

EL CAPITAN
Pipe Line Survey
Line and Level Revisions

W191

MICROFILMED
JAN 11 1965

Preliminary Survey El Capitan Pipe Line

	Page
Relocation Sta 141+00 to 150+85	— 1
Levels on revised line	— 2
Levels over "A" Line (Bissell)	— 4 to 42
Levels from 1157 to 1220+08 (Boren)	— 43 to 51
Levels from 1217 to 1222 (Boren)	— 52
Levels from 413+40.8 to 428+90.7	— 53 to 54
Transit Notes "D" Line	— 56 to 57
Relocation 135+03.0 to 173+44.8	— 59

MICROFILMED

JAN 9 1965

①

ang Brng Dst Mag

Forward Hub 34°03'P H. G. 538°35'W

148+87.6 = 150+85 = 1487.6

+78

8

7

6

5

4

3

1

142+0

+22

+20

+07

529°03'W

Sta 141+00 35°55'P

814°35'W

135+50

56°52'E

Relocation Sta 141+0 to 150+85 1

Dec 30-1925

C

(Boren
Ruplinger
Simson
The molds)

148+87.6 New = 150+85 old



Edgar Rd

" Rd



B

C

(P)

Levels on Revised Line
Sta 141+00 to 148+87.6 = 150+85

2

B.M.

503.054

Nail on Power pole Left Sta 134+0

2.720 505.774

TP

0.060 505.714

4.050 509.764

141+00 3.4 506.4 ✓

+22 2.9 .9

142+00 4.3 505.5 ✓

143+00 4.9 504.9 ✓

144+00 4.9 504.9 ✓

TP

4.948 504.816

6.010 510.826

145+00 7.1 503.7 ✓

146+00 9.5 501.2 ✓

147+00 10.0 500.8 ✓

148+00 9.2 501.4 ✓

148+87.6 + 150+85 of old line 7.9 502.9 ✓

← Record Elev

B.M. near Sta 149 1.585 509.241 509.255

3

3

④

Sta -	+	H. b.	-	Elev
P.M.	Sta 98	400 - Hub.		333.390
	6.55	W 339.942		
0+00 P.C.	981	+ 89 6	3.8	336.1
+25	982	+ 146	5.0	334.9 ✓
+50	"	+ 39 6	5.8	334.1 ✓
+75	"	+ 64 6	5.5	334.4 ✓
1+00	"	+ 89 6	5.3	334.6
+25	983	+ 14 6	4.7	335.2 <i>check</i>
+50	"	+ 39 6	4.6	335.2
+75	"	+ 64 6	6.5	333.4
2+00	983	+ 59 6	10.5	329.4
F.P.		329.405	11.644	328.298 ✓
	1107	337.405		
2+25			4.1	
T.P.			11.706	317.699 327.699 ✓
T.P.			11.644	328.298 ✓
	0.284	328.582		
2+25	984	+ 14 6	3.3	315.3
T.P.			10.525	318.051
	1092	319.149		
+50	984	+ 64 6	2.5	316.6
+75	"	+ 64 6	10.1	309.0
T.P.			11.324	307.825 ✓
	0.203	308.028		
3+00	984	+ 89 6	7.7	300.3
	8.131	334.93		

 Bissell - (1/4-5-6-7/26)
 Reynolds -
 Ruplinger -

4

331.93

8131

25.362

202

25.565

333.390

307.825

← 10° →

↑
↓

5

5

S. 2	0.203	308.028	-	307.82
T.P.	+	T	-	Elev.
			11.793	296.235
	0.396	296.631		
3+30 EC	985+196		7.9	289.8
T.P.			10.946	285.685
	1.988	287.673		28
T.P.			11.508	276.165
	0.450	276.615		
4+00	985+896		7.9	269.7
T.P.			11.100	265.515
	0.595	266.110		
T.P.			10.946	255.164
	2.728	257.892		
5+00	986+896		8.2	249.7
T.P. (72)			11.025	246.867
	1.880	248.747		
T.P. (55+55)			11.722	237.565
	2.297	239.842		
6+00	987+896		13.6	226.2
+35	988+246		15.6	214.4
+40	" + 296		13.1	226.7
7	988+896		4.5	235.3

78,500
 8700
 70,280
 307,820
 237,565



⑥

2.297
+

239.847

1.381

237.545

E1.

238.461

T.P.

11.605 250.066

8+04 B.C. 989+80²

4.5 245.6

+25.4 990+03²

2.9 247.2

+50.4 990+27²

7.4 246.9

+84.7 E.C. 990+64²

3.9 246.2

9 99076³

6.4 243.9

+70 991+06³

10.7 239.9

10 991+76³

11.5 238.6

11 992+76³

10.7 239.4

993.16³

+40

10.1 240.0

12 993+76³

9.7 240.4

25.2

T.P.

13.907
1.566

239.827

11.385
12.766

238.681

13902
12766
1.136
237.545
238.681

6

check

checked
plotting to
here
P.E.R.



⑦

1.156

235.681

7

239.837

12+75 994+11² 7.2 ✓ 232.6

+89.9 (P) 994+66² 25 ✓ 237.3

12+276 85.995+03. 5.6 ✓ 234.2

+47⁶ 995+23 7.2 ✓ 232.6

+72⁶ 995+48 7.7 ✓ 232.1

+97⁶ " 173 9.0 ✓ 230.8

11=995+156

14+276 995+98² 11. ✓ 228.8

T.P. 10.71 ✓ 229.123

1.04 ✓ 230.165

+47⁶ 996+23.2 3.4 ✓ 226.8

+72⁶ 996+48 5.9 ✓ 224.3

+97⁶ " 173 9.4 ✓ 220.8

2198

T.P. & B.M. - on Hub. Pl. N+05² 11.62 ✓ 218.548 ✓

0.759 ✓ 19.308

Small gully

-22.336

+ 2198

-20.138

235.681

218.548

start



8

15 = 996 + 75.6
0.757
79,200

218.543

15 + m⁶ 996 + 98² 1.7 217.6

+ 47.6 997 + 23² 6.8 212.5

T.P. - 11.100 208.200
0.024 208.214

15 + j⁶ 997 + 48² 1.7 206.9

+ 97⁶ " 73² 7.4 200.8

16 + m⁶ 997 + 95.6 11.5 196.7

T.P. 11.34~~8~~ 196.881
1.047 197.928

16 + 60⁶ EC: 998 + 40.5 7.6 190.3

T.P. & 16 + 80⁶ 999 + 60.5 11.0² 186.916 ✓
10.850 197.766
33.45⁵

17 + 998 + 90.5 13.1 184.7

+ 10 999 + 00.5 16.0 179.8

+ 15 999 + 15.5 13.7 184.1

$\frac{170}{14} = 10 \text{ min} - \text{Serap} -$

-33.457

1878
-31.627
218.543
186.916

8

check

ok

ok

ok

ok

⑨

10.850

186.916

197.766

+77.057

2580

+74.891

186.916

261.807

18+ 999+90 $\bar{5}$

28 195.0

T.P.

0.549 197.217

11.462 208.679

0.217 208.462

T.P. 11.096

219.558

19+ 1000+90 $\bar{5}$

34 216.2

T.P.

0.073 219.485

10.908 230.393

T.P.

0.658 229.741

11.442 241.183

20+ 1001+90 $\bar{5}$

78 233.7

T.P.

0.445 240.739

T.P.

10.540 251.279

0.740 251.039

T.P.

11.153 262.192

21+ 1002+90 $\bar{5}$

10.0 252.2

11.451

0.385 261.807

10.591

272.398

φ

9

(10) +10.581 261.507

22+ 1003+90^E 272.348
2.0 270.4

T.P. 0.680 271.718
11.418 283.136

23 1001+90^E 7.2 275.9

T.P. 0.445 282.691
11.281 293.972

TP 0.176 293.796
10.375 304.171

24 1005+90^E 5.0 299.2
22+01^E 182^B

T.P. 0.132 304.039
10.435 314.474

24+76^B 1000+096 8.5 306.0

+51^B 1006+34^L 4.2 310.3
T.P. 0.097 314.377

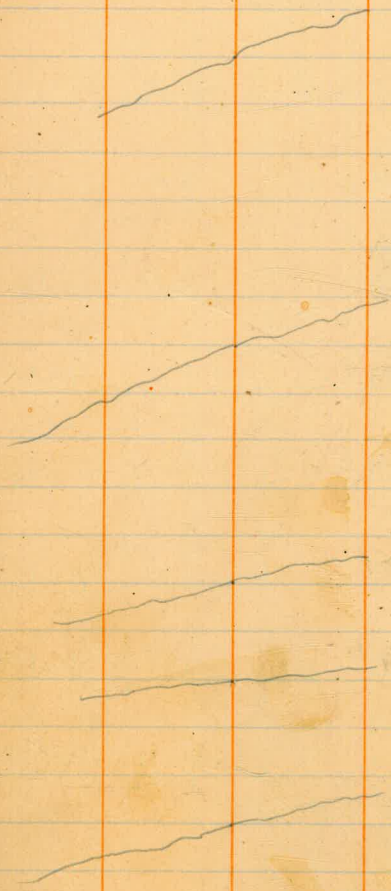
10.848 325.225
24+76^B 1006+59^E 8.4 316.8

25+01^B 64.949 00. 325.2
T.P. 1006+92^B 0.612 324.413

11.137 335.550

+62.948
- 2342
+62.606
261.507
324.413

check



$25 = 1006 + 90 \text{ E}$

11.137

326.412

335.550

$25 + 25 \text{ E}$

1007 + 63

2.0

333.6

T.P.

0.916

334.634

11.1 x 8

345.782

B.M. on P.I. Hub - 25 + 55 E

9.808

335.970 ✓

$25 + 51 \text{ E}$

1007 + ⁵¹2

8.2

337.6

76 E

1007 + ⁶⁹2

6.0

339.8

$26 = 1007 + 90 \text{ E}$

$70 + 01 \text{ E}$

1007 + 922

5.0

340.8

$+ 76 \text{ E}$

1008 + 172

3.7

342.5

$+ 51 \text{ E}$

1008 + 122

2.7

343.6

$+ 76 \text{ E}$

1008 + 672

0.5

345.3

T.P.

24.285

0.116

345.666 ✓

11.652

357.318

27 =

1008 + 81

$27 + 01 \text{ E}$

Ec. 1008 + 82 E

9.7

348.0

984

27

1011

+ 22.285

1.032

+ 21.253

326.413

345.666

11

25

11.65

345.666

357.318

25+ 17+09² BC1008196² 8.4 348.9-T 34.3 1009+15² 6.5 350.8
" +40²

59.3 4.6 352.7

B

84.3 " +65² 3.7 353.6

25 28 = 1009+81

78+09.3 " +96² 2.7 354.6

26 TP 2.200 355.118 ✓

76 9.400 360.518

+34.3 1010+15² 10. - 350.5+59.3 " +40² 9.1 355.4+84.3 " +65² 8.0 356.1

29 = 1010+81

- 79+09² " +96² 7.7 356.82 +11² EC 1011+02² 7.4 357.1

21

30 = 1011+81 6.3 358.2

12

11.652

22

9.45

345.666

355.118

355.118

9,000

364.578

4

13

31+

1012+81

4.8

359.7

32+

1013+81

3.5

361.0

33+

1014+81

1.3

363.2

T.P.

0.585

363.933

6.478

370.411

+50

~~15.878~~
1015+31

5.8

364.6

check

+75

1015+56

7.8

362.6

30+07.1

1015+88+

4.5

365.9

+100

1016+28+

8.2

362.2

+60

1016+48'

4.5

365.9

35+

1016+81

8.5

361.9

+70

1017+01

8.8

361.6

+40

1017+11

5.7

364.7

	15878			
		370.411	0.555	
36+	1017+81	9.8	360.6	
+20	1018+01	7.0	363.4	
37+	1018+81	10.2	360.2	
+35	1019+16	7.6	362.8	
T.P.		7.1000	362.971	
	0.525	363.496	8.075	
38+	1019+81 16.403	3.2	360.3	
39	1020+81	5.3	358.2	
40	1021+81	6.1	359.4	
+20	1022+01	7.6	355.9	
+35	1022+16	6.4	357.1	
41	1022+81	8.5	355.0	

clock

	16,403	8.025	
	363,496		
+30	1023+11	5.7	357.8
+50	1023+31	8.6	358.9
42	1023+81	8.7	354.8
160	1024+41	6.4	357.1
+80	1024+61	8.7	354.8
43+	1024+81	6.4	357.1
TP	16,403 0.420	5.921 13.946	357.575 ✓
	357.995 358.0		
44+	1025+81	3.9	354.1
70	1026+01	2.0	356.0
45+	1026+81	5.1	352.9
475	Bin. 30 L. Hub	3.958	354.037 ✓
46+	1027+81	5.3	352.7

+16,403
 -13,946
 + 2,457
 357,118
 357,575



	0.470	358.0	357.575	
		357.995		
47+	1028+81	8.0	350.0	
+40	1029+21	5.8	352.2	
48+	1029+81	9.6	348.4	
<u>+50</u>	<u>PC1030+31²</u>	9.2	348.8	
+75	1030+56	10.6	347.4	
49+ P ¹	1030+81	10.5	347.5	
F.F.		10.826	347.169	
	0.861	348.030		
	1.241			
+25	1031+06	2.3	345.7	
+50	EC1031+31 ²	4.4	343.6	
50+ EC	1031+81	5.8	342.2	
+50	1032+31	8.0	340.0	

check

1.281
TP 3x8.030 10.8+6 11.571 336.459

0.2x8 336.707

51+ 1032+81 4.5 332.2

TP 11.000 325.707

0.218 325.925

52+ 1033+81 4.8 321.1

+35 1034+16 9.2 316.7

TP 11.470 314.455

0.140 314.595

+45 1034+76

14.4 300.4

53 1034+81 11.5 303.1

54+ 1035+81 6.4 313.2

TP 10.540 314.055

1.889
10.935 324.990

10.540
15.409

+1.889

41.007

-0.520

357.575

314.055

Span pipe



de

on edge

	10.575		314.015
T.P.	324.990	0.775	324.215
	10.700	334.915	
ST+	1036+81	8.1	326.8

B.M. 30 R Sta ST+00
& T.P. Hub.

	4.635	5.108	329.807 ✓
1/5/76		5.883	? PER.
			→ 329.807

11.492 341.299

ST+	1037+81	3.8	337.5
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T.P.		4.274	337.025
	3.576	340.601	

ST+00	1038+21	2.1	338.5
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ST+	1038+81	5.0	335.6
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+80	1039+31	7.7	332.9
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15.068 4.274

4.1635
5.883
+15.775
314.015
329.807

Plotted to here
by PER.

15.068 240.601 4.274
 T.P. 11.750 328.851

4.626 333.477

+42.282
 16.263
 +25.919
 329.801
 355.726

58+ 1039+81 8.4 325.1

+25 1040+06 13.0 320.5

T.P. & 58+70 0.140 338.337

10.992 344.329

59+ 1040+81 5.1 339.2

T.P. 0.084 344.245

+40 1041+21 0.4 343.9

11.596 355.841

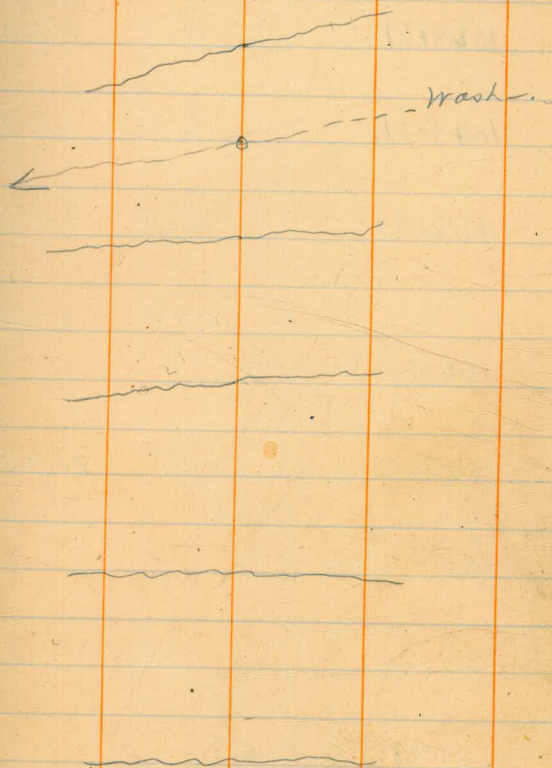
60 1041+81 5.2 350.6

T.P. 4.282 0.115 355.726 ✓

3.058 358.784

16.363

61 1042+81 4.5 354.3



	<u>3.058</u>	358.784		
62+	1043+81	3.4	355.4	
63+	1044+81	4.8	354.0	
64	1045+81	6.5	352.3	
65	1046+81	10.8	348.5	
T.P.		11.784	347.050	
	0.600	347.650		
66	1047+81	7.8	339.8	
2-#66 stations - 66A66b. 0.80s - 1.00 s time.				
BM & T.P.	20 L. 66b. <u>3.658</u>	11.769	336.381 ✓	
	0.088	336.469		
66b.67	1048+81	1.8	335.2	
67 68	1049+81	4.7	331.8	

-23.003
3658
 -19.345
357726
 336.381

0.088 376.469

68+69 1050+81 7.2 329.3 ✓

69+70 1051+81 9.4 327.1

70+71 1052+81 10.4 326.1

71+72 1053+81 9.8 326.7

72+73 1054+81 8.6 327.9

73+74 1055+81 9.5 327.0

T.P. 8.608 327.861

1.828 329.689

74+75 1056+81 5.6 324.1

75+76 1057+81 6.8 323.4

76+77 1058+81 6.8 322.9

T.P. 11.776 317.913

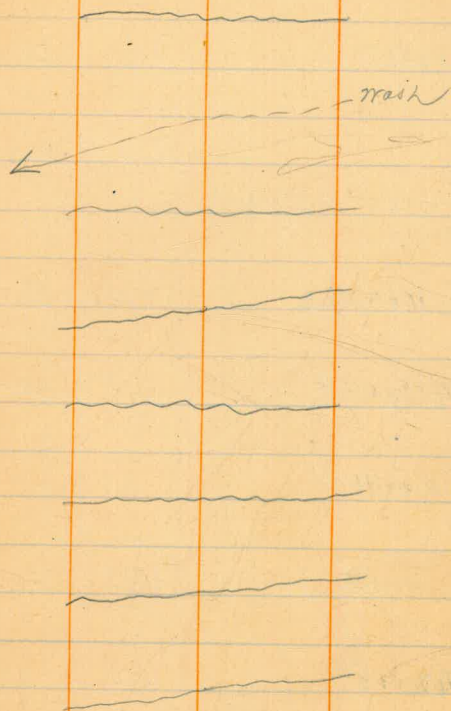
1.916

-6.384

check

T.P.	1916	-20,754	317,917
	0.862	318.775	
77 78	1059+81	2.5	316.5
+75	1060+56	11.-	307.8
78 79	1060+81	7.7	311.1
79 80	1061+81	6.4	312.4
80 81	1062+81	5.9	312.9
81 82	1063+81	7.2	311.6
82 83	1064+81	9.2	309.6
83 84	1065+81	6.8	312.0
T.P.	2770	2810	315,965 ✓
	11,476	25,194	
	327,441	1,920	325,521 ✓
84 85	1066+81	10.5	316.9

-25,194
 2778
 -20,416
 336,787
 315,965



Brown 925, 1078- 118

	11.476		315.965 ✓	✓ PER
		327.441		
85+86	1067+81	5.9	321.5	
8687	1068+81	3.0	320.4	
T.P.		2798	324.648	
	6.559	331.207		
	106481	18.035		
88+89, P.C.	1069+90.2	6.2	325.0	
+ 34.8	1070+158	6.5	324.7	
+ 59.8	" + 408			
↓				
B.M. 76' h.	87+55 Hub	(4.55)	326.652	B.M. ✓ PER
+ 84.8	1070+658	6.7	325.0	
	107081			
88+89	" + 908	6.7	326.9	
+ 19.0	EC 1071+008	6.6	324.6	
8990	1071+91	7.7	324.0	

18.035

2793

315965

✓
VPER

24

9091

1072+81

331.207

9.7

321.5

-25.642

+20.017

-5.625

315.965

310.140

T.P.

1.982

321.650

11.529

319.668

9192

1072+81

3.2

318.2

9293

1074+81

5.2

316.4

Jul

9394

1075+81

6.9

314.7

94+53⁴PC 1076+34⁵

8.2

313.0

+78⁴

" +594

9.6

312.0

95
94+03⁴

1076+81

10.7

310.9
~~311.0~~

PER

T.P.

26.017

1056

311.198

11.510
~~11.542~~

310.140 ✓

+78⁴1077+09⁴

1.7

309.5

+53⁴" +34⁴

3.2

308.0

+83⁴PC 1077+64⁵

6.1

305.1

✓
PER

+ 4,348
- 57,160
- 52,832
370,150
257,308

Down
stay back

1.058 311.198
9560 1077+81 7.7 303.9

T.P. 3000 11.875 299.323
0.665 299.988

+84² 1078+647 6.2 293.8 0

9697 1078+81 8.8 291.2

T.P. 10.996 288.992
1.072 290.064
11.520 278.544
0.650 279.194

9798 1079+81 9.0 270.2

TP & B.M. w/ 97+10 Hub 11.177 268.017

TP 0.902 268.920
4.244 11.612 257.308 ✓
0.382 257.691 57.180

9899 1080+81 6.7 251.0
~~11.520 246.161~~

check

TP 0.783 257.691 11.073 246.618

TP 0.677 247.295 11.476 235.819

0.724 236.543

99+100 1081+81 7.4 229.1

T.P. 11.710 224.833

0.438 225.271

T.P. 11.525 213.746

0.106 213.852

100+101 1082+81 7.6 206.2

TP & BM - 20-R-100+20-Rock 11.197 202.655

1.450 204.105

T.P. 2.978 10.888 193.217 ✓

0.640 193.857

10110 ✓ 1083+81 6.7 187.2

T.P. 11.224 182.633 ✓

.640

193.217
10.584
182.633

✓
check
PER

- 67.869

+ 3.778

- 64.091

257.308

193.217

Down
from
back

TP				182.633	PER
TP	0.634	183.267	11.376	171.891	
102+107	0.135	172.026		171.4	PER
TP	1084+81		0.6	171.5	
TP			11.310	160.716	
	0.096	161.212			
	1.265				
TP+B.M. Hub-30t. 102+80			11.395	149.817	
			34.081		
103101	0.004	150.221			
	1085+81		3.1	149.1	
TP			10.502	139.719	
	1.076			149.817	
		150.893			
	1.745		11.182	139.711	
	0.397	140.108			
104105	1086+81		2.6	139.5	
100	1087+41		8.2	131.9	
175	1087+56		11.1	129.0	
105+80	1087+81		10.7	129.4	

check

~~45.763~~
~~+ 27.05~~
~~- 42.518~~
~~182.633~~
~~140.115~~

~~34.081~~
~~1.265~~
~~32.816~~
~~182.633~~
~~149.817~~
~~10.106~~
~~139.711~~

~~11.182~~
~~1.076~~
~~10.106~~

Dinner dog food

Old Flat

Edge of marsh

dr ✓

Edge ✓

139.711

✓
PBR

28

T.P. 0.297 100.108
11.530 128.578

1.461 130.039

106107 1088+81 2.9 126.1

107108 1089+81 8.3 121.7

1089 1090+81 9.4 120.6

T.P. 11.773 118.266

1.078 119.344

109110 1091+81 3.7 115.6

110111 1092+81 8.4 110.9

JP 1.946 11.200 108.134 ✓
34.512

1.148 109.282

111112 1093+81 2.5 106.8

112113 1094+81 0.4 103.9

- 34.578

2976

- 31.577

139.711

108.134

A/r flat

→

✓
BPER

111.6
45
99.8
117.6

	1.148			
X311 ⁴	1095+81	109.282	6.1	102.9
+50	1096+31		7.7	101.6
+85	1096+66		7.7	101.6
1141 ⁵	1096+81		8.6	100.7
T.P.			1.570	107.712
	3.932	111.600		
11511 ⁶	1097+81		3.9	107.7
11611 ⁷	1098+81		4.8	107.3
+91 ²	BC 1099+72 ¹		6.7	104.9
18=1099+81				
118+16 ²	1099+97 ²		7.9	103.7
+41 ²	1100+22 ²		9.0	102.6
+66 ²	" +47 ²		11.8	99.8
TP			11.459	100.185
	5.000		13.079	

check

2' Wash

Edge of man

2' Deep

Edge ✓

TP

5.080

13.029

100.185

✓
PER

10.3
91.3
10.2

30

2.038 102.223

117+91² 1100+72² 6.2 96.0

1100+81

119+16² 1100+97² 8.7 93.5

check

+41² 1101+22² 10.3 91.9

+66² "+47² 10.8 91.4

+91² "+72² 12.9 89.3

TP

10.850

91.369

0.795 92.164

70 = 1101+81

119+16² 1101+97² 2.1 90.1

41² 1102+22² 2.7 89.5

66² "+47² 3.2 88.8

91² "+72² 4.1 88.1

121 = 1102+81

120+16² 1102+97² 4.1 88.1

7.914

28.482

V PER

	7913	23.889		
120+41	1103+22 ²	92164	4.3	87.9
66	" +47 ²		4.3	87.9
91	<u>EC</u> 1103+22 ²		7.8	84.4
124	1103+81		7.0	85.2
123	1104+81		5.1	87.1
BM&T.P.		3,020	89.144	
	266	91.806		
124	1105+81		5.7	86.1
+20	1106+01		5.4	86.4
124	1106+81		6.7	85.7
125	1107+81		7.5	84.3
127	1108+81		7.9	83.9
T.P.		0.830	90.976	
	10.575	77.738		

check

In ck.

egg ck.

Nail - Squ. Tree - 30 R. 122 + 20

egg mark 2' deep -

✓ ✓ ✓

T.P. 10.575 27.733 106.124
90.976

✓ P.E.R.

12.9 10.616 101.592
1109+81 126 89.0

104.781
7.011
112.190

112.3
7.9
104.4
112.3

32

T.P. 11.122 112.761 0.852 101.139

check

12.8 1110+81 7.9 104.4
94.4

7.415 104.846

24.312

38.601 = 104.781

(.065)

- 3.288

179+227) B.C. 11114054 104.846 ✓

10.942 104.781

115.723

11.5 104.2

8.3 107.4

1.449 114.274

11.638 125.912

1482 89 117.0

1732 4.0 121.9

1982 9 125.0

✓
PER

check

T.P.	125.912	0.863	125.049
	10.640	135.689	
130 ¹ +23 ²		7.8	127.9
+48 ²		5.8	129.9
+73 ²		4.5	131.2
+98 ²		4.1	131.6
138 ² +23 ² = <u>EC</u> 1114+554		3.6	132.1
132 ³		5.0	130.7
138 ⁴		7.1	128.6
138 ⁵		5.3	130.4
138 ⁶		4.4	131.3
138 ⁷		3.6	132.1

135.689

✓
PER

1378

1.1 134.6

T.B

0.697 134.992

11.168

146.160

check

+02² BC

11.6 134.6

+

+27²

11.6 134.6

+52²

10.7 135.5

+77²

9.6 136.6

139+022

8.0 138.2

+27²

6.4 139.3

+52²

7.0 139.2

+77²

8.2 138.0

	146.160			✓ PER
139 + 02 ²		9.2	137.0	
+ 27 ²		9.9	136.3	check
+ 47 ²		9.4	136.8	
140		7.0	139.2	
+ 49 ² <u>EC</u>		(8.846)	137.314	✓ PER 137.312
141		2.9	143.3	
+ P.		1.302	144.818	
	5.060		149.878	
142		5.0	144.5	
143		5.5	144.4	
+ 64 ² <u>PC</u>		4.2	145.7	
+ 89 ²		3.9	146.0	

1x9.878

✓
PER

36

144 + 14² 4.6 1x5.3

+ 34² 3.2 1x6.7

+ 64² 3.4 1x6.5

+ 89² 4.7 1x5.2

145 + 14² 4.6 1x5.3

+ 35 5.0 1x4.9

+ 44² E.C 6.9 1x3.0

+ 50 6.5 1x3.4

146 9.7 1x0.2

TP. 11.686 138.192

0.112 138.304

147 2.3 136.0

check



on the Hill



	138.30x			✓ PER
148		7.3	131.0	check
149 T.P.		11.358	126.946	
	3638	129.584		
		(2335)	127.249	✓ PER (27.27)
149		5.0	124.6	
TP		11.223	118.361 ✓	
	2905	121.266 ✓		
150		4.4	116.9	
151		9.6	111.7	
152 T.P.		10.738	110.528 ✓	
	2310	112.838		
152		4.1	109.7 108.9	PER
148 ² PC		6.2 ✓	106.6 106.8	

152+73 $\frac{1}{2}$	113.838	7.3	105.5 105.7	✓ PER
+98 $\frac{1}{2}$		8.2	104.6 104.8	PER
153+23 $\frac{1}{2}$		8.0	104.4 104.6	
		5.668	107.170	✓ 107.169
+48 $\frac{1}{2}$		8.5	104.3	
+73 $\frac{1}{2}$		8.7	104.1	check
158+98 $\frac{1}{2}$		8.7	104.1	
150+23 $\frac{1}{2}$		7.9	104.9	
+48 $\frac{1}{2}$		7.3	105.5	
+73 $\frac{1}{2}$		6.8	106.0	
+98 $\frac{1}{2}$		5.8	107.0	
155+23 $\frac{1}{2}$		4.9	107.9	

TP	112838	4.103	108.735
155+48 $\frac{1}{2}$	0.593 109.328	+0.5	108.9 109.8
65		+1.1	108.2 109.4
+73 $\frac{1}{2}$		2.9	106.4
TP		11.785	97.943
+98 $\frac{1}{2}$ E.C.	2.372 100.315	5.8	94.5
156+50		6.1	94.2
+75.		5.3	95.0
159		7.7	92.6
+44		8.8	91.5

✓
PER.

PER.



158 100,315 7.2 93.1

159 4.6 95.7

160 2.3 98.0

+80- T.P. on Hub. 1,807 98.508

.8946 107.454

9.448 98.006 97.955

161 8.6 98.8

162 7.5 99.9 PER

163 5.9 101.6 PER

164 5.2 102.3

165 4.2 103.2

166 2.4 105.0 PER

✓
PER

9448
97006

107.0
71

995 925
75 75

107.0 100.0 107 107.4
107.5 75 75

100.0 99.9 107.4

✓
PER

107.454

166187⁸ + TP

0.000 107.454

8.840

116.294

167

8.7 107.6

168

7.5 108.8

169

5.9 110.4

170

4.5 111.8

171

3.0 113.3

+ TP

2.7 113.6

172

1.7 114.6

+ P

0.112 116.182

11.775

127.957

(128.0)

173

11.7 116.7

174

9.7 118.3

128.0
121.957

✓
PER

0.463

42.

175 6.9 121.1

+57 5.6 122.4

check

176 4.7 123.3

177 3.3 124.7

178 1.4 126.6

T.P. 1.205 126.752

9.606 136.358

179 5.7 130.7

180 3.3 133.1

+946 = 1151 + 186 1.6 134.8

D.M. at Bdy 0.463 135.895 135.933

-250
 1157+88
 1148+50
 1148+68
 1090
 101.023
 135.933

✓
PER1157+186
50

+22 Bk Hd. +92 6.0 135.0
 +25 ck bet. +72 10.4 130.6

+35 Lck. +85 11.8 129.2

+56 1149+06
ck. bet. Bk Hd. 9.9 131.1

+58 Top Bk Hd. +08 4.5 136.5

1154 1149+50 7.5 133.5

1153 1150+50 3.9 137.1

1154 1151+50 1.4 139.6

HP 0.762 140.961

1155 11652 152.414
1152+50 10.8 142.1

1156 = 1153+48.8 6.6 145.8

-251
1157 1154+48.8 4.1 149.3

check

2' below cor. of Rd-

In E. Gutter.

153.414

✓
E

PER

In E. Gutter

1158 = 1155 + 0.3⁴ 1.7 150.7

-0.57

TP 11.965 0.010 152.404

164.369

1159 1156 + 48⁴ 11.5 152.91160 1157 + 48⁵ 7.4 157.01161 1158 + 48⁵ 4.0 160.4+0.47^{pl}

= 1159 + 0.3

1162 1159 + 48⁵ 0.7 163.7

TP 0.558 163.816

11.224 175.040

1163 1160 + 48⁵ 8.6 166.41164 1161 + 48⁴ 5.9 169.1

2060 175.032 - 2060 172.980 172.972

PER

1165 1162 + 48 2.0 173.0

TP 0.041 174.591

✓
PER.

T.P. 174.591

11.9 x 7 186.538

1166 1163 + 47 10.1 176.6

1167 1164 + 46⁰ 6.7 179.81168 1165 + 46[±] 3.9 182.6

check

T.P. 0.776 185.796

11.3 x 9 197.145

1169 1166 + 46[±] 10.7 186.41170 1167 + 46[±] 6.7 190.81171 1168 + 46[±] 3.5 193.6

7.965 197.165 7.965 189.180 189.200

T.P. 0.572 196.643

11.303 207.946

1172 1169 + 46[±] 10.6 197.3

✓
PER

207.946

1173 1170+45 7.4 200.5

1174 1171+44 4.1 203.8

+ 22 Pl. = 1172+43

1175 1172+43 1.9 206.0

T.P. 0.200 207.606

1176 10.305 207.951
1173+43 8.5 209.4

1177 1174+42 5.7 212.2

4.449 216.0
217.962 ~~4449~~ 213.502 213.513

1178 1175+42 3.2 214.8

T.P. 0.154 217.808
10.695 218.503

1179 1176+42 10.2 218.3

1180 1177+42 7.2 221.3

+ 39
Bot. 18" Culv. 8.4 220.1

✓
PER

1181	228.503 1178+42 ²	4.8	223.7
1182 ✓	1179+42	7.4	226.1
T.P.	10.620 238.649	0.474	228.019
1183 ✓	1180+42	10.7	228.3
1184	1181+42	7.9	230.9
+95	1182+37 18" G.L.C. Bot.	7.4	231.2
1185	1182+42	5.8	232.8
+10 1186	1182+5 ✓ 1183+42	3.6	235.0
1187	1184+40	1.2	237.4
T.P.	11.858 250.481	0.026	238.673
1188	E=25' 1185+89	11.0	239.5

shook

✓
PER

	250.481		
	10,166	250.000	10,166
			250.315
			250.278
1188+38	1185+77		
	Tap 40" Culv.	12.1	238.3
1189	1186+35	8.8	241.6 ✓ check
1190	1187+34	5.0	245.0 ✓
1191	1188+30.9	1.3	249.1 ✓
	(-269)		
TP		0.104	250.302
	11,951		262.293
1192	1189+31	8.5	253.8 ✓
1193	1190+31	4.1	258.2 ✓
1194	1191+31		262.7 ✓
TP		0.255	262.038
	(11,940)		
	11,924		273.972
1195	1192+31	6.8	267.2
+15 =	11,922		272.9
1196	1193+31	4.1	277.0
	(11,952)		
TP		0.61	271.91

1187+78
69

48

	250.28		
	10.88		
		47.1	251.16
		11.4	
1188		239.8	
		9.2	
1189		242.0	
		5.8	
1190		245.0	
		5.4	
1191		249.3	
		5.0	
TP		250.36	
		+ 11.7	
47.1		262.06	
		5.4	
1192		253.7	
		4.1	
1193		258.0	
		0.52	
TP		261.74	
		+ 10.28	
		272.02	
		9.8	
1194		262.7	
		5.1	
		267.4	
		1.1	
		271.14	

✓
PDR

281.491

	11.730	283.640		271.91
1197	1194+31		7.7	275.9
+60 =	1194+40 ⁵			
1198 ²⁶⁹	1195+31		25	281.1
T.P. + B.M.		2135	281.505	281.491

B.M. 281.491

	11.812	293.303			check
1199+0	1196+31		7.3	286.0	
1200+0	1197+31		2.5	290.8	
TP			0.440	292.863	

	10.400	303.263		
1201+0	1198+31		7.3	296.0
1202+0	1199+31		1.5	301.9
TP			0.220	303.043

	9.727	312.770		
1203+0	1200+31		5.2	307.6
²⁶⁹ +28 = 1200+56.7			0.6	312.0
1204+0	1201+31		0.220	312.550
TP				

	10.606	323.156		
1205	1202+31		4.0	317.2
1206+0	1203+31		1.7	321.5
TP + B.M.			1.480	321.676 321.748

	11.190	332.938		
1207	1204+31		5.0	327.9

Record

✓ PER

	332.938		
TP		0.270	332.668
	10.370	343.038	
1208	1205+31	2.9	333.1
+0V	= 1207+31.7		
1209	1206+3	6.0	337.0
+22	= 1206+57.7		
○ form Bezellr	4.583	338.455	
TP		1.785	341.253
	5.580	346.833	
1210+17		4.6	342.2
+5.2		2.2	344.6
TP		11.895	334.938
	7.100	342.038	
1210+85		11.2	330.8
1211+0		4.7	337.3
TP		2.040	339.998
	12.750	352.757	
1211+21		6.0	346.7
TP		2.700	350.047
	12.150	362.197	
+40		8.5	353.7
+65		8.4	353.8
+72		4.9	357.3
1212+0		4.3	357.9
+50		4.3	357.9
+57		4.7	357.5

check

sto 040 of 'B' 117x

362197

✓
PFR

51

+70		4.0	358.2	
1212+94.1		2.2	360.0	
1213+00		2.2	360.0	
1214+0		4.3	357.9	
1215+0		4.5	357.7	
TP		4.170	358.027	358.028
	7.543	365.571		
1216+0		10.1	355.5	
1216+95		12.9	352.7	check
121700		12.2	353.4	
1218+0		9.6	356.0	
1219+0		7.2	358.4	
in gutter N. side		7.9	357.7	
on curb N "		6.8	358.9	
1220+0		6.1	359.5	
+08		6.5	359.1	
on Bm SWX		1.750	363.821	363.85

Record

Record Elev

El Cajon Blvd
of Parked area

El Cajon & Pawley

Line from 1210+17
Via Fairmount ave ✓
PER

Near 1209+0

Peg at 341.253
10.673 351.926

1210+17 9.7 342.2
1211+00 5.0 346.9
TP 1.420 350.506

10.135 360.641

1212+0 9.3 351.3
1213+0 5.7 354.9
1214+0 5.2 358.4
1215+0 4.8 355.8
1216+0 4.6 356.0
1217+0 4.4 356.2
TP 4.135 356.446

8.227 364.673

1218+0 8.1 356.6
1219+0 7.9 356.8
1220+0 7.7 357.0
+33 6.8 357.4
+71.8 curb 6.5 358.2
1221+0 6.5 358.2
1222+0 5.8 358.9

PI of Line thru Alley 5.6 369.1
0.878 343.795 363.85

check

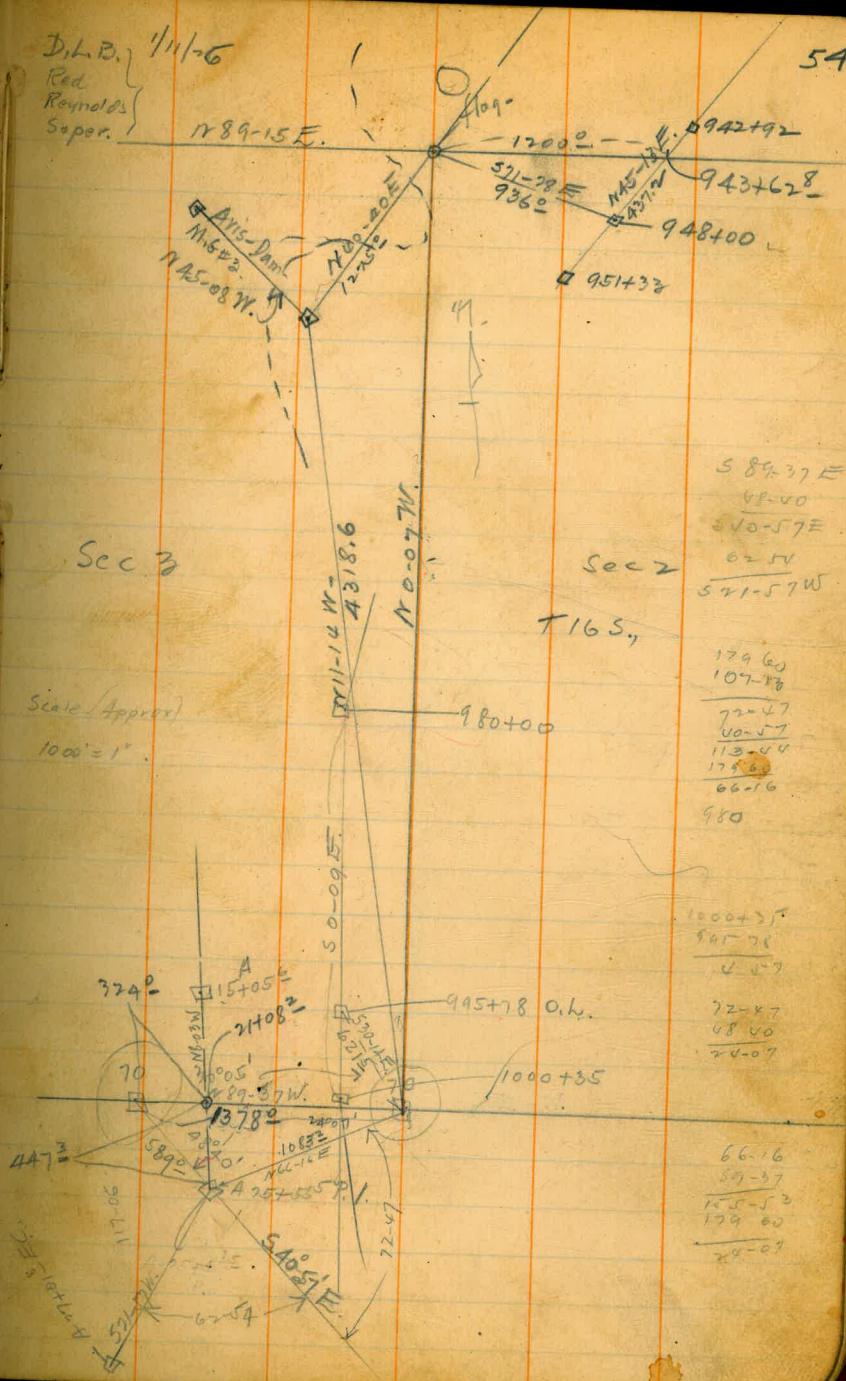
Record Use

B.M. p.c. 27773 Sta W777				417.355	Sta	+	413.209	-	Elev.
Sta	+	+	-	Elev.					
	4.170	421.525 ✓			420+80.9B.C.			6.8	406.4
413+40.9B.C.			1.7	419.8	421+25				
					TP			8.576	404.633 ✓
418+13			2.3	419.2		5.080	409.713 ✓		
414+85.3E.C.			5.5	416.0	422+25			5.5	404.2
415+00			4.9	416.6	422+40			5.3	404.4
415+25			6.2	415.3	422+45			3.2	406.5
416+00			10.7	410.8	423+68.7E.C.			4.8	404.9
TP			1						
		12.458		409.067 ✓	424+00			5.0	404.7
	4.142	413.209 ✓							
416+50			5.5	407.7	425+00			4.7	405.0
417+00			5.6	407.6	426+00			4.9	404.8
418+00			4.8	408.4	427+00			4.6	405.1
419+00			5.3	407.9	427+ ²⁵ ₁₅			5.7	404.0
420+00			6.1	407.1	427+30			7.8	401.9

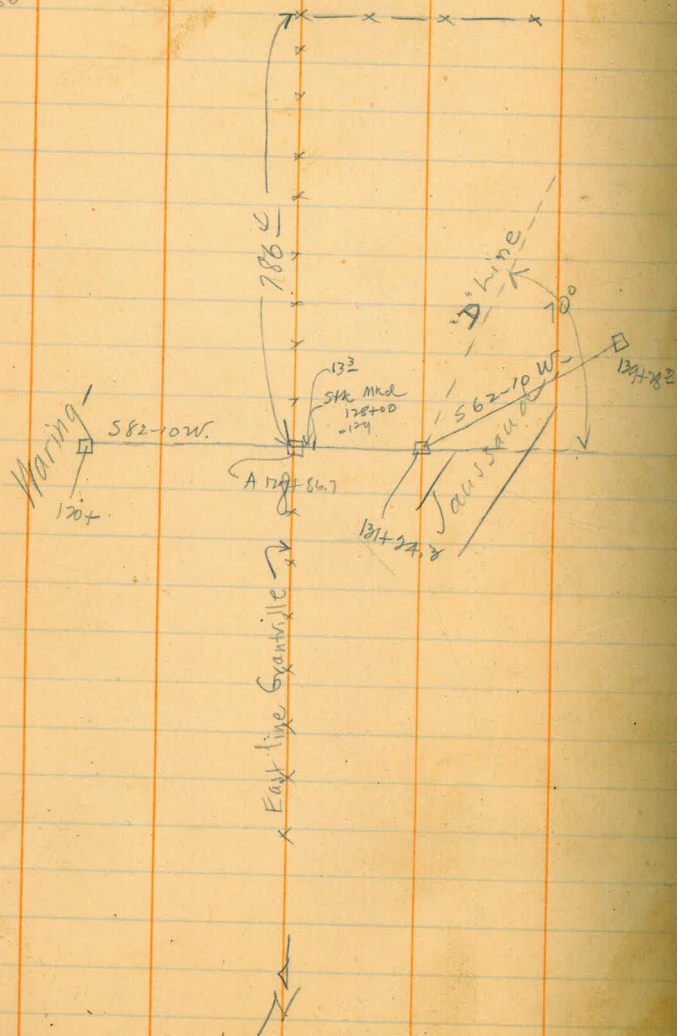
Sta	T	Elev.
	409.713	
427+40	5.3	400.6
427+90	6.2	403.5
428+00	9.0	400.9
+15	9.4	400.3
+25	6.0	403.9
+31	6.1	403.6
40 Param	7.3	402.6
60 ✓	7.3	402.4
428+00 P.L. +T.P.	8.715	400.998
5.495	406.493	
	6.080	400.413

D.L.B. 1/11-6
Red Reynolds Super.

54



128+00
133
178+86



N/A
 P.L.
 Pinned

D. Line Beg. at "A" 129+22.7

237.0

$139+22$ F.C. = $1123+42.4$ O.L.
 $R = 2800'$ S40-10W

$10^\circ C$
 $T = 142.9$
 $E = 17.5$
 $L = 280$
 25' chds.
 $R = 572.96$

1830.6

137+85 P.L. = $1121+96.4$ O.L.

137
 +42 BC
 136
 135
 134+
 133+
 21.3
 132+72.7 F.C.

369.3

130+97.2 ctr. of Curve

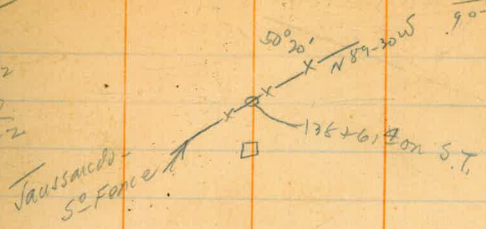
200.0
 $T = 201.6$
 $E = 63.2$
 $L = 350$
 $R = 286.48$
 25' chds

A 131+22.7 P.L. L 70°00'

$129+22.7 = 1111+05.4$
 BC on A line
 S62-10W

713.9

100.6
 24.0
 76.4
 $137+85$
 1386.1



56

$136+32$
 $136+67$
 $136+92$
 $137+17$
 + 62
 + 67

1364
 1372
 72.7
 369.3
 143.6
 201.6
 713.9

26-11
 13-57
 27-24
 27.9

Put 2 cons - piers - 1135+75

1141+39.3 EC = 1139+03⁸ S6°46'W

1140+30 Pl. L46-47
1 226

1139+05.4 DC = 1136+69⁶

S40°04'W

200C

T = ~~123.9~~

E = ~~22.7~~

L = 223.9

25' chords

R = 286.48

25.6

1180+30
1 226
1181+54.6



235.8

206.8

207.2

Gd. Inst.

H.I.

206.8

208.775

Inst. at 1100 on tang- ptg - 50

	Azi	Dist.	Va.	
	81°30'	20.0	-14°	
	111°00'	25.0	-16°10'	
	48°00'	160.0	-25°40'	
	61°30'	170.0	-26°20'	up 2
	36°00'	188.0	-22°20'	
	27°10'	122.0	-28°20'	up 2
359-60	8°10'	112.0	-29°30'	up 2
18-60	341°20'	100.0	-28°10'	up 4
	350°30'	125.0	-13°30'	
	7°00'	130.0	-15°30'	
	17°45'	155.0	-14°30'	
	6°30'	156	-7°10'	
	0°00'	159	-3°30'	
	352°00'	153	-2°15'	
	348°00'	50	-26°00'	up 2
	33°00'	55	-26°10'	up 3

Hmng

Diff
E1

2022

Elev

18	-5.78	196.9	✓
22	-6.78	195.9	✓
130	-6.78	139.4	✓
138	-70.0	132.2	✓
160	-66.0	136.2	✓
94	-53.0	149.2	✓
85	-50.0	152.2	✓
78	-45.6	156.6	✓
117	-26.78	173.9	✓
121	-33.4	168.8	✓
145	-37.6	164.6	✓
152	-19.4	182.8	✓
158	-9.7	191.5	✓
158	-6.0	196.2	✓
47	-70.8	181.4	✓
58	-74.6	179.6	✓

Road

58

207.540
92
206.575

175 + 59.3

170 + 71.2 P.O.T. = 175 + 59.6 E.C.

175 + 59.6 S42°43'W
170 + 70.9 E.C.

E=8.1
T=107.7
R=716.20
D=8°
L=213.8

~~169 + 64.8~~ 17° 06'

173 + 45.8
~~174 + 44.5~~
168 + 57.1 B.C.

173 + 44.8 = 168 + 56.1 S59°49'W 1.0
168 + 56.1 E.C.

E=1.7
T=19.6
R=114.59
D=50°
L=38.9

Δ 168 + 36.8 19° 27' R

168 + 17.2 B.C.

S40°22'W 3233.5
Δ 135 + 83.7 4° 02' L

S44°24'W 80.7

135 + 03.0 E.C.

174 + 53.2 Old Sta 174 + 68

128.3

(173 + 44.5)

173 + 24.9 E.C.

3253.1
135 + 83.7 P.O.T

Sta	Hor L	Bear	Vert L	H. I	Rod	Vert. Dist	Elev.	Hor Dist
K 25+51	A 58° 11' R	*				229.5		
			-9° 35'		6.83	-112.3		665 ^x Frd from "G"
J 23+71	P.O.T	W				221.7		
			-13° 20'		5.11	-115.1		485 ⁶⁶⁵ Frd. from "G"
I 23+45	P.O.T.					222.3		
			-14° 02'		4.87	-114.5		459 ⁶⁶⁵ Frd. from "G"
HH 23+04	P.O.T	N 39° 20' W				219.4		
			-16° 19'		4.53	-122.4		418 ⁶⁶⁵ Frd. from "G"
Δ 9 18+86	A 10° 17' L	*				336.8		
			-11° 18'		2.23	-42.9		215 ^x Frd from "F"
H F 16+71	P.O.T					379.7		
			-2° 03'		1.18	-4.2		119 ⁶⁶⁵ Frd from "D"
E 10+52	P.O.T	W				286.9		
			-10° 57'		5.18	-97.0		500 ⁶⁶⁵ Back from "D"
D 15+52	P.O.T					383.9		
A			+8° 47'		6.04	+91.2		590 ⁶⁶⁵ Frd. from "B"
C 2+19	P.O.T.	N 29° 03' W				190.4		
			-16° 34'		1.11	-30.6		103 ⁶⁶⁵ Frd. from Sta "A"
B 9+62	P.O.T.					292.7		
			+4° 25'		9.67	+74.2		962 ⁶⁶⁵ Frd from 0+00
Δ A 1+16	P.O.T					231.0		
			+1° 15'		1.15	+2.5		116.0 ⁶⁶⁵ Frd. from 0+00
0+00	A 05° 00' R					218.5		= Sta 15+05.6 "A" Line
12+89.9		S 45° 52' N						Sta on "A" Line

Sta.	Hor. L	Bear.	Vert. L	H. I.	Rod	Vert. Dist.	Elev.	Hor. Dist.	
W59+31.5A	27°32'R						279.8		
		N61°40'E	-1°09'		0.74	- 1.5		75	Frd from "V"
V58+55.5A	37°01'R						281.3		
		N24°39'E	-0°40'		2.53	- 3.0		254	Frd from "U"
+ U56+01.5A	10°49'L						284.3		
		N35°28'E	-1°10'		1.83	- 3.7		184	Frd from "T"
T54+17.5A	15°19'L						288.0		
		N50°47'E	-0°49'		3.74	- 5.3		375	Frd from "S"
S50+42.5A	12°27'30"R						293.3		
		N38°19.5'E	-1°02'		6.70	- 12.1		671	Frd from "R"
R43+71.5A	30°03'30"R						305.4		
		N8°16'E	-2°26'		2.16	- 9.1		217	Frd from "Q"
Q41+54.5A	60°02'30"L						314.5		
		N68°18.5'E	-2°43'		1.32	- 6.3		133	Frd from "P"
+ P40+21.5A	12°26'R						320.8		
		N55°52.5'E	+2°57'		3.90	+ 20.1		390	Frd from "O"
A036+31.5A	31°12'R						300.7		
		N24°40.5'E	+4°14'		4.00	+ 29.5		399	Frd from "N"
I N32+39.5A	13°00'R						271.2		
		N11°40.5'E	+3°21'		1.03	+ 6.1		104	Frd from "M"
M31+35.5A	25°17'L						265.1		
		N36°57.5'E	+4°06'		2.94	+ 21.0		292.5	Frd from "L"
A L28+43A	18°6'30"R						244.1		
		N18°51'E	+3°51'		2.92	+ 19.6		292	Frd from "K"
K25+51A	58°11'R						224.5		
		(H39-20W)	-9°35'		6.83	- 112.3		665	Frd from "G"

Sta.	Hor. \angle	Bear.	Vert. \angle	H.L.	Rod	Vert. Dist.	Elev.	Hor. Dist.	
I, 93+46 Δ	13°20'30" L						293.1 294.1		
		S65°52.5'E	-3°20'		3.56	✓ 20.7	313.8	356	Frd from "H,"
H, 89+90 Δ	29°08' L						314.8		
		S36°44.5'E	-4°06'		2.11	✓ - 15.1	328.9	211	Frd. from "G,"
+ G, 87+79 Δ	50°50' R						329.9		
		S87°34.5'E	-3°28'		1.59	✓ - 9.7	338.6	159	Frd from "F,"
F, 86+20 Δ	35°12' L						339.6		
		S52°22.5'E	-3°42'		2.16	✓ - 13.9	352.5	216	Frd from "E,"
E, 84+04 Δ	30°29'30" R						353.5		
		S82°52'E	-1°20'		3.66	✓ - 8.5	361.0	367	Frd from "D,"
D, 80+37 Δ	36°39' R								
		N60°29'E	+0°31'		0.80	✓ + .72	360.3	81	Frd from "C,"
C, 79+56 Δ	21°43' R								
		N38°46'E	+3°22'		6.92	✓ + 40.6	691	691	Frd from "B,"
+ B, 72+65 Δ	19°16'30" R						319.7		
		N24°29.5'E	+1°56'		5.36	✓ + 18.1	537	536.5	Frd from "A,"
Δ A, 67+28.5 Δ	21°44' R						301.6		
		N2°42.5'E	+0°28'		0.93	✓ + 0.8	94	94	Frd from "Z"
I Z, 66+34.5 Δ	56°09'30" R						300.8		
		N53°27'W	+3°49'		3.16	✓ + 21.0	316	316	Frd from "Y"
Y, 63+18.5 Δ	47°39'30" L						279.8		
		N5°47.5'W	+1°12'		0.74	✓ + 1.5	75	75	Frd from "X"
Δ X, 62+43.5 Δ	99°59'30" L						278.3		
		N89°12'E	-0°17'		3.12	✓ - 1.5	313	313	Frd from "W"
W, 59+30.5 Δ	27°32' R						279.8		

Sta.	Hor. L	Bear.	Vert. L	H. I.	Rod	Vert. Dist	Elev.	Hor. Dist.	
U,	$\Delta 8^{\circ}06'30''R$						284.5		
T,	$\Delta 19^{\circ}16'30''R$		$-0^{\circ}08'$		6.56	- 1.5	284 286.0	657	Frd from "T,"
S,	$\Delta 68^{\circ}57'L$		$+13^{\circ}02'$		0.68	+ 3.7		69	Frd from "S,"
R,	$\Delta 36^{\circ}36'30''R$		$-0^{\circ}58'$		6.60	- 11.2	282.3	661	Frd from "R,"
Q,	$\Delta 70^{\circ}24'R$		$-1^{\circ}18'$		1.18	- 2.7	293.5	119	Frd from "Q"
P,	$\Delta 22^{\circ}20'L$		$-0^{\circ}05'$		4.78	- .72	296.2	479	Frd from "P,"
O,	$\Delta 26^{\circ}05'30''L$		$-2^{\circ}26'$		2.30	- 9.7	296.9	231	Frd. from "O,"
N,	Δ		$-3^{\circ}28'$		0.91	- 5.5	306.6	92	Frd from "N,"
M,	$111+60 \Delta$	$N7^{\circ}04'E$	$-3^{\circ}40'$		6.66	- 42.6	312.1 354.7 355.7	664	Frd. from "M,"
L,	$108+44 \Delta$	$N7^{\circ}52'E$	$-1^{\circ}55'$		3.15 ✓	- 10.5 ✓	365.2 366.2	316 ✓	Frd from "L,"
K,	$105+60 \Delta$	$N38^{\circ}07.5'E$	$+2^{\circ}15'$		2.83 ✓	+ 11.1 ✓	354.1 355.1	284 ✓	Frd from "K,"
J,	$99+83 \Delta$	$N61^{\circ}19'E$	$+2^{\circ}22'$		5.78 ✓	+ 23.9 ✓	330.2 331.2	577 ✓	Frd. from "J,"
I,	$93+46 \Delta$	$S79^{\circ}13'E$	$+3^{\circ}20'$		6.38 ✓	+ 37.1 ✓	293.1 294.1	637 ✓	Frd. from "I,"

Relocation El Monte Park
April 1926

= 127+85.1 E.C.
127+87.5 E.C.

Δ 126+92.7 25°45' L ✓

125+94.3 B.C. ✓

570°24' W 172.0

124+22.3 E.C. ✓

Δ 122+46.2 14°07' L ✓

120+69.3 B.C.

584°31' W 417.5 ✓

116+51.8 E.C. ✓

Δ 116+32.5 8°23' L ✓

116+12.2 B.C.

N87°06' W

E=117.1 ✓
T=98.4 ✓
R=430.50 ✓
D=13°20' ✓
L=193.2 ✓

P.I.

3

7

4

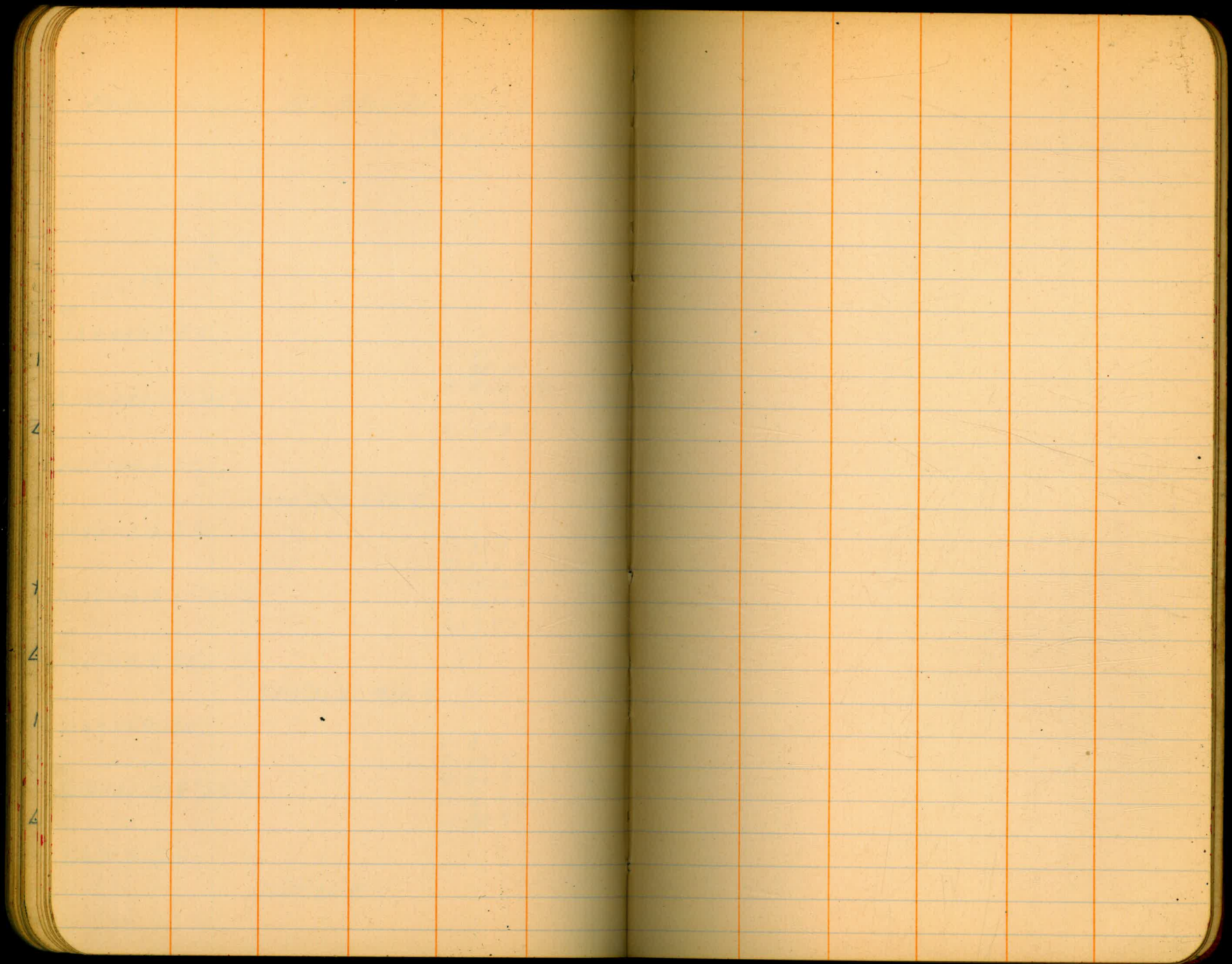
4

P.I.

614.0

P.I.

E=0.7 ✓
T=19.6 ✓
R=267.45 ✓
D=21°32' ✓
L=38.9 ✓



130+74.3 P.L. L. 70°00' KA+12-40

10° C.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in for column and top row. The number in body

of table in same row and column gives distance level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod and find distance in table. If it does not make the slight adjustment

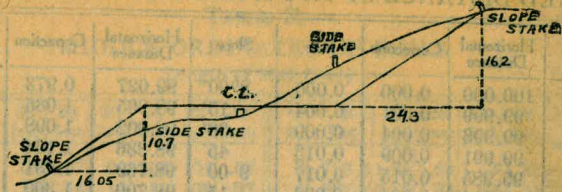
**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00										0
1	1.50	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

T
E
20' 4011.9
200.6
201.6
126
62.2
62.2

MH cover

Iron Pipe 357.877

Iron B 258.024

" 263.85

1127 300 1130 1133

300
300
900.00
60
900.00

80
50
6000

505.770
3.590
502.184

300

265.078
926
264.152

Coules

M3340

1100
1110
1120

4011.9
200.5

4011.9
200.5
1.
201.5

1374.85
1314.27
5.123
2.216
71.5

110.3
78
51.1
25.64
11
55.8