

EL CAPITAN
Pipe Line Survey
Levels &
Cross Sections — No 7

Level + #7.
Cross Sections

W197

MICROFILMED
JAN 21 1965

Profile Levels and
Cross Sections of Final
Location as Rerun, Keeping
within County Highway Right-of-
Way thru Mission Gorge.

April 1926

Sta	+	π	-	Elev.
		304.657		
811+42 ⁸⁷			6.5	298.2 ✓
+52 ⁸⁷			6.9	299.8 ✓
+62 ⁸⁷			7.3	297.4 ✓
+70 ⁸⁷	E.C.		7.7	297.0 ✓
T.P.			7.514	297.143 ✓
	1.496	298.589 ✓		
812+00			3.4	295.2 ✓
813+00			5.7	292.9 ✓
814+00			8.5	290.1 ✓
T.P. + B.M.	87 -90		8.131	290.458 ✓
	2.824	293.282 ✓		
815+00			5.4	287.9 ✓
+66 ³³	B.C.		5.9	287.4 ✓
T.P.			5.265	288.017 ✓
	5.670	293.687 ✓		

Lt. R Rt.

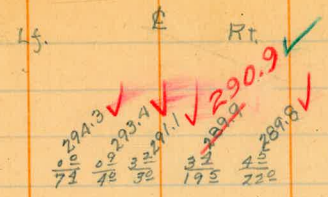
304.2 ✓
 100 100
 100 100
 304.3 ✓
 100 100
 304.7 ✓
 100 100
 304.1 ✓
 100 100
 304.7 ✓
 100 100
 297.1 ✓
 100 100
 298.1 ✓
 100 100

298.6 ✓
 100 100
 297.2 ✓
 100 100
 297.0 ✓
 100 100
 296.2 ✓
 100 100
 293.4 ✓
 100 100
 291.4 ✓
 100 100
 288.2 ✓
 100 100

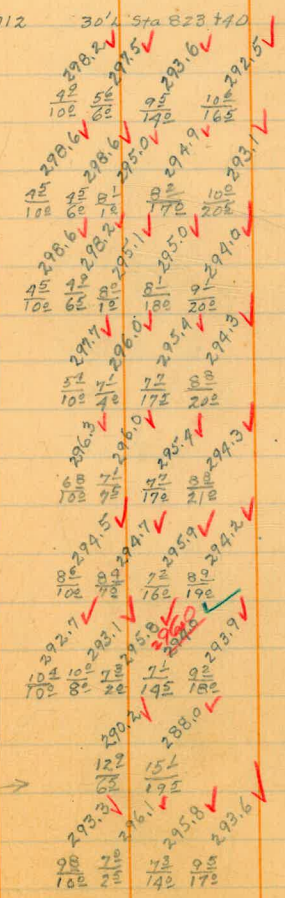
287.4 ✓
 100 100
 286.1 ✓
 100 100
 286.0 ✓
 100 100
 285.0 ✓
 100 100

Record Elev. 290.459

Sta	+	x	-	Elev.
		294.348		
B22+00		3.9		290.9 ✓
T.P.		2.455		291.893 ✓
	11,256	303.149		
B.M. - #88	#91		3.730	299.419 ✓
B23+00		9.6		293.5 ✓
+51 ²⁹	B.C.	8.2		294.9 ✓
+61 ²⁹		8.0		295.1 ✓
+71 ²⁹		7.7		295.9 ✓
+81 ²⁹		7.3		295.8 ✓
+91 ²⁹		7.2		295.9 ✓
B24+01 ²⁹		7.1		296.0 ✓
+05	12" concrete culvert	7.0		296.1 ✓
+10 ²⁶	E.C.	6.8		296.3 ✓ 297.3

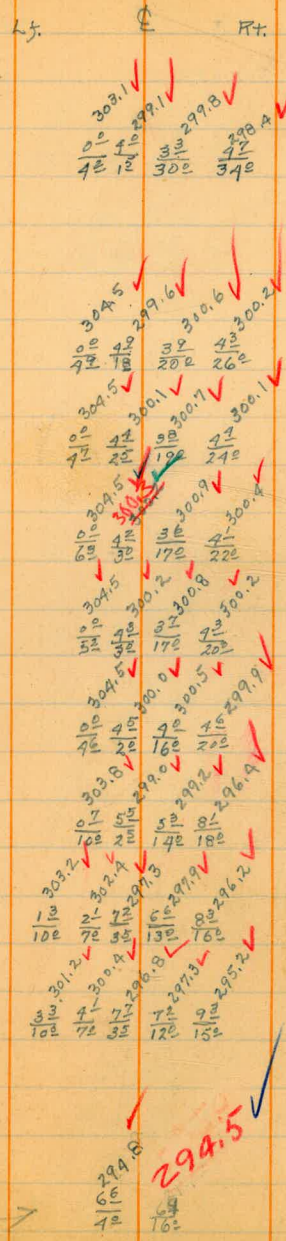


Record Elev. - 299.412



flowline →

Sta	T	K	-	Elev
		305.149		
824+99.66	B.C.		3.9	299.2 ✓
T.P.			2.984	300.165 ✓
	4.360	304.525 ✓		
825+09.2			4.8	299.7 ✓
+19.2			4.5	300.0 ✓
+29.2			4.3	300.2 ✓
+39.2			4.4	300.1 ✓
+49.66	E.C.		4.5	300.0 ✓
826+00			5.4	299.1 ✓
+81	P.I.		7.1	297.4 ✓
827+00			7.6	296.9 ✓
			6.542	297.983 ✓
	3.439	301.422 ✓		
+37	8" Concrete Culvert		5.1	296.3 ✓

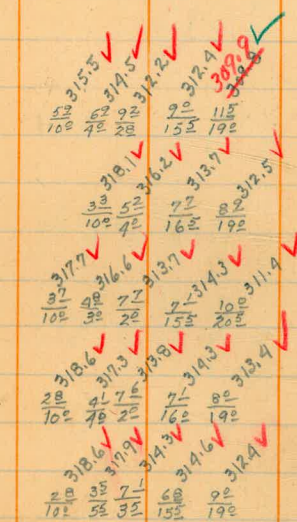
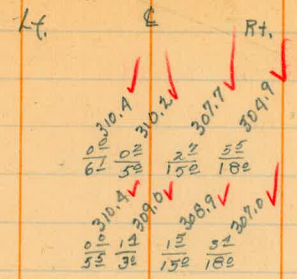


Sta	+	-	Elev.
		301.422	
B28+00		5.2	296.2 ✓
B29+00		4.8	296.6 ✓
+39 ⁶⁶	B.C.	4.4	297.0 ✓
+49 ³		4.1	297.3 ✓
+59 ²		4.0	297.4 ✓
+69 ²		3.9	297.5 ✓
+79 ²		3.8	297.6 ✓
+89 ⁶⁶	E.C.	3.7	297.7 ✓
T.P.		4.119	297.303 ✓
	8.505	305.808	
B30+00		7.8	298.0 ✓
+34 ⁸⁴	B.C.	7.2	298.6 ✓
+59		6.6	299.2 ✓

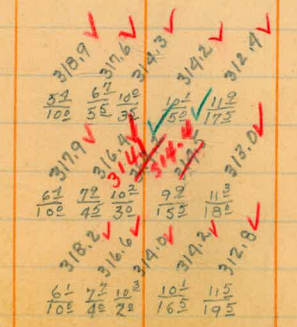
Lt. E Ft.

300.6 ✓
 $\frac{48}{100} \frac{22}{50} \frac{52}{50} \frac{52}{50} \frac{52}{50} \frac{52}{50} \frac{52}{50} \frac{52}{50} \frac{52}{50} \frac{52}{50}$
 299.1 ✓
 296.1 ✓
 296.0 ✓
 299.5 ✓
 296.1 ✓
 $\frac{33}{100} \frac{43}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40}$
 296.5 ✓
 296.5 ✓
 295.0 ✓
 298.2 ✓
 $\frac{32}{100} \frac{43}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40}$
 297.1 ✓
 297.2 ✓
 296.2 ✓
 299.9 ✓
 $\frac{15}{100} \frac{22}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40}$
 299.0 ✓
 297.3 ✓
 297.4 ✓
 296.6 ✓
 299.9 ✓
 $\frac{15}{100} \frac{18}{50} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40} \frac{41}{40}$
 299.6 ✓
 297.3 ✓
 297.3 ✓
 296.5 ✓
 299.4 ✓
 $\frac{20}{100} \frac{25}{50} \frac{37}{50} \frac{40}{50} \frac{40}{50} \frac{40}{50} \frac{40}{50} \frac{40}{50} \frac{40}{50} \frac{40}{50}$
 298.8 ✓
 297.7 ✓
 297.4 ✓
 296.3 ✓
 299.3 ✓
 $\frac{21}{100} \frac{42}{50} \frac{38}{50} \frac{38}{50} \frac{38}{50} \frac{38}{50} \frac{38}{50} \frac{38}{50} \frac{38}{50} \frac{38}{50}$
 299.1 ✓
 297.6 ✓
 297.6 ✓
 295.9 ✓
 299.7 ✓
 $\frac{12}{100} \frac{23}{50} \frac{30}{40} \frac{37}{40} \frac{37}{40} \frac{37}{40} \frac{37}{40} \frac{37}{40} \frac{37}{40} \frac{37}{40}$
 299.1 ✓
 297.5 ✓
 297.7 ✓
 295.1 ✓
 301.0 ✓
 $\frac{48}{100} \frac{56}{70} \frac{58}{50} \frac{58}{50} \frac{58}{50} \frac{58}{50} \frac{58}{50} \frac{58}{50} \frac{58}{50} \frac{58}{50}$
 300.2 ✓
 297.9 ✓
 295.9 ✓
 301.9 ✓
 $\frac{33}{100} \frac{43}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40} \frac{42}{40}$
 298.3 ✓
 299.0 ✓
 296.8 ✓
 302.0 ✓
 $\frac{38}{100} \frac{42}{70} \frac{62}{40} \frac{62}{40} \frac{62}{40} \frac{62}{40} \frac{62}{40} \frac{62}{40} \frac{62}{40} \frac{62}{40}$
 301.6 ✓
 299.6 ✓
 299.6 ✓
 295.1 ✓
 298.9 ✓

Sta	+	T	-	Elev.
		310.377		
833+69 ⁹³	E.C.		3.5	306.9 ✓
8.34+00			1.7	308.7 ✓
T.P.			0.819	309.558 ✓
	11.817	321.375 ✓		
834+60 ⁶¹	B.C.		9.8	311.6 ✓
+85 ⁶			8.6	312.8 ✓
835+10 ⁶			7.9	313.5 ✓
+85 ⁶			7.6	313.8 ✓
+62 ⁶⁹	E.C.		7.2	314.2 ✓
T.P.+B.M. #10 #93		1.942		319.433 ✓
	4.864	324.282		319.418 = Record Elev.
836+00			10.0	314.3 ✓
+21 ⁶²			10.3	314.0 ✓
+31 ⁶			10.3	314.0 ✓



Record Elev. 319.418 Huber Post Sta 835+36 8' L Newline

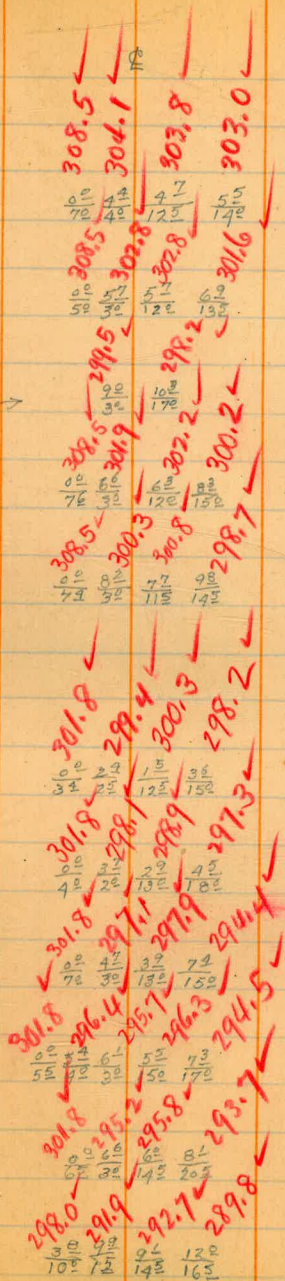


Sta	+	x	-	Elev.
		318.279		
838+392			7.3	311.0
T.P.		5.252		313.027
	5.969	318.996		
+492			8.4	310.6
+57 ⁵⁷	E.C.		8.9	310.1
839+00			10.6	308.4
T.P.		11.718		307.278
	1.173	308.451		
839+762 ¹	B.C.		2.9	305.6
+862			3.3	305.2
+962			3.6	304.9
840+062			3.9	304.6
+162			4.2	304.3
+262			4.4	304.1

314.7	314.5	310.6	311.7	311.5
$\frac{36}{100}$	$\frac{38}{70}$	$\frac{72}{40}$	$\frac{66}{130}$	$\frac{68}{150}$
314.5	314.1	309.9	311.4	310.7
$\frac{45}{100}$	$\frac{42}{70}$	$\frac{91}{100}$	$\frac{76}{130}$	$\frac{88}{150}$
314.7	314.2	309.7	311.1	310.2
$\frac{43}{100}$	$\frac{48}{70}$	$\frac{92}{100}$	$\frac{72}{120}$	$\frac{88}{150}$
312.8	311.8	308.3	308.6	307.2
$\frac{42}{100}$	$\frac{72}{70}$	$\frac{107}{70}$	$\frac{103}{110}$	$\frac{117}{130}$
308.5	305.5	305.5	305.7	304.4
$\frac{61}{100}$	$\frac{30}{30}$	$\frac{20}{110}$	$\frac{41}{140}$	
308.5	308.2	305.2	305.2	304.2
$\frac{54}{100}$	$\frac{30}{100}$	$\frac{10}{120}$	$\frac{40}{140}$	
308.5	304.8	305.1	304.7	303.6
$\frac{50}{100}$	$\frac{12}{30}$	$\frac{32}{120}$	$\frac{40}{150}$	
308.5	304.4	305.1	304.7	303.8
$\frac{50}{100}$	$\frac{9}{30}$	$\frac{33}{120}$	$\frac{40}{150}$	
308.5	304.3	304.2	303.0	302.9
$\frac{50}{100}$	$\frac{40}{30}$	$\frac{40}{120}$	$\frac{55}{140}$	
304.0	304.0	304.0	302.9	
$\frac{40}{100}$	$\frac{40}{30}$	$\frac{40}{120}$	$\frac{76}{140}$	

Sta	+	π	-	Elev.
		308.451		
838	840+29 ³⁶	E.C.	4.4	304.1 ✓
	+71	P.I.	5.7	302.8 ✓
	+99	16" C.I.P. Culvert	6.7	301.8 ✓
841+00			6.7	301.8 ✓
839	+31 ²²	B.C.	6.0	300.5 ✓
	T.P.		6.479	299.972 ✓
	1.875	301.847 ✓		
839+	+56 ²		2.7	299.1 ✓
	+81 ²		3.7	298.1 ✓
842+06 ²			4.6	297.2 ✓
840	+31 ²		6.0	295.8 ✓
	+46 ⁵	E.C.	6.7	295.1 ✓
843+00			9.7	292.1 ✓

Flow line →



Sta	+	X	-	Elev.
		321.847		
83 843+19	P.I.		11.0	290.8 ✓
	T.P.		9.432	292.415 ✓
	0.298	292.713		
844+00			8.0	284.7 ✓
+05 ⁸⁷	B.C.		8.5	284.2 ✓
	T.P.		11.781	280.932 ✓
8	0.583	281.515		
B.M. #	90 #94		10.869	270.646 ✓
	40.869	281.515		
			0.583	280.932 ✓
83	6.736	287.668		
844+302			5.6	282.1 ✓
+55 ²			7.8	279.9 ✓
84	+80 ²		9.5	278.2 ✓
			6.736	280.932 ✓
	0.579	281.511		
845+0582	E.C.		4.9	276.6 ✓

296.2 ✓	291.1 ✓	291.4 ✓	288.2 ✓
$\frac{56}{62}$	$\frac{102}{62}$	$\frac{104}{122}$	$\frac{136}{142}$
292.7 ✓	284.4 ✓	284.8 ✓	284.4 ✓
$\frac{0}{62}$	$\frac{83}{32}$	$\frac{72}{62}$	
292.7 ✓	284.1 ✓	284.4 ✓	
$\frac{0}{62}$	$\frac{86}{42}$	$\frac{83}{72}$	
287.7 ✓	282.2 ✓	282.6 ✓	279.0 ✓
$\frac{0}{62}$	$\frac{55}{42}$	$\frac{51}{122}$	$\frac{82}{142}$
287.7 ✓	280.2 ✓	280.8 ✓	279.3 ✓
$\frac{0}{72}$	$\frac{115}{22}$	$\frac{62}{132}$	$\frac{84}{152}$
287.7 ✓	278.4 ✓	278.9 ✓	277.9 ✓
$\frac{0}{72}$	$\frac{115}{32}$	$\frac{102}{122}$	$\frac{82}{142}$
281.5 ✓	276.9 ✓	277.3 ✓	274.6 ✓
$\frac{0}{72}$	$\frac{115}{32}$	$\frac{102}{122}$	$\frac{82}{142}$

Nail in Tree, 15' R 845+00 Record Elev. ~~269.615~~ 270.666

Sta	+ X	-	Elev.
		281.511	
845+53	P.I.	7.8	273.7 ✓
+68	15" C.I.P. Culvert.	8.4	273.1 ✓
846+00		10.0	271.5 ✓
T.P.		9.542	271.969 ✓
	0.823	272.792 ✓	
847+00		4.5	268.3 ✓
+23	P.I.	5.1	267.7 ✓
848+00		6.2	266.6 ✓
T.P.		5.481	267.361 ✓
	4.225	271.586 ✓	
B.M. # 95		11.811	259.775 ✓
+42	12" Concrete Culvert.	5.0	266.6 ✓
849+00		4.9	266.7 ✓
+1288	B.C.	4.9	266.7 ✓

Flow Line	Elev.
	281.5
	274.2
	274.6
	273.1
	271.0
	269.5
	272.5
	270.3
	272.8
	268.5
	269.3
	267.1
	272.8
	267.2
	272.8
	266.5
	269.3
	260.5
	259.774
Record Elev.	259.0
	271.6
	264.7
	263.8
	267.4
	265.6
	266.8
	267.2
	265.9

Sta	+	π	-	Elev.
		271.586		
8	849+222		4.9	266.7 ✓
	+322		4.8	266.8 ✓
	+372 ⁶ E.C.		4.8	266.8 ✓
	+97 ¹⁴ B.C.		4.6	266.8 ✓
	850+222 ¹		4.8	266.8 ✓
	+387 ⁷ E.C.		4.5	267.1 ✓
	T.P.		3.236	268.350 ✓
8	5.907	274.257 ✓		
	851+00		6.9	267.9 ✓ 267.9
	852+00		5.2	269.1 ✓
8	+131 ⁸ B.C.		5.1	269.2 ✓
	+38 ⁵		4.7	269.6 ✓
	+54 ¹¹ E.C.		4.2	270.1 ✓

271.6 ✓
 $\frac{0.0}{80} \frac{18}{50} \frac{4.0}{30}$
 269.8 ✓
 $\frac{0.0}{70} \frac{5.1}{30} \frac{4.1}{130} \frac{4.0}{140}$
 271.6 ✓
 $\frac{0.0}{80} \frac{18}{50} \frac{4.0}{30}$
 266.7 ✓
 $\frac{0.0}{70} \frac{5.1}{30} \frac{4.1}{130} \frac{4.0}{140}$
 271.6 ✓
 $\frac{0.0}{80} \frac{18}{50} \frac{4.0}{30}$
 266.8 ✓
 $\frac{0.0}{70} \frac{5.1}{30} \frac{4.1}{130} \frac{4.0}{140}$
 271.6 ✓
 $\frac{0.0}{80} \frac{18}{50} \frac{4.0}{30}$
 266.8 ✓
 $\frac{0.0}{70} \frac{5.1}{30} \frac{4.1}{130} \frac{4.0}{140}$
 271.6 ✓
 $\frac{0.0}{80} \frac{18}{50} \frac{4.0}{30}$
 266.8 ✓
 $\frac{0.0}{70} \frac{5.1}{30} \frac{4.1}{130} \frac{4.0}{140}$
 271.6 ✓
 $\frac{0.0}{80} \frac{18}{50} \frac{4.0}{30}$
 267.1 ✓
 $\frac{0.0}{70} \frac{5.1}{30} \frac{4.1}{130} \frac{4.0}{140}$
 274.3 ✓
 $\frac{0.0}{90} \frac{2.7}{50} \frac{5.2}{20} \frac{5.2}{130} \frac{10.0}{150}$
 271.6 ✓
 $\frac{0.0}{90} \frac{2.7}{50} \frac{5.2}{20} \frac{5.2}{130} \frac{10.0}{150}$
 267.9 ✓
 $\frac{0.0}{40} \frac{4.0}{30} \frac{4.0}{130} \frac{5.0}{160}$
 274.3 ✓
 $\frac{0.0}{60} \frac{4.0}{30} \frac{4.0}{130} \frac{5.0}{160}$
 269.1 ✓
 $\frac{0.0}{40} \frac{4.0}{30} \frac{4.0}{130} \frac{5.0}{160}$
 274.3 ✓
 $\frac{0.0}{60} \frac{4.0}{30} \frac{4.0}{130} \frac{5.0}{160}$
 269.2 ✓
 $\frac{0.0}{40} \frac{4.0}{30} \frac{4.0}{130} \frac{5.0}{160}$
 274.3 ✓
 $\frac{0.0}{40} \frac{4.0}{30} \frac{4.0}{130} \frac{5.0}{160}$
 269.6 ✓
 $\frac{0.0}{40} \frac{4.0}{30} \frac{4.0}{130} \frac{5.0}{160}$
 274.3 ✓
 $\frac{0.0}{70} \frac{4.1}{30} \frac{3.8}{140} \frac{5.0}{150}$
 270.1 ✓
 $\frac{0.0}{70} \frac{4.1}{30} \frac{3.8}{140} \frac{5.0}{150}$

May-1

SIMPSON - INST.
REYNOLDS - Red
Isbell - 4

(15)

Sta	+	T	-	Elev
		274.257		
853+00			3.7	270.6 ✓
+45 ⁰⁵	B.C.		3.4	270.9 ✓
+55 ⁰⁵			3.4	270.9 ✓
+65 ⁰⁵			3.4	270.9 ✓
T.P.			3.202	271.055 ✓
	4.247	275.302 ✓		
+75 ⁰⁵			4.5	270.8 ✓
+78 ⁰⁰	E.C.		4.4	270.9 ✓
854+00			4.7	270.6 ✓
855+00			5.9	269.4 ✓
+05	14' X 20' wooden bridge		5.9	269.4 ✓
T.P.			7.409	267.893 ✓
	1.413	269.306 ✓		
856+00			1.7	267.6 ✓

274.3 ✓
270.7 ✓
270.9 ✓
269.3 ✓
271.3 ✓
271.3 ✓
267.2 ✓
271.3 ✓
267.8 ✓
269.8 ✓
271.3 ✓
271.3 ✓
271.3 ✓
271.5 ✓
270.7 ✓
271.5 ✓
271.5 ✓
267.2 ✓
270.8 ✓
271.1 ✓
266.9 ✓
270.8 ✓
270.8 ✓
268.4 ✓
271.3 ✓
269.0 ✓
269.8 ✓
265.9 ✓
265.0 ✓
269.2 ✓
269.2 ✓
261.5 ✓
269.3 ✓
267.5 ✓
267.9 ✓
266.2 ✓

Flow line
Top
↓
6.1
14.2

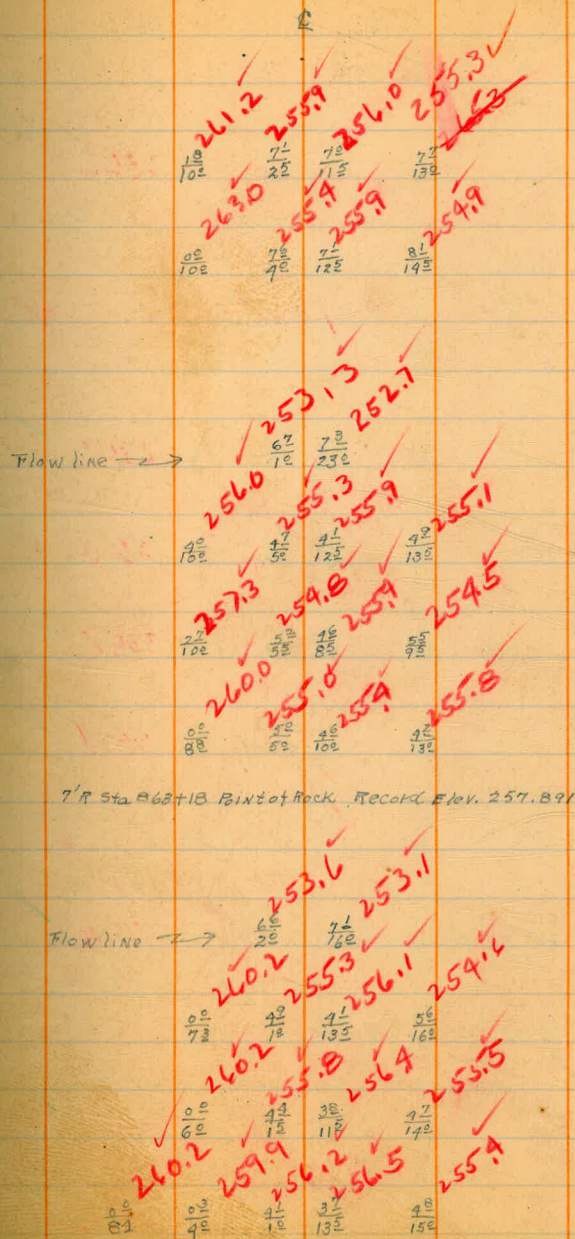
Sta	T	T	Elev.
		269.306	
856+72	P.I.	4.1	265.2 ✓
857+00		4.9	264.4 ✓
858+00		6.9	262.4 ✓
B.M. # 12A	#96	8.968	260.338 ✓
T.P.		8.121	261.185 ✓
	1.832	263.017	
859+00		2.6	260.4 ✓
+06 ³¹	B.C.	2.7	260.3 ✓
+31 ³²		3.2	259.8 ✓
+56 ³³		3.7	259.3 ✓
+81 ³⁴		4.5	258.5 ✓ 263.0
+83 ³⁵	E.C.	4.6	258.4 ✓
860+00		5.4	257.6 ✓

Record Elev. 260.340 - 16' x 868+42 Point on Rock

269.3 ✓
265.3 ✓
265.7 ✓
264.9 ✓
269.3 ✓
264.5 ✓
265.0 ✓
264.2 ✓
269.3 ✓
263.1 ✓
269.3 ✓

263.0 ✓
260.1 ✓
260.7 ✓
259.8 ✓
263.0 ✓
260.0 ✓
260.9 ✓
260.3 ✓
263.0 ✓
259.4 ✓
260.0 ✓
258.2 ✓
263.0 ✓
258.9 ✓
259.9 ✓
259.2 ✓
263.0 ✓
258.8 ✓
258.9 ✓
258.4 ✓
261.4 ✓
258.1 ✓
258.8 ✓
258.5 ✓
261.6 ✓
257.6 ✓
258.3 ✓
257.7 ✓

Sta	+	X	-	Elev.
		263.017		
860+75	P.I.		7.4	255.6 ✓
861+00			7.6	255.4 ✓
T.P.			7.582	255.435 ✓
	4.572	260.007		
+34	18" C.I.P. Culvert.		5.2	254.8 ✓
862+00			4.4	255.6 ✓
863+00			5.1	254.9 ✓
864+00			4.9	255.1 ✓
T.P. + B.M. # 2	#97		2.123	257.884 ✓ 257.891 - Record Elev.
	2.295	260.186		
+28E	16" C.I.P. Culvert.		4.8	255.4 ✓
865+11	P.I.		4.9	255.3 ✓
866+00			4.3	255.9 ✓
+2329	B.C.		4.0	256.2 ✓



T.P. Sta. 862+18 Point of Rock. Record Elev. 257.891

Sta	t	π	-	Elev.
		260.186		
866+48 ^B			4.0	256.2 ✓
T.P.			4.259	255.927 ✓
	5.118	261.045 ✓		
866+72 ⁴	E.C.		4.8	256.2 ✓
867+00			5.2	255.8 ✓
+55 ⁵⁷	B.C.		7.6	253.4 ✓
+80 ^E			8.3	252.7 ✓
868+05 ^E			8.4	252.6 ✓
+12 ²²	E.C.		8.5	252.5 ✓
+15 ²	16" C.I.P. Culvert		8.4	252.6 ✓
T.P.			7.937	253.108 ✓
	7.192	260.300		
B.M. # 78A-98			9.030	251.270 ✓

260.12 ✓
 256.1 ✓
 256.6 ✓
 255.5 ✓
 261.0 ✓
 259.7 ✓
 256.10 ✓
 256.8 ✓
 256.11 ✓
 261.0 ✓
 259.6 ✓
 255.7 ✓
 256.4 ✓
 255.7 ✓
 259.8 ✓
 258.1 ✓
 253.5 ✓
 259.5 ✓
 255.3 ✓
 258.3 ✓
 257.4 ✓
 252.7 ✓
 253.7 ✓
 253.6 ✓
 256.2 ✓
 252.3 ✓
 253.1 ✓
 252.5 ✓
 256.1 ✓
 252.0 ✓
 253.0 ✓
 250.2 ✓
 250.3 ✓
 248.9 ✓
 Flowline →
 Rock 12' Sta 868+22 Recod at Elev. 251.270

McCarty X
Saper-rod
Anderson-rod

(19)

Sta + π - Elev.

#98

May 3

BM# ~~93A~~ 10.869 262.139 ✓ 251.270 ✓

869+00 7.8 254.3 ✓

870+00 3.1 259.0 ✓

870+34.72 1.2 260.9 ✓

T.P. 2.515 π ✓ 263.829 0.825 261.314 ✓

870+44.7 2.4 261.4 ✓

870+54.7 1.9 261.9 ✓

870+64.7 1.7 262.1 ✓

262.1 $\frac{00}{98}$ 254.1 $\frac{80}{40}$ 255.0 $\frac{71}{100}$ 254.6 $\frac{75}{120}$ 252.9 $\frac{93}{130}$

262.1 $\frac{00}{50}$ 258.8 $\frac{33}{33}$ 259.9 $\frac{22}{132}$ 253.5 $\frac{80}{160}$

262.1 $\frac{00}{30}$ 261.0 $\frac{11}{18}$ 262.7 $\frac{11}{170}$ 261.4 $\frac{24}{195}$

263.8 $\frac{00}{34}$ 261.4 $\frac{24}{20}$ 262.5 $\frac{13}{100}$ 263.3 $\frac{05}{210}$ 258.8 $\frac{50}{240}$

263.8 $\frac{00}{32}$ 262.9 $\frac{09}{24}$ 262.8 $\frac{10}{100}$ 263.3 $\frac{05}{190}$ 258.5 $\frac{55}{210}$

263.8 $\frac{00}{40}$ 262.5 $\frac{13}{30}$ 263.0 $\frac{08}{100}$ 263.4 $\frac{04}{160}$ 258.8 $\frac{50}{180}$

Sta.	+	π	-	Elev
870+72 ²⁸		263.829	1.7	262.1
871+00			2.1	261.7
871+37 P.I.			3.3	260.5
872+00			5.1	258.7
872+16 ⁴³			5.5	258.3
872+41 ⁴			5.8	258.0
872+66 ⁴			6.2	257.6
872+70			8.1	255.7
872+91 ⁴			6.2	257.6

(20)

263.8 $\begin{array}{r} 00 \\ 40 \end{array}$	262.3 $\begin{array}{r} 15 \\ 28 \end{array}$	262.9 $\begin{array}{r} 09 \\ 100 \end{array}$	263.2 $\begin{array}{r} 06 \\ 150 \end{array}$	258.8 $\begin{array}{r} 50 \\ 180 \end{array}$
263.8 $\begin{array}{r} 00 \\ 58 \end{array}$	261.5 $\begin{array}{r} 23 \\ 35 \end{array}$	262.8 $\begin{array}{r} 18 \\ 129 \end{array}$	258.8 $\begin{array}{r} 50 \\ 160 \end{array}$	
263.8 $\begin{array}{r} 00 \\ 35 \end{array}$	260.5 $\begin{array}{r} 33 \\ 25 \end{array}$	261.0 $\begin{array}{r} 28 \\ 121 \end{array}$	258.9 $\begin{array}{r} 49 \\ 140 \end{array}$	
263.8 $\begin{array}{r} 00 \\ 46 \end{array}$	258.7 $\begin{array}{r} 51 \\ 24 \end{array}$	259.4 $\begin{array}{r} 44 \\ 124 \end{array}$	256.0 $\begin{array}{r} 78 \\ 140 \end{array}$	
263.8 $\begin{array}{r} 00 \\ 60 \end{array}$	258.5 $\begin{array}{r} 53 \\ 23 \end{array}$	259.3 $\begin{array}{r} 45 \\ 132 \end{array}$	256.8 $\begin{array}{r} 70 \\ 151 \end{array}$	
263.8 $\begin{array}{r} 00 \\ 62 \end{array}$	258.1 $\begin{array}{r} 57 \\ 28 \end{array}$	258.7 $\begin{array}{r} 51 \\ 128 \end{array}$	254.8 $\begin{array}{r} 90 \\ 208 \end{array}$	
263.8 $\begin{array}{r} 00 \\ 73 \end{array}$	257.1 $\begin{array}{r} 67 \\ 32 \end{array}$	258.4 $\begin{array}{r} 54 \\ 140 \end{array}$	254.0 $\begin{array}{r} 98 \\ 212 \end{array}$	
Flow line concrete culvert - 12"				
263.8 $\begin{array}{r} 00 \\ 50 \end{array}$	257.6 $\begin{array}{r} 63 \\ 28 \end{array}$	258.2 $\begin{array}{r} 56 \\ 116 \end{array}$	253.1 $\begin{array}{r} 107 \\ 173 \end{array}$	

Sta.	+	π	-	Elev
873+05 ³²		263.829	6.1	257.7 ✓
873+79 ⁰	P.I.		5.7	258.1 ✓
874+00			54	258.4 ✓
874+84 ⁷⁹			54	258.4 ✓
T.P.	1.053	259.952	4.930	258.899 ✓
874+94 ⁰			1.7	258.3 ✓
875+04 ⁰			1.8	258.2 ✓
875+14 ⁰			2.2	257.8 ✓
875+24 ⁰			2.5	257.5 ✓

(21)

263.8 $\frac{00}{66}$	258.0 $\frac{50}{26}$	258.8 $\frac{50}{123}$	253.3 $\frac{105}{194}$
263.8 $\frac{00}{62}$	258.2 $\frac{56}{30}$	258.9 $\frac{49}{114}$	257.1 $\frac{67}{143}$
263.8 $\frac{00}{72}$	258.4 $\frac{54}{32}$	259.0 $\frac{48}{125}$	256.8 $\frac{70}{160}$
263.8 $\frac{00}{39}$	258.5 $\frac{53}{20}$	259.4 $\frac{06}{130}$	255.4 $\frac{46}{182}$
260.0 $\frac{00}{28}$	258.2 $\frac{18}{23}$	259.6 $\frac{04}{140}$	255.6 $\frac{44}{200}$
260.0 $\frac{00}{34}$	258.1 $\frac{19}{20}$	259.5 $\frac{05}{164}$	256.6 $\frac{34}{215}$
260.0 $\frac{00}{41}$	258.0 $\frac{20}{30}$	259.1 $\frac{00}{170}$	255.7 $\frac{43}{225}$
260.0 $\frac{00}{51}$	257.7 $\frac{23}{30}$	258.6 $\frac{14}{154}$	254.8 $\frac{52}{210}$

Sta.	+	π	-	Elev.
875+34 ⁷		259.952	3.1	256.9 ✓
876+00			7.2	252.8 ✓
876+53 ⁰	P.I.		10.4	249.6 ✓
BM # 94 ⁹⁹	0.090	251.252 ✓	8.802	251.150 ✓ Recorded 251.162
877+00			5.1	246.2 ✓ 246.1
877+23 ⁵			7.0	244.3 ✓ 244.2
877+48 ⁶			8.8	242.5 ✓ 242.4
877+73 ⁶			10.3	241.0 ✓ 240.9
877+86 ⁰			11.2	240.1 ✓ 240.0

(22)

260.0 $\begin{array}{r} 0^{\circ} \\ 4^{\circ} \end{array}$	257.2 $\begin{array}{r} 2^{\circ} \\ 3^{\circ} \end{array}$	257.8 $\begin{array}{r} 2^{\circ} \\ 12^{\circ} \end{array}$	254.1 $\begin{array}{r} 5^{\circ} \\ 18^{\circ} \end{array}$
260.0 $\begin{array}{r} 0^{\circ} \\ 5^{\circ} \end{array}$	253.1 $\begin{array}{r} 6^{\circ} \\ 2^{\circ} \end{array}$	253.8 $\begin{array}{r} 6^{\circ} \\ 12^{\circ} \end{array}$	250.9 $\begin{array}{r} 9^{\circ} \\ 18^{\circ} \end{array}$
260.0 $\begin{array}{r} 2^{\circ} \\ 10^{\circ} \end{array}$	249.7 $\begin{array}{r} 10^{\circ} \\ 2^{\circ} \end{array}$	250.4 $\begin{array}{r} 9^{\circ} \\ 14^{\circ} \end{array}$	247.4 $\begin{array}{r} 12^{\circ} \\ 16^{\circ} \end{array}$
251.3 $\begin{array}{r} 1^{\circ} \\ 10^{\circ} \end{array}$	249.8 $\begin{array}{r} 1^{\circ} \\ 5^{\circ} \end{array}$	246.4 $\begin{array}{r} 4^{\circ} \\ 1^{\circ} \end{array}$	257.7 $\begin{array}{r} 3^{\circ} \\ 21^{\circ} \end{array}$
251.3 $\begin{array}{r} 0^{\circ} \\ 9^{\circ} \end{array}$	244.8 $\begin{array}{r} 6^{\circ} \\ 2^{\circ} \end{array}$	245.9 $\begin{array}{r} 5^{\circ} \\ 21^{\circ} \end{array}$	243.7 $\begin{array}{r} 7^{\circ} \\ 25^{\circ} \end{array}$
248.9 $\begin{array}{r} 2^{\circ} \\ 10^{\circ} \end{array}$	247.2 $\begin{array}{r} 4^{\circ} \\ 6^{\circ} \end{array}$	242.4 $\begin{array}{r} 8^{\circ} \\ 2^{\circ} \end{array}$	243.8 $\begin{array}{r} 7^{\circ} \\ 19^{\circ} \end{array}$
246.3 $\begin{array}{r} 5^{\circ} \\ 10^{\circ} \end{array}$	244.8 $\begin{array}{r} 6^{\circ} \\ 6^{\circ} \end{array}$	241.1 $\begin{array}{r} 10^{\circ} \\ 3^{\circ} \end{array}$	241.6 $\begin{array}{r} 9^{\circ} \\ 13^{\circ} \end{array}$
246.8 $\begin{array}{r} 4^{\circ} \\ 10^{\circ} \end{array}$	244.9 $\begin{array}{r} 6^{\circ} \\ 5^{\circ} \end{array}$	239.8 $\begin{array}{r} 11^{\circ} \\ 2^{\circ} \end{array}$	240.8 $\begin{array}{r} 10^{\circ} \\ 14^{\circ} \end{array}$
			239.3 $\begin{array}{r} 12^{\circ} \\ 26^{\circ} \end{array}$
			238.5 $\begin{array}{r} 13^{\circ} \\ 27^{\circ} \end{array}$
			238.0 $\begin{array}{r} 13^{\circ} \\ 20^{\circ} \end{array}$

Sta.	+	π	-	Elev.
8 878+00		251.252	11.9	239.3 239.4 ✓
8 T.P.	4.023	242.774 ✓	12.501	238.751 ✓
8 878+36 ³⁶		5.0		237.8 ✓
8 878+464		5.2		237.6 ✓
8 878+564		5.3		237.5 ✓
8 878+664		5.6		237.2 ✓
8 878+764		5.8		237.0 ✓
8 878+793 ⁴		6.1		236.7 ✓
878+93		7.5		235.3 ✓ Flow line
8 879+00		6.0		236.8 ✓

(23)

244.7 ✓ $\frac{66}{100}$	239.2 ✓ $\frac{121}{200}$	240.1 ✓ $\frac{112}{132}$	238.2 ✓ $\frac{131}{168}$
240.6 ✓ $\frac{22}{100}$		238.6 ✓ $\frac{42}{142}$	236.0 ✓ $\frac{68}{212}$
241.7 ✓ $\frac{11}{100}$	237.8 ✓ $\frac{59}{25}$	238.7 ✓ $\frac{46}{152}$	235.7 ✓ $\frac{71}{208}$
242.8 ✓ $\frac{02}{58}$	237.5 ✓ $\frac{53}{23}$	237.9 ✓ $\frac{49}{172}$	236.6 ✓ $\frac{62}{202}$
242.1 ✓ $\frac{07}{100}$	240.2 ✓ $\frac{26}{35}$	237.4 ✓ $\frac{54}{202}$	234.0 ✓ $\frac{88}{252}$
242.8 ✓ $\frac{02}{74}$	239.4 ✓ $\frac{34}{35}$	237.1 ✓ $\frac{57}{25}$	237.7 ✓ $\frac{51}{188}$
242.8 ✓ $\frac{02}{80}$	238.9 ✓ $\frac{39}{32}$	237.0 ✓ $\frac{58}{28}$	237.7 ✓ $\frac{51}{188}$
242.8 ✓ $\frac{02}{102}$	240.7 ✓ $\frac{21}{55}$	236.3 ✓ $\frac{65}{22}$	237.6 ✓ $\frac{52}{162}$
			235.4 ✓ $\frac{74}{232}$

1 Con. Culvert

Sta.	+	π	-	Elev.
880+00		242.774	6.0	236.8 ✓
880+07 ⁸⁸			6.1	236.7 ✓
880+17 ⁹			6.0	236.8 ✓
880+27 ⁹			5.8	237.0 ✓
880+37 ⁹			5.8	237.0 ✓
880+39 ⁷⁴			5.8	237.0 ✓
881+00			5.0	237.8 ✓
881+59 P.I.			4.6	238.2 ✓
882+00			3.9	238.9 ✓

242.8 $\frac{0^{\circ}}{82}$	241.8 $\frac{1^{\circ}}{69}$	236.5 $\frac{6^{\circ}}{32}$	237.3 $\frac{5^{\circ}}{151}$	233.9 $\frac{8^{\circ}}{224}$
242.8 $\frac{0^{\circ}}{91}$	240.8 $\frac{2^{\circ}}{53}$	236.6 $\frac{6^{\circ}}{30}$	237.3 $\frac{5^{\circ}}{163}$	233.7 $\frac{9^{\circ}}{230}$
242.8 $\frac{0^{\circ}}{95}$	240.5 $\frac{2^{\circ}}{47}$	236.8 $\frac{6^{\circ}}{24}$	237.4 $\frac{5^{\circ}}{172}$	234.2 $\frac{8^{\circ}}{242}$
242.8 $\frac{0^{\circ}}{102}$	239.7 $\frac{3^{\circ}}{43}$	237.4 $\frac{5^{\circ}}{30}$	237.5 $\frac{5^{\circ}}{180}$	235.6 $\frac{7^{\circ}}{252}$
240.1 $\frac{2^{\circ}}{100}$	239.4 $\frac{3^{\circ}}{52}$	237.3 $\frac{5^{\circ}}{35}$	237.5 $\frac{5^{\circ}}{170}$	234.9 $\frac{7^{\circ}}{230}$
240.4 $\frac{2^{\circ}}{100}$	239.3 $\frac{3^{\circ}}{62}$	237.6 $\frac{5^{\circ}}{40}$	237.5 $\frac{5^{\circ}}{172}$	234.7 $\frac{8^{\circ}}{242}$
242.8 $\frac{0^{\circ}}{79}$	241.2 $\frac{1^{\circ}}{42}$	237.8 $\frac{5^{\circ}}{30}$	238.5 $\frac{4^{\circ}}{170}$	235.3 $\frac{7^{\circ}}{254}$
242.8 $\frac{0^{\circ}}{60}$	242.4 $\frac{0^{\circ}}{53}$	238.7 $\frac{4^{\circ}}{20}$	238.9 $\frac{3^{\circ}}{130}$	235.6 $\frac{7^{\circ}}{180}$
242.4 $\frac{0^{\circ}}{100}$	239.0 $\frac{3^{\circ}}{40}$		239.3 $\frac{3^{\circ}}{132}$	234.8 $\frac{8^{\circ}}{190}$

McCarty-rod
Reynolds T
Anderson-rod

(25)

Sta.	+	T	-	Elev.
883+00		242.774	1.6	241.2

242.8 $\begin{array}{r} 00 \\ 23 \end{array}$	241.3 $\begin{array}{r} 15 \\ 12 \end{array}$	241.8 $\begin{array}{r} 10 \\ 154 \end{array}$	239.2 $\begin{array}{r} 36 \\ 195 \end{array}$
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T.P.		1.025	241.749	May 4
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$\frac{0}{10}$	$\frac{75}{2.7}$	$\frac{22}{14}$	$\frac{110}{174}$
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10.196 ~~251.935~~ **251.945**

883+40		10.0	241.9
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251.0 $\begin{array}{r} 09 \\ 10 \end{array}$	242.2 $\begin{array}{r} 32 \\ 2.7 \end{array}$	242.4 $\begin{array}{r} 95 \\ 14 \end{array}$	240.9 $\begin{array}{r} 170 \\ 17.4 \end{array}$
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883+70		9.6	242.3	16" C.I.P. Cabot
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243.4
 $\begin{array}{r} 249.1 \\ 85 \\ 10 \end{array}$

240.1 $\begin{array}{r} 118 \\ 64 \end{array}$	242.0 $\begin{array}{r} 22 \\ 4.8 \end{array}$	242.5 $\begin{array}{r} 92 \\ 133 \end{array}$	240.2 $\begin{array}{r} 112 \\ 15 \end{array}$
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884+00		8.8	243.1
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242.8 $\begin{array}{r} 91 \\ 10 \end{array}$	245.4 $\begin{array}{r} 83 \\ 112 \end{array}$	240.1 $\begin{array}{r} 118 \\ 145 \end{array}$
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884+15		8.2	243.7
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249.3 $\begin{array}{r} 24 \\ 102 \end{array}$	244.7 $\begin{array}{r} 72 \\ 92 \end{array}$	244.0 $\begin{array}{r} 79 \\ 118 \end{array}$	240.6 $\begin{array}{r} 113 \\ 156 \end{array}$
---	--	---	--

884+47 ^e		6.3	245.6
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251.9 $\begin{array}{r} 02 \\ 55 \end{array}$	245.4 $\begin{array}{r} 65 \\ 3.0 \end{array}$	246.1 $\begin{array}{r} 58 \\ 15.0 \end{array}$	244.5 $\begin{array}{r} 74 \\ 175 \end{array}$
--	---	--	---

884+72 ^a		5.6	246.9
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251.9 $\begin{array}{r} 02 \\ 44 \end{array}$	246.8 $\begin{array}{r} 51 \\ 3.0 \end{array}$	247.9 $\begin{array}{r} 40 \\ 12.5 \end{array}$	250.0 $\begin{array}{r} 19 \\ 182 \end{array}$	246.9 $\begin{array}{r} 50 \\ 24.0 \end{array}$
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Sta	+	x	-	Elev.
884+97 ²			3.9	248.0 ✓
		10.914	0.801	251.144 ✓
886+22.9			12.6	249.5 ✓ 249.4
885+47 ²			11.0	251.1 ✓ 251.0
885+72 ²			9 ^e	252.5 ✓ 252.4
885+84 ²			8 ²	253.2 ✓ 253.1
886+00			7.9	254.2 ✓ 254.1
887+00			5.5	256.6 ✓ 256.5
887+39 ²			6.4	255.7 ✓ 255.6

251.945
~~251.835~~
262.058
~~262.048~~

251.9 ✓ 251.8 70	251.6 ✓ 251.5 50	248.0 ✓ 247.9 3.0	248.8 ✓ 248.7 135	248.4 ✓ 248.3 165
254.5 ✓ 254.4 7 ^e 10 ^e	252.7 ✓ 252.6 9 ^e 51	249.5 ✓ 249.4 12 ^e 3.0	250.0 ✓ 249.9 12 ^e 12 ^e	249.2 ✓ 249.1 12 ^e 14 ^e
256.9 ✓ 256.8 5 ^e 10 ^e	255.7 ✓ 255.6 6 ^e 63	251.0 ✓ 250.9 11 ^e 3.0	251.4 ✓ 251.3 10 ^e 12 ^e	250.1 ✓ 250.0 12 ^e 15 ^e
259.2 ✓ 259.1 2 ^e 10 ^e	256.4 ✓ 256.3 5 ^e 53	252.5 ✓ 252.4 9 ^e 3.0	253.1 ✓ 253.0 8 ^e 12 ^e	251.3 ✓ 251.2 10 ^e 14 ^e
261.2 ✓ 261.1 0 ^e 10 ^e	260.2 ✓ 260.1 1 ³ 10 ^e	257.7 ✓ 257.6 8 ^e 3.0	259.0 ✓ 258.9 8 ^e 13 ^e	251.3 ✓ 251.2 10 ^e 14 ^e
262.1 ✓ 262.0 0 ^e 63	261.3 ✓ 261.2 0 ^e 42	259.8 ✓ 259.7 7 ³ 3.0	255.0 ✓ 254.9 7 ^e 13 ^e	252.3 ✓ 252.2 8 ^e 16 ^e
262.1 ✓ 262.0 0 ^e 52	256.5 ✓ 256.4 5 ^e 4 ^e	257.1 ✓ 257.0 5 ^e 11 ^e	255.0 ✓ 254.9 7 ^e 13 ^e	254.7 ✓ 254.6 7 ^e 14 ^e
259.0 ✓ 258.9 3 ^e 10 ^e	255.6 ✓ 255.5 6 ^e 5.0	256.1 ✓ 256.0 6 ^e 12 ^e	256.1 ✓ 256.0 6 ^e 12 ^e	253.4 ✓ 253.3 8 ^e 14 ^e

Sta.	+	π	-	Elev.
		262.058		
887+492			6.7	255.4 255.3 ✓
887+592			7.4	254.7 254.6 ✓
887+692			7.8	254.3 254.2 ✓
887+792			7.9	254.2 254.1 ✓
887+82 ³⁴			8.1	254.0 253.9 ✓
B.M. 95A #100			3.030	259.028 259.018 ✓
B.M. 95B #101	1.711	253.315		251.604 ✓
888+00			0.0	253.3 ✓

262.1	255.3	255.8	254.3
262.1	255.0	255.5	254.3
262.1	254.3	254.8	251.7
258.0	253.9	254.4	251.3
257.8	253.7	254.1	250.9

B.M.#100 Recorded Elev. = 259.092

B.M.#101 Recorded Elev = 251.604

253.3	253.1	253.3
02	02	02
24	25	10

Sta	+	π	Elev
888+15 [±]		253.315 ✓	0.4 252.7 ✓
888+25 [±]		1 [±]	252.2 ✓
888+35 [±]		1 [±]	251.9 ✓
888+45 [±]		1 [±]	251.7 ✓
888+55 [±]		1 [±]	251.7 ✓
888+58 [±]		1 [±]	251.7 ✓
Concrete culvert 888+90			
889+00		2 [±]	250.6 ✓

253.3 0.2 3.1	252.6 0.2 2.2	253.2 0.1 1.0	
253.3 0.0 3.5	252.7 0.6 4.0	253.2 0.1 14.0	252.0 1.3 17.0
253.3 0.2 4.3	252.7 1.1 3.0	252.9 0.4 15.0	251.3 2.2 18.0
253.3 0.2 6.3	251.6 1.2 4.0	252.4 0.2 15.0	251.1 3.2 18.5
	253.3 0.2 8.2	252.1 1.2 15.0	249.6 3.2 19.0
	253.3 0.4 8.6	251.2 2.1 7.0	252.1 1.2 15.0
			250.1 3.2 17.5
			249.0
Flow line 1 253.3 0.2 3.1	250.5 2.8 2.2	251.2 2.1 13.5	249.0 4.3 16.5

	+	π	Elev.
		2533150	
889+6350	4.1	249.2	✓
889+7350	4.1	249.2	✓
889+8350	4.3	249.0	✓
889+9350	4.2	248.6	✓
890+0350	5.1	248.2	✓
890+1350	5.5	247.8	✓
890+2350	6.0	247.3	✓
890+3350	6.5	246.8	✓

2533.3 00 62	249.7 30 30	250.1 32 132	248.3 50 164
2533 00 62	249.1 42 30	249.8 35 112	247.6 63 155
2533 00 52	249.1 42 35	249.5 38 112	248.3 52 132
2533 00 52	249.1 42 42	249.2 41 112	246.9 67 135
3533.3 00 52	248.5 40 42	249.0 43 112	246.7 64 124
2533 00 42	248.0 53 30	248.8 45 125	246.6 62 143
2533 00 37	247.3 60 25	248.4 49 145	246.7 66 182
2533 00 46	247.1 62 32	247.7 56 158	246.3 70 180

	+	✓ -	Elev.
		✓	2533.15
8904482		6.8	246.5 ✓
14" concrete 890+93		8.5	242.8 ✓
891+00		7.2	246.1 ✓
891+40		6.2	246.6 ✓
891+55		6.0	247.3 ✓
891+75		4.9	248.4 ✓
14" concrete 891+85		6.3	247.0 ✓
891+96.34		3.2	249.6 ✓
I.P.		✓	2966 250.349 ✓
	10.937	261.286	

2533 00 2533	246.9 6.4 25	247.7 5.4 142	246.2 7.1 175
246.5 6.8 270.2	246.4 6.2 40	246.5 6.8 132	244.9 8.4 155
250.1 3.3 170.2	247.2 6.1 22	247.2 6.1 103	
2533 00 3233	247.6 5.2 22	247.8 5.5 10	
	248.7 4.4 102	248.9 4.4 112	247.6 5.2 138
	250.3 3.4 102	249.9 3.4 115	247.5 5.8 132

+	π	-	Elev.
	261.286		
892+212	10e		251.3 ✓
892+4752	81		258.2 ✓
893+00	5.6		255.7 ✓
893+434	5.3		256.0 ✓
893+534	5.3		256.0 ✓
893+634	5.3		256.0 ✓
893+734	5.6		255.7 ✓
893+834	55		255.8 ✓

261.3 0e 7e	259.7 7e 42	251.1 10e 24	252.3 7e 193	250.7 10e 23e
261.3 0e 42	253.4 7e 24	254.1 7e 168	258.4 3e 181	
261.3 0e 81	257.5 3e 36	255.9 5e 32	255.7 5e 14e	253.4 7e 18e
261.3 0e 43	256.3 5e 24	256.5 4e 142	254.9 6e 17e	
261.3 0e 8e	256.4 4e 34	256.3 5e 144	254.0 7e 1e4	
261.3 0e 95	256.1 5e 33	256.2 5e 154	253.3 8e 17e	
261.3 0e 9e	258.5 7e 35	256.1 5e 24	255.9 5e 155	254.0 7e 17e
261.3 0e 57	256.1 5e 24	256.3 5e 152	254.6 6e 181	

Sta	+	Δ	-	Elev
		261.286		
893	+91.44		5.5	255.8 ✓
893	+00	256.7	6.097 ✓	255.189 ✓
		257.756		
894	+00		2.2	255.8 ✓
894	+102.4		2.2	255.6 ✓
894	+36.0		2.5	255.3 ✓
894	+61.0		2.8	255.0 ✓
894	+80.24		3.3	254.5 ✓
895	+00		3.7	254.1 ✓

(32)

$\frac{0.0}{6.3}$	$\frac{5.4}{2.4}$	$\frac{5.0}{1.5}$	$\frac{6.7}{1.9}$
261.3 ✓	255.9 ✓	256.3 ✓	255.0 ✓
$\frac{0.0}{4.8}$	$\frac{2.1}{3.3}$	$\frac{1.5}{1.3}$	$\frac{3.4}{1.7}$
257.8 ✓	255.7 ✓	256.3 ✓	254.9 ✓
$\frac{0.0}{6.5}$	$\frac{2.2}{4.2}$	$\frac{2.0}{1.2}$	$\frac{4.4}{1.5}$
257.8 ✓	255.4 ✓	255.8 ✓	253.4 ✓
$\frac{0.0}{3.8}$	$\frac{2.6}{2.2}$	$\frac{2.2}{1.2}$	$\frac{1.3}{1.6}$
257.8 ✓	255.2 ✓	255.6 ✓	253.5 ✓
$\frac{0.0}{4.6}$	$\frac{2.2}{4.0}$	$\frac{2.5}{1.4}$	$\frac{3.9}{1.7}$
257.8 ✓	255.1 ✓	255.3 ✓	253.9 ✓
$\frac{0.0}{4.2}$	$\frac{3.8}{1.0}$	$\frac{3.1}{1.2}$	$\frac{4.8}{1.4}$
257.8 ✓	255.0 ✓	254.7 ✓	253.0 ✓
$\frac{0.0}{4.2}$	$\frac{3.8}{1.8}$	$\frac{3.2}{1.4}$	$\frac{4.4}{1.6}$
257.8 ✓	254.0 ✓	254.6 ✓	253.9 ✓

+	Δ	-	Elev.
	257.756		
895+09 ^e	3.9	253.9 ✓	
895+55	4.7	253.1 ✓	
12" C.I.P. Curve 895+63	6.9	250.9 ✓	
896+00	5.4	252.4 ✓	
896+06 ³⁰	5.5	252.3 ✓	
896+30 ⁸	5.2	252.2 ✓	
896+55 ²	6.2	251.7 ✓	
896+75 ²⁴	6.3	251.5 ✓	

0 ^e 3.9	257.8 ✓	0 ^e 3.2	259.1 ✓	0 ^e 3.2	259.4 ✓	0 ^e 4.2	253.4 ✓
0 ^e 4.1	253.7 ✓	0 ^e 4.1	253.7 ✓	0 ^e 4.2	253.5 ✓	0 ^e 6.2	251.7 ✓
0 ^e 5.4	257.8 ✓	0 ^e 5.4	252.4 ✓	0 ^e 5.5	253.9 ✓	0 ^e 6.2	252.0 ✓
0 ^e 5.5	256.9 ✓	0 ^e 5.5	255.6 ✓	0 ^e 5.2	252.1 ✓	0 ^e 6.2	251.5 ✓
0 ^e 5.2	257.8 ✓	0 ^e 5.2	256.3 ✓	0 ^e 5.2	251.8 ✓	0 ^e 7.2	250.0 ✓
0 ^e 6.2	251.8 ✓	0 ^e 6.2	251.8 ✓	0 ^e 6.2	251.9 ✓	0 ^e 7.2	249.9 ✓
0 ^e 6.3	255.5 ✓	0 ^e 6.3	254.2 ✓	0 ^e 6.3	251.6 ✓	0 ^e 7.2	250.0 ✓

Sta	+	π	-	Elev
		257.756		
897+00		6.3	251.5	✓
897+20		6±	251.4	✓
12" ^{concrete} culvert 897+34		8.0 low line 9±	248.7	✓
B.M. 96		5.089	252.667	✓
	5.642	258.309		
898+00		7.7	250.6	✓
898+06		7.7	250.6	✓
899+00		6.7	251.6	✓
899+59		5.3	253.0	✓

12 102	22 48	63 25	6 152	72 172
32 102	38 52	63 41	6 112	100 142
32 102	48 52	75 32	7± 142	80 172
35 102	46 52	72 22	70 142	72 162
42 102		60 42	6 132	80 172
00 74	52 23	52 242	60 282	

256.1 ✓
 255.1 ✓
 251.5 ✓
 254.1 ✓
 254.0 ✓
 251.5 ✓
 251.7 ✓
 250.1 ✓
 254.6 ✓
 253.5 ✓
 250.8 ✓
 251.2 ✓
 250.3 ✓
 254.8 ✓
 253.7 ✓
 250.6 ✓
 251.3 ✓
 250.6 ✓
 253.6 ✓
 251.4 ✓
 252.2 ✓
 250.3 ✓
 258.3 ✓
 253.1 ✓
 253.1 ✓
 251.4 ✓

Sta	+	λ	-	Elev
		2583.09		
900+00		4.1		254.2 ✓
900+18.22		3.9		254.4 ✓
900+43.2		3.5		254.8 ✓
reconcrete culvert 900+60		flow line 4.8		253.5 ✓
900+68.2		3.0		255.3 ✓
900+88.95		2.2		255.6 ✓
901+00		2.5		255.8 ✓
T.P.		0.946		257.363 ✓
	3.739	261.102		
BM #103		3.448		251.654 ✓

1.6 10.2	2.2 4.8	4.1 2.4	3.6 15.2	4.2 17.8
2.2 10.2	5.2 4.1	4.1 2.2	3.2 12.2	5.2 13.2
1.8 10.2	2.1 6.3	4.6 5.2	3.4 15.2	4.2 19.2
1.2 10.2	1.2 5.2	3.2 4.2	2.2 15.2	5.2 7.2
0.4 5.2	2.2 3.2	2.4 12.2	0.2 16.2	4.2 2.3
0.2 3.2	2.4 2.5	2.1 12.2	1.4 16.2	3.2 21.4

BM #103 Recorded Elev. = 251.665

MAY-8.

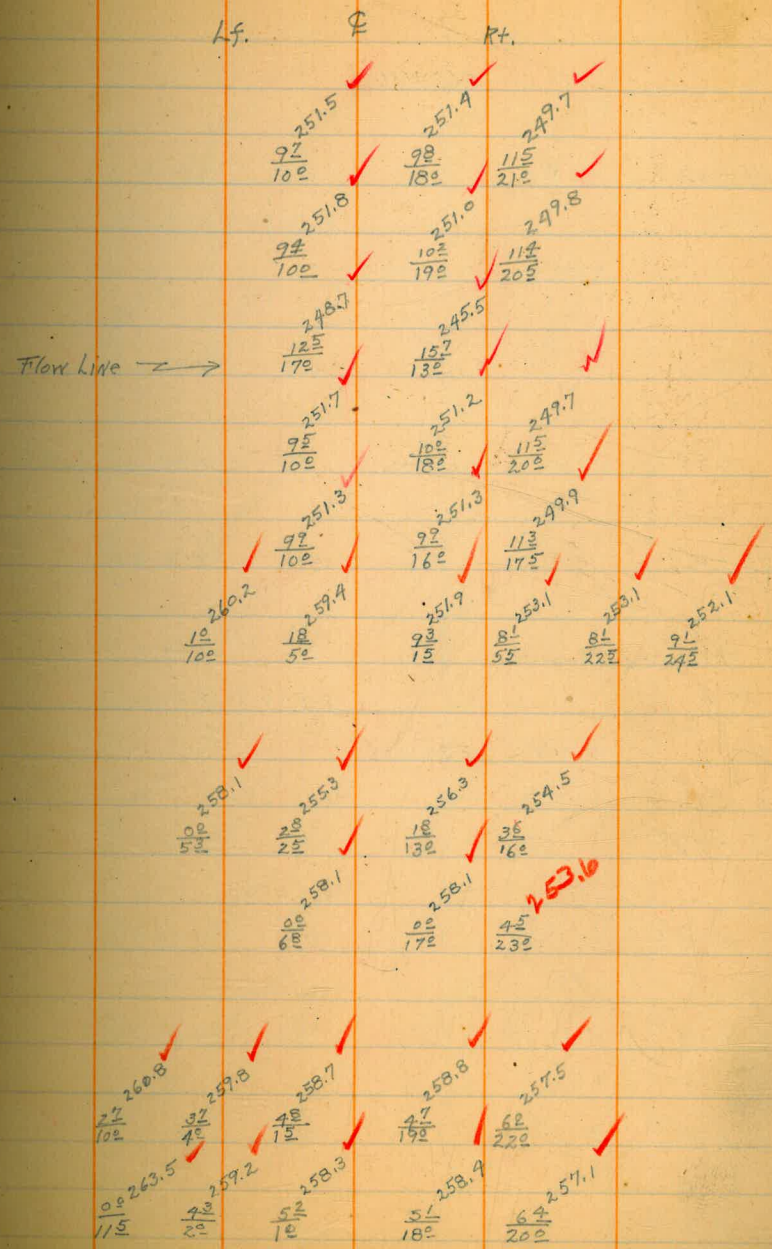
SIMPSON - Inst.
Isbell - Rod.
Anderson - "

(36)

Sta	+	π	-	Elev.	
B.M. #103				251.665	X
	9.581				
		261.246			
901+270			5.2	256.0	✓
+370			5.2	256.0	✓
+470			5.1	256.1	✓
+570			5.1	256.1	✓
+670			5.3	255.9	✓
+770			5.5	255.7	✓
+870			5.8	255.4	✓
+930	E.C.		6.0	255.2	✓
902+00			6.4	254.8	✓
+54 ⁹³	B.C.		8.5	252.7	✓
+64 ⁹			9.0	252.2	✓

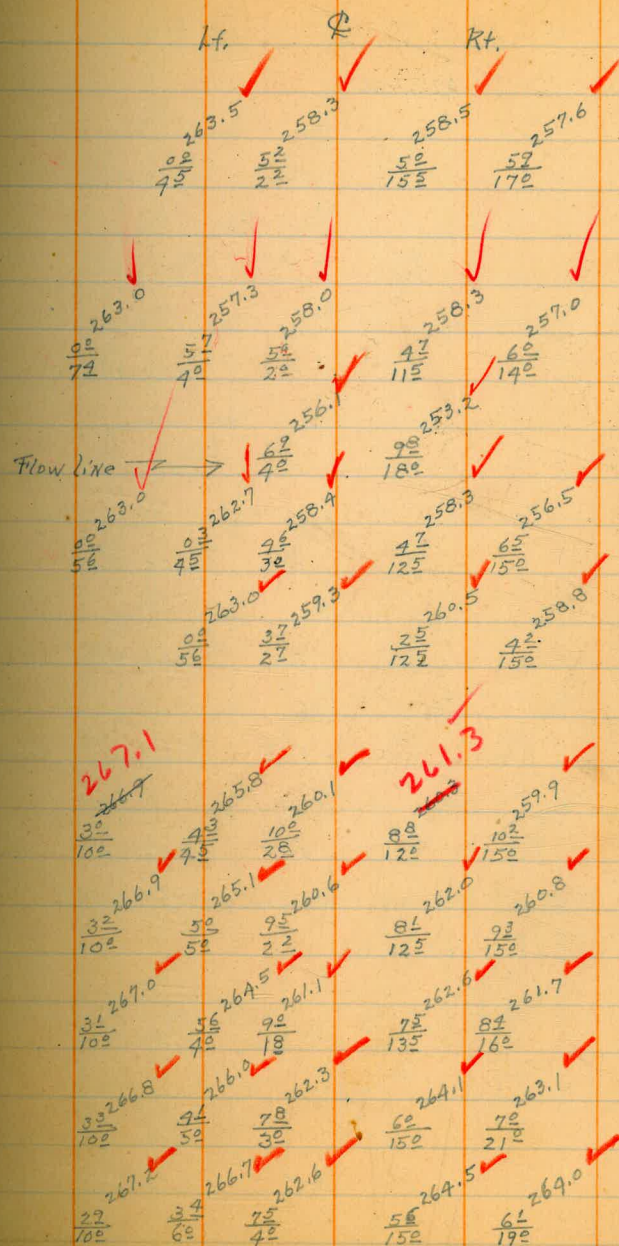
L	R	RT
0.0 77	261.2	255.9
0.0 75	261.2	256.0
0.0 54	261.2	256.3
0.0 74	261.2	256.1
0.0 62	261.2	255.9
0.0 67	261.2	256.1
0.0 77	261.2	255.2
0.0 74	261.2	255.1
0.0 85	261.2	255.7
5.3 145	255.7	253.1
9.0 100	255.9	250.1
4.6 153	256.6	254.4
4.2 142	257.0	255.8
4.1 145	257.1	256.0
4.2 155	257.0	255.8
4.3 170	256.9	256.2
4.4 200	256.8	255.6
4.7 210	256.7	255.2
5.1 230	256.1	255.0
5.5 240	255.7	254.3
5.5 240	255.7	254.3
7.1 128	252.1	250.8
9.1 175	252.1	250.1

Sta	+ π	- Elev.
	261.246	
902+74 ²	9.4	251.8
+84 ²	9.7	251.5
+87 ²	18" C. I. P. Culvert on Curve. 9.7	251.5
+94 ²	9.7	251.5
903+02 ⁵²	E. C., 9.8	251.4
904+00	6.4	254.8
T. P.	9.581	251.665
	6.451	258.116
904+66 ⁰	P. I. 2.0	256.1
905+00	0.3	257.8
T. P.	1.270	256.896
	6.631	263.977
905+42 ⁰	P. I. 4.6	258.9
906+00	5.1	258.4



		263.477			
906+420	P.I.		5.2	258.3	✓
T.P.			5.192	258.285	✓
	4.703	262.988			
907+00			4.8	258.2	✓
+590	12" Concrete Culvert		5.0	258.0	✓
908+00			4.6	258.4	✓
+78 ⁶⁸	B.C.		3.1	259.9	✓
T.P.			2.351	260.637	✓
	9.509	270.196			
909+032			9.5	260.6	✓
+282			8.8	261.3	✓
+38 ⁹⁴	E.C.		8.6	261.5	✓
+72 ⁷²	B.C.		7.2	262.9	✓
+82 ⁵			6.7	263.4	✓

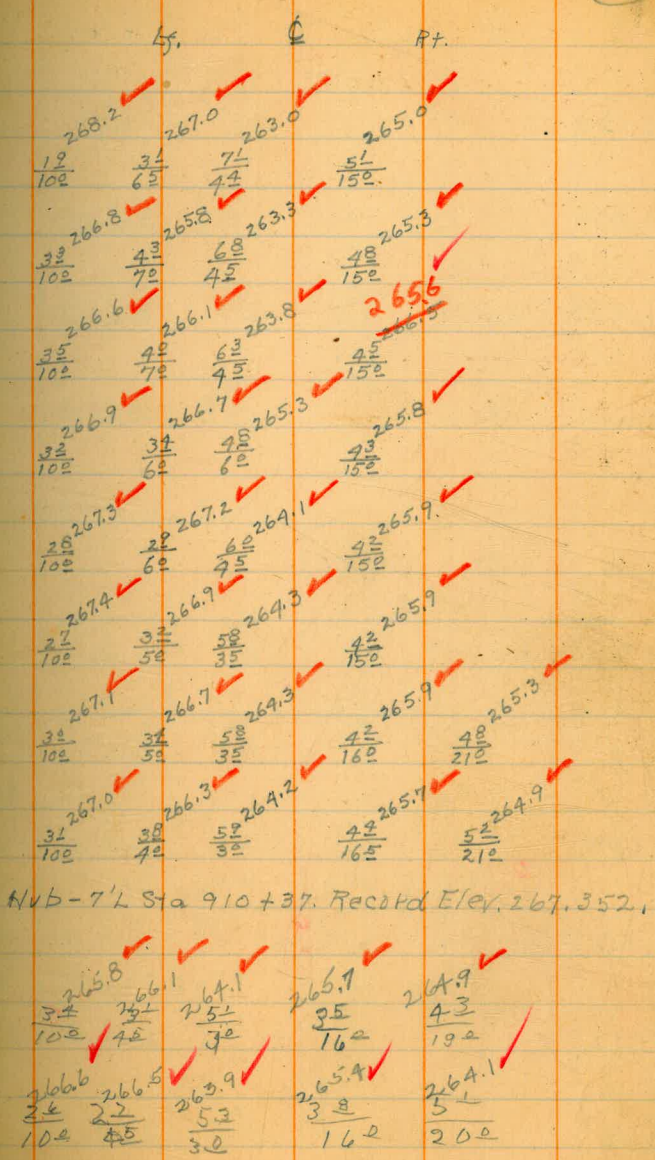
(38)



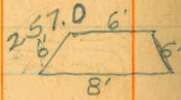
+ π ✓ - Elev

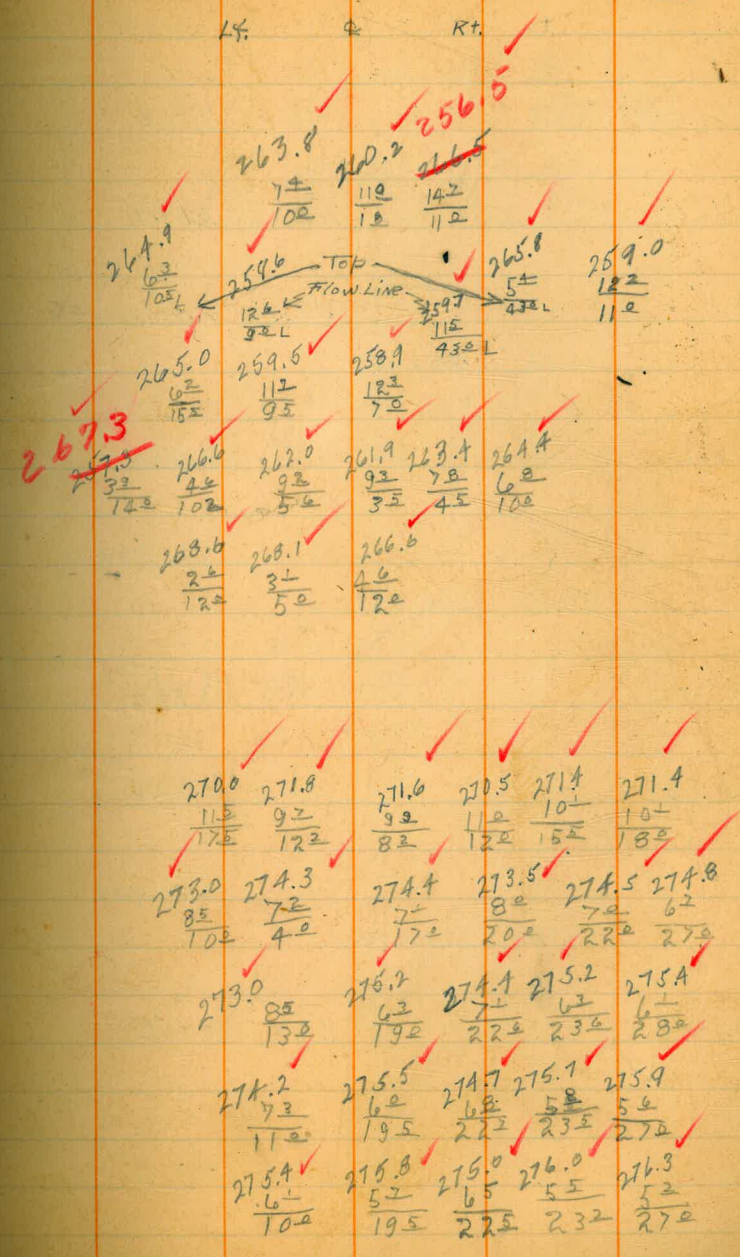
270.196

909+92.5	6.3	263.8	✓
910+02.5	6.0	264.1	✓
+12.5	5.7	264.4	✓
+22.5	5.4	264.7	✓
+32.5	5.3	264.8	✓
+42.5	5.4	264.7	✓
+52.5	5.4	264.7	✓
+62.5	5.5	264.6	✓
T.P. + B.M. #104	2.796	267.350	✓
1.832	269.187		
910+72.5	4.8	264.4	✓
910+82.5	4.9	264.3	✓



NVB-7' L Sta 910+37. Record Elev. 267.352.

	+	π	-	Elev.
				266.13 ⁵
	5.038		271.17 ³	
915+43			9.0	262.2
915+87 ^e	center of Wash. opp. wooden Culvert.		14.2	257.0
				
916+00			11.6	259.6
916+31			10.1	261.1
916+51			4.3	266.9
T.P.			1384	269.78 ⁹
	11.695		281.78 ⁴	
917+00			9.4	272.1
917+33 ^e	B.C.		6.9	274.6
917+43 ^e			6.1	275.4
917+53 ^e			5.4	276.1
917+63 ^e			4.5	277.0



	+	⌊	-	Elev
917+49 ⁷³	E.C.	281.48 ⁴	3.7	277.8
918+00			1.6	279.9
T.P.		0.282		281.20 ²
919+00		11.969	71	293.169
T.P.		12.549	9	305.537
920+00			11.1	294.4
921+00			4.9	300.6
T.P.		10.188	6	314.674
922+00			8.9	305.8
923+00			2.8	311.9

L	C	R
276.0 5 ⁵ 10 ⁰	277.6 4 ⁰ 7 ²	276.4 5 ¹ 18 ⁵
277.0 4 ⁵ 70 ⁰	279.9 6 ⁰ 4 ⁰	278.0 2 ⁷ 14 ²
290.1 3 ¹ 12 ²	289.5 3 ² 4 ⁸	286.6 6 ⁰ 2 ⁵
296.8 8 ² 10 ⁰	296.5 9 ⁰ 6 ²	299.3 11 ² 3 ²
302.3 3 ² 10 ⁰	302.0 3 ⁵ 5 ²	300.6 4 ² 2 ²
305.1 9 ⁶ 9 ²	305.3 9 [±] 2 ²	306.0 8 ² 15 ²
311.6 3 ¹ 10 ⁰	311.5 3 ² 1 ²	311.9 2 ² 15 ²

+	T	-	Elev
T.P. & B.M. #105	314.67 ⁶	0.771	313.905 313.897 - Record Elev.
	12.121		326.018 ²⁹
924+00		8.3	317.7
925+00		1.1	324.9
T.P.		0.214	325.804
	9.044		334.868
926+00		5.7	329.2
926+292	BC	5.0	329.9
926+542		4.3	330.6
926+792		3.9	331.0
927+042		3.6	331.3
927+292		4.4	330.5
7542		5.1	329.8

#105
B.M. #97C 12' 872.923 + 30 Record Elev. 313.897.

318.0	318.0
318.0	8.0
8.0	15.0
70.0	
323.9	324.7
2.1	1.0
70.0	15.0
329.1	329.6
5.8	5.3
10.0	15.0
329.8	330.5
5.1	4.0
10.0	3.0
	15.0
330.3	331.3
4.6	3.6
10.0	2.5
	15.0
330.8	331.6
4.1	3.2
10.0	2.5
	15.0
330.6	331.6
4.3	3.2
10.0	15.0
329.7	331.3
5.2	3.6
10.0	3.5
	15.0
329.0	330.6
5.2	4.3
10.0	2.5
	15.0
	330.3
	4.6
	15.0

	+	π	-	Elev
		334.868		
+79.2			5.9	329.0 ✓
928 + 0A.2			5.9	328.0 ✓
+29.2			7.8	327.1 ✓
+54.2			8.7	326.2 ✓
+79.2			9.5	325.4 ✓
+89.23 E.C.			9.6	325.3 ✓
T.P.			5.361	329.507 ✓
	1.147	330.654 ✓		

T.P. + B.M. #106 11.689 318.965
318.971 - Recor'd Elev.

327.7 ✓
 $\begin{array}{r} 73 \\ 102 \\ \hline 326.8 \end{array}$ ✓
 $\begin{array}{r} 225.8 \\ 81 \\ 102 \\ \hline 325.0 \end{array}$ ✓
 $\begin{array}{r} 325.0 \\ 91 \\ 102 \\ \hline 324.2 \end{array}$ ✓
 $\begin{array}{r} 324.2 \\ 107 \\ 102 \\ \hline 323.8 \end{array}$ ✓
 $\begin{array}{r} 323.8 \\ 111 \\ 102 \\ \hline 322.8 \end{array}$ ✓
 330.1 ✓
 $\begin{array}{r} 48 \\ 28 \\ \hline 229.0 \end{array}$ ✓
 $\begin{array}{r} 229.0 \\ 81 \\ 102 \\ \hline 327.8 \end{array}$ ✓
 $\begin{array}{r} 327.8 \\ 91 \\ 102 \\ \hline 326.7 \end{array}$ ✓
 $\begin{array}{r} 326.7 \\ 102 \\ 102 \\ \hline 324.2 \end{array}$ ✓
 $\begin{array}{r} 324.2 \\ 107 \\ 102 \\ \hline 323.8 \end{array}$ ✓
 $\begin{array}{r} 323.8 \\ 111 \\ 102 \\ \hline 322.8 \end{array}$ ✓
 229.1 ✓
 $\begin{array}{r} 229.1 \\ 81 \\ 102 \\ \hline 327.8 \end{array}$ ✓
 $\begin{array}{r} 327.8 \\ 91 \\ 102 \\ \hline 326.7 \end{array}$ ✓
 $\begin{array}{r} 326.7 \\ 102 \\ 102 \\ \hline 324.2 \end{array}$ ✓
 $\begin{array}{r} 324.2 \\ 107 \\ 102 \\ \hline 323.8 \end{array}$ ✓
 $\begin{array}{r} 323.8 \\ 111 \\ 102 \\ \hline 322.8 \end{array}$ ✓
 228.5 ✓
 $\begin{array}{r} 228.5 \\ 81 \\ 102 \\ \hline 327.5 \end{array}$ ✓
 $\begin{array}{r} 327.5 \\ 91 \\ 102 \\ \hline 326.5 \end{array}$ ✓
 $\begin{array}{r} 326.5 \\ 102 \\ 102 \\ \hline 324.2 \end{array}$ ✓
 $\begin{array}{r} 324.2 \\ 107 \\ 102 \\ \hline 323.8 \end{array}$ ✓
 $\begin{array}{r} 323.8 \\ 111 \\ 102 \\ \hline 322.8 \end{array}$ ✓
 225.4 ✓
 $\begin{array}{r} 225.4 \\ 81 \\ 102 \\ \hline 325.2 \end{array}$ ✓
 $\begin{array}{r} 325.2 \\ 91 \\ 102 \\ \hline 324.2 \end{array}$ ✓
 $\begin{array}{r} 324.2 \\ 107 \\ 102 \\ \hline 323.8 \end{array}$ ✓
 $\begin{array}{r} 323.8 \\ 111 \\ 102 \\ \hline 322.8 \end{array}$ ✓

B.M. #106 Recor'd Elev. 318.971

B.M. #106

9.60

328.570

3.9

324.7

929+00

930+00

8.1

320.5

+07⁶⁶

8.9

319.7

+32^L

10.2

318.4

+57^L

11.3

317.3

B.M. #106

2.309

321.280

5.2

316.1

930+82^L

931+05

12" Concrete
Flow line Culvert

7.9

313.4

+06^B

6.7

314.6

932+00

9.7

311.6

10.681

310.599

1.464

312.063

933+00

5.4

306.7

May 12. Noon
and
Return May 14.

Elev. Elev. B.M.

318.971

318.971

313.1

314.6

311.6

310.599

306.7

306.7

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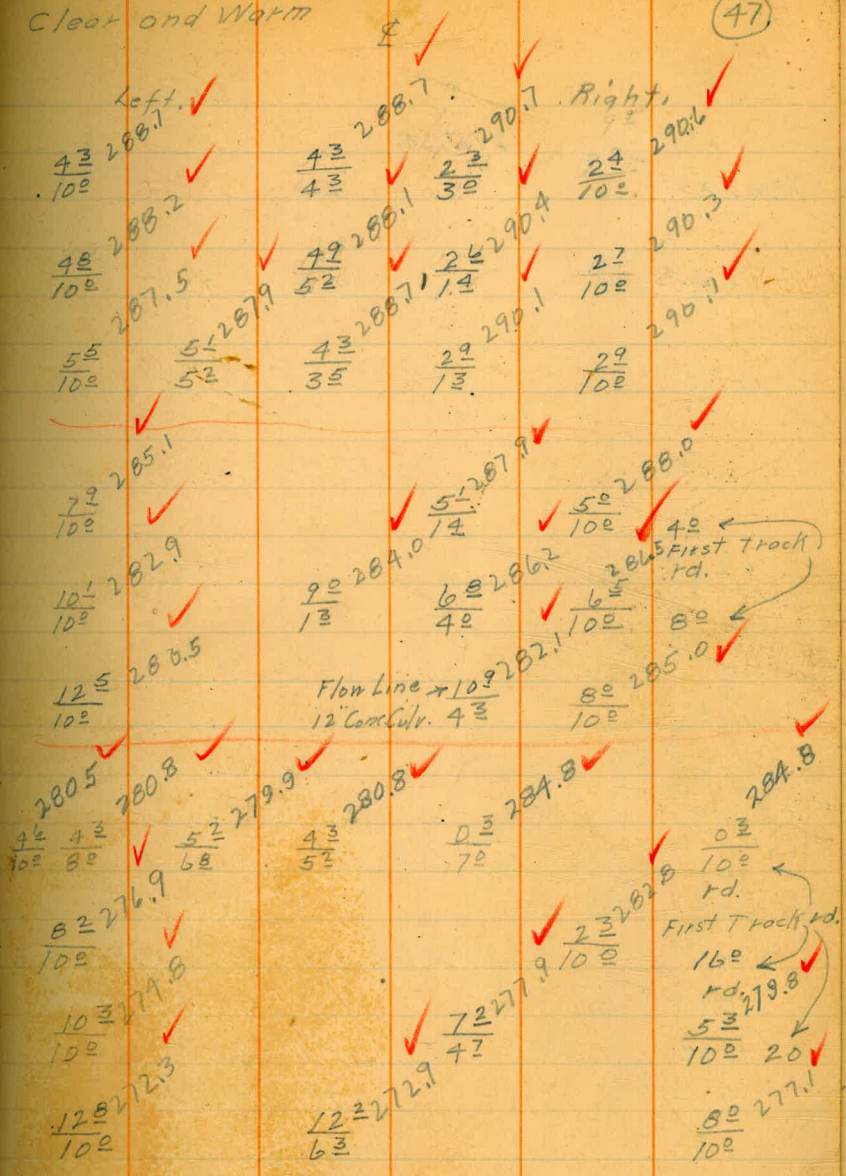
May 14.

Leach Note
Duermit
Webb Rod
Claremont Rd.

Clear and Warm

(47)

	+	π	-	Elev.	Elev. B.M.
		292.979			
936+935			3.0	299.9 290.0	
9 +96.84			3.3	289.7	
937+00		291.221	3.3	289.7	
B.M. #77E #107			2.342	290.637	290.648
	2.342	292.990			
+30.89			5.7	287.3 286.3	
+55.9			8.4	284.6	
+78			11.3	281.7	
T.P.			11.18	281.872	
	3.218	285.090			
937+80.2			3.1	282.0	
938+05.2			6.1	279.0	
+30.9			8.3	276.8	
+55.9			10.3	274.8	
T.P. Stake			11.370	273.720	
	1.524	275.244			



	+	T	-	Elev.
		275.241		
938+809			3.8	271.4 ✓
+82 ⁵⁶			4.2	271.0 ✓
939+00			5.2	270.0 ✓
+01 ⁸⁸			5.4	269.8 ✓
+269			7.4	267.8 ✓
+519			9.0	266.2 ✓
+769			11.2	264.0 ✓
Sta 939+769 T.P. Stake			10.845	264.399 ✓
	1.16	sub set up		265.56 ✓
940+019 175			7.3	258.3 ✓
		First Bank of dry wash		
+07.6			8.2 ←	257.4 ✓
+149		Center of dry wash	9.7	255.9 ✓
+19.4			9.0 ←	256.6 ✓
		Bank of dry wash		
+269			6.4	259.2 ✓
+4563			2.5	263.1 ✓

Left
42270.5 ✓
100
48 270.4 ✓
100
64 268.8 ✓
100
65 268.7 ✓
100
82 266.5 ✓
100
110 264.2 ✓
100
140 261.2 ✓
100
79 257.7 ✓
100
93 256.3 ✓
100
72 258.4 ✓
100
50 260.6 ✓
100
12 263.7 ✓
100
88 258.8 ✓
100
77 257.9 ✓
100
55 260.1 ✓
100

Right
20 273.2 ✓
100
21 273.1 ✓
100
34 271.8 ✓
100
32 271.5 ✓
100
59 269.3 ✓
100
73 267.9 ✓
100
103 265.0 ✓
100
69 258.7 ✓
100
71 258.5 ✓
100
95 256.1 ✓
100
68 258.8 ✓
100
80 257.6 ✓
100
37 256.7 ✓
100
94 256.2 ✓
100
37 261.9 ✓
100

	+	π	-	Elev.
T.P. Sta 939+76.9				264.399
	10.344	274.743		
941+00			7.2	267.5
T.P. Rock			2.857	271.886
	10.948	282.834		
941+95.82			7.1	275.7
942+00			6.7	276.1
+20.8			4.7	278.1
B.M. #977 #108			4.982	277.852 277.873
	10.957	288.830		
+45.8			8.0	286.8
+70.8			5.6	283.2
+95.8			2.7	286.1
T.P.			0.902	287.928
	11.425	299.353		
943+20.8			11.1	288.3
+45.8			8.3	291.1
+70.8			4.9	294.5

Left	Right
$\frac{7.2}{10.0} 267.5$	$\frac{8.2}{10.0} 266.8$
$\frac{5.5}{10.0} 277.3$	$\frac{275.1}{7.7} 10.0$
$\frac{277.6}{5.2} 10.0$	$\frac{277.3}{7.4} 10.0$
$\frac{279.3}{3.5} 10.0$	$\frac{274.9}{4.0} 8.3$
$\frac{282.0}{6.8} 10.0$	$\frac{279.7}{9.1} 10.0$
$\frac{284.1}{7.2} 10.0$	$\frac{282.1}{6.1} 10.0$
$\frac{286.8}{2.0} 10.0$	$\frac{285.0}{3.2} 10.0$
$\frac{289.8}{9.0} 10.0$	$\frac{287.4}{11.8} 10.0$
$\frac{291.7}{5.2} 10.0$	$\frac{290.7}{8.2} 10.0$
$\frac{297.0}{2.1} 10.0$	$\frac{293.5}{5.2} 10.0$
$\frac{289.0}{10.0} 10.0$	
$\frac{291.7}{7.2} 4.0$	
$\frac{296.2}{3.2} 5.0$	

Center of abandoned Road.

+ π - Elev

943 + 90⁰⁰ 299.353
10.837 309.427
2.6 296.8 ✓
0.763 298.590 ✓

944 + 00 11.4 298.0 ✓

945 + 00 3.2 306.2 ✓

T.P 0.575 308.852 ✓
4.449 313.301 ✓

39⁰⁰ 4.3 309.0 ✓

946 + 00 0.9 312.9 ✓

+ 21⁰⁰ 1.8 311.5 ✓

+ 93⁰⁰ 6.5 306.8 ✓

947 + 00 7.1 306.2 ✓

Left
299.0 ✓
 $\frac{0.0}{10^0}$

299.7 ✓
 $\frac{9.2}{10^0}$

300.0 ✓
 $\frac{1.0}{10^0}$

299.2 ✓
 $\frac{10.2}{4^0}$

301.2 ✓
 $\frac{2.2}{6^0}$

310.4 ✓
 $\frac{2.0}{10^0}$

312.5 ✓
 $\frac{0.2}{10^0}$

311.5 ✓
 $\frac{0.0}{10^0}$

306.5 ✓
 $\frac{6.0}{10^0}$

306.0 ✓
 $\frac{7.3}{10^0}$

309.4 ✓
 $\frac{3.2}{3.2}$

Right
296.1 ✓
 $\frac{3.3}{3^0}$

Right
296.0 ✓
 $\frac{3.4}{10^0}$

~~296.7~~

~~297.7~~

306.2 ✓
 $\frac{3.2}{10^0}$

~~309.6~~

~~309.6~~

312.5 ✓
 $\frac{0.0}{10^0}$

312.1 ✓
 $\frac{1.2}{10^0}$

307.4 ✓
 $\frac{5.2}{10^0}$

306.8 ✓
 $\frac{6.5}{10^0}$

May 15 -

Dvermitt
Webb
Clovert

(51)

	+	∇	-	Elev	Elev. B.M.
		313.301			
T.P.			11.600	301.701	
Stake T.P. 947+56 May 15.	0.888	302.589			
947+56			0.9	301.7	
948+00			5.3	297.3	
Stake T.P. 948+55	0.634	292.773	10.450	292.139	
949+00			4.8	288.0	
+40 ²			6.6	286.2	First Bank of Dry Wash
+49 ³			9.6	283.2	∅ of Dry Wash
+64 ³			7.7	285.1	2 nd Bank of Dry Wash
950+00			6.8	286.0	
951+00			5.5	287.3	
952+00			1.9	290.9	
Stake T.P. 952+15	11.251	303.074	0.950	291.823	

Left	Right
301.5 $\frac{1.2}{10^{\circ}}$	301.8 $\frac{0.8}{10^{\circ}}$
297.0 $\frac{5.2}{10^{\circ}}$	297.5 $\frac{5.2}{10^{\circ}}$
288.4 $\frac{4.2}{10^{\circ}}$	287.7 $\frac{5.1}{10^{\circ}}$
286.5 $\frac{6.2}{10^{\circ}}$	286.8 $\frac{6.2}{8^{\circ}}$
284.4 $\frac{8.2}{10^{\circ}}$	285.8 $\frac{7.2}{10^{\circ}}$
287.0 $\frac{5.2}{10^{\circ}}$	284.9 $\frac{7.2}{10^{\circ}}$
288.3 $\frac{4.2}{10^{\circ}}$	285.2 $\frac{7.2}{10^{\circ}}$
291.2 $\frac{1.2}{10^{\circ}}$	286.1 $\frac{6.2}{10^{\circ}}$
	289.6 $\frac{3.2}{10^{\circ}}$

Centre of old road
7°

Center of abandoned road
13°

	+	7	-	Elev.	Elev. B.M.
		303.074			
952+53 ³³			10.0	293.1	
+78 ³			8.8	294.3	
953+03 ³			7.6	295.5	
+28 ³			6.6	296.5	
+53 ³			5.6	297.5	
+78 ³			4.9	298.2	
+98 ³³			4.4	298.7	
954+00			4.2	298.9	
Stake T.P. → +70			2.111	300.963	
		10.062		311.025	
+72			10.1	300.9	
955+00			12.4	298.6	

Left	Right
95293.5 $\frac{95}{100}$	291.8 $\frac{110}{100}$
85 294.6 $\frac{85}{100}$	292.9 $\frac{100}{100}$
73 295.8 $\frac{73}{100}$	294.1 $\frac{90}{100}$
297.1 $\frac{60}{100}$	295.0 $\frac{80}{100}$
298.2 $\frac{40}{100}$	296.5 $\frac{60}{50}$
299.0 $\frac{40}{100}$	295.8 $\frac{70}{100}$
299.4 $\frac{30}{100}$	296.4 $\frac{60}{100}$
299.5 $\frac{30}{100}$	297.0 $\frac{60}{100}$
299.5 $\frac{30}{100}$	296.9 $\frac{60}{100}$
303.8 $\frac{70}{100}$	300.0 $\frac{110}{50}$
302.4 $\frac{80}{100}$	297.0 $\frac{140}{30}$
	295.6 $\frac{150}{100}$

296.5
 $\frac{60}{50}$

297.9
 $\frac{50}{80}$

299.5
 $\frac{30}{40}$

299.6
 $\frac{30}{40}$

± of old road

Leach Notes
Duer m. H. T.
Barley - R. S.
clover

May 17

Clear and Warm -

+ π - Elev.

955+30 311.025 14.7 296.3

+40 14.5 296.5

+44² 13.2 297.6

+69² 10.4 300.6

956+00 3.0 306.0

B.M. # 110 3.252 307.773 307.689

1.263 309.762

T.P. 10.876 320.638

May 17 1.039 319.599

11.555 331.154

957+00 5.7 325.5

+30 T.P. .810 330.344

11.174 341.518

957+49 7.4 334.1

+78²² 4.5 337.0

Stake. T.P. +98² .882 340.636

10.844 351.480

B.M. # 111 3.580 347.900 347.834

3' from left 354.683

edge road. 6.849 354.749

Left

10² / 10² 300.1

10² 2300.1 / 10² 300.0

11² / 10² 13² / 7² 13² 297.5 / 3²

299.1 / 11² / 10²

306.1 / 4² / 10²

323.9 / 7² / 10²

331.9 / 9² / 10²

335.0 / 6² / 10²

±

14² 296.9 / 1.0

13² / 2² 13² 297.7

14² 296.7 / 1²

14² 296.7 / 1²

14² 296.7 / 1²

336.3 / 5² / 5²

Right

13² 297.7 / 10²

12² / 10² 12² 298.11

12² / 10² 12² 298.11

302.3 / 8² / 10²

310.6 / 0.2 / 10²

326.5 / 4² / 10²

335.1 / 6² / 10²

339.3 / 2² / 10²

+	T	-	Elev.
	354.683		
	354.749		
950+00		14.7	390.0
959+00		5.0	349.7
T.P. + 90		0.809	353.874
	365.821		
	315.887		
11.947			
960+00		7.6	358.2
		.732	365.089
	375.994		
	376.060		
10.905			
+77		10.0	366.0
961+00		7.7	368.3
T.P.		.826	375.168
	386.712		
	386.778		
11.544			
+82		11.0	375.7
+91.2	small wash	14.9	371.8
962+00		11.9	374.8
+046		11.8	374.9
+11		8.6	378.1
+260		7.1	379.6

Left	Right
338.1	341.9
338.1	341.9
$\frac{16.6}{100}$	$\frac{12.8}{100}$
347.1	352.2
$\frac{7.6}{100}$	$\frac{2.5}{100}$
348.8	
$\frac{5.9}{64}$	
356.0	360.1
$\frac{9.8}{100}$	$\frac{5.6}{100}$
364.6	367.8
$\frac{11.2}{100}$	$\frac{8.2}{70}$
366.7	368.6
$\frac{9.3}{100}$	$\frac{8.0}{100}$
369.9	369.4
$\frac{16.8}{70}$	$\frac{6.6}{100}$
370.3	376.8
$\frac{16.4}{100}$	$\frac{9.2}{100}$
375.6	377.4
$\frac{11.1}{100}$	$\frac{9.3}{100}$
376.6	377.3
$\frac{10.1}{100}$	$\frac{9.4}{70}$
377.4	377.3
$\frac{9.3}{61}$	$\frac{9.4}{100}$
376.0	378.0
$\frac{10.2}{100}$	$\frac{8.2}{68}$
375.1	378.3
$\frac{11.6}{100}$	$\frac{8.4}{100}$
377.0	378.9
$\frac{9.2}{100}$	$\frac{7.8}{100}$
376.2	379.1
$\frac{10.5}{40}$	$\frac{7.6}{100}$
377.3	
$\frac{9.4}{70}$	
374.2	
$\frac{12.5}{15}$	
377.7	
$\frac{9.4}{25}$	
374.6	
$\frac{12.1}{10}$	
375.8	
$\frac{10.9}{50}$	
379.9	
$\frac{6.8}{50}$	
376.2	
$\frac{10.5}{80}$	
378.1	
$\frac{8.6}{75}$	

	T	-	Elev.	Recorded B.M. Elev.
	386.712			
	386.778			
962+345		8.0	378.7	
+40		5.6	381.1	
B.M.# 112		3.081	383.631	Recorded. 383.643
	11.254		394.897	
962+96 ^{1/2}		8.1	386.8	
963+21 ^{1/2}		5.2	389.7	
+46 ^{1/2}		1.3	393.6	
		.679	394.218	
T.P	10.083		404.301	
+71 ^{1/2}		9.1	395.2	
+96 ^{1/2}		5.4	398.9	
964+21 ^{1/2}		4.0	400.3	
+46 ^{1/2}		3.5	406.8	
+71 ^{1/2}		3.8	400.5	
+96 ^{1/2}		3.6	400.7	

Left	Right
380.0 $\frac{62}{100}$	380.1 $\frac{62}{100}$
380.8 $\frac{59}{100}$	380.9 $\frac{58}{100}$
387.7 $\frac{72}{100}$	387.0 $\frac{72}{100}$
390.6 $\frac{43}{100}$	389.7 $\frac{52}{100}$
393.6 $\frac{13}{100}$	393.0 $\frac{19}{100}$
395.5 $\frac{88}{100}$	395.7 $\frac{86}{100}$
398.8 $\frac{55}{100}$	397.8 $\frac{65}{100}$
400.3 $\frac{40}{100}$	400.5 $\frac{38}{100}$
400.8 $\frac{35}{100}$	400.5 $\frac{38}{100}$
401.0 $\frac{32}{100}$	400.9 $\frac{34}{100}$
400.5 $\frac{39}{100}$	399.8 $\frac{45}{100}$
400.4	

May 18

Leach-1150
Duermit
Clavert
Bailey

Cool and Hazy

(56)

+ π - Elev.

404.301 ✓

965 + 21¹

3.2 401.1 ✓

+ 32⁸

3.0 401.3 ✓

B.M. # 112A

9.220 ~~395.081~~ 395.074 ✓

9.220 404.294 ✓

1.063 403.231 ✓

11.518 414.799 ✓

966 + 00

10.2 404.5 ✓

+ 30

7.8 406.9 ✓

+ 48

7.4 407.3 ✓

967 + 00

4.0 410.7 ✓

B.M. on rock.
May 18

9.535 405.214 405.190 ✓

9.550 414.740 ✓

967 + 54¹³

3.3 411.4 ✓

+ 79¹

2.7 412.0 ✓

968 + 04¹

4.0 410.7 ✓

+ 15⁶³

4.0 410.7 ✓

Left

400.5 ✓
 $\frac{38}{100}$

402.7 ✓
 $\frac{21}{100}$

405.1 ✓
 $\frac{96}{100}$

407.8 ✓
 $\frac{62}{100}$

408.3 ✓
 $\frac{64}{100}$

411.3 ✓
 $\frac{34}{100}$

412.0 ✓
 $\frac{27}{100}$

412.0 ✓
 $\frac{27}{100}$

411.7 ✓
 $\frac{35}{100}$

410.9 ✓
 $\frac{38}{100}$

Right

400.6 ✓
 $\frac{38}{100}$

400.6 ✓
 $\frac{32}{100}$

403.9 ✓
 $\frac{102}{100}$

405.3 ✓
 $\frac{94}{100}$

406.7 ✓
 $\frac{85}{100}$

409.6 ✓
 $\frac{51}{100}$

410.7 ✓
 $\frac{42}{100}$

411.5 ✓
 $\frac{32}{100}$

410.5 ✓
 $\frac{42}{100}$

410.0 ✓
 $\frac{47}{100}$

	+	T	-	Elev.
		414.740		
969+00			11.0	403.7
B.M. # 114 on rock				405.190 405.190
	.793	405.983		
970+00			12.2	392.8
970+00 T.P. rock			11.757	399.226
	1.038	395.264		
B.M. # 115			9.290	385.974 385.983
	9.290	395.273		
970+65 T.P. Lath			11.856	383.417
	7.46	390.88 391.88		
970+51			4.5	386.4
970+65 T.P. Lath				383.417
	1.020	384.437		
970+66			1.8	382.6
971+00			6.1	378.3
+30			12.0	372.4
T.P.			11.680	372.757
	1.100	373.857		
+78			14.8	359.0
+87			16.2	357.7

Left	Right
404.1 $\frac{10.6}{10.2}$	403.9 $\frac{10.8}{10.2}$
B.M. 30 Left 969+00	
393.7 $\frac{12.3}{10.2}$	394.6 $\frac{11.4}{10.2}$
B.M. # C.L. 15 R 970+60	
386.2 $\frac{4.7}{10.2}$	386.3 $\frac{4.6}{10}$
383.0 $\frac{14}{10.2}$	381.6 $\frac{2.8}{10.2}$
377.9 $\frac{6.5}{10.2}$	377.8 $\frac{6.6}{10.2}$
372.0 $\frac{12.4}{10.2}$	372.3 $\frac{12.1}{10.2}$
363.3 $\frac{10.6}{10.2}$	360.3 $\frac{13.6}{13}$
361.6 $\frac{12.3}{10.2}$	360.1 $\frac{13.8}{12}$
359.8 $\frac{14.4}{10.2}$	360.3 $\frac{13.6}{6.2}$
	360.2 $\frac{13.7}{10.2}$
	361.0 $\frac{12.9}{10.2}$

	+	T	-	Elev
		373.857		✓
971+92			12.6	361.3 ✓
972+00			9.9	364.5 ✓
BM # DL #116			10.045	363.812 ✓
	10.045	373.867		✓
			0.569	373.298 ✓
	11.440	384.738		✓
972+40			10.5	374.2 ✓
973+00			6.4	378.3 ✓
T.P			0.591	384.147 ✓
	11.514	395.661		✓
974+00			7.4	388.3 ✓
+6691			4.2	391.5 ✓
975+00			4.3	391.4 ✓
976+00			3.3	392.7 ✓
T.P			4.465	391.196 ✓
	4.634	395.830		✓
977+00			3.8	392.0 ✓
+8842			6.0	389.8 ✓

Left ✓

$$\begin{array}{r} 360.5 \\ \underline{134} \\ 108 \end{array}$$

$$\begin{array}{r} 360.7 \\ \underline{137} \\ 81 \end{array}$$

$$\begin{array}{r} 363.2 \\ \underline{107} \\ 108 \end{array}$$

Right ✓

$$\begin{array}{r} 361.8 \\ \underline{121} \\ 108 \end{array}$$

$$\begin{array}{r} 365.8 \\ \underline{81} \\ 108 \end{array}$$

28' R Sta. 972+00

374.8 ✓

$$\begin{array}{r} 374.8 \\ \underline{99} \\ 108 \end{array}$$

$$\begin{array}{r} 379.0 \\ \underline{52} \\ 108 \end{array}$$

374.7 ✓

$$\begin{array}{r} 374.7 \\ \underline{108} \\ 108 \end{array}$$

$$\begin{array}{r} 378.0 \\ \underline{62} \\ 108 \end{array}$$

389.6 ✓

$$\begin{array}{r} 389.6 \\ \underline{61} \\ 108 \end{array}$$

387.5 ✓

$$\begin{array}{r} 387.5 \\ \underline{82} \\ 108 \end{array}$$

392.9 ✓

$$\begin{array}{r} 392.9 \\ \underline{28} \\ 108 \end{array}$$

390.5 ✓

$$\begin{array}{r} 390.5 \\ \underline{52} \\ 108 \end{array}$$

392.3 ✓

$$\begin{array}{r} 392.3 \\ \underline{32} \\ 108 \end{array}$$

390.6 ✓

$$\begin{array}{r} 390.6 \\ \underline{51} \\ 108 \end{array}$$

392.9 ✓

$$\begin{array}{r} 392.9 \\ \underline{28} \\ 108 \end{array}$$

391.5 ✓

$$\begin{array}{r} 391.5 \\ \underline{42} \\ 108 \end{array}$$

391.4 ✓

$$\begin{array}{r} 391.4 \\ \underline{44} \\ 108 \end{array}$$

392.6 ✓

$$\begin{array}{r} 392.6 \\ \underline{32} \\ 108 \end{array}$$

390.6 ✓

$$\begin{array}{r} 390.6 \\ \underline{52} \\ 108 \end{array}$$

389.1 ✓

$$\begin{array}{r} 389.1 \\ \underline{62} \\ 108 \end{array}$$

	+	π	-	Elev.
		395.830		
978	+13.4		6.3	389.5
	+38.4		6.7	389.1
	+63.4		6.9	388.9
	+88.4		7.2	388.6
979	+13.4		6.5	389.3
	+38.4		6.7	389.1
	+63.4		8.9	386.9
	+88.4		11.9	383.9
T.P.		11.842		383.988
		1.275		385.283
980	+13.4		4.0	381.3
	+35.25		7.7	377.6
BM #	118		4.352	380.931
				380.956
		4.352		385.302
			11.229	374.073

Left	Right
390.1 <u>52</u> 100	389.0 <u>68</u> 100
389.9 <u>52</u> 100	388.4 <u>74</u> 100
389.6 <u>62</u> 100	388.3 <u>75</u> 100
389.6 <u>62</u> 100	387.7 <u>81</u> 100
390.2 <u>52</u> 100	388.1 <u>72</u> 100
389.3 <u>65</u> 100	388.4 <u>74</u> 100
387.0 <u>88</u> 100	386.6 <u>92</u> 100
383.4 <u>124</u> 100	384.5 <u>113</u> 100
380.6 <u>42</u> 100	381.7 <u>36</u> 100
377.3 <u>82</u> 100	378.1 <u>72</u> 100
B.M. # F.L. 17' L 980+13.4	

	+	∓	-	Elev.
				374.073 ✓
981+00	1.517	375.590	4.1	371.5 ✓
			11.736	363.854 ✓
982+00	0.929	364.783	3.9	360.9 ✓
			11.686	353.097 ✓
983+00	0.694	353.791	5.7	348.1 ✓
984+00			12.3	341.5 ✓
			11.584	342.207 ✓
+20	0.841	343.048	1.9	341.1 ✓
+58			4.7	338.3 ✓
985+00			6.2	336.8 ✓
986+00			11.6	331.4 ✓
987+00			9.8	333.2 ✓
B.M.#114			9.588	333.460 ✓
	0.853	334.219		333.366 ✓

Left	Right
371.3 ✓ $\frac{4.3}{10^2}$	371.7 ✓ $\frac{3.9}{10^2}$
361.1 ✓ $\frac{3.7}{10^2}$	361.2 ✓ $\frac{3.6}{10^2}$
347.6 ✓ $\frac{6.2}{10^2}$	348.4 ✓ $\frac{5.4}{10^2}$
340.8 ✓ $\frac{13.0}{10^2}$	342.9 ✓ $\frac{10.2}{10^2}$
339.7 ✓ $\frac{3.3}{10^2}$	342.3 ✓ $\frac{0.2}{10^2}$
337.8 ✓ $\frac{5.2}{10^2}$	338.9 ✓ $\frac{4.1}{10^2}$
336.2 ✓ $\frac{6.8}{10^2}$	337.1 ✓ $\frac{5.9}{10^2}$
331.9 ✓ $\frac{12.1}{10^2}$	332.0 ✓ $\frac{11.0}{10^2}$
332.2 ✓ $\frac{10.8}{10^2}$	331.2 ✓ $\frac{8.8}{10^2}$
B.M.#114	5'R 986+90

	+	π	-	Elev.
987+17 ⁰⁵		334.219	1.3	332.9
+66			7.4	326.8
T.P.			11.836	322.383
	.508	322.891		
988+00			5.2	317.7
T.P.			11.374	311.517
	1.198	312.715		
			11.128	301.587
	1.304	302.891		
+62			4.7	298.12
B.M. #122			6.675	296.216
				296.233
	"A" 3.125	299.358		
	6.675	302.908		
	"A"	11.843		287.515
Stake T.P.			11.493	291.915
	"A" 0.827	288.342		
	0.660	292.075		
988+90			5.2	286.9
989+00			7.7	284.4
+16			12.0	280.1
	"A"	7.793		280.529
		11.513		280.562
	"A" 1.033	281.582		
	1.207	281.769		
	"A"	11.510		270.072
		11.681		270.088

Left.	Right.
331.5 $\frac{27}{100}$	333.7 $\frac{02}{100}$
325.4 $\frac{88}{100}$	327.8 $\frac{64}{100}$
316.4 $\frac{65}{100}$	319.0 $\frac{32}{100}$
296.6 $\frac{63}{100}$	299.0 $\frac{32}{100}$
B.M. #114 R	26' R 987+77
283.9 $\frac{82}{100}$	289.7 $\frac{24}{100}$
281.8 $\frac{103}{100}$	287.0 $\frac{51}{100}$
277.9 $\frac{142}{100}$	281.5 $\frac{106}{100}$

May 25, 1926
10 A.M.

Daermitt. T.
Clavert
Bailey
Cross-section

Note: All cross-sections to be
subtracted from H.I.
marked "A."

(62)

+ T - Elev.

"A" - 1.093 271.165
1.570 271.658

270.072 ✓
270.088

T.P.

11.452 260.206 ✓

.821 261.027

990+00

2.9 258.1

Stake TR "A" 7.080 261.280

10.965 260.200 ✓

+58

11.8 249.2

"A" 7.498 253.782 ✓

Record Elev. used

B.M. # 123

"A" - 0.842 254.651
7.236 261.045

7.236 253.791 253.809

T.P.

11.703 249.342 ✓

0.615 249.957

T.P.

"A" - 11.552 249.299 ✓
11.736 238.221 ✓

"A" - 1.262 244.561
1.075 239.296

991+00 ✓

2.2 237.1

"A" Stake T.P. 1.153 239.090

"A" 11.624 232.937 ✓

+46

11.9 227.4

+71 Center of dry
wash

13.7 225.6

+88.7 ✓

14.6 224.7

+90.7

12.4 226.9 ✓

Stake T.P. "A" - 11.424 244.573

"A" 0.941 233.149 ✓

992+00 ✓

10.4 228.9

Left

Right

151
100 255.8 ✓

102
100

260.3 ✓

68
100

247.9 ✓
(To be subtracted from)

48
100

249.9 ✓

Record Elev. used

B.M. # 114B

24' R 990+52

81
100

236.5 ✓

74
100

237.2 ✓

62
100

227.2

72
100

226.7

65
100

227.6

52
100

228.4

52
100

228.4

62
100

227.2

72
100

227.6

82
100

225.9

85
100

225.6

62
100

227.2

62
100

227.2

62
100

227.2

52
100

228.7

62
100

227.2

96
100

224.5

92
100

224.7

52
100

225.0

92
100

225.0

72
100

229.4

98
100

224.3

95
100

224.6

127
100

231.9

181
100

226.5 ✓

+ "A" $\frac{\pi}{244.573}$
239.296

992+16

6.9 232.4

0.877 238.119

10.588 249.007

993+00

9.2 239.8

0.803 243.770

Stake TR

"A" 9.568 253.328

+57.06

3.3 245.7

8.479 248.857

Record Elev. used. 244.803

B.M. #14 "A" 8.479 253.312

+82.1

2.4 246.16

994+07

2.5 246.5

+32.1

3.7 245.3

+41.39

3.0 246.10

995+00

10.6 238.4

996+00

8.5 240.15

T.P.

"A" 8.979 244.333

"A" 3.947 248.280
7.260 247.967

B.300 240.707

+47

8.2 239.8

+85

8.7 239.3

Left

Right

$\frac{106}{100}$ 239.0

$\frac{148}{100}$ 229.8

$\frac{18}{100}$ 242.8

$\frac{82}{100}$ 236.4

$\frac{72}{100}$ 248.8
Subtract from 253.312

$\frac{110}{100}$ 242.3

$\frac{29}{100}$ 250.4

$\frac{102}{100}$ 249.1

$\frac{26}{100}$ 250.7

$\frac{106}{100}$ 242.7

$\frac{46}{100}$ 248.7

$\frac{112}{100}$ 241.4

$\frac{45}{100}$ 248.8
 $\frac{56}{72}$ 247.7

$\frac{112}{100}$ 242.1

$\frac{82}{100}$ 245.1

$\frac{173}{42}$ 236.0
 $\frac{193}{100}$ 233.5

$\frac{88}{100}$ 244.5

$\frac{173}{100}$ 236.0

$\frac{40}{100}$ 243.8

$\frac{92}{40}$ 238.6
 $\frac{111}{65}$ 237.2
 $\frac{123}{100}$ 236.0

$\frac{48}{100}$ 243.5

$\frac{109}{26}$ 237.9
 $\frac{108}{42}$ 237.5
 $\frac{144}{100}$ 233.9

Party. - Cross-sections, No Profile

Dnermit, Notes
 Reynolds, T
 Clowry
 Anderson, R
 Seibel

Note, All Cross-sections to
 be taken from H.I.
 marked "A"

(64)

	+ "A"	-	Elev.
	$\frac{248.280}{297.967}$		
997+00		6.4	241.6 ✓✓
+30		6.4	241.6 ✓✓
Stake T.P.	"A" 8.480	8.480	239.800 ✓✓
+97		16.6	231.4 ✓✓
998+00		16.1	231.9 ✓✓
+30		10.7	237.3 ✓✓
998+46 ³		10.9	237.1 ✓✓
T.P.		11.348	236.619 ✓✓
	.518		237.137 ✓✓
999+00		4.2	232.9 ✓✓
+17 ⁸⁰		5.3	231.8 ✓✓
+42 ⁸		6.5	230.6 ✓✓
Stake T.P.	"A" 12.573	12.573	231.675 ✓✓
+67 ⁸		8.1	229.0 ✓✓
+92 ⁸		10.3	226.8 ✓✓
1000+17 ⁸		12.4	224.7 ✓✓

May. 26, 1926
 2:45 P.M.

Left

Right

$\frac{28}{100}$	245.5 ✓✓	$\frac{75}{22}$	240.8	$\frac{92}{60}$	238.0	$\frac{98}{74}$	236.8	$\frac{115}{100}$	236.8
$\frac{28}{100}$	245.5 ✓✓								
$\frac{28}{100}$	235.7 ✓✓								
$\frac{80}{100}$	236.4 ✓✓								
$\frac{78}{100}$	240.4 ✓✓								
$\frac{38}{100}$	239.8 ✓✓								
$\frac{42}{100}$	235.8 ✓✓								
$\frac{82}{100}$	234.4 ✓✓								
$\frac{98}{100}$	232.5 ✓✓								
$\frac{112}{100}$	230.5 ✓✓								
$\frac{38}{100}$	228.0 ✓✓								
$\frac{63}{100}$	225.7 ✓✓								
$\frac{86}{100}$									

238.4

228.0

£

+	π	-	Elev.	Left	Right
	237.137				

1000 + 428					
"A"	12.460	221.805	✓		
"A"	1.685	223.490	✓		
	1.809	227.828			
B.M. #126	4.940	218.550	✓		
#115	9.285	218.543			

B.M. #115-A	"A"	11.271	212.219	212.286
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Contd in Book #8 Page #1

+

π

-

Elev.

±

(66)

Left

Right

(67)

(68)

(69)

April 30

(70)

B.M ^s	Elev.	Location
# 85	333.103 ²	Tree 50' L 800+23
# 87	290.459	30' R 813+90 Hub in Post
# 88	299.412	30' L 823+40
# 90	319.418	Nail in Post 2' L 836+00
# 90 ¹ / ₂	269.615	Nail in Tree 15' R 845+00
# 90A	259.805	20' R 847+21 Rock in River Bed
# 92A	260.340	16' R 858+42 Point of Rock
# 93	257.891	7' R 863+18 Point of Rock
# 93A	251.270.	12' L 868+22 Point of Rock

281.515
269.615
119.00

+	T	-	Elev.
10.179	300.827		290.648
		1.700	
			299.127
9.582	308.709		
		.371	
			308.338
11.352	319.690		
		.650	
			319.040
			318.971
.651	319.622		
		11.347	
			308.275
1.197	309.472		
		10.431	
			299.041

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

IMPROVED TABLES

AND

INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connections.

Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

6432

2.710

1.384

0.202

0.181

1.051

0.214

5.341

3 09.145

0.771

3 08.374

3

4.737

490

416

331.082

11.689

319.393

343.048

8.022

335.026

324.926

.690

0.771

218.576

9.287

289

85

32

53

227.328

9.288

218.043

2.123

249.077

8.300

70

214.679

0.771

213.903

19
23

42

150
58

385.283

4352

380.731

399.04

318.971

.069

202.048

25

8.733

267.332

8.733

258.599

.138

290.780

990.698

.132

957.79

30

49

11.289

351.480

3.582

347.900

.839

.066

+46

25

71.7

90.7

330.65.4

11.689

318.965

100

113

88.7

100

93

90.7

4.354

223.490

218.576

4.914

223.490

4.940

218.550