

EL CAPITAN  
Pipe Line Survey  
Levels — No 3

A

LEVEL BOOK

389

W193A

MICROFILMED  
JAN 4 1965

El Capitan Pipe Line Survey

Levels and profile over preliminary survey (from Sta. 1037+00 to Sta. 1150+55, run by C.M. Boren — Page 3 to 25

Levels and cross-sections over relocated line Sta. 9+33.8 to 110+31.7, run by Leach and McCarty — 25 —

## List of B.M. From 994+00 -

B.M. No.	Elev.	Location	
343.846		2 x 2 Hub 18' R Sta. 994+00	
334.450		Hub 65' L Sta. 1000+75	
272.993		2 x 2 Hub 30' L 1007+50	
384.109		B.M. + T.E. Lath 11 1011+82	
320.646		Lath 7' L 1018+16	
360.992		2 x 2 Hub 7' L 1025+0	
349.652		2 x 2 Hub 10' R 1036+90	
328.918		2 x 2 Hub 55' ± R 1042+00	
324.921		2 x 2 Hub 60' R 1045+80	
344.891		Lath 13' L 1053+68	
338.962		2 x 2 Hub 15' L 1061+00	
335.403		2 x 2 Hub 18' L 1072+50	
297.011		2 x 2 Hub 15' R 1075+30	
269.116		2 x 2 Hub 40' R 1085+75	
258.142		2 x 2 Hub 18' L 1088+73	
229.522		2 x 2 " 7' L 1097+00	
190.559		2 x 2 Hub 11' R 1102+72	
87.845		(nailed) 2 x 2 Hub 80' L 1107+00	
104.781		Nail in 8" tree 1' L 12897 A line	
137.312		(nailed) Hub 35' R A 1111+00	
140.950		Nail in post 30' R A 1144+55	
127.224		2 x 2 Hub 15' L A 149+10	
107.169		(nailed) Hub 18' L A 153+25	
97.955		Hub 30' R A 153+85	
110.826		Hub 65' R A 171+00	
135.938		Bolt Head Fairmont Sta. 1151+25 County Bridge	

B.M. #	Elev.	Location	
153.855		2 x 2 Hub Near Sta 1153+00	
172.987		2 x 2 Hub 10' L 1164+63	
187.990		Hub 25' R 1170+65	
213.528		Hub 5' L 1174+50	
240.308		Hub 8' L 1188+00	
251.596		Hub 32' R 1198+21	
220.960		Lath 1 1200+00	
321.748		Hub 6' L 1203+96	
358.088		Iron Bolt in Alloy	
363.850		Brass Plug in Carb E. L. Cajon + Boulder	



Sta	+	x	B.M.	-	Elev
	2.221	351.873			349.652
1037+00			3.5		348.4 ✓
+45			4.7		347.2 ✓
+80			8.6		343.3 ✓
1038+0			9.6		342.3 ✓
+50			12.2		339.7 ✓
1039+0			10.9		341.0 ✓
+50			8.4		343.5 ✓
1040+0			8.8		343.1 ✓
T.P.			8.736		343.137 ✓
	1.520	344.657			
+50			2.5		342.2 ✓
1041+0			4.5		340.2 ✓
+35			7.1		337.6 ✓
T.P.			11.335		333.322 ✓
	2.668	335.990			
1042+0			8.5		327.5 ✓
T.P. on B.M.			7.070		328.920 328.918 ✓
	0.385	329.303			
+40			8.7		320.6 ✓
T.P.			11.445		317.858 ✓
	0.405	318.263			
+70			7.7		310.6 ✓
T.P.			11.417		306.846 ✓
	0.520	307.366			

near sta. 1036+00

3

Jan 2 '26  
Boren-Rod  
Red-Ins  
Rup-Rec.

Record  
Elev. ✓

2x2 Hub 55'-R. 1042+0

Sta	+	307.366 K	-	Elev.
1043+0			7.1	300.3 ✓
T.P.			11.152	296.214 ✓
	2.302	298.516		
T.P.			11.625	286.891 ✓
	2.745	299.636		
+35			7.2	282.4 ✓
T.P.			11.993	277.643 ✓
	0.652	278.295		
+80			0.6	277.7 ✓
1044+0			3.9	274.4 ✓
+35			9.2	
			8.2	259.1 ✓
T.P.			11.599	266.695 ✓
	9.440	276.136		
+90			10.4	265.7 ✓
+92			11.6	264.5 ✓
1045+0			11.8	264.3 ✓
T.P.			2.020	274.16 ✓
	11.826	285.942		
+18			9.2	276.7 ✓
T.P.			1.825	284.117 ✓
	11.588	295.705		
+45			12.2	283.5 ✓
			1.105	294.600 ✓
T.P.	11.933	306.433		
+70			10.1	296.3 ✓

PER.

Sta.	+	306.433 T	-	Elev.
1046+0			1.3	305.1 ✓
T.P.			0.055	306.378 ✓
	11.825	318.203		PER
+40			11.0	307.2 ✓
+60			2.3	315.9 ✓
T.P.			0.100	318.103 ✓
	11.534	329.637		
1047+0			3.8	325.9 ✓
+15			0.1	329.5 ✓
T.P. on B.M.			4.715	324.922 334.921
	10.516	335.137		
+35			0.5	334.9 ✓
T.P.			0.253	335.184 ✓
	10.789	345.973		
+60			3.8	342.2 ✓
+85			1.6	344.4 ✓
1084+0			1.4	344.6 ✓
T.P.			0.565	345.408 ✓
+25			<del>0.5</del>	
	7.625	353.033		
+25			7.6	345.4 ✓
1049+0			7.7	345.3 ✓
+75			6.1	346.9 ✓
1050+0			5.3	347.7 ✓
+50			3.9	349.1 ✓

2x2 Hub 60'R 1045+80

Record Elev.

	+	353.033	-	Elev.	
1051+0			3.6	349.4	✓
+50			2.5	350.5	✓ PER
1052+0			1.7	351.3	✓
+30			1.2	351.8	✓
1053+0			4.4	348.6	✓ Rec Elev
T.P. on B.M.			8.160	344.873	344.891
	0.546	345.437			
+70			1.8	343.6	✓
1154+0			6.8	338.6	✓
+30			11.9	333.5	✓
T.P.			11.657	333.780	
	0.565	334.345			
1055+0			9.1	325.2	✓
T.P.			11.495	322.850	
	2.255	330.105			
1056+0			10.5	319.6	✓
+40			10.3	319.8	✓
+65			7.9	322.2	✓
+85			7.6	322.5	✓
1057+0			6.3	323.8	✓
+30			4.0	326.1	✓
+55			1.0	329.0	✓
T.P.			0.045	330.060	
	6.330	336.390			
1058+0			8.3	333.1	✓

Lath 13' L 1053+68



Sta.	+	336.390	-	Elev.
1058+30			2.3	334.1 ✓
+55			1.9	334.5 ✓
+80			2.1	334.3 ✓
1059+0			3.2	333.2 ✓
1060+0			6.0	330.4 ✓
1061+0			8.4	328.0 ✓
T.P. on BM.			7.407	328.983 ✓
	1.180	<del>330.142</del> 316.3		328.962 ✓
1062+0			4.9	325.2 ✓
+50			5.9	324.2 ✓
+75			5.2	324.9 ✓
1063+0			6.0	324.1 ✓
+85			3.9	326.2 ✓
1064+0			5.1	325.0 ✓
T.P.			11.913	318.229 ✓
	0.150	318.379		
1065+0			2.9	315.5 ✓
+20			<del>4.9</del> 10.7	313.5 ✓
+30			7.5	310.9 ✓
+82			<del>12.1</del>	
+40			10.0	308.4 ✓
T.P.			11.790	306.589 ✓
	5.710	312.299		
+70			10.6	301.7 ✓
+75			13.0	299.3 ✓
+85			6.7	305.6 ✓
1066+0			4.6	307.7 ✓

2x2 Hub 15' L 1061+0

center of Draw.  
slopes to left of line.

Sta	+	T	-	Elev.
T.P.		312.299	3.691	308.608
	8.160	316.768		
1066+70			5.7	311.1 ✓
1067+0			6.1	310.7 ✓
+50			5.5	311.3 ✓
1068+0			3.7	313.1 ✓
1069+0			5.8	311.0 ✓
T.P.			5.635	311.133
	9.190	320.323		
+40			8.2	312.1 ✓
1070+0			7.4	312.9 ✓
+50			4.6	315.7 ✓
T.P.			2.931	317.392
	11.311	328.703		
1071+0			10.6	318.1 ✓
+35			9.0	319.7 ✓
+55			6.9	321.8 ✓
1072+0			5.9	322.8 ✓
T. Ron B.M.			3.315	325.388 325.403
	4.205	329.608		
+25			5.9	323.7 ✓
+50			4.2	325.4 ✓
+70			5.2	324.4 ✓
1073+0			4.4	325.2 ✓
+20			4.2	325.4 ✓

PER

Red Elev.

2 x 8 Hub 18" L 1072+50

Sta.	+	Σ	-	Elev.
1073+60		329.608	4.8	324.8 ✓
+80			3.5	326.1 ✓
1074+0			4.8	324.8 ✓
+55			4.2	325.4 ✓
1075+0			5.4	324.2 ✓
+45			5.5	324.1 ✓
1076+0			8.1	321.5 ✓
+30			9.7	319.9 ✓
+45			9.5	320.1 ✓
<del>1077</del>			11.136	318.472
T.P.	1.400	319.872		
1077+0			2.8	317.1 ✓
+18			3.0	316.9 ✓
+50			4.9	315.0 ✓
+65			3.6	316.3 ✓
+75			4.2	315.7 ✓
+90			7.1	312.8 ✓
1079+0			6.9	313.0 ✓
+15			7.4	312.5 ✓
+25			8.7	311.2 ✓
+50			10.2	309.7 ✓
T.P.			11.591	308.281
	0.922	309.203		
1079+0			5.7	303.5 ✓
+32			11.3	297.9 ✓

	+	309.203 +	-	Elev.	Reg Elev.
T.P. on B.M.			11.190	298.013	298.011
	1.388	299.399			
1079+70			11.9	287.5	✓
T.P.			11.685	287.544	
	0.039	287.583			
1080+0			9.5	279.3	✓
T.P.			11.677	276.06	✓
	1.154	277.260			
T.P.			11.821	265.439	PER
	0.466	265.905		<del>289.081</del>	
+50			1.2	264.7	✓
T.P.			11.462	254.443	
	0.765	255.208			
T.P.			9.605	245.603	
	0.765	246.368			
1081+00			4.0	242.4	✓
TP			12.808	233.560	
	1.280	234.840			
TP			12.917	221.923	
	1.102	223.025			
TP			12.137	210.888	
	0.063	210.951			
+80			9.4	202.3	✓
1082+00			10.5	200.4	✓

2x2 Hub 15'R 1079+30

Jan 4 1926  
 Garcia Instr.  
 Simpson Rod.

210.951

Sta	+	X	-	ELEV	
TP			12.360	198.591	♀
	3.167	201.758			
+10			5.0	196.8	PER
TP			11.895	189.863	
	8.585	198.448			
+30			11.1	187.3	✓
+55			10.8	187.6	✓
+60			12.0	186.4	✓
+72			16.4	188.0	✓
1083+00			3.5	194.9	✓
TP			1.300	197.148	
	11.727	208.875			
+10			10.7	198.2	✓
TP			0.915	207.960	
	12.168	220.128			
TP			0.720	219.408	
	12.262	231.670			
+78			10.6	221.1	✓
1084+0			3.2	228.5	
TP			0.400	231.270	
	11.260	242.530			
TP			0.355	242.175	
	12.970	255.145			
1085			4.9	250.2	✓
TP			0.875	254.270	

St.	+	x	-	254.270 Elev
	11.290	265.560		
1085+26			9.2	256.4 ✓
TP			4.590	260.970
	9.695	270.665		
TP on B.M.			1.580	269.085 269.116
	0.031	269.147		Use Record Elev
TP	11.604		12.604	256.543 ← <del>256.543</del>
	3.293	<del>259.836</del>		
1086+00			1.9	257.9 ✓
+75			10.1	249.7 ✓
TP			11.335	249.501 ←
	5.586	254.087		
1086+94			11.2	242.9 ✓
1087+0			7.7	246.4 ✓
+35			1.7	242.4 ✓
TP			0.295	253.792
	9.662	263.454		
+64			5.5	258.0 ✓
1088+00			3.5	260.0 ✓
+30			1.8	<del>261.7</del> ✓
TP on B.M.			5.265	259.189 258.112
	7.975	266.117		
1088+73			3.2	262.9 ✓
1089+0			4.0	262.1 ✓
+30			6.8	259.3 ✓

Record Elev

PPR

Record Elev

40' R 1085+75

Check Lim. for error!

+	x	=
0.836	269.952	

266.117

1089+50		4.2	259.9	✓
1090+0		11.4	254.7	✓
1091+0		12.4	253.7	✓
TP		12.249	253.168	✓
	2.650		255.818	
+35		2.7	253.1	✓
1092+0		7.0	249.8	✓
+15		7.6	248.2	✓
TP		12.811	243.007	✓
	3.180		246.187	
1093+0		4.2	242.0	✓
1094+0		7.9	238.3	✓
1095+0		12.1	234.1	✓
TP		12.090	234.097	✓
	4.625		238.722	
1096+0		5.6	233.1	✓
1097+00		7.2	231.5	✓
TP on B.M.		9.050	229.672	✓
	3.550		233.222	
1098+00.3		3.7	229.5	✓
1099+00		8.5	224.7	✓
TP		12.487	220.535	✓
	0.680		221.215	
1099+85		1.7	219.5	✓
1100+00		3.4	217.8	✓

Record B.M.

7' L 1097+40

221.215

1101+00

TP

10.3 210.9 ✓

12.450 208.565 ✓

0.303 208.868

1102+0

7.4 201.4 ✓

+24

11.5 197.4 ✓

TP

12.441 196.427 ✓

0.640 197.067

1102+72

TP on BM.

6.7 190.4 ✓

6.427 190.640 190.559

use Record Elev

0.467 191.026

1103+0

TP

8.0 183.0 ✓

12.610 178.416 ✓

0.950 179.366

+35

4.3 175.1 ✓

+55

11.8 167.6 ✓

TP

12.150 167.216 ✓

2.665 169.881

+70

TP

6.2 163.7 ✓

12.532 157.349 ✓

1.568 158.917

1104+00

6.0 152.9 ✓

+65

7.7 151.2 ✓

TP

12.540 146.377 ✓

1.250 147.627

Record Elev

PER

11' R 1102+72



St.	+	π	-	Elev	
		147.627			
TP			12.450	135.177	✗
	2.030	137.207			PER
1105+0			10.3	127.9	✓
TP			12.820	124.387	
	2.627	127.014			
TP			12.847	114.167	
	0.490	114.657			
1106+00			3.7	116.0	✓
TP			12.342	102.315	
	0.180	102.495			
1106+68			1.4	101.1	✓
+79			4.2	98.3	✓
+84			7.5	95.0	✓
1107+00			11.8	91.7	✓
TP			12.726	89.769	
	3.387	93.146			
+12			6.2	86.9	✓
+23			7.8	85.4	✓
TP 017 BM <sub>1</sub>			5.420	87.726	87.845
	2360	90205			use Record Elev
1108+0			5.2	85.0	✓
+80			5.6	86.5	84.6 ✓
+84			7.6	82.6	✓
1109+0			7.5	82.7	✓

80' L 1107+0

	30.205			
TP		5.490	84.715	PER
	5A55	90.170		
1110+00		5.2	85.0	✓
+05		5.4	84.8	✓
+10		7.5	82.7	✓
+20		4.2	86.0	✓
1111+00		5.2	85.0	✓
1112+00		6.1	84.1	✓
1112+02	A125+21	6.1	84.1	✓
1113+00		2.3	87.9	✓
TP +16		1.5	89.7	✓
		2.383	87.787	

	11.266	99.053		
TP		0.372	98.681	
	12.896	111.577		
TP		0.342	111.235	
	12.680	123.915		
TP		0.405	123.510	
	12.892	136.402		
1113+90		9.9	126.5	✓
1114+00		5.8	130.6	✓
TP	49.734	3.503	132.899	✓
	12.151	145.050		
+28		4.0	141.0	✓

Redline

approx intersect of Blue &  
 A125+21 = 1112+02

49734

45732

+45112

89569

137899

Jan 5 1926

Running Transit  
 as a Level

Boren Inst.  
 Simpson Rod.

Sto	+	-	Elev
TP	12.157	143.050	0.460 144.590
+54	12.610	157.200	8.8 148.4
TP + B.M.	8.873	164.258	1.815 155.385
1115+00			5.8 158.5
+20			2.2 162.1
+40			2.4 161.9
+45			2.9 161.4
TP			12.911 151.347
TP	1700	153.047	11.675 141.372
116+00	1.653	143.025	6.9 136.1
TP			11.565 131.460
+22	5.830	137.290	10.8 126.5
+46			12.4 124.9
+53			11.1 126.2
TP			0.710 136.580
1117+0	12.464	149.044	7.9 141.1
TP	<del>12.263</del>	<del>141.004</del>	0.303 148.741
TP	12.263	141.004	1.357 159.647

PER.

Hub 15' R St. 1115+00

55781  
 39479  
 +15.842  
 132294  
 148.141

Sta	+	$\pi$	-	PC9
	11.640	177.287 <del>170.287</del>		159.647
TP			0.367	170.920
	11.930	182.850		
TP			0.448	182.402
	12.190	194.592		
1118+0			3.5	191.1
TP			0.323	194.269
	12.842	207.111		
T.P.			1.100	206.011
	13.000	219.011		
T.P.			0.553	218.458
	12.585	231.043		
1118+60			9.1	221.9
T.P. #			0.647	230.396
	12.150	242.546		
+80			12.1	232.4
1119+0			6.6	235.9
+05			5.4	237.1
+18			3.4	239.1
T.P. *			1.655	240.891
	12.811	253.702		
+40			10.1	243.6
1120+0			2.9	250.8
T.P. on B.M.	11.411		0.700	253.002
	12.155	265.167		

11.211  
5.293  
+105.648  
148.741  
254.359  
1.357  
253.002

2x2 Hub 18'R 1120+00

Sta	12115	265.157	-	Elev.
	+	T		
1120+35			9.3	255.9 ✓
+50			4.9	260.3 ✓
+85			0.6	264.6 ✓
T.P.			0.295	264.862 ✓
	11.790	276.652		
1121+0			8.9	267.8 ✓
+40			1.3	275.4 ✓
T.P.			1.107	275.545 ✓
	11.085	286.630		
T.P.			0.108	286.522 ✓
	11.783	298.305		
1122+0			11.1	287.2 ✓
T.P.			0.290	298.015 ✓
	12.257	310.272		
1123+0			6.5	303.8 ✓
T.P.			0.587	309.685 ✓
	12.050	321.735		
+70			4.8	316.9 ✓
1124+0			1.2	320.5 ✓
T.P.			0.095	321.640 ✓
	12.285	333.925		
+50			6.4	327.5 ✓
1125+0			0.1	333.8 ✓
T.P. on BM	83.405		0.608	333.317 ✓
	11.680	344.997	3.090	

PER

83405  
 3090  
 89315  
 753002  
 227317

10' L 1125+00 2 x 2 Hub.

Sta	+	π	-	Elev.	
1125+50			5.3	339.7 ✓ <del>339.7</del>	
+80			2.7	342.3 ✓	
1126+0			2.3	342.7 ✓	
+20			2.3	342.7 ✓	
1127+0			3.1	341.9 ✓	
T.P.			3.125	341.872	
	2.650	344.522			
+70			4.5	340.0 ✓	
1128+0			7.7	336.8 ✓	
T.P.			12.485	332.037 ✓ T.P.	
<del>150</del>	2.320	334.357			
+50			2.9	331.5 ✓	
1129+0			9.9	324.5 ✓	
+25			13.0	321.4 ✓	
T.P.			12.701	321.656	
	2.432	324.088			
+75			12.2	311.9 ✓	
T.P. on B.M.			12.130	311.958 ✓ 311.958	
	2.940	314.898			
1130+0			7.6	307.3 ✓	
T.P.			12.906	302.092	
	5.570	307.662			
+30			6.9	302.8 ✓	
T.P.			2.962	303.900 ✓	
	9.882	313.782			

57.009  
 27.192  
 — 29.417  
 333.717  
 — 303.900

2x2 Hob 1129+75

1128+75

Sta.	+	π	-	Elev.
1130+80	2.8	313.782	2.8	311.0 ✓
1131+0			0.3	313.5 ✓
T.P.			0.400	313.382 ✓
	12.325	325.707		
T.P.			0.415	325.292 ✓
	12.920	338.282		
1132+0			9.5	328.8 ✓
1132+50			5.0	333.3 ✓
1133+0			0.8	337.5 ✓
T.P.			0.787	337.495 ✓
	2.815	340.310		
+8			1.8	338.5 ✓
+46			2.7	337.6 ✓
+56			3.4	336.9 ✓
1134+0			13.1	327.2 ✓
T.P.			12.410	327.900 ✓
	1.610	329.510		
+32			9.8	319.7 ✓
T.P.			12.670	316.840 ✓
	2.445	319.285		
+70			13.0	306.3 ✓
T.P.			12.710	306.575 ✓
	3.750	310.325		
1135+0			10.6	299.7 ✓
T. Pon B.M.			11.945	298.380 ✓
				298.379 ✓

2x2 H-6 B'R 113570

Sta.	+	T	-	Elev.
				297.380
	2.222	301.602		
1135+15			4.4	297.2 ✓
T.P.			12.471	289.131 ✓
	2.061	291.192		
1136+0			4.6	286.6 ✓
+42			7.0	284.2 ✓
+44			8.1	283.1 ✓
+46			7.0	284.2 ✓
+70			5.0	286.2 ✓
1137+0			4.8	286.4 ✓
T.P.			3.340	287.852 ✓
	4.090	291.942		
+60			1.9	290.0 ✓
1138+0			4.4	287.5 ✓
+28			6.9	285.0 ✓
+51			10.0	281.9 ✓
T.P.			12.324	279.618 ✓
	1.060	280.678		
+85			6.7	279.9 ✓
1139+0			9.0	271.6 ✓
T.P.			12.730	267.948 ✓
	0.345	262.293		
+40			11.5	256.8 ✓
TP			12.750	256.543 ✓
	0238	255.781		

Note

The - Rod on TP was originally Recorded as 11.730. This threw us out one foot at Sta. 11514 at BM. Upon a check backward over TP & BM, this was proven to be 12.738 as now recorded

CMB.



Sta	+	255.781	-	Elev.	
TP on B.M.			11.743	244.038	244.037
	0.264	244.402			Hub C.L. 1140+0
1140+0			1.7	242.7	✓
1140+30			9.8	234.6	✓
TP			12.470	231.932	✓
	2.247	234.179			
1141+0			3.2	231.0	✓
+30			4.5	229.7	✓
+65			6.3	227.9	✓
1142+0			9.0	226.2	✓
+25			11.1	223.1	✓
TP			12.310	221.869	✓
	2.260	224.129			
1142+55			3.3	220.8	✓
1143+00			6.4	217.7	✓
+10			6.8	217.3	✓
TP			12.450	212.679	✓
	1.210	212.889			
1143+70			1.2	211.7	✓
1143+90			1.6	211.3	✓
1144+00			2.6	210.3	✓
+15			4.5	208.4	✓
+50			6.9	206.0	✓
+80			8.1	204.8	✓
1145+00			10.8	202.1	✓

Jan 6. 1926

Boren  
Simpson  
RuplingerInst.  
Book  
Rod

Sta.	+	212889 T	-	Elev.
TP on B.M.			8.490	204.399 <del>204.318</del> ✓
	1.164	205.563		
1145+10			8.3	197.3 ✓
TP			11.195	194.368 ✓
	0.122	194.490		
TP			12.827	181.663 ✓
	0.928	182.591		
TP			12.483	170.108 ✓
	1.355	171.463		
TP			12.760	158.703 ✓
?	3.685	162.388		
1145+77			7.5	154.9 ✓
+82			11.5	150.9 ✓
+85			8.6	153.8 ✓
+92			7.5	154.9 ✓
1146+00			4.0	158.4 ✓
TP			0.840	161.548 ✓
	11.300	172.848		
TP			0.145	172.703 ✓
	9.860	182.563		
TP			0.140	182.423 ✓
	10.960	193.383		
1146+40			8.43	184.0 ✓
+50			4.3	189.1 ✓
+59.5			0.8	192.6 ✓

2x2 Hvb. 10' L Sta 1145+00

Sta.	+	193.383 T	-	Elev	
1146+75			4.0	189.4 ✓	
1147+00			9.1	184.3 ✓	
TP			11.240	182.143	PER
	3.358	185.501			
1147+75			10.1	175.4 ✓	
TP			12.480	173.021	
	3.420	176.441			
1148+00			5.0	171.4 ✓	
+20			10.7	165.7 ✓	
1149+00			10.5	165.9 ✓	
+20			9.1	167.3 ✓	
TP			13.000	163.441	
	0.513	163.954			
1149+36.1			1.7	163.3 ✓	
TP			11.324	152.630	
	0.615	153.245			
1150+00			6.8	146.4 ✓	
+25			9.4	143.8 ✓	
TP			11.455	141.790	
	3.265	145.055			
1150+34.6			5.0	140.1 ✓	
+55			9.4	135.7 ✓	
TP on B.M			9.113	135.942	135.938

Bolt in N. End of Fairmount Bridge

Levels from 9+33.8 to 19+77.5

McCarty-Ins  
Eeach-rod  
Reynolds-rod

Jan 26  
clear

Sta.	+	π	-	El.
BM# 2				570.564
7+2	6.506	577.070		
9+33.8			5.9	571.2 ✓
9+52.5			5.7	571.4 ✓
9+57.1			7.7	569.4 ✓
9+58.8			7.8	569.3 ✓
9+63.0			7.1	570.0 ✓
9+62			7.2	569.9 ✓
9+83.8			7.1	570.0 ✓
10+08.8			7.3	569.8 ✓
10+33.8			7.7	569.4 ✓
10+58.8			8.3	568.8 ✓ <del>569.8</del>
10+83.8			8.0	569.1 ✓
TP on BM	6.504			570.566

573.4 ✓	572.1 ✓	568.8 ✓	569.6 ✓
$\frac{32}{100}$	$\frac{50}{22}$	$\frac{83}{45}$	$\frac{85}{100}$
573.7 ✓		568.9 ✓	568.7 ✓
$\frac{34}{100}$		$\frac{82}{70}$	$\frac{84}{100}$
571.3 ✓			568.6 ✓
$\frac{58}{100}$			$\frac{85}{100}$
571.0 ✓			568.6 ✓
$\frac{61}{100}$			$\frac{85}{100}$
572.7 ✓	572.0 ✓	571.1 ✓	568.7 ✓
$\frac{44}{100}$	$\frac{51}{60}$	$\frac{60}{45}$	$\frac{84}{100}$
571.2 ✓			568.7 ✓
$\frac{53}{100}$			$\frac{84}{100}$
573.0 ✓	571.3 ✓	569.0 ✓	568.9 ✓
$\frac{41}{100}$	$\frac{58}{28}$	$\frac{81}{12}$	$\frac{82}{100}$
574.8 ✓	572.0 ✓	571.0 ✓	569.1 ✓
$\frac{23}{100}$	$\frac{51}{32}$	$\frac{61}{22}$	$\frac{82}{15}$
			568.9 ✓
			$\frac{82}{22}$
			568.7 ✓
			$\frac{84}{32}$
			568.4 ✓
			$\frac{82}{100}$
574.7 ✓		568.2 ✓	567.9 ✓
$\frac{24}{100}$		$\frac{82}{32}$	$\frac{92}{100}$
574.3 ✓	572.5 ✓	567.7 ✓	567.6 ✓
$\frac{28}{100}$	$\frac{45}{52}$	$\frac{74}{34}$	$\frac{95}{100}$
574.8 ✓	571.0 ✓	567.9 ✓	567.3 ✓
$\frac{23}{100}$	$\frac{61}{18}$	$\frac{92}{14}$	$\frac{98}{100}$

	+	$\pi$	-	Elev
TP				570.566
	4.994	575.560		
11+08.8			5.7	569.9
11+				
11+33.8			4.2	571.4
11+58.8			3.9	571.7
11+68.0			4.3	571.3
11+72.2			4.2	571.4
				568.9
11+95.5			6.7	<del>569.9</del>
11+97.7			6.0	569.6
11+99.3			5.5	570.1
12+22.3			2.2	573.4
TP			0.428	575.132
	6.314	581.446		
12+47.7			5.8	575.6

				$\epsilon$
574.1	570.8	568.0	567.2	567.0
$\frac{15}{100}$	$\frac{48}{16}$	$\frac{76}{32}$	$\frac{84}{63}$	$\frac{86}{70}$
574.1	570.9	568.8	567.7	567.4
$\frac{15}{100}$	$\frac{47}{19}$	$\frac{68}{56}$	$\frac{79}{83}$	$\frac{82}{70}$
573.5	570.9	570.3	569.6	568.2
$\frac{21}{100}$	$\frac{47}{35}$	$\frac{53}{42}$	$\frac{62}{49}$	$\frac{74}{89}$
				$\frac{76}{100}$
573.4	570.6	568.6	568.4	
$\frac{22}{100}$	$\frac{52}{33}$	$\frac{72}{92}$	$\frac{72}{102}$	
573.2	570.8	569.1	568.5	
$\frac{24}{100}$	$\frac{48}{42}$	$\frac{65}{72}$	$\frac{71}{102}$	
571.4	569.7	567.9	568.4	568.1
$\frac{42}{100}$	$\frac{52}{03}$	$\frac{72}{43}$	$\frac{72}{56}$	$\frac{75}{102}$
571.6	570.0	568.8	568.2	568.1
$\frac{42}{100}$	$\frac{56}{06}$	$\frac{68}{17}$	$\frac{74}{22}$	$\frac{75}{45}$
				$\frac{71}{54}$
				$\frac{75}{102}$
571.8	569.9	569.1	568.1	
$\frac{38}{100}$	$\frac{52}{13}$	$\frac{63}{22}$	$\frac{75}{102}$	
570.2	573.3	569.6	569.0	568.7
576.0?	$\frac{54}{100}$	$\frac{23}{22}$	$\frac{62}{82}$	$\frac{62}{94}$
				$\frac{62}{102}$
579.0	573.3	569.4	568.5	
$\frac{24}{100}$	$\frac{81}{31}$	$\frac{128}{72}$	$\frac{129}{102}$	

Sta	+	π	-	Elev
		581.446		
12+60.2			7.1	574.3 ✓
12+72.7			9.9	571.5 ✓
12+97.7			6.9	574.5 ✓
13+07.7			7.0	574.4 ✓
13+09.2			5.2	576.2 ✓
13+22.7			4.8	576.6 ✓
13+25.3			4.8	576.6 ✓
350				
13+60.3			3.8	577.6 ✓
14+24.4			5.1	576.3 ✓
TP		583.422 ✓	5.739	575.70.7 ✓
	7.715	(583.418)		
14+54.4			6.5	576.9 ✓
14+78.9			9.9	573.5 ✓

581.4

579.6	577.9	576.9	573.3	569.9	564.4	568.3
$\frac{18}{100}$	$\frac{35}{66}$	$\frac{45}{32}$	$\frac{81}{11}$	$\frac{115}{32}$	$\frac{130}{63}$	$\frac{131}{100}$
576.6	576.2	574.9	568.6			568.1
$\frac{28}{100}$	$\frac{52}{52}$	$\frac{66}{48}$	$\frac{128}{44}$			$\frac{133}{100}$
579.6	577.0	571.7	569.9	569.1	568.9	
$\frac{18}{100}$	$\frac{44}{32}$	$\frac{92}{42}$	$\frac{115}{56}$	$\frac{123}{84}$	$\frac{125}{100}$	
579.9	577.7	575.2	572.1	569.9	669.6	
$\frac{15}{100}$	$\frac{32}{28}$	$\frac{62}{12}$	$\frac{93}{53}$	$\frac{115}{85}$	$\frac{118}{100}$	
579.4		574.4	573.3	571.9	570.1	569.4
$\frac{16}{100}$		$\frac{70}{13}$	$\frac{81}{31}$	$\frac{95}{52}$	$\frac{113}{75}$	$\frac{120}{100}$
576.0		575.4	573.4	571.2	570.3	
$\frac{09}{100}$		$\frac{56}{19}$	$\frac{80}{40}$	$\frac{102}{81}$	$\frac{114}{100}$	
576.0		575.7	573.6	571.5	570.9	
$\frac{10}{100}$		$\frac{52}{25}$	$\frac{78}{43}$	$\frac{99}{78}$	$\frac{113}{100}$	
581.4		574.4	571.5		570.3	
$\frac{00}{100}$		$\frac{70}{60}$	$\frac{99}{83}$		$\frac{111}{100}$	
Foot of Large Boulder		574.9			571.4	
		$\frac{25}{85}$			$\frac{100}{100}$	

Foot of Large Boulder

Large Boulders

Two Rods - one on other

576.2	573.9	572.4	583.4
$\frac{32}{100}$	$\frac{80}{19}$	$\frac{95}{42}$	$\frac{110}{100}$
576.7	572.0	566.4	565.6
$\frac{67}{100}$	$\frac{114}{40}$	$\frac{140}{49}$	$\frac{170}{83}$

McCarty -  
Inst. to 3M#3  
Leach  
Reynolds

Jan 27  
Clear-cold

Sta.	+	π	-	575.707
TP	0.638	576.345		
15+00.2			5.1	571.2
15+08.6			6.0	570.3
15+60.5			7.0	569.3
TP			9.170	567.175
	6.81	573.98		
16+00			4.3	570.7
TP	6.767	573.942		
16+64			10.2	563.7
16+73			12.2	561.7
16+77			11.5	562.4
TP			10.584	563.358
	10.430	573.788		
17+00			11.3	562.5
Jan. 27 -				
17+15.6			10.1	563.7
17+19.0			6.3	567.5

€				
574.1 ✓ $\begin{array}{r} 573.1 \\ 23 \\ \hline 700 \end{array}$	570.6 ✓ $\begin{array}{r} 57 \\ 25 \\ \hline 72 \end{array}$	567.1 ✓ $\begin{array}{r} 92 \\ 72 \\ \hline 100 \end{array}$	566.2 ✓ $\begin{array}{r} 101 \\ 100 \end{array}$	576.3
573.7 ✓ $\begin{array}{r} 26 \\ 700 \end{array}$	569.5 ✓ $\begin{array}{r} 60 \\ 26 \\ \hline 700 \end{array}$	566.7 ✓ $\begin{array}{r} 96 \\ 40 \end{array}$	565.6 ✓ $\begin{array}{r} 107 \\ 100 \end{array}$	
570.4 ✓ $\begin{array}{r} 59 \\ 100 \end{array}$			566.2 ✓ $\begin{array}{r} 101 \\ 100 \end{array}$	
570.3 ✓ $\begin{array}{r} 32 \\ 700 \end{array}$			565.5 ✓ $\begin{array}{r} 85 \\ 116 \end{array}$	574.0
562.1 ✓ $\begin{array}{r} 118 \\ 100 \end{array}$		Boulder	563.5 ✓ $\begin{array}{r} 109 \\ 100 \end{array}$	573.9
565.0 ✓ $\begin{array}{r} 87 \\ 700 \end{array}$	563.5 ✓ $\begin{array}{r} 104 \\ 60 \\ \hline 50 \end{array}$	561.7 ✓ $\begin{array}{r} 123 \\ 72 \end{array}$	562.4 ✓ $\begin{array}{r} 115 \\ 700 \end{array}$	
565.6 ✓ $\begin{array}{r} 81 \\ 700 \end{array}$	564.6 ✓ $\begin{array}{r} 93 \\ 86 \end{array}$	564.0 ✓ $\begin{array}{r} 99 \\ 67 \end{array}$	562.1 ✓ $\begin{array}{r} 121 \\ 63 \end{array}$	562.2 ✓ $\begin{array}{r} 112 \\ 76 \\ \hline 100 \end{array}$
		562.4 ✓ $\begin{array}{r} 115 \\ 30 \end{array}$		
		561.8 ✓ $\begin{array}{r} 121 \\ 63 \end{array}$		
		562.1 ✓ $\begin{array}{r} 112 \\ 76 \end{array}$		
568.0 ✓ $\begin{array}{r} 58 \\ 100 \end{array}$	562.9 ✓ $\begin{array}{r} 109 \\ 51 \\ \hline 100 \end{array}$	561.6 ✓ $\begin{array}{r} 122 \\ 100 \end{array}$		573.8
569.7 ✓ $\begin{array}{r} 41 \\ 100 \end{array}$	567.4 ✓ $\begin{array}{r} 64 \\ 17 \end{array}$		562.3 ✓ $\begin{array}{r} 115 \\ 700 \end{array}$	
570.0 ✓ $\begin{array}{r} 38 \\ 100 \end{array}$		563.4 ✓ $\begin{array}{r} 100 \\ 16 \end{array}$	562.0 ✓ $\begin{array}{r} 112 \\ 100 \end{array}$	
		563.1 ✓ $\begin{array}{r} 103 \\ 49 \end{array}$		

	+	$\bar{\Lambda}$	-	Elev
65.5 17+ <del>32.6</del>		573.788	4.8	569.0 ✓
17+50.5			5.1	568.7 ✓
18+00			5.8	568.0 ✓
18+47.5 74			7.4	566.4 ✓
18+54.9			9.6	564.2 ✓
18+74.2			9.8	564.0 ✓
18+89.5 $\frac{10E}{100R}$				
18+91.2			10.0	563.8 ✓
19+00			9.8	564.0 ✓
19+17.9 96			10.2	563.6 ✓
19+27.5 TP			9.8	564.0 ✓
	12.732	576.090	10.430	563.358 ✓
19+52.5			10.6	565.5 ✓
19+77.5			5.1	571.0 ✓

Two  
rods

571.1 ✓ $\frac{22}{100}$	568.0 ✓ $\frac{50}{51}$	563.6 ✓ $\frac{102}{75}$	563.4 ✓ $\frac{104}{100}$	573.8 ✓
571.9 ✓ $\frac{19}{100}$	567.7 ✓ $\frac{61}{42}$	564.7 ✓ $\frac{91}{65}$	563.7 ✓ $\frac{101}{89}$	563.5 ✓ $\frac{103}{100}$
571.0 ✓ $\frac{28}{100}$	567.2 ✓ $\frac{66}{38}$	565.4 ✓ $\frac{84}{51}$	563.6 ✓ $\frac{102}{78}$	563.3 ✓ $\frac{105}{100}$
569.6 ✓ $\frac{42}{100}$	567.2 ✓ $\frac{66}{11}$	564.0 ✓ $\frac{98}{22}$	563.5 ✓ $\frac{103}{100}$	
568.8 ✓ $\frac{50}{100}$	566.7 ✓ $\frac{71}{31}$		564.0 ✓ $\frac{98}{100}$	
568.3 ✓ $\frac{55}{100}$	568.2 ✓ $\frac{56}{95}$	564.2 ✓ $\frac{96}{45}$	563.7 ✓ $\frac{101}{100}$	562.7 ✓
567.9 ✓ $\frac{59}{100}$	567.7 ✓ $\frac{61}{90}$	564.3 ✓ $\frac{95}{80}$	563.6 ✓ $\frac{102}{45}$	562.4 ✓ $\frac{114}{58}$
564.4 ✓ $\frac{94}{100}$		563.8 ✓ $\frac{100}{70}$	562.5 ✓ $\frac{113}{28}$	561.7 ✓ $\frac{121}{100}$
563.6 ✓ $\frac{102}{100}$	563.9 ✓ $\frac{99}{100}$	560.2 ✓ $\frac{138}{57}$		560.8 ✓ $\frac{130}{100}$
563.7 ✓ $\frac{101}{100}$	564.2 ✓ $\frac{98}{66}$	563.5 ✓ $\frac{103}{43}$	562.6 ✓ $\frac{112}{54}$	559.1 ✓ $\frac{147}{100}$
561.5 ✓ $\frac{86}{100}$	566.8 ✓ $\frac{93}{31}$	564.8 ✓ $\frac{113}{18}$		561.2 ✓ $\frac{126}{100}$
573.5 ✓ $\frac{26}{110}$		564.5 ✓ $\frac{66}{82}$		564.7 ✓ $\frac{114}{100}$
				576.1 ✓ $\frac{567.0}{91}$



Leach-Inst. Clear 4  
 McCarly-Rod Cool  
 Reynolds-Rod

£

BM# 3

576.090

Recorded

5.916 570.174 570.171

570.171

T.P. 7.316 577.487

20+02.5 4.7 572.8

20+17.9 4.4 573.1

20+27.5 4.1 573.4

20+52.5 6.0 571.5

20+72.5 7.3 570.2

20+77.5 8.1 569.4

20+81.5 9.5 568.0

21+03.5 7.8 569.7

22+50 T.P. on rock 5.170 572.317

5.661 (577.978)

21+48.8 7.7 570.3

Foot of rock -  $\frac{3}{10} = 574.0$  ✓  
 $\frac{2}{10} = 575.2$  ✓  
 $\frac{3}{6} = 574.0$  ✓  
 $\frac{4}{4} = 572.7$  ✓  
 $\frac{2}{8} = 570.5$  ✓  
 $\frac{7}{10} = 570.2$  ✓  
 $\frac{2}{10} = 574.9$  ✓  
 $\frac{4}{4} = 573.1$  ✓  
 $\frac{5}{10} = 571.7$  ✓  
 $\frac{3}{10} = 574.0$  ✓  
 $\frac{6}{3} = 571.0$  ✓  
 $\frac{7}{7} = 569.9$  ✓  
 $\frac{8}{5} = 568.1$  ✓  
 $\frac{8}{10} = 568.9$  ✓  
 $\frac{6}{10} = 570.8$  ✓  
 $\frac{6}{4} = 571.0$  ✓  
 $\frac{7}{18} = 569.9$  ✓  
 $\frac{9}{5} = 568.4$  ✓  
 $\frac{9}{10} = 567.7$  ✓  
 $\frac{4}{10} = 572.6$  ✓  
 $\frac{7}{3} = 570.4$  ✓  
 $\frac{8}{2} = 569.3$  ✓  
 $\frac{9}{5} = 568.4$  ✓  
 $\frac{9}{10} = 567.7$  ✓  
 $\frac{4}{10} = 573.1$  ✓  
 $\frac{9}{19} = 567.8$  ✓  
 $\frac{10}{10} = 566.6$  ✓  
 $\frac{2}{10} = 575.1$  ✓  
 $\frac{5}{2} = 572.3$  ✓  
 $\frac{9}{3} = 568.1$  ✓  
 $\frac{10}{10} = 567.9$  ✓

From H.I. elev  
 577.978

Sta.	+	∏	-	Elev.
		(577.978)		
21+72.4			8.8	569.2 ✓
21+96.4			9.6	568.4 ✓
22+06.4			9.5	568.5 ✓
22+16.4			9.2	568.8 ✓
22+26.4			8.8	569.2 ✓
22+36.4			8.3	569.7 ✓
22+46.4			8.3	569.7 ✓
22+56.4			7.9	570.1 ✓
22+66.4			5.6	572.4 ✓ T.P. near sta-22+50 572.317
	10.982	583.299		
22+72.1			8.0	575.3 ✓
23+00			4.9	578.4 ✓
+13 sta 23+20 T.P. on Rock.			3.8	579.5 ✓
			1.311	581.988 ✓

Note - This elev.  
Taken from  
H.J. 592.210

574.2 ✓	571.5 ✓	568.3 ✓	568.2 ✓
$\frac{38}{100}$	$\frac{65}{40}$	$\frac{92}{15}$	$\frac{98}{100}$
573.5 ✓	572.5 ✓	568.7 ✓	568.8 ✓
$\frac{45}{100}$	$\frac{52}{70}$	$\frac{92}{20}$	$\frac{99}{100}$
573.0 ✓	570.5 ✓	568.9 ✓	568.6 ✓
$\frac{50}{100}$	$\frac{75}{50}$	$\frac{92}{32}$	$\frac{92}{100}$
	571.8 ✓	569.2 ✓	568.8 ✓
	$\frac{62}{100}$	$\frac{88}{60}$	$\frac{92}{100}$
	571.5 ✓	569.5 ✓	569.0 ✓
	$\frac{52}{100}$	$\frac{85}{50}$	$\frac{88}{100}$
	571.3 ✓	570.0 ✓	569.2 ✓
	$\frac{52}{100}$	$\frac{80}{41}$	$\frac{85}{100}$
	572.9 ✓	569.9 ✓	569.5 ✓
	$\frac{52}{100}$	$\frac{82}{24}$	$\frac{81}{100}$
	575.5 ✓	570.2 ✓	569.9 ✓
	$\frac{22}{100}$	$\frac{48}{30}$	$\frac{78}{100}$
	573.8 ✓	575.6 ✓	570.5 ✓
	$\frac{42}{50}$	$\frac{24}{28}$	$\frac{75}{100}$
	577.6 ✓	571.1 ✓	570.2 ✓
	$\frac{04}{74}$	$\frac{62}{16}$	$\frac{75}{100}$
	579.3 ✓	576.0 ✓	570.8 ✓
	$\frac{40}{100}$	$\frac{73}{06}$	$\frac{122}{50}$
	582.1 ✓	577.6 ✓	570.8 ✓
	$\frac{12}{100}$	$\frac{52}{22}$	$\frac{122}{100}$
	583.0 ✓	578.6 ✓	573.5 ✓
	$\frac{92}{100}$	$\frac{74}{40}$	$\frac{98}{70}$
	579.5 ✓	576.1 ✓	571.9 ✓
	$\frac{1311}{581.988}$	$\frac{72}{52}$	$\frac{112}{100}$
		$\frac{82}{72}$	$\frac{102}{100}$
			$\frac{574.6}{573.2}$

Sta	+	π	—	Elev.
				581.988
	10.222			592.210
23+49.3		7.3		584.9
24+00		3.9		588.3
24+52.9 24+80 T.P. rock-		3.2		589.0
	2.386			589.824
	4.72			594.54
24+77.3 Jan. 28 '26		5.7		588.8 T.P. Sta. 24+80 589.824
	12.620			602.444
25+01.6		12.5		589.9
25+17.3		10.8		591.6
25+42.3	Two rods	14.5		587.9
25+55.1		13.6		588.8
25+67.3		8.1		594.3
25+92.3		5.7		596.7

Note - These elev. Taken from HZ 594.54

$\frac{34}{10^{\circ}}$ 588.8	$\frac{10^{\circ}}{7^{\circ}}$ 581.5	$\frac{15^{\circ}}{10^{\circ}}$ 577.4
$\frac{0^{\circ}}{10^{\circ}}$ 592.2	$\frac{7^{\circ}}{8^{\circ}}$ 584.9	$\frac{9^{\circ}}{10^{\circ}}$ 583.0 Two rods
$\frac{14}{10^{\circ}}$ 593.1	$\frac{34}{3^{\circ}}$ 591.1	$\frac{6^{\circ}}{10^{\circ}}$ 585.3
$\frac{0^{\circ}}{10^{\circ}}$ 593.8	$\frac{8^{\circ}}{5^{\circ}}$ 586.0	$\frac{11^{\circ}}{8^{\circ}}$ 582.6
$\frac{7^{\circ}}{10^{\circ}}$ 594.7	$\frac{13^{\circ}}{10^{\circ}}$ 589.4	$\frac{12^{\circ}}{10^{\circ}}$ 582.1
$\frac{6^{\circ}}{10^{\circ}}$ 596.4	$\frac{15^{\circ}}{2^{\circ}}$ 586.7	$\frac{18^{\circ}}{6^{\circ}}$ 583.8
$\frac{5^{\circ}}{10^{\circ}}$ 596.8	$\frac{17^{\circ}}{2^{\circ}}$ 591.2	$\frac{18^{\circ}}{10^{\circ}}$ 583.8
$\frac{5^{\circ}}{10^{\circ}}$ 597.4	$\frac{10^{\circ}}{2^{\circ}}$ 592.2	$\frac{16^{\circ}}{3^{\circ}}$ 585.6
$\frac{3^{\circ}}{10^{\circ}}$ 598.7	$\frac{7^{\circ}}{4^{\circ}}$ 594.6	$\frac{17^{\circ}}{10^{\circ}}$ 584.8 Two rods
$\frac{13}{10^{\circ}}$ 601.1	$\frac{16^{\circ}}{10^{\circ}}$ 586.4	$\frac{17^{\circ}}{10^{\circ}}$ 587.7
	$\frac{5^{\circ}}{10^{\circ}}$ 594.1	$\frac{14^{\circ}}{1^{\circ}}$ 588.3
	$\frac{8^{\circ}}{0.5}$ 594.9	$\frac{14^{\circ}}{10^{\circ}}$ 587.7
	$\frac{13^{\circ}}{2^{\circ}}$ 589.4	$\frac{13^{\circ}}{10^{\circ}}$ 589.0
	$\frac{7^{\circ}}{4^{\circ}}$ 594.9	$\frac{11^{\circ}}{9^{\circ}}$ 590.8
		$\frac{11^{\circ}}{10^{\circ}}$ 590.5

Sta.	+	$\pi$	-	Elev
		602.444		
26+17.3			4.6	597.8
26+36.3			5.5	596.9
26+66.3			6.2	596.2
27+00			8.2	594.2
27+43 Sta 27+43 T.P. Rock			13.0	589.4
			12.981	589.463
	.465	589.928		
27+77.5			3.6	586.3
				589.463
	3.00	592.46		
27+87.5			7.1	585.4
27+97.5			6.8	585.7
28+07.5			7.5	585.0
28+17.6 Sta 28+00 T.P. Rock			9.9	582.6
			12.945	576.983

Leach- $\pi$  Clear &  
McCarly-Rod. : Cool  
Reynolds-Rod  
Jan. 28, 1926  
Start -  
28+47.3

$\frac{1}{10}$	600.8	$\frac{8}{10}$	594.0
$\frac{2}{10}$	600.3	$\frac{9}{10}$	592.6
$\frac{3}{10}$	599.8	$\frac{11}{10}$	591.4
$\frac{4}{10}$	598.2	$\frac{10}{10}$	588.9
$\frac{5}{10}$	594.5	$\frac{10}{10}$	590.328
$\frac{7}{10}$	597.4	$\frac{9}{10}$	589.928
$\frac{5}{8}$	597.3	$\frac{9}{10}$	592.6
$\frac{1}{10}$	590.6	$\frac{7}{6}$	584.9
$\frac{16}{7}$	575.5	$\frac{17}{10}$	592.46
$\frac{22}{10}$	587.2	$\frac{8}{4}$	581.0
$\frac{17}{7}$	572.4	$\frac{17}{10}$	572.1
$\frac{24}{10}$	590.1	$\frac{11}{5}$	583.8
$\frac{8}{4}$	581.4	$\frac{9}{6}$	582.9
$\frac{3}{10}$	588.7	$\frac{18}{10}$	574.4
$\frac{11}{5}$	581.4	$\frac{12}{7}$	579.7
$\frac{5}{10}$	587.5	$\frac{19}{10}$	573.2
$\frac{11}{3}$	580.9	$\frac{12}{6}$	573.7
$\frac{12}{6}$	580.1	$\frac{19}{10}$	573.2
$\frac{18}{8}$	573.7		

Note: This elev. taken from H.I. 590.328

Note: These elevs. taken from H.I. 592.46

Sta.	+	⌈	-	Elev.
				576.983
	8.27	(585.25)		
28+47.3			4.9	580.3
28+70.3			9.5	575.7
28+72.3			15.9	569.3
28+97.3			17.7	567.5
29+01.3			18.1	567.1
29+09.3			19.0	566.2
				576.983
	0.850	577.833		
29+22.3			12.2	565.6
29+25.3			13.4	564.4
29+47.3			14.1	563.7
29+72.3			14.9	562.9
T.P. Rock.			11.893	565.940

Elev. T.P.  
Sta 29+00

$\frac{0.6}{100}$ 584.7	$\frac{8.2}{70}$ 577.2
$\frac{3.2}{100}$ 581.4	$\frac{14.9}{60}$ 570.4
$\frac{4.7}{100}$ 580.6	$\frac{15.8}{70}$ 569.5
$\frac{10.3}{100}$ 575.0	$\frac{16.4}{100}$ 568.9
$\frac{11.5}{100}$ 573.8	$\frac{16.6}{100}$ 568.7
$\frac{11.7}{100}$ 573.6	$\frac{17.2}{60}$ 568.1
$\frac{13.2}{50}$ 571.7	$\frac{18.6}{100}$ 566.7
$\frac{18.5}{100}$ 566.7	$\frac{18.9}{100}$ 566.4
$\frac{19.7}{100}$ 565.6	
$\frac{5.9}{100}$ 571.9	$\frac{12.2}{100}$ 565.1
$\frac{6.9}{100}$ 571.8	$\frac{13.8}{100}$ 564.0
$\frac{7.8}{100}$ 570.0	$\frac{14.3}{100}$ 563.5
$\frac{10.4}{42}$ 567.6	$\frac{15.8}{100}$ 562.0
$\frac{10.8}{82}$ 570.7	
$\frac{9.8}{42}$ 568.0	
$\frac{12.9}{26}$ 564.9	
$\frac{13.3}{20}$ 564.5	
Foot of Boulder	
$\frac{10.2}{70}$ 567.6	
$\frac{15.5}{14}$ 562.3	

Sta.	+	π	-	Elev.
	5.310	571.250	✓	565.940
B.M. #4			2.400	568.850
				565.940
	0.61	(566.55)	✓	
29+97.3			5.0	561.6
30+22.3			5.8	560.8
30+47.3			6.5	560.1
30+61.7			6.1	560.5
30+85.8			7.2	559.4
31+10.6			7.6	559.0
31+23.0			7.2	559.4
31+35.8			6.3	560.3
31+60.8			5.2	561.4

Leach π  
 McCarty - Rod  
 Reynolds - Rod  
 Jan 28, 1926  
 From  
 Sta. 19+77.5  
 to  
 Sta. 31+60.8  
 Recorded  
 Elev. T.P. Rod

Foot of Boulder

$\frac{2^0}{10^0}$  569.6 ✓  
 $\frac{3^0}{10^0}$  563.0 ✓  
 $\frac{4^0}{10^0}$  562.2 ✓  
 $\frac{5^0}{10^0}$  562.1 ✓  
 $\frac{6^0}{10^0}$  562.0 ✓  
 $\frac{7^0}{10^0}$  562.0 ✓  
 $\frac{8^0}{10^0}$  562.0 ✓  
 $\frac{9^0}{10^0}$  562.0 ✓  
 $\frac{10^0}{10^0}$  562.0 ✓  
 $\frac{11^0}{10^0}$  561.5 ✓  
 $\frac{12^0}{10^0}$  561.6 ✓  
 $\frac{13^0}{10^0}$  561.5 ✓  
 $\frac{14^0}{10^0}$  561.5 ✓  
 $\frac{15^0}{10^0}$  560.9 ✓  
 $\frac{16^0}{10^0}$  560.2 ✓  
 $\frac{17^0}{10^0}$  560.4 ✓  
 $\frac{18^0}{10^0}$  560.4 ✓  
 $\frac{19^0}{10^0}$  560.4 ✓  
 $\frac{20^0}{10^0}$  560.4 ✓  
 $\frac{21^0}{10^0}$  559.0 ✓  
 $\frac{22^0}{10^0}$  558.9 ✓  
 $\frac{23^0}{10^0}$  558.9 ✓  
 $\frac{24^0}{10^0}$  558.9 ✓  
 $\frac{25^0}{10^0}$  558.9 ✓  
 $\frac{26^0}{10^0}$  558.9 ✓  
 $\frac{27^0}{10^0}$  558.9 ✓  
 $\frac{28^0}{10^0}$  558.9 ✓  
 $\frac{29^0}{10^0}$  558.9 ✓  
 $\frac{30^0}{10^0}$  558.9 ✓  
 $\frac{31^0}{10^0}$  558.9 ✓  
 $\frac{32^0}{10^0}$  558.9 ✓  
 $\frac{33^0}{10^0}$  558.9 ✓  
 $\frac{34^0}{10^0}$  558.9 ✓  
 $\frac{35^0}{10^0}$  558.9 ✓  
 $\frac{36^0}{10^0}$  558.9 ✓  
 $\frac{37^0}{10^0}$  558.9 ✓  
 $\frac{38^0}{10^0}$  558.9 ✓  
 $\frac{39^0}{10^0}$  558.9 ✓  
 $\frac{40^0}{10^0}$  558.9 ✓  
 $\frac{41^0}{10^0}$  558.9 ✓  
 $\frac{42^0}{10^0}$  558.9 ✓  
 $\frac{43^0}{10^0}$  558.9 ✓  
 $\frac{44^0}{10^0}$  558.9 ✓  
 $\frac{45^0}{10^0}$  558.9 ✓  
 $\frac{46^0}{10^0}$  558.9 ✓  
 $\frac{47^0}{10^0}$  558.9 ✓  
 $\frac{48^0}{10^0}$  558.9 ✓  
 $\frac{49^0}{10^0}$  558.9 ✓  
 $\frac{50^0}{10^0}$  558.9 ✓  
 $\frac{51^0}{10^0}$  558.9 ✓  
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 $\frac{68^0}{10^0}$  558.9 ✓  
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 $\frac{71^0}{10^0}$  558.9 ✓  
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 $\frac{73^0}{10^0}$  558.9 ✓  
 $\frac{74^0}{10^0}$  558.9 ✓  
 $\frac{75^0}{10^0}$  558.9 ✓  
 $\frac{76^0}{10^0}$  558.9 ✓  
 $\frac{77^0}{10^0}$  558.9 ✓  
 $\frac{78^0}{10^0}$  558.9 ✓  
 $\frac{79^0}{10^0}$  558.9 ✓  
 $\frac{80^0}{10^0}$  558.9 ✓  
 $\frac{81^0}{10^0}$  558.9 ✓  
 $\frac{82^0}{10^0}$  558.9 ✓  
 $\frac{83^0}{10^0}$  558.9 ✓  
 $\frac{84^0}{10^0}$  558.9 ✓  
 $\frac{85^0}{10^0}$  558.9 ✓  
 $\frac{86^0}{10^0}$  558.9 ✓  
 $\frac{87^0}{10^0}$  558.9 ✓  
 $\frac{88^0}{10^0}$  558.9 ✓  
 $\frac{89^0}{10^0}$  558.9 ✓  
 $\frac{90^0}{10^0}$  558.9 ✓  
 $\frac{91^0}{10^0}$  558.9 ✓  
 $\frac{92^0}{10^0}$  558.9 ✓  
 $\frac{93^0}{10^0}$  558.9 ✓  
 $\frac{94^0}{10^0}$  558.9 ✓  
 $\frac{95^0}{10^0}$  558.9 ✓  
 $\frac{96^0}{10^0}$  558.9 ✓  
 $\frac{97^0}{10^0}$  558.9 ✓  
 $\frac{98^0}{10^0}$  558.9 ✓  
 $\frac{99^0}{10^0}$  558.9 ✓  
 $\frac{100^0}{10^0}$  558.9 ✓

	+	π	-	
				548.340
5.241	553.581	0.070		553.511
10.820	564.331	1.664		562.667
5.871	568.538	7.711		560.827
1.775	562.602	11.287		551.315
1.382	552.697	7.595		545.102

		0.332		547.366
4.479	551.845	6.723		545.122

RK  
85+95

545.421				
550.418				
		542392		8.6116

1.5,297				5365
		10.259		572.326

				548.340
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.274	548.614			
		10.730		537.884

5882 Jan 28  
2 PM  
McCarty T  
Leach-rods  
Reynolds

	+	∏	-	Elev
BM # 4				568.844
	0.140	568.984		<del>561.9</del> 560.9
31+85.8			10.71	
32+10.8			5.7	563.3
32+22.7			5.5	563.5
32+61.5			5.0	564.0
103				
32+71.8			5.9	563.1
32+76.5			8.3	560.7
32+86.5			8.4	560.6
33+11.5			8.4	560.6
TP			10.482	558.502
	5.88	564.38		
33+36.5			4.8	559.6
33+61.5			5.6	558.8
33+86.5			7.1	557.3

	+	∏	-	Elev
				564.4
				<del>46</del> 100
				565.4
				<del>36</del> 100
				565.9
				<del>31</del> 100
				565.7
				<del>33</del> 100
				563.7
				<del>53</del> 100
				562.6
				Fl of Boulder <del>64</del> 90
				561.5
				<del>75</del> 100
				564.1
				<del>49</del> 100
				563.4
				<del>10</del> 100
				562.0
				<del>24</del> 100
				559.9
				<del>45</del> 100
				561.7
				<del>73</del> 100
				559.2
				<del>98</del> 100
				558.4
				<del>106</del> 100
				560.7
				<del>83</del> 100
				559.4
				<del>96</del> 100
				562.1
				<del>62</del> 100
				560.9
				<del>81</del> 100
				559.1
				<del>92</del> 100
				562.8
				<del>62</del> 100
				560.7
				<del>83</del> 100
				560.2
				<del>89</del> 100
				560.8
				<del>82</del> 100
				559.6
				<del>48</del> 100
				558.2
				<del>108</del> 100
				562.0
				<del>24</del> 100
				557.4
				<del>70</del> 100
				555.0
				<del>94</del> 100
				555.6
				<del>88</del> 100
				554.4
				<del>100</del> 100



+	∇	-	Elev
	564.38		558.502
34+11.5 Jan 29, 26 T.P.	1.720	8.4	556.0 ✓
34+36.5		5.1	555.1 ✓
34+52.3		5.4	554.8 ✓
35+45.7 23		7.2	553.0 ✓
35+48.0 14.7		7.5	552.7 ✓
35+60.4		8.0	552.2 ✓
35+85.4		8.2	552.0 ✓
36+10.4		8.5	551.7 ✓
36+35.4		8.9	551.3 ✓
36+60.4		8.1	552.1 ✓
36+85.4		5.3	554.9 ✓
36+82.4 37		5.5	554.7 ✓
36+86.1		4.2	556.0 ✓

€	€	€
558.1 ✓ $\frac{57}{100}$		554.0 ✓ $\frac{104}{100}$
557.8 ✓ $\frac{24}{100}$		553.5 ✓ $\frac{67}{100}$
557.0 ✓ $\frac{32}{100}$		553.0 ✓ $\frac{72}{100}$
554.9 ✓ $\frac{53}{100}$	552.5 ✓ $\frac{72}{100}$	551.4 ✓ $\frac{80}{100}$
554.8 ✓ $\frac{54}{100}$	554.3 ✓ $\frac{59}{72}$	551.3 ✓ $\frac{61}{100}$
554.7 ✓ $\frac{55}{100}$	553.0 ✓ $\frac{72}{60}$	551.2 ✓ $\frac{89}{100}$
554.2 ✓ $\frac{60}{100}$	552.5 ✓ $\frac{72}{30}$	551.1 ✓ $\frac{66}{100}$
553.8 ✓ $\frac{64}{100}$	554.3 ✓ $\frac{59}{72}$	551.0 ✓ $\frac{89}{100}$
554.2 ✓ $\frac{60}{100}$	552.5 ✓ $\frac{72}{32}$	550.9 ✓ $\frac{93}{100}$
553.9 ✓ $\frac{63}{100}$	551.9 ✓ $\frac{83}{50}$	550.8 ✓ $\frac{94}{100}$
558.2 ✓ $\frac{20}{100}$	551.9 ✓ $\frac{83}{50}$	550.5 ✓ $\frac{92}{100}$
557.6 ✓ $\frac{20}{100}$	551.9 ✓ $\frac{83}{50}$	550.0 ✓ $\frac{102}{100}$
558.5 ✓ $\frac{17}{100}$	551.9 ✓ $\frac{83}{50}$	550.3 ✓ $\frac{99}{100}$
	551.5 ✓ $\frac{87}{33}$	550.3 ✓ $\frac{99}{100}$
	550.4 ✓ $\frac{98}{54}$	550.3 ✓ $\frac{99}{100}$
	554.5 ✓ $\frac{46}{08}$	550.3 ✓ $\frac{99}{100}$
	551.8 ✓ $\frac{84}{48}$	550.3 ✓ $\frac{99}{100}$
	554.0 ✓ $\frac{62}{20}$	550.3 ✓ $\frac{99}{100}$
	551.2 ✓ $\frac{70}{52}$	550.3 ✓ $\frac{99}{100}$
	554.6 ✓ $\frac{36}{28}$	550.3 ✓ $\frac{99}{100}$
	553.9 ✓ $\frac{63}{62}$	550.3 ✓ $\frac{99}{100}$

+	π	-	Elev
	560.222		
36+90.9		4.2	556.0 ✓
36+93.9		4.1	556.1 ✓
TP		4.374	555.848 ✓
	5.35	(561.20)	
36+97.7		7.0	554.2 ✓
37+05.6		8.6	552.6 ✓
37+30.0		8.0	553.2 ✓
37+34.8		5.0	556.2 ✓
69			
37+41.2		6.1	555.1 ✓
37+51.2		9.6	551.6 ✓
37+55.6		10.6	550.6 ✓
37+61.2		7.7	553.5 ✓
37+71.2		7.7	553.5 ✓
37+75.6		8.1	553.1 ✓

Jan 29  
McCarty π  
Loach-rod  
Reynolds."

Clear and  
warm

558.8

557.8

14  
100

554.6 ✓

26  
100

559.9 ✓

23  
100

559.1 ✓

21  
100

559.3 ✓

19  
100

550.6 ✓

106  
100

558.7

25  
100

Ft of Boulder

560.3

160.3

98  
100

558.2 ✓

30  
100

558.3 ✓

29  
100

557.2 ✓

40  
100

556.6 ✓

46  
100

€

553.A ✓

68  
88

Ft of Boulder

552.1 ✓

92  
100

551.5 ✓

92  
30

551.1 ✓

101  
100

550.2 ✓

110  
100

549.7 ✓

120  
100

558.1

31  
72

Ft of Boulder

553.5

72  
54

548.9

123  
100

555.7 ✓

55  
100

548.4 ✓

128  
100

556.8 ✓

44  
52

548.6 ✓

126  
100

556.4 ✓

48  
28

548.7 ✓

125  
100

552.4 ✓

88  
42

549.0 ✓

122  
100

552.3 ✓

89  
32

548.1 ✓

132  
100

Sta	+	π	-	Elev.	✓
		(561.20)		555.898	✓
37+78.5			9.8	551.4	✓
37+81.2			9.5	551.7	✓
37+82.2			7.8	553.4	✓
37+85.9			7.6	553.6	✓
37+87.3			9.8	551.4	✓
37+91.1			10.0	551.2	✓
37+95.4			8.9	552.3	✓
38+00			12.7	548.5	✓
38+22.1			12.0	549.2	✓
TP	4.901	560.749			
TP			1.726	559.023	RK 38+85
	11.05	(570.07)			
38+47.1			17.0	553.1	✓
38+72.1			16.9	553.2	✓

€	€	€
556.5 ✓ $\frac{47}{100}$	553.7 ✓ $\frac{75}{24}$	548.2 ✓ $\frac{130}{100}$
551.9 ✓ $\frac{93}{72}$	556.8 ✓ $\frac{44}{100}$	548.2 ✓ $\frac{130}{100}$
553.8 ✓ $\frac{74}{30}$	551.1 ✓ $\frac{41}{100}$	548.2 ✓ $\frac{130}{100}$
550.6 ✓ $\frac{106}{23}$	556.9 ✓ $\frac{43}{100}$	548.1 ✓ $\frac{131}{100}$
551.4 ✓ $\frac{98}{08}$	556.9 ✓ $\frac{43}{100}$	548.1 ✓ $\frac{131}{100}$
554.5 ✓ $\frac{62}{08}$	556.3 ✓ $\frac{49}{100}$	547.8 ✓ $\frac{134}{100}$ Two rods
553.0 ✓ $\frac{82}{32}$	556.1 ✓ $\frac{51}{100}$	547.7 ✓ $\frac{135}{100}$
548.5 ✓ $\frac{127}{22}$	556.1 ✓ $\frac{51}{100}$	547.6 ✓ $\frac{136}{100}$
551.5 ✓ $\frac{27}{67}$	555A ✓ $\frac{58}{52}$	547.1 ✓ $\frac{141}{100}$
548.2 ✓ $\frac{130}{20}$	554A ✓ $\frac{68}{40}$	
	550A ✓ $\frac{108}{20}$	
	548.2 ✓ $\frac{130}{20}$	
	Ft. of Boulder	
559A ✓ $\frac{107}{100}$		
560.2 ✓ $\frac{10}{100}$		
554.7 ✓ $\frac{65}{30}$		
547.9 ✓ $\frac{51}{76}$		
547.4 ✓ $\frac{56}{100}$		
548.2 ✓ $\frac{48}{100}$		

559.023

A 570.07

38+85.1	13.8	556.3 ✓
39+10.8	8.3	561.8 ✓
39+35.8	3.7	566.4 ✓
39+60.8	9.0	561.1 ✓
39+85.8	9.9	560.2 ✓
40+00.2	9.9	560.2 ✓
40+14.7	13.9	556.2 ✓
40+16.7	18.3	551.8 ✓
40+25.8	13.6	556.5 ✓
40+29.8	20.8	549.3 ✓
40+70.5	D 7.1	545.9 ✓
	18.8	
40+80.5	18.8	551.3 ✓

Ft of Boulder

558.0 ✓

A  $\frac{121}{22}$

568.3 ✓

A  $\frac{18}{100}$

574.6 ✓

C  $\frac{15}{100}$

572.7 ✓

C  $\frac{34}{100}$

567.1 ✓

A  $\frac{30}{100}$

567.4 ✓

A  $\frac{27}{100}$

565.6 ✓

A  $\frac{45}{100}$

564.4 ✓

A  $\frac{52}{100}$

564.6 ✓

A  $\frac{55}{100}$

568.0 ✓

A  $\frac{21}{100}$

555.3 ✓

A  $\frac{148}{100}$

A  $\frac{107}{100}$

C

5505 ✓

D  $\frac{25}{85}$

566.1 ✓

A  $\frac{40}{52}$

547.8 ✓

D  $\frac{52}{80}$

559.7 ✓

A  $\frac{104}{70}$

548.9 ✓

D  $\frac{41}{32}$

547.4 ✓

D  $\frac{54}{72}$

547.2 ✓

D  $\frac{58}{75}$

555.8 ✓

A  $\frac{143}{15}$

551.0 ✓

D  $\frac{20}{20}$

549.7 ✓

D  $\frac{33}{43}$

547.1 ✓

D  $\frac{59}{45}$

546.6 ✓

D  $\frac{64}{100}$

555.2 ✓

A  $\frac{149}{10}$

548.5 R ✓

D  $\frac{50}{14}$

546.9 ✓

D  $\frac{62}{44}$

546.4 ✓

D  $\frac{66}{100}$

553.2 ✓

A  $\frac{179}{50}$

545.2 ✓

D  $\frac{78}{100}$

546.2 ✓

D  $\frac{68}{24}$

545.2 ✓

D  $\frac{88}{100}$

Sta	+	π	-	Elev.
				559.023
40+96.5	SR	A 570.07	16.0	554.1 ✓
41+25.7	SR		6.3	563.8 ✓
41+43.5	SR		13.1	557.0 ✓
41+55.0	SR		10.4	559.7 ✓
TP	2.13	B 561.15		
TP	10.93	569.95		
			5.83	564.12 ✓
	11.98	C 576.10		
TP	8.242	567.265		
			12.642	554.623 ✓
TP	0.524	555.147		Recorded
BM# 5			11.465	543.682 ✓
TP	9.35	D 553.03		
TP	6.52	E 550.20		

E

561.7 ✓	544.5 ✓	544.5 ✓
A $\frac{84}{100}$	$\frac{85}{85}$	D $\frac{85}{100}$
570.0 ✓		554.9 ✓
A $\frac{0.1}{100}$		A $\frac{152}{100}$
561.5 ✓	564.3 ✓	546.2 ✓
A $\frac{26}{100}$	A $\frac{58}{76}$	E $\frac{40}{100}$
569.7 ✓	569.7 ✓	545.2 ✓
A $\frac{0.7}{90}$		E $\frac{52}{100}$

Sta.	+	$\bar{\pi}$	-	Elev.
B.M. # 5				543.678
Sta. 43+47.8	10.201	553.879	A	
T.P. Rock		.210		553.669
41+78.6	S.R.	"B"	1.7	571.6
42+00		A	10.3	543.6
42+09.4		A	5.6	548.3
42+10.		A	8.7	545.2
42+27		A	1.5	552.4
42+28		A	5.8	548.1
42+39.4		"C"	11.5	555.7
42+43.4		"C"	12.6	554.6
+ 47.4		"C"	11.5	555.7
42+44.4		"C"	16.0	551.2
42+55.2		A		
42+68.4		A	0.7	553.2
+ 83.2		2.8 A		551.1

Leach -  $\pi$   
McCarthy - Rod  
Reynolds.  
Jan. 29 '26

Cool  
&  
cloudy

£

D	$\frac{6.2}{10.0}$	570.7	A	$\frac{11.0}{10.0}$	542.9
C	$\frac{14.4}{10.0}$	552.8	A	$\frac{12.4}{10.0}$	541.5
C	$\frac{9.1}{10.0}$	557.8	A	$\frac{12.3}{10.0}$	541.6
C	$\frac{12.4}{10.0}$	554.8	A	$\frac{12.3}{10.0}$	541.6
C	$\frac{7.0}{10.0}$	560.2	A	$\frac{12.3}{10.0}$	541.6
C	$\frac{9.6}{10.0}$	557.6	A	$\frac{12.8}{10.0}$	541.1
C	$\frac{2.1}{10.0}$	565.1	A	$\frac{13.0}{10.0}$	540.9
C	$\frac{1.3}{10.0}$	565.9	A	$\frac{11.0}{10.0}$	542.0
C	$\frac{3.2}{10.0}$	564.0	A	$\frac{11.3}{10.0}$	542.6
C	$\frac{6.4}{10.0}$	560.8	"C"	$\frac{20.6}{10.0}$	546.6
"C"	$\frac{5.3}{10.0}$	561.9	"C"	$\frac{19.5}{10.0}$	547.7
"C"	$\frac{3.6}{10.0}$	563.6	A	$\frac{8.5}{10.0}$	545.3
"C"	$\frac{6.9}{3.0}$	560.3	A	$\frac{12.4}{10.0}$	541.8
"C"	$\frac{6.4}{6.8}$	547.5			

Sta.	+	π	-	Elev.
Jan. 30 '26				553.669
T.P.	12.51	566.18 ✓		
	8.92	"B" 573.32 ✓	1.78	564.40 ✓
Rocky pt. above T.P. Sta. 42+43.4		"C" 567.21 ✓	6.86	566.46 ✓
	.75			
42+93.4		"C" 13.0		554.2 ✓
+99.4		"C" 17.6		549.6 ✓
43+09		"C" 17.4		552.8 ✓
+33.8		"C" 18.8		548.4 ✓
+47.8 Top of large Boulder		"C" 10.3		556.9 ✓
	10.76	577.22 ✓		566.46 <small>El. T.P. near Sta. 42+43.4</small>
T.P.	8.17	"D" 584.90 ✓	.49	576.73 ✓
	1.21	E 554.88 ✓		553.669 <small>El. T.P. near Sta. 43+47.8</small>
Feb. 1, 1926				553.669
Sta. 46+50	5.283	558.952 ✓		
T.P. Rock			10.207	548.745 ✓
			10.193	

Leach T. McCarty-Rod  
Reynolds "  
Jan. 30 '26

Cool  
&  
cloudy -

$\frac{17}{10} = 565.5$  ✓  
 $\frac{5}{10} = 561.6$  ✓  
 $\frac{5}{10} = 562.2$  ✓  
 $\frac{9}{10} = 558.2$  ✓  
 $\frac{6}{10} = 560.3$  ✓  
 $\frac{8}{7} = 559.2$  ✓  
 $\frac{14}{7} = 553.2$  ✓  
 $\frac{13}{7} = 553.3$  ✓  
 $\frac{13}{10} = 541.1$  ✓  
 $\frac{12}{10} = 542.0$  ✓  
 $\frac{20}{10} = 547.2$  ✓  
 $\frac{13}{10} = 541.2$  ✓  
 $\frac{14}{10} = 552.7$  ✓  
 Top of rock

Leach-T Cool  
 McCarty-Rod 4  
 Reynolds cloudy

Sta.	+	∧	-	Elev.
		558.952		
43+54.8			8.2	<del>550.8</del> 551.0 ✓
+72.8			8.0	<del>551.0</del> 552.0 ✓
+97.8			6.7	<del>552.3</del> 553.3 ✓
44+22.8			9.6	<del>549.4</del> 550.4 ✓
+47.8			10.9	<del>548.1</del> 549.1 ✓
+75.5			12.2	<del>546.8</del> 547.8 ✓
45+00			13.8	<del>545.2</del> 546.2 ✓
				T.P. 553.669 Sta. 43+47.8
	6.59	F 560.26 ✓		
				T.P. 548.745 Sta. 46+50
	7.01	G 555.75 ✓		
46+00			11.5	<del>544.3</del> ✓
46+52.8			13.8	<del>542.0</del> ✓
				46+50 548.745
Sta 48+30 T.P. Rock	1.060	549.805 ✓	12.880	<del>536.925</del> ✓

Foot of Blk.

F

G

G

$\frac{6.7}{4} \begin{matrix} 552.3 \\ 553.3 \end{matrix}$  ✓  
 $\frac{12.3}{6.2} \begin{matrix} 546.7 \\ 547.7 \end{matrix}$  ✓  
 $\frac{15.4}{10.2} \begin{matrix} 543.6 \\ 544.6 \end{matrix}$  ✓  
 $\frac{2.1}{10.2} \begin{matrix} 558.2 \\ 559.2 \end{matrix}$  ✓  
 $\frac{0.8}{10.2} \begin{matrix} 558.2 \\ 559.2 \end{matrix}$  ✓  
 $\frac{3.5}{10.2} \begin{matrix} 555.5 \\ 556.5 \end{matrix}$  ✓  
 $\frac{4.3}{10.2} \begin{matrix} 552.7 \\ 553.7 \end{matrix}$  ✓  
 $\frac{6.3}{10.2} \begin{matrix} 552.7 \\ 553.7 \end{matrix}$  ✓  
 $\frac{8.0}{10.2} \begin{matrix} 551.0 \\ 552.0 \end{matrix}$  ✓  
 $\frac{7.1}{10.2} \begin{matrix} 548.7 \\ 549.7 \end{matrix}$  ✓  
 $\frac{9.8}{10.2} \begin{matrix} 546.0 \\ 547.0 \end{matrix}$  ✓  
 $\frac{16.3}{10.2} \begin{matrix} 539.6 \\ 540.6 \end{matrix}$  ✓  
 $\frac{18.1}{10.2} \begin{matrix} 537.7 \\ 538.7 \end{matrix}$  ✓

Two rods

$\frac{15.4}{10.2} \begin{matrix} 544.6 \\ 545.6 \end{matrix}$  ✓  
 $\frac{14.5}{10.2} \begin{matrix} 544.5 \\ 545.5 \end{matrix}$  ✓  
 $\frac{12.3}{10.2} \begin{matrix} 546.8 \\ 547.8 \end{matrix}$  ✓  
 $\frac{15.1}{10.2} \begin{matrix} 543.9 \\ 544.9 \end{matrix}$  ✓  
 $\frac{17.3}{10.2} \begin{matrix} 541.7 \\ 542.7 \end{matrix}$  ✓  
 $\frac{18.4}{10.2} \begin{matrix} 540.6 \\ 541.6 \end{matrix}$  ✓  
 $\frac{18.0}{10.2} \begin{matrix} 540.4 \\ 541.4 \end{matrix}$  ✓



Sta.	+	$\pi$	-	Elev.	Le
		549.805			
46+72.8			10.8	539.0	
+82.8			10.6	539.2	
+92.1			11.2	538.6	
47+00			11.3	538.5	
+27			13.2	536.6	
+49		H	13.4	536.4	T.P.
	6.04	(542.96)		536.925	48+30
+74			7.0	536.0	
+99			6.4	536.6	
48+24			6.3	536.7	
+28.3			6.5	536.5	
+41			8.5	534.5	
764			7.3	535.7	

$\frac{6^0}{10^0}$ 543.8	$\frac{13^0}{10^0}$ 536.2
$\frac{6^5}{10^0}$ 543.3	$\frac{14^0}{10^0}$ 535.8
$\frac{6^8}{10^0}$ 543.0	$\frac{14^3}{10^0}$ 535.6
$\frac{6^9}{10^0}$ 542.9	$\frac{13^2}{10^0}$ 535.9
$\frac{7^9}{10^0}$ 541.9	$\frac{13^2}{10^0}$ 536.3
$\frac{4^2}{2^0}$ 538.6	$\frac{13^5}{10^0}$ 536.3
$\frac{13^0}{10^0}$ 536.8	$\frac{6^2}{10^0}$ 543.7
H $\frac{3^2}{10^0}$ 539.8	H $\frac{4^2}{10^0}$ 536.7
$\frac{13^1}{4^2}$ 536.4	H $\frac{6^2}{9^0}$ 536.3
H $\frac{13^3}{10^0}$ 541.7	$\frac{6^2}{10^0}$ 543.7
H $\frac{6^5}{2^2}$ 536.4	$\frac{7^3}{8^0}$ 535.7
H $\frac{7^3}{8^0}$ 535.7	H $\frac{6^9}{10^0}$ 536.1
H $\frac{3^5}{10^0}$ 539.5	H $\frac{7^2}{5^5}$ 535.3
H $\frac{4^3}{10^0}$ 538.7	H $\frac{7^6}{10^0}$ 535.4
H $\frac{4^5}{10^0}$ 538.5	H $\frac{8^3}{3^3}$ 534.7
H $\frac{5^2}{10^0}$ 537.8	H $\frac{8^5}{10^0}$ 534.5
H $\frac{5^5}{9^0}$ 537.5	H $\frac{8^0}{2^4}$ 535.0
H $\frac{3^7}{10^0}$ 539.3	H $\frac{8^2}{10^0}$ 534.3
H $\frac{8^5}{3^0}$ 544.5	H $\frac{8^7}{10^0}$ 544.3
H $\frac{9^0}{10^0}$ 534.0	H $\frac{8^2}{10^0}$ 544.3
H $\frac{9^0}{10^0}$ 534.0	H $\frac{8^2}{10^0}$ 544.3

Sta	+	-	Elev.	Leach. T McCarly Rod Reynolds T.P. 48+30
	6.262	543.187	536.925	
51+40 T.P. Rock			3.479	539.708
49+00			4.5	538.7
+35.8			4.3	538.9
+45.8			4.5	538.7
+55.8			4.6	538.6
+65.8			5.7	537.5
+74.1			6.1	537.1
+95			5.3	537.9
Feb. 2 '26				T.P. 536.925 Sta. 48+30
	7.94	544.86		
				T.P. 539.708 Sta. 51+40
	2.85	542.56		
50+00			6.8	535.8
+12			5.6	537.0

Cool  
&  
Cloudy

I	$\frac{28}{100}$	542.1
	$\frac{02}{100}$	542.5
	$\frac{29}{100}$	540.3
	$\frac{39}{100}$	539.3
	$\frac{49}{100}$	538.3
	$\frac{42}{100}$	538.5
J	$\frac{42}{100}$	538.4
	$\frac{51}{70}$	537.5
	$\frac{72}{80}$	535.7
	$\frac{69}{86}$	536.3
	$\frac{86}{10}$	534.6
	$\frac{53}{48}$	537.9
	$\frac{52}{13}$	537.3
	$\frac{66}{32}$	536.6
	$\frac{75}{20}$	535.7
	$\frac{98}{100}$	533.4
	$\frac{72}{80}$	535.7
	$\frac{81}{100}$	534.8
	$\frac{86}{10}$	534.6
	$\frac{87}{100}$	534.5
	$\frac{79}{30}$	535.3
	$\frac{99}{100}$	533.3
	$\frac{94}{72}$	533.8
	$\frac{92}{100}$	532.5
	$\frac{77}{100}$	535.5
J	$\frac{42}{100}$	538.3
	$\frac{73}{60}$	535.3
	$\frac{69}{100}$	535.7
	$\frac{59}{50}$	536.7
	$\frac{78}{100}$	534.8

Sta.	+	$\bar{\pi}$ J (542.56)	-	Elev.
50+50			5.1	537.5 ✓
51+00			2.6	540.0 ✓
+42.9			3.3	539.3 ✓
+50.2			4.8	537.8 ✓
52+00			5.7	536.9 ✓
+69.9			6.0	536.6 ✓
	1.22			T.P. 539.708 51+40
	1.221	540.929 ✓		
B.M. # 6			1.282	539.647 539.618 ✓ Recorded.

$\frac{37}{100}$	538.9 ✓	$\frac{37}{100}$	538.9 ✓	$\frac{54}{80}$	537.2 ✓	$\frac{64}{100}$	536.2 ✓
$\frac{20}{100}$	540.6 ✓	$\frac{49}{24}$	537.7 ✓	$\frac{38}{100}$	538.8 ✓	$\frac{52}{100}$	537.4 ✓
$\frac{21}{100}$	540.2 ✓	$\frac{38}{100}$	538.8 ✓	$\frac{56}{100}$	537.0 ✓	$\frac{56}{100}$	537.0 ✓
$\frac{56}{100}$	537.0 ✓	$\frac{63}{100}$	536.3 ✓	$\frac{62}{100}$	536.4 ✓		

Feb. 2  
 9:15 AM  
 McCarty  
 Leach-rod  
 Reynolds

Sta.	+	π	-	Elev.
BM# 6				539.618
	0.966	540.584		
	<del>0.967</del>	<del>540.585</del>		
52+94.9			4.3	536.3
53+19.9			4.3	536.3
53+44.9			4.5	536.1
53+65.9			5.7	534.9
53+82.9			5.4	535.2
54+00			4.6	536.0
55+00			3.3	537.3
TP	3.794	544.317	0.061	540.523
55+12			6.8	537.5
55+25.2			4.2	540.1
55+42.0			7.0	537.3
55+69.4			3.6	540.7

536.3		536.1
$\frac{43}{100}$		$\frac{45}{100}$
535.7	536.3	536.0
$\frac{49}{100}$	$\frac{43}{60}$	$\frac{46}{100}$
535.6		536.1
$\frac{50}{100}$		$\frac{45}{100}$
535.8		535.9
$\frac{48}{100}$	536.1	$\frac{47}{100}$
	$\frac{45}{70}$	536.8
535.7	536.1	$\frac{48}{100}$
$\frac{49}{100}$	$\frac{45}{70}$	$\frac{48}{100}$
537.2		535.9
$\frac{34}{100}$	536.4	$\frac{47}{100}$
	$\frac{42}{80}$	535.6
541.3		$\frac{51}{100}$
$\frac{20}{100}$	535.6	
	$\frac{50}{40}$	
542.0		536.8
$\frac{23}{100}$	539.6	$\frac{75}{100}$
	$\frac{47}{55}$	
541.1		537.4
$\frac{32}{100}$		$\frac{69}{87}$
537.6		539.0
$\frac{67}{100}$		$\frac{53}{86}$
541.0		538.0
$\frac{33}{100}$		$\frac{63}{70}$
		537.3
		$\frac{70}{100}$
		540.0
		$\frac{43}{100}$

	544.317		
55+94.4		7.6	536.7 ✓
56+19.4		9.4	534.9 ✓
56+44.4		9.4	534.9 ✓
56+69.4		9.6	534.7 ✓
56+94.4		9.4	534.9 ✓
TP	3.874	539.532 ✓	535.658 ✓
		535.738	531.864
57+19.4		8.659	57+15 ✓
		4.7	534.8 ✓
57+34.7		4.4	535.1 ✓
58+00		5.0	534.5 ✓
58+25		5.2	534.3 ✓
58+31		3.6	535.9 ✓
58+58		3.7	535.8 ✓
59+00		5.6	533.9 ✓
59+42		6.4	533.1 ✓

538.7 ✓	537.1 ✓	€	536.1 ✓
$\frac{58}{100}$	$\frac{72}{75}$		$\frac{82}{100}$
536.7 ✓		534.9 ✓	534.8 ✓
$\frac{76}{100}$		$\frac{94}{52}$	$\frac{95}{100}$
535.3 ✓			534.7 ✓
$\frac{90}{100}$			$\frac{96}{100}$
535.0 ✓			534.4 ✓
$\frac{93}{100}$			$\frac{99}{100}$
535.1 ✓		534.6 ✓	533.9 ✓
$\frac{44}{100}$		$\frac{92}{35}$	$\frac{104}{100}$
535.1 ✓		533.6 ✓	533.4 ✓
$\frac{44}{100}$		$\frac{52}{50}$	$\frac{61}{100}$
535.2 ✓		534.0 ✓	533.2 ✓
$\frac{43}{100}$		$\frac{55}{51}$	$\frac{63}{100}$
536.2 ✓		533.8 ✓	533.5 ✓
$\frac{33}{100}$		$\frac{62}{70}$	$\frac{60}{100}$
535.7 ✓	535.9 ✓		534.2 ✓
$\frac{38}{100}$	$\frac{36}{65}$		$\frac{53}{100}$
535A ✓			532.1 ✓
$\frac{41}{100}$			$\frac{68}{100}$
	538.1 ✓		532.9 ✓
	$\frac{14}{65}$		$\frac{66}{100}$
	Ft. of Boulder		531.7 ✓
535.9 ✓	535.1 ✓		$\frac{78}{100}$
$\frac{36}{100}$	$\frac{44}{80}$		
		532.3 ✓	530.6 ✓
		$\frac{72}{80}$	$\frac{90}{100}$
537.3 ✓			
$\frac{22}{100}$			

Sta	+	$\pi$	-	Elev
		539.532		
		535.738		
TP	10.838	546.668	3.702	535.830
		542.874		532.036
59+65			14.0	532.7
59+70			16.6	530.1
59+75			14.1	532.6
59+91			12.4	534.3
59+92.5			9.5	537.2
60+00			7.0	539.7
60+16.9			5.7	541.0
60+23.7			3.0	543.7
60+41.9			1.9	544.8
60+66.9			4.0	542.7
60+91.9			4.1	542.6
BM#7				Recorded
		549.29	0.634	546.034
	3.26	549.27		546.027

Two rods

533.9

$$\frac{120}{100}$$

532.3

$$\frac{144}{100}$$

534.2

$$\frac{125}{100}$$

541.3

$$\frac{54}{100}$$

543.2

$$\frac{35}{100}$$

545.4

$$\frac{13}{100}$$

546.0

$$\frac{33}{100}$$

546.2

$$\frac{05}{100}$$

546.7

$$\frac{0.0}{100}$$

546.0

$$\frac{0.7}{100}$$

544.1

$$\frac{26}{100}$$

C

531.4

$$\frac{153}{100}$$

529.8

$$\frac{169}{100}$$

530.2

$$\frac{165}{100}$$

529.7

$$\frac{170}{100}$$

529.7

$$\frac{170}{100}$$

537.0

$$\frac{97}{100}$$

532.0

$$\frac{142}{100}$$

530.5

$$\frac{162}{100}$$

533.5

$$\frac{132}{100}$$

532.4

$$\frac{143}{100}$$

531.3

$$\frac{154}{100}$$

536.8

$$\frac{99}{100}$$

534.6

$$\frac{121}{100}$$

532.2

$$\frac{145}{100}$$

537.9

$$\frac{80}{100}$$

533.5

$$\frac{132}{100}$$

535.0

$$\frac{112}{100}$$

541.0

$$\frac{57}{100}$$

539.3

$$\frac{74}{100}$$

539.4

$$\frac{73}{100}$$

541.6

$$\frac{51}{100}$$

539.8

$$\frac{69}{100}$$

Sta.	+	∇	-	Elev.
B.M. #7			1	546.027
Sta 63+00 T.P. Rock	0.612	546.639	✓	
		11.639		535.000 ✓
61+11.3		5.7		540.9 ✓
+15.6		6.2		540.4 ✓
+25.6		7.4		539.2 ✓
+35.6		7.9		538.7 ✓
+45.6		8.9		537.7 ✓
+55.1		9.9		536.7 ✓
				535.000 T.P. Sta. 63+00
	7.24	A (542.24)	✓	
62+00		8.5		533.7 ✓
+45		9.3		532.9 ✓
+76		11.2		531.0 ✓
63+00		12.0		530.2 ✓

$\frac{4.5}{10.0}$	542.1 ✓	$\frac{7.8}{10.0}$	538.8 ✓
$\frac{4.9}{10.0}$	541.7 ✓	$\frac{8.1}{10.0}$	538.5 ✓
$\frac{6.0}{10.0}$	540.6 ✓	$\frac{9.1}{10.0}$	537.5 ✓
$\frac{6.6}{10.0}$	540.0 ✓	$\frac{10.4}{10.0}$	536.2 ✓
$\frac{7.5}{10.0}$	539.1 ✓	$\frac{11.2}{9.0}$	535.4 ✓
$\frac{7.9}{10.0}$	538.7 ✓	$\frac{14.8}{10.0}$	531.8 ✓
$\frac{6.4}{10.0}$	535.8 ✓	$\frac{11.2}{10.0}$	534.7 ✓
$\frac{6.7}{10.0}$	535.5 ✓	$\frac{9.8}{6.4}$	532.4 ✓
$\frac{9.5}{10.0}$	532.7 ✓	$\frac{11.2}{10.0}$	530.3 ✓
$\frac{11.5}{10.0}$	530.7 ✓	$\frac{11.2}{10.0}$	531.0 ✓
$\frac{10.0}{2.0}$	532.1 ✓	$\frac{11.2}{9.0}$	530.5 ✓
$\frac{12.0}{10.0}$	530.0 ✓	$\frac{12.0}{10.0}$	529.9 ✓

Sta.	+	π	-	Elev
				535.000 T.P. Sta. 63+00
63+50		542.24	11.0	531.2 ✓
64+00			10.5	531.7 ✓
				535.000
Sta 66+40 T.P. Rock	5.155	540.155 ✓	9.350	530.805 ✓
+27			7.2	533.0 ✓
+37			9.5	530.7 ✓
+70			5.5	534.7 ✓
65+00			4.4	535.8 ✓
+49.3			2.5	537.7 ✓
		540.155		
T.P.		B	.76	539.40 ✓
	10.39	549.79 ✓		
+74.3			14.1	535.7 ✓
+99.3			14.9	534.9 ✓

$\frac{94}{102}$ 532.8 ✓	$\frac{98}{51}$ 532.4 ✓	$\frac{114}{102}$ 531.1 ✓
$\frac{98}{102}$ 532.4 ✓		$\frac{116}{102}$ 530.6 ✓
$\frac{62}{102}$ 533.4 ✓	$\frac{95}{72}$ 530.7 ✓	$\frac{93}{102}$ 530.9 ✓
$\frac{84}{102}$ 531.6 ✓		530.6 ✓
$\frac{31}{102}$ 537.1 ✓	$\frac{84}{72}$ 531.8 ✓	$\frac{96}{102}$ 531.5 ✓
$\frac{12}{102}$ 532.3 ✓	$\frac{82}{102}$ 531.7 ✓	$\frac{82}{102}$ 531.5 ✓
$\frac{82}{102}$ 531.4 ✓	$\frac{61}{52}$ 534.1 ✓	$\frac{85}{85}$ 531.7 ✓
		$\frac{82}{102}$ 531.5 ✓
		$\frac{72}{102}$ 532.3 ✓
$\frac{54}{102}$ 544.9 ✓	$\frac{78}{102}$ 542.0 ✓	$\frac{112}{102}$ 538.1 ✓
$\frac{42}{102}$ 545.0 ✓	$\frac{102}{82}$ 539.8 ✓	$\frac{185}{102}$ 531.3 ✓
		$\frac{185}{102}$ 531.2 ✓
		530.9 ✓
		530.9 ✓
		531.9 ✓



Sta.	+	T	-	Elev.
				Leach-T McCarty Rod Reynolds T.P. Sta. 66+40
12.73		(543.53)		530.805
66+24.3			10.2	533.3
+49.3			10.1	533.4
+74.3			8.4	535.1
				530.805
12.69		(543.49)		
+99.3			8.6	534.9
Feb. 3 '26				
67+24.3			6.0	537.5
+38.2			5.3	538.2
+78			7.4	536.1
T.P.			3.18	540.31
				530.805
568+80			7.128	537.33
T.P. Rock			2.053	535.880
67+90			3.7	534.2

Cool &  
Cloudy

$\frac{29}{100} 540.6$   
 $\frac{82}{02} 535.3$   
 $\frac{112}{10} 531.6$   
 $\frac{131}{100} 530.4$   
 $\frac{02}{100} 543.5$   
 $\frac{125}{83} 541.8$   
 $\frac{75}{70} 539.6$   
 $\frac{127}{47} 530.8$   
 $\frac{131}{100} 530.4$   
 $\frac{35}{100} 540.0$   
 $\frac{98}{30} 532.7$   
 $\frac{123}{54} 531.2$   
 $\frac{128}{100} 530.7$   
 $\frac{52}{100} 523.4$   
 $\frac{65}{90} 522.1$   
 $\frac{132}{65} 515.4$   
 $\frac{127}{85} 531.1$   
 $\frac{126}{100} 530.9$   
 $\frac{59}{100} 522.7$   
 $\frac{98}{80} 518.8$   
 $\frac{117}{100} 532.1$   
 $\frac{53}{100} 522.3$   
 $\frac{123}{20} 516.3$   
 $\frac{109}{100} 532.6$   
 $\frac{100}{100} 518.63$   
 $\frac{106}{100} 532.9$   
 $\frac{18}{100} 536.1$   
 $\frac{44}{100} 533.5$

Sta.	+	T	-	Elev.
		537.933		534.4 ✓ <del>534.5</del>
68+00			3.5	
+55			2.8	535.1 ✓
+79			2.5	535.4 ✓
+85			2.3	535.6 ✓ 535.880
B.M. # 8.	11.702	547.582 ✓	.420	547.162 ✓ 547.161 <small>Recorded.</small>
	5.91	<u>553.07</u> ✓		
69+00			14.1	539.0 ✓
+34			6.8	546.3 ✓
+80.9			5.6	547.5 ✓
+90.9			6.1	547.0 ✓
70+00.9			6.6	546.5 ✓
+10.9			6.9	546.2 ✓

$\frac{22}{100}$	535.2 ✓
$\frac{18}{100}$	536.1 ✓
$\frac{15}{100}$	536.4 ✓
$\frac{02}{100}$	537.7 ✓
$\frac{02}{36}$	537.7 ✓
$\frac{41}{100}$	533.8 ✓
$\frac{35}{100}$	534.4 ✓
$\frac{30}{100}$	534.9 ✓
$\frac{27}{100}$	535.2 ✓

$\frac{82}{100}$	549.0 ✓
$\frac{92}{100}$	548.9 ✓
$\frac{32}{100}$	549.5 ✓
$\frac{41}{100}$	549.0 ✓
$\frac{42}{100}$	548.4 ✓
$\frac{49}{100}$	538.2 ✓
$\frac{102}{100}$	543.0 ✓
$\frac{161}{25}$	537.0 ✓
$\frac{72}{20}$	545.9 ✓
$\frac{70}{90}$	545.3 ✓
$\frac{74}{70}$	545.7 ✓
$\frac{80}{56}$	546.1 ✓
$\frac{82}{73}$	544.9 ✓
$\frac{163}{100}$	536.8 ✓
$\frac{122}{40}$	540.9 ✓
$\frac{122}{100}$	540.9 ✓
$\frac{93}{100}$	543.8 ✓
$\frac{105}{80}$	542.6 ✓
$\frac{103}{80}$	542.8 ✓
$\frac{102}{80}$	542.7 ✓
$\frac{106}{100}$	542.5 ✓

Sta.	+	π	-	Elev.
		553.07		
70+20.			6.8	546.3 ✓
+ 42			7.9	545.2 ✓
+ 52			10.2	542.9 ✓
BM# 8				547.161 11 AM McCarty π Leach-rod Reynolds-"
	8.800	555.961		
71+00			13.0	543.0 ✓
71+18.2			12.0	544.0 ✓
71+43.2			11.9	544.1 ✓
71+68.2			11.7	544.3 ✓
71+74.2			11.4	544.6 ✓
71+82.2			8.8	547.2 ✓
71+93.2			6.9	549.1 ✓
72+18.2			5.6	550.4 ✓
72+35.1			7.2	548.8 ✓

$\frac{50}{100}$ 548.1 ✓	$\frac{72}{35}$ 545.9 ✓	$\frac{103}{53}$ 542.8 ✓	$\frac{107}{100}$ 542.4 ✓
$\frac{63}{100}$ 546.6 ✓	$\frac{81}{13}$ 549.7 ✓	$\frac{101}{30}$ 542.7 ✓	$\frac{108}{100}$ 542.3 ✓
$\frac{62}{100}$ 547.0 ✓	$\frac{66}{63}$ 546.5 ✓		$\frac{102}{100}$ 542.4 ✓
545.5 ✓	543.4 ✓	543.0 ✓	542.4 ✓
$\frac{105}{100}$	$\frac{126}{75}$	$\frac{130}{60}$	$\frac{136}{100}$ Two rods
546.3 ✓	544.9 ✓		544.3 ✓
$\frac{92}{100}$	$\frac{111}{80}$		$\frac{112}{100}$
545.0 ✓		544.1 ✓	543.2 ✓
$\frac{110}{100}$		$\frac{119}{34}$	$\frac{120}{42}$
548.8 ✓	547.0 ✓	544.1 ✓	543.7 ✓
$\frac{72}{100}$	$\frac{90}{49}$	$\frac{111}{22}$	$\frac{113}{90}$
549.6 ✓	544.9 ✓		543.7 ✓
$\frac{64}{100}$	548.0 ✓		$\frac{123}{100}$
550.6 ✓	$\frac{80}{50}$	544.1 ✓	543.7 ✓
$\frac{54}{100}$	549.6 ✓	$\frac{113}{90}$	$\frac{119}{100}$
552.1 ✓	544.2 ✓		543.9 ✓
$\frac{39}{100}$	$\frac{64}{72}$	544.2 ✓	$\frac{121}{100}$
552.6 ✓	551.4 ✓	547.9 ✓	544.4 ✓
$\frac{34}{100}$	$\frac{46}{45}$	$\frac{81}{36}$	$\frac{116}{80}$
550.8 ✓		549.4 ✓	544.4 ✓
$\frac{53}{100}$		$\frac{116}{80}$	$\frac{116}{100}$
	547.3 ✓		546.4 ✓
	$\frac{87}{80}$		$\frac{96}{100}$
	548.0 ✓		545.5 ✓
	$\frac{80}{42}$		$\frac{105}{100}$

Sta	+	π	-	Elev
		555.961		
72+39.1			7.8	548.2 ✓
72+46.1			9.3	546.7 ✓
73+00			8.7	547.3 ✓
T.P.	3.701	546.917	12.745	543.216 ✓
74+00			5.2	541.7 ✓
74+73			10.2	536.7 ✓
75+00			11.3	535.6 ✓
75+14			8.3	538.6 ✓
75+37			9.9	537.0 ✓
T.P.	3.401	538.675	11.643	535.274 ✓
75+87.5			6.8	531.9 ✓
76+07.2			9.1	529.6 ✓
76+27.1			9.8	528.9 ✓
76+55			10.9	527.8 ✓

549.9 ✓ $\frac{61}{100}$	548.1 ✓ $\frac{79}{13}$	546.1 ✓ $\frac{99}{60}$	545.5 ✓ $\frac{105}{100}$
548.4 ✓ $\frac{76}{100}$			544.5 ✓ $\frac{115}{100}$
548.4 ✓ $\frac{76}{100}$			546.1 ✓ $\frac{99}{100}$
542.0 ✓ $\frac{49}{100}$			540.9 ✓ $\frac{60}{100}$
541.3 ✓ $\frac{56}{100}$	540.3 ✓ $\frac{66}{76}$	537.1 ✓ $\frac{98}{36}$	536.3 ✓ $\frac{106}{100}$
542.5 ✓ $\frac{44}{100}$		539.4 ✓ $\frac{75}{24}$	534.7 ✓ $\frac{123}{100}$
542.2 ✓ $\frac{47}{100}$	541.0 ✓ $\frac{59}{64}$	539.2 ✓ $\frac{77}{30}$	533.8 ✓ $\frac{134}{100}$
541.0 ✓ $\frac{59}{100}$		534.4 ✓ $\frac{125}{28}$	532.0 ✓ $\frac{149}{100}$ Two rods
535.6 ✓ $\frac{31}{100}$		536.4 ✓ $\frac{105}{20}$	533.0 ✓ $\frac{132}{55}$
534.2 ✓ $\frac{45}{100}$		531.3 ✓ $\frac{74}{17}$	530.5 ✓ $\frac{82}{30}$
533.9 ✓ $\frac{48}{100}$			529.7 ✓ $\frac{90}{100}$
529.6 ✓ $\frac{91}{100}$			528.9 ✓ $\frac{98}{100}$
	528.0 ✓ $\frac{107}{50}$		528.3 ✓ $\frac{104}{100}$
			527.5 ✓ $\frac{112}{100}$

Sta	+	π	-	Elev.	3 PM McCarty π Leach-rod Reynolds
		538.675			
77+00			11.8	526.9	Recorded
BM# 9			8.759	529.916	529.904
<hr/>					
B.M. # 9				529.904	529.904
Sta 80+70	4.228	534.132			
TP Rock			4.086	530.046	
77+44			7.7	526.4	
B.C					
77+78.0			6.8	527.3	
+85			6.0	528.1	
78+03			4.9	529.2	
+28			4.7	529.4	
+53			3.9	530.2	
+78			2.2	531.9	
+98			2.5	531.6	
79+03			1.9	532.2	

527.0	526.7	526.0
$\frac{117}{100}$	$\frac{120}{50}$	$\frac{127}{100}$
526.6	527.3	526.1
$\frac{75}{100}$	$\frac{68}{77}$	$\frac{80}{100}$
527.5	528.0	527.2
$\frac{66}{100}$	$\frac{61}{70}$	$\frac{69}{100}$
528.2	529.8	527.6
$\frac{52}{100}$	$\frac{43}{80}$	$\frac{65}{100}$
530.7	529.8	528.5
$\frac{34}{100}$	$\frac{43}{80}$	$\frac{56}{100}$
530.8		
$\frac{33}{100}$		
530.7		530.0
$\frac{34}{100}$		$\frac{41}{100}$
532.2		531.2
$\frac{19}{100}$		$\frac{29}{100}$
532.7		531.3
$\frac{12}{100}$		$\frac{28}{100}$
532.0		531.2
$\frac{11}{100}$		$\frac{29}{100}$

Sta.	+	Δ	-	Elev
		534.132		
79+28			2.7	531.4
79+44.5-Back				
=79+43.7 Ahead			3.3	530.8
				T.P. 530.046 80+70
	7.05	537.10		
+47.5			5.9	531.2
+72.5			5.2	531.9
+97.5			3.8	533.3
80+22.5			3.2	533.9
+47.5			3.5	533.6
+72.5			5.0	532.1
+97.5			6.4	530.7
81+22.5			7.3	529.8
+36.8			7.1	530.0

533.2 ✓  
02  
100  
534.3 ✓  
28  
100

530.1 ✓  
40  
100  
530.0 ✓  
41  
100

534.2 ✓  
29  
100

530.2 ✓  
69  
24  
530.3 ✓  
68  
70

534.1 ✓  
30  
100

530.2 ✓  
69  
100  
530.5 ✓  
64  
100

536.3 ✓  
08  
100  
536.9 ✓  
02  
100

534.3 ✓  
28  
50

532.0 ✓  
51  
100

535.0 ✓  
21  
100

531.7 ✓  
54  
100

534.0 ✓  
31  
100

530.7 ✓  
64  
100  
528.9 ✓  
82  
100

531.8 ✓  
53  
100  
530.8 ✓  
63  
100

528.8 ✓  
83  
100  
528.3 ✓  
43  
100

531.3 ✓  
58  
100



Sta	+	$\pi$	-	Elev.
		c		Leach $\pi$ McCart $\pi$ Rod Reynolds Feb. 9, '26 10-A.M.
		541.487		
85+00			8.4	533.1
				540.229
	D			
	8.912	549.141		
B.M # 10			1.797	547.344
				547.366
				Recorded
BM # 10	3.052			McCart $\pi$ Leach-rod Reynolds
	<del>3.052</del>	550.418		R.K. 85+95
TP			5.297	547.366
			5.397	545.121
85+08			13.2	545.021
				537.2
85+17			9.5	540.9
85+24			12.5	537.9
85+71			12.2	538.2
85+78.0			10.0	540.4
85+93.3			6.5	543.9
86+00		A	7.2	543.2
				on Boulder
TP	2.10	541.42	11.10	539.32
	6.677	551.798	0.466	551.332
		51.798		551.332
86+04			12.3	539.6

538.3				526.2
$\frac{10^e}{10^e}$				$\frac{15^e}{10^e}$
540.5				526.9
$\frac{99}{10^e}$				$\frac{235}{10^e}$ Two rods
543.4				536.3
$\frac{7^e}{10^e}$	541.5	541.7		14.1
Top of large Cl. Boulder	$\frac{8.9}{4.5}$	$\frac{8.7}{2^e}$		$\frac{10^e}{10^e}$
				579.6
CL.	544.6			A $\frac{118}{10^e}$
Edge of Boulder	$\frac{5^e}{10^e}$			532.4
	546.5			A $\frac{9^e}{10^e}$
	$\frac{39}{10^e}$			534.6
	547.2			$\frac{159}{10^e}$
	$\frac{32}{10^e}$			536.8
	548.4			$\frac{136}{10^e}$
	Ft of large Boulder	$\frac{2^e}{7^e}$		535.7
	548.8			541.0
	B $\frac{3^e}{10^e}$			537.8
	545.9			535.7
	$\frac{45}{5^e}$			94
	541.0			$\frac{126}{6^e}$
				57
				$\frac{147}{10^e}$
				Ft of Boulder
	546.1			534.2
	$\frac{57}{10^e}$			$\frac{17^e}{10^e}$



	551.798		551.332
87+00		12.0	539.8 ✓
87+74		5.2	546.6 ✓
88+00		2.2	549.6 ✓
88+35		C 7.9	551.5 ✓
TP	8.08	C 559.41 ✓	
88+60		8.4	551.0 ✓
88+81		6.0	553.4 ✓
88+89.5		8.0	551.4 ✓
89+00		7.9	551.5 ✓
89+37		D 6.1	553.3 ✓
TP	11.323	D 562.655	560.836 ✓ RK 91+88
89+62.		D 2.1	560.6 ✓
89+83		E 6.5	566.7 ✓
Feb. 4, '26			
90+00		E 7.6	565.6 ✓
90+23		D 7.7	555.0 ✓

546.2 ✓			532.0 ✓
B $\frac{55}{100}$			B 198 Two rods
554.2 ✓			538.0 ✓
C $\frac{52}{100}$			B $\frac{138}{100}$
551.7 ✓			539.6 ✓
C $\frac{17}{100}$			B $\frac{122}{100}$
558.7 ✓			544.1 ✓
C $\frac{07}{100}$			B $\frac{72}{100}$
554.9 ✓			546.1 ✓
Ft of SR Cliff $\frac{45}{88}$			C $\frac{133}{100}$
558.0 ✓			545.5 ✓
Ft of large Boulder $\frac{14}{58}$			C $\frac{139}{100}$
561.8 ✓			541.9 ✓
D $\frac{09}{100}$			C $\frac{175}{100}$
560.7 ✓			543.9 ✓
D $\frac{20}{100}$			C $\frac{155}{100}$
547.2 ✓			546.4 ✓
			C $\frac{130}{100}$
Center line foot of large boulder			553.6 ✓
565.3 ✓			D $\frac{92}{100}$
E $\frac{79}{73}$			560.7 ✓
572.1 ✓			D $\frac{20}{100}$
E $\frac{11}{100}$			557.5 ✓
571.7 ✓			D $\frac{52}{100}$
E $\frac{15}{100}$			547.2 ✓
563.8 ✓			D $\frac{155}{100}$
E $\frac{94}{100}$			

Feb. 5  
McCarthy  
Leach-rod  
Reynolds

Clear and  
cobl

Sta	+	$\pi$	-	Elev.
90+51.2		562.655 <del>562.655</del>	D 2.1	560.836 560.6 ✓
90+55			D 2.1	560.6 ✓
TP	12.36	573.20 ✓		
90+60	0.75		F 13.1	548.5 ✓
TP	0.75	561.59 ✓		
90+71			F 10.7	550.9 ✓
90+81			F 15.3	546.3 ✓ 545.3 ✓
91+00			F 12.9	548.7 ✓
91+52			F 8.3	553.3 ✓
91+62.7			F 9.2	552.4 ✓
91+87.7			F 3.7	557.9 ✓
92+12.7			H 11.4	560.8 ✓ <del>561.8</del>
92+37.7			H 8.5	563.7 ✓
92+57			H 9.4	562.8 ✓
92+62.7			H 13.4	558.8 ✓

568.1 ✓ E $\frac{51}{100}$	565.4 ✓ E $\frac{78}{62}$	553.1 ✓ D $\frac{96}{100}$
568.3 ✓ E $\frac{49}{100}$	566.8 ✓ E $\frac{64}{90}$	543.3 ✓ G $\frac{79}{100}$
567.8 ✓ E $\frac{54}{100}$	565.9 ✓ E $\frac{73}{72}$	540.5 ✓ G $\frac{107}{100}$
566.6 ✓ F $\frac{50}{100}$	563.5 ✓ F $\frac{81}{54}$	548.0 ✓ F $\frac{130}{75}$
566.8 ✓ F $\frac{48}{100}$		546.2 ✓ F $\frac{154}{100}$
558.0 ✓ F $\frac{30}{100}$		538.0 ✓ G $\frac{132}{100}$
559.3 ✓ F $\frac{23}{100}$		537.9 ✓ G $\frac{133}{100}$
560.3 ✓ F $\frac{13}{100}$		543.5 ✓ G $\frac{72}{100}$
564.3 ✓ H $\frac{79}{100}$		545.7 ✓ G $\frac{55}{100}$
567.5 ✓ H $\frac{47}{100}$		551.3 ✓ F $\frac{103}{100}$
569.2 ✓ H $\frac{30}{100}$		553.7 ✓ F $\frac{79}{100}$
568.5 ✓ H $\frac{37}{100}$		556.6 ✓ F $\frac{50}{90}$
568.2 ✓ H $\frac{40}{100}$	567.0 ✓ H $\frac{52}{72}$	558.2 ✓ F $\frac{34}{70}$
	562.5 ✓ H $\frac{97}{51}$	554.4 ✓ F $\frac{72}{80}$
		552.2 ✓ F $\frac{94}{100}$
		551.7 ✓ F $\frac{99}{100}$

Sta	+	π	-	Elev
92+65			H 14.8	560.836 557.4 ✓
92+87.7			H 12.8	559.4 ✓
93+02			H 13.1	559.1 ✓
93+12.7			H 12.6	559.6 ✓
93+20			H 11.4	560.8 ✓
93+37.7			H 15.3	556.9 ✓
93+48.7		F 561.59	H 15.5 12.25	556.7 549.34 ✓
T.P.	1.81	G 551.15		
T.P.	11.380	H 57.2216	9.541	562.675 <sup>RK</sup> 94+73
94+00			H 6.6	565.6 ✓
94+48.5 Fwd = 94+37.6 Back			H 7.3	564.9 ✓
94+73			H 10.7	561.5 ✓
94+98.6			I 8.2	555.8 ✓
95+23.6			I 12.5	551.5 ✓

566.8 ✓ H $\frac{54}{100}$	561.2 ✓ H $\frac{110}{60}$	551.0 ✓ F $\frac{106}{100}$
567.9 ✓ H $\frac{43}{100}$	563.7 ✓ H $\frac{85}{35}$	552.0 ✓ F $\frac{96}{85}$
567.6 ✓ H $\frac{46}{100}$	565.0 ✓ H $\frac{72}{42}$	551.6 ✓ F $\frac{100}{70}$
567.2 ✓ H $\frac{50}{100}$	563.1 ✓ H $\frac{91}{29}$	547.7 ✓ F $\frac{78}{70}$
566.3 ✓ H $\frac{59}{100}$	558.2 ✓ H $\frac{140}{33}$	547.7 ✓ F $\frac{139}{82}$
566.8 ✓ H $\frac{54}{100}$	559.3 ✓ H $\frac{129}{32}$	547.3 ✓ F $\frac{143}{100}$
568.0 ✓ H $\frac{42}{100}$	563.7 ✓ H $\frac{85}{80}$	549.0 ✓ F $\frac{82}{52}$
571.2 ✓ H $\frac{10}{100}$	553A ✓ F $\frac{82}{52}$	549.0 ✓ F $\frac{126}{82}$
569.6 ✓ H $\frac{26}{100}$	551.5 ✓ F $\frac{104}{80}$	548.6 ✓ F $\frac{130}{100}$
567.1 ✓ H $\frac{51}{100}$	554.3 ✓ I $\frac{97}{42}$	549.2 ✓ F $\frac{124}{100}$
561.3 ✓ H $\frac{109}{100}$	553.0 ✓ I $\frac{110}{50}$	560.6 ✓ H $\frac{112}{100}$
557.5 ✓ I $\frac{65}{100}$	551.7 ✓ I $\frac{123}{80}$	561.0 ✓ H $\frac{112}{100}$
		556.6 ✓ H $\frac{156}{100}$
		544.8 ✓ I $\frac{172}{100}$
		542.1 ✓ J $\frac{118}{100}$

Feb 6  
McCarty  
Leach-rod  
Reynolds

Clear and Cool

Elev. 562.675

RK. 95+95

Sta.	+	π	-	Elev.
TP	1.323	563.998	10.481	553.517
95+48.6			J 6.1	547.8
95+73.6			J 8.0	545.9
95+98.6			J 9.0	544.9
96+23.6			J 9.6	544.3
TP	0.070	553.587		Recorded
BM#12	0.918	549.264	5.241	548.346
BM#11	10.820	541.772	3.252	546.012
TP	0.42	553.9.4		
96+46.9			K 2.9	539.1
97+00			K 11.2	530.8
TP	1.02	K 542.00	12.96	540.98
TP	8.82	L 541.70	9.12	532.88
97+50			L 6.0	535.7
97+91.2			L 8.2	533.5
BM#12	0.989	549.329		548.340
BM#11			3.322	546.007

BM #11 seems to be .01 out. The rod cannot be plumbed.

552.1  
I  $\frac{113}{100}$   
552.3  
I  $\frac{117}{100}$   
550.1  
I  $\frac{13.3}{100}$   
550.3  
I  $\frac{137}{100}$

€  
540.2  
J  $\frac{137}{70}$   
541.4  
J  $\frac{125}{59}$   
540.9  
K  $\frac{11}{60}$   
540.4  
K  $\frac{16}{50}$   
537.2  
J  $\frac{167}{80}$   
537.0  
J  $\frac{167}{100}$   
535.6  
K  $\frac{64}{100}$   
533.4  
K  $\frac{86}{80}$   
532.8  
K  $\frac{92}{100}$   
539.3  
J  $\frac{146}{100}$

547.4  
J  $\frac{65}{100}$   
540.3  
J  $\frac{136}{100}$

541.4  
J  $\frac{125}{30}$   
537.5  
K  $\frac{45}{37}$   
529.8  
K  $\frac{123}{80}$   
529.4  
K  $\frac{126}{100}$   
523.7  
K  $\frac{183}{100}$

Two rods.

541.1  
L  $\frac{06}{100}$   
540.6  
L  $\frac{11}{100}$

539.3  
L  $\frac{24}{80}$

528.0  
L  $\frac{13.3}{100}$   
527.3  
L  $\frac{144}{100}$

Sta +  $\pi$  - Elev.   
 Feb. 6, 26   
 B.M #12 548.340   
 Sta. 98+50 .090 548.430   
 T.P. Rock 10.546 —   
 11.443 537.884   
 .545   
 537.532   
 98+16.2 A 7.5 530.9   
 A   
 Sta 99+75 .545 538.429   
 T.P. Rock 9.802 528.627   
 98 +41.2 12.3 526.1   
 +66.2 13.5 524.9   
 +91.2 12.0 526.4   
 99+16.2 12.9 525.5   
 +28.5 12.5 525.9   
 +830   
 Sta 101+90 1.839 "B" 530.466   
 T.P. Rock 5.555 524.911   
 100+00 5.7 524.8   
 +20 5.4 525.1

Leach-T Clear   
 McCarty-Rod &   
 Reynolds Cool   
 Feb 6, 1926

Home

Wrong rod reading -

534.8   
 $\frac{13.6}{10^0}$

532.3   
 $\frac{6.1}{10^0}$

530.8   
 $\frac{7.6}{10^0}$

530.7   
 $\frac{7.2}{10^0}$

530.3   
 $\frac{8.1}{10^0}$

531.1   
 $\frac{7.3}{10^0}$

528.8   
 $\frac{1.2}{10^0}$

527.8   
 $\frac{2.2}{10^0}$

523.7   
 $\frac{14.7}{10^0}$

521.5   
 $\frac{16.9}{10^0}$

519.9   
 $\frac{10.6}{10^0}$

520.5   
 $\frac{10^0}{10^0}$

520.5   
 $\frac{10^0}{10^0}$

521.2   
 $\frac{9.3}{10^0}$

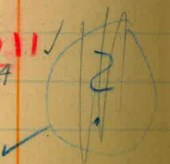
522.0   
 $\frac{8.5}{10^0}$

523.5   
 $\frac{7^0}{10^0}$

Sta	+	T	-	Elev
		B		
		529.569	530.466 ✓	
100+38			2.6	527.9 ✓
+50			3.4	527.1 ✓
+81			3.4	527.1 ✓
101+00			1.1	529.4 ✓
T.P			1.96	<del>528.61</del> 528.51 <del>527.61</del>
+10	5.66	C		
		<del>533.21</del>		530.5
		<del>534.21</del>		<del>530.6</del>
		534.17		529.6
+22			3.7	<del>531.2</del> <del>531.3</del>
+35			3.0	<del>530.3</del> <del>526.6</del> <del>526.4</del>
+51			7.6	<del>525.7</del> <del>529.2</del> <del>529.3</del>
+77			5.0	<del>528.3</del> <del>525.2</del> <del>525.3</del>
102+00			9.0	524.3
Feb. 8.				528.9
+25			5.3	<del>529.0</del> <del>528.0</del> 529.911 ✓ 524.014
+70	10.57	D		
		<del>535.48</del>		531.3
		534.58		530.4

528.5 ✓				
$\frac{2.0}{10.0}$				
528.7 ✓				
$\frac{1.8}{10.0}$				
528.1 ✓				
$\frac{6.2}{10.0}$				
530.2 ✓				
$\frac{0.3}{10.0}$				
529.5 ✓				
$\frac{3.1}{5.0}$				
527.4 ✓				
$\frac{5.5}{10.0}$				
525.0 ✓				
$\frac{4.8}{10.0}$				
525.7 ✓				
$\frac{3.6}{10.0}$				
526.9 ✓				
$\frac{1.5}{10.0}$				
528.9 ✓				
531.3 ✓				
$\frac{2.9}{10.0}$				
530.4				
531.8 C				
$\frac{2.4}{10.0}$				
530.9				
528.7				
$\frac{2.4}{10.0}$				
527.8				
$\frac{5.3}{10.0}$				
529.8				
$\frac{4.4}{10.0}$				
528.9				
$\frac{7.4}{10.0}$				
525.7				
$\frac{7.5}{10.0}$				
530.5				
$\frac{3.7}{10.0}$				
529.6				
532.7 ✓				
$\frac{2.8}{10.0}$				
531.8				
529.2 C				
$\frac{4.7}{7.5}$				
528.3				
$\frac{6.5}{10.0}$				
525.7				
$\frac{8.5}{10.0}$				
524.8				
526.9				
$\frac{7.4}{10.0}$				
524.6				
$\frac{9.6}{10.0}$				
527.6				
$\frac{6.6}{10.0}$				
526.7				
528.9 ✓				
$\frac{6.6}{10.0}$				
528.0				
$\frac{6.6}{10.0}$				

edge of rock



Sta.

+

A

-

Elev.

Leach T.  
McCarty Rod  
Reynolds  
Feb. 8, '26~~535.48~~  
~~534.58~~

528.9 ✓

102+90

6.6 528.0

527.6 ✓

103+00

7.9 526.7

2.950 524.911

2.950 527.861 ✓

6.972 520.889 520.889

524.911

3.00 527.91 ✓

+22

2.3 525.6 ✓

+58

1.3 526.6 ✓

104+00

1.8 526.1 ✓

+25

2.5 525.4 ✓

531.2 ✓

~~530.3~~ $\frac{43}{100}$ 

530.3 ✓

 $\frac{53}{100}$ 

527.4 ✓

~~526.5~~ $\frac{84}{100}$ 

526.7 ✓

 $\frac{88}{100}$ 

526.6 ✓

 $\frac{13}{100}$ 

526.9 ✓

 $\frac{10}{100}$ 

527.1 ✓

 $\frac{08}{100}$ 

527.5 ✓

 $\frac{04}{100}$ 

526.7 ✓

 $\frac{12}{80}$ 

524.6 ✓

 $\frac{33}{100}$ 

525.5 ✓

 $\frac{24}{100}$ 

525.6 ✓

 $\frac{23}{100}$ 

524.3 ✓

 $\frac{36}{100}$

10 AM  
McCarty X  
Leach-rod  
Reynolds

BM # 13	+	π	-	Elev.	
	12.818	533.709	1.116	520.891	Stump. 106+56
104+60			6.1	527.6	
105+00			7.3	526.4	
105+27			8.9	524.8	
105+59.1			5.9	527.8	
105+84.1			5.8	527.9	
105+98			7.5	526.2	
106+09.1			6.0	527.7	
106+34.1			4.6	529.1	
106+49.6			5.9	527.8	
TP	3.20	535.79			
106+56.7			5.4	528.3	
106+81.7			6.3	527.4	
TP	2.010	534.603	13.090	521.513	Stump Sta 107+56
107+06.7			9.0	525.6	

530.3

$\frac{34}{100}$

529.9

$\frac{38}{100}$

529.3

$\frac{44}{100}$

531.1

$\frac{26}{100}$

531.9

$\frac{18}{100}$

530.8

$\frac{29}{100}$

531.7

$\frac{20}{100}$

534.9

$\frac{09}{100}$

534.3

$\frac{15}{100}$

534.8

$\frac{10}{100}$

533.8

$\frac{20}{100}$

529.9

$\frac{43}{100}$

531.1  
 $\frac{26}{45}$

524.6

$\frac{91}{67}$

524.0

$\frac{97}{114}$

522.9

$\frac{108}{100}$

520.7

$\frac{130}{100}$

525.0

$\frac{128}{100}$

521.8

$\frac{140}{100}$

521.5

$\frac{143}{100}$

522.1

$\frac{137}{100}$

525.2

$\frac{106}{100}$

526.2

$\frac{90}{100}$

526.1

$\frac{97}{100}$

523.7

$\frac{121}{100}$

520.6

$\frac{140}{100}$

Two rods





B.M.#1	-1409.3'L. Nail in Tree Sta.	571.460 Elev
BM#2	11+50 20'R in Sycamore	570.564
BM#3	19+95 23'R Pt on Boulder	570.171
BM#4	32+22 20'L Oak tree	568.844
BM#5	41+33 14'R Pt on Boulder	543.678
BM#6	53+05 18'R Nail in Oak	539.618
BM#7	60+85 15'L Nail in Oak	546.027
BM#8	70+70 5'L Pt on Boulder	547.161
BM#9	77+50 11'L Nail in Oak	529.904
BM#10	84+96 16'L Nail in Oak	547.366
BM#11	97+40 15'L Leaning tree	545.997
BM#12	97+92 15'L Pt on Rock	548.340
BM#13	104+45 Round peg at foot of post North of road	520.891

1246

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder  
stake for any width roadway, slope 1% to 1.  
If ground is nearly level, the cut or fill at side  
stake is located by the double entry method in

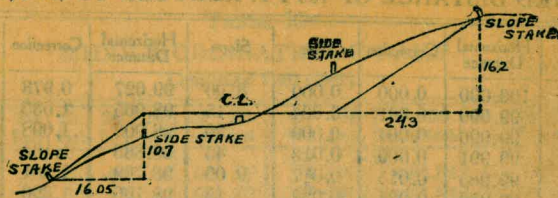
IMPROVED TABLES

AND

INFORMATION

TABLE No. 2.

To find Tangent and External for curve of  
any other radius by means of curve and  
add constant found in column of connection.  
Degree of curve with a given length may be found  
by dividing tangent (or external) opposite L by  
given tangent (or external).  
The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

11.702

10.482

4.374 TP 36+90

455.848  
Elev

+ 1 X  
4.901 560.799

1.726 559.023 RK 38+85

~~9.316 568.339~~

8.242 567.265

12.642 554.623 BM

9524 0555.147

11.465

554.623

555.961  
12.745

555.147  
11.465

543.216 -73+50

546.917  
11.643

543.682

535.274 -75+70  
3.901

540.523

538.675  
8.759

5.31864

529.916

42+68.4

535.738

3.702

12+83.2

2.8

6.9

12.1

532.036

539.618

0.966

540.584

0.061

540.523

3.794

544.317

8.659

535.658

3.874

539.532

3.702

535.830

10.838

524.992

535.830

10.838

546.668

0.634

546.034 -BM

546.027

10.07

535.658

5.110

520.891  
519.992  
.899

537.889  
536.987  
.897

11.443  
.897  
12.340

11.443  
.897  
10.546

547.366  
5.397

541.969  
3.052

545.021  
6.677

551.698  
0.466

551.232  
1.819

549.413  
11.323

560.736  
11.380

572.116  
9.541

562.575  
1.323

563.898  
10.481

553.417  
0.070

553.487  
5.241

548.246

569.250  
19  
568.844  
2.400

571.244  
5.304

565.940  
12.400

588.340

565.940  
12.400

578.340  
1.356

576.984  
12.818

589.802  
0.332

589.470  
12.103

601.573  
11.741

589.832  
2.354

592.186  
10.190

581.996  
1.289

583.285  
13.090

570.195

570.195

577.467  
5.717  
571.770

593.3

5.65 4.4 12.00

754 x 2 15.6

5280

269.116  
0.31

269.197  
11.604

257.503  
3.293

260.836  
11.335

249.501  
5.586

255.097  
0.295

254.792  
5.662

254.254  
5.262

289.189  
150.8

569.250  
568.344  
4.06

540.929  
1.282

539.647  
6.18

0.45  
44.200  
126  
290  
320  
20

12.00  
4.4  
52.80  
48

269.116  
0.836  
269.952

2579

566.340  
1  
565.940

205 144

13.5

700 x 1 = 5280

572.326  
13.090

585.416

559.236

583.285  
13.090

570.195  
1.71  
0.29