EL "CAPITAN"

Pipe Line Survey

Levels — No 4

& Cross. Sections

LEVEL BOOK

380

W194

Sta. 110 +39 to Sta. 447+00

Levels and Cross Sections

511.913
511.898
.015

BM#14			574.366		
	1.157	575.523	7.246	568.277	
	0.101	568.378	11.863	556.515	
	0.067	556.582	11.318	545.264	
	0.579	545.843	11.846	533.997	
	1.051	535.048	11.067	523.981	
	0.080	524.061	12.163	511.898	
	2.772	514.670	6.165	508.505	
	4.463	512.968	4.505	508.463	
				508.445	463
	4.505	512.950	4.463	508.487	445
	6.175	514.662	2.790	511.872	.018
					898
					872
					16
BM#16				503.054	
	2.075	505.129	2.930	502.199	
					191
	2.080	505.134	2.943	502.191	184
					.007
	2.943				
	~~2.942~~	505.127		502.184	
			2.080	502.047	
		505.134			
		4.559			
		500.575			

Paper Profile and Quantities

Sta.	Elev.	Grade	Cut	Cu. Yds.	Class.
0+00	571.8				
1+	569.7				
+21	569.7				
+25	571.1				
+47.5	571.1				
+90.2	575.5				
2+32.9	580.6				
+61	578.0				
3	580.0				
+35	580.1				
+65	575.7				
+80	577.0				
4	575.6				
+25	573.5				
+35	570.8				
+55	570.0				
+56.8	570.7				
5+	572.4				
6+	575.3				
+50	579.6				
7+	577.9				
+25	577.6				
+48.5	576.4				
8+	571.5				
+15	570.3				
+50.5	570.4				

	+	↑ (7.887)	− (1.164)	Elev.	
B.M. #19 =				500.758	B.M. #19
	7.887	508.645			
			5.696	502.949	
	4.519	507.468			
					Recorded
B M #20			2.841	504.627	504.635
B.M #14				574.366	
	1.032	575.398			
			12.280	563.118	
	.796	563.914			
			12.325	551.589	
	1.821	553.410			
			12.990	540.420	
	.938	541.358			
T.P. 114+25			7.354	534.004	
			12.281	529.077	
	1.125	530.202			
			11.433	518.769	
	.733	519.502			
T.P. 114+75			7.589	511.913	

Sta.	Elev.	Grade	Cut	Cu. Yds.	Class
9+54	571.5				
10+		565.00			
10+46	569.8				
11+		566.00			
11+48	571.8				
12+46	574.5				
12+50		573.00			
13+49.4	577.2				
13+50		575.00			
14+		574.00			
14+21.7	575.8				
14+49.7	576.5				
14+50		572.00			
14+97	570.2				
15+		567.50			
15+45	569.2				
16+48	565.4				
16+50		563.00			
18+49	566.3				
18+81	563.9				
19+		558.00			
19+48	564.7				
19+50		559.00			

+	π	−	Elev. 534.004
1.164	535.168		
		11.742	523.426
1.510	524.936		
		13.022	511.914
			446.620
10.773	457.393		
		9.732	447.661
7.130	554.791		
		7.075	447.716
4.312	452.028		
		3.133	448.895
			446.191
1.783	447.884		
		5.210	442.674
4.055	446.729		
		6.342	440.387
4.151	444.538		
		6.900	437.638
6.400	444.038		
		5.108	438.930

Sta.	Elev.	Grade	Cut	Cu. Yds.	Class.
20+04	571.7				
20+52	571.5				
20+75		564.00			
20+94.9	569.4				
21+50	570.3				
21+75		564.00			
22+48	569.9				
22+75		568.00			
23+25		576.00			
23+43	584.8				
23+75		581.00			
24+44	589.1				
24+71.6	587.6				
25+		586.00			
25+92	596.6				
26+		588.00			
26+46.1	595.8				
26+50		587.00			
27+37	590.0				
27+50		584.00			
27+71.2	586.1				
27+95	585.7				
28+		580.00			

	+	π	−	Elev.	.680 .649 .036
				403.777	
	5.072	408.849			
			1.205 1.2005	407.644	
	7.549	415.193			
			1.560	413.633	
B.M.#48				407.212	
	3.929	411.141			
			4.021	407.120	
	12.389	419.509			
			2.200	417.309	417.160 .149 (error)

Sta.	Elev.	Grade	Cut	Cu. Yds.	Class.
28+46.6	579.0	✓			
29+		566.00			
29+46.6	566.4	✓			
30+		556.00			
30+11	561.5	✓ Ok to here 1/27/15 —		D.L.B. H.G.Mc	
30+50	560.6				
31+44	560.0				
32+45	564.0				
34+41	555.3				
35+43	552.4				
36+43	551.0				
37+44.2	563.8				
38+49	551.4				
	561.8				

Profile Levels
and Cross-Sections of
Final Location —

From Station - 110+39
To - 447+00

Sta	+	HI	−	Elev		Left	℄	Right
110+39		525.023	9.8	523.691 515.2		-9.9/10.0 (515.1)		10.0/10.0 (525.0) 2
110+67.6			11.2	513.8		8.2/10.0 (516.8)	10.5/0.8 (514.5)	10.9/10.0 (514.1)
110+69.4			10.7	514.3		8.3/10.0 (516.7)	11.1/0.6 (513.9)	10.8/10.0 (514.2)
111+00			9.1	515.9		7.6/10.0 (517.4)		10.2/10.0 (514.8)
TP	12.246	535.937	1.026	534.911	Rock 112+00			
111+74			5.2	530.7		1.4/10.0 (534.5)	6.5/3.5 (529.4) 7.4/6.0 (528.5)	9.7/10.0 (526.2)
112+00			3.9	532.0		On Boulder 4.9/10.0 (531.0)	7.6/1.3 (528.3)	6.2/10.0 (529.7)
T.P.	12.443	C 547.354	0.969	546.385	Rock 112+50			
112+22			2.1	545.3		D 11.5/10.0 (547.7)	C 2.8/1.1 (544.6) C 6.1/4.0 (541.2) 541.3	C 8.2/10.0 (539.2)
T.P.	12.772	D 559.157	0.190	558.967	Rock 112+75			
T.P	12.655	E 571.622	1.301	570.321	Rock 113+00			
112+80			E 7.8	563.8		E 5.0/10.0 (566.6)		E 12.3/10.0 (559.3)
113+00			E 3.2	568.4		E 0.1/10.0 (571.5)		E 5.7/10.0 (565.9)
T.P.	9.834	F 580.155	5.790	574.365	BM# 14 574.366			
113+11.5			F 5.0	575.2		F 5.1/10.0 (575.1)		F 4.0/10.0 (576.2)
113+21.5			4.8	575.4		4.2/10.0 (576.0)		2.5/10.0 (577.7)
113+28.5			6.2	574.0		575.3 4.9/10.0	5.6/7.6 (574.6)	3.9/10.0 (576.3)

Feb 9 McCarty-π Reynolds-rod Clear and cool

		580.155						
113+42.5			11.8	568.4	Rock 113+50	10.3/10.0 569.9 (56 8.4 struck out)		12.1/10.0 568.1
T.P			11.880	568.276				
	0.130	568.406	12.464	555.942	T.P.			
113+79			14.3	554.1		13.1/10.0 555.3	⊙	15.8/10.0 552.6
T.P	0.909	A 556.851	11.583	545.268	Rock 114+00			
113+91			7.4	549.5		6.5/10.0 550.4	⊙	9.5/10.0 547.4
	0.191	B 545.459	11.459	534.000	Rock 114+25			
114+00			2.7	542.8		A 12.1/10.0 544.8	⊙	2.9/10.0 542.6
114+07			7.0	538.5		6.2/10.0 539.3		6.0/10.0 539.5
114+14			11.5	534.0		9.8/10.0 535.7		C 5.4/10.0 529.3
TP	0.675	C 534.675	11.697	522.978				
114+24½			7.2	527.5		3.4/10.0 531.3	⊙	10.0/10.0 524.7
TP	1.377	D 524.355	12.453	511.902	Rock 114+75			
114+49½			6.5	517.9		4.6/10.0 519.8	⊙	8.1/10.0 516.3
T.P	3.338	515.240						
114+74½			D 13.0	511.4		3.4/10.0 511.8 (514.8 struck out)	⊙	4.4/10.0 510.8
114+99½			5.2	510.0		4.9/10.0 510.3		4.9/10.0 510.3
115+24.1			4.7	510.5		4.8/10.0 510.4		4.8/10.0 510.4
115+49.1			4.7	510.5		5.0/10.0 510.2		4.7/10.0 510.5

		515.240			
115+96.4			4.9	510.3	
116+00			4.9	510.3	
116+12.9	BC		4.2	511.0	
116+32.5			4.8	510.4	
	EC		5.0'	510.2	
117+00			5.3	509.9	
118+00			5.7	509.5	
119+00			6.7	508.5	
120+00			6.8	508.4	
T.P.	4.192	512.707	6.725	508.515	Recorded
BM#15			4.225	508.482	508.445

This elevation found by peg line to be 508.505

BM found by peg line to be 508.463 - Checked to .002 by second peg line. Does not affect H.I.'s for computing ground elevations.

$\frac{5^{\circ}}{10^{\circ}}$ 510.2 $\frac{5^{1}}{10^{\circ}}$ 510.1 $\frac{4^{5}}{10^{2}}$ 510.7 $\frac{4^{8}}{10^{\circ}}$ 510.4 $\frac{5^{\circ}}{10^{2}}$ 510.2 $\frac{5^{5}}{10^{\circ}}$ 509.7 $\frac{5^{8}}{10^{\circ}}$ 509.4 $\frac{6^{6}}{10^{\circ}}$ 508.6 $\frac{4^{3}}{10^{\circ}}$ 510.9

$\frac{4^{8}}{7^{\circ}}$ 510.4 $\frac{5^{3}}{10^{\circ}}$ 509.9

$\frac{4^{9}}{5^{\circ}}$ 510.3 $\frac{5^{4}}{8^{\circ}}$ 509.8 $\frac{5^{3}}{10^{\circ}}$ 509.9

$\frac{4^{8}}{5^{5}}$ 510.4 $\frac{5^{3}}{6^{\circ}}$ 509.9 $\frac{5^{3}}{10^{\circ}}$ 509.9

$\frac{4^{9}}{5^{\circ}}$ 510.3 $\frac{5^{5}}{6^{\circ}}$ 509.7 $\frac{5^{3}}{10^{\circ}}$ 509.9

$\frac{5^{1}}{5^{5}}$ 510.1 $\frac{5^{7}}{7^{\circ}}$ 509.5 $\frac{5^{5}}{10^{\circ}}$ 509.7

$\frac{5^{3}}{5^{\circ}}$ 509.9 $\frac{5^{8}}{7^{\circ}}$ 509.4 $\frac{5^{6}}{10^{\circ}}$ 509.6

$\frac{5^{9}}{4^{\circ}}$ 509.3 $\frac{6^{2}}{5^{\circ}}$ 509.0 $\frac{6^{1}}{10^{\circ}}$ 509.1

$\frac{6^{7}}{6^{\circ}}$ 508.5 $\frac{6^{8}}{7^{\circ}}$ 508.4 $\frac{6^{6}}{10^{\circ}}$ 508.6

$\frac{6^{8}}{7^{\circ}}$ 508.4 $\frac{7^{4}}{8^{5}}$ 507.8 $\frac{7^{3}}{10^{\circ}}$ 507.9

509.9

See page 1

	+	Π	−	Elev.
BM#15				508.445
T.P.	4.505	512.950	4.463	508.487
TP	4.275	512.762		
120+98.9			4.9	507.9
121+23.9			5.2	507.6
121+48.9			5.2	507.6
121+73.9			5.3	507.5
121+98.9			5.5	507.3
122+23.9			5.2	507.6
122+48.9			5.6	507.2
122+73.9			5.4	507.4
122+98.9			5.4	507.4
123+23.9			5.3	507.5
123+48.9			5.4	507.4

508.2
4.6 / 10.2

507.9
4.9 / 10.2

507.7
5.1 / 10.2

507.6
5.2 / 10.2

507.2
5.6 / 10.2

507.1
5.7 / 10.2

507.5
5.3 / 10.2

507.3
5.5 / 10.2

507.6
5.2 / 10.2

507.4
5.4 / 10.2

507.7
5.1 / 10.2

507.2
5.6 / 10.2

507.3
5.5 / 10.2

507.4
5.4 / 8.0

507.1
5.7 / 9.2

507.2
5.6 / 10.2

507.5
5.3 / 10.2

507.6
5.2 / 10.2

507.5
5.3 / 10.2

507.6
5.2 / 10.2

507.6
5.2 / 10.2

507.5
5.3 / 10.2

507.6
5.2 / 10.2

507.6
5.2 / 10.2

507.3
5.3 / 10.2

507.3
5.3 / 10.2

		512.762		
123+73.9			5.2	507.6
123+94.7			5.0	507.8
125+00			5.5	507.3
T P	3.802	509.773	6.791	505.971
125+91.9			4.0	505.8
126+16.9			4.0	505.8
126+41.9			4.0	505.8
126+66.9			4.3	505.5
126+91.9			4.6	505.2
127+16.9			4.6	505.2
127+41.9			4.8	505.0
127+66.9			4.9	504.9
127+85.1			4.8	505.0
128+00			4.6	505.2

507.3 5 5 / 10

Ft. of tree 507.9 4 9 / 8

507.3 5 5 / 10

506.1 3 7 / 10

505.8 4 / 10

505.5 4 3 / 10

505.8 4 / 8

505.8 4 / 10

505.8 4 / 7

505.4 4 4 / 6

505.4 4 4 / 10

505.6 4 2 / 10

505.1 4 7 / 8

505.3 4 5 / 10

505.1 4 7 / 10

505.1 4 7 / 10

505.1 4 7 / 10

505.1 4 7 / 10

505.1 4 7 / 10

505.1 4 7 / 5

504.6 5 3 / 6

504.7 5 1 / 3

504.6 5 2 / 2

504.7 5 1 / 1

504.6 5 2 / 2

507.7 5 1 / 10

507.6 5 2 / 10

507.5 5 3 / 10

505.8 4 / 10

506.0 3 8 / 10

505.9 3 9 / 10

505.7 4 1 / 10

505.4 4 4 / 10

505.1 4 7 / 10

505.1 4 7 / 10

505.2 4 6 / 10

505.3 4 5 / 10

505.2 4 6 / 10

	+	T	−	Elev
		509.773		
129+00			4.3	505.5
130+00			4.9	504.9
131+00			5.6	504.2
132+00			6.6	503.2
TP	4.382	507.657	6.498	503.275
BM#16			4.610	503.047
133+00			4.8	502.9 / ~~502.8~~
133+04.1			4.8	502.9 / ~~502.8~~
133+27.2			4.9	502.8 / ~~502.7~~
133+50.3			4.7	503.0 / ~~502.9~~
134+00			5.2	502.5 / ~~502.4~~
134+25.3			5.1	502.6 / ~~502.5~~
BM#16	4.610	507.664		503.054
134+50.3			5.1	502.6
134+75.3			5.2	502.5

Recorded 503.054

505.7
41 / 10

504.9
49 / 10

504.4
54 / 10

503.5
63 / 10

503.2
45 / 10

503.1
46 / 10

503.3
44 / 10
503.1
503.2
46 / 10

503.0
47 / 10

502.7
50 / 10

502.3
52 / 10

502.1
56 / 10

505.5
43 / 15

505.2
46 / 20

504.6
52 / 05

504.4
54 / 25

503.8
65 / 35

503.2
45 / 20

502.8
48 / 10

503.1
46 / 20

503.1
46 / 10

503.0
47 / 13

502.7
~~502.8~~
50 / 20

502.6
51 / 70

502.3
54 / 80

505.8
40 / 10

505.2
46 / 10

504.8
50 / 10

503.6
62 / 10

503.0
47 / 10

503.0
47 / 10

503.0
47 / 10

502.9
48 / 10

~~502.5~~ 502.6
52 / 10

502.9
48 / 10

503.1
46 / 10

502.7
50 / 10

(6)

		507.664			
135+00.3			5.5	502.2	
135+03.0			5.6	502.1	
136+00			5.7	502.0	
136+01.0			5.7	502.0	
137+00			5.6	502.1	
T.P.	5.793	506.364	7.093 ~~7.073~~	500.571	Recorded
BM#17			4.180	502.184	502.184
T.P.	4.180	506.364	5.793	500.571	
T.P.	3.531	504.102			
137+97			2.5	501.6	
138+00			3.5	500.6	
138+70			2.2	501.9	
138+73			3.2	500.9	
138+89			11.7	492.4	
139+00			7.3	496.8	

502.5 52 10⁰

502.5 52 10⁰

502.1 56 10⁰

502.1 56 10⁰

502.4 53 10⁰

502.6 51 10⁰

502.6 51 10⁰

501.8 59 10⁰

501.8 59 10⁰

501.6 61 10⁰

501.9 22 10⁰

501.8 23 10⁰

499.9 42 10⁰

499.3 48 10⁰

491.4 127 10⁰

496.3 78 10⁰

500.6 35 2⁰

501.6 25 2⁰

492.1 12⁰ 4⁰

490.8 133 92 Cistern

501.3 28 10⁰

501.5 26 10⁰

502.5 16 10²

502.2 14 10⁰

10⁸ on top

495.8 83 10⁰

Wed. Feb 10

Sta.	+	↑	−	Elev.
		504.102		
139+13			1.4	502.7
140+00			1.9	502.2
T.P.	2.983	505.376	1.709	502.393
140+57.1	P.O.T.		3.7	501.7
141+00			4.3	501.1
142+00			4.1	501.3
143+00			4.8	500.6
144+00			5.3	500.1
144+15			7.2	498.2
145+00			8.4	497.0
TP BM 143+90			6.802	498.574

B.M. 143+90				498.574
	3.558	502.132		
145+86			4.5	497.6
+88			5.1	497.0

(6)

℄

503.5	502.2
06/10	19/10
502.1	502.3
28/10	18/10
501.6	501.5
38/10	39/10
501.1	501.3
43/10	41/10
501.1	501.2
43/10	42/10
500.8	500.4
46/10	50/10
500.2	499.1
52/10	63/10
499.9	497.6
55/10	78/10
497.0	496.8
84/10	86/10

Nail in tree 30' R

497.4	497.0
47/10	51/10
497.3	497.2
48/10	49/10

Leach ⊼
McCarty Rod.
Reynolds "
Feb. 10, '26

Cool & cloudy

Sta.	+	⊼	−	Elev.						
		502.132								
147+00			5.8	496.3	$5^{7}/10^{o}$	496.4			$5^{9}/10^{o}$	496.2
148+00			6.1	496.0	$4^{5}/10^{o}$	497.6	$6^{6}/3^{o}$	495.5	$6^{7}/10^{o}$	495.4
+50 148+40			3.1	499.0	$3^{1}/10^{o}$	499.0			$4^{2}/10^{o}$	497.9
T.P. B.M. Nail in stump			3.113	499.019						
	3.275	502.294								
149+00			3.3	499.0	$3^{2}/10^{o}$	499.1			$3^{4}/10^{o}$	498.9
150+00			3.8	498.5	$3^{7}/10^{o}$	498.6			$3^{8}/10^{o}$	498.5
151+00			4.4	497.9	$4^{4}/10^{o}$	497.9			$4^{4}/10^{o}$	497.9
152+00			4.8	497.5	$5^{0}/10^{o}$	497.3			$4^{8}/10^{o}$	497.5
+57			4.9	497.4	$5^{1}/10^{o}$	497.2			$4^{7}/10^{o}$	497.6
+59.3			4.4	497.9	$4^{4}/10^{o}$	497.9			$4^{5}/10^{o}$	497.8
+60.7			5.8	496.5	$5^{9}/10^{o}$	496.4			$5^{9}/10^{o}$	496.4
+63.7			5.8	496.5	$5^{9}/10^{o}$	496.4			$5^{9}/10^{o}$	496.4
+64.7			4.8	~~497.4~~ 497.5	$4^{7}/10$	497.6			$4^{9}/10^{o}$	497.4

Sta.	+	↑	−	Elev.	
		502.294			
152+67.7			5.3	497.0	
153+00			5.6	496.7	
154+00			6.3	496.0	
T.P.			5.931	496.363	
	5.468	501.831			
B.M.			1.081	500.750	500.758 Recorded
				500.758	
	1.081	501.839			
155+00			6.3	495.5	
+44			7.1	494.7	
156+00			6.5	495.3	
157+00			7.0	494.8	
158+00			7.8	494.0	
159+00			7.8	494.0	
+74			7.9	493.9	
T.P.			7.465	494.374	
	2.686	497.060			

℄

(10)

$\frac{5\ 2}{10}$ 497.1 $\frac{5\ 6}{10}$ 496.7

$\frac{5\ 6}{10}$ 496.7 $\frac{5\ 7}{10}$ 496.6

$\frac{6\ 0}{10}$ 496.3 $\frac{6\ 2}{10}$ 496.1

$\frac{6\ 3}{10}$ 495.5 $\frac{6\ 2}{10}$ 495.6

$\frac{6\ 2}{10}$ 495.6 edge of 16" standpipe. $\frac{7\ 0}{1\ 6}$ 494.8 $\frac{6\ 5}{2\ 2}$ 495.3 Top of standpipe $\frac{6\ 5}{10}$ 495.3

$\frac{6\ 6}{10}$ 495.2 $\frac{6\ 8}{10}$ 495.0

$\frac{7\ 0}{10}$ 494.8 $\frac{6\ 7}{10}$ 495.1

$\frac{7\ 6}{10}$ 494.2 $\frac{7\ 5}{10}$ 494.3

$\frac{7\ 4}{10}$ 494.4 $\frac{7\ 9}{10}$ 493.9

$\frac{7\ 7}{10}$ 494.1 $\frac{7\ 6}{10}$ 494.2

Sta	+	↑	−	Elev.
		497.060		
159+77			3.5	493.6
160+00			3.9	493.2
161+00			4.1	493.0
162+00			4.2	492.9
163+00			4.7	492.4
164+00			5.2	491.9
165+00			5.3	491.8
165+15			5.4	491.7
166+00			5.1	492.0
T.P.			5.192	491.868
	13.022	504.890		
B.M #20			.281	504.609

Recorded 504.635

Note: run peg line up road - B.M. checks out O.K. This error will not change any H.I. between B.M's enough to change ground elevation.

℄

$\frac{3\,1}{10\,0}$ 493.4

$\frac{3\,8}{10\,0}$ 493.3

$\frac{4\,0}{10\,0}$ 493.1

$\frac{4\,2}{10\,0}$ 492.9

$\frac{4\,5}{10\,0}$ 492.6

$\frac{5\,2}{10\,0}$ 491.9

$\frac{5\,3}{10\,0}$ 491.8

$\frac{5\,2}{14\,3}$ 491.9 stand pipe

$\frac{5\,4}{10\,0}$ 491.7

$\frac{5\,5}{10\,0}$ 491.6

(11)

$\frac{3\,1}{10\,0}$ 493.4

$\frac{3\,8}{10\,0}$ 493.3

$\frac{4\,1}{10\,0}$ 493.0

$\frac{4\,3}{10\,0}$ 492.8

$\frac{4\,8}{10\,0}$ 492.3

$\frac{5\,3}{10\,0}$ 491.8

$\frac{5\,3}{10\,0}$ 491.8

$\frac{5\,5}{10\,0}$ 491.6

$\frac{5\,6}{10\,0}$ 491.5

Noon
McCarty x
Leach-rod
Reynolds-"

BM#20	0.651	505.286		504.635
	9.687	505.967	9.006	496.280
167+00			15.0	491.0 ~~490.0~~
168+00			15.4	490.6 ~~489.6~~
168+14.2			14.0	492.0 ~~491.0~~
168+24.2			11.6	494.4
168+34.2			9.7	496.3
168+44.2			10.0	496.0
168+53.0 =173+44.5			10.4	495.6
173+45.2			10.4	495.6
173+70.2			11.8	494.2
173+95.2			12.1	493.9
174+20.2			12.4	493.6 ~~494.3~~
174+45.2			12.2	493.8 ~~494.5~~

		⊙		
491.3				491.1
14.7/10.0 (494.0)	493.1	491.1		14.9/10.0 (491.0)
12.0/10.0 (497.7)	12.9/7.3	14.9/5.4	490.3	15.0/10.0 (490.4)
8.3/10.0 (499.1)	497.9	497.1	15.7/3.7 (490.7)	15.6/10.0 (490.0)
6.9/10.0 (500.8)	8.1/8.2	8.9/4.0 (497.1)	15.3/7.0	16.0/10.0 (490.9)
5.2/10.0 (502.4)		8.9/4.0 (496.6)	495.5	15.1/10.0 (491.7)
3.6/10.0 (502.5)		9.4/2.2	10.5/3.3 (494.9)	14.3/10.0 (492.0)
3.5/10.0 (502.5)			11.2/4.6 (494.9)	14.0/10.0 (492.0)
3.5/10.0 (501.5)	496.9 ~~497.9~~	495.2	11.2/4.6 (493.5)	14.0/10.0 (491.6)
4.5/10.0 (500.1)	9.1/3.0 (496.7)	10.8/2.0 (494.9)	12.5/6.7 (492.7)	14.4/10.0 (491.9)
5.9/10.0 (498.9)	9.3/5.0	11.1/0.7	13.3/2.4 (491.6)	14.1/10.0 (491.4)
7.3/10.0 (498.6)			14.4/4.6 (492.7) 491.3	14.6/10.0 (490.6)
7.4/10.0			13.3/2.3 14.7/4.6	15.4/10.0

Sta	+	℄	−	Elev.
		505.967		
174+70.2			12.6	493.4
174+95.2			11.9	494.1
175+20.2			12.2	493.8
TP	6.599	501.412	11.154	494.813
175+45.2			7.9	~~493.5~~ 493.6
175+59.6			7.8	493.6
176+00			8.2	493.2
177+00			8.7	492.7
BM#21			8.934	492.478 Recorded 492.472

Leach - ℄ 2:00 P.M.

B.M #21				492.472
	3.918	496.390		
178+00			6.2	490.2
+62.7			7.3	489.1
87.7			7.4	489.0
179+12.7			7.0	489.4

℄

498.8		490.6	490.6
72 / 10		154 / 85	154 / 10
498.1			490.4
79 / 10			156 / 10
499.0	494.9		490.3
70 / 10	111 / 32		157 / 10
~~499.2~~ 499.2	494.3 ⊙ 492.2		~~490.3~~ 490.3
22 / 10	71 / 20	92 / 50	106 / 10
~~499.5~~ 499.5			490.4
19 / 10			110 / 10
499.0	494.7	491.4	490.1
24 / 10	67 / 40	102 / 70	113 / 10
499.1		~~491.9~~ 490.9	490.0
23 / 10		105 / 68	114 / 10

26 / 10 493.8	51 / 65 491.3		79 / 10 488.5
51 / 10 491.3	63 / 80 490.1		84 / 10 488.0
40 / 10 492.4	60 / 70 490.4	72 / 65 488.7	87 / 10 487.7
26 / 20 493.8	57 / 55 490.7	72 / 70 488.5	87 / 10 487.7

Sta.	+	π	−	Elev.
		496.390 ✓		
179+37.7			6.9	489.5 ✓
+62.7			7.0	489.4 ✓
+87.7			7.1	489.3 ✓
180+12.7			7.6	488.8 ✓
+37.7			8.0	488.4 ✓
+62.7			8.2	488.2 ✓
+87.7			8.0	488.4 ✓
181+03.1			8.3	488.1 ✓
182+00			9.5	486.9 ✓
182+22.6			9.9	486.5 ✓
			ctr. 14" concrete pipe	
183+00			9.2	487.2 ✓
B.M. #22			5.024 ✓	491.366 ✓ Recorded. 491.366 ✓

℄

493.7 $\frac{2.7}{10.0}$ ✓	490.6 $\frac{5.8}{4.6}$ ✓	488.6 $\frac{7.8}{7.0}$ ✓	487.6 $\frac{8.8}{10.0}$ ✓		
493.1 $\frac{3.3}{10.0}$ ✓	490.9 $\frac{5.5}{6.0}$ ✓	487.5 $\frac{8.9}{10.0}$ ✓			
492.8 $\frac{3.6}{10.0}$ ✓	489.9 $\frac{6.5}{2.0}$ ✓	487.9 $\frac{8.5}{10.0}$ ✓			
491.7 $\frac{4.7}{10.0}$ ✓	490.9 $\frac{5.5}{9.0}$ ✓	490.0 $\frac{6.4}{5.5}$ ✓	489.4 $\frac{7.0}{4.2}$	488.1 $\frac{8.3}{8.5}$ ✓	487.2 $\frac{9.2}{10.0}$ ✓
489.7 $\frac{6.7}{10.0}$ ✓	487.7 $\frac{8.7}{7.0}$ ✓	486.8 $\frac{9.6}{7.6}$ ✓	486.5 $\frac{9.9}{10.0}$ ✓		
489.0 $\frac{7.4}{10.0}$ ✓	487.7 $\frac{8.7}{4.5}$	487.1 $\frac{9.3}{5.1}$ ✓	486.3 $\frac{10.1}{10.0}$ ✓		
489.2 $\frac{7.2}{10.0}$ ✓	487.7 $\frac{8.7}{4.0}$ ✓	487.0 $\frac{9.4}{5.0}$ ✓	486.2 $\frac{10.2}{10}$ ✓		
489.1 $\frac{7.3}{10.0}$ ✓	487.3 $\frac{9.1}{5.1}$ ✓	486.6 $\frac{9.8}{5.9}$ ✓	485.9 $\frac{10.5}{10}$ ✓		
487.5 $\frac{8.9}{10.0}$ ✓	486.5 $\frac{9.9}{8.0}$ ✓	486.2 $\frac{10.2}{10.0}$ ✓			
487.2 $\frac{9.2}{10.0}$ ✓	485.8 $\frac{10.6}{10.0}$ ✓				
488.6 $\frac{7.8}{10}$	486.7 486.6 $\frac{9.7}{5.4}$	486.0 $\frac{10.4}{7.5}$ ✓	487.1 $\frac{9.3}{10.0}$ ✓		

3 PM
McCarty-X
Leach-rod
Reynolds-"

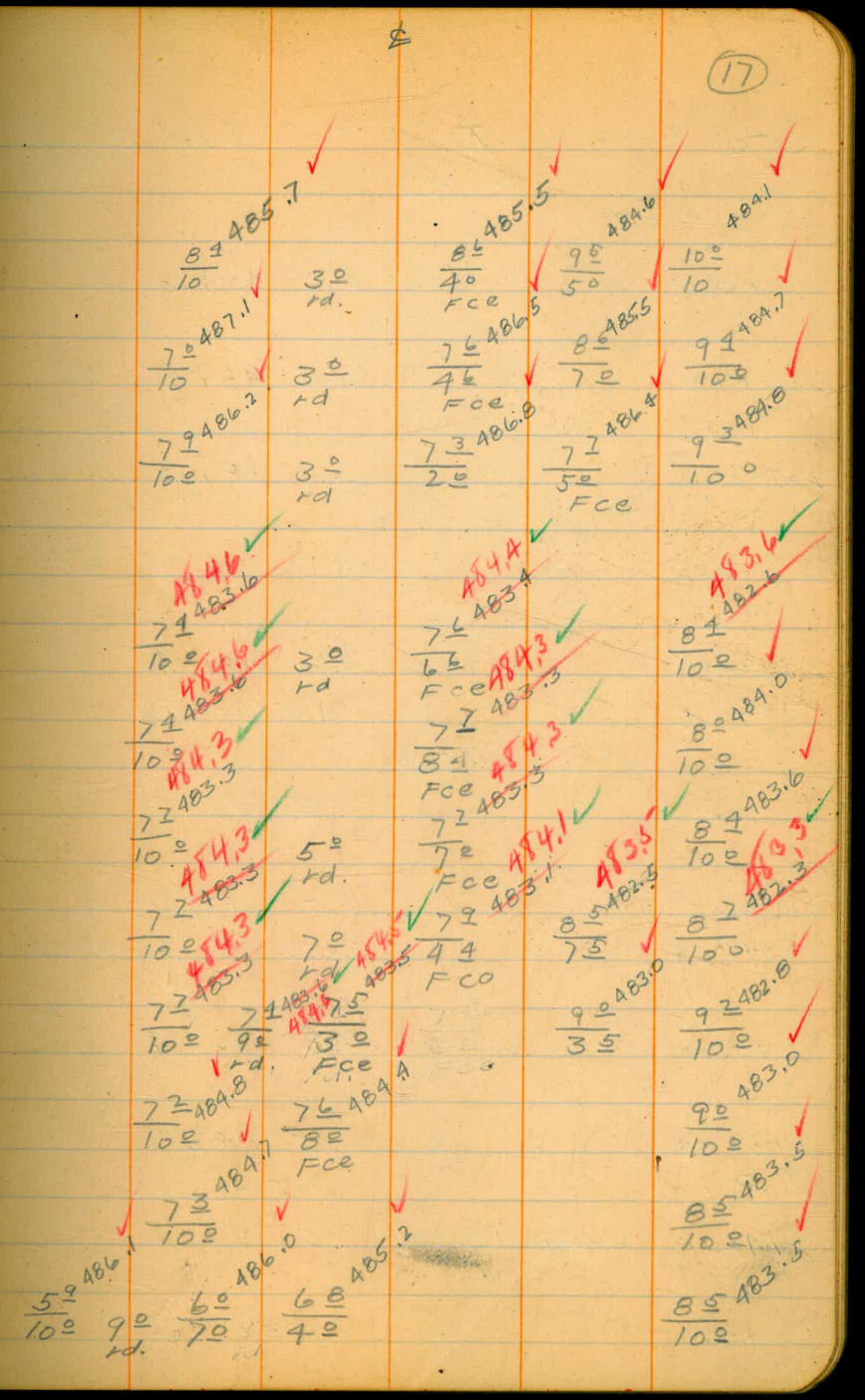
BM#22	1.985	493.351		491.366
184+00			6.9	486.5 ~~486.4~~
185+00			4.7	488.7 ~~488.6~~
185+83			5.3	488.1 ~~488.0~~
186+00			5.3	488.1 ~~488.0~~
187+00			5.6	487.8 ~~487.7~~
188+00			5.5	487.9 ~~487.8~~
189+00			1.2	492.2 ~~492.1~~
TP	9.726	497.652	5.425	487.926
189+55			4.2	493.5 ~~493.4~~
190+00			4.1	493.6 ~~493.5~~ ~~493.5~~
191+00			5.2	492.5 ~~492.4~~
192+00			5.6	492.1 ~~492.0~~
193+00			6.5	491.2 ~~491.1~~
TP				

Station	Left		℄		Right
BM#22	488.0 ~~487.9~~		487.0 ~~486.9~~		486.4 ~~486.3~~
184+00	5.4/10.0 489.1 ~~489.0~~	6.4/6.3			7.0/10.0 488.4 ~~488.3~~
185+00	4.3/10.0				5.0/10.0
185+83	4.7/10.0 488.7		5.0/7.3 488.4		5.6/10.0 487.8
186+00	4.8/10.0 488.6				6.0/10.0 487.4
187+00	5.4/10.0 488.0		6.1/5.0 487.3	7.8/8.4 485.6	8.1/10.0 485.3
188+00	5.0/10.0 488.4		5.2/3.5 488.2		6.0/10.0 487.4
189+00	0.7/10.0 492.7		1.5/5.4 491.9	2.0/6.4 491.4	2.4/10.0 491.0
189+55	3.5/10.0 494.1		4.1/4.0 493.6		5.0/10.0 492.7
190+00	3.4/10.0 494.3				4.6/10.0 493.1
191+00	4.3/10.0 493.4		4.7/7.6 493.0	5.2/8.6 492.5	5.5/10.0 492.2
192+00	4.8/10.0 492.9			5.7/8.7 492.0	6.1/10.0 491.6
193+00	5.9/10.0 491.8		6.9/5.7 490.8, 6.4/8.0 491.3		7.0/10.0 490.7

								¢		
		497.652								
TP	1.511	492.727	6.436	491.216						
194+00			3.1	489.6		2.5/10.0 490.2		3.9/6.4 488.8		3.7/10.0 489.0
195+00			5.0	487.7		5.0/10.0 487.7		4.7/8.4 488.0		5.2/10.0 487.5
195+63			7.0	485.7		6.9/10.0 485.8		6.7/0.7 486.0		6.0/10.0 486.7
196+00			7.6	485.1		7.3/10.0 485.4			7.9/9.0 484.8	8.3/10.0 484.4
197+00.			8.5	484.2		8.2/10.0 484.5		8.7/8.2 484.0		9.2/10.0 483.5
197+50			7.8	484.9		7.0/10.0 485.7				9.1/10.0 483.6
BM#24			1.838	490.889	Recorded 490.912					
198+00			5.3	487.4		4.1/10.0 488.6				6.7/10.0 486.0
198+20			3.6	489.1		2.9/10.0 489.8		3.7/4.0 489.0	5.4/9.0 487.3	5.5/10.0 487.2
198+75			2.7	490.0		1.9/10.0 490.8		2.8/4.3 489.9		4.1/10.0 488.6
199+00			2.9	489.8		2.3/10.0 490.1		3.2/6.7 489.5		4.1/10.0 488.6
200+00			6.2	486.5		5.9/10.0 486.8		6.5/5.7 486.2	7.7/8.4 485.0	7.9/10.0 489.8

Party - Leach T
Reynolds Rd
Todd

Sta.	+	T	−	Elev.	
B.M. #24				490.912	
	3.200	494.112			
201+00			8.6	485.5	
202+00			7.4	486.7	
203+00			7.7	486.4	Recorded.
B.M. #25			7.820	486.292	486.282
	5.680	491.962			
204+00			7.6	484.4	
+12.4			7.8	484.2	
+37.4			7.8	484.2	
+62.4			7.9	484.1	
+87.4			8.2	483.8	
205+12.4			8.4	483.6	
+37.4			7.8	484.2	
+62.4			7.1	~~484.9~~ ~~485.9~~ 484.9	



Sta	+	H	−	Elev.
		491.962		
+87.4			6.4	485.6 / 484.6
206+09.4			6.5	485.5 / 484.5
207+00			3.7	488.3 / 487.3
208+00			4.1	487.9 / 486.9
209+00			9.6	482.4 / 481.4
T.P.			7.435	484.527
	6.981	491.508		
210+00			11.8	479.7
211+00			10.5	481.0 Recorded.
B.M.#26			5.153	486.355 484.347
212+00			9.8	481.7
213+00			9.5	482.0
T.P.			7.875	483.633
214+00	2.654	486.287	4.5	481.8

℄

(18)

Fce on ℄

Fce on ℄

Fce

Fce

Fce

Fce

Fce

Sta.	+	⊼	−	Elev.
		486.287		
215+00			4.8	481.5 ✓
216+00			6.3	480.0 ✓
+21.2			6.6	479.7 ✓
+31.2			6.5	479.8 ✓
+41.2			6.5	479.8 ✓
+51.2			6.6	479.7 ✓
+61.2			6.5	479.8 ✓
+71.2			6.3	480.0 ✓
+81.2			6.2	480.1 ✓
+91.2			6.3	480.0 ✓
217+01.2			6.4	479.9 ✓
+11.2			6.5	479.8 ✓

℄

$\frac{4^{5}}{10^{0}}$ 481.8 ✓ — 6^{0} rd.
$\frac{6^{0}}{10^{0}}$ 480.3 ✓ — 6^{0} rd.
$\frac{6^{1}}{10^{0}}$ 480.2 ✓ — 4^{0} rd.
$\frac{6^{0}}{10^{0}}$ 480.3 ✓ — 3^{0} rd
$\frac{6^{0}}{10^{0}}$ 480.3 ✓ — 1^{0} rd.
$\frac{5^{9}}{10^{0}}$ 480.4 ✓
$\frac{5^{9}}{10^{0}}$ 480.4 ✓
$\frac{5^{8}}{10^{0}}$ 480.5 ✓
$\frac{5^{7}}{10^{0}}$ 480.6 ✓
$\frac{5^{8}}{10^{0}}$ 480.5 ✓
$\frac{6^{8}}{10^{0}}$ 479.5 ✓
$\frac{6^{1}}{10^{0}}$ 480.2

Rd.

$\frac{5^{0}}{9^{0}}$ 481.3 ✓
$\frac{7^{0}}{9^{0}}$ 479.3 ✓
$\frac{7^{1}}{9^{0}}$ 479.2 ✓
✓
$\frac{7^{4}}{8^{5}}$ 478.9 ✓
$\frac{7^{3}}{7^{0}}$ 479.0 ✓
$\frac{8^{0}}{8^{0}}$ Fce 478.3

$\frac{6^{2}}{10^{0}}$ 480.1 ✓
$\frac{7^{3}}{10^{0}}$ 479.0 ✓
$\frac{7^{4}}{10^{0}}$ 478.9 ✓
$\frac{7^{7}}{10^{0}}$ 478.6 ✓
$\frac{8^{2}}{10^{0}}$ 478.1 ✓
$\frac{8^{4}}{10^{0}}$ 477.9 ✓
$\frac{8^{7}}{10^{0}}$ 477.6 ✓
$\frac{7^{9}}{10^{0}}$ Fce 478.4 ✓
$\frac{6^{6}}{10^{0}}$ 479.7 ✓
$\frac{6^{3}}{10^{0}}$ 480.0 ✓
$\frac{6^{7}}{10^{0}}$ 479.6 ✓
$\frac{7^{1}}{10^{0}}$ ~~487.2~~ 479.2

Sta.	+	I	−	Elev.	
		486.287			
217+21.2			6.6	479.7	
+31.2			6.7	479.6	
+41.2			6.8	479.5	
+51.2			6.9	479.4	
+62.2			7.0	479.3	
218+00			7.2	479.1	
219+00			7.6	478.7	
B.M. #27			5.477	480.810	Recorded 480.800
	4.713	485.523			
220+00			5.5	480.0	
221+00			5.2	480.3	
	4.810	485.610			
+41.8			5.1	480.5	
+51.8			5.0	480.6	
+61.8			5.0	481.6	

Rd.

$\frac{6^2}{10^0}$ 480.1 $\frac{6^4}{10^0}$ 479.9 $\frac{6^5}{10^0}$ 479.8 $\frac{6^7}{10^0}$ 479.6 $\frac{6^2}{10^0}$ 479.6 $\frac{6^9}{10^0}$ 479.4 $\frac{7^2}{10^0}$ 479.1

$\frac{5^4}{10^0}$ 480.1 $\frac{4^8}{10^0}$ 480.7 $\frac{4^8}{10^0}$ 480.8 $\frac{4^7}{10^0}$ 480.9 $\frac{4^7}{10^0}$ 480.9

$\frac{7^3}{7^0}$ 479.0 $\frac{7^6}{8^0}$ 478.7 $\frac{7^5}{5^0}$ 478.8 $\frac{7^9}{3^0}$ 478.4 $\frac{10^4}{8^0}$ 475.9

8° rd.

$\frac{5^6}{3^0}$ 479.9 $\frac{5^1}{3^0}$ 480.4 $\frac{5^0}{3^0}$ 480.6 $\frac{4^9}{1^0}$ 480.7 $\frac{4^9}{1^0}$ 480.7

5° rd. 3° rd. 5° rd. 5° rd. 5° rd.

$\frac{9^1}{6^0}$ 476.1 $\frac{9^2}{4^5}$ 476.4 $\frac{9^0}{6^0}$ 476.6 $\frac{9^0}{6^0}$ 476.6

$\frac{7^2}{10^0}$ 478.6 $\frac{7^2}{10^0}$ 479.1 $\frac{7^1}{10^0}$ 479.2 $\frac{8^4}{10^0}$ 477.9 $\frac{8^2}{10^0}$ 478.1 $\frac{9^5}{10^0}$ 476.8 $\frac{10^5}{10^0}$ 475.8

$\frac{10^1}{10^0}$ 475.9 $\frac{9^2}{10^0}$ 476.3 $\frac{10^8}{10^0}$ 474.8 $\frac{9^8}{10^0}$ 475.8 $\frac{9^8}{10^0}$ 475.8

Sta	+	Π 485.610	−	Elev.
221+71.8			4.7	480.9
+81.8			4.7	480.9
+91.8			4.6	481.0
222+01.8			4.7	480.9
+11.8			4.7	480.9
+21.8			4.8	480.8
+31.8			5.2	480.4
+41.8			6.2	479.4
+51.8			6.0	479.6
+61.8			6.3	479.3
+65.4			6.4	479.2
223+00			7.7	477.9

℄

	481.0	476.9	476.2
	4 6 / 10 = 481.1	8 2 / 6 =	9 4 / 10 =
6 = rd.	4 6 / 12		
	481.2	477.2	476.2
7 = rd.	4 4 / 2 = 480.9	8 4 / 5 5	9 4 / 10 =
	481.1	477.5	476.2
7 = rd.	4 7 / 10 = 480.9	8 1 / 4 = 476.9	9 4 / 10 = 475.7
7 = rd.	4 7 / 10 = 476.7	8 2 / 4 =	9 9 / 10 = 474.9
8 = rd.	8 9 / 4 7	477.4	10 7 / 10 = 475.9
8 = rd.	8 2 / 3 = 476.9		9 7 / 10 = 476.3
9 = rd.	8 2 / 3 3 / 476.8		9 3 / 10 = 476.3
8 = rd.	8 8 / 4 = 477.1		9 3 / 10 = 476.5
6 = rd.	8 5 / 4 = 479.2	476.9	9 1 / 10 = 476.6
8 = rd.	6 4 / 2 = 479.2	8 7 / 6 = 476.7	9 2 / 10 = 476.6
7 = rd.	6 4 / 2 4	8 2 / 7 2	9 2 / 10 = 477.1
℄ rd.			8 5 / 10 =

Sta.	+	℄	−	Elev.
		485.610		
224+00			9.7	475.9
+90.4			8.2	477.4
225+00.4			7.8	477.8
+10.4			7.4	478.2
+20.4			6.8	478.8
+30.4			8.5	477.1
+40.4			9.0	476.6
+50.4			6.7	478.9
+60.4			6.7	478.9
+70.4			7.6	478.0
+80.4			8.3	477.3
+85.4			8.2	477.4

475.9

9 2 / 10 0 — 477.4

8 0 / 10 0 — 478.0

7 6 / 10 0 — 478.5

7 1 / 10 0 — 479.1 — 478.5

6 5 / 10 0 — 479.4

6 2 / 10 0 — 6 2 / 3 4 — 479.4

5 9 / 10 0 — 480.0

5 6 / 10 0 — 480.3

4 7 / 10 0 — 481.6

4 1 / 10 0 — 482.3

3 3 / 10 0 — 482.4

3 2 / 10 0

℄

475.4 — 474.4

1 0 / Ld. — 10 2 / 8 6 — 477.4 — 476.1

7 0 / Ld. — 8 2 / 5 2 — 9 5 / 7 5 Fce — 477.5 — 476.9

7 0 / Ld. — 7 8 / 5 5 — 8 2 / 7 0 — 477.6

7 0 / Ld. — 8 1 / 5 0 Fce — 477.3 — 476.3

9 0 / Ld. — 8 3 / 2 3 Fce

1 0 / Fce — 478.9

6 2 / 5 2 Fce

480.2

5 4 / 5 5 — 476.0

7 4 / 3 0 — 478.2

7 4 / 4 0

22

475.1 — 475.4

10 5 / 10 0 — 475.4

10 2 / 10 0 — 474.8

10 8 / 10 0 — 474.6

11 0 / 10 0 — 474.3

11 3 / 10 0 — 474.2

11 4 / 10 0 — 474.1

10 9 / 10 0 — 474.9

7 2 / 10 0 — 477.1

7 9 / 10 0 — 477.2

8 4 / 10 0 — 476.6

9 0 / 10 0 — 476.5

9 1 / 10 0

Sta.	+	⊼	−	Elev.	
		485.610			
226+00			7.4	478.2	
T.P.			0.823	484.787	
	12.318	497.105			
B.M.#28			10.590	486.515	Recorded 486.482
	10.593	497.075			
Feb. 24.					
227+00			12.5	484.6	
+72.8			4.8	492.3	
+82.8			4.1	493.0	
T.P.			0.672	496.403	
	5.732	502.135			
+92.8			9.4	492.7	
228+02.8			9.2	492.9	
+12.8			9.1	493.0	
+22.8			9.3	~~493.8~~ 492.8	
+32.8			9.0	493.1	
+42.8			9.2	492.9	

8

(23)

← Ran peg line and checked my elevation within .009 (486.506)

18" Tree

Sta.	+	℄	−	Elev.
		502.135		
T.P. sta 228+75			.609	501.526
	1.443	502.969		
228+52.8			10.7	492.3 / ~~492.2~~
+62.8			11.1	491.9 / ~~491.8~~
+73.5			11.3	491.7 / ~~491.6~~
229+00			11.2	491.8 / ~~491.7~~
+50				
230+00			13.0	490.0 / ~~489.9~~
T.P.	1.43	500.94	3.460	499.509
230+92.5				
231+00			5.6	493.3
+33.4			1.5	499.4
+43.4			1.0	499.9
+53.4			1.0	499.5
+63.4			1.0	499.9
+73.4			1.2	499.7

498.5 / ~~498.4~~			487.8 / ~~487.7~~
4⁵/10⁰ 498.3 / ~~498.2~~			15²/10⁰ 487.7 / ~~487.6~~
4⁷/10⁰ 498.0 / ~~497.9~~			15⁸/10⁰ 486.9 / ~~486.8~~
5⁰/10⁰ 498.1 / ~~498.0~~	12" Tree 4⁵		16¹/10⁰ 486.7 / ~~486.6~~
4⁹/10⁰ 495.6			17⁰/10⁰ 486.0 / ~~485.9~~
"A" 3³/10⁰ 497.6 / ~~497.5~~	10" Tree 2⁰		15⁹/10⁰ "A" 487.6 / ~~487.5~~
A 1³/10⁰ 499.6	A 1⁵/5⁵ 499.4	10" Tree 4⁵	A 12⁰/10⁰ 488.9
1⁵/10⁰ 499.4 / ~~499.3~~		8⁰ rd.	5⁻²/5⁰ 495.7 / 496.9 / 6⁵/10⁰ 494.4
1⁴/10⁰ 499.5		7⁰ rd.	4⁰/6⁰ 500.3 / 498.1 / 4³/10⁰ 496.2
1⁴/10⁰ 499.5 / ~~499.4~~		7⁰ rd.	0⁶/25 / 2⁸/50 / 4²/10⁰ 496.7
1⁵/10⁰ 499.4		7⁰	0⁶/3⁰ 500.1 / 497.8 / 3¹/8⁰ 3⁵/10⁰ 497.4
1⁷/10⁰ 499.2		7⁰ rd	0⁸/3⁸ 3⁸/10⁰ 497.1

Party
Leach π
Reynolds-Rod
Todd -"

Sta.	+	π	−	Elev.
				499.509
	1.734	501.243		
Feb. 25 231+83.4			1.6	499.6
+93.4			1.8	499.4
232+03.4			1.9	499.3
+08.4			2.0	499.2
+23.4			2.4	498.8
+47.4			3.0	498.2
+72.4			4.8	496.4
+97.4			6.4	494.8
233+22.4			7.5	493.7
+47.4			9.0	492.2
+73.4			9.3	491.9
T.P.			9.893	491.350
	3.785	495.135		

499.1		499.9	496.4
2.1 / 10.0	6.0 / rd	1.3 / 4.0	4.8 / 10.0
498.9		500.0	495.7
2.3 / 10.0	6.0 / rd	1.2 / 4.0	5.5 / 10.0
498.7		498.6	~~494.5~~ 494.9
2.5 / 10.0	6.0 / rd	2.6 / 4.0	6.3 / 10.0
498.6		499.2	495.0
2.6 / 10.0	6.0 / rd.	2.0 / 4.0	6.2 / 10.0
498.4		498.6	494.7
2.8 / 10.0	7.0 / rd	2.6 / 4.0	7.0 / 10.0
497.8		498.2	493.5
3.4 / 10.0	8.0 / rd	3.0 / 2.0	7.7 / 10.0
496.8		492.7	491.7
4.4 / 10.0 rd.		9.0 / 7.0	9.5 / 10.0
496.1	496.2	492.6	490.4
5.1 / 10.0 rd.	5.0 / 2.0	8.6 / 4.0	10.8 / 10.0
~~495.~~ 495.2	495.6	490.5	488.6
6.0 / 10.0	5.6 / 3.0	10.7 / 5.0	12.6 / 10.0
494.1	494.7	489.8	488.0
7.1 / 10.0	7.0 / 2.0	11.4 / 4.0	13.2 / 10.0
493.4	~~494.0~~ 493.0	487.9	487.1
2.8 / 10.0	8.2 / 2.0	13.3 / 5.0	14.1 / 10.0

Sta.	+	HI	−	Elev
		495.135		
233+97.4			4.1	491.0
234+18.8			3.8	491.3 ~~491.4~~
+43.8			4.4	490.7
+68.8			5.9	489.2
+93.8			6.5	488.6
235+18.8			8.4	486.7
+43.8			8.4	486.7
+69.8			8.7	486.4
236+00			8.6	486.5
237+00			12.1	483.0
+10.3			11.9	483.2
B.M.#29			10.022	485.113 485.125
	4.365	489.490		

℄

493.0
2.1 / 10.0
492.9
2.2 / 10.0
492.7
2.4 / 10.0
492.5
2.6 / 10.0
492.2
2.9 / 10.0
491.9
3.2 / 10.0
491.5
3.6 / 10.0
490.6
4.5 / 10.0
490.2
4.9 / 10.0
484.2
10.9 / 10.0
484.1
11.0 / 10.0
484.1
6.0 / Ld
7.0 / Ld.

492.5
2.6 / 3.0
492.8
2.3 / 2.0
2.7 / 3.0
492.4
2.7 / 6.0
492.3
2.8 / 6.0
492.0
3.1 / 8.0
491.4
3.7 / 8.0
483.9
11.2 / 3.0
Ld
Power pole
4.0

485.7
9.4 / 7.0
492.4
488.0 ~~488.0~~
7.1 / 2.0
484.5
10.6 / 7.0
485.3
9.8 / 4.0
487.7
7.4 / 6.0

485.1
10.0 / 10.0
484.7
10.4 / 10.0
484.8
10.3 / 10.0
485.0
10.1 / 10.0
484.2
10.9 / 10.0
483.9
11.2 / 10.0
483.7
11.4 / 10.0
484.4
10.7 / 10.0
483.7
11.4 / 10.0
480.3
14.8 / 10.0
481.4
13.2 / 10.0

Sta.	+	HI	−	Elev.
	4.46	(489.58)		
237+20.3			6.1	483.5
+30.3			5.8	483.8
+40.3			5.7	483.9
+50.3			5.7	483.9
+60.3			5.7	483.9
+70.3			5.7	483.5
80.3			5.9	483.7
+90.3			6.1	483.5
238+00.3			6.4	483.2
+10.3			6.6	483.0
+18.2			6.7	482.9
239+00			11.1	478.5

		℄		
484.1 5.5/10.0	4.0/rd.			482.4 7.2/10.0
484.1 5.5/10.0	4.0/rd.			482.8 6.8/10.0
484.2 5.4/10.0	3.0/rd.			483.0 6.6/10.0
484.2 5.4/10.0	3.0/rd.			483.1 6.5/10.0
484.2 5.4/10.0		rd.		483.1 6.5/10.0
484.4 5.2/10.0		rd.		483.9 5.7/10.0
484.4 5.2/10.0		rd	484.0 5.6/6.0	483.5 6.1/10.0
484.1 5.5/10.0		rd	483.7 5.9/5.0	483.2 6.4/10.0
483.7 5.9/10.0		rd	483.3 6.3/5.0	482.9 6.7/10.0
483.5 6.1/10.0		rd.		482.1 7.5/10.0
483.4 6.2/10.0	480.5	479.6 rd		481.6 8.0/10.0
480.6 9.0/10.0 rd.	9.7/7.0	10.0/4.4		477.0 12.6/10.0

Sta.	+	HI	−	Elev.
		489.58		
239+69.6			12.7	476.9
+94.6			13.0	476.6
240+19.6			14.5	475.1
T.P.		489.490	10.783	478.707
	2.550	481.257		
+44.6			6.1	475.2
+69.6			7.4	473.9
+99.6			8.7	472.6
241+19.6			10.2	471.1
+30.3			10.8	470.5
242+00			13.2	468.1
T.P.			12.705	468.552
	1.968	470.520		
243+00			4.2	466.3
244+00			5.1	465.4

Left	Elev.			℄		Elev.	Right	Elev.
11.7/10.0	477.9, 476.9	5.0/rd.			14.0/4.0	475.6	14.6/10.0	475.0, 475.5
12.7/10.0	475.8	3.0/rd.				475.9, 475.4	14.1/10.0	475.1
13.8/10.0				rd.	13.7/5.0		14.2/7.0, 14.5/10.0	
6.7/10.0	474.6		8.0/rd		2.0/rd		6.6/10.0	474.7
7.7/10.0	473.6		7.0/rd		3.0/rd		8.0/10.0	473.3
9.0/10.0	472.3		8.0/rd		3.0/rd.		9.0/10.0	472.3
10.2/10.0 rd.	471.1				2.0/rd.		10.2/10.0	471.1
10.8/10.0 rd	470.5				2.0/rd.		11.2/10.0	470.1
13.3/10.0 rd	468.0				2.0/rd.		13.6/10.0	467.7
4.3/10.0	466.2				1.0/rd.		4.6/10.0	465.9
4.8/10.0	465.7			rd			5.8/10.0	464.7

	+	HI	−	Elev.	
		470.520			
245+00			5.2	465.3	
+02.3			5.3	465.2	
+27.3			5.2	465.3	
+52.3			5.1	465.4	Recorded
B.M. #30			4.666	465.854	465.854
+	4.902	470.756			
+77.3			5.0	465.8	
246+02.3			4.7	466.1	
+24.4			4.5	466.3	
247+00			4.3	~~466.4~~ 466.5	
+11			4.9	466.4	
+36.8			4.7	466.1	
+61.8			5.0	465.8	
+86.8			5.2	465.6	

465.5 5.0/10.0	1.0/rd.			464.3 6.2/10.0
465.5 5.0/10.0	2.0/rd.		464.6	464.6 6.5/10.0
465.7 4.8/10.0	2.0/rd.		465.3 5.9/8.0	463.9 6.6/10.0
466.0 4.5/10.0	3.0/rd.	5.2/5.0	464.2 6.3/9.0 Fce	463.9 6.6/10.0
466.3				464.6
4.3/10.0	2.0/rd			6.2/10.0
466.6 4.2/10.0	4.0/rd.	466.3	467.1	464.4 6.4/10.0
466.7 4.1/10.0 ~~466.7~~ 466.9	6.0/rd.	4.5/2.0	3.7/4.0 6.6/6.0	464.2 465.9 4.9/8.0 465.8 5.0/10.0
3.9/10.0	rd.	466.0 4.8/5.0	467.3 3.5/7.7	467.1 3.7/10.0
466.8 4.0/10.0	rd.	466.1 4.7/6.4	466.6 4.2/7.5	466.5 4.3/10.0
466.4 4.4/10.0	rd.	466.1 4.7/8.8		465.8 5.0/10.0
466.0 4.8/10.0	rd.	465.6		465.0 5.8/10.0
465.8 5.0/10.0		5.2/7.0		464.1 6.7/10.0

	+	T	−	Elev.
		470.756		
248+01.8			5.5	465.3
+26.8			5.8	465.0
+61.8			6.1	464.7
+77.6			6.3	464.5
249+00			6.6	464.2
250+00			7.6	463.2
T.P.			5.330	465.426
	2.201	467.627		462.8
251+00			4.8	462.9 462.6
BM #31			6.301	461.326 461.347
	8.023	469.370		
252+00			7.2	462.2
253+00			6.3	463.1
254+00			5.7	463.7
255+00			3.4	466.0

Ran Peg line and checked my elev. To .008 (461.334)

469.370

256+00		2.6	466.8
+01.7		2.6	466.8
+11.7		2.5	466.9
+21.7		2.6	466.8
+31.7	on Boulder	2.5	466.9
+41.7		2.9	466.5
+51.7		1.9	467.5
+61.7		2.5	466.9
+71.7		4.9	465.0
+81.7		5.3	464.1
+91.7		5.2	464.2
257+01.7		4.8	464.6

	+	℄	−	Elev.
		469.370		
+11.7			4.6	464.8
+21.7			4.6	464.8
257+31.9				
257+25.9			4.9	464.5
			5.016	464.354
	3.339	467.693		462.123 Recorded
B.M. #32,			5.570	463.123 463.139
258+00			3.9	463.8
259+00			5.6	462.1
+78.1			7.0	460.7
B.M. #32				463.139
	2.089	465.218		
259+86.1			4.7	460.5
+96.1			4.7	460.5
260+06.1			4.6	460.6
+16.1			4.6	460.6
+26.1			4.6	460.6

466.0 463.7 463.0 462.4

3 4 / 10 0 — 3 7 / 1 6 — 0 5 FCE — 6 4 / 5 0 — 7 0 / 10 0

465.9 465.7 467.1

3 5 / 10 0 — 3 7 / 3 9 — 0 5 FCE — 7 3 / 9 0 — 7 3 / 10 0

462.8

465.7 465.5

3 7 / 10 0 — 3 9 / 3 0 — 0 5 FCE — 6 6 / 4 5 — 7 1 / 10 0

462.3

0 5 FCE

463.9 463.5 459.6 459.7

3 8 / 10 0 — 3 9 / 1 0 — 6 0 FCE — 7 9 / 7 0 — 8 0 / 10 0

5 0 Ld.

462.4

5 1 / 10 0

461.9

5 8 / 10 0

460.6 Ld. 460.5

467.7

0 0 / 2 0 — 7 1 / 1 5 — 5 0 Ld. — 6 8 / 10 0

460.9

463.0 460.8

1 0 0 / 7 0 — 4 6 / 4 0 — 2 0 Ld. — 4 3 / 10 0

to

465.2 460.7 460.9

0 0 / 5 0 — 4 5 / 3 0 — 2 0 Ld. — 4 3 / 10 0

460.8

465.2 460.6

0 0 / 4 0 — 4 3 / 3 5 Ld. — 4 9 / 10 0

465.2 460.6

0 0 / 6 3 — 4 6 / 4 0 Ld. — 4 9 / 10 0

465.2 460.8

0 0 / 8 0 — 4 9 / 5 5 Ld. — 4 9 / 10 0

	+	π	−	Elev.
		465.218		
260+36.1			4.6	460.6
262+45.8 = 260+45.0			4.7	460.5
263+00			4.9	460.3
264+00			5.3	459.9
265+00			4.4	460.8
266+00			6.7	458.5
T.P.			6.810	458.408
	4.378	462.786		
267+00			4.8	458.0
268+00			4.6	458.2
269+00			5.3	457.5
270+00			5.5	457.3
271+00			6.5	456.3

℄ 460.7

	0.0 / 8.0	4.5 / 5.0 rd		460.8 4.4 / 10.0
	0.0 / 6.0	4.3 / 5.0 rd		4.5 / 10.0
	0.0 / 2.2		5.0 / rd.	4.7 / 10.0
	0.0 / 3.3	4.6 / 13	3.0 / rd.	5.2 / 10.0
4.8 / 10.0		3.0 / rd.		460.1 5.1 / 10.0
6.9 / 10.0		8.0 / rd		6.5 / 10.0
4.6 / 10.0			6.0 / rd	5.6 / 10.0
4.9 / 10.0 rd.			7.0 / rd.	4.9 / 10.0
	0.0 / 7.0	5.5 / 3.5		5.1 / 10.0 15.0 / rd.
2.1 / 10.0	5.7 / 6.0	rd.		5.3 / 10.0
	0.0 / 7.0	6.3 / 5.0 rd.		6.4 / 10.0

		462.786		
271+66.4			7.8	455.0
+91.4			8.0	454.8
272+16.4			8.4	454.4
T.P.			5.600	457.186
	1.703	458.889		
+41.9			4.8	454.1
+66.4			5.0	453.9
+91.4			5.4	453.5
273+16.4			5.7	453.2
273+41.4			5.6	453.3
+96.2			5.7	453.2
274+00			5.7	453.1
B.M. #33			3.058	455.831

Recorded 455.815

454.1

Party -
Leach T
Reynolds-Rod
Todd
March 6, 1926

Cloudy & Warm

Sta:	+	T	-	Elev.
B.M. # 33				455.815
	9.715	465.530		
274+67.3			12.2	453.3
+92.3			12.1	453.4
275+17.3			11.4	454.1
+42.3			11.6	453.9
+67.3			11.4	454.1
+92.3			11.4	454.1
276+17.3			11.7	453.8
+47.3			12.4	453.1
277+00			13.1	452.4
+37			13.9	451.6
+55			9.8	455.7
278+00			10.3	453.2

Sta.	+	$\overline{\wedge}$	−	Elev.
		465.530		
278+63.5			9.0	456.5
+65.5			13.4	452.1
+88.5			13.4	452.1
T.P. Rock in road.			11.992	453.538
	5.246	458.784		
279+13.5			6.1	452.7
+38.5			5.7	453.1
+44.3			5.7	453.1
280+00			5.3	453.5
281+00			5.0	453.8
+26.2			5.0	453.8
+51.2			5.0	453.8
+76.2			4.9	453.9
282+01.2			5.0	453.8

		℄		
461.5		451.9		452.4
$\frac{3^7}{10^0}$ 461.3	458.5	$\frac{13^6}{1^0}$	$\frac{5^0}{rd}$	$\frac{13^1}{10^0}$ 452.4
$\frac{4^2}{10^0}$ 461.7	$\frac{7^0}{3^0}$ 459.3	$\frac{5^0}{rd.}$		$\frac{13^1}{10^0}$ 452.9
$\frac{3^8}{10^0}$ 458.8	$\frac{6^2}{4^0}$ 452.5	$\frac{2^0}{rd.}$		$\frac{12^6}{10^0}$ 453.5
$\frac{0^0}{7^0}$ Bank- 458.8	$\frac{6^3}{5^0}$ 452.9	rd	Rd.	$\frac{5^3}{10^0}$ 453.7
$\frac{0^0}{8^0}$ 458.8	$\frac{5^9}{7^0}$ 453.2			$\frac{5^1}{10^0}$ 453.7
$\frac{0^0}{7^0}$ 458.8	$\frac{5^6}{7^0}$ 453.5			$\frac{5^1}{10^0}$ 454.0
$\frac{0^0}{8^0}$ 455.7	$\frac{5^3}{6^0}$ 453.5	rd		$\frac{4^8}{10^0}$ 454.1
$\frac{3^1}{10^0}$ 453.5 $\frac{5^2}{9^0}$		$\frac{2^0}{rd.}$		$\frac{4^7}{10^0}$ 453.8
$\frac{5^3}{10^0}$ 453.3		$\frac{5^0}{rd}$	$\frac{7^0}{rd.}$	$\frac{5^9}{10^0}$ 453.6
$\frac{5^3}{10^0}$ 453.5		$\frac{7^0}{rd.}$	$\frac{10^0}{rd.}$	$\frac{5^2}{10^0}$ 453.8
$\frac{6^2}{10^0}$ 453.4		$\frac{6^0}{rd.}$		$\frac{5^0}{10^0}$ rd 453.9
$\frac{5^4}{10^0}$		$\frac{6^0}{rd.}$		$\frac{4^9}{10^0}$ rd

Sta	+	⊼	−	Elev.
		458.784		
282+26.2			4.9	453.9
+51.2			4.9	453.9
+76.1			5.0	453.8
283+00			4.7	454.1
T.P.			1.875	456.909
	8.325	465.234		
+80.9			9.6	455.6
284+05.9			8.6	456.6
+30.9			8.0	457.2
+55.9			8.3	456.9
284+80.9			8.6	456.6
285+05.9			9.1	456.1
+30.9			9.8	455.4
+55.9			10.3	454.9

℄

457.3 1.5/10.0	453.6 5.2/9.0	5.0 rd.		454.1 4.7/10.0 rd.
457.9 0.9/10.0	453.5 5.3/6.0	4.0 rd		454.3 4.5/10.0
458.8 0.0/5.5	453.9 4.9/1.5	3.0 rd.		454.4 4.4/10.0
458.1 0.0/4.0		4.0 rd.		454.5 4.3/10.0
456.7 8.5/10.0	456.3 8.9/4.0	5.0 rd.		456.2 9.0/10.0
458.3 6.9/10.0	457.0 8.2/4.0	456.5 8.7/3.0	3.0 rd	456.8 8.4/10.0
458.3 6.9/10.0	457.1 8.1/5.0	(4) rd.		456.9 8.3/10.0
457.0 8.2/10.0		(4) rd		456.3 8.9/10.0
456.5 8.7/10.0		(4) rd		456.2 9.0/10.0
459.1 6.1/10.0	456.7 9.5/4.0	(4) rd		456.2 9.0/10.0
462.3 2.9/10.0	460.9 4.3/7.0	455.3 9.9/2.0	3.0 rd	456.0 9.2/10.0
461.5 3.4/10.0	460.5 4.7/6.0	455.0 10.2/1.0	3.0	455.7 9.5/10.0

Sta.	+	T	−	Elev.						
		465.234								
286+00			10.2	455.0	461.4 2.8/10.0	461.4 3.6/7.0	454.9 10.3/2.0	2.0 rd.		455.6 9.6/10.0
287+00			11.1	454.1	462.4 2.8/10.0	462.1 3.1/9.0	454.0 11.2/2.0	2.0 rd.		454.6 10.6/10.0
288+00			12.9	452.3	460.6 4.6/10.0	459.1 6.1/7.0	453.2 12.0/2.0	3.0 rd.		452.6 12.6/10.0
+05.9			12.9	452.3	460.3 4.9/10.0	459.2 6.0/8.0	453.3 11.9/4.0	4.0 rd.		452.5 12.7/10.0
+30.9			13.9	451.3	458.9 6.3/10.0	458.5 6.7/9.0	451.5 13.7/1.0	3.0 rd.		451.9 13.3/10.0
+55.9			13.7	451.5	457.8 7.4/10.0		456.2 9.0/4.0	450.9 14.3/1.0	4.0 rd.	451.4 13.8/10.0
+62.8			13.3	451.9	457.8 7.4/10.0		456.3 8.9/3.0	450.8 14.4/1.0	6.0 rd.	451.2 14.0/10.0
289+00			11.9	453.3	453.3 11.9/10.0		454.0 11.2/4.0		7.0 rd	450.5 14.7/10.0
				456.909						
	1.433	458.342								
B.M. # 34			11.750	446.592 446.620 Recorded.						
				446.620						
	10.667	457.287								
290+00			6.2	451.1	454.1 3.2/10.0		452.6 4.7/3.5	448.6 8.7/3.0	5.0 rd	448.9 8.4/10.0
+62			9.3	448.0	452.6 4.2/10.0	450.0 7.3/3.0	448.4 8.9/1.5	3.0 rd		448.5 8.8/10.0

Sta.	+	⊼	−	Elev.
		457.287		
291+00			9.1	448.2
292+00			9.6	447.7
T.P. Rock in road.			9.620	447.667
	7.140	454.807		
293+00			7.3	447.5
294+00			5.9	448.9
+30.6			5.4	449.4
+55.6			5.3	449.5
+80.6			5.2	449.6
295+05.6			5.3	449.5
+30.6			5.2	449.6
+55.6			5.5	449.3
+66.6			6.0	448.8
296+00			7.1	447.7

				℄		
449.3 8.0/10.0				3.0 rd.		448.3 9.0/10.0
452.2 5.1/10.0			450.5 6.8/2.5	3.0 rd		447.8 9.5/10.0
454.2 0.6/10.0	452.1 2.7/4.5	448.1 6.7/2.0	447.6 7.2/1.5	2.0 rd		447.8 7.0/10.0
453.0 1.8/10.0	450.4 4.1/3.0		448.8 6.0/2.0	2.0 rd		449.3 5.5/10.0
451.7 3.1/10.0	450.2 4.6/3.0		449.3 5.5/1.5	2.0 rd		449.6 5.2/10.0
450.4 4.4/10.0				2.0 rd.		449.6 5.2/10.0
450.9 3.9/10.0		450.0 4.8/1.1	449.7 5.1/1.0	4.0 rd.		449.8 5.0/10.0
452.1 2.7/10.0	451.8 3.0/7.0	450.0 4.8/0.5	449.6 5.2/0.2	5.0 rd.		449.7 5.1/10.0
451.5 3.2/10.0				4.0 rd		449.5 5.3/10.0
451.8 3.0/10.0			449.3 5.5/0.4	448.7 6.1/0.3	5.0 rd.	449.2 5.6/10.0
453.7 1.2/10.0			449.3 5.5/0.4	4.0 rd		448.9 5.9/10.0
451.3 3.5/10.0	453.1 1.7/4.0		447.9 6.9/1.5	3.0 rd.		448.2 6.6/10.0

Sta.	+	π	−	Elev.
		454.807		
296+50			7.6	447.2
297+00			7.9	446.9
+09.5			8.0	446.8
T.P			7.081 ~~7.081~~	447.726
	4.561	452.287 ~~432.287~~		
			3.382	448.905 448.876
	10.26	"A" 459.14		
297+35.5			12.1	447.0
+59.5			12.2	446.9
+84.5			12.1	447.0
+99.0			12.2	446.9
299+00			13.6	445.5
300+00			14.4	444.7 ?
+50				
	5.696	454.572		

452.0				447.7
$\frac{2^8}{10^0}$				$\frac{7^1}{10^0}$
450.2	448.5	447.1	$\frac{4^0}{rd}$	446.9
$\frac{4^6}{10^0}$	$\frac{6^2}{4^0}$	$\frac{7^2}{1^0}$	$\frac{3^0}{rd}$	$\frac{7^9}{10^0}$
449.0		447.6		447.5
$\frac{5^8}{10^0}$		$\frac{7^3}{5^0}$	$\frac{3^0}{rd.}$	$\frac{7^3}{10^0}$

Ran peg line and check B.M within .019 (448.895)

~~449.8~~	449.2	447.1		~~447.4~~
$\frac{9^3}{10^0}$	$\frac{9^9}{9^0}$	$\frac{12^0}{8.4\,P}$	$\frac{3^0}{rd.}$	$\frac{11^7}{10^0}$
~~448.6~~	448.4 ~~448.4~~	~~447.2~~		~~447.3~~
$\frac{10^5}{10^0}$	$\frac{10^2}{6^5}$	$\frac{11^9}{4^5}$	$\frac{4^0}{rd.}$	$\frac{11^8}{10^0}$
~~448.5~~	~~448.5~~	~~446.9~~		~~447.2~~
$\frac{10^6}{10^0}$	$\frac{10^6}{8^0}$	$\frac{12^2}{5^0}$	$\frac{1^0}{rd.}$	$\frac{11^9}{10^0}$
~~448.8~~	~~448.5~~	~~446.8~~		~~447.1~~
$\frac{10^3}{10^0}$	$\frac{10^2}{9^0}$	$\frac{12^3}{6^0}$		$\frac{12^0}{10^0}$
~~457.1~~		~~456.4~~		~~446.1~~
$\frac{1^2}{10^0}$		$\frac{2^2}{7^0}$	$\frac{3^0}{rd}$	$\frac{13^0}{10^0}$
~~454.1~~		~~452.1~~		~~445.5~~
$\frac{5^0}{10^0}$		$\frac{7^0}{6^0}$	$\frac{2^0}{rd.}$	$\frac{13^6}{10^0}$
~~453.2~~		~~445.4~~		~~445.4~~
$\frac{5^9}{10^0}$		$\frac{13^2}{2^0}$	3^0	$\frac{13^7}{10^0}$

Sta	+	℄	−	Elev.
		454.572		
T.P 302+40			10.436	444.136
March 2, 1926	6.080	450.216		
B.M. # 37			6.377	443.839 443.824
B.M. #36			4.110	446.106 446.101
				446.101
~~301+00~~	4.110	450.211		
301+00			4.9	445.3
301+30.6			5.2	445.0
+55.6			5.6	444.6
+80.6			6.0	444.2
302+05.6			6.2	444.0
302+30.6			6.6	443.6
+51.7			6.8	443.4
B.M. # 36	+2			446.101
	1.225	447.326		
T.P. sta. 305+00			4.650	442.676
303+00			4.5	443.8

Impossible to plumb rod.

446.2 — 4 2/10 — 446.6 — 3 6/10 — 446.0 — 4 2/10 — 446.0 — 4 2/10 — 445.6 — 4 6/10 — 445.5 — 5 0/10 — 446 — 4 0/10 — 444.9 — 2 4/10

445.6 — 4 6/6 (4 rd) — 445.1 — 5 1/5 0 — 444.7 — 5 5/3 5 — 444.1 — 5 5/4 0 (2 0 rd.) — 444.1 — 6 1/4 0 (2 0 rd. / 4 0 rd. / 5 0 rd. / 4° rd.)

445.5 — 4 7/10 0 — 445.1 — 5 1/10 0 — 444.8 — 444.7 — 5 4/10 0 — 444.4 — 444.3 — 5 8/10 0 — 445.1 — 5 1/10 0 — 443.8 — 443.7 — 6 4/10 0 — 443.8 — 443.7 — 6 4/10 0 — 443.4 — 3 9/10 0

Sta.	+	π	−	Elev.
T.P. 305+00				442.676
	(12.66)	455.34		
304+00			13.5	441.8
	+86.7		12.0	443.3
305	+11.7		11.7	443.6
	+36.7		12.5	442.8
	+61.7		12.3	443.0
	+86.7		12.0	443.3
306+05.3			12.9	442.4
307+00			12.7	442.6
308+00			14.3 ~~10.1~~	441.0
T.P. Sta. 305+00				442.676
	3.823	446.499		
	+56.2		5.3	441.2
	+81.2		5.2	441.3

℄

12.66
3.823

(44)

449.6
5 2
10 0

452.3
3 0
10 0

452.2
3 1
10 0

450.8
4 5
10 0

452.7
2 6
10 0

453.3
2 0
10 0

452.1
3 2
10 0

451.1
4 2
10 0

445.2
10 1
10 0

442.1
4 4
10 0

442.3
4 2
10 0

444.8
10 5
15

447.0
8 3
3 0

447.9
7 4
5 0

448.5
6 8
3 0

450.2
5 1
8 0

449.6
5 7
6 0

448.0
7 3
4 0

446.5
8 8
2 4

443.7
11 6
5 5

443.8
11 5
3 0

441.4
5 1
4 9

441.5
5 0
5 2

4 0 rd.
4 0 rd.
4 0 rd.
4 0 rd.
4 0 rd.
5 0 rd.
4 0 rd.
2 0 rd.
2 0 rd.
2 0 rd.

442.5
12 8
10 0

442.0
13 3
1 0

442.2
13 1
1 0

442.2
13 1
0 5

442.1
13 2
0 5

441.9
13 4
1 0

441.5
13 8
3 0

6 0 rd.

442.5
12 8
10 0

442.6
12 7
10 5

442.6
12 7
10 5

442.6
12 7
10 5

442.4
12 9
10 0

442.4
12 9
10 5

442.3
13 0
10 5

442.0
13 3
10 0

441.5
13 8
10

441.6
4 9
10 0

441.6
4 9
10 0

Sta	+	ℸ	−	Elev.
		446.499		
309+06.2			5.4	441.1
+31.2			5.7	440.8
+56.2			6.0	440.5
+81.2			6.3	440.2
310+03.1			6.6	439.9
311+00			7.5	439.0
T.P.	4.003	444.394	6.108	440.391
+50			5.5	438.9
312+00			5.6	438.8
+11.5			5.3	439.1
312+53.6			5.0	439.4
+95.2			4.9	439.5
313+00			4.8	439.6

℄

45

442.5	441.2			441.4
4 2 / 10	5 3 / 5 0	2 0 rd.		5 1 / 10
440.5	440.9			441.2
6 0 / 10	5 6 / 4 2	2 0 rd.		5 3 / 10
440.2				440.9
6 3 / 10		3 0 rd.		5 6 / 10
439.7				440.6
6 6 / 10		3 0 rd.		5 9 / 10
442.1	440.3			440.3
4 4 / 10	6 2 / 7 1	3 0 rd.		6 2 / 10
442.5	441.0	438.8		439.4
4 2 / 10	5 5 / 5 2	7 1 / 4 2	2 0 rd.	7 1 / 10
	444.4	438.9		439.0
	0 2 / 7 2 Top of bank	5 5 / 6 5 rd.		5 4 / 10
438.6				439.1
5 8 / 10	6 0 rd.	9 0 rd.		5 3 / 10
438.4				439.1
5 8 / 10	7 2 rd.	8 0 rd.		5 3 / 10
439.3		439.1		435.0
5 1 / 10		5 3 / 4 0		9 4 / 10
439.3		439.2		435.1
5 1 / 10		5 3 / 5 2		9 3 / 10
439.3		439.1		435.3
5 1 / 10		5 3 / 5 0	2 0 rd.	9 1 / 10

Sta.	+	℄	−	Elev.
		444.394		
313+55.7			4.9	439.5
+80.7			4.6	439.8
314+05.7			4.8	439.6
+30.7			5.0	439.4
+55.7			5.2	439.2
+80.7			5.6	438.8
315+05.7			7.0	437.4
+30.7			7.1	436.7
+41.3			7.1	437.3
			6.800	437.594
	4.769	442.363		
U.S.G.S. B.M			3.447	438.916
"				438.916
changed set ups. →	3.604	442.520		
	~~3.090~~	~~442.820~~		
315+80			6.2	436.3

439.5 4.9 10°

439.5 4.9 10°

439.5 4.9 10°

439.4 5.0 10°

439.2 5.2 10°

439.1 5.2 10°

439.0 5.4 10°

438.9 rd. 5.5 10°

438.9 rd. 5.5 10°

439.3 5.1 6°

1° rd.

439.8 4.6 6°

R rd.

439.5 4.9 7°

R rd.

439.4 5.0 5°

R rd.

439.1 5.3 5°

3° rd.

7° rd.

439.1 5.3 5°

438.9 5.5 7°

438.9 5.5 9°

436.4 8.2 10°

437.5 6.9 10°

437.4 7.0 10°

437.1 7.3 10°

435.2 9.2 10°

434.7 9.7 10°

434.9 9.5 10°

434.8 9.6 10°

436.0 8.4 10°

438.7 3.8 10°

438.9 3.6 7°

436.6 5.9 3°

435.9 6.6 10°

Sta	+	Ⲡ	-	Elev.
		442.520		
316+00			4.2	438.3
317+00			5.2	437.3
318+00			5.3	437.2
319+00			5.4	437.1
320+00			5.9	436.6
321+00			6.1	436.4
322+00			6.5	436.0
T.P.			6.480	436.040
	4.168	440.208		
323+00			4.5	435.7
324+00			4.8	435.4
325+00			5.0	435.2
326+00			5.6	434.6
327+00			5.7	434.5

℄

438.6
$\frac{3^9}{10^0}$
437.6
$\frac{4^9}{10^0}$
437.3
$\frac{5^2}{10^0}$
437.1
$\frac{5^4}{10^0}$ rd.
436.6
$\frac{5^9}{10^0}$ rd
436.4
$\frac{6^1}{10^0}$ rd
436.2
$\frac{6^2}{10}$ — 9° rd.
436.0
$\frac{4^2}{10^0}$ — 8° rd.
436.0
$\frac{4^2}{10^0}$ — 9° rd
435.0
$\frac{5^2}{10^0}$ — 9° rd.
434.9
$\frac{5^3}{10^0}$
434.6
$\frac{5^6}{10^0}$ — 9° rd

~~435.0~~
7^5 Fce

435.3
$\frac{4^9}{7^5}$

438.2
$\frac{4^3}{10^0}$
436.5
$\frac{6^0}{10^0}$
437.0
$\frac{5^5}{10^0}$ Fce
437.1
$\frac{5^4}{10^0}$
436.8
$\frac{5^7}{10^0}$
436.2
$\frac{6^3}{10^0}$
436.0
$\frac{6^5}{10^0}$
435.6
$\frac{4^6}{10^0}$
435.4
$\frac{4^8}{10^0}$
435.1
$\frac{5^1}{10^0}$
435.3
$\frac{4^9}{10^0}$
434.5
$\frac{5^7}{10^0}$

Sta	+	℄	−	Elev.	
		440.208			
328+00			5.7	434.5	
			5.082	435.126	
	8.563	443.689			
329+00			8.8	434.9	
330+00			6.7	437.0	
331+00			6.4	437.3	
332+00			5.7	438.0	
333+00			2.8	440.9	
B.M.# 39			2.400	441.289	441.278 Recorded
		441.278			
	7.840	449.118			
334+23.2			7.3	441.8	
+48.2			8.4	440.7	
+73.2			7.7	441.4	
+98.2			7.7	441.4	

434.7
5 5
10°
rd

435.4
8 5
10°

438.2
5 5
10°

438.3
5 4
10°
rd.

435.4
5 3
7°

438.7
5 0
10°

441.8
19
10°
4°
rd.

441.8
7 3
10°

441.9
7 2
10°

441.8
7 3
10°
3°
rd.

441.6
7 5
10°
5°
rd.

R
rd

434.5
5 7
10°

434.9
8 8
10°

436.4
7 3
10°

436.8
6 9
10°

437.4
6 3
10°

440.0
3 7
10°

441.3
7 8
10°

440.7
8 4
10°

440.4
8 7
10°

440.4
8 7
10°

Sta.	+	π	−	Elev.
		449.118		
B.M.#39				441.278
	7.750	449.028		
335+23.2			8.0	441.0
+48.2			7.6	441.4
+73.2			7.4	441.6
+98.2			7.0	442.0
336+01 +03			6.9	line crosses culvert.
+20				442.1
+23.2			6.6	442.4
+48.2			6.1	442.9
+72.5			5.4	443.6
337+00			5.1	443.9
338+00			1.7	447.3
			.179	448.849 ~~448.939~~
	11.413	460.262 ~~460.352~~		
B.M.#40			10.230	450.03 ~~450.122~~ 450.117 Recorded.
339+00			8.6	451.7

℄

441.7 — 7.3/10.0 — 8.0 rd. — 440.2 — 8.8/10.0

441.7 — 7.8/10.0 — 6.0 — 440.6 — 8.4/10.0

443.1 — 6.9/10.0 — 6.0 — 440.5 — 8.5/10.0

442.4 — 6.6/10.0 — 441.9 — 7.1/4.0 — 440.6 — 8.4/9.0 — 439.8 — 9.2/5.0 (flow line culvert 18") — 441.8 — 7.2/10.0

441.6 — 8.4/20.0 Top culvert — 443.0 — 6.0/19.0 flow line culvert — Top culvert — 10.0

442.8 — 6.2/10.0 — 3.0 rd — 442.7 — 6.8/8.0 — 441.5 — 7.5/8.0 — 443.0 — 6.0/9.0 — 442.6 — 6.4/10.0 — 443.0 — 6.0/10.0

443.1 — 5.9/10.0

443.6 — 5.4/10.0 — 444.2 — rd — 443.8 — 5.2/4 — 443.0 — 6.0/9.0 — 444.1 — 4.6/4.5 — 5.0/10.0 — 444.0 — 444.8 — 4.2/10.0

4.8/10.0 — 447.2 — 4.2 rd. — 447.3 — 7.6 fence — 447.9

1.8/10.0 — 7.0 rd. — 1.7/9.0 — 7.0 rd — 1.1/10.0

452.2 — 8.1/10.0 — 5.0 rd. — 451.4 — 8.0/7.0 — 455.5 — 4.8/10.0

Sta	+	HI	-	Elev.				℄			
					B.M. #40 450117 Recorded						
	10.230	460.347									
346+00			2.4	457.9		457.6 2.7/10.0 rd			4.0 rd.	457.4 2.9/9.0	458.1 2.2/10.0
T.P.			1.154	459.193							
	12.439	471.632									
341+00			10.2	461.4		461.6 10.0/10.0		5.0 rd.	6.0 rd		461.0 10.6/10.0
+62.9			7.1	464.5		464.0 7.6/10.0		6.0 rd	6.0 rd.		464.0 7.6/10.0
342+00			5.3	466.3		466.0 5.6/10.0		9.0 rd.	6.0 rd		465.8 5.8/10.0
T.P			1.651	469.981							
	12.347	482.328									
343+00			12.0	470.3		470.3 12.0/10.0			470.1 12.2/6.0	5.0 rd.	473.7 8.6/10.0
344+00			4.9	477.4		475.0 7.3/10.0	6.0 rd.	475.1 7.2/2.0			480.0 2.3/10.0
T.P.			2.852	479.476							
	8.18	487.66 (487.56)									
344+95			6.0	481.7		479.0 8.7/10.0	478.6 9.1/6.0; 8.0 rd	481.2 6.5/4.0			482.9 4.8/10.0
345+00			6.2	481.5		479.1 8.6/10.0	8.0 rd.; 478.8 8.9/6.0	479.9 7.8/4.0; 480.5 7.2/15			482.9 4.8/10.0
346+00			8.5	479.2		478.7 9.0/10.0	7.0 rd.		479.6 8.1/6.0		480.6 7.1/10.0
	2.308	481.784									
347+00			5.3	476.5		475.9 5.9/10.0	6.0 rd.	475.4 6.4/4.0			476.1 5.7/10.0

Party
Leach T
Reynolds-Rod
Ruplinger-

Sta.	+	T	−	Elev.
		481.784		
348+00			9.5	472.3
T.P.			12.491	469.293
	2.694	471.987		
			5.738	466.249
March 3,			Recorded	466.272
				466.272
	4.565	470.837		
349+00			2.7	468.1
350+00			5.3	465.5
351+00			6.9	463.9
352+00			7.4	463.4
353+00			10.1	460.7
354+00			12.0	458.8
355+00			12.3	458.5
T.P.			11.475	459.362
	4.480	463.842		
+21			6.7	457.1
+30 center of stream bed			7.6	456.2

Cool
Cloudy

4.565

(51)

472.6				472.5
9 2 / 10	8 rd.			9 3 / 10
468.5		469.1		469.8
2 3 / 10	6 rd	1 2 / 7		1 8 / 10
465.5		466.1		466.5
5 3 / 10	6 rd	4 2 / 4 5		4 3 / 10
464.2				464.0
6 6 / 10	3 rd.			6 8 / 10
461.1		463.1		462.6
6 2 / 10	rd	7 2 / 4 0		8 2 / 10
461.0		460.8	461.3	461.6
9 8 / 10	rd.	10 / 3 0	9 5 / 6 0	9 2 / 10
459.3	1 rd.			459.0
11 5 / 10				11 8 / 10
459.1				458.4
11 / 10	4 rd.			12 4 / 10
	457.6			457.1
	6 2 / 2 9			6 2 / 10
	456.3			456.4
	7 5 / 2 0			2 4 / 10

Sta	+	℄	−	Elev.
		463.842		
355+43			6.2	457.6
356+00			5.7	458.1
357+00			5.1	458.7
358+00			3.9	459.9
359+00			2.6	461.2
360+00			1.1	462.7
T.P.			0.876	462.966
	4.547	467.513		
B.M. #42			9.489	458.024 Recorded 458.035
+25				
+25.6			4.8	462.7
+35.6			4.8	462.7
+45.6			4.8	462.7
+55.6			4.7	462.8
65.6			4.5	463.0

458.7
5 1/10
458.9
4 9/10
459.0
4 8/10
460.3
3 5/10
461.7
2 1/10
463.2
0 6/10

458.6
5 2/5°
2°
rd.
4°
rd
2°
rd
1°
rd.

456.4
7 4/10
458.0
5 8/10
458.5
5 7/10
459.4
4 4/10
460.5
3 3/10
462.1
1 7/10

463.2
4 3/10
463.2
4 3/10
rd
463.1
4 4/10
463.0
4 5/10
463.0
4 5/10
7°
rd

3°
rd
4°
rd.
5°
rd
8°
rd.
8°
rd

462.2
5 3/10
462.2
5 3/10
462.2
5 3/10
462.2
5 3/10
461.9
5 6/9°
462.3
5 3/rd.

Sta.	+	↑	-	Elev.
		467.513		
+75.6			4.9	463.1
+85.6			4.4	463.1
+95.6			4.5	463.0
361+05.6			4.6	462.9
+15.6			4.9	462.6
+25.6			5.2	462.3
+35.6			5.4	462.1
45.6			5.7	461.8
+55.6			6.1	461.4
+65.6			6.3	461.2
+77.5			6.5	461.0
362+00			6.9	460.6

462.5 462.6 463.1 462.8 462.7 462.4 462.2 462.5 462.4 462.0 462.3 461.7 462.0 461.5 461.8 461.3 461.9 460.9 461.8 461.3 460.6 461.3 461.0 460.4 460.7 460.0

5° rd. 7° rd. 7° rd. 6° rd. 5° rd. 3° rd. 3° rd. 3° rd. 3° rd. 3° rd.

461.9 462.1 462.3 462.4 462.3 462.2 462.0 461.7 461.5 461.3 461.0 460.4

12° rd. 12° rd. 13° rd. 14° rd. 15° rd. 16° rd. 16° rd. 16° rd. 15°

Sta.	+	℄	−	Elev.
		467.513		
363+00			8.7	458.8
B.M. #42				458.035
	2.666	460.701		
364+00			3.8	456.9
365+00			5.5	455.2
366+00			6.9	453.8
367+00			8.5	452.2
368+00			9.7	451.0
T.P.			9.470	451.231
	3.083	454.314		
369+00			4.2	450.1
370+00			5.2	449.1
371+00			5.1	449.2
372+00			3.4	450.9
T.P. in road Sta. 373			9.790	444.524
	0.777	445.301		

℄ 2.666

(54)

458.9 — 8 6/10 — 458.3 — 9 2/8 — 5 0 rd.

458.5 — 9 0/10 — 15 0 rd.

456.9 — 3 8/10 — 456.9 — 3 8/7 0 — 456.3 — 4 4/6 5 — 4 0 rd.

456.7 — 4 0/10 — 456.1 — 4 6/10

455.1 — 5 6/10 — 454.8 — 5 9/5 8 — 4 0 rd.

453.5 — 7 2/10 — 6 0 rd.

453.5 — 7 2/10 — 12 0 rd.

451.7 — 9 0/10 — 6 0

451.9 — 8 8/10 — 12 0 rd.

450.6 — 10 1/10 — 6 0

450.7 — 10 0/10 — 12 0 rd.

449.5 — 4 8/10 — 7 2 rd.

449.5 — 4 5/10

448.7 — 5 6/10 — 7 2 rd.

449.1 — 5 2/5 0

448.7 — 5 6/10 rd.

449.6 — 4 7/10 3

450.7 — 3 6/10

451.0 — 3 3/9 0 — 454.3 — 0 0/10 0

Sta.	+	⊼	−	Elev.	
		445.301			
	4.56	"A" 449.08		444.524	T.P. in road 373.
373+00			"A" 3.1	446.0	
				439.3	
374+00			6.0	~~443.1~~	
				437.2	
375+00			8.1	~~441.0~~	
				438.0	
376+00			7.3	~~441.8~~	
T.P.			9.960	435.341	
	.551	435.892			
B.M. #43			2.885	433.007	Recorded 432.996
377+00			1.6	434.3	
378+00			5.3	430.6	
379+00			7.8	428.1	
B.M.# 43				432.996	
	2.885	435.881			
T.P.			12.529	423.352	
	1.506	424.858			
380+00			3.3	421.6	
381+00			7.3	417.6	

			℄		
444.6 "A" 4.5/10.0	445.5 "A" 3.3/5.0	2.0/rd		446.3 2.8/10.0 "A"
438.6 6.2/10.0			L rd	439.4 5.9/10.0
437.4 7.9/10.0			(L) rd.	437.4 7.9/10.0
439.1 6.2/10.0	439.0 6.3/5.0	437.9 7.4/2.0	2.0 rd.	437.9 7.4/10.0
435.0 0.9/10.0		434.9 1.0/3.0		434.6 1.3/10.0
430.6 5.3/10.0			(L) rd.	431.3 4.6/10.0
428.3 7.6/10.0	428.5 7.4/5.0	427.9 8.0/1.0	(L) rd.	428.5 7.4/10.0
422.6 2.3/10.0			L rd	422.1 2.8/10.0
417.8 7.1/10.0			(L) rd	417.9 7.0/10.0

Sta.	+	π	−	Elev.
		424.858		
382+00			10.4	414.5
383+00			11.6	413.3
T.P. sta 383+00			11.190	413.668 ~~413.630~~
	1.867	415.535		
384+00			3.5	412.0
385+00			5.0	410.5
386+00			6.3	409.2
387+00			7.3	408.2
388+00			7.9	407.6
T.P.			7.855	407.680
	3.382	~~411.526~~ 411.062		
389+00			2.9	408.2
390+00			6.3	404.8
391+00			7.6	403.5
392+00			7.6	403.5

(60)

415.8	415.7	414.5	415.1
9 1 / 10	9 3 / 10	10 4 / 15 (L) rd	9 8 / 10
413.9		413.7	413.8
11 / 10		11 2 / 4	11 1 / 10
413.1		412.6	412.3
2 4 / 10		2 9 / 4 (L) rd	3 2 / 10
411.5	411.1	410.5	410.9
4 2 / 10	4 4 / 5	5 0 / 4 5	4 6 / 10
410.0	410.7	408.8	409.4
5 5 / 10	4 8 / 6 5	6 7 / 5	6 1 / 10
408.4		(L) rd	408.6
7 / 10			6 9 / 10
407.9			408.0
7 6 / 10			7 6 / 10
408.3			408.2
2 8 / 10			2 9 / 10
403.5	404.6	2 rd.	405.0
7 6 / 10	6 6 / 5	2 rd.	6 1 / 10
402.4			403.8
8 2 / 10			7 3 / 10
402.7	403.4	2 rd.	403.6
8 4 / 10	7 2 / 4	2 rd.	7 5 / 10

Sta	+	∧	−	Elev.
		411.062		
392+70.2			7.5	403.6
B.M.#44			7.253	403.809
B.M.#44			403.777	403.777
	12.463	416.240		
393+00			12.0	404.2
394+00			5.7	410.5
T.P.			0.198	416.042
	11.271	427.313		
395+00			11.0	416.3
396+00			6.4	420.9
397+00			4.3	423.0
T.P.			1.438	425.875
	7.788	433.663		
398+00			8.2	425.5
398+15.0			7.8	425.9
399+00			5.4	428.3
400+00			4.1	429.6
B.M.#45			3.270	430.393

430.396

403.5
7.6
10°

404.4
11.8
10°

411.5
4.2
10°

410.3
5.9
5.6

409.7
6.6
5°

418.6
8.2
10°

423.6
4.2
10°

424.6
2.7
10°

422.8
4.5
2.6

427.7
6.6
10°

427.0
6.2
4°

425.4
8.3
10°

427.9
5.8
10°

427.1
6.4
3.6

425.8
2.9
10°

430.4
3.3
10°

429.8
3.9
3.6

428.1
5.4
1.5

430.9
2.8
10°

430.1
3.4
0.5

61

403.5
2.6
10°

404.4
11.8
10°

411.1
5.1
10°

416.8
10.5
10°

420.4
6.9
10°

423.3
4.8
10°

425.9
7.8
10°

426.3
2.4
10°

428.8
4.9
10°

430.2
3.5
10°

Sta	+	⊼	−	Elev.
B.M. #45				430.396
	6.695	437.091		
401+00			5.6	431.5
402+00			5.1	432.0
403+00			4.4	432.7
404+00			4.7	432.4
405+00			5.6	431.5
406+00			7.4	429.7
T.P.			9.173	427.918
	1.466	429.384		
407+00			2.5	426.9
408+00			6.5	422.9
B.M. #46			7.430	421.954 421.954
	1.150	423.104		
409+00			3.1	420.0
410+00			4.8	418.3
411+00			6.5	416.6

433.1	432.7	430.9	431.4
4 2 / 10 0	4 1 / 3 0	6 2 / 0 5	5 7 / 10 0
433.8	433.7	431.6	432.2
3 3 / 10 0	3 4 / 2 5	5 5 / 1 2	4 9 / 10 0
434.0	433.5	432.0	432.3
3 1 / 10 0	3 2 / 2 0	5 1 / 3 0	4 8 / 10 0
433.3	433.2	431.1	431.4
3 8 / 10 0	3 9 / 2 0	6 0 / 4 0	5 2 / 10 0
431.8		429.7	429.9
5 3 / 10 0		7 4 / 4 0	7 2 / 10 0
429.5		427.6	428.1
7 6 / 10 0		9 5 / 5 0	9 0 / 10 0
426.8		424.3	425.1
2 6 / 10 0		5 1 / 4 0	4 3 / 10 0
422.7		421.6	421.7 421.2 421.4
6 7 / 10 0		7 8 / 3 0	7 7 8 3 / 6 0 6 5 / 8 0 / 10 0
420.0		419.0	418.6 418.8
3 1 / 10 0		4 1 / 6 2	4 5 / 6 5 / 4 3 / 10 0
418.4		416.9	417.1
4 7 / 10 0		6 3 / 7 0	6 0 / 10 0
416.4		415.8	415.9
6 7 / 10 0		7 3 / 8 0	7 2 / 10 0

3° rd.

5°

5° rd.

8° rd.

rd.

rd.

rd.

Sta.	+	HI	−	Elev.
		423.104		
412+00			5.7	417.4
413+00			3.0	420.1
+31.4			2.5	420.6
+56.4			2.3	420.8
+81.4			2.7	420.4
414+06.4			4.2	418.9
+31.4			4.6	418.5
(should be 56.4) +51.4			5.1	418.0
+74.6			6.7	416.4
B.M.#47			5.964	417.140 417.160
BM#47			417.160	
	5.964	423.124		
T.P.			6.383	416.741
	2.049	418.790		
415+00			2.1	
+07.5				

℄

417.9
$5^{2}/10^{\circ}$
420.7
$2^{4}/10^{\circ}$
421.0
$2^{1}/10^{\circ}$
420.9
$2^{2}/10^{\circ}$
420.8
$2^{3}/10^{\circ}$
420.4
$2^{2}/10^{\circ}$
417.8
$5^{3}/10^{\circ}$
417.4
$5^{7}/10^{\circ}$
416.2
$6^{9}/10^{\circ}$

420.2
$2^{9}/7^{\circ}$

419.4
$3^{2}/2^{5}$

416.3
$6^{8}/7^{\circ}$
419.0
$4^{1}/5^{\circ}$
419.8
$3^{3}/6^{\circ}$
419.6
$3^{5}/7^{\circ}$
419.[illegible]
$3^{9}/3^{\circ}$

9° rd
9° rd
9° rd
6°
4° rd

416.5
$6^{6}/10^{\circ}$ rd
419.6
$3^{5}/10^{\circ}$ rd
419.9
$3^{2}/10^{\circ}$
419.8
$3^{3}/10^{\circ}$
419.8
$3^{3}/10^{\circ}$
419.5
$3^{6}/10^{\circ}$
418.3
$4^{8}/10^{\circ}$
417.8
$5^{3}/10^{\circ}$
416.8
$6^{3}/10^{\circ}$

center of road

$2^{3}/10^{\circ}$
Power pole 7°
$2^{4}/7^{\circ}$
$2^{9}/8^{5}$
$2^{8}/10^{\circ}$

Leach π
Reynolds Rod
Ruplinger "

Warm and cloudy

℄

Sta	+	π	−	Elev.					
		418.790							
416+00			8.0		$\frac{8^{2}}{10^{0}}$				$\frac{7^{5}}{10}$
+41			11.4		$\frac{11^{2}}{10}$				$\frac{11^{0}}{10^{0}}$
417+00			11.7		$\frac{11^{3}}{10^{0}}$				$\frac{11^{8}}{10^{0}}$
418+00			10.7		$\frac{10^{5}}{10^{0}}$				$\frac{10^{8}}{10^{0}}$
419+00			11.2		$\frac{11^{0}}{10^{0}}$				$\frac{11^{1}}{10^{0}}$
T.P.			11.015 (~~11.05~~)	407.775					
	3.992	411.767							
			4.710	407.057					

Sta	+	π	−	Elev.					
Mar. 4, 1926									
B.M. # 47				417.160					
	2.660	419.820							
415+00			3.2	416.6	416.5 $\frac{3^{3}}{10^{0}}$		416.3 $\frac{3^{5}}{7^{0}}$	415.9 $\frac{3^{9}}{8^{5}}$	415.9 $\frac{3^{9}}{10^{0}}$
+07.5						Powe pole 7^{0}			
416+00			9.0	410.8	410.2 $\frac{9^{6}}{10^{0}}$				411.4 $\frac{8^{4}}{10^{0}}$
+41			12.5	407.3	407.0 $\frac{12^{8}}{10^{0}}$				407.7 $\frac{12^{1}}{10^{0}}$
417+00			12.7	407.1	407.5 $\frac{12^{3}}{10^{0}}$				406.9 $\frac{12^{9}}{10^{0}}$
418+00			11.6	408.2	408.2 $\frac{11^{6}}{10^{0}}$				408.0 11^{8}

	+	π	−	Elev.
		419.820		
419+00			12.2	407.6
420+00			12.8	407.0
T.P.			12.853	406.967
	4.020	410.987		
B.M# 48			3.923	407.064 / 407.060 ~~407.212~~
B.M# 48				407.060 ~~407.212~~
	5.027	412.087 ~~412.239~~		
420+77.4			5.7	406.4 ~~406.5~~
421+02.4			6.1	406.0 ~~406.1~~
+27.4			6.0	406.1 ~~406.2~~
+52.4			5.6	406.5 ~~406.6~~
+77.4			5.8	406.3 ~~406.4~~
422+02.4			6.1	406.0 ~~406.1~~
+24				
+27.4			6.2	405.9 ~~406.0~~
+39	1st edge stream bed		8.0	404.1 ~~404.2~~

406.9	407.7
$12^{9}/10^{0}$	$12^{1}/10^{0}$
406.9	407.0
$12^{9}/10^{0}$	$12^{8}/10^{0}$

Ran peg line and checked my elev. within .009 (407.073)

406.2 ~~406.3~~	406.5 ~~406.6~~
$5^{9}/10^{0}$	$5^{6}/10^{0}$
406.2 ~~406.3~~	405.9 ~~406.0~~
$5^{9}/10^{0}$	$6^{2}/10^{0}$
406.4 ~~406.5~~	405.9 ~~406.0~~
$5^{7}/10^{0}$	$6^{2}/10^{0}$
406.4 ~~406.5~~	406.3 ~~406.4~~
$5^{7}/10^{0}$	$5^{8}/10^{0}$
406.3 ~~406.4~~	406.1 ~~406.2~~
$5^{8}/10^{0}$	$6^{0}/10^{0}$
406.2 ~~406.3~~	405.8 ~~405.9~~
$5^{9}/10^{0}$	$6^{3}/10^{0}$
404.9 ~~405.0~~	406.0 ~~406.1~~
$7^{2}/10^{0}$	$6^{1}/10^{0}$
404.2 ~~404.3~~	404.4 ~~404.5~~
$7^{9}/10^{0}$	$7^{7}/10^{0}$

Line crosses fence

Changes due to corrected B.M's

Sta	+	T	−	Elev.
		412.087 ~~412.239~~		
422+52.4			8.1	404.0 ~~404.1~~
	+57.42nd edge stream bed.		8.0	404.1 ~~404.2~~
	+66.9		5.9	406.2 ~~406.3~~
	+77.4		5.7	406.4 ~~406.5~~
423+02.4			6.2	405.9 ~~406.0~~
	+27.4		6.9	405.2 ~~405.3~~
	+52.4		7.3	404.8 ~~404.9~~
	+65.2		7.6	404.5 ~~404.6~~
T.P.		410.271	7.531	404.556 ~~404.708~~
	5.715	~~410.423~~		
424+00			5.6	404.7 ~~404.8~~
425+00			5.5	404.8 ~~404.9~~
426+00			5.7	404.6 ~~404.7~~
427+00			5.6	404.7 ~~404.8~~

404.9 ~~405.0~~ 7 2/10°
406.3 ~~406.4~~ 5 8/10°
406.4 ~~406.5~~ 5 7/10°
406.2 ~~406.3~~ 5 9/10°
405.7 ~~405.8~~ 6 4/10°
405.2 ~~405.3~~ 6 9/10°
404.8 ~~404.9~~ 7 3/10°
404.7 ~~404.8~~ 7 4/10°
~~404.8~~ 404.7 5 6/10°
~~405.0~~ 404.9 5 4/10°
~~404.6~~ 404.5 5 8/10°
~~404.3~~ 404.2 6 1/10°

~~405.1~~ ~~405.0~~ 405.1 ~~405.0~~ 7 2/10°
~~404.2~~ ~~404.3~~ 7 9/9°
405.9 ~~406.0~~ 6 2/7°

404.0 ~~404.1~~ 8 1/10°
404.0 ~~404.1~~ 8 1/10°
~~404.2~~ 404.1 8 2/10°
~~405.5~~ 405.4 6 7/10°
~~406.4~~ 406.3 5 8/10°
~~405.5~~ 405.4 6 7/10°
~~405.2~~ 405.1 7 0/10°
~~405.2~~ 405.1 7 0/10°
~~405.0~~ 404.9 5 4/10°
~~405.1~~ 405.0 5 3/10°
~~405.5~~ 405.4 4 9/10°
~~405.2~~ 405.1 5 3/10°

	+		−	Elev.
		410.271		
427+27				
+38			6.6	403.7
+44			8.2	402.1
+56			5.9	404.4
T.P.		406.175	6.123	404.148
	2.027	406.321		
+80			2.1	404.1
+89			2.6	403.6
428+00			5.7	400.5
+12			6.8	399.4
+21			3.0	403.2
+34.4			3.0	403.2
+44.4			4.0	402.2
+54.4			3.9	402.3

401.8 / 401.9 — 8.5 / 10.0

403.7 / 403.8 — 6.6 / 10.0

404.3 / 404.4 — 6.0 / 10.0

403.1 — 3.1 / 11.0

402.8 / 402.9 — 3.4 / 10.0

403.2 / 403.3 — 3.0 / 10.0

400.8 / 400.9 — 5.4 / 10.0

400.0 / 400.1 — 6.2 / 10.0

403.4 / 403.5 — 2.8 / 10.0

402.5 / 402.6 — 3.7 / 10.0

401.7 / 401.8 — Line crosses fence — 8.6 / 5.4

402.2 / 402.3 — 8.1 / 7.0

Peppe tree 24" 6.0

403.0 / 403.1 — 5.0

402.9 / 403.0 — Top Bridge — 3.3 / 5.0

403.4 / 403.4 — 2.9 / 5.0

400.7 / 400.8 — 5.5 / 8.0

399.0 / 399.1 — 7.2 / 8.0

400.1 / 400.2 — 6.1 / 6.0

402.3 / 402.4 — 3.9 / 7.0

edge pavement

400.5 / 400.6 — 5.5 / 4.0

399.8 / 399.9 — 6.4 / 9.0

400.3 / 400.4 — center of stream — 5.9 / 2.5

0.5 edge pavement

403.8 / 403.9 — 6.5 / 10.0

401.9 / 402.0 — 8.4 / 10.0

404.1 / 404.2 — 2.1 / 10.0

Top

400.1 / 400.2 — 6.1 / 10.0

403.6 / 403.7 — 2.6 / 10.0

403.3 / 403.4 — 2.9 / 10.0

402.4 / 402.5 — 3.8 / 10.0

402.4 / 402.5 — 3.8 / 10.0 — on pavement

on pavement

Station	+	HI	−	Elev.
		406.175 ~~406.327~~		
+64.4			3.8	402.4 ~~402.5~~
+74.4			3.8	402.4 ~~402.5~~
+84.4			3.9	402.3 ~~402.4~~
+94.4			4.2	402.0 ~~402.1~~
429+04.4			4.4	401.8 ~~401.9~~
+14.4			5.2	401.0 ~~401.1~~
+24.4			5.1	401.1 ~~401.2~~
+34.4			5.5	400.7 ~~400.8~~
+45 429+47.6 = 431+38.6			5.5	400.7 ~~400.8~~
+56				?
432+00			5.5	400.7 ~~400.8~~
433+00			6.9	399.8 ~~399.9~~

on pavement

Right of ℄

~~402.4~~ 402.3 — 3.9 / 10.0 — 8.0 edge pavement — ~~402.4~~ 402.3 — 3.9 / 10.0

on pavement — ~~402.4~~ 402.3 — 3.9 / 10.0 — 8.5 edge pavement — ~~402.4~~ 402.3 — 3.9 / 10.0

on pavement — ~~402.4~~ 402.3 — 3.9 / 10.0 — 2.0 edge pavement — ~~401.8~~ 401.7 — 4.5 / 10.0

on pavement — ~~402.4~~ 402.3 — 3.9 / 10.0 — 2.0 edge pavement — 401.3 ~~401.4~~ — 400.8 ~~400.9~~ — ~~401.0~~ 400.9 — 5.3 / 10.0

on pavement — ~~402.3~~ 402.2 — 4.0 / 10.0 — 6.0 — 4.9 / 4.0 — 5.4 / 7.0 — ~~401.3~~ 401.2 — 5.0 / 10.0

~~402.2~~ 402.1 — 4.1 / 10.0 — 401.3 ~~401.4~~ — 400.8 ~~400.9~~ — 4.9 / 1.5 — 5.4 / 4.0 — ~~401.8~~ 401.7 — 4.5 / 10.0

on pavement — ~~402.2~~ 402.1 — 4.1 / 10.0 — 8.0 edge pavement — ~~400.0~~ 401.9 — 4.3 / 10.0

edge pavement — ~~402.1~~ 402.0 — 4.2 / 10.0 — 401.6 ~~401.7~~ — 4.6 / 4.0 — 400.9 ~~401.0~~ — 5.3 / 5.0 — 401.4 ~~401.5~~ — 4.8 / 6.0 — ~~401.7~~ 401.6 — 4.6 / 10.0

~~401.9~~ 401.8 — 4.4 / 10.0 — 401.7 ~~401.8~~ — 4.5 / 6.0 — 401.0 ~~401.1~~ — 5.2 / 3.0 — 400.8 ~~400.9~~ — 5.4 / 2.0 — 401.6 ~~401.7~~ — 4.6 / 3.5 — 10.0 6" Tree — 4.5 / 10.0 ~~401.8~~ 401.7

starting of row of elm trees

~~401.6~~ 401.5 — 4.7 / 10.0 — 401.2 ~~401.3~~ — 5.6 / 2.0 — 400.7 ~~400.8~~ — 5.5 / 1.5 — 8.3 — 400.8 ~~400.9~~ — 5.4 / 3.0 — 401.5 ~~401.6~~ — 4.7 / 5.0 — ~~401.6~~ 401.5 — 4.7 / 10.0

~~400.9~~ 400.8 — 5.4 / 10.0 — 400.3 ~~400.4~~ — 5.9 / 3.0 — ~~401.0~~ 400.9 — 5.3 / 10.0

			Elev.
		406.175 ~~406.327~~	
434 +00			398.9 ~~399.0~~
	7.3		
435+00	8.0		398.2 ~~398.3~~
Co. B.M. #49	5.950	400.225 ~~400.377~~	~~400.220~~ ~~400.256~~
Co. B.M. #49		400220 ~~400.256~~	
	3.845	404.065 ~~404.101~~	
436+00	6.5		397.6
437+00	7.0		397.1
+66	6.5		397.6 crown of 20' road.
+94			
438 +00	7.4		396.7
+28			
+71			
+85			
+91			
439+00	9.2		394.9
+04			
440+00	8.4		395.7
441+00	9.1		395.0
T.P	~~8.880~~	395.185 ~~395.221~~	

~~400.1~~ ~~400.2~~	~~399.9~~ ~~400.0~~	~~398.9~~ ~~399.0~~	399.4 5	400.1	400.1
6 1 / 10	6 3 / 7	7 3 / 2	6 7 / 2	6 1 / 5	6 1 / 10
~~399.4~~ ~~399.5~~	~~399.1~~ ~~399.2~~	~~398.5~~ ~~398.6~~	398.5 4	398.5 7	398.7 6
6 8 / 10	7 1 / 7	7 8 / 3	7 8 / 1	6 5 / 4	6 6 / 10
398.8	398.6	397.6	397.7	398.7	398.7
5 3 / 10	5 5 / 8	6 5 / 2	6 4 / 2	5 4 / 4	5 4 / 10
398.5	398.2	397.6	397.2	398.4	398.3
5 6 / 10	5 9 / 8	6 5 / 6	6 9 / 2	5 7 / 5	5 8 / 10
398.9					396.5
5 7 / 10					7 6 / 10
399.1	399.0	396.7	Power pole 6	396.9	397.0
5 / 10	5 / 9	7 4 / 4	7 2 / 2	7 1 / 6	6 3 / 10
End of row of elm trees 6					
wing of bridge 2				6 Power pole	
center of bridge 9					
395.1			394.8	395.5	394.2
9 / 10			9 3 / 5	8 6 / 6	7 9 / 10
Flow line wing of bridge 5					
396.4	396.0		394.2		395.7
7 1 / 10	8 1 / 9		7 9 / 3		8 1 / 10
395.7	394.8				395.1
8 4 / 10	9 3 / 8				9 / 10

Sta.	+	HI	−	Elev.
				395.186 (~~395.221~~)
	5.282	400.467 (~~400.503~~)		
441+87			5.9	394.6
442+00			6.0	394.5
+46				
442+96			6.4	394.1
443+00			5.4	395.1
+03			4.7	395.8
+10			6.4	394.1
444+00			6.7	393.8
445+00			6.1	394.4
445+70			5.0 Crown of 15' driveway	395.5
446+00			5.4	395.1
447+00			7.4	393.1
T.P.			7.640	392.827 (~~392.863~~)
	6.543	399.370 (~~399.406~~)		

℄

(70)

395.4 5.1/10.0
395.3 5.2/10.0
395.7 4.8/10.0
396.2 4.3/10.0
396.0 4.5/10.0
395.4 5.1/10.0
395.2 5.3/10.0
395.7 4.8/10.0
395.6 4.9/10.0
395.8 4.7/10.0
394.9 5.6/10.0

395.0 5.5/9.0
394.7 5.8/7.0
394.1 6.4/6.0
394.6 5.9/6.0
395.2 5.3/5.0
393.5 7.0/5.0

394.5 6.0/7.0
Powe pole 5½

395.1 5.4/10.0
395.1 5.4/10.0
395.3 5.2/10.0
394.3 6.2/10.0
395.0 5.5/10.0
395.4 5.1/10.0
394.3 6.2/10.0
393.6 6.9/10.0
394.5 6.0/10.0
395.6 4.9/10.0
395.2 5.3/10.0
392.9 7.6/10.0

Contd. in Level Book #5. Page #1

#76802 also #76109

BM#15 508.445 Power Pole 100' L
121+30

BM#16 503.054 Power Pole 26104
6' L 134+30

BM#17 502.184 Oak Tree 6' R
137+90

BM#18 509.255 Nail in fence
130' L 147+45

BM#19 500.758 Sycamore tree
15' R 156+00

BM#20 504.635 Oak 12' L
165+45

BM#21 492.472 Hub in fence
4' R. 177+50

BM#22 491.366 Pole 40' L
183+32

BM#23 491.419 Peg 8' L
188+80

BM#24 490.912 Nail in Pole 73938
25' L 197+95

BM#25 486.282 Nail in tel. pole
30' L 203+82

BM#26 484.342 Nail in Power pole
#73929-30' L 211+25

BM#27 480.800 Oak 20' L
219+60

BM#28 486.482 Corner fence post
65' L 225+30

BM#29 485.125 Hub on Pole 5' R
235+55

BM#30 465.854 Nail in post 3' L
245+60

BM#31 461.347 Nail in fence 20' R
of gate 251+95

BM#32 463.134 Nail in Sycamore
48' R 260+10

BM#33 455.815 Sycamore tree
20' L 275+65

BM#34 446.620 Nail in 12" Cottonwood
80' R 286+65

BM#35 448.876 Nail in Sycamore
25' R 297+90

905
876
.029

895
876
.019

BM#14 574.37 nail in 12" diam. oak 20' left
Sta 113+21
top of cape Horn ridge

Should be 486.39
Aug. 3-'21
P.G.

IMPROVED TABLES
AND
INFORMATION

.00189

1000 / 5280 x .1

.00189
12
378
189
.2268

.018 .006
528 | 10.00
5 28
4720
4224

496.390
5.029
491.366

1000 / 5280 x .1

482
445
037

100 .02
528 | 1000

495
221
224

204
184
20
184
15

635
504.609
.026

.0189
.00189
11
189
189
2079

.0189
5280 | 100.00
5280
47200
42240
496.00

439.870
905 438.930
895 .900

444.603
2.400
442.203
441.278
.925

.010

.020 lower
.148
.168
021
.148

444.603
1.220
443.383
3.858
447.241
5.029
442.212
441.278
.934

377.
356
.021

198
184
14.00

.026
912 | 1400
889 | 10564
.023
3440
3168
272

809
403.777
.032

336+

407.212
407.064
.158

417.140

41
417.309
417.160
.149

400.756
400.377
79

.121

.148
.111
.038

21
407.044
.168
.121
.047