

EL CAPITAN  
Pipe Line Survey  
Levels — No 5  
& Cross Sections

LEVEL BOOK

380

W195

No. 5

MICROFILMED  
JAN 4 1965

366,362

203

.059

505

030

.075



26.4000  
Profile Levels and  
Cross Sections of Final  
Location --

From Station - 447+99

To - 810+37.8

Contd. from Level Book  
#4 - Page # 70

Party  
Leach T.  
Reynolds  
Ruplinger

Cloudy  
and Cool  
Mar. 4, 1926

①

Station	Dist.	Elev.	Notes
447+99		399.370 <del>399.406</del>	
448+00	7.1	399.23	
449+00	6.8	392.5	
B.M. #50	5.450	393.920 393.956 393.930 393.949	
B.M. #50	2.820	394.750 <del>396.769</del>	
450+00	5.2	391.6	
451+00	6.6	390.2	
+ 89			
452+00	6.8	390.0	
453+00	6.7	390.1	
454+00	9.10	391.9	
455+00	4.7	392.1	
T.P.	4.241 3.631	392.509 <del>392.528</del> 396.140 396.159	

Station	Dist.	Elev.	Notes
		392.6	
		392.8	flow line culvert.
		393.7	
		392.8	
		391.7	
		391.2	
		390.3	
		390.5	
		388.8	
		390.12	culvert
		390.0	
		390.0	
		392.2	
		392.8	
		393.2	



Party  
Leach T  
Reynolds R  
Roplinger

+ T  
389.997  
390.017

Elev.

463+00

4.5 385.5

33  
100  
edge pave.

386.7

32  
50  
48  
20

41  
30  
Fce

starting of row  
of trees

385.5

44  
100

464+00

+75

5.9 384.1

44  
100

385.6

42  
50

34  
30  
Fce Tel. pole

384.6

54  
100

465+00

6.9 383.1

53  
100

384.7

52  
60  
65  
30

34  
30  
Fce

Tel. pole

384.5

52  
100

466+00

+53

+90

7.3 382.7

57  
100  
edge pave

384.3

52  
30  
Fce

384.1

383.7

63  
100

467+00

7.3 383.7

60  
100  
edge pave

384.9

36" Tree  
30

62  
30  
Fce

383.1

382.7

73  
100

468+00

T.P.  
March 5,  
+70  
+80

Sta. 466+90  
4.518  
388.005  
388.105

6.430

7.9 382.1

383.567  
383.587

63  
100

384.0

72  
20  
Fce

382.1

383.0

382.6

74  
100

469+00

6.8 381.3

46  
100  
edge pave

6' Culvert

Flow line

80  
60  
40  
20

67  
20

wings of culvert

70  
30  
Fce

50 Tel. pole

381.1

381.5

470+00

+30

7.2 380.9

46  
100

383.5

51  
50

62  
35

70  
75  
Fce

382.1

381.3

471+00

+95

7.1 381.0

46  
70

383.5

54  
35

70  
50

40 Tel. pole

60  
80  
Fce

381.2

74  
100

50 Tel. pole.

+	π	-	Elev.
	388.085		
	<del>388.105</del>		
472+00			7.9 380.2
473+00			7.5
T.P	4.955	383.130	380.6
		<del>383.150</del>	
BM#52	4.877	382.848	382.843
"		<del>382.800</del>	<del>382.807</del>
		<del>382.843</del>	
		<del>383.057</del>	
	387.199		
BM#53	4.356	<del>388.213</del>	
473+82	5.498	381.701	381.700
		<del>382.715</del>	<del>381.711</del>
474+00			4.8 <del>382.4</del>
475+00			5.7 <del>381.5</del>
+10			6.9 <del>380.3</del>
476+00			6.8 <del>380.4</del>
+15			7.1 <del>380.1</del>
477+00			9.1 <del>378.1</del>
+27			<del>379</del>
+31			
479+00			9.8 <del>377.4</del>
			<del>378</del>

42/100  
42/100  
edge pave.

Note: This BM is out 1.

≠ crosses road.

edge pavt.

edge

383.4

382.5  
379.7  
380.1  
380.9

56/59  
58/30  
84/20  
80/45  
100/90  
73/100

Fce  
Fce  
Fce  
Fce

380.5  
76/10  
Fce

381.6

5/100  
68/100  
7/100

380.8

381.0

7/100

380.0

40 Fce  
40 Tel. pole

380.

7/100

378.4

40 Tel. pole

378.4

80 pole

376.9

100 Fce  
85 Fce

376.4

80 Tree (18")

376.0

77.0  
104 Fce  
110 Fce  
100

382.4

48/30

382.1

54/60

382.3

48/30

382.3

40 Fce

377.8

48 Fce

380.8

64/40

379.9

78/50

376.7

100 Fce

376.8

70 Fce

381.6

380.8

380.0

380.

378.4

376.9

376.4

376.0

	T	Elev.
	382.139 <del>380.213</del>	
479+49.7	9.2	378.0 ✓ <del>379.0</del>
+74.7	8.0	379.2 ✓ <del>380.2</del>
+99.7	7.3	379.9 ✓ <del>380.9</del>
480+03		
+24.7	8.3	378.9 ✓ <del>379.9</del>
+49.7	8.0	379.2 ✓ <del>380.2</del>
+56.2	8.2	379.0 ✓ <del>380.0</del>
B.M #53	381.700 381.717	
3445	385.145 <del>385.162</del>	
481+00	5.9	379.2 ✓ <del>379.2</del>
+33		3
482+00	6.8	378.X ✓ <del>379.8</del>
+93		2 ✓
483+00	5.9	379.8 ✓
		4 ✓
484+00	6.7	378.8 ✓
+61		1 ✓
485+00	8.0	379.8 ✓
		2 ✓
486+00	7.9	377.8 ✓

380.4 ✓ <del>381.4</del>				
68 100	380.4 ✓	74 50	379.8 ✓ <del>380.8</del>	97 70
68 100	380.3 ✓	70 25	380.2 ✓ <del>381.2</del>	70 100
62 100	380.4 ✓	70 25	380.0 ✓	87 80
68 100	380.3 ✓	72 40	380.1 ✓	95 105
67 100	380.3 ✓	71 30	380.2 ✓	75 10
47 100	380.5 ✓	72 40	380.1 ✓	75 100
47 100	380.5 ✓	72 40	380.1 ✓	75 100
52 100	380.2 ✓	71 40	380.1 ✓	75 100
52 100	379.6 ✓	71 40	380.1 ✓	75 100
52 100	379.3 ✓	71 40	380.1 ✓	75 100
52 100	379.1 ✓	71 40	380.1 ✓	75 100
61 100		67 45		



	T	-	Elev.
	385.145		378.555
	385.162		378.572
	383.086	6.590	
4.531	383.703		
486+28			
+45			
487+00		5.5	377.6
+95			
488+00		5.2	377.9
			<del>377.7</del>
489+00		5.5	377.6
+60			
490+00		5.7	377.4
+30			
491+00		6.6	376.6
+25			
492+00		7.5	375.6
+79			
+98			
+85			375.3
+50.9		7.8	375.4
T.P		5.454	377.632
	383.386		377.649
5.754	383.403		
+75.9		6.9	376.5
+86		8.9	374.5

9.1  
4/42

378.9  
42  
100

378.8  
42  
100

378.4  
42  
100

edge pave  
50  
100

377.8  
53  
100

edge pave  
54  
100

Flow line  
6' culvert  
53  
100

377.8

9.1  
4/42

378.5  
46  
60

378.6  
45  
50

378.4  
42  
30

377.8  
53  
30

377.3  
50  
40

377.2  
50  
40

377.0  
50  
40

377.2  
50  
30

377.0  
50  
30

377.0  
91  
40

377.2  
50  
30

377.0  
54  
40

377.0  
93  
55

377.8  
52  
100

377.9  
52  
100

377.5  
52  
100

377.7  
54  
100

376.8  
63  
100

375.8  
73  
100

375.8  
73  
100

375.8  
73  
100

376.1  
80  
70

375.4  
82  
100

376.2  
82  
100

374.8  
86  
100

Tel. pole.  
50  
18" Tree  
50

Tel. pole  
50

Tel. pole  
40

18" tree.  
80

Tel. pole  
50

4" Guy pole  
70  
Tel. pole

	+	T	-	Elev.
		303.386		
		<del>303.403</del>		
493+	00.9		7.9	375.5
	+25.9		8.7	374.7
	+50.9		8.9	374.5
	+75.9		9.0	374.4
494+	00.9		8.6	374.8
	+25.9		8.4	375.0
	+50.9		8.3	375.1
	+75.9		7.4	376.0
495+	02.1 =			
	495+		6.6	376.8
	+17		6.9	376.5
	B.M #55		3.910	379.476
				379.454
	495+			379.493
	+37		6.9	377.0
	+51			376.0
	+61		6.2	377.2
	+75			

	2	7
	5.5 377.9	8.3 375.1
	10.0 ← edge pole	10.0
	5.5 377.9	8.2 375.3
	10.0 ←	10.0
	5.5 377.9	8.2 374.7
	10.0	10.0
	5.5 377.8	8.2 375.1
	10.0	10.0
	6.4 377.3	8.3 375.1
	6.0	10.0
	5.5 377.8	8.3 375.1
	10.0	10.0
	5.5 377.6	8.1 375.3
	10.0	10.0
	5.2 377.7	8.2 374.5
	10.0	10.0
	5.2 377.7	7.2 375.7
	10.0	10.0
	5.2 377.7	7.2 376.4
	10.0	10.0
	5.2 377.7	7.0 376.4
	10.0	10.0
	5.2 377.7	7.5 375.9
	10.0	10.0
	5.0 378.4	7.3 376.1
	10.0	10.0
	4.2 379.2	7.3 375.4
	9.0	10.0
	5.3 378.1	8.0 375.4
	2.0	10.0
	2.6 380.8	8.0 375.4
	10.0	10.0
	5.3 378.2	
	6.0	
	Tel. pole 9.2	

	+	T	-	Elev.
		383.384		
		<del>383.403</del>		
496+00			7.4	376.0 ✓
497+00			9.6	373.8 ✓
B.M.#55				<del>379.454</del> ✓
				<del>379.508</del> ✓
	7.247	386.701 ✓		
		<del>386.755</del>		
498+00			12.2	<del>374.1</del> ✓
				374.5 ✓
498+87			12.4	374.4 ✓
499+12			11.9	374.4 ✓
				374.9 ✓
+37			11.8	<del>375.0</del> ✓
+52				0 ✓
+62			8.7	378.1 ✓
+72				5 ✓
+87			9.2	377.1 ✓
500+12.0			8.2	378.0 ✓
				5 ✓
+37.0			7.0	379.0 ✓
				6 ✓
+62			6.1	<del>380.1</del> ✓
				380.6 ✓
+87			5.2	381.0 ✓

68	376.6 ✓		
100			
82	379.7 ✓		
100			
112	375.56 ✓		
100			
124	379.43 ✓		
100			
122	374.45 ✓		
100			
122	376.48 ✓		
100			
92	376.48 ✓		
100			
76	379.41 ✓		
100			
79	378.48 ✓		
100			
68	379.9 ✓		
100			
42	382.40 ✓		
100			
40	382.87 ✓		
100			
40	383.8 ✓		
100			
74	379.43 ✓		
100			
73	379.54 ✓		
100			
82	375.0 ✓		
40			
82	374.9 ✓		
100			
13	373.46 ✓		
50			
13	373.56 ✓		
30			
13	373.16 ✓		
60			
108	375.9 ✓		
30			
12	373.98 ✓		
100			
12	373.98 ✓		
100			
12	374.5 ✓		
100			
12	374.4 ✓		
100			
93	377.5 ✓		
20			
113	375.4 ✓		
30			
13	373.87 ✓		
100			
83	378.54 ✓		
15			
115	375.42 ✓		
100			
73	379.5 ✓		
30			
86	378.1 ✓		
60			
113	375.4 ✓		
100			
74	376.45 ✓		
100			
73	379.47 ✓		
100			
73	379.54 ✓		
80			

Boulder 5' high on 4'

Boulder 4' high on 2' left

± on rock.

"R" 100  
100

(8)

	+	T	-	Elev.
		386.701		
		<del>386.765</del>		
T.P.		4.374		382.327
		3.374		382.31
	11.465	393.792		
		393.816		
501+09.1		12.0		381.8
501+86.3		8.7		385.1
502+11.3		8.6		385.2
+36.3		8.3		385.5
+44		8.2		385.6
+61.3		7.7		386.1
+86.3		7.7		386.1
+99		9.0		384.8
503+01.3		8.4		385.4
+11.3		9.1		384.7
+36.3		10.8		383.0
T.P.		10.350		383.442
				383.446

Note - Rod reading accidentally erased. Thinking was changing the elevations in the (100<sup>th</sup>) place

$\frac{92}{102} 384.1$	$\frac{154}{102} 378.4$
$\frac{55}{102} 388.3$	$\frac{65}{82} 387.3$
$\frac{46}{102} 389.2$	$\frac{91}{22} 384.7$
$\frac{46}{102} 389.2$	$\frac{106}{82} 383.2$
$\frac{52}{102} 388.6$	$\frac{107}{89} 383.1$
$\frac{49}{102} 388.9$	$\frac{118}{102} 382.0$
$\frac{40}{102} 389.8$	$\frac{98}{62} 384.0$
$\frac{41}{102} 389.7$	$\frac{131}{85} 380.7$
$\frac{50}{102} 388.8$	$\frac{144}{102} 379.4$
$\frac{48}{102} 389.0$	$\frac{170}{102} 376.8$
$\frac{51}{102} 388.87$	$\frac{101}{55} 383.7$
$\frac{69}{102} 386.9$	$\frac{109}{52} 382.9$
	$\frac{171}{102} 376.7$
	$\frac{142}{102} 378.9$
	$\frac{112}{102} 382.1$
	$\frac{127}{102} 381.1$
	$\frac{129}{62} 380.9$
	$\frac{168}{102} 377.0$

	+	T. 2	-	Flev
				383.442
				383.496
	6.585	390.027		382.0
503+61.3		390.001	8.0	<del>382.1</del>
+86.3			9.9	380.1
504+1.1.3			11.5	378.5
+26.0			11.9	378.1
505+0.0			10.9	379.1
+549			11.0	379.0
+79.9			9.9	380.1
506+0.9			8.6	381.4
+29.9			7.7	382.3
+549			7.0	383.0
+79.9			7.0	383.0
507+0.9			6.7	383.3

	+	T. 2	-	Flev
				383.442
				383.496
	6.585	390.027		382.0
503+61.3		390.001	8.0	<del>382.1</del>
+86.3			9.9	380.1
504+1.1.3			11.5	378.5
+26.0			11.9	378.1
505+0.0			10.9	379.1
+549			11.0	379.0
+79.9			9.9	380.1
506+0.9			8.6	381.4
+29.9			7.7	382.3
+549			7.0	383.0
+79.9			7.0	383.0
507+0.9			6.7	383.3

	+	T	-	Elev.
		390.027		
		390.001		
507+299			10.3	379.7 ✓ 379.8
+54.9			11.9	378.1 ✓ 379.2
T.P. on rock (sta 507+549)			11.356	378.671
	5.165	383.836		
B.M. #56			10.021	373.815 ✓ 373.757 374.021
B.M. #56				
	5.435	379.192 379.756		
B.M. #57			2.759	376.433 ✓ 376.677 ✓ 376.461 ✓
	7.655	384.116		
+81.0			7.0	377.1 ✓
508+00			7.4	376.7 ✓
509+00			11.6	372.5 ✓
510+00			10.7	373.4 ✓
510+95.4			13.3	370.8 ✓
51100			13.6	370.5 ✓
B.M. #57				376.461 ✓ 376.420
	1.014	377.434 377.475		

Recorded:  
373.757  
374.021

Note: This B.M. has since been destroyed and new one established

377.434  
1.014  
376.420

$\frac{7.6}{100}$	382.5 ✓	
$\frac{100}{100}$	380.1 ✓	
$\frac{11.8}{75}$	378.42 ✓	
$\frac{12.5}{35}$	377.45 ✓	
$\frac{14.3}{100}$	375.27 ✓	
$\frac{16.4}{100}$	373.1 ✓	
$\frac{4.2}{100}$	379.4 ✓	
$\frac{6.1}{50}$	378.0 ✓	
$\frac{5.2}{100}$	378.4 ✓	
$\frac{6.2}{70}$	377.9 ✓	
$\frac{10.0}{100}$	374.1 ✓	
$\frac{10.4}{100}$	373.7 ✓	
$\frac{10.4}{100}$	373.1 ✓	
$\frac{11.0}{100}$	373.1 ✓	
$\frac{11.0}{100}$	373.1 ✓	
$\frac{12.0}{100}$	372.1 ✓	
$\frac{11.9}{100}$	372.2 ✓	
$\frac{14.3}{100}$	374.3 ✓	
$\frac{9.8}{100}$	375.9 ✓	
$\frac{12.0}{100}$	372.1 ✓	
$\frac{11.9}{100}$	372.2 ✓	
$\frac{14.3}{100}$	374.3 ✓	
$\frac{12.0}{100}$	372.1 ✓	
$\frac{14.3}{100}$	374.3 ✓	

Note: The rod reading encircled is wrong. The elevation of the T.P. near sta. 507+549 should be 378.671. This error is unaccounted for. The elev. of all the stations were checked and found to be OK. The Bench is out .2.

373.0  
371.3

Leach T  
Reynolds  
Ruplinger  
March 8, 26

Cloudy and Warm

(12)

	+	T	-	Elev.
		377.434		
		<del>377.473</del>		
507	+41		8.3	369.17 <del>369.2</del>
	512+00		13.1	364.3 <del>364.4</del>
T.	+48		12.6	364.8 <del>364.9</del>
B.	513+00		12.2	365.4 <del>365.3</del>
B.	513+51.3		12.0	364.4 <del>365.5</del>
B.	+7.63		12.1	364.23 <del>365.4</del>
	514+01.3		12.0	364.4 <del>365.5</del>
	+26.3		12.5	364.9 <del>365.0</del>
50	+50		12.4	363.70 <del>365.1</del>
50	+51.3		11.965	365.510 <del>365.469</del>
	+65.5		6.7	364.17 <del>363.2</del>
51	B.M.# 58 March 8, 26		6.0	363.8 <del>364.9</del>
	B.M.# 58			
51	515+00	5.465		370.934
B	516+00			

B.M.# 58. El. 365.469  
- Rod  
11.765  
377.434

62	371.2			
100				
82	369.82			
100				
90	368.4			
100				
95	367.9			
100				
93	368.4			
100				
92	368.1			
100				
95	367.9			
100				
92	368.40			
100				
95	367.9			
100				
94	368.40			
100				
95	367.9			
100				
92	367.87			
100				
35	367.5			
100				
33	367.3			
80				
42	366.8			
100				
43	366.8			
80				
52	365.8			
30				
64	369.6			
20				
70	369.0			
80				
72	363.3			
100				
73	363.7			
100				
79	363.1			
100				

Flow line  
12' culvert

	+	π	-	Elev
		367.97		
		370.934		
50	517+0.0		6.9	322.7 ✓ 364.0
	+91			
	518+0.0		8.1	311.7 ✓ 362.8
T	519+0.0		8.3	307.5 ✓ 362.6
B	520+0.0		10.4	302.4 ✓ 360.5
B	521+0.0		10.8	307.0 ✓ 360.1
	522+0.0		11.3	308.5 ✓ 359.6
	B.M.# 58		4.758	366.176 366.164
	1.001	367.44		367.165
5	523+0.0		6.5	360.0 ✓ 360.7
5	524+0.0		5.5	361.0 ✓ 361.7
5	525+0.0		7.2	357.2 ✓ 360.0
5	526+0.0		6.5	360.0 ✓ 360.7
5	527+0.0		6.7	357.3 ✓ 360.5

42	366.3	10°
52	365.8	6°
62	365.8	3°
75	363.5	4°
78	363.7	8°
76	363.4	10°
52	365.8	10°
53	365.7	8°
75	363.4	2°
82	362.8	4°
52	365.3	10°
52	365.1	7°
75	363.4	9°
86	362.4	2°
83	362.7	3°
52	365.1	6°
107	360.6	10°
69	363.11	10°
75	362.4	8°
106	360.4	2°
106	360.4	7°
75	362.4	10°
75	362.4	8°
103	361.0	4°
98	361.2	8°
96	361.9	10°
78	363.12	10°
82	362.8	7°
100	360.6	3°
107	360.6	5°
93	361.8	10°
44	362.8	10°
42	362.5	7°
61	361.1	2°
65	360.7	9°
52	362.1	10°
46	362.3	10°
52	361.8	6°
48	362.4	5°
59	361.3	2°
52	361.5	10°
47	362.3	10°
54	361.8	5°
68	360.4	2°
73	359.7	8°
71	360.1	10°
46	362.6	10°
52	362.0	5°
64	361.1	2°
65	361.0	5°
42	362.5	10°
50	362.7	3°
64	360.8	10°

2

Power Pole

Recorded



	+	↑	-)	Elev.
50	528+00	366.47 ✓ 367.165	6.5	360.7 ✓ 318.8 ✓
	T.P. sta. 528+00	3.310	3.296	363.869 ✓
7	529+00	367.179 ✓ 311.48 ✓	7.1	360.1 ✓ 359.2 ✓
E	530+00		6.8	360.4 ✓ 357.6 ✓
B	531+00		6.5	360.7 ✓ 355.8 ✓
B	755.0		6.9	360.3 ✓ 355.6 ✓
	532+00		7.1	360.1 ✓ 359.4 ✓
5	533+00		7.1	360.1 ✓ 357.4 ✓
5	534+00		7.2	360.0 ✓ 357.5 ✓
	T.P.	4.416	4.416	362.763 ✓ 361.347 ✓
5		4.556	4.820	362.499 ✓ 362.544 ✓
5	B.M.#60			
		5.570	5.570	368.114 ✓ 361.13 ✓
5	535+00		8.1	360.0 ✓ 357.8 ✓
B	+90			
	536+00			

46	362.16 ✓	50	362.12 ✓	63	360.9 ✓
100		60		100	
46	362.16 ✓	51	362.11 ✓	73	360.2 ✓
100		49		100	
46	362.16 ✓	52	361.3 ✓	56	361.6 ✓
100		30		100	
45	362.7 ✓	53	361.9 ✓	73	360.0 ✓
100		30		100	
95	362.7 ✓	52	361.5 ✓	75	359.7 ✓
100		30		100	
44	362.7 ✓	57	361.8 ✓	82	359.0 ✓
100		25		100	
45	362.7 ✓	53	361.9 ✓	79	359.3 ✓
100		30		30	
45	362.7 ✓	55	361.7 ✓	92	357.5 ✓
100		40		50	
53	362.78 ✓	63	361.9 ✓	99	358.12 ✓
100		30		10	
92	358.2 ✓	98	358.3 ✓		
50	Flow line				

Note: For pag line and check within .009 of my elev.

culvert

T  
368.114

536+00 9.3 358.8 ✓

537+00 7.7 360.4 ✓

538+00 7.7 360.4 ✓

539+00 6.9 361.2 ✓

540+00 5.4 362.7 ✓

541+00 4.8 363.3 ✓

542+00 4.8 363.3 ✓

543+00 5.4 362.7 ✓

544+00 6.3 361.8 ✓

B.M # 106 6.374 361.740 ✓

366.235 ✓

~~366.299~~

4.520

545+00 5.2 361.1 ✓

546+00 5.4 360.9 ✓

Recorded  
361.735

361.735 ✓

(15)

5 362.8 ✓  
100  
on pave.

5 362.8 ✓  
100  
pave.

5 362.8 ✓  
100  
on pave.

4 363.4 ✓  
100  
pave.

5 363.0 ✓  
88  
pave.

5 362.5 ✓  
82  
pave.

4 362.0 ✓  
85  
pave.

4 361.8 ✓  
82

5 362.2 ✓  
50  
362.2 ✓

6 362.7 ✓  
30  
362.7 ✓

5 362.4 ✓  
25  
362.4 ✓

5 363.4 ✓  
35  
363.4 ✓

5 362.8 ✓  
40  
362.8 ✓

6 362.4 ✓  
40  
362.4 ✓

4 361.4 ✓  
40  
361.4 ✓

5 361.2 ✓  
40  
361.2 ✓

5 360.6 ✓  
40  
360.6 ✓

9 358.5 ✓  
20  
358.5 ✓

9 358.5 ✓  
40  
358.9 ✓

8 360.4 ✓  
30  
360.4 ✓

5 362.4 ✓  
20  
362.4 ✓

5 363.4 ✓  
50  
363.4 ✓

6 361.8 ✓  
60  
361.8 ✓

5 360.7 ✓  
10  
360.7 ✓

5 360.8 ✓  
100  
360.8 ✓

357.9 ✓  
100  
358.0 ✓

358.7 ✓  
100  
358.7 ✓

360.9 ✓  
100  
361.0 ✓

362.9 ✓  
100  
363.0 ✓

362.9 ✓  
100  
363.0 ✓

362.9 ✓  
100  
363.0 ✓

362.9 ✓  
100  
363.0 ✓

362.9 ✓  
100  
363.0 ✓

362.9 ✓  
100  
363.0 ✓

+	T	-	Elev.
	<del>366.255</del> <del>366.299</del>		
547+00		5.6	360.7 ✓
548+00		4.7	361.0 ✓
549+00		5.2	361.1 ✓
550+00		5.5	360.8 ✓
551+00		6.0	360.3 ✓
552+00		6.5	359.8 ✓
553+00		6.2	360.1 ✓
T.P.		3.158	<del>363.097</del> <del>363.141</del>
	B.063		
+38	371.160 <del>371.204</del>		
554+00		8.9	362.3 ✓
+75		7.0	364.2 ✓
555+00		6.5	364.7 ✓
556+00		5.1	366.1 ✓

361.0 ✓ $\frac{42}{85}$	361.0 ✓ $\frac{52}{32}$	360.6 ✓ $\frac{57}{42}$	360.7 ✓ $\frac{56}{102}$
361.5 ✓ $\frac{42}{85}$	<del>361.0</del> 361.1 ✓ $\frac{52}{22}$	361.2 ✓ $\frac{57}{35}$	361.1 ✓ $\frac{52}{102}$
edge pare. 361.4 ✓ $\frac{41}{84}$	361.1 ✓ $\frac{52}{32}$		360.7 ✓ $\frac{56}{102}$
361.3 ✓ $\frac{52}{85}$	361.1 ✓ $\frac{52}{42}$	360.6 ✓ $\frac{52}{22}$	360.0 ✓ $\frac{62}{102}$
361.2 ✓ $\frac{51}{80}$	360.4 ✓ $\frac{52}{25}$		359.3 ✓ $\frac{70}{102}$
361.2 ✓ $\frac{51}{85}$	360.6 ✓ $\frac{52}{32}$	359.4 ✓ $\frac{62}{25}$	358.7 ✓ $\frac{76}{42}$
361.7 ✓ $\frac{46}{80}$	360.9 ✓ $\frac{54}{22}$	358.9 ✓ $\frac{74}{62}$	358.3 ✓ $\frac{82}{10}$
		358.4 ✓ $\frac{72}{92}$	358.7 ✓ $\frac{76}{102}$
	Flow line $\frac{126}{35}$ culvert (3')	258.6	
363.2 ✓ $\frac{80}{80}$	362.8 ✓ $\frac{84}{22}$	361.5 ✓ $\frac{102}{45}$	360.0 ✓ $\frac{112}{102}$
364.7 ✓ $\frac{65}{80}$		364.5 ✓ $\frac{62}{82}$	364.7 ✓ $\frac{62}{102}$
edge pare. 365.1 ✓ $\frac{61}{80}$	364.5 ✓ $\frac{67}{15}$	365.0 ✓ $\frac{62}{72}$	366.2 ✓ $\frac{50}{92}$
366.2 ✓ $\frac{52}{85}$	365.9 ✓ $\frac{52}{22}$	366.2 ✓ $\frac{44}{62}$	368.6 ✓ $\frac{26}{102}$

	+	T	-	Elev.
B.M. #62		371.160 <del>371.201</del>		368.959 Recorded 2.201 <del>369.003</del> 368.990
	2.394	371.384 <del>371.126</del>		368.990
556+76			5.0	366.4 ✓ <del>366.2</del>
+90			5.0	366.4 ✓ <del>366.2</del>
557+00			5.2	366.2 ✓ <del>366.0</del>
558+00			5.5	365.9 ✓
559+00			6.8	364.6 ✓
+16			6.9	364.5 ✓
+20			9.5	361.9 ✓
+24			6.8	364.6 ✓
560+00			6.1	365.3 ✓
561+00			4.1	367.3 ✓
+21.5			3.1	368.3 ✓

366.4 ✓ 50 80 pavement.	366.5 ✓ 42 22	366.4 ✓ 52 102
366.4 ✓ 50 80 366.4 ✓	center of 15' driveway	365.9 ✓ 55 109 365.9 ✓
366.4 ✓ 50 80	366.11 ✓ 53 85	363.6 ✓ 78 109 363.11 ✓ 82 109
366.6 ✓ 48 80 pavement.	365.8 ✓ 52 25	362.7 ✓ 82 40 362.5 ✓ 82 109
366.7 ✓ 42 80	365.7 ✓ 52 50	363.0 ✓ 64 109
366.7 ✓ 47 80	365.8 ✓ 56 28	362.4 ✓ 90 23
366.7 ✓ 42 80	365.8 ✓ 56 30	Flow line 12' culvert
367.2 ✓ 42 80 pavement.	366.3 ✓ 51 29	364.3 ✓ 71 29
368.5 ✓ 21 75	368.0 ✓ 34 29	363.5 ✓ 79 59
368.8 ✓ 26 75 pavement.	366.3 ✓ 51 30	362.3 ✓ 91 99
		362.5 ✓ 91 109
		369.3 ✓ 51 109
		367.6 ✓ 38 109
		center of 15' driveway

+	↑	-	Elev.
	<del>371.384</del> <del>371.426</del>		
561+52		2.6	368.8 ✓
562+00		0.3	371.1 ✓
	<del>376.952</del>	3.517	<del>367.909</del> ✓
563+00	9.085 <del>376.994</del>	4.7	372.3 ✓
564+00		4.9	372.1 ✓
565+00		6.0	371.0 ✓
566+00		6.1	370.9 ✓
567+00		6.3	370.7 ✓
+54		6.5	370.5 ✓
+80		6.7	370.3 ✓
568+00		6.9	370.1 ✓
	<del>374.178</del>	7.067	<del>369.085</del> ✓
	5.093 <del>374.220</del>		
+34		4.2	370.0 ✓

↑	↓	↑	↓	↑	↓
369.3 ✓		369.5 ✓		370.9 ✓	
$\frac{21}{72}$		$\frac{19}{25}$		$\frac{61}{75}$	
370.0 ✓		370.9 ✓		372.4 ✓	
$\frac{14}{75}$		$\frac{05}{70}$		$\frac{46}{20}$	
370.9 ✓		370.6 ✓		372.2 ✓	
$\frac{61}{75}$		$\frac{64}{25}$		$\frac{48}{100}$	
edge pavement					
371.2 ✓		370.9 ✓		372.1 ✓	
$\frac{58}{75}$		$\frac{61}{30}$		$\frac{42}{15}$	
371.3 ✓					
$\frac{52}{70}$					
371.0 ✓					
$\frac{60}{70}$					
370.7 ✓					
$\frac{60}{72}$					
370.5 ✓					
$\frac{65}{70}$					
370.3 ✓					
$\frac{71}{70}$					
370.1 ✓					
$\frac{65}{70}$					
369.9 ✓					
$\frac{65}{70}$					
369.5 ✓					
$\frac{71}{70}$					
370.2 ✓					
$\frac{40}{70}$					
369.9 ✓					
$\frac{71}{60}$					
369.5 ✓					
$\frac{42}{40}$					
368.8 ✓					
$\frac{54}{100}$					

+	T	-	Elev.
	374.178		
	<del>374.220</del>		
569+00		5.2	369.0
570+00		6.3	367.9
			<del>365.9</del>
571+00		5.8	368.4
BM # 63		8.492	365.686
# 63			365.728
			365.698
	8.903		<del>365.728</del>
	374.601		
	<del>374.665</del>		
+29		6.2	368.4
572+00		5.9	368.7
+34		5.5	369.1
573+00		5.3	369.3
+19		5.4	369.2
573+50		5.5	369.1
574+00		5.6	369.0
575+00		5.2	369.4
	5.471		369.130
			<del>367.194</del>

369.8 ✓  
~~44~~  
 73 ✓  
 pare. ✓  
~~369.17~~  
~~44~~  
 73 ✓  
 369.7 ✓  
~~44~~  
 72 ✓  
 369.8 ✓  
~~44~~  
 72 ✓  
 pare. ✓  
~~369.87~~  
~~44~~  
 72 ✓  
 369.8 ✓  
~~44~~  
 68 ✓  
 369.8 ✓  
~~44~~  
 68 ✓  
 369.8 ✓  
~~44~~  
 74 ✓  
 369.8 ✓  
~~44~~  
 70 ✓  
 369.8 ✓  
~~44~~  
 70 ✓  
 369.8 ✓  
~~44~~  
 70 ✓  
 pare. ✓

369.4 ✓  
~~48~~  
 30 ✓  
 369.1 ✓  
~~52~~  
 30 ✓  
 369.2 ✓  
~~50~~  
 30 ✓  
 365.1 ✓  
~~92~~  
 90 ✓  
 365.0 ✓  
~~92~~  
 50 ✓  
 363.2 ✓  
~~110~~  
 80 ✓  
 365.0 ✓  
~~92~~  
 100 ✓  
 364.4 ✓  
~~98~~  
 100 ✓  
 363.7 ✓  
~~115~~  
 100 ✓  
 362.9 ✓  
~~112~~  
 92 ✓  
 364.5 ✓  
~~102~~  
 90 ✓  
 364.1 ✓  
~~106~~  
 90 ✓  
 368.2 ✓  
~~65~~  
 50 ✓  
 368.8 ✓  
~~52~~  
 70 ✓  
 368.9 ✓  
~~52~~  
 100 ✓  
 367.5 ✓  
~~72~~  
 50 ✓  
 368.1 ✓  
~~63~~  
 70 ✓  
 368.9 ✓  
~~52~~  
 100 ✓  
 366.4 ✓  
~~80~~  
 100 ✓  
 368.1 ✓  
~~60~~  
 100 ✓  
 369.4 ✓  
~~55~~  
 100 ✓

Leach  
Reynolds  
Rupling or  
Mar. 9, '26

Cloudy

♀

(20)

Sta.	+	π	-	Elev.
Mar. 9, 1926				<del>369.130</del> <del>367.194</del>
	5.718	<del>374.848</del> <del>374.912</del>		<del>369.16</del> <del>357.6</del>
576+00			5.2	<del>369.15</del> <del>359.5</del>
577+00			5.3	<del>369.5</del> <del>359.5</del>
578+00			5.3	<del>369.5</del> <del>359.5</del>
+58			4.8	<del>370.0</del> <del>360.0</del>
579+00			5.0	<del>369.8</del> <del>359.8</del>
580+00			7.1	<del>367.7</del> <del>357.7</del>
B.M. # 64			9.548	<del>365.300</del> <del>365.298</del> <del>365.298</del> <del>365.298</del>
" # 64	5.228	<del>370.526</del> <del>370.597</del>		<del>365.300</del> <del>365.298</del> <del>365.298</del>
581+00			4.1	<del>366.4</del>
582+00			4.3	<del>366.2</del>
583+00			5.1	<del>365.4</del>
584+00			5.6	<del>364.9</del>
585+00			6.3	<del>364.2</del>

~~367.9~~  
~~49~~  
~~69~~  
 pave.  
~~42~~ 370  
~~62~~  
 pave  
~~45~~  
~~69~~  
~~370.11~~  
~~42~~  
~~62~~  
 pave  
~~369.87~~  
~~51~~  
~~62~~  
~~368.24~~  
~~64~~  
~~65~~  
~~22~~ 367  
~~62~~  
 pave  
~~36~~  
~~62~~  
~~42~~ 366  
~~62~~  
~~365.5~~  
~~50~~  
~~64~~  
~~364.11~~  
~~58~~  
~~64~~

center of road. (40')

~~369.87~~  
~~51~~  
~~20~~  
~~369.13~~  
~~55~~  
~~48~~  
~~369.1~~  
~~57~~  
~~100~~  
~~369.1~~  
~~57~~  
~~100~~  
~~368.16~~  
~~62~~  
~~55~~  
~~369.87~~  
~~54~~  
~~100~~  
~~369.15~~  
~~53~~  
~~100~~  
~~367.98~~  
~~70~~  
~~20~~  
~~365.43~~  
~~52~~ 365  
~~63~~  
~~100~~  
~~366.18~~  
~~42~~  
~~55~~  
~~100~~  
~~364.8~~  
~~52~~  
~~20~~  
~~50~~  
~~95~~  
~~100~~  
~~365.104~~  
~~55~~  
~~20~~  
~~50~~  
~~362.82~~  
~~80~~  
~~83~~  
~~100~~  
~~364.11~~  
~~64~~  
~~20~~  
~~63~~ 363  
~~62~~  
~~60~~  
~~70~~  
~~100~~

+	T	-	Elev.
	<u>370.52</u>		363.1 ✓
586+00		7.4	363.300 ✓
T.P.		7.226	<del>363.371</del>
	<u>372.067</u>		
8767	<u>372.138</u>		
587+00		9.3	362.8 ✓
+15		9.0	
588+00		9.0	363.1 ✓
+44.9		8.8	363.3 ✓
+54.9		8.5	363.6 ✓
+64.9		8.8	363.3 ✓
74.9		8.4	363.7 ✓
84.9		8.1	364.0 ✓
94.9		7.6	364.5 ✓
589+04.9		5.9	367.2 ✓
			<del>369.7</del>
+14.9		5.7	364.4 ✓

364.10 ✓  
 $\frac{65}{63}$   
 pavo.

363.7 ✓  
 $\frac{84}{63}$

364.5 ✓  
 $\frac{78}{78}$

~~365.0~~  
 $\frac{75}{100}$  364.6 ✓

364.7 ✓  
 $\frac{74}{100}$

364.6 ✓  
 $\frac{75}{100}$

364.7 ✓  
 $\frac{74}{100}$

364.6 ✓  
 $\frac{75}{100}$

364.4 ✓  
 $\frac{72}{100}$

363.9 ✓  
 $\frac{68}{100}$

364.9 ✓  
 $\frac{52}{100}$

364.9 ✓  
 $\frac{52}{100}$

363.2 ✓  
 $\frac{82}{05}$

360.8 ✓  
 $\frac{43}{18}$  Flow line

363.9 ✓  
 $\frac{82}{20}$

364.4 ✓  
 $\frac{72}{60}$

363.9 ✓  
 $\frac{82}{40}$

364.3 ✓  
 $\frac{78}{60}$

364.3 ✓  
 $\frac{78}{60}$

364.3 ✓  
 $\frac{78}{70}$

364.4 ✓  
 $\frac{72}{60}$

365.9 ✓  
 $\frac{62}{69}$

367.2 ✓  
 $\frac{49}{63}$

Top of 1<sup>st</sup> rail.

362.18 ✓  
 $\frac{72}{20}$

362.16 ✓  
 $\frac{72}{50}$

361.18 ✓  
 $\frac{82}{100}$

361.18 ✓  
 $\frac{112}{100}$

361.7 ✓  
 $\frac{104}{100}$

362.5 ✓  
 $\frac{96}{100}$

364.7 ✓  
 $\frac{94}{100}$

363.3 ✓  
 $\frac{88}{100}$

363.9 ✓  
 $\frac{83}{100}$

365.5 ✓  
 $\frac{66}{100}$

366.1 ✓  
 $\frac{60}{100}$

366.5 ✓  
 $\frac{54}{100}$

367.0 ✓  
 $\frac{51}{100}$

(21)



+ T - Elev.

372.067  
~~372.170~~

+20.7	4.9 ← Top of rail	367.2 ✓
+29.9	5.2	367.9 ✓
+27.3	4.8 ← Top rail	367.3 ✓
+34.9	4.8	367.3 ✓
+35.6	Top rail → 4.5	367.6 ✓
+41.8	Top rail → 4.5	367.6 ✓
+44.9	4.7	367.4 ✓
+53.7	Top rail 4.8	367.3 ✓
+54.9	5.0	367.1 ✓
+59.2	4.8	367.3 ✓
+64.9	4.7	367.4 ✓
+74.9	4.6	367.5 ✓
589+78.0 =		
589+79.7	4.6	367.5 ✓
589+90.7	4.8	367.3 ✓
590+15.7	4.9	367.2 ✓
+40.7	3.7	368.4 ✓
T.P.	2.863	369.204 ✓

3.555 ~~372.070~~  
372.759

366.0 ✓	366.5 ✓	367.3 ✓
$\frac{52}{100}$	$\frac{56}{90}$	$\frac{48}{33}$
366.9 ✓		Top rail
$\frac{52}{100}$		Top rail

367.0 ✓	367.4 ✓
$\frac{45}{100}$	$\frac{42}{40}$

367.8 ✓	367.5 ✓
$\frac{43}{100}$	$\frac{46}{100}$

Stations in road.

367.5 ✓  
~~368.5~~

367.4 ✓	367.5 ✓
$\frac{42}{100}$	$\frac{42}{100}$

368.4 ✓
$\frac{37}{100}$

367.1 ✓
$\frac{52}{100}$
67.3 ✓
$\frac{48}{100}$

366.5 ✓
$\frac{56}{100}$
366.7 ✓
$\frac{52}{100}$

367.0 ✓
$\frac{54}{100}$
367.0 ✓
$\frac{51}{100}$

367.0 ✓
$\frac{51}{100}$
367.3 ✓
$\frac{48}{100}$

366.9 ✓
$\frac{52}{100}$
368.0 ✓
$\frac{41}{100}$

Sta.	T	Elev.
B.M. # 65	<del>372.759</del> 372.752	<del>369.559</del> 369.552
	3.200	<del>369.630</del> 369.602
590+65.7	3.8	369.0
+90.7	3.8	369.0
591+15.7	4.3	368.5
+31.3	4.6	368.2
592+00	5.3	367.5
593+00	6.6	366.2
T.P.	7.881	<del>364.871</del> 364.801
B.M. # 66	4.336	<del>369.207</del> 369.237
594+00	4.1	<del>364.417</del> 364.402
595+00	5.5	363.7
+01		
+22 center at 15' rd.	5.9	363.3
596+00	6.4	362.8
+52		

$\frac{36}{100}$ 369.42	$\frac{41}{45}$ 368.2	$\frac{38}{100}$ 369.0
$\frac{35}{100}$ 369.43	$\frac{45}{45}$ 368.43	$\frac{36}{100}$ 369.2
$\frac{30}{100}$ 369.40	$\frac{25}{45}$ 368.45	$\frac{32}{100}$ 369.1
$\frac{40}{100}$ 368.58	$\frac{41}{18}$ 368.32	$\frac{39}{100}$ 368.9
$\frac{48}{100}$ 368.40	$\frac{50}{40}$ 367.8	$\frac{49}{100}$ 367.9
$\frac{63}{100}$ 366.45	$\frac{60}{63}$ 366.48	$\frac{61}{100}$ 366.7
$\frac{48}{100}$ 365.2	$\frac{43}{25}$ 364.9	$\frac{45}{100}$ 364.7
$\frac{40}{100}$ 363.9	$\frac{40}{20}$ 365.2	
$\frac{53}{100}$ 363.7	$\frac{55}{30}$ 363.9	$\frac{42}{100}$ 364.5
$\frac{55}{100}$ 363.7	$\frac{55}{40}$ 363.7	$\frac{35}{100}$ 363.0
$\frac{59}{100}$ 363.3	$\frac{60}{40}$ 363.2	$\frac{70}{100}$ 362.2
	$\frac{69}{20}$ 362.3	

52 Tel. pole

B.M.#66

+ 3.100  $\overline{367.502}$

Elev.  $\overline{369.402}$

596+54 5.2 362.3 ✓

+73 598+00 9.9 362.6 ✓

+72

+82. 5.0 362.5 ✓

+86 5.3 362.2 ✓

599+00 center of 20' road. 5.0  $\overline{362.5}$

0.750  $\overline{361.822}$  6.430  $\overline{361.072}$

600+00 0.4 361.4 ✓

601+00 2.2 359.6 ✓

+28 602+00 3.6 358.2 ✓

+40 +50

603+00 4.5 357.3 ✓

+60 604+00 6.1 355.7 ✓

$\overline{360.8}$   
Flow line culvert  
 $\overline{362.9}$   $\overline{362.5}$   $\overline{362.8}$   $\overline{361.7}$   $\overline{361.3}$

$\overline{362.7}$   $\overline{362.4}$   $\overline{363.1}$   $\overline{362.8}$   
Tel. pole

$\overline{362.7}$   $\overline{362.4}$   $\overline{364.0}$   $\overline{362.3}$   
Tel. pole

$\overline{362.6}$   $\overline{362.4}$   $\overline{362.3}$   $\overline{362.3}$   
Tel. pole

$\overline{361.87}$   $\overline{360.43}$   $\overline{361.32}$   $\overline{359.6}$

$\overline{358.5}$   $\overline{358.4}$   $\overline{358.6}$   $\overline{358.10}$   
Tel. pole

$\overline{357.3}$   $\overline{357.40}$   $\overline{358.10}$   $\overline{358.10}$   
Tel. pole

$\overline{355.9}$   $\overline{355.16}$   $\overline{355.18}$   $\overline{355.17}$   
Tel. pole

+		T	Elev.
		<del>361.822</del> ✓ 361.815	
604+85			
605+00	6.1	355.7 ✓	
606+40	6.8	355.0 ✓	
<del>B.T.P. #66</del>	7.175	354.647 ✓	
	2.088	356.837 ✓	
605+91			
606+00	3.7	353.0 ✓	
607+00	4.4	352.3 ✓	
+ 26			
608+00	5.9	350.8 ✓	
+ 49			
609+00	5.6	351.1 ✓	
+ 42			
+ 70	center of 15' road.	351.5 ✓	
610+00	6.3	350.4 ✓	
611+00	5.5	351.2 ✓	
612+00	7.2	349.5 ✓	
	8.050	348.685 ✓	

(25)

18

			Test pole		355.4 ✓
72	73	69	74		64
102	80	52	72	70	64
rd.	rd.	rd.	rd.	50	100
357.6 ✓	354.0 ✓	354.9 ✓	354.7 ✓	354.8	355.4 ✓
353.2 ✓	351.7 ✓	351.6 ✓	352.0 ✓	351.7 ✓	352.8
350.9 ✓	350.8 ✓	351.1 ✓	351.1 ✓	351.2	352.0 ✓
350.4 ✓	350.2 ✓	350.7 ✓	350.5 ✓	351.2	352.6 ✓
350.0 ✓	349.8 ✓	350.3 ✓	349.4 ✓	351.1	351.2 ✓
348.6 ✓	348.2 ✓	352.0 ✓	347.2 ✓	351.1	351.7 ✓
347.5 ✓	347.2 ✓	351.6 ✓	351.6 ✓	351.6	351.0 ✓
					351.3 ✓
					352.5 ✓
					352.0 ✓

Note: B.T. has been tampered with.

	+	+	-	Elev.	BM.
	1.457			<del>348.787</del>	<del>348.787</del>
				<del>350.142</del>	<del>350.142</del>
613+00			2.4	347.7	
+30					
614+00			4.9	345.2	
+52					
615+00			6.1	344.0	
+87					
616+00			5.2	344.9	
+98					
617+00			7.3	342.8	
BM #69				<del>343.470</del>	<del>343.482</del>
BM #67			6.672	<del>343.572</del>	<del>343.573</del>
+28				<del>343.482</del>	<del>343.482</del>
	3.820			<del>347.302</del>	<del>347.302</del>
+46					
618+00			4.7	342.6	
+20					
619+00			4.7	342.6	
-41					
620+00			4.6	342.7	
+03					
+63					
621+00			5.1	342.2	
+85					

	346.71			346.71	
	<del>346.87</del>			<del>346.87</del>	
	<del>345.7</del>			<del>345.7</del>	
	<del>345.9</del>			<del>345.9</del>	
	<del>344.6</del>			<del>344.6</del>	
	<del>343.1</del>			<del>343.1</del>	
	<del>343.1</del>			<del>343.1</del>	
	<del>341.7</del>			<del>341.7</del>	
	<del>342.7</del>			<del>342.7</del>	
	<del>342.4</del>			<del>342.4</del>	
	<del>342.1</del>			<del>342.1</del>	
	<del>342.1</del>			<del>342.1</del>	
	<del>342.2</del>			<del>342.2</del>	
	<del>342.3</del>			<del>342.3</del>	
	<del>342.2</del>			<del>342.2</del>	
	<del>341.9</del>			<del>341.9</del>	
	<del>342.8</del>			<del>342.8</del>	
	<del>342.7</del>			<del>342.7</del>	
	<del>342.9</del>			<del>342.9</del>	
	<del>342.4</del>			<del>342.4</del>	

	+	T	-	Elev.
		<del>347.302</del>		<del>341.9</del> ✓
		<del>347.413</del>		<del>342.0</del>
622+00			5.4	<del>341.9</del>
623+00			5.7	<del>341.6</del> ✓
+09				<del>341.7</del>
T.P.			5.469	<del>341.833</del>
		<del>345.688</del>		<del>341.999</del>
	3.855	<del>345.799</del>		<del>341.0</del> ✓
624+00			4.7	<del>341.1</del>
+32				<del>340.6</del> ✓
625+00			5.1	<del>340.7</del>
+59				<del>340.2</del> ✓
626+00			5.5	<del>340.3</del>
#71				<del>342.308</del> 342.314
B.M. #68			3.380	<del>342.419</del> 342.432
#71				<del>342.314</del>
B.M. #62				<del>342.432</del>
		<del>344.584</del>		<del>342.432</del>
	2.270	<del>344.702</del>		<del>340.4</del> ✓
626+07			4.9	<del>339.8</del>
627+00				<del>339.7</del> ✓
+39				<del>339.8</del>
628+00			5.2	<del>339.5</del> ✓
+11				<del>339.4</del> ✓
629+00			5.5	<del>339.2</del> ✓
+32				<del>339.1</del> ✓

(27)

<del>53</del> 342.11 ✓	<del>54</del> 341.9 ✓	<del>52</del> 341.76 ✓	<del>52</del> 342.13 ✓
<del>100</del>	<del>100</del>	<del>20</del>	<del>45</del>
<del>54</del> 341.9 ✓	<del>52</del> 341.81 ✓	<del>52</del> 341.81 ✓	<del>52</del> 341.87 ✓
<del>100</del>	<del>100</del>	<del>20</del>	<del>100</del>
<del>80</del> rd.	<del>80</del> rd.	<del>80</del> rd.	Tel. pole. 60
<del>43</del> 341.53 ✓	<del>42</del> 341.40 ✓	<del>42</del> 341.55 ✓	<del>43</del> 341.54 ✓
<del>100</del>	<del>40</del>	<del>40</del>	<del>100</del>
<del>48</del> 340.9 ✓	<del>48</del> 340.4 ✓	<del>48</del> 340.5 ✓	<del>48</del> 340.9 ✓
<del>100</del>	<del>100</del>	<del>30</del>	<del>100</del>
<del>80</del> rd.	<del>80</del> rd.	<del>80</del> rd.	701 pole 65
<del>51</del> 340.16 ✓	<del>52</del> 339.9 ✓	<del>52</del> 340.63 ✓	<del>53</del> 340.54 ✓
<del>100</del>	<del>100</del>	<del>100</del>	<del>100</del>
<del>80</del> rd.	<del>80</del> rd.	<del>80</del> rd.	701 pole 63
<del>43</del> 340.43 ✓	<del>42</del> 340.72 ✓	<del>42</del> 340.72 ✓	<del>45</del> 340.41 ✓
<del>100</del>	<del>70</del> rd.	<del>30</del>	<del>100</del>
<del>48</del> 339.48 ✓	<del>65</del> Flow line culvert. 15	<del>65</del> 5' culvert	<del>48</del> 339.9 ✓
<del>100</del>	<del>50</del> rd.	<del>40</del>	<del>42</del> 339.9 ✓
<del>54</del> 339.43 ✓	<del>52</del> 339.12 ✓	<del>52</del> 339.12 ✓	<del>42</del> 339.9 ✓
<del>100</del>	<del>100</del>	<del>20</del>	<del>100</del>
<del>80</del> rd.	<del>80</del> rd.	<del>80</del> rd.	38340.88
<del>53</del> 339.43 ✓	<del>64</del> 338.15 ✓	<del>52</del> 339.16 ✓	<del>42</del> 339.9 ✓
<del>100</del>	<del>100</del>	<del>30</del>	<del>100</del>
<del>80</del> rd.	<del>80</del> rd.	<del>80</del> rd.	Loose dirt
			62 Tel. pole
			340.15
			41
			60
			701 pole 60

Party  
Leach &  
Reynolds &  
Ruplinger  
Mar. 10. 21

Cool and Cloudy

+ T  
~~344.584~~  
~~344.702~~

Elev

630+00

6.2

338.4  
~~338.5~~

+51

631+00

6.8

337.8  
~~337.9~~

+72

632+00

6.6

338.0  
~~338.197~~

+12

T.P.

6.387

+95

4.775

342.972  
~~343.090~~

633+00

5.5

337.5  
~~337.6~~

Mar. 10.

634+00

6.0

337.0  
~~337.1~~

+13

635+00

6.2

336.8  
~~336.9~~

+39

636+00

6.4

336.6  
~~336.7~~

B.M.# 61

3.695

339.277 339.266  
~~339.295~~ ~~339.315~~

Mar. 10

2.440

341.704  
~~341.833~~

339.266  
~~339.313~~

636+60

637+00

+81.5

638+00

5.4

336.3  
~~336.7~~

5.8

335.9  
~~336.0~~

6.2  
~~338.15~~  
100

6.2  
~~338.011~~  
100

5.2  
~~337.7~~  
100

5.2  
~~337.5~~  
100

6.2  
~~337.1~~  
100

5.2  
~~336.9~~  
100

5.2  
~~336.16~~  
100

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

6.2  
~~337.9~~  
100

6.2  
~~336.8~~  
100

5.2  
~~337.41~~  
100

6.2  
~~336.9~~  
100

6.2  
~~336.6~~  
100

6.2  
~~336.4~~  
100

6.2  
~~337.2~~  
100

6.2  
~~335.16~~  
100

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

6.2  
~~338.0~~  
100

6.2  
~~337.18~~  
100

6.2  
~~338.11~~  
100

6.2  
~~337.4~~  
100

6.2  
~~338.2~~  
100

6.2  
~~337.87~~  
100

6.2  
~~337.2~~  
100

6.2  
~~336.16~~  
100

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

6.2  
~~338.17~~  
100

6.2  
~~339.13~~  
100

6.2  
~~338.1~~  
100

6.2  
~~337.18~~  
100

6.2  
~~338.1~~  
100

6.2  
~~337.16~~  
100

6.2  
~~337.2~~  
100

6.2  
~~336.16~~  
100

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

(28)

6.2  
~~338.17~~  
100

6.2  
~~337.1~~  
100

6.2  
~~337.9~~  
100

6.2  
~~336.9~~  
100

6.2  
~~337.54~~  
100

6.2  
~~336.9~~  
100

6.2  
~~336.17~~  
100

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

Flowline  
Tel. pole

6.2 Top of pile of loose dirt

	T	Elev.
	<del>341.706</del> 341.706	
639+00	5.8	<del>335.9</del> 335.9
640+00	6.1	<del>335.6</del> 335.6
+23		
641+00	6.5	<del>335.2</del> 335.2
T.P.	6.180	<del>335.526</del> 335.526
	4.995	<del>340.521</del> 340.521
#73	<del>340.648</del>	
B.M. #70	3.811	<del>336.710</del> 336.710 <del>336.837</del> 336.713 <del>336.827</del>
642+00	3.811	<del>336.837</del> 336.713
+39		
642+00	5.8	<del>334.7</del> 334.7
+55		
643+00	5.7	<del>334.8</del> 334.8
+74		
644+00	5.5	<del>335.0</del> 335.0
+97		
645+00	5.4	<del>335.1</del> 335.1
+56.2		
	5.6	<del>334.9</del> 334.9
646+00	5.7	<del>334.8</del> 334.8
+15		
T.P.	5.628	<del>334.896</del> 334.896

(29)

$\frac{52}{100}$ 335.18	$\frac{60}{20}$ 335.14	$\frac{53}{100}$ Tel. pole 53 336.4
$\frac{64}{100}$ 335.16	$\frac{64}{15}$ 335.13	$\frac{65}{20}$ Tel. pole 65 335.4
$\frac{60}{100}$ 335.17	$\frac{65}{20}$ 335.2	$\frac{65}{20}$ 335.6
	70	$\frac{71}{30}$ Tel. pole 65 334.6
	70	$\frac{71}{100}$ 334.6
$\frac{54}{100}$ 335.11	$\frac{56}{75}$ 334.9	$\frac{53}{20}$ 335.2
$\frac{55}{100}$ 335.10	$\frac{49}{60}$ 335.16	$\frac{55}{65}$ Tel. pole 65 335.1
$\frac{53}{100}$ 335.12	$\frac{51}{70}$ 335.14	$\frac{55}{70}$ 335.2
$\frac{53}{100}$ 335.12	$\frac{57}{50}$ 334.9	$\frac{58}{70}$ 335.3
$\frac{53}{100}$ 335.14	$\frac{56}{50}$ 335.3	$\frac{52}{70}$ Tel. pole 65 335.3
		$\frac{52}{100}$ 335.3
$\frac{53}{100}$ 335.3		$\frac{53}{100}$ 335.2
		$\frac{53}{100}$ 335.3
		Tel. pole 90



	+	T	-	Flev.
	4.305	<del>339.315</del>		<del>334.896</del> <del>335.010</del>
646+44.5				
647+00			4.6	<del>334.6</del> <del>334.7</del>
+28				
648+00			5.1	<del>334.1</del> <del>334.2</del>
+35				
+48 center of 15' driveway	5.1			<del>334.1</del> <del>334.2</del>
649+00			5.2	<del>334.0</del> <del>334.1</del>
+65				
B.M.#71			3.648	<del>335.553</del> <del>335.558</del> <del>335.667</del> <del>335.677</del> <del>335.558</del> <del>335.677</del>
B.M.#71				
	3.519	<del>339.077</del> <del>339.196</del>		
650+00			5.4	<del>333.7</del> <del>333.8</del>
+77				
651+00			5.4	<del>333.7</del> <del>333.8</del>
+90				
652+00			4.5	<del>334.6</del> <del>334.7</del>
653+00			4.3	<del>334.8</del> <del>334.7</del>
+04				
6 +48				

$\frac{45}{100} 334.87$	Guy Pole. 65	$\frac{40}{100} 335.12$
$\frac{49}{100} 334.83$	Tel. pole 85	$\frac{40}{100} 335.12$
$\frac{49}{100} 334.43$	Tel. pole 85	$\frac{40}{100} 334.16$
$\frac{49}{100} 334.13$	Tel. pole. 90	$\frac{46}{100} 334.16$
$\frac{54}{100} 333.87$	Tel. pole 80	$\frac{42}{100} 334.16$
$\frac{48}{100} 334.52$	Tel. pole 90	$\frac{50}{100} 334.11$
$\frac{43}{100} 334.88$	Tel. pole 90	$\frac{40}{100} 335.1$
$\frac{48}{85} 334.43$	334.6	$\frac{38}{100} 335.3$
$\frac{42}{100} 334.9$	Tel. pole. 80	
$\frac{44}{90} 334.7$	Eucy tree (2' d) 90	

	+	T	-	Elev
654+00		<del>339.196</del> 339.077	4.3	<del>334.9</del> 334.8
+24				
+29				
655+00			3.5	<del>335.7</del> 335.6
T.P.			3.403	<del>335.793</del> 335.674
	3.027	<del>338.020</del> 338.701		
+42				
656+00			4.3	<del>334.5</del> 334.4
+61				
657+00			4.5	<del>334.5</del> 334.2
+29				
+29			9.8	<del>334.0</del> 333.9
+43				
+80				
658+00			4.7	<del>334.1</del> 334.0
+28				
+50			4.9	<del>333.8</del> 333.8
+97				
B.M. #72			3.425	<del>335.299</del> 335.276
659+00			5.0	<del>333.8</del> 333.7
660+00			6.0	<del>332.8</del> 332.7
+19				
B.M. #72				<del>335.292</del> 335.271
	2.010	<del>337.102</del> 337.281		

(31)

$\frac{41}{100}$ 335.40					
$\frac{35}{100}$ 335.46					
$\frac{38}{50}$ 335.40					
$\frac{32}{100}$ 334.18					
$\frac{44}{100}$ 334.13					
$\frac{43}{100}$ 334.54					
$\frac{45}{100}$ 334.21					
$\frac{50}{100}$ 333.27					
$\frac{51}{100}$ 333.16					
$\frac{61}{100}$ 332.16					
$\frac{63}{90}$ 332.54					
$\frac{58}{80}$ 332.9					
Tel. pole. 80					
Eucy. Tree (1.5)					
Tel. pole. 80					
Eucy. Tree (1.5)					
Tel. pole. 80					
Eucy. Tree (1.5)					
Tel. pole. 90					
Tel. pole. 80					
Eucy. Tree (1.5)					
Tel. pole. 90					

+	↑	-	Elev.
	<u>337.28</u>		
661+00		4.8	332.5 <u>332.6</u>
+33			
662+00		5.6	331.7 <u>331.8</u>
+55			
+69			
663+00		5.1	332.2 <u>332.3</u>
+73			
664+00		6.2	331.1 <u>331.2</u>
+96			
665+00		6.5	330.8 <u>330.9</u>
T.P.		6.145	331.136 <u>331.257</u>
3,025	334.161		
	<u>334.282</u>		
666+00		3.4	330.8
+12			
667+00		3.7	330.5
+30			
668+00		4.5	329.7
+45			
669+00		5.5	328.9
+67			
670+00		6.3	327.9
+94			
671+00		7.0	327.2

\$

<u>46</u> 332.87	48 332.15
100	100
Tel. pole.	
190	56 331.87
	100
Tel. pole.	
90	
Eucy. tree. (2')	
90	56 331.7
	100
Tel. pole.	
90	65 330.48
	100
Tel. pole	65 330.4
85	100
36 330.16	38 330.54
100	100
Tel. pole	
90	
39 330.13	39 330.43
100	100
Tel. pole	
85	
45 329.7	50 329.42
100	100
Tel. pole	
85	
47 329.8	58 328.54
100	100
Tel. pole	
90	
57 328.88	58 328.16
100	100
Tel. pole.	
90	
60 328.12	65 327.16
100	100
Tel. pole	
85	
73 326.9	73 326.9
100	100

+	T	-	Elev.
	334.161		
	<del>334.202</del>		
672+00		7.4	326.8
T.P.			326.86
	330.876	7.675	<del>326.160</del>
4.390	<del>330.997</del>		
673+21			
673+00		4.8	326.1
+56			
674+00		5.4	325.5
(673+68)			
674+82		5.2	325.7
675+00			
#77		5.7	325.2
B.M. #75			327.076
#77		3.800	<del>327.197</del>
B.M. #73			327.060
	329.855		<del>327.201</del>
2.795	<del>329.996</del>		
676+00		5.0	324.9
+18			
677+00		5.3	324.6
+44			
678+00		6.0	323.9
+66			
679+00		5.5	324.4
T.P.		2.745	327.110
+34		5.6	324.3

+	T	-	Elev.
	334.161		
	<del>334.202</del>		
672+00		7.4	326.8
T.P.			326.86
	330.876	7.675	<del>326.160</del>
4.390	<del>330.997</del>		
673+21			
673+00		4.8	326.1
+56			
674+00		5.4	325.5
(673+68)			
674+82		5.2	325.7
675+00			
#77		5.7	325.2
B.M. #75			327.076
#77		3.800	<del>327.197</del>
B.M. #73			327.060
	329.855		<del>327.201</del>
2.795	<del>329.996</del>		
676+00		5.0	324.9
+18			
677+00		5.3	324.6
+44			
678+00		6.0	323.9
+66			
679+00		5.5	324.4
T.P.		2.745	327.110
+34		5.6	324.3

Note culvert runs parallel to line





Party  
Leach  
Reynolds  
Ruplinger.

329.576  
~~329.121~~

Elev.

692+72.3

5.1 324.5

+97.3

5.4 324.2

693+22.3

4.9 324.8

B.M. # 75

2.967 ~~326.751~~

March 11.

3.296 ~~329.917~~  
~~330.057~~

326.609 326.621

~~326.761~~

~~326.761~~

694+47.3

5.4 324.5

+72.3

5.3 324.6

+97.3

5.0 324.9

694+24.0

5.5 324.4

695+00

5.3 324.6

696+00

5.3 324.6

697+00

5.3 324.6

698+00

5.7 324.2

(36)

~~41 325.65~~  
~~100~~

~~32 325.87~~  
~~100~~

~~42 325.76~~  
~~100~~

~~49 325.15~~  
~~100~~

~~95 325.34~~  
~~100~~

~~44 325.35~~  
~~100~~

~~45 325.64~~  
~~100~~

~~46 325.53~~  
~~100~~

~~43 325.86~~  
~~100~~

~~43 325.86~~  
~~100~~

~~46 325.53~~  
~~100~~

~~51 324.55~~  
~~30~~

~~48 324.98~~  
~~20~~

~~50 324.16~~  
~~30~~

~~58 324.51~~  
~~25~~

~~50 324.53~~  
~~30~~

~~51 324.8~~  
~~50~~

~~52 324.82~~  
~~25~~

~~52 324.82~~  
~~40~~

~~56 324.53~~  
~~40~~

~~58 324.81~~  
~~45~~

~~59 324.20~~  
~~25~~

~~52 324.54~~  
~~100~~

~~42 324.9~~  
~~100~~

~~48 324.88~~  
~~100~~

~~50 324.9~~  
~~100~~

~~90 325.10~~  
~~100~~

~~48 325.20~~  
~~100~~

~~42 325.12~~  
~~100~~

~~49 325.10~~  
~~100~~

~~48 325.81~~  
~~100~~

~~52 324.77~~  
~~100~~

~~48 325.21~~  
~~100~~

	T	-	Elev.
	<u>329.917</u> <del>330.057</del>		
6699+00		5.6	324.13
T.P.		4.830	<u>325.087</u> <del>325.227</del>
	4.330		<u>329.417</u> <del>329.557</del>
700+00		5.1	324.3
701+00		5.2	324.7
702+00		5.5	323.9
703+00		6.0	323.4
704+00		7.2	322.7
705+00		8.2	321.7
B.M.# <del>76</del> +80		4.188	<u>325.229</u> <u>325.279</u> <del>325.369</del> <del>325.329</del>
			<u>325.279</u> <del>325.363</del>
	0.809		<u>326.088</u> <del>326.172</del>
706+00		5.8	320.3
707+00		6.4	319.7
708+00		7.0	319.1
709+00		7.6	318.5

	$\frac{47}{100}$	325.42
	$\frac{42}{100}$	325.49
	$\frac{42}{100}$	325.44
	$\frac{43}{100}$	325.40
	$\frac{51}{100}$	324.83
	$\frac{60}{100}$	323.64
	$\frac{70}{100}$	322.84
	$\frac{46}{100}$	321.5
	$\frac{55}{105}$	320.6
	$\frac{59}{109}$	320.2
	$\frac{67}{102}$	320.4
	$\frac{59}{25}$	329.10
	$\frac{53}{39}$	329.46
	$\frac{55}{59}$	329.44
	$\frac{57}{109}$	329.47
	$\frac{55}{29}$	323.9
	$\frac{44}{39}$	325.40
	$\frac{45}{59}$	324.9
	$\frac{44}{109}$	325.40
	$\frac{55}{29}$	323.8
	$\frac{44}{39}$	325.40
	$\frac{45}{59}$	324.4
	$\frac{44}{109}$	325.40
	$\frac{56}{29}$	323.5
	$\frac{47}{39}$	324.7
	$\frac{48}{59}$	324.4
	$\frac{48}{109}$	324.6
	$\frac{64}{29}$	323.0
	$\frac{51}{25}$	324.3
	$\frac{51}{109}$	324.3
	$\frac{73}{13}$	322.1
	$\frac{60}{29}$	323.4
	$\frac{57}{109}$	323.7
	$\frac{82}{15}$	321.2
	$\frac{73}{29}$	322.1
	$\frac{62}{109}$	322.5
	$\frac{59}{17}$	320.2
	$\frac{46}{39}$	321.5
	$\frac{45}{109}$	321.6
	$\frac{64}{29}$	319.7
	$\frac{55}{39}$	320.5
	$\frac{53}{109}$	320.8
	$\frac{72}{62}$	318.4
	$\frac{60}{89}$	320.1
	$\frac{60}{109}$	320.7
	$\frac{84}{75}$	317.7
	$\frac{65}{90}$	319.6
	$\frac{64}{109}$	319.7



	+	T	-	Elev.
		<del>326.088</del> 326.172		
6 710+00			8.5	317.6 ✓
T.P.			9.210	<del>316.878</del> 316.962
	4.976	<del>321.854</del> 321.938		
6 711+00			4.9	317.0 ✓
6 712+00			6.1	315.8 ✓
6 713+00			6.6	315.3 ✓
6 714+00			8.4	313.5 ✓
+19			9.7	312.2 ✓
+17.5			8.1	313.8 ✓
+84			7.0	314.9 ✓
+94			5.7	316.2 ✓
6 715+00			5.2	316.7 ✓
B.M. #77			3.098	<del>318.752</del> 318.699 ✓
#81				<del>318.840</del> 318.821 ✓
#77				<del>318.699</del> 318.821 ✓
	2.085	<del>320.784</del> 320.926		
6 716+00			4.1	316.7 ✓

<del>319.0</del> 319.0				
<del>317.0</del> 317.0				
<del>316.9</del> 316.9				
<del>319.12</del> 319.12				
<del>319.13</del> 319.13				
<del>316.2</del> 316.2				
<del>318.7</del> 318.7				
<del>318.9</del> 318.9				
<del>315.0</del> 315.0				
<del>318.4</del> 318.4				
<del>315.10</del> 315.10				
<del>319.6</del> 319.6				
<del>313.7</del> 313.7				
<del>313.2</del> 313.2				
<del>313.7</del> 313.7				
<del>312.8</del> 312.8				
<del>311.9</del> 311.9				
<del>311.5</del> 311.5				
<del>314.8</del> 314.8				
<del>314.8</del> 314.8				
<del>316.6</del> 316.6				
<del>316.7</del> 316.7				
<del>315.2</del> 315.2				
<del>315.3</del> 315.3				
<del>313.3</del> 313.3				
<del>313.1</del> 313.1				
<del>313.1</del> 313.1				
<del>315.3</del> 315.3				
<del>316.9</del> 316.9				
<del>316.9</del> 316.9				
<del>315.13</del> 315.13				
<del>316.8</del> 316.8				
<del>316.0</del> 316.0				
<del>315.9</del> 315.9				
<del>315.4</del> 315.4				
<del>316.3</del> 316.3				
<del>316.4</del> 316.4				
<del>315.9</del> 315.9				
<del>316.3</del> 316.3				

(38)

	+	T	-	Elev.
		320.784		
		<del>320.900</del>		
6	716+29.4		4.4	316.4
	+54.4		4.4	316.4
6	+79.4		4.6	316.0
6	717+04.4		5.1	315.7
6	+14.4		6.6	314.2
	+29.4		5.4	315.4
	+48.2		5.6	315.2
6	718+00		6.3	314.5
6	719+00		5.8	315.0
6	720+00		6.4	314.4
			6.222	314.562
				<del>314.604</del>
6	721+00	4.820	5.7	313.7
	+44.5			

(39)

$\frac{42}{100}$	$\frac{56}{30}$	$\frac{46}{25}$	$\frac{46}{100}$
$\frac{52}{100}$	$\frac{52}{45}$	$\frac{42}{35}$	$\frac{42}{100}$
$\frac{55}{100}$	$\frac{58}{70}$	$\frac{45}{60}$	$\frac{55}{100}$
$\frac{42}{100}$			$\frac{55}{100}$
$\frac{55}{100}$			$\frac{55}{100}$
$\frac{48}{100}$			$\frac{64}{75}$
$\frac{50}{100}$			$\frac{72}{100}$
$\frac{52}{100}$			$\frac{80}{100}$
$\frac{55}{100}$			$\frac{60}{100}$
$\frac{60}{100}$			$\frac{65}{100}$
$\frac{56}{100}$			$\frac{72}{100}$
			$\frac{68}{100}$
			$\frac{62}{100}$
			$\frac{52}{100}$

Flow line  
2' culvert.

100  
22  
63

(40)

	+	Π	-	Elev.
		319.382		
		<del>319.504</del>		
6 722+00			5.1	314.3
	+63		5.9	314.0
6 723+00			5.0	314.4
724+00			4.9	315.0
6 725+00			4.7	314.7
726+00			4.2	315.3
B.M. #82			2.010	317.372 317.376
#82				<del>317.494 317.530</del>
#78				<del>317.376</del>
	3.376	320.752		<del>317.530</del>
6 727+00			5.3	315.5
6 728+00			5.8	316.0
6 729+00			8.3	312.5
	+98.7			
6 730+00			8.0	312.8
730+06				
	+23.7		8.4	312.4

	52	314.32	
	100		
			center of driveway
	43	315.40	
	100		
	40	315.54	
	100		
	44	315.43	
	60	315.76	
	45	315.87	
	100		
	32	315.87	
	100		
	35	315.9	
	49		
	50	315.98	
	100		
	51	315.87	
	10		
	73	313.55	
	100		
	76	313.32	
	100		
	91	311.57	
	100		
		Flow line	
		18" culvert.	
	77	313.31	
	100		
	85		
	FCC		
	90		
	FCC		
	90		
	FCC		
	82		
	FCC-		

	50	314.54	
	100		
	55	313.78	
	100		
	53	314.52	
	100		
	50	314.54	
	100		
	45	314.9	
	100		
	53	315.21	
	100		
	62	314.76	
	100		
	93	311.45	
	100		
	86	312.32	
	100		
	88	312.10	
	100		

+ T - Elev.

320.752

~~320.986~~

730 + 48.7	8.5	312.3
+ 73.7	8.4	312.4
+ 98.7	7.8	313.0
731 + 23.7	7.8	313.0
+ 48.7	7.8	313.0
T.P.	7.900	<u>312.852</u>
4.225		<u>317.077</u>
+ 73.7	4.8	312.3
+ 98.7	4.9	312.2
732 + 23.7	5.7	311.4
+ 53.7	6.1	311.0
+ 74		
+ 82	8.3	308.8
733 + 00	7.2	309.9

$\frac{72}{100}$	313.1
$\frac{75}{100}$	313.3
$\frac{76}{100}$	313.32
$\frac{82}{100}$	312.88
$\frac{84}{100}$	312.87
$\frac{42}{100}$	312.76
$\frac{53}{100}$	311.88
$\frac{42}{100}$	312.54
$\frac{48}{100}$	312.3
$\frac{52}{100}$	311.9
$\frac{50}{100}$	312.21

61 311.0  
 45 310.9  
 62 311.0  
 35 309.32  
 72 Flow line  
 40 6" culvert.  
 55 311.76  
 80

(41)

80 Fce	97 311.54
78 Fce	95 311.3
60 Fce	86 312.32
72 Fce	83 312.5
45 Fce	85 312.35
78 Fce	85 312.76
80 Fce	45 312.1
80 Fce	50 312.8
95 Fce	53 311.7
69 Fce	69 310.8
95 Fce	80 308.4
82 Fce	308.9

	+	̄	-	Elek
		<u>317.077</u> <del>317.231</del>		
734+00.			5.0	312.1 ✓
735+00			4.9	312.3 ✓
B.M. #77			6.660	<u>310.417</u> 310.410 ✓
#83				<del>310.571</del> 310.545 ✓
				<del>310.545</del> 310.410 ✓
	1.066	<u>312.276</u> <del>312.411</del>		
736+00			2.6	309.7 ✓
737+00			4.0	308.3 ✓
738+00			5.3	307.0 ✓
739+00			6.8	305.5 ✓
+56			7.2	305.1 ✓
740+00			6.7	305.6 ✓
741+00			3.6	308.7 ✓
+50			1.4	310.9 ✓
742+00			1.3	311.0 ✓
T.P.			3.065	<u>309.211</u> <del>309.346</del>

(42)

54 100	311.87 ✓		90 Fce	64 100	311.40 ✓
57 100	312.41 ✓		95 Fce	54 100	311.87 ✓
19 100	310.54 ✓		92 Fce	26 100	310.987 ✓
32 100	308.76 ✓		95 Fce	44 100	307.9 ✓
52 100	307.70 ✓		92 Fce	56 100	306.87 ✓
65 100	305.78 ✓		90 Fce	70 100	305.45 ✓
65 100	305.78 ✓		92 Fce	67 100	305.76 ✓
74 100	305.32 ✓		55 Fce	39 100	306.9 ✓
98 100	307.54 ✓		79 Fce	54 100	310.7 ✓
36 100	308.7 ✓		39 Fce	18 100	310.5 ✓
33 100	309.7 ✓		59 Fce	8 100	310.7 ✓
32 100	309.21 ✓		95 Fce	02 100	311.5 ✓
32 100	309.7 ✓		95 Fce	02 100	311.5 ✓
32 100	309.7 ✓				

3.465

312.676

309.211

Elev.

~~309.346~~

310.3

309.4

306.4

305.8

303.3

300.9

302.2

303.3

306.126 306.095

~~306.261~~ ~~306.300~~

11.2

302.0

10.7

303.0

11.6

302.1

7.503

313.678  
~~313.975~~

+32

+32

+50

+63

(43)

310.76  
100

309.45  
100  
Fce

308.40  
100  
Fce

306.76  
100

305.54  
100  
Fce

302.4  
100  
Fce

303.3  
100  
Fce

304.2  
100  
Fce

302.2  
100  
Fce

302.4  
100  
Fce

303.2  
100  
Fce

302.7  
100  
Fce

38  
100  
11

48  
100

76  
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72  
100

98  
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114  
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76  
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72  
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114  
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94  
100

82  
100

102  
100

102  
100

102  
100

102  
100

102  
100

102  
100

Note: Ran peg line on check my  
within 209

90  
Fce

90  
Fce

90  
Fce

302.2  
100  
Fce

302.9  
100  
Fce

302.7  
100  
Fce

	+	T	-	Elev.
		<u>313.678</u>		
750+00			9.8	303.9
751+00			8.0	305.2
752+00			6.0	307.7
753+00			2.8	310.9
T.P.			1.255	<u>312.423</u>
	7.996	<u>320.419</u>		<u>312.718</u>
754+00			5.4	315.0
755+00			4.7	315.7
756+00			5.0	315.4
757+00			6.3	314.1
758+00			7.5	312.9
+39			6.9	313.5
+46			9.0	311.4
+52			7.7	312.7

				(44)
				304.40
				305.7
				308.52
				311.41
				315.23
				315.84
				315.63
				313.9
				312.9
				313.5
				309.8
				311.41
				313.2
				313.5
				309.8
				311.41





322.865  
~~321.73~~ Elev.

765+70			
766+00	2.9	320.0	
T.P.	1.203	321.662	
	12.497	334.287	
767+00	7.5	326.7	
768+00	5.6	328.6	
769+00	4.7	329.5	
+30.3	3.9	330.8	
+55.3	2.6	331.6	
+80.3	1.2	333.0	
B.M. #86	0.162	333.997	333.989
	6.548	340.737	<del>334.131</del>
770+05.3	6.5	334.2	
+31.4	5.4	335.3	
771+00	3.5	337.2	

(46)

Flow line culvert (12")

04 100	322.65	29 89	23 30	320.76	22 100	320.22
88 100	325.4	82 79	22 30	326.52	74 100	327.1
59 100	328.3	52 55	55 40	328.7	53 10	328.5
33 100	331.0	37 79	44 35	329.8	51 100	329.1
22 100	332.0	24 75	34 45	330.8	41 100	330.1
13 100	332.9	14 85	22 62	333.2	38 100	331.2
05 100	333.6	02 85	12 69	333.2	30 100	332.5
64 100	334.3	52 90	37 90	337.8	12 100	332.5
52 100	335.5				65 100	339.2
39 100	337.3				54 100	335.3
					41 100	336.5

	+	+	-	Elev.
		<u>340.737</u>		
772+00			9.5	332.2 ✓
773+00			8.1	332.6 ✓
+83				
774+00			10.3	330.4 ✓
775+00			8.2	332.5 ✓
T.P.			7.597	<u>333.140</u>
	8.968	<u>342.108</u>		
776+00		<u>342.050</u>	8.8	333.3 ✓
777+00			7.1	335.0 ✓
778+00			6.0	336.1 ✓
779+00			4.2	337.9 ✓
780+00			2.3	339.8 ✓
B.M. #87				341.658 341.454
		<u>349.487</u>	.450	<u>341.600</u> <u>341.613</u>
781+00	8.033	<u>349.646</u>		
			7.8	341.7 ✓
782+00			4.7	344.8 ✓

41 336.6 ✓  
 10°  
 66 339.1 ✓  
 10°  
 105 Flow line  
 10° 12" culvert.  
 94 331.6 ✓  
 10°

72 333.0 ✓  
 10°

82 333.89 ✓  
 10°

68 335.23 ✓  
 10°

58 336.73 ✓  
 10°

44 338.0 ✓  
 10°

340.2 ✓  
 12 340.1 ✓  
 10°

73 342.3 ✓  
 10°

44 345.5 ✓  
 10°

77 333.0 ✓  
 5°  
 82 332.5 ✓  
 6°  
 105 330.7 ✓  
 8°

333.5 ✓  
 815  
 50

90  
 Fce.  
 98  
 Fce.

(47)  
 510 335.7 ✓  
 10°  
 78 332.9 ✓  
 10°  
 105 330.2 ✓  
 10°  
 81 332.6 ✓  
 10°  
 85 333.45 ✓  
 10°  
 333.0  
 71 333.9 ✓  
 10°  
 63 335.78 ✓  
 10°  
 45 337.56 ✓  
 10°  
 25 339.56 ✓  
 10°  
 79 341.76 ✓  
 10°  
 52 344.83 ✓  
 10°

	+	T	-	Elev.
		<u>349.487</u> <del>349.021</del>		
7	783+00		5.0	344.5
7	784+00		6.4	343.1
7	785+00		5.0	344.5
7	786+00		3.0	346.5
7	T.P.		3.030	<u>346.457</u> <del>346.16</del>
		10.540		
7	787+00	<u>356.997</u> <del>357.156</del>	9.3	347.7
7	788+00		7.2	348.8
7	789+00		5.0	352.0
	B.M. #84		4.247	<u>352.750</u> <del>352.909</del> 352.759
		4.247		
	+348	<u>357.001</u> <del>357.157</del>	4.5	352.5
	790+00		5.9	351.1
	+44		8.9	348.1
	791+00		9.0	348.0
	T.P.		8.718	<u>348.283</u> <del>348.439</del>

	+	T	-	Elev.
				423.952
				100
				58
				100
				42
				10
				25
				100
				80
				100
				62
				100
				45
				100
				45
				100
				75
				100
				45
				100
				75
				100
				59
				100
				64
				100
				80
				100
				75
				100
				80
				100
				75
				100

	+	π	-	Elev.
				348.283
	2.630	<del>350.913</del>		<del>348.759</del>
791+89			5.6	345.3 ✓
+94			7.6	343.3 ✓
792+00			5.6	345.3 ✓
+30			5.0	345.9 ✓
+63			6.5	344.4 ✓
793+00			9.1	341.8 ✓
+81			11.2	339.7 ✓
794+00			12.7	338.2 ✓
T.P			11.486	<del>339.583</del>
	2.788	<del>342.215</del>		<del>342.371</del>
+03			4.3	337.9 ✓
+06			5.6	336.6 ✓
+11			4.5	337.7 ✓

(49)

$\frac{42}{100}$	346.20 ✓	50 FCE	$\frac{62}{100}$	344.2 ✓
$\frac{53}{100}$	345.86 ✓	60 FCE	$\frac{86}{100}$	342.53 ✓
$\frac{48}{100}$	346.31 ✓	60 FCE	$\frac{65}{100}$	344.53 ✓
$\frac{42}{100}$	346.22 ✓	60 FCE	$\frac{68}{100}$	345.1 ✓
$\frac{61}{100}$	344.8 ✓	56 FCE	$\frac{72}{100}$	343.7 ✓
$\frac{60}{80}$	344.9 ✓	55 FCE	$\frac{92}{100}$	341.2 ✓
$\frac{62}{55}$	344.7 ✓	55 FCE	$\frac{116}{80}$	339.53 ✓
$\frac{62}{34}$	344.2 ✓	45 FCE	$\frac{138}{100}$	338.1 ✓
$\frac{83}{100}$	342.6 ✓	45 FCE	$\frac{48}{100}$	337.8 ✓
$\frac{102}{100}$	340.0 ✓	45 FCE	$\frac{48}{100}$	337.8 ✓
$\frac{102}{75}$	340.31 ✓	45 FCE	$\frac{76}{100}$	334.86 ✓
$\frac{125}{100}$	338.53 ✓	45 FCE		
$\frac{45}{100}$	337.77 ✓	45 FCE		
$\frac{32}{100}$	338.75 ✓	45 FCE		
$\frac{32}{100}$	338.75 ✓	45 FCE		
$\frac{52}{35}$	337.0 ✓	45 FCE		
$\frac{48}{50}$	337.4 ✓	45 FCE		

1500  
33  
67

+

342.215

Elev.

794+18

4.5 337.7

795+00

3.6 338.6

+63

1.8 340.4

796+00

2.8 339.4

797+00

7.1 335.1

798+00

9.7 332.5

799+00

10.6 331.6

10.816 331.379

7.535

338.934  
339.090

799+96

800+00

11.3 327.6

B.M.# 89

332.104 332.103

6.830

338.934  
339.085

6.830 332.260 332.255

800+67

6.8 332.8

801+00

9.9 334.5

±

32  
100

338.75

31  
100

338.8

24  
100

339.8

24  
100

339.8

24  
100

339.8

64  
100

335.8

81  
100

333.8

114  
100

330.8

112 Flow line

95  
100

327.7

97 12' culvert

95  
100

329.64

109 32' 8" 0

70  
100

331.9

38  
100

335.51

45  
FCC

40  
FCC

30  
FCC

35  
FCC

30  
FCC

30  
FCC

30  
FCC

30  
FCC

30  
FCC

45

60  
FCC

65  
FCC

(50)

53  
100

42  
100

28  
100

32  
100

75  
100

104  
100

104  
100

112  
100

69  
100

49  
100

336.9

338.8

339.8

339.8

339.8

339.8

331.8

331.8

331.8

327.40

332.40

334.40

340.2

340.2

340.2

340.2

340.2

340.2

340.2

340.2

340.2

340.2

340.2

340.2

340.2

340.2

340.2

	+	T	-	Elev.
801+02.1 =		338.934		
800+99.2		<del>339.085</del>	4.2	334.7 ✓
801+24.2			4.2	334.7 ✓
801+49.2			4.4	334.5 ✓
+ 74.2			5.4	333.5 ✓
+ 99.2			5.0	333.9 ✓
802+24.2			5.0	333.9 ✓
+ 49.2			5.2	333.7 ✓
+ 74.2			6.1	332.8 ✓
+ 99.2			6.9	332.0 ✓
803+24.1			8.2	330.7 ✓
804			11.0	327.9 ✓
T.P.			12.220	326.714 ✓
	0.768	327.482		<del>326.865</del>
805+00		<del>327.633</del>	5.6	321.9 ✓

Abandoned

$\frac{32}{100}$	335.4 ✓	65	Fce	$\frac{42}{100}$	334.3 ✓
$\frac{37}{100}$	335.8 ✓	55	Fce	$\frac{42}{100}$	334.7 ✓
$\frac{44}{100}$	334.7 ✓	44	Fce	$\frac{42}{100}$	333.9 ✓
$\frac{49}{100}$	334.0 ✓	22	Fce	$\frac{42}{69}$	334.1 ✓
$\frac{49}{100}$	334.7 ✓	25	Fce	$\frac{52}{100}$	333.4 ✓
$\frac{42}{100}$	334.9 ✓	48	Fce	$\frac{52}{100}$	333.4 ✓
$\frac{51}{100}$	333.8 ✓	72		$\frac{56}{100}$	333.5 ✓
$\frac{42}{100}$	334.7 ✓	52		$\frac{52}{100}$	333.7 ✓
$\frac{58}{100}$	333.8 ✓	63		$\frac{63}{100}$	332.8 ✓
$\frac{62}{100}$	332.7 ✓	71		$\frac{71}{100}$	331.8 ✓
$\frac{84}{100}$	330.7 ✓	80		$\frac{80}{100}$	330.9 ✓
$\frac{112}{100}$	327.7 ✓	115		$\frac{115}{100}$	327.4 ✓
$\frac{51}{100}$	322.5 ✓	54		$\frac{54}{100}$	322.1 ✓



Void

+ T - Elen

307.879  
308.030

810+00

7.8

300.1

+27.8

8.6

299.3

+37.8

8.6

299.3

+47.8

8.7

299.3

+57.8

8.8

299.2

+67.8

8.9

299.1

+77.8

9.1

298.9

87.8

9.2

298.8

97.8

9.3

298.7

811+07.8

9.6

298.4

3.369  
308.048  
308.199

3.200

304.679  
304.830

811+17.8

9.8

298.1

+27.8

10.1

298.1

Contd. in Level Book #7.  
Page #1.  
Abandoned.

Void

(53)

299.4  
119 83  
11. 100 299.4  
306.0  
82 84  
100 301.6 95 80  
62 88  
100 80 70  
301.9 299.1 rd.  
61 82  
100 7 299.050  
302.3 300.6 299.050 rd.  
53 72 92 40  
100 75 60 40 rd.  
304.3 300.4 298.5  
32 46 94  
100 80 40 rd.  
305.1 302.7 298.8  
29 43 82 92  
100 65 40 30 rd.  
306.4 304.4 299.2 298.7  
16 31 82 93  
100 50 20 15 rd.  
306.8 305.3 299.9 298.6  
3 27 81 94  
100 59 30 70 rd.  
306.2 304.9  
R 10  
100 53 20 rd.  
305.1 304.4  
30 30 299.2  
30 35 304.5  
306.4 37 299.3  
100 45 100



Leach T  
Reynolds  
Roplinger

Ad

Warm & windy

	+	Void	-	Elev.
			<del>303.199</del>	
811 + 32.8			10.2	298.0
+ 97.8			10.5	297.7
+ 57.8			10.7	297.5
+ 67.8			10.7	297.5
+ 77.8			10.9	297.3
+ 83.1			11.3	296.9
812 + 00			11.7	296.5
+ 63			14.3	293.9
813 + 00			15.3	296.9
T.P. sta. 813 + 25			11.539	<del>296.509</del>
March 13, 1926		301.439		<del>296.509</del>
		4.930		<del>301.570</del>
B.M. # 87			10.950	<del>290.489</del>
			10.949	301.589
813 + 37			10.0	291.6
+ 68			5.2	296.4

Void

(54)

									299.0
									92
									10.0
									298.7
									95
									10.0
									298.5
									92
									10.0
									298.1
									10.0
									297.7
									10.0
									10.0
									297.5
									10.0
									297.0
									11.0
									10.0
									294.2
									14.0
									10.0
									293.0
									15.0
									10.0
									292.2
									94
									10.0
									291.1
									10.0

Note: - Ran peg line and check my elev. with n. 034 - (By Roplinger)

	+	T	-	Elev.
		301.589		
814+00			7.1	294.5
+69			5.3	296.3
815+00			12.9	288.2
T.P. Sta. 815+75 (rock)			3.289	298.300
	6.300	304.600		
+20 <sup>2</sup>			10.9	294.6
+34			7.5	297.1
+45.0			7.9	296.9
+53			6.8	297.8
+59			6.1	298.5
+60			5.9	299.5
+67 foot of rock			3.2	301.4
				304.0
+70			.6	Top of rock
+95	Top of rock		1.3	303.3

300.2	290.0	289.7	290.5
$\frac{11}{100}$	$\frac{116}{30}$	$\frac{119}{45}$	$\frac{111}{100}$
301.6		288.3	286.1
$\frac{0.2}{100}$		$\frac{13.3}{80}$	$\frac{13.3}{100}$
294.4	295.1	286.7	287.9
$\frac{7.2}{100}$	$\frac{6.5}{30}$	$\frac{14.9}{80}$	$\frac{13.2}{100}$
302.2	291.3		
$\frac{2.4}{100}$		297.9	287.5
302.8		$\frac{16.7}{70}$	$\frac{17.1}{100}$
$\frac{1.8}{100}$		288.1	286.1
302.6		$\frac{16.9}{70}$	$\frac{17.2}{100}$
$\frac{2.0}{100}$		288.1	287.6
302.4		294.3	$\frac{17.0}{100}$
$\frac{1.2}{100}$		$\frac{10.3}{30}$	288.7
302.6		295.2	288.8
$\frac{2.0}{100}$		$\frac{9.4}{60}$	$\frac{15.9}{100}$
302.2		295.3	288.9
$\frac{1.4}{100}$		$\frac{9.3}{10}$	$\frac{15.8}{100}$
302.9		296.0	288.7
$\frac{1.2}{50}$		$\frac{8.6}{60}$	$\frac{15.7}{100}$
		297.8	288.7
		$\frac{6.8}{70}$	$\frac{15.9}{100}$



	+	T	-	Elev.
		313.49		
816+90			13.8	297.7
+91			15.4	298.1
817+00			15.7	297.8
+50			6.2	307.3
+76			9.5	304.0
+85			7.7	315.8
818+00			7.9	305.6
+29			10.1	303.4
+50			6.9	306.6
819+00			9.5	304.0
+35			6.1	307.4
+48			8.6	304.9

(57)

	D	F	Elev.
306.3			
D $\frac{68}{100}$			
306.8			
D $\frac{67}{100}$			
307.4			
D $\frac{61}{100}$			
310.2			
D $\frac{13}{100}$			
310.8			
D $\frac{27}{100}$			
311.7			
D $\frac{18}{100}$			
312.4			
D $\frac{21}{100}$			
307.8			
D $\frac{57}{100}$			
310.5			
D $\frac{30}{100}$			
309.1			
D $\frac{44}{100}$			
311.3			
D $\frac{23}{100}$			
311.5			
D $\frac{20}{100}$			
306.5			
E $\frac{20}{30}$			
301.0			
D $\frac{125}{20}$			
305.4			
D $\frac{81}{70}$			
308.9			
D $\frac{76}{05}$			
301.5			
D $\frac{120}{100}$			
301.2			
D $\frac{123}{100}$			
299.3			
D $\frac{142}{100}$			
300.4			
D $\frac{131}{100}$			
299.2			
D $\frac{123}{60}$			
301.1			
D $\frac{142}{100}$			
300.4			
D $\frac{124}{100}$			
302.1			
D $\frac{115}{70}$			
300.8			
D $\frac{131}{100}$			
302.0			
D $\frac{122}{100}$			
298.8			
D $\frac{115}{45}$			
302.0			
D $\frac{141}{100}$			

	+	T D	-	Elev.
		313.49		
+68			5.5	308.0
				301.973
		"E"		
	2.22	303.65		
	6.976	310.451		
820+00			6.4	304.1
+22			7.7	302.8
+40			10.6	299.9
+74			8.8	301.7
821+00			9.3	301.2
+13			8.4	302.1
+43			9.0	301.5
+56			10.4	300.1
+68			9.5	301.0
822+00			12.5	298.0

312.7				302.2
D $\frac{0.8}{10^0}$			6°	$\frac{11.3}{10^0}$
			Fcc	
				298.7
809.2				$\frac{11.8}{10^0}$
$\frac{1.3}{10^0}$			6°	299.1
			Fcc	
307.1				$\frac{12.1}{10^0}$
$\frac{3.4}{10^0}$			5.3	295.2
			Fcc	
305.9				296.7
$\frac{5.3}{10^0}$			7.2	$\frac{14.3}{10^0}$
			Fcc	295.2
305.3				$\frac{13.8}{8^0}$
$\frac{7.2}{10^0}$			5.2	299.3
			Fcc	
303.8				$\frac{12.3}{10^0}$
$\frac{9.4}{10^0}$			7.4	298.0
			Fcc	$\frac{12.5}{10^0}$
303.4				298.6
$\frac{4.8}{10^0}$			6.1	$\frac{11.9}{10^0}$
			Fcc	298.1
305.4				$\frac{11.2}{4.5}$
$\frac{5.1}{10^0}$			4.8	297.9
			Fcc	$\frac{12.6}{10^0}$
306.0				297.0
$\frac{4.5}{10^0}$			5.2	$\frac{12.1}{8.5}$
			Fcc	
304.5				297.6
$\frac{6.0}{10^0}$			7.0	$\frac{11.2}{4.5}$
			Fcc	298.1
303.5				$\frac{12.4}{10^0}$
$\frac{7.0}{10^0}$			5.9	297.9
			Fcc	$\frac{12.6}{10^0}$
303.2				297.0
$\frac{7.3}{10^0}$			8.4	$\frac{13.5}{10^0}$
			Fcc	296.3
301.1				$\frac{15.2}{10^0}$
$\frac{9.7}{10^0}$			5.3	
			Fcc	
301.0				
$\frac{9.5}{10^0}$			11.2	
			Fcc	
302.2				
$\frac{8.3}{10^0}$			5.3	
			Fcc	
300.4				
$\frac{10.1}{10^0}$			11.2	
			Fcc	
296.7				
$\frac{13.8}{6.3}$				

	+	∇	-	Elev.
		310.451		
B 22 + 08.4			13.0	297.5
+ 33.4			12.1	298.4
B.M. # 88 New set up. 12.900 12.727		312.899	10.843	299.608
+ 58.4			15.1	297.4
+ 83.4			14.0	298.5
B 23 + 08.4			12.5	300.0
+ 33.4			13.5	299.0
+ 58.4			16.3	296.2
B 23 + 83.4			17.0	295.5
+ 97			20.5	292.0
B 24 + 08.4			18.1	294.4
B 24 + 15.9 = B 25 + 15.9 =			15.0	296.7
B 25 + 91			10.5	302.0

Recorded:  
309.431  
299.599  
Corrected

	+	∇	-	Elev.
		310.451		
			13.0	297.5
			12.1	298.4
		312.899	10.843	299.608
			15.1	297.4
			14.0	298.5
			12.5	300.0
			13.5	299.0
			16.3	296.2
			17.0	295.5
			20.5	292.0
			18.1	294.4
			15.0	296.7
			10.5	302.0

(59)

12  
829.089  
114  
770

300.9	298.9	298.6	296.5	293.0
$\frac{96}{100}$	$\frac{116}{60}$	$\frac{119}{49}$	$\frac{140}{60}$	$\frac{155}{100}$
301.7		Fce 300.3		293.8
$\frac{88}{100}$		$\frac{102}{45}$		$\frac{162}{100}$
		Fce		
12.2		48		$\frac{181}{100}$
$\frac{116}{100}$		Fce		
		53	$\frac{52}{65}$	$\frac{198}{100}$
		Fce		
$\frac{112}{100}$	$\frac{121}{80}$	55	$\frac{153}{25}$	$\frac{182}{75}$
		Fce		$\frac{182}{100}$
				rd.
$\frac{125}{100}$	$\frac{132}{80}$	48	$\frac{172}{45}$	$\frac{176}{100}$
		Fce		70
				rd.
$\frac{139}{100}$		$\frac{142}{30}$	$\frac{171}{20}$	$\frac{169}{100}$
		Fce		70
				rd.
$\frac{172}{100}$	$\frac{178}{85}$	$\frac{174}{35}$	$\frac{122}{30}$	$\frac{162}{100}$
				80
		Fce		rd.
$\frac{192}{100}$		Flowline 21.9 20 12" culvert	$\frac{185}{21}$	$\frac{162}{50}$
				80
				rd.
$\frac{170}{100}$		$\frac{173}{20}$	$\frac{186}{20}$	$\frac{159}{90}$
		Fce		$\frac{158}{100}$
$\frac{143}{100}$			$\frac{161}{45}$	$\frac{162}{60}$
				$\frac{155}{100}$
$\frac{88}{100}$		20		
		Fce		
		25		
		Fce		
				70
				$\frac{113}{100}$

	+	∓	-	Elev.
		312.499		
B26+00			3.1	
T.P. sta. B27+70			7.486	305.013
	9.130	314.143		
B26+60			2.1	
B27+00			4.1	
B27+50			5.1	
B28+00			9.1	
+32			10.1	
+65			9.6	
B29+00			11.7	
+41			12.7	
+60			15.8	
+92			16.7	
B30+00			15.6	

$\frac{13}{100}$	$\frac{27}{40}$	20 Fce		$\frac{42}{100}$
$\frac{07}{100}$		25 Fce	$\frac{31}{83}$	$\frac{33}{100}$
$\frac{58}{100}$		30 Fce		$\frac{16}{100}$
$\frac{33}{100}$		40 36 Fce		$\frac{74}{100}$
$\frac{73}{100}$		40 Fce	$\frac{101}{50}$	$\frac{112}{100}$
$\frac{79}{100}$	$\frac{82}{80}$	42 Fce		$\frac{121}{100}$
$\frac{73}{100}$		40 Fce	$\frac{122}{60}$	$\frac{132}{100}$
$\frac{88}{100}$	$\frac{104}{70}$	60 Fce		$\frac{138}{100}$
$\frac{103}{100}$	$\frac{110}{75}$	117 55 Fce		$\frac{152}{100}$
$\frac{140}{100}$		75 Fce	$\frac{171}{90}$	$\frac{181}{100}$
$\frac{154}{100}$		75 Fce	$\frac{175}{60}$	$\frac{174}{100}$
$\frac{151}{100}$		72 Fce	$\frac{150}{20}$ $\frac{173}{40}$	$\frac{171}{100}$

	+	π	-	Elev.
		314143		
830+19			16.5	
+38			14.8	
+60			15.0	
831+00			11.7	
+70			5.8	
832+00			5.5	
+20			4.7	
+36			4.8	
833+00			0.8	
T.P. 832+97 10' R			2.010	312.135
		12.485 324.618		
+45			6.2	
+81			7.5	
834+00			6.0	

(61)

$\frac{156}{100}$	80 Fce	$\frac{174}{40}$	80 rd.	$\frac{160}{100}$
$\frac{132}{100}$	$\frac{132}{85}$ Fce	$\frac{166}{30}$	70 rd.	$\frac{166}{100}$
$\frac{132}{100}$	80 Fce	$\frac{166}{38}$	80 rd.	$\frac{163}{10}$
$\frac{92}{100}$	$\frac{102}{80}$ Fce	$\frac{135}{90}$		$\frac{193}{100}$
$\frac{52}{100}$	$\frac{56}{80}$ Fce			$\frac{68}{100}$
$\frac{27}{100}$	$\frac{30}{85}$ Fce	$\frac{48}{30}$		$\frac{65}{100}$
$\frac{33}{100}$	$\frac{36}{80}$ Fce			$\frac{44}{100}$
$\frac{32}{100}$	$\frac{34}{90}$			$\frac{52}{100}$
$\frac{98}{100}$	Fce			$\frac{26}{100}$
$\frac{53}{100}$	Fce			$\frac{74}{100}$
$\frac{59}{100}$	Fce			$\frac{85}{100}$
$\frac{57}{100}$				$\frac{76}{100}$



Leach T  
Reynolds  
Ruplinger

62

+ T - Elev.

324.618

834+20

4.9

+93

7.8

835+00

6.8

+36.5

6.9

+46.5

6.7

+56.5

6.4

+66.5

6.5

+76.5

6.5

+86.5  
March 16  
B.M# 90

6.4

5.020

Recorded  
319.598 319.505

+ 8.756 328.261

835+96.5

9.7

836+06.5

10.5

+16.5

10.1

$\frac{3.15}{10.0}$

$\frac{6.9}{10.0}$

$\frac{6.5}{10.0}$

$\frac{5.6}{10.0}$

$\frac{5.6}{10.0}$

$\frac{5.4}{10.0}$

$\frac{5.4}{10.0}$

$\frac{4.9}{10.0}$

$\frac{4.5}{10.0}$

Note: - Run peg line and check my elev.  
to 001 (By Ruplinger) (329.435)

$\frac{8.0}{10.0}$

$\frac{7.7}{10.0}$

$\frac{7.8}{10.0}$

9.0  
Fce

7.0  
Fce

4.0  
Fce

0.5  
Fce

2.0  
Fce

$\frac{5.8}{6.0}$

$\frac{7.1}{3.0}$

$\frac{7.9}{6.0}$

$\frac{11.0}{5.0}$

$\frac{11.2}{2.5}$

$\frac{19.3}{4.0}$

$\frac{7.3}{10.0}$

$\frac{9.1}{10.0}$

$\frac{8.0}{10.0}$

$\frac{8.1}{10.0}$

$\frac{6.8}{10.0}$

$\frac{7.8}{10.0}$

$\frac{8.1}{10.0}$

$\frac{7.8}{8.0}$   $\frac{10.8}{10.0}$

$\frac{10.8}{10.0}$

$\frac{14.3}{10.0}$   
rd.

$\frac{14.2}{10.0}$

$\frac{14.0}{10.0}$

	+	T	-	Elev.
		328.261		
830+22.9			10.2	
837+00			10.9	
+031	Line crosses fence		10.9	
+28.1			9.5	
+53.1			8.5	
+78.1			10.2	
838+03.1			6.5	
+28.1			5.6	
+53.1			4.9	
+78.1			4.0	
839+03.1			3.8	
+28.1			5.1	

$\frac{80}{100}$	25' Fce	$\frac{109}{15}$	$\frac{142}{40}$ 60 rd.	$\frac{139}{100}$
$\frac{88}{100}$	05 Fce	$\frac{144}{60}$		$\frac{142}{100}$ rd.
$\frac{86}{100}$		$\frac{115}{35}$	$\frac{142}{60}$	$\frac{141}{100}$ rd.
$\frac{63}{100}$			$\frac{112}{80}$	$\frac{129}{100}$
$\frac{63}{100}$	50 Fce			$\frac{102}{100}$
$\frac{52}{100}$				$\frac{95}{100}$
$\frac{33}{100}$		$\frac{35}{80}$		$\frac{93}{100}$
$\frac{42}{100}$				$\frac{62}{100}$
$\frac{25}{100}$				$\frac{68}{100}$
$\frac{10}{100}$				$\frac{64}{100}$
$\frac{15}{100}$		$\frac{21}{35}$		$\frac{70}{100}$
$\frac{29}{100}$				$\frac{84}{100}$

	+	T	-	Elev.
		328.261		
	+53.1		7.4	
	T.P. sta. 839+55		9.504	318.757
		2.601	321.358	
	840+00		4.3	
	+39		7.4	
	841+00		8.4	
	+59.5		6.4	
	+97.5		7.3	
	842+22.5		8.9	
	+47.5		12.6	
	+72.5		11.6	
	+98.7		48.8"	
	T.P. on back 843+00		11.596	309.762
		1.380	311.142	
	843+00		4.9	

$\frac{45}{100}$

$\frac{105}{100}$

$\frac{03}{100}$

$\frac{62}{70}$

$\frac{75}{100}$

$\frac{24}{100}$

$\frac{42}{40}$

$\frac{84}{22}$   
Fce

$\frac{95}{50}$

$\frac{123}{80}$

$\frac{160}{100}$

$\frac{28}{100}$

$\frac{70}{40}$

$\frac{100}{40}$

$\frac{175}{70}$

$\frac{184}{100}$   
rd.

$\frac{02}{100}$

$\frac{56}{30}$

$\frac{62}{12}$   
Fce

$\frac{119}{90}$

$\frac{130}{100}$

$\frac{19}{100}$

$\frac{34}{80}$

$\frac{122}{100}$

$\frac{30}{100}$

$\frac{55}{80}$

$\frac{96}{20}$

$\frac{118}{25}$   
Fce

$\frac{180}{100}$

$\frac{52}{100}$

$\frac{91}{70}$

$\frac{42}{160}$

$\frac{115}{1100}$

$\frac{56}{100}$

$\frac{26}{140}$

$\frac{46}{160}$

$\frac{146}{1100}$

$\frac{72}{100}$

$\frac{66}{150}$

$\frac{160}{1100}$

$\frac{33}{100}$

$\frac{67}{150}$

$\frac{165}{1100}$

2  
100  
26  
74

(65)

+      π      -      Elev.

311.142

843+30	A 11.8
+74	A 7.1
+85	A 7.1
844+00	A 6.1
+288	A 6.9
+53.8	A 5.0
+78.8	A 5.1
845+03.8	A 10.0
+28.8	A 9.7
+31.9	A 10.4
+44	A 9.3
+49	A 13.8

D $\frac{88}{100}$	$\frac{58}{50}$ A	$\frac{189.922}{100}$ A
D $\frac{66}{100}$	$\frac{85}{40}$ A	$\frac{99}{100}$ B
D $\frac{66}{100}$	$\frac{11\frac{1}{2}}{65}$ A	$\frac{109}{100}$ B
D $\frac{43}{100}$	$\frac{11\frac{3}{4}}{30}$ A	$\frac{78}{100}$ B
D $\frac{50}{100}$	$\frac{86}{35}$	$\frac{32}{30}$ A
D $\frac{31}{100}$	$\frac{84}{22}$ A	$\frac{158}{100}$
D $\frac{45}{100}$	$\frac{61}{55}$	$\frac{97}{10}$
D $\frac{18}{100}$ A	$\frac{45}{70}$ A	$\frac{159}{100}$
D $\frac{66}{100}$	$\frac{66}{30}$ A	$\frac{132}{100}$
D $\frac{73}{100}$	$\frac{12\frac{1}{2}}{30}$	$\frac{195}{100}$ A
D $\frac{78}{100}$	$\frac{97}{60}$	$\frac{12\frac{3}{4}}{50}$
D $\frac{44}{100}$ A	$\frac{61}{80}$ A	$\frac{20\frac{1}{2}}{100}$ A
		$\frac{20\frac{1}{2}}{100}$ A
		$\frac{24}{100}$ C
		$\frac{01}{100}$ C

Reynolds replaced by Soper 10 AM

Party -  
Leach T  
Reynolds Ad  
Ruplinger "  
March 17

Cloudy and  
Warm

112  
18  
134

103  
37

17  
11  
4

(66)

+ T - Elen

311.142

845 + 57.7

10.2

$\frac{23}{100} A$

$\frac{189}{100} A$

+ 82.7

13.0

$\frac{58}{100} A$

$\frac{240}{100} A$

B.M. # 91

10.502 300.640 300.649

Recorded

T.P. in road

12.760 298.382

0.721 299.103

B

T.P. in road

12.997 286.106

2.640 288.746

C

T.P. on rock sta 843 + 00

309.762

6.820 316.582

D

March - 17.26  
B.M. # 91

300.649

2.289 302.938

F

846 + 07.7

A 6.3

$\frac{25}{100} A$

A  $\frac{35}{30}$

A  $\frac{45}{20}$

$\frac{23}{1100}$

+ 32.7  
92

B 9.4

$\frac{109}{100} A$

$\frac{106}{1100} B$

+ 42.0

B 7.4

$\frac{117}{100} A$

B  $\frac{34}{50}$   
Fce

$\frac{134}{1100} B$

+ 52.7

B 3.8

$\frac{111}{100} A$

65  
Fce

$\frac{106}{1100} B$

+ 78

B 2.6

$\frac{58}{100} A$

A  $\frac{112}{49}$

$\frac{136}{1100} B$

847 + 00

12.1

$\frac{28}{100} A$

A  $\frac{81}{30}$

$\frac{110}{100} B$

+       $\pi$       -      E/er  
          P  
          302.938

897 +28.6      B 2.2  
 +53.6      B 3.2  
 +61.0      B 4.7  
 +70.0      B 1.4  
 +78.6      B 1.9  
 848 +03.6      B 3.0  
 +28.6      B 3.3  
 +39.0      B 2.1

T.P. rock 848+38      B      11.945      290.993  
          .809      291.802

         C      300.65  
          5.87      306.52

T.P. rock 848+38      D      290.993  
          4.568      295.561

+

119      105  
 13      35  
 127      141  
 (67)

$\frac{34}{100}$       P  $\frac{111}{30}$       B  $\frac{112}{100}$   
 $\frac{42}{100}$       B  $\frac{122}{100}$   
 $\frac{56}{100}$       B  $\frac{144}{100}$   
 $\frac{32}{100}$       B  $\frac{116}{100}$   
 $\frac{50}{100}$       B  $\frac{53}{50}$       B  $\frac{113}{100}$   
 $\frac{52}{100}$       B  $\frac{114}{100}$   
 $\frac{80}{100}$       B  $\frac{102}{100}$   
 $\frac{62}{100}$       B  $\frac{92}{100}$

10°

10°

+

$\overline{D}$   
295.561

-

Elev.

+

+

849+03.6

+28.6

+46.7

850+00

+06.6

+18.6

+22.6

+31.6

10.7

+92

753.6

D 10.3

D 5.7

D 11.9

D 9.8

D 0.2

D 11.9

E 5.6

E 4.5

E 3.2

8.4

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

D  $\frac{2\frac{3}{4}}{10^0}$

D  $\frac{49}{10^0}$

D  $\frac{2^0}{10^0}$

$\overline{10^0}$

2

(68)

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

$\overline{10^0}$

852 922  
25  
648

166  
20  
3-6

(69)

+	$\frac{\pi}{D}$	-	Elev.
850+81.6		D 10.6	
+96.6		E 7.1	
851+06.6		D 11.3	
+16.6		D 11.7	
+28.0		E 7.4	
+32		E 5.1	
+45.6		E 3.8	
+78		E 2.4	
B.M. #92		10.380	285.181 285.262
+86		11.9	
852+00		E 9.2	
+28		E 5.0	
+64.8		E 10.4	

Recorded.

$\frac{10}{10^2}$		$\frac{10}{10^2}$
D $\frac{49}{10^2}$		$\frac{10}{10^2}$
$\frac{10}{10^2}$		$\frac{10}{10^2}$
$\frac{7}{10}$		$\frac{10}{10^2}$
D $\frac{7\frac{1}{2}}{10^2}$		$\frac{10}{10^2}$
D $\frac{7^2}{10^2}$		$\frac{10}{10^2}$
D $\frac{1^8}{10^2}$		$\frac{10}{10^2}$
D $\frac{6^1}{10^2}$	D $\frac{10^1}{9}$	$\frac{10}{10^2}$
D $\frac{15}{10^2}$	Foot of rock	$\frac{10}{10^2}$
D $\frac{4^1}{10^2}$		$\frac{10}{10^2}$
D $\frac{4^4}{10^2}$	D $\frac{9^9}{7^2}$	$\frac{10}{10^2}$
D $\frac{8^5}{10^2}$		$\frac{10}{10^2}$



Party  
Ledch T  
Ruplinger P  
Soper "  
March 18 '26

♀

(70)

+

+

-

Elev.

295.561

852+92.3

E 6.4

$\frac{64}{D 100}$

14

853+06.3

Top of rock covered  
by 1" of dirt → D 9.5

$\frac{25}{D 100}$

+17.3

E 3.5

$\frac{35}{D 100}$

+42.3

E 3.1

$\frac{52}{D 100}$

+53.3

D 10.3

$\frac{30}{D 100}$

+67.3

D 0.7

$\frac{30}{D 100}$

+92.3

E 8.3

$\frac{105}{D 100}$

+94.9

$\frac{111}{D 100}$

T.P. rock sta. 849+05 E 10.930 284.631

March 18, 26 1.522 286.153

$\frac{75}{D 100}$

(71)

	+	-	Elev.
	4.820	367.408	362.588
			4.555 362.853
304.1345	4.270	367.123	31
338.1315			3170 362.953
6.000	3.224	367.177	.915 366.262
			342A32
1.883	344.315		306.390
6.555	342.945		3.475 309.470
3.004	312.474		1.791 310.683
			543
			138

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from the side stake to the stake on the slope. To estimate the difference in elevation between the side stake and slope stake by this method, add this amount if cut, elevate if fill. Add this amount to cut or fill and the distance from the rod at the top of the slope to the side stake. If it does not make the slight adjustment necessary.

**IMPROVED TABLES AND INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given  $I$  may be found by dividing tangent (or external), opposite  $I$  by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

BM-# 48-407.064

#49-400.377



570.292  
2850  
500.432

19.137  
95

10.380

25.181

21.51 274.021  
375.845

27  
461  
1250

45.0  
5020  
329.750

51.100  
5.020  
321.730

97.5  
38  
89.5

505  
120  
1025