85.5				
BS on 428					
to 430		297.2	+ ✓	289-47½	N69-30W
π@ 430	670 + 81.7				
BS on 429					
to 431		292.4	✓	295-45	N64-30W
	673 + 74.1				

2183.4 ✓

+ on rock

586-55W

N69.50W

N63-31W

N60-57W

N42-48W

N84-14W

N70-12W

N64-15W

1-23-23 (cloudy)

RC. Wueste	} Transit
P. Horan	
Ed Ketchum	} chain
OC. Palmer	

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @431	673+74.1				
B.S. on 430					
to 432		233.7	✓	301-35	N58-40W
π @432	676+07.8				
B.S. on 431					
to 433		297.7	-	270-02 $\frac{1}{2}$	West
π @433	679+05.5				
B.S. on 432					
to 434		185.3	✓	251-45	572-00W
π @434	680+90.8				
B.S. on 433					
to 435		242.8	+	263-15 $\frac{1}{2}$	584-30W
π @435	683+33.6				
B.S. on 434					
to 436		638.6	✓	257-02	576-30W
π @436	689+72.2				
B.S. on 435					
to 437		145.8	✓	291-30	N68-30W
π @437	691+18.0				
B.S. on 436					
to 438		172.5	✓	230-03	550-15W
π @438	692+90.5				
B.S. on 437					
to 439		172.7	✓	250-45	571-00W
	694+13.2				

2039.1

Ⓟ	N58-25W
	N89-58W
	571-45W
Ⓟ	583-16W
Ⓟ	577-02W
	N68-30W
	550-03W
	570-45W

Co.	Sta.	Dist.	Defl.	Az.	Mag. Co.
π @ 439	694+13.7				
BS. on 438					
to 440		92.9		268-26	S88-30W
π @ 440	695+06.1				
BS. on 439					
to 441		297.5		279-24	N80-15W
π @ 441	698+03.6				
BS. on 440					
to Δ				285-23	N74-30W

New Start with Corrected Azimuth

π @ 441	698+03.6				
FS. on Δ				285-26 $\frac{1}{2}$	
to 442		44.1		319-15	N40-30W
π @ 442	698+47.7				
BS. on 441					
to 443		125.2		331-12	N28-40W
π @ 443	699+72.9				
BS. on 442					
to 444		243.7		33-59	N34-00E
π @ 444	702+16.6				
BS. on 443					
to 445		293.7		344-11 $\frac{1}{2}$	N15-40W
π @ 445	705+10.3				
BS. on 444					
to 446		392.7		338-59	N21-10W
	709+03.0	1489.8			

+ on rock

S88-26W

N80-36W

= Δ

N74-37W X

(105-26 $\frac{1}{2}$ plus 180-00 = 285-26 $\frac{1}{2}$ = minus 3 $\frac{1}{2}$ Error - see page 58)

N40-45W

N28-48W

(151-12)

+ on rock on rocky point

N33-59E

N15-40W

(164-11 $\frac{1}{2}$)

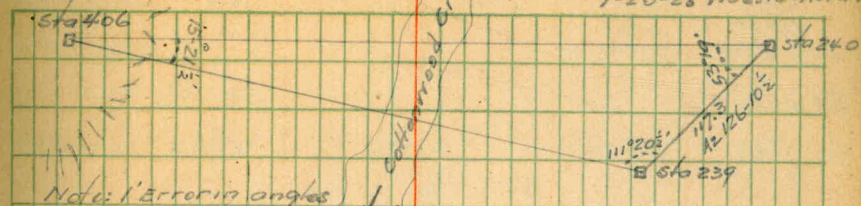
N21-01W

Ties.

Co	Sta	Dist	Defl.	Az	Mag Co
X@ 240	320+58.9				
B ₂ on 239				126-10 $\frac{1}{2}$	553-50E
to 406	606+45.3			359-29 $\frac{1}{2}$	N 0-30W

57

Solazar Hill



Azimuth Checks.

Co.	Sta.	Dist.	Defl.	Az	Mag. Co.
π @ 239	319+41.6				
FS on				126-10 $\frac{1}{2}$	S 53-50 E
to 406	606+45.3			14-50	N 14-50 E
* ————— *					
π @ 1 = Δ	0+00				
FS on Δ	• Station's offset			331-05	
to Δ			9-28 Rt	340-43	N 19-15 W
π @ Δ					
BS on Δ					
to Δ			124-43 $\frac{1}{2}$ Rt	105-26 $\frac{1}{2}$	S 74-15 E
π @ Δ					
BS on Δ					
to Δ	606-453		7-13-15 Lt	103-13-15	S 76-35 E
π @ Δ					
BS on Δ					
to 239	319+41.6		91-24 Rt	194-37 $\frac{1}{2}$	S 14-50 W
* ————— *					
π @ Δ					
FS on Δ				105-26 $\frac{1}{2}$	
to 507	841+65.0			57-49 $\frac{1}{2}$	N 58-00 E
* ————— *					
π @ Δ					
BS on Δ				340-43	
to Δ			34-50 $\frac{1}{2}$ Rt	15-33 $\frac{1}{2}$	N 15-35 E

58

See page 51

1-20-23
Wueste-Horan

195-17 (15-17) [+ 0°27' Error]

1-20-23
Wueste-Horan

(mean of 4 readings)

(mean of 4 readings)

1-22-23
Wueste-Horan

(mean of 4 readings)

[+ 0°13' Error]

57-49 $\frac{1}{2}$ + 180 = 237-49 $\frac{1}{2}$ (238-01 $\frac{1}{2}$ Seapage Book
plus 0°12' Error)(15-47 = + 0°13 $\frac{1}{2}$ ' Error)2-11-23
Wueste-Krausig

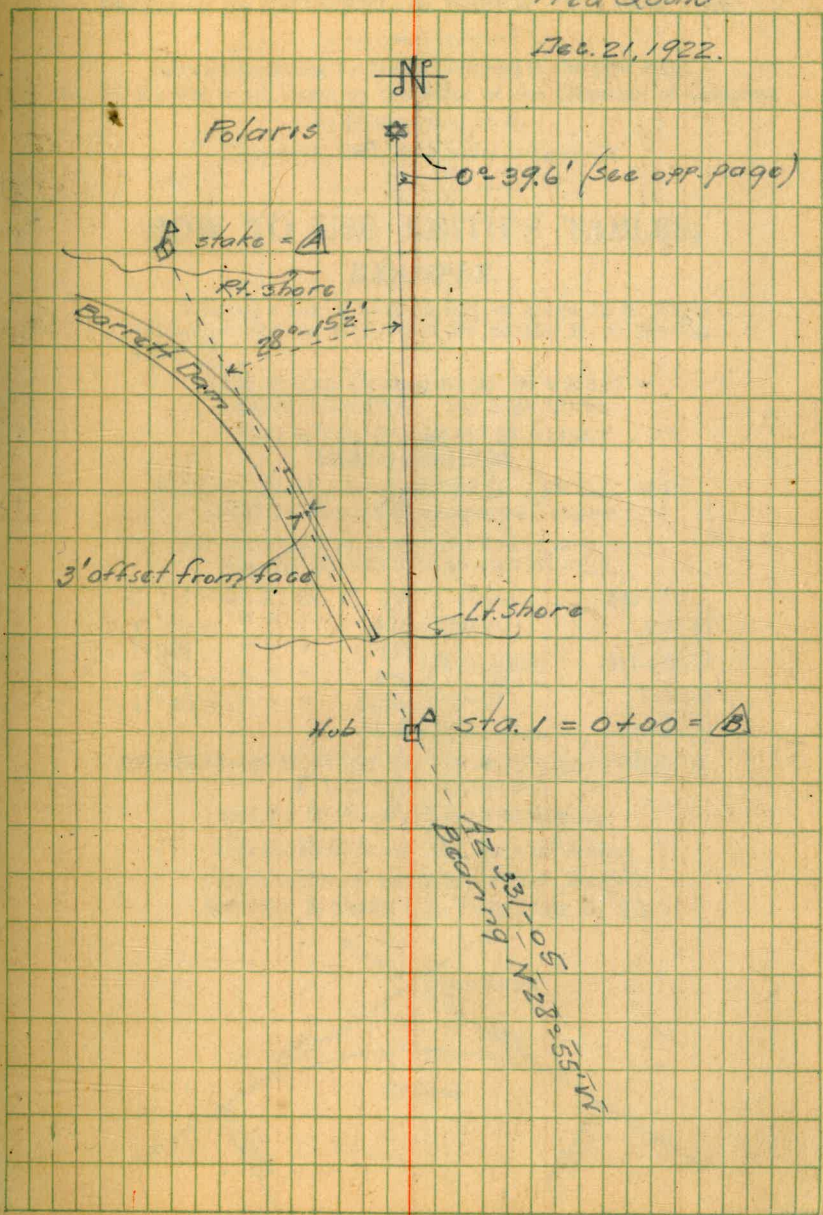
Traverse 1710' Barrett Reservoir Contour.
Azimuth Determination

Data: Observers station, latitude $N32^{\circ}40.5'$,
Longitude $W116^{\circ}40.4'$, Date 12-21-22
Standard time of observation 9^h19^m
Local mean time of observation $9^h32.3^m$

U.C. Dec 16, 1922 (long $90^{\circ}W$)	7-54.6 PM
Change in 5 days (5×3.94)	- 19.7
U.C. Dec 21, 1922 (long $90^{\circ}W$)	7-34.9 PM
Long. correction ($26^{\circ}40.4' = 15 \times 0.16$)	- 03
U.C. Dec 21, 1922 (long $116-40.4W$)	7-34.6 PM
Observation	9-32.3 PM
Mean solar interval after U.C.	1-57.7
Reduction to sidereal interval (III) +	0.33
Sidereal interval = hour angle	1-58
Azimuth from Table II	39.8
Table IIIa (Polar dist $1^{\circ}6'14''$)	- 0.2
Azimuth of Polaris	39.6
Polaris $396'$ W of meridian	

R.G. Wwaste
Oell Brumbaugh
O.S. Palmer
Fred Quaid

Dec. 21, 1922.



KEITH'S RAILROAD CURVE TABLES.

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HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an-Ext. of about 12 ft. Angle
of Intersection or I. P. = $23^{\circ} 20'$ to the R. at Station
542+72.

Ext. in Tab. IV opposite $23^{\circ} 20' = 120.87$
 $120.87 \div 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. IV opp. $23^{\circ} 20' = 1183.1$
 $1183.1 \div 10 = 118.31$.

Tab. V correction for A. $23^{\circ} 20'$ for a 10° Cur. = 0.16
 $118.31 + 0.16 = 118.47 =$ corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333 =$ L. C.

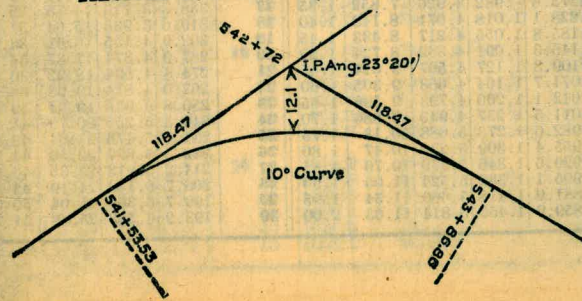
$2^{\circ} 19\frac{1}{2}' =$ def. for sta.	542	I. P. = sta.	542+72
$4^{\circ} 49\frac{1}{2}' =$ " " "	+50	Tan. =	1.18.47
$7^{\circ} 19\frac{1}{2}' =$ " " "	543	B. C. = sta.	541+53.53
$9^{\circ} 49\frac{1}{2}' =$ " " "	+50	L. C. =	2.33.33
$11^{\circ} 40' =$ " " "	543+	E. C. = Sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^{\circ} \text{ Cur.}) = 139.41' =$
 $2^{\circ} 19\frac{1}{2}' =$ def. for sta. 542.

Def. for 50 ft. = $2^{\circ} 30'$ for a 10° Curve.

Def. for 36.86 ft. = $1^{\circ} 50\frac{1}{2}'$ for a 10° Curve.

(These tables are published in Field Books of
KEUFFEL & ESSER Co., New York, N. Y.)



28-15 $\frac{1}{2}$
 39 $\frac{1}{2}$
 28 55
 300
 331 00
 9 33
 321 27
 340-43
 124-43 $\frac{1}{2}$

465 26 $\frac{1}{2}$
 360
 105-26 $\frac{1}{2}$
 2 13 $\frac{1}{2}$
 103-13 $\frac{1}{2}$
 180
 283 13

~~126 159
 126 159
 256
 2540
 2169
 3880~~

285-23
 180
 105-23
 2713 | 3300 .0121
 2713

5870
 5426
 4440

103-13 $\frac{1}{2}$
 91 2 $\frac{1}{2}$ RT
 19-4 37 $\frac{1}{2}$
 180

374-37 $\frac{1}{2}$
 14-37 $\frac{1}{2}$ 3rd count
 14-50 50
 115 13 error

53 606
 53 76
 53 330

195-17
 194 37
 0-40
 35 pnd

115 | 40.0
 34.5
 55.0
 53 | 320.6

340-43
 15-33 (N1535E) 195-33
 50-24

50
 19-17
 15-23
 3451
 15-33
 3450
 50-23
 5024
 1533
 3451

Defl to RT @ A

124-43+
 249-27 $\frac{1}{2}$
 14-11
 128-54
 360
 4 | 498 52
 124-43-30

N19-00W
 574-15E
 120
 57
 174
 43

124 43
 134 44 $\frac{1}{2}$
 124 43 $\frac{1}{2}$
 124 43
 174
 43 $\frac{1}{2}$

374-11
 249-27 $\frac{1}{2}$
 124-43 $\frac{1}{2}$
 498.54
 374 11
 124 43

9-38 RT
 19-16
 28-55
 4 | 38-32
 9-38

N.19-15W

2-14 Lt
 4-26 $\frac{1}{2}$
 6-40
 4 | 8-53
 2-13 $\frac{1}{2}$

576-35E
 214
 212 $\frac{1}{2}$
 213 $\frac{1}{2}$
 213

91 23
 182-48
 91-24

1-20-23

53-19
 111-20 $\frac{1}{2}$
 164-39 $\frac{1}{2}$
 180
 1520 $\frac{1}{2}$
 5310
 111-20 $\frac{1}{2}$
 1521 $\frac{1}{2}$
 18001

340-43
 124 43 $\frac{1}{2}$
 465 26 $\frac{1}{2}$
 360
 105 26 $\frac{1}{2}$
 2 13 $\frac{1}{2}$
 103-13 $\frac{1}{2}$

133.6 ✓ 78.760 96.17-8) 6.517
 134.7 ✓ 971 64.2 359.24 20.457
 126 2720.4
 75.1 ✓ 78.760 67.3 253.19 55
 68.2 ✓ 971.75 64.7 150 6
 75.1 ✓ 8847.75 65.3 306 6
 118.8 ✓ 2749 2329 ✓ 52.19 52.543
 81.3 ✓ 537.9 60.8 224 27+20.4
 119.3 ✓ 2530 1002 ✓ 25 28+20.6
 161.1 ✓ 1081 ✓ 26 29+28.7
 180.3 ✓ 170 750 ✓ 27 30+01.7
 879.2 ✓ 157.8 64.1 ✓ 28 30+65.8
 1189.5 ✓ 179.0 ✓ 29 32+44.8
 2068.7 ✓ 17/130 68.9 ✓ 30 33+13.7
 180.3 ✓ 18 56.9 31 33+70.6
 1248.4 ✓ 128 1800 32 35+50.6
 161.1 ✓ 16726 104.7 33 36+55.3
 1742.73 ✓ 182.45 64.2 34 37+19.5
 119.3 ✓ 152.15 48.15 35 37+67.65
 16408.0 ✓ 144 2+5.6 36 39+83.25 ✓
 81.3 ✓ 171.7 37 41+54.95
 15426.7 ✓ 13 ✓
 118.8 ✓
 4407.9 ✓ 12 ✓
 75.1 ✓
 3332.8 ✓ 11 ✓
 282 ✓
 121646 ✓ 10 ✓
 75.1 ✓
 895 ✓ 9 ✓
 41.15 ✓ 24.59 ✓
 75.32 ✓ 14.36 ✓
 41.15 ✓
 906 ✓
 24690 ✓
 7035 ✓
 728190 ✓
 4135 ✓
 1071 ✓
 364 ✓
 72.8 ✓
 3728 ✓
 10.11 ✓
 21208
 180
 34500
 3706
 3204
 359232
 180
 179232
 27+20.4
 60.8
 26+59.6
 2432.8
 2426.7
 65.3
 21-27+6.14
 64.7
 20-22+96.7
 67.3
 19-22+29.4
 64.2
 18-21+65.2
 96.5
 20+68.7
 1517
 180
 37517
 1450
 1518

469.9
 520.9
 170
 167.1
 933
 245
 2017

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1. 3688
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

5749
 237493
 182
 1200
 841
 605
 143
 237120
 30
 250