

EL CAPITAN
Pipe Line Survey
Levels &
Cross Sections # 8

W198

MICROFILMED
JAN 21 1965

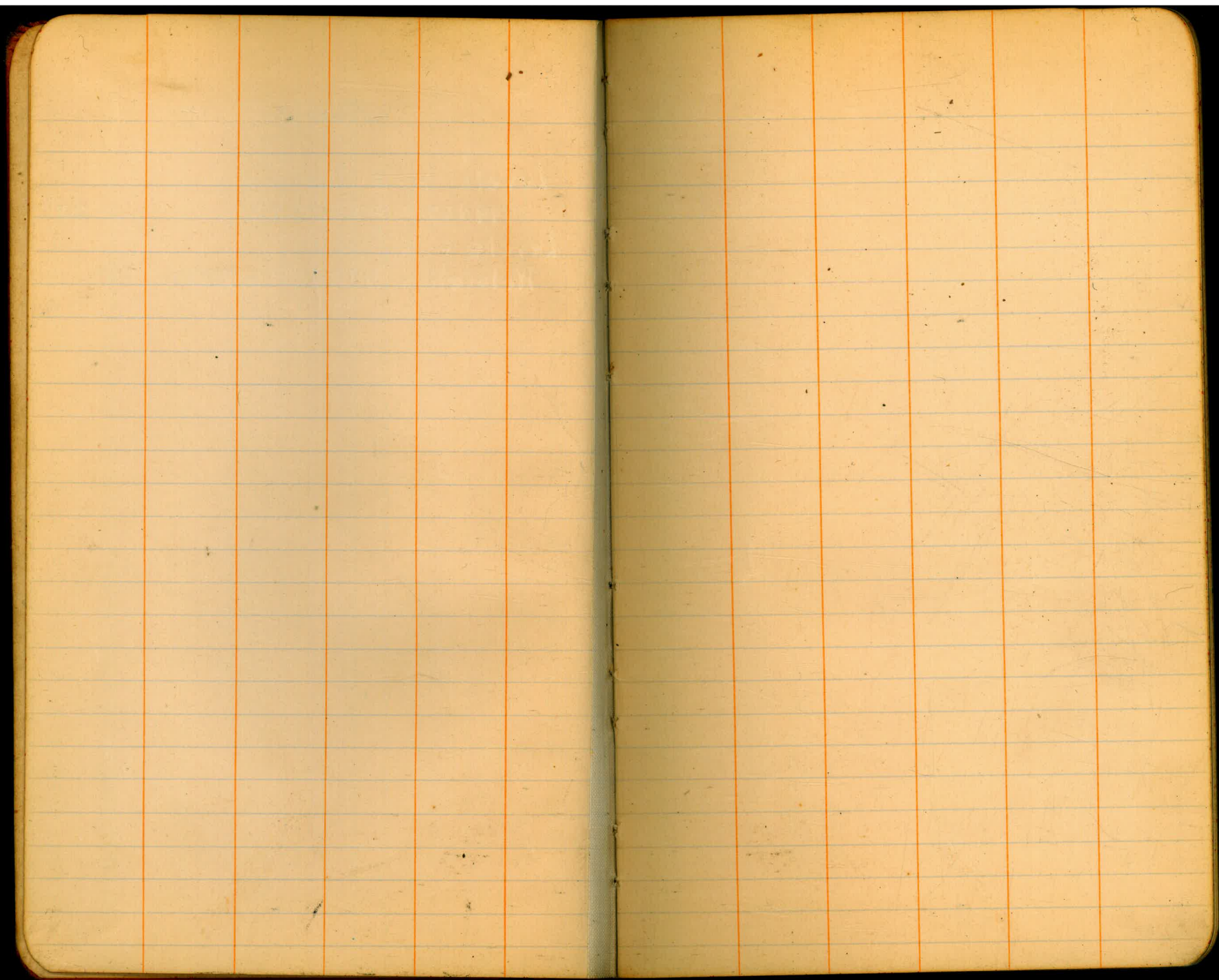
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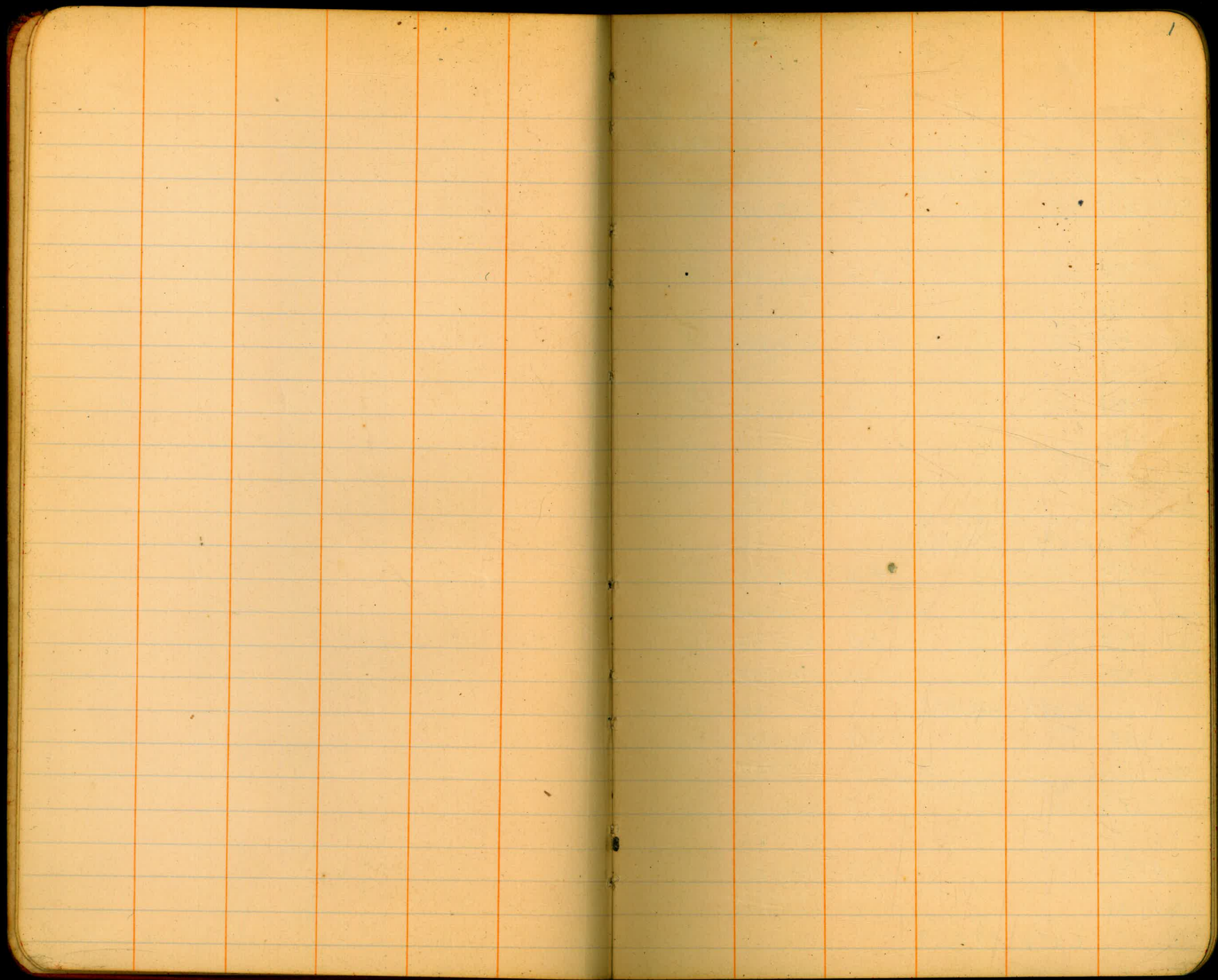
Index

Levels + X Sections
999+67^g - 1099+72^g 1-27

Levels + X Sections

Relocation 492+68^l - 789+00 28-





May 19, 1926

Profile

Dueymit. T
Bailey Rod
Clavert.

Note, All cross-sections to be subtracted from H.I. 2
marked "A"

May 27, 1926
Cross-Sections.

Dueymit. T
Bailey Rods.
Clavert.

	+	∓	-	Elev.	Elev. B.M.
BM. # 115					218.576
	12.493 "A"	231.067			
999+67 ^B	11.230	229.806	0.7	229.106	
+92 ^B			3.0	226.806	
1000+17 ^B			5.0	224.806	
+42 ^B			7.6	222.206	
+67 ^B			11.0	218.806	
Stake T.P.	0.941 "A"	219.509	11.236	218.570	
	0.990	219.560			
+92 ^B			4.6	215.0	
				214.960	
B.M. # 115-A			7.229	212.280	212.286
1001+17 ^B			8.8	210.8	
				210.760	
Stake T.P.			11.567	207.993	
	0.894	208.887			
+42 ^B			3.9	205.0	
				204.987	
Stake T.P.	0.582	208.392 "A"	11.699	207.810	
+67 ^B			8.8	200.1	
				200.087	
+87 ⁹²			12.3	196.6	
				196.587	
Stake T.P.	1.284	198.598	11.474	197.314	
	1.696	199.109			

Left:

290.2	$\frac{0^2}{10^2}$
228.0	$\frac{3^2}{10^2}$
225.9	$\frac{5^2}{10^2}$
222.8	$\frac{8^2}{10^2}$
219.2	$\frac{11^2}{10^2}$
215.8	$\frac{3^2}{10^2}$
211.7	$\frac{7^2}{10^2}$
206.2	$\frac{13^2}{10^2}$
202.8	$\frac{7^2}{10^2}$
197.5	$\frac{10^2}{10^2}$

Right:

228.1	$\frac{3^2}{10^2}$
226.0	$\frac{5^2}{10^2}$
223.9	$\frac{7^2}{10^2}$
221.6	$\frac{9^2}{10^2}$
218.5	$\frac{12^2}{10^2}$
214.4	$\frac{5^2}{10^2}$
209.9	$\frac{7^2}{10^2}$
203.9	$\frac{15^2}{10^2}$
199.0	$\frac{9^2}{10^2}$
196.1	$\frac{12^2}{10^2}$

	T	-	Elev.
McCarty's Stationing	198.598		187.200
	199.109	11.398	187.200
A" 5.824	193.024		
998 + 55		12.7	186.4
Stake T.P.		11.877	187.232
	11.163	198.395	
998 + 82°		14.0	184.4
	First Bank of Dry Wash		
+ 85°		15.4	183.0
+ 92°		18.1	180.3
	E of Dry Wash		
+ 94°		17.9	180.5
999 + 00		16.8	181.6
	Second Bank of Dry Wash		
+ 04°		14.7	183.7
+ 16°		14.3	184.1
Stake T.P.	A" 0.745	192.279	197.677
999 + 90°	12.676	204.955	0.718
	11.309	208.986	
1000 + 00		9.1	199.956
Stake T.P.	A" 0.832	204.123	208.390
1000 + 45°	12.864	216.987	0.596
	11.384	219.774	

Left

Right

6 ^z / _{10^c}	186.3	6 ^z / _{10^c}	186.3
7 ^z / _{10^c}	185.3	8 ^z / _{2^z}	184.2
8 ^z / _{10^c}	184.5	11 ^z / _{3^c}	181.3
10 ^z / _{10^c}	182.6	12 ^z / _{2^z}	180.9
10 ^z / _{10^c}	182.3	12 ^z / _{2^z}	180.9
12 ^z / _{10^c}	180.8	12 ^z / _{10^c}	180.9
11 ^z / _{10^c}	181.8	12 ^z / _{7^z}	180.1
10 ^z / _{10^c}	181.8	12 ^z / _{10^c}	180.9
12 ^z / _{10^c}	180.8	12 ^z / _{10^c}	180.9
11 ^z / _{10^c}	181.1	9 ^z / _{10^c}	183.8
11 ^z / _{10^c}	181.7	10 ^z / _{1^c}	183.8
5 ^z / _{10^c}	199.2	9 ^z / _{10^c}	184.0
		7 ^z / _{10^c}	200.2

	+	"A"	T	-	Elev.	Elev. B.M.
			216.987			
			219.774			
Stake T.P.	"A"	11.408	227.591	0.804	216.183	
		11.227	230.180	0.821	218.953	
1001+00			10.1		220.1	
Stake T.P.	"A"	12.957	239.657	0.891	226.700	
		11.847	241.273	0.754	229.426	
BM # 115 B			4.570		235.087	Record Elev. Used
T.P.	"A"	12.795	247.876	6.183	235.090	235.081
		11.617	246.698			
1002+00			9.2		237.5	
Stake T.P.	"A"	12.778	259.857	0.795	247.061	
		11.678	257.500	0.876	245.822	
P.L.I.			3.0		254.5	
1002+86 ⁹³	"A"	12.450	271.531	0.778	259.081	
"A - Stake T.P.			0.5		257.0	
1003+00			1.003		256.97	
Stake T.P.		11.470	267.967			
Stake T.P.		7.700	274.857	0.810	267.157	
1003+40 ⁹⁴			7.6		267.3	
Stake T.P.	"A"	12.474	283.132	0.873	270.658	
1004+00			2.4		272.5	

Left

Right

 $\frac{82}{100}$ $\frac{122}{100}$ $\frac{82}{100}$ $\frac{162}{100}$ $\frac{82}{100}$ $\frac{142}{100}$

218.8

235.2

251.2

254.8

263.3

268.2

 $\frac{62}{100}$ $\frac{81}{100}$ $\frac{23}{100}$ $\frac{112}{100}$ $\frac{02}{100}$ $\frac{72}{100}$

221.5

239.8

257.6

260.2

270.6

275.9

May 28, 1926. Duermitt T
 Webb }
 Clavert } Rds.
 Cross-sections

Note: All Cross-sections to be taken from 5
 H.L. marked "A"

	+	T	-	Elev.	Elev. B.M.
		283.132			
		274.857			
Stake T.P.			1.149	273.708	
	11.863	285.571			
1004 + 39 ^e			12.4	273.2	
	E of Dry Wash				
+ 80 ^e			8.7	276.91	
			0.669	282.463	
Stake T.P. - A	12.883	295.346			
1005 + 00			4.5	281.111	
Stake T.P.			0.810	284.760	
	11.663	296.423			
+ 39 ^e	E of Dry Wash		7.9	288.5	
			1.060	294.286	
Stake T.P.			0.610	295.813	
	A=12.524	306.810			
	11.735	307.548			
+ 82 ⁰⁰			6.9	300.6	
			0.842	305.968	
Stake T.P. A	12.368	318.336			
1006 + 07 ^e			0.9	306.6	
Stake T.P.			1.028	306.520	
	11.963	318.483			
+ 32 ^e			7.4	311.1	
			1.457	316.879	
Rock T.P. "A"	12.410	329.289			
+ 57 ^e			1.3	317.2	
Rock T.P.			1.580	316.903	
	10.938	327.841			

	Left	Right
	269.3	276.6
	$\frac{138}{100}$	$\frac{65}{100}$
	273.2	280.4
	$\frac{92}{100}$	$\frac{22}{100}$
	277.8	283.9
	$\frac{175}{100}$	$\frac{115}{100}$
	286.6	291.4
	$\frac{82}{100}$	$\frac{32}{100}$
	299.1	303.0
	$\frac{72}{100}$	$\frac{38}{100}$
	305.1	308.5
	$\frac{132}{100}$	$\frac{98}{100}$
	309.7	312.7
	$\frac{86}{100}$	$\frac{56}{100}$
	314.6	317.3
	$\frac{142}{100}$	$\frac{120}{100}$

May 28, 1926

	+	T	-	Elev.	Elev. B.M.
		327.289			
		327.841			
1006+82 ^e			0.4	327.4	
Stake T.P.		"A" 0.605		328.684	
		12.924	0.921	326.920	
		11.281		338.201	
1007+07 ^e			3.1	335.1	
Stake T.P.		"A" 2.838		338.720	
		8.666	0.625	337.576	
		9.364		346.940	
B.M. #116A		"A" 5.416		342.020	
T.P.		5.420	4.921	342.019	341.959
		7.415		349.374	
+32 ^e			11.4	338.0	
+57 ^e			9.5	339.9	
+82 ^e			8.4	341.0	
1008+07 ^e			6.9	342.5	
+32 ^e			5.5	343.9	
+57 ^e			3.6	345.8	
Stake T.P.		"A" 0.672		346.707	
+82 ^e		"A" 11.222		357.929	
Stake T.P.			0.9	348.5	
			0.549	348.825	

6.

Left	Right
326.2	328.3
$\frac{31}{10^e}$	$\frac{10}{10^e}$
333.8	335.8
$\frac{73}{10^e}$	$\frac{58}{10^e}$
338.0	338.9
$\frac{73}{10^e}$	$\frac{85}{10^e}$
339.6	340.2
$\frac{78}{10^e}$	$\frac{72}{10^e}$
340.6	341.3
$\frac{68}{10^e}$	$\frac{61}{10^e}$
342.4	342.8
$\frac{50}{10^e}$	$\frac{46}{10^e}$
343.9	344.1
$\frac{35}{10^e}$	$\frac{32}{10^e}$
345.5	346.2
$\frac{19}{10^e}$	$\frac{12}{10^e}$
348.0	348.9
$\frac{92}{10^e}$	$\frac{90}{10^e}$

	+	π	-	Elev.	Elev. B.M.
				348.825	
	11.112	A-357.929 359.937			
1008 + 90°			10.5	349.4	
1009 + 15°			8.8	351.1	
+ 40°			7.1	352.8	
+ 65°			6.2	353.7	
+ 90°			5.5	354.4	
1010 + 15°			5.3	354.6	
+ 40°			4.4	355.5	
+ 65°			3.8	356.1	
Stake T.P.	A-9.210	A-0.961 366.178		356.968	
+ 90°			3.1	356.8	
1011 + 02°			2.8	357.1	
Stake T.P.			1.772	358.165	
	9.308	367.473			
1012 + 00			8.5	359.0	

Left	Right
348.6	349.9
$\frac{9^{\circ}}{10^{\circ}}$	$\frac{8^{\circ}}{10^{\circ}}$
350.7	351.5
$\frac{7^{\circ}}{10^{\circ}}$	$\frac{6^{\circ}}{10^{\circ}}$
352.2	352.8
$\frac{5^{\circ}}{10^{\circ}}$	$\frac{5^{\circ}}{10^{\circ}}$
353.3	353.8
$\frac{4^{\circ}}{10^{\circ}}$	$\frac{4^{\circ}}{10^{\circ}}$
353.7	354.8
$\frac{4^{\circ}}{10^{\circ}}$	$\frac{3^{\circ}}{10^{\circ}}$
354.3	355.0
$\frac{3^{\circ}}{10^{\circ}}$	$\frac{2^{\circ}}{10^{\circ}}$
354.9	355.9
$\frac{3^{\circ}}{10^{\circ}}$	$\frac{2^{\circ}}{10^{\circ}}$
355.7	356.5
$\frac{2^{\circ}}{10^{\circ}}$	$\frac{1^{\circ}}{10^{\circ}}$
356.8	357.1
$\frac{9^{\circ}}{10^{\circ}}$	$\frac{9^{\circ}}{10^{\circ}}$
357.3	357.4
$\frac{8^{\circ}}{10^{\circ}}$	$\frac{8^{\circ}}{10^{\circ}}$
358.3	359.0
$\frac{7^{\circ}}{10^{\circ}}$	$\frac{7^{\circ}}{10^{\circ}}$

	+	π	-	Elev.	Elev. B.M.
		366.178 367.473			
1013+00			6.2	361.3	✓
+30°			6.5	361.0	✓
+56°			5.8	361.7	✓
1014+00			6.6	360.9	✓
+37°			5.0	362.5	✓
+59°			5.4	362.17	✓
+83°			3.6	363.9	✓
1015+00			4.9	362.6	✓
Stake T.P.	A = 4.267 3.968	368.492 367.483	A 1.953 3.958	364.225 363.515	✓
1015+27°			2.9	364.65	✓
+57°			4.8	362.7	✓
+88°			2.2	365.3	✓

Left		Right
362.0	✓	362.4
$\frac{4^{\circ}}{10^{\circ}}$	✓	$\frac{5^{\circ}}{10^{\circ}}$
360.9	✓	361.9
$\frac{5^{\circ}}{10^{\circ}}$	✓	$\frac{4^{\circ}}{10^{\circ}}$
362.6	✓	361.0
$\frac{3^{\circ}}{10^{\circ}}$	✓	$\frac{5^{\circ}}{10^{\circ}}$
360.8	✓	362.4
$\frac{5^{\circ}}{10^{\circ}}$	✓	$\frac{3^{\circ}}{10^{\circ}}$
363.3	✓	361.9
$\frac{2^{\circ}}{10^{\circ}}$	✓	$\frac{4^{\circ}}{10^{\circ}}$
362.6	✓	361.9
$\frac{3^{\circ}}{10^{\circ}}$	✓	$\frac{4^{\circ}}{10^{\circ}}$
364.2	✓	363.7
$\frac{2^{\circ}}{10^{\circ}}$	✓	$\frac{2^{\circ}}{10^{\circ}}$
362.7	✓	362.8
$\frac{3^{\circ}}{10^{\circ}}$	✓	$\frac{5^{\circ}}{10^{\circ}}$
363.3	✓	363.8
$\frac{5^{\circ}}{10^{\circ}}$	✓	$\frac{7^{\circ}}{10^{\circ}}$
362.6	✓	362.6
$\frac{5^{\circ}}{10^{\circ}}$	✓	$\frac{5^{\circ}}{10^{\circ}}$
364.1	✓	365.5
$\frac{4^{\circ}}{10^{\circ}}$	✓	$\frac{5^{\circ}}{10^{\circ}}$

	π	π	Elev.	Elev. B.M.
	$\pi = \frac{368.492}{367.483}$			
1016+00		4.0	363.5	
+23°		5.3	362.2	
+46°		3.6	363.9	
1017+00		6.0	361.5	
B.M. #16B	$\pi = \frac{366.153}{366.133}$	5.380	362.103	362.106
	$\pi = \frac{366.153}{366.367}$			
+28°		1.7	364.7	
+58°		5.7	360.7	
1018+00		3.4	363.0	
+07°		2.7	363.7	
+33°		6.0	360.4	
+61°		4.8	361.6	
+88°		6.4	360.0	
1019+00		5.8	360.6	

Left	Right
363.0	362.9
$\frac{5^5}{10^2}$	$\frac{5^6}{10^2}$
362.9	362.9
$\frac{5^6}{10^2}$	$\frac{6^1}{10^2}$
362.3	365.5
$\frac{6^2}{10^2}$	$\frac{3^0}{10^2}$
361.5	361.6
$\frac{7^0}{10^2}$	$\frac{6^9}{10^2}$
364.2	364.3
$\frac{2^0}{10^2}$	$\frac{1^8}{10^2}$
360.6	360.8
$\frac{5^6}{10^2}$	$\frac{5^2}{10^2}$
362.8	361.7
$\frac{3^7}{10^2}$	$\frac{4^7}{10^2}$
363.4	362.2
$\frac{2^8}{10^2}$	$\frac{5^3}{10^2}$
360.4	360.7
$\frac{5^8}{10^2}$	$\frac{5^5}{10^2}$
360.3	362.8
$\frac{5^7}{10^2}$	$\frac{3^3}{10^2}$
360.0	360.1
$\frac{6^2}{10^2}$	$\frac{6^1}{10^2}$
359.9	361.1
$\frac{6^3}{10^2}$	$\frac{5^1}{10^2}$

+ "A" ~~366.153~~ ^{366.153} - Elev. Elev. B.M.

1019+13 ^e	4.3	362.1
+33 ^e	6.7	359.7
1020+00	8.0	358.4
+44 ^e	6.7	359.7
+67 ^e	8.4	358.0
1021+00	9.7	356.7
Stake T.P.	8.605	357.528
	9.602	356.765
	3.085	359.850
+13 ^e	2.5	357.3
+43 ^e	4.0	355.8
+73 ^e	2.6	357.2
1022+00	4.0	355.8
+30 ^e	4.5	355.3
+55 ^e	3.9	355.9

~~360.169~~ ^{360.169}

~~357.548~~ ^{357.548}

±

Left	360.34
$\frac{5.8}{10^e}$	359.75
$\frac{6.7}{10^e}$	359.0
$\frac{7.2}{10^e}$	358.7
$\frac{8.2}{10^e}$	358.12
$\frac{8.9}{10^e}$	357.78
$\frac{9.6}{10^e}$	356.46
$\frac{9.6}{10^e}$	357.23
$\frac{9.9}{10^e}$	355.89
$\frac{4.3}{10^e}$	355.47
$\frac{4.5}{10^e}$	356.36
$\frac{3.6}{10^e}$	356.12
$\frac{4.0}{10^e}$	355.0
$\frac{5.2}{10^e}$	354.7

Right	362.19
$\frac{3.3}{10^e}$	360.0
$\frac{6.2}{10^e}$	358.7
$\frac{7.2}{10^e}$	360.0
$\frac{6.2}{10^e}$	357.89
$\frac{8.2}{10^e}$	356.78
$\frac{9.4}{10^e}$	356.78
$\frac{9.9}{10^e}$	355.46
$\frac{2.6}{10^e}$	358.12
$\frac{2.2}{10^e}$	356.0
$\frac{4.2}{10^e}$	355.3
$\frac{4.0}{10^e}$	355.4
$\frac{4.7}{10^e}$	355.75

	+	360.169 359.850	-	Elev.	Elev. B.M.
10	1022+67°		5.2	354.6	
	1023+00		2.4	357.4	
10	+29		4.7	355.1 355.2	
	1024+00		5.1	354.8	357.260
	Rock T.P.	359.240 359.220	5.133	357.240 354.717	
		A" 1.980 6.448			
	P.O.T.				
10	1024+76°		4.0	357.2	
5+	1025+00		5.6	355.6	
	+22°		7.0	354.2	
	+84°		6.8	354.4	
	1026+00		5.3	355.9	
10	B.M. #117 May 20	Hub 25' L. 1.148	7.165	354.000	354.020
	1026+17°		1.3	353.9	
	+40°		0.8	354.4	

Left	Right
$\frac{5^2}{10^2}$ 354.78	$\frac{5^2}{10^2}$ 355.01
$\frac{3^6}{10^2}$ 356.56	$\frac{3^5}{10^2}$ 356.77
$\frac{4^3}{10^2}$ 355.89	$\frac{5^1}{10^2}$ 355.01
$\frac{5^2}{10^2}$ 355.0	$\frac{4^9}{10^2}$ 355.23
$\frac{2^6}{10^2}$ 356.6	$\frac{2^4}{10^2}$ 356.8
$\frac{4^2}{10^2}$ 354.3	$\frac{3^2}{10^2}$ 356.0
$\frac{4^2}{10^2}$ 354.5	$\frac{5^0}{10^2}$ 354.2
$\frac{4^8}{10^2}$ 354.9	$\frac{4^7}{10^2}$ 354.5
$\frac{5^2}{10^2}$ 354.0	$\frac{3^2}{10^2}$ 356.2
$\frac{5^2}{10^2}$ 354.0	$\frac{4^9}{10^2}$ 354.3
$\frac{3^7}{10^2}$ 355.5	$\frac{5^3}{10^2}$ 353.9

May 20, 1926

Profile

Duermit. π
Bailey
Clavert. Rod.

+ $\overset{A}{\cancel{359.240}}$ - Elev. Elev. B.M.
 $\frac{359.240}{355.168}$

Station	Angle	Dist.	Elev.	Elev. B.M.
1027+00		2.1	353.1	354.010
B.M. # 117 (TP)		5.230	353.990	354.020
	+49°	0.8	354.4	
	+74°	2.6	352.6	
	+88°	1.9	353.3	
1028+00		2.7	352.5	
	+21°	3.3	351.9	
	+35°	3.2	352.0	
	+56°	5.3	349.9	
1029+00		5.5	349.7	
	+28°	3.1	352.1	
	+52°	6.4	348.8	
1030+00		6.5	348.7	

Left	Right
$\frac{6}{10} = 353.1$	$\frac{5}{10} = 354.0$
$\frac{12}{10} = 353.9$	$\frac{13}{10} = 354.3$
$\frac{22}{10} = 352.7$	$\frac{3}{10} = 352.4$
$\frac{12}{10} = 353.7$	$\frac{5}{10} = 352.5$
$\frac{3}{10} = 352.6$	$\frac{3}{10} = 351.9$
$\frac{3}{10} = 352.9$	$\frac{3}{10} = 351.3$
$\frac{27}{10} = 353.3$	$\frac{4}{10} = 350.9$
$\frac{23}{10} = 350.1$	$\frac{47}{10} = 350.9$
$\frac{53}{10} = 349.8$	$\frac{56}{5} = 350.0$
$\frac{58}{10} = 352.1$	$\frac{5}{10} = 349.7$
$\frac{35}{10} = 349.1$	$\frac{53}{10} = 350.3$
$\frac{65}{10} = 348.2$	$\frac{6}{10} = 349.0$
$\frac{72}{10} = 348.2$	$\frac{73}{10} = 348.9$

+ A $\frac{\pi}{355.585}$ - Elev. Elev. B.M.
 $\frac{355.168}{355.168}$

			Elev.	Elev. B.M.
1	1030 + 17 ^e	5.7	349.5	
	+ 31 ^e	7.3	347.9	
1	+ 43 ^e	8.4	346.8	
	+ 56 ^e	7.1	348.1	
	+ 81 ^e	8.6	346.6	
1	1031 + 06 ^e	9.7	345.5	
5	+ 31 ^e	11.8	343.4	
	Stake T.P. A' 1.437	12.153	343.432	
		344.869		
	1032 + 00	13.7	341.5	
	Rock T.P.	11.741	343.427	
		1.229	344.656	
	1032 + 21 ^e	3.8	340.9	
	P.O.T.			
	+ 41 ^e	6.8	337.9	
	+ 70 ^e	12.1	332.6	
	1033 + 00	13.3	331.4	

Left	Right
$\frac{6^e}{10^e}$ 349.2	$\frac{6^e}{10^e}$ 347.2
$\frac{7^e}{10^e}$ 347.6	$\frac{7^e}{10^e}$ 347.5
$\frac{8^e}{10^e}$ 346.6	$\frac{8^e}{10^e}$ 347.1
$\frac{9^e}{10^e}$ 348.0	$\frac{8^e}{10^e}$ 347.5
$\frac{7^e}{10^e}$ 346.5	$\frac{8^e}{10^e}$ 346.3
$\frac{9^e}{10^e}$ 344.9	$\frac{9^e}{10^e}$ 345.8
$\frac{10^e}{10^e}$ 343.8	$\frac{9^e}{10^e}$ 343.5
$\frac{11^e}{10^e}$ 341.6	$\frac{12^e}{10^e}$ 341.3
$\frac{5^e}{10^e}$ 340.8	$\frac{3^e}{10^e}$ 339.6
$\frac{7^e}{10^e}$ 338.8	$\frac{5^e}{10^e}$ 337.6
$\frac{6^e}{10^e}$ 337.6	$\frac{7^e}{5^e}$ 336.7
$\frac{11^e}{10^e}$ 333.4	$\frac{12^e}{10^e}$ 332.0
$\frac{13^e}{10^e}$ 331.3	$\frac{14^e}{5^e}$ 329.8

	+	π	-	Elev.	Elev. B.M.
		344.869			
		344.656			
1033+15 ^e			14.5	330.2	
Stake T.P.	"A"	12.943		331.926	
		0.937	11.120	333.536	
		1.424			
Stake T.P.	"A"	12.499		320.364	
		1.137	11.251	323.709	
		0.748			
1034+00			6.4	318.1	
Stake T.P.	"A"	12.659		308.842	
		3.542	11.223	313.234	
		0.965			
1034+68 ^e		First Bank of Wash	13.3	300.9	
+ 71 ^e		2 ^d of Dry Wash	13.8	300.4	
+ 74 ^e			13.8	300.4	
+ 77 ^e		Second Bank of Dry Wash	11.6	302.6	
+ 80 ^e			10.1	304.1	
1035+00			7.4	306.8	
Stake T.P.	"A"	0.984		311.295	
		12.268	2.139	312.061	
		10.812			
1035+23			12.8	310.1	



	π	Elev.	Elev. B.M.
	π 323.663 322.873		
1036+00	6.7 A 2.169 1.368	316.2 321.499 321.505	
Stake T.P.	11.145 332.645 9.372 330.877		
1037+00	1.5 2.912 1.138	329.4 329.733 329.739	329.782
B.M. #118 (T.P.)	11.990 341.772 11.129 340.911		
1038+00	2.1	338.8	
P.O.T. +35	2.7	338.2	
1039+00	5.8 A 9.073 11.280	335.1 332.699 329.631	
Stake T.P.	A 0.780 333.479 3.575 333.206		
1039+56	1.9	331.3	
1040+00	8.6	324.6	
+14° First Bank of Dry Wash.	11.7	321.5	
+15° E of Dry Wash	12.6	320.6	
+16° Second Bank of Dry Wash.	12.0	321.2 321.2	
+38°	8.1	325.1	

Left	Right
314.2	317.4
$\frac{95}{100}$	$\frac{63}{100}$
328.7	330.0
$\frac{39}{100}$	$\frac{26}{100}$
338.3	339.4
$\frac{35}{100}$	$\frac{22}{100}$
336.7	339.9
$\frac{51}{100}$	$\frac{19}{100}$
333.0	338.7
$\frac{82}{100}$	$\frac{51}{100}$
329.6	332.8
$\frac{32}{100}$	$\frac{07}{100}$
322.0	327.9
$\frac{115}{100}$	$\frac{56}{100}$
319.8	323.6
$\frac{137}{100}$	$\frac{97}{100}$
321.2	323.3
$\frac{122}{92}$	$\frac{132}{32}$
320.5	322.7
$\frac{132}{32}$	$\frac{124}{16}$
321.4	321.1
$\frac{111}{52}$	$\frac{321.7}{100}$
322.4	322.7
$\frac{132}{102}$	$\frac{132}{32}$
319.7	320.6
$\frac{132}{102}$	$\frac{122}{20}$
320.0	321.8
$\frac{132}{102}$	$\frac{112}{43}$
319.9	321.2
$\frac{132}{102}$	$\frac{112}{62}$
326.2	322.7
$\frac{73}{103}$	$\frac{102}{102}$
	326.0
	$\frac{75}{102}$

May 29, 1926
Cross-sections

Duermitt, Notes
Todd, T.
Anderson, Rods.
Webb }

Note, All Cross-sections to be taken from H. E.
marked "A"

	+ "A"	π	-	Elev.	Elev. B.M.
		333.479			
		333.206			
Stake T.P.		"A"	1.243	332.236	
	12.614	344.850	0.986	332.220	
	11.722	343.942			
1041+00			3.2	340.7	
		"A"	1.760	343.090	
Stake T.P.			0.868	343.074	
	11.704	354.794			
	11.752	354.826			
1041+30 ^e			8.6	346.2	
1042+00			3.8	351.0	
		"A"	0.688	354.106	
Stake T.P.			0.793	354.073	
	6.238	360.344			
	5.214	359.307			
1043+00			4.9	354.4	
+81'			3.7	355.6	
1044+00			4.0	355.3	
1045+00			5.3	354.0	
1046+00			7.2	352.1	
1047+00			11.5	347.8	
		"A"	11.850	348.494	
Stake T.P.			10.827	348.480	
	0.889	349.383			
	1.220	349.700			

Left	Right
341.3	339.7
$\frac{35}{10^e}$	$\frac{51}{10^e}$
346.9	345.7
$\frac{72}{10^e}$	$\frac{91}{10^e}$
351.0	351.1
$\frac{38}{10^e}$	$\frac{32}{10^e}$
May 29, 1926.	
354.4	353.7
$\frac{52}{10^e}$	$\frac{56}{10^e}$
355.6	355.8
$\frac{47}{10^e}$	$\frac{45}{10^e}$
355.0	355.5
$\frac{53}{10^e}$	$\frac{48}{10^e}$
353.8	354.5
$\frac{65}{10^e}$	$\frac{58}{10^e}$
352.0	352.4
$\frac{83}{10^e}$	$\frac{79}{10^e}$
348.3	347.9
$\frac{12^e}{10^e}$	$\frac{12^e}{10^e}$

	+	T	-	Elev.	Elev. B.M.
	A	349.383			
		349.700			
B.M. #119 a	A	2.773	6.923	342.460	342.445
		345.218	7.257	342.443	342.445
		1.505		343.950	
1048+00			4.6	339.4	
1049+00			9.2	334.8	
B.M. #119	A	8.866		336.352	
		1.070	7.597	336.343	336.344
		1.461		336.353	
1050+00			6.0	331.8	
1051+00			8.6	329.2	
1052+00			11.1	326.7	
Stake T.P.	A	10.678		326.747	
		5.950	11.057	326.748	
		5.606		332.354	
1052+30°			5.2	327.2	
+50°			6.3	326.1	
1053+00			6.4	326.0	
1054+00			5.7	326.7	
P.O.T.			4.5	327.9	
1055+00					

Right.

Left.

339.7	337.6
$\frac{52}{102}$	$\frac{56}{102}$
335.3	334.3
$\frac{92}{102}$	$\frac{102}{102}$
332.9	330.9
$\frac{50}{102}$	$\frac{62}{102}$
329.5	328.9
$\frac{72}{102}$	$\frac{82}{102}$
326.6	326.5
$\frac{108}{102}$	$\frac{102}{102}$
326.5	327.1
$\frac{52}{102}$	$\frac{52}{102}$
326.1	325.6
$\frac{62}{102}$	$\frac{62}{102}$
326.4	325.7
$\frac{58}{102}$	$\frac{62}{102}$
326.9	326.5
$\frac{52}{102}$	$\frac{52}{102}$
328.1	327.7
$\frac{42}{102}$	$\frac{45}{102}$

	+	π	-	Elev.	Elev. B.M.
		332.197 332.354			
+54°			3.6	328.8	
1056+00			5.5	326.9	
+44°			6.1	326.3	
1057+00			8.4	324.0	
B.M. #119-b	A	8.020		324.162	
	A	3.646	327.802	8.210	324.144
		3.670	327.826		324.156
1058+00			4.5	323.3	
P.O.T.					
+55°			4.2	323.6	
1059+00			5.4	322.4	
+70°			9.2	318.6	
1060+00			12.7	315.1	
Stake T.P.	A	11.205		316.597	
	A	1.400	317.997	11.258	316.568
		1.552	318.120		
1060+68°			9.6	308.5	
					First Bank of Dry Wash
+71°			10.5	307.6	
					E of Dry Wash

Left	Right
328.7	328.2
$\frac{3^{\circ}}{10^{\circ}}$	$\frac{4^{\circ}}{10^{\circ}}$
327.2	326.6
$\frac{5^{\circ}}{10^{\circ}}$	$\frac{5^{\circ}}{10^{\circ}}$
325.8	326.4
$\frac{6^{\circ}}{10^{\circ}}$	$\frac{5^{\circ}}{10^{\circ}}$
323.9	324.8
$\frac{8^{\circ}}{10^{\circ}}$	$\frac{7^{\circ}}{10^{\circ}}$
323.4	323.1
$\frac{7^{\circ}}{10^{\circ}}$	$\frac{4^{\circ}}{10^{\circ}}$
324.5	323.2
$\frac{3^{\circ}}{10^{\circ}}$	$\frac{4^{\circ}}{10^{\circ}}$
322.6	322.2
$\frac{5^{\circ}}{10^{\circ}}$	$\frac{5^{\circ}}{10^{\circ}}$
318.8	318.8
$\frac{9^{\circ}}{10^{\circ}}$	$\frac{9^{\circ}}{10^{\circ}}$
315.3	315.0
$\frac{12^{\circ}}{10^{\circ}}$	$\frac{12^{\circ}}{10^{\circ}}$
307.0	309.3
$\frac{11^{\circ}}{10^{\circ}}$	$\frac{8^{\circ}}{10^{\circ}}$
306.6	308.8
$\frac{11^{\circ}}{10^{\circ}}$	$\frac{9^{\circ}}{10^{\circ}}$
307.6	
$\frac{10^{\circ}}{5^{\circ}}$	

	+ A	T	-	Elev.	Elev. B.M.
		317.997			
		318.120			
1060+73°	Second Bank of Dry Lake:	9.8		308.3	
1061+00		7.0		311.1	
1062+00		6.1		312.0	
1063+00		5.3		312.8	
1064+00		7.0		311.1	
A Stake T.P.	A-7.038	317.487	A-7.548	310.449	
1065+00		8.7		309.4	
Stake T.P.		7.865		310.255	
	10.222	320.477			
1066+00		8.1		312.4	
A Stake T.P.	A-12.388	328.106	A-11.769	315.718	
1067+00		2.8		317.7	
(T.P.)		0.890		319.587	
	10.717	330.304			
1068+00		8.5		321.8	
1069+00		5.6		324.7	
B.M. #120	(T.P.)	3.720	A-3.720	324.376	
	A-5.552	329.913	6.003	324.301	324.361
	5.880	330.241			
1069+90.9		5.3		324.9	

19

Left	Right
307.5	309.2
$\frac{10^2}{10^2}$	$\frac{8^2}{10^2}$
309.5	311.8
$\frac{8^2}{10^2}$	$\frac{6^2}{10^2}$
311.3	312.9
$\frac{6^2}{10^2}$	$\frac{5^2}{10^2}$
312.4	313.2
$\frac{5^2}{10^2}$	$\frac{4^2}{10^2}$
311.2	310.6
$\frac{6^2}{10^2}$	$\frac{7^2}{10^2}$
309.1	310.1
$\frac{8^2}{10^2}$	$\frac{7^2}{10^2}$
311.5	312.8
$\frac{6^2}{10^2}$	$\frac{4^2}{10^2}$
316.8	318.1
$\frac{11^2}{10^2}$	$\frac{10^2}{10^2}$
321.8	322.3
$\frac{6^2}{10^2}$	$\frac{5^2}{10^2}$
324.0	325.3
$\frac{4^2}{10^2}$	$\frac{2^2}{10^2}$
325.5	325.1
$\frac{4^2}{10^2}$	$\frac{4^2}{10^2}$

	+	"A"	Elev.	Elev. B. M.
1070+15 ²	5.5	329.913 330.241	324.7	
+40 ²	5.0		325.2	
+65 ²	4.3		325.9	
+90 ²	5.3		324.9	
1071+00 ²	5.4		324.8	
+70 ²	5.2		325.0	
1072+00	6.1		324.1	
+30 ²	6.9		323.3	
Stake T.P.	A=3.400	326.524	A=6.789	323.124
+70 ²	6.5		323.7	
1073+00	9.1		321.1	
+12 ²	8.4		321.841	
Stake T.P.	10.154		320.087	
	3.643		323.730	

Left	Right
325.0	324.6
$\frac{4^2}{10^2}$	$\frac{5^2}{10^2}$
325.6	325.2
$\frac{4^3}{10^2}$	$\frac{4^2}{10^2}$
326.2	324.4
$\frac{3^2}{10^2}$	$\frac{5^5}{10^2}$
325.4	324.5
$\frac{7^2}{10^2}$	$\frac{5^2}{10^2}$
325.7	324.6
$\frac{4^2}{10^2}$	$\frac{5^3}{10^2}$
325.1	324.8
$\frac{4^2}{10^2}$	$\frac{5^1}{10^2}$
324.0	323.7
$\frac{5^2}{10^2}$	$\frac{6^2}{10^2}$
323.5	322.8
$\frac{6^2}{10^2}$	$\frac{7^1}{10^2}$
324.1	322.5
$\frac{2^2}{10^2}$	$\frac{4^2}{10^2}$
321.5	320.3
$\frac{5^2}{10^2}$	$\frac{6^2}{10^2}$
323.0	320.5
$\frac{4^2}{10^2}$	$\frac{6^2}{10^2}$

Cross-sections
June 1, 1926

Duermil, A.
Baker,
Moultrie, (Rods.
Hammer,)

Note: All cross-sections to be taken from 21
H.I. marked "A."

+ A - 326.524
323.730

	-	Elev.	Elev. B.M.
1074+00	5.8	317.9	✓
1075+00	7.4	316.3	✓
A - Stake T.P.	A - 3.873 320.114	10.283 316.241	✓
1076+00	8.9	314.8	✓
+34 ⁵	10.5	313.2	✓
+59 ⁵	11.5	312.2	✓
+84 ⁵	12.5	311.2	✓
Stake T.P.	A - 8.882 1.249 1.609	311.292 312.465 314.074	✓
1077+09 ⁵	3.7	310.4	✓
1077+34 ⁵	5.8	308.3	✓
+59 ⁵	7.4	306.7	✓
+64 ⁵	8.1	306.0	✓
1078+00	11.8	302.3	✓
Stake T.P.	A - 10.130 1.299 1.379	302.351 302.351 303.730	✓

Left

318.7
 $\frac{7^8}{10^2}$

316.7

$\frac{9^8}{10^2}$

$\frac{4^9}{10^2}$

$\frac{6^6}{10^2}$

$\frac{7^2}{10^2}$

$\frac{8^9}{10^2}$

$\frac{2^3}{10^2}$

$\frac{3^4}{10^2}$

$\frac{5^4}{10^2}$

$\frac{6^0}{10^2}$

$\frac{9^3}{10^2}$

Right

317.7

$\frac{8^8}{10^2}$

315.7

$\frac{10^8}{10^2}$

314.1

$\frac{6^6}{10^2}$

313.5

$\frac{6^6}{10^2}$

311.6

$\frac{8^5}{10^2}$

310.6

$\frac{9^5}{10^2}$

310.1

$\frac{2^4}{10^2}$

307.3

$\frac{5^2}{10^2}$

305.8

$\frac{6^2}{10^2}$

305.1

$\frac{7^4}{10^2}$

301.5

$\frac{11^0}{10^2}$

June 1, 1926

	+	π	-	Elev.	Elev. B.M.	Left	Right
		303.650					
		303.730					
Rock T.P.	A	0.958	292.190	12.418	291.232		
		1.291	293.236	11.785	291.945	287.5	287.9
1079+00			4.6	288.6		$\frac{22}{100}$	$\frac{43}{100}$
Rock T.P.	A	0.727	280.038	12.879	279.311		
		1.093	282.887	11.442	281.794		
Stake T.P.			8.191	274.696			
		1.311	276.007				
B.M. #121	A	1.570	269.489	12.119	267.919	Record Elev.	
		1.658	269.603	8.097	267.910	267.945	268.1
1080+00			1.1	268.5		$\frac{10}{100}$	$\frac{14}{100}$
Stake T.P.	A	0.919	258.521	11.887	257.602		
		1.148	258.769	11.982	257.621	248.4	248.2
1081+00			10.2	248.6		$\frac{102}{100}$	$\frac{103}{100}$
Rock T.P.	A	0.936	246.859	12.598	245.923		
		0.924	247.945	11.748	247.021		
Stake T.P.	A	0.940	235.318	12.481	234.378		
		0.811	237.306	11.450	236.475	225.7	226.5
1082+00			10.8	226.6		$\frac{96}{100}$	$\frac{88}{100}$
Rock T.P.	A	0.937	223.541	12.714	222.604		
		0.813	227.114	11.003	226.301		
Rock T.P.	A	1.084	212.111	12.514	211.027		
		0.908	216.130	11.892	215.222	203.9	204.9
1083+00			11.9	204.2		$\frac{82}{100}$	$\frac{72}{100}$

May 21, 1926
Profite

Overhaul, T
Bulley } Red.
Clavert }

Duermitt-Notes.
Reynolds-X
Anderson-Red
Bichet

Cross Sections

Note, All cross-sections to be taken from H.I. marked "A"

23

	+ A	T	Elev.	Elev. B.M.
Stake T.P. May 21	0.237 1.288	212.111 215.130	12.080 11.525	179.531 204.605
Rock T.P.	0.392 0.858	197.619 195.773	12.541 10.978	187.227 194.915
1084+00		10.8 11.797	185.0 175.822	
Rock T.P.	0.895 0.953	176.217 185.384	11.342	184.431
Rock T.P.	0.343 0.854	164.958 174.304	12.702 11.934	164.015 173.450
1085+00		6.3 12.739	168.0 152.219	
Rock T.P.	0.582 0.752	152.801 163.224	11.832	162.472
Rock T.P.	1.707	153.024	11.907	151.317
1085+70°		3.5	149.5	
1086+00		7.5 8.783	145.5 144.018	Record Elev. used.
B.M. #123-a	0.245 1.429	144.304 145.488	9.024	144.000 144.059
1087+00		10.2	135.3	

Left Right

June 2, 1926.

3± 102	184.2	186.0
72 102	169.0 157.3	166.0 154.3
82 42	168.4 156.7	
22 102	150.1	148.6
61 102	146.7	144.4
71 102	136.6	132.9

	+	π	-	Elev.	Elev. B.M.
		"A" 144.304 145.488			
1087+43 ^e	First Bank of Wash.	14.8	130.7		
+ 57 ^e	4 ^e of Dry Wash.	16.5	129.0		
Rock T.P. - A	"A" 0.870	132.926	12.256	132.048	
+ 90 ^e		15.9	129.6		
+ 96 ^e		16.6	128.9		
1088+00	Second Bank of Wash.	15.9	129.6		
Stake T.P. (Sta. 1087+25)		10.975	134.513		
		1.057	135.570		
1088+54 ^e		9.9	125.7		
Stake T.P.		8.847	126.723		
		1.940	128.663		
1089+00		2.9	125.8		
ACT. P.	"A" 2.405	128.080	7.251	125.675	
1090+00		7.4	121.3		
1091+00		8.6	120.1		
Stake T.P.	"A" 1.325	121.660	7.743	120.337	
		1.122	121.425	8.360	120.303

29

♀

Left.	Right.
132.7	130.6
$\frac{116}{100}$	$\frac{137}{100}$
132.2	132.0
$\frac{122}{100}$	$\frac{123}{100}$
131.8	130.2
$\frac{125}{60}$	$\frac{138}{50}$
130.5	130.6
$\frac{138}{50}$	$\frac{132}{50}$
129.0	129.7
$\frac{32}{100}$	$\frac{27}{100}$
128.3	128.9
$\frac{48}{50}$	$\frac{32}{100}$
128.4	128.1
$\frac{46}{100}$	$\frac{38}{50}$
126.5	127.0
$\frac{45}{100}$	$\frac{31}{70}$
126.3	126.0
$\frac{67}{100}$	$\frac{39}{100}$
124.5	122.6
$\frac{84}{100}$	$\frac{69}{100}$
121.2	120.4
$\frac{67}{100}$	$\frac{65}{100}$
119.8	
$\frac{83}{100}$	$\frac{72}{100}$

+ "A" $\frac{7}{121.660}$ - Elev. Elev. B.M.
 $\frac{121.425}{121.425}$

1092+00	6.7	114.7
1093+00	11.3	110.1
Stake. T.P.	$\frac{11.592}{11.390}$	$\frac{110.068}{110.035}$
	$\frac{2.458}{1.243}$	$\frac{112.526}{111.278}$
1094+00	5.1	106.2
First Bank of Dry Wash		
+ 82°	6.8	104.5
+ 92° E of Dry Wash.	8.1	103.23
+ 97° Second Bank of Wash.	7.9	103.4
1095+00	7.2	104.1
+ 30°	7.8	103.5
+ 70°	8.1	103.23
+ 80°	9.9	101.4
+ 86°	8.3	103.0

Left	114.1	Right	115.6
$\frac{7\frac{2}{10}}{10\frac{2}{10}}$	110.2	$\frac{6\frac{1}{10}}{10\frac{2}{10}}$	110.5
$\frac{11\frac{5}{10}}{10\frac{2}{10}}$	106.0	$\frac{11\frac{2}{10}}{10\frac{2}{10}}$	106.7
$\frac{6\frac{5}{10}}{10\frac{2}{10}}$	103.2	$\frac{5\frac{8}{10}}{10\frac{2}{10}}$	104.3
$\frac{9\frac{3}{10}}{10\frac{2}{10}}$	104.8	$\frac{8\frac{1}{5}}{5\frac{2}{10}}$	103.9
$\frac{7\frac{2}{10}}{10\frac{2}{10}}$	103.9	$\frac{9\frac{2}{5}}{5\frac{2}{10}}$	103.4
$\frac{7\frac{6}{10}}{10\frac{2}{10}}$	104.9	$\frac{9\frac{2}{10}}{8\frac{2}{10}}$	103.2
$\frac{10\frac{4}{7}}{10\frac{2}{10}}$	104.7	$\frac{8\frac{2}{5}}{2\frac{5}{10}}$	103.2
$\frac{8\frac{1}{10}}{10\frac{2}{10}}$	104.4	$\frac{10\frac{2}{20}}{2\frac{5}{10}}$	102.6
$\frac{9\frac{2}{10}}{10\frac{2}{10}}$	103.3	$\frac{9\frac{3}{5}}{5\frac{2}{10}}$	102.6
$\frac{9\frac{2}{10}}{10\frac{2}{10}}$	103.1	$\frac{9\frac{1}{10}}{10\frac{2}{10}}$	103.5
$\frac{9\frac{2}{10}}{10\frac{2}{10}}$	102.8	$\frac{10\frac{2}{10}}{10\frac{2}{10}}$	101.7
$\frac{9\frac{2}{10}}{10\frac{2}{10}}$	102.8	$\frac{10\frac{2}{10}}{10\frac{2}{10}}$	101.6
$\frac{9\frac{2}{10}}{10\frac{2}{10}}$	102.7	$\frac{10\frac{2}{10}}{10\frac{2}{10}}$	101.6
$\frac{9\frac{2}{10}}{10\frac{2}{10}}$	102.7	$\frac{10\frac{2}{10}}{10\frac{2}{10}}$	101.9
$\frac{9\frac{2}{10}}{10\frac{2}{10}}$	102.7	$\frac{11\frac{1}{10}}{10\frac{2}{10}}$	101.9

	+	-	Elev.	Elev. B.M.
	A	112.526		
		111.278		
1096+00		8.5	102.8	
	A	9.239	103.287	
B.M. #123-6		8.028	103.250	103.272
	A	6.298	109.585	
		8.772	112.044	
First Bank of Dry Wash				
1096+17°		10.0	102.0	
E of Dry Wash				
+44°		12.2	99.8	
Second Bank of Dry Wash				
+74°		10.5	101.5	
+87°		11.3	100.7	
1097+00		11.3	100.7	
Stake T.P.	A	1.622	107.963	
		3.418	111.381	
1098+00		4.4	107.6	
1099+00		5.2	106.8	
+72°		7.2	104.8	
	A	8.729	102.652	
Stake T.P.		6.858	105.186	
	A	2.230	104.882	
		1.302	106.480	
	A	12.022	92.860	
Stake T.P.		11.570	94.918	
	A	1.763	94.623	
		1.493	96.411	

Left	Right
102.7	102.5
$\frac{9^{\circ}}{10^{\circ}}$	$\frac{10^{\circ}}{10^{\circ}}$ $\frac{11^{\circ}}{2^{\circ}}$ $\frac{11^{\circ}}{10^{\circ}}$
102.1	101.3
$\frac{7^{\circ}}{10^{\circ}}$	$\frac{8^{\circ}}{2^{\circ}}$ $\frac{8^{\circ}}{5^{\circ}}$ $\frac{8^{\circ}}{10^{\circ}}$
101.5	101.1
$\frac{8^{\circ}}{10^{\circ}}$	$\frac{7^{\circ}}{2^{\circ}}$ $\frac{9^{\circ}}{3^{\circ}}$ $\frac{7^{\circ}}{7^{\circ}}$ $\frac{7^{\circ}}{10^{\circ}}$
99.0	100.5
$\frac{10^{\circ}}{10^{\circ}}$	102.1
98.7	101.6
$\frac{10^{\circ}}{10^{\circ}}$	$\frac{8^{\circ}}{10^{\circ}}$
98.5	101.1
$\frac{10^{\circ}}{10^{\circ}}$	$\frac{8^{\circ}}{10^{\circ}}$
111	101.5
$\frac{11^{\circ}}{10^{\circ}}$	$\frac{10^{\circ}}{7^{\circ}}$ $\frac{9^{\circ}}{5^{\circ}}$ $\frac{8^{\circ}}{10^{\circ}}$
106.4	108.8
$\frac{5^{\circ}}{10^{\circ}}$	$\frac{2^{\circ}}{10^{\circ}}$
106.7	107.1
$\frac{4^{\circ}}{10^{\circ}}$	$\frac{7^{\circ}}{10^{\circ}}$
104.8	105.4
$\frac{6^{\circ}}{10^{\circ}}$	$\frac{6^{\circ}}{10^{\circ}}$

+ ~~A~~ ~~94.623~~ ~~96.411~~ - Eley. Eley. B.M.

Stake T.P. ~~A~~ 8.307 86.316
~~A~~ 4.121 90.437 10.177 86.234
~~A~~ 4.548 90.782

B.M. #124 ~~A~~ 1.293 89.144
~~A~~ 1.685 89.097 89.146

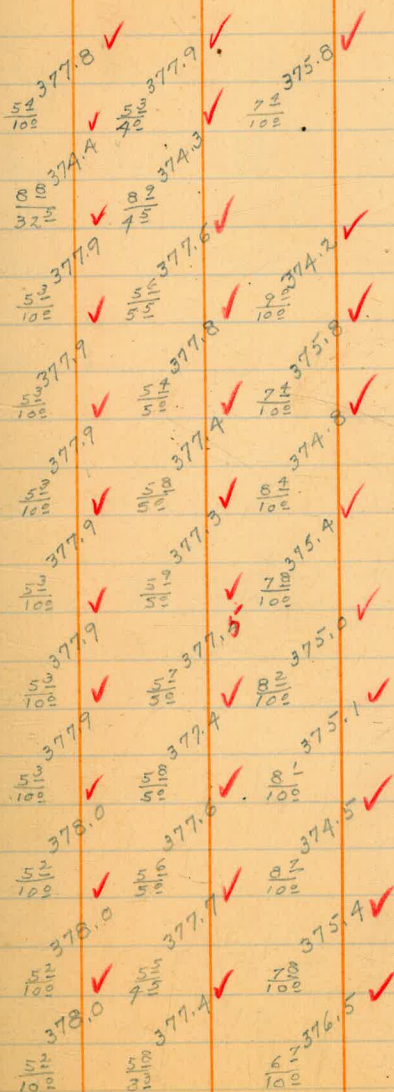
June-3. Relocation.

Simpson - Inst.
Isbell - Rod
Osborne - "

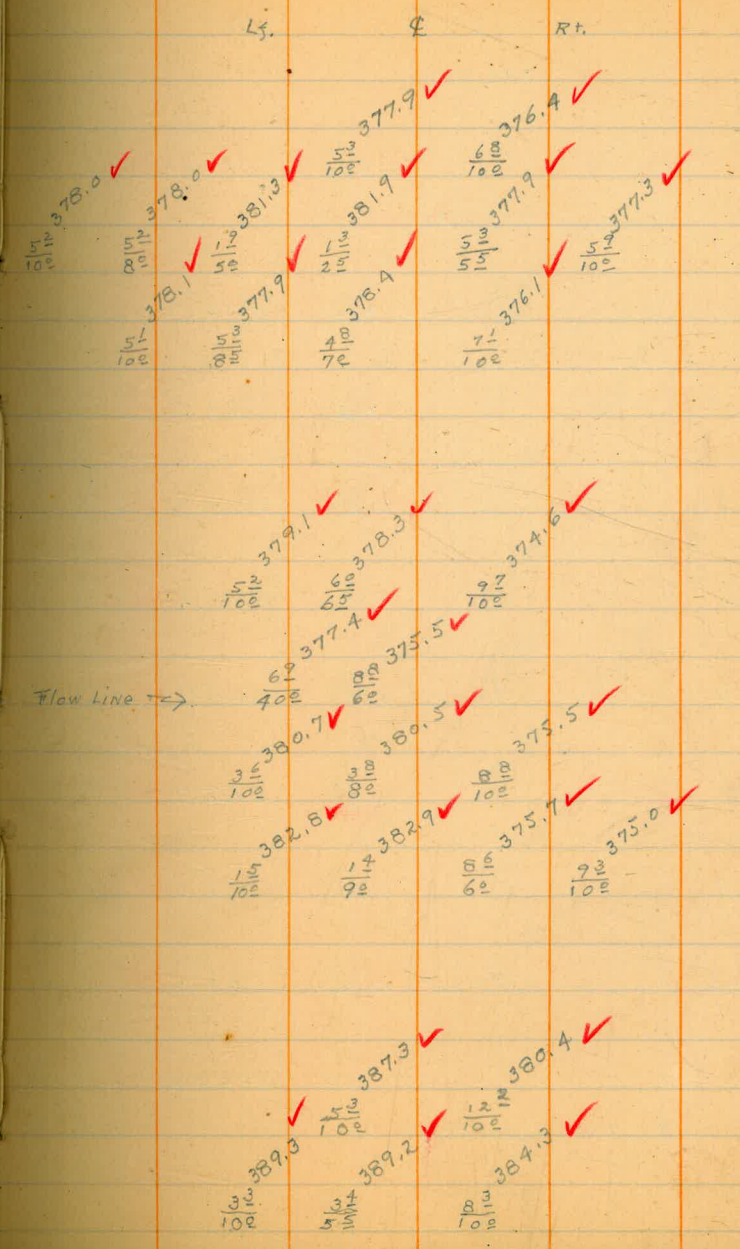
28

Sta	+	T	-	Elev.
	3.720	383.174		379.454 B.M. #55.
492+68L	B.C.		7.3	375.9
+85L	6'x2' Concrete Culvert.		8.9	374.3
+93L			8.2	375.6
493+18L			8.4	374.8
+43L			8.8	374.4
+68L			8.5	374.7
+93L			8.6	374.6
494+18L			8.3	374.9
+43L			7.9	375.3
+68L			7.4	375.8
+84L	E.C.		6.7	376.5

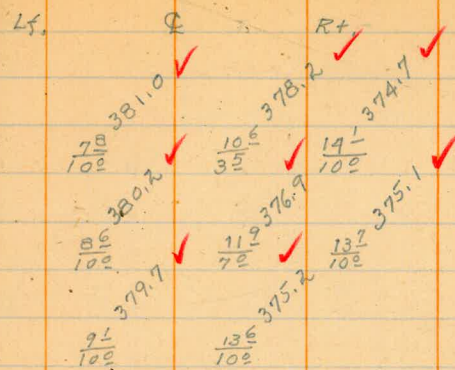
Flow Line →



Sta	+ π	- Elev.
		383.174
495+28.3	5.7	377.5 ✓
+60.8	2.2	381.0 ✓
496+00	6.6	376.6 ✓
T.P.	3.720	379.454 ✓
4.862	389.316 ✓	
497+00	9.1	375.2 ✓
+35. 12" Concrete Culvert.	8.3	376.0 ✓
498+00	8.2	376.1 ✓
499+00	6.7	377.6 ✓
T.P.	1.660	382.656 ✓
9.971	392.627 ✓	
500+00	9.3	383.3 ✓
501+00	6.0	386.6 ✓



Sta	+ x	-	Ele.
	388.834		
504 + 01 ²		10.0	378.8 ✓
+ 26 ³		11.0	377.8 ✓
504 + 33 ⁸ = 504 + 30 ³ E.C.		11.2	377.6 ✓
	3.488		385.346 ✓
9.108	394.454 ✓		
	12.048		382.406 ✓
1.274	383.680 ✓		
	9.915		373.765 ✓



Check on B.M. # 56 - Record Elev. - 373.757

June-3- Relocation.

Sta	+	T	-	Elev.
				336.713
	2.720	339.433	✓	
642+00	P.I.	4.7		334.7 ✓
643+00		4.3		335.1 ✓
	T.P.	4.657		334.776 ✓
	5.407	340.183	✓	
644+00		4.7		335.5 ✓
645+00		4.7		335.5 ✓
646+00		4.9		335.3 ✓
647+00		5.4		334.8 ✓
	T.P.	5.434		334.749 ✓
	4.414	339.163	✓	
648+00		4.9		334.3 ✓
649+00		5.1		334.1 ✓

B.M. # 73 - 640 + 60 - Pole # 72297



Row Tel. Poles 10' Ft.

Sta		T	Elev.	
		339.163		
649+85E	12" C.I.P. Culvert,	6.0	333.2 ✓	
650+00		5.6	333.6 ✓	
T.P. + B.M. #74	---	3.666	335.557 ✓	
	3.387	338.944 ✓		
651+00		5.1	333.8 ✓	
652+00		4.7	334.2 ✓	
653+00		4.2	334.7 ✓	
654+00		4.1	334.8 ✓	
654+25	P.I.	3.6	335.1 ✓	
T.P.		4.0.63	334.881 ✓	
	4.762	339.643 ✓		
655+00		4.1	335.5 ✓	
656+00		5.1	334.5 ✓	

Flow-Line.

332.6 ✓
332.3 ✓
334.9 ✓
334.9 ✓
333.8 ✓

$\frac{4.7}{100}$ $\frac{4.7}{100}$ $\frac{6.0}{100}$ $\frac{5.2}{100}$

Record Elev. 335.558

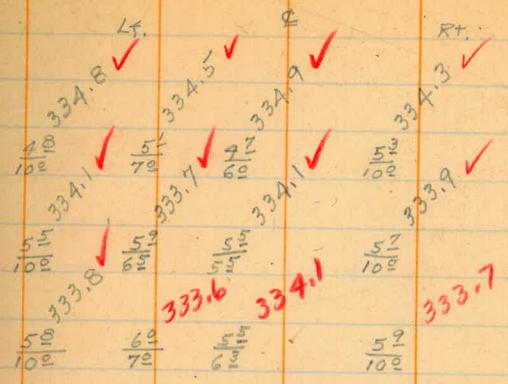
334.4 ✓
334.2 ✓
334.6 ✓
334.5 ✓
333.5 ✓
335.1 ✓
334.7 ✓
335.0 ✓
334.8 ✓
334.5 ✓
335.3 ✓
334.9 ✓
335.2 ✓
334.7 ✓
335.7 ✓
335.2 ✓
335.5 ✓
334.9 ✓
335.7 ✓
335.3 ✓
335.6 ✓
335.0 ✓

$\frac{4.4}{100}$ $\frac{4.2}{100}$ $\frac{4.7}{100}$ $\frac{5.2}{100}$ $\frac{5.1}{100}$ $\frac{4.4}{100}$ $\frac{4.2}{100}$ $\frac{4.7}{100}$ $\frac{5.2}{100}$ $\frac{5.1}{100}$ $\frac{4.4}{100}$ $\frac{4.2}{100}$ $\frac{4.7}{100}$ $\frac{5.2}{100}$ $\frac{5.1}{100}$ $\frac{4.4}{100}$ $\frac{4.2}{100}$ $\frac{4.7}{100}$ $\frac{5.2}{100}$ $\frac{5.1}{100}$

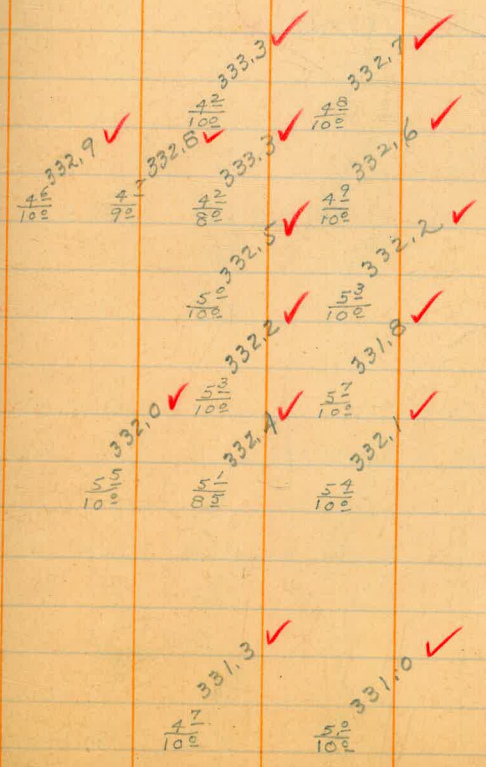
336.0 ✓
335.4 ✓
335.8 ✓
335.2 ✓
335.6 ✓
335.3 ✓
334.9 ✓
335.2 ✓
334.4 ✓
334.4 ✓

$\frac{5.6}{100}$ $\frac{4.7}{100}$ $\frac{5.3}{100}$ $\frac{4.2}{100}$ $\frac{4.7}{100}$ $\frac{5.2}{100}$ $\frac{4.7}{100}$ $\frac{4.2}{100}$ $\frac{5.2}{100}$

Sta.	+ T	- T	Elev.
			339.643
657+00		5.4	334.2 ✓
658+00		5.6	334.0 ✓
659+00		6.0	333.6 ✓
T.P. + B.M. # 75		4.372	335.271 ✓
	2.186		337.457 ✓
660+00		4.8	332.7 ✓
661+00		4.5	333.0 ✓
+ 50 P.I.		5.2	332.3 ✓
662+00		5.6	331.9 ✓
663+00		5.3	332.2 ✓
T.P.		5.420	332.037 ✓
	3.978		336.015 ✓
664+00		5.1	330.9 ✓



Record Elev. 335.271



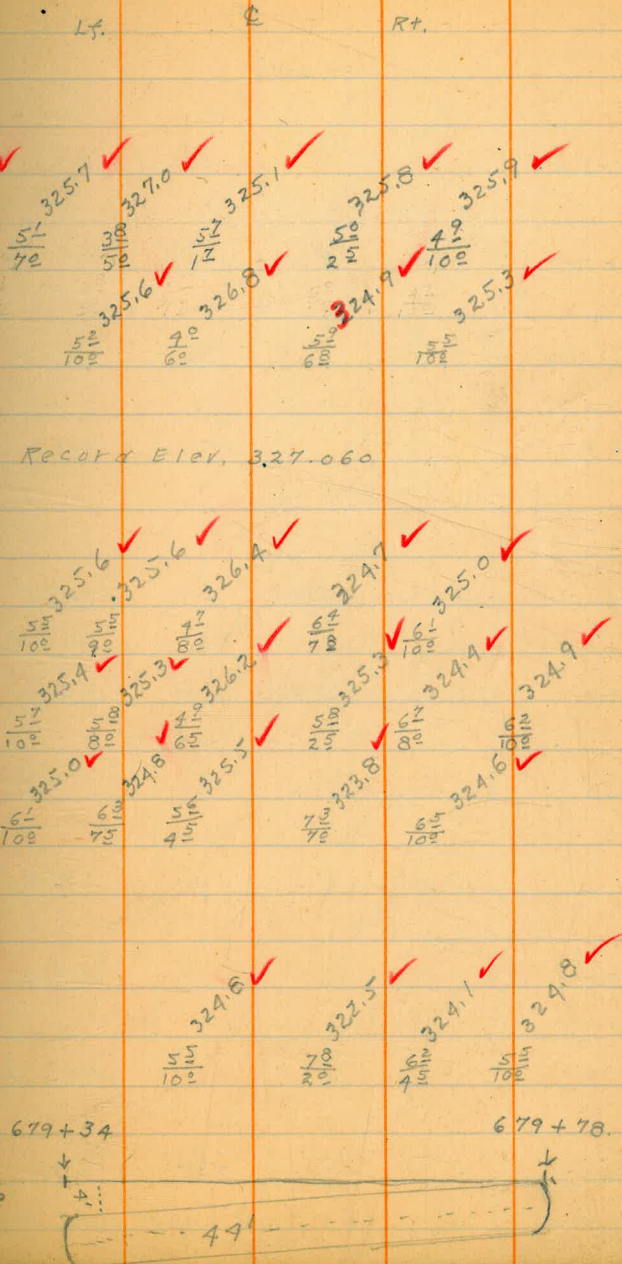
Sta	+ X	-	Elev.
		336.015	
665+00		5.4	330.6 ✓ 331.6
666+00		5.5	330.5 ✓ 331.5
667+00		5.9	330.1 ✓
T.P. + B.M. #76	3.308		332.707
	2.478	335.194 ✓	332.716 Record Elev.
668+00		5.6	329.6 ✓
669+00		6.9	328.3 ✓
670+00		7.4	327.8 ✓
T.P.	6.701		320.493 ✓
	3.593	332.086 ✓	
671+00		5.5	326.6 ✓
672+00		6.1	326.0 ✓
673+00		6.1	326.0 ✓

Lf.	Rt.
$\frac{5}{100}$	$\frac{5}{100}$
330.8 ✓	331.0 ✓
$\frac{5}{100}$	$\frac{5}{100}$
330.8 ✓	330.6 ✓
$\frac{5}{100}$	$\frac{5}{100}$
330.5 ✓	330.5 ✓
$\frac{5}{100}$	$\frac{5}{100}$
329.9 ✓	329.6 ✓
$\frac{5}{100}$	$\frac{5}{100}$
329.9 ✓	328.8 ✓
$\frac{6}{100}$	$\frac{6}{100}$
328.3 ✓	328.0 ✓
$\frac{6}{100}$	$\frac{6}{100}$
327.8 ✓	328.8 ✓
$\frac{7}{100}$	$\frac{7}{100}$
327.5 ✓	327.1 ✓
$\frac{7}{100}$	$\frac{7}{100}$
326.8 ✓	326.9 ✓
$\frac{5}{100}$	$\frac{5}{100}$
326.5 ✓	326.3 ✓
$\frac{5}{100}$	$\frac{5}{100}$
326.9 ✓	326.3 ✓

Sta	+	T	-	Elev.
		332.086		
T.P.			5.157	326.929 ✓
	3.862	330.791 ✓		
674+00			5.6	325.2 ✓
675+00			5.3	325.5 ✓
T.P. + B.M. #77			3.738	327.053 ✓ 327.060
	4.062	331.122 ✓		
676+00			6.0	325.1 ✓
677+00			6.0	325.1 ✓
678+00			6.3	325.8 324.8 ✓
T.P.			5.894	325.228 ✓
	5.042	330.270 ✓		
679+00			6.3	324.0 ✓
679+34			7.7	322.6 ✓
679+78			7.7	322.6 ✓

Flow Line
Culvert. →

16" concrete
Culvert.



June-4-

SIMPSON - Inst.
ISBELL - Rod
OSBORNE - "

CLEAR AND HOT.

Sta	+ T	- Elev.
	330.270	
679+34	5.1	325.2 ✓
679+78	7.2	323.1 ✓
	Center lines opposite culvert.	
680+00	5.8	324.5 ✓
T.P.	5.719	324.551 ✓
	3.829	328.380 ✓
680+35	4.1	324.3 ✓
+74	10.5	317.9 ✓
	opp 20' x 50' bridge	
+91	5.8	322.6 ✓
	West wing wall	
681+00	3.5	324.9 ✓
682+00	4.2	324.2 ✓
683+00	5.0	323.4 ✓
684+00	5.3	323.1 ✓
T.P. + B.M. #78	3.246	325.134 ✓

325.7 ✓	325.5 ✓	326.0 ✓	325.7 ✓	324.8 ✓	322.9 ✓	329.3 ✓	324.5 ✓
$\frac{7}{100}$	$\frac{8}{100}$	$\frac{4}{70}$	$\frac{4}{70}$	$\frac{6}{40}$	$\frac{7}{40}$	$\frac{6}{70}$	$\frac{5}{100}$
326.2 ✓	326.2 ✓	326.2 ✓	326.2 ✓	326.2 ✓	326.2 ✓	326.2 ✓	326.2 ✓
$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$
327.1 ✓	327.0 ✓	327.0 ✓	327.0 ✓	327.0 ✓	327.0 ✓	327.0 ✓	327.0 ✓
$\frac{13}{90}$	$\frac{14}{100}$	$\frac{14}{100}$	$\frac{14}{100}$	$\frac{14}{100}$	$\frac{14}{100}$	$\frac{14}{100}$	$\frac{14}{100}$
327.2 ✓	327.2 ✓	327.2 ✓	327.2 ✓	327.2 ✓	327.2 ✓	327.2 ✓	327.2 ✓
$\frac{9}{80}$	$\frac{9}{80}$	$\frac{9}{80}$	$\frac{9}{80}$	$\frac{9}{80}$	$\frac{9}{80}$	$\frac{9}{80}$	$\frac{9}{80}$
326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓
$\frac{12}{100}$	$\frac{12}{50}$	$\frac{12}{50}$	$\frac{12}{50}$	$\frac{12}{50}$	$\frac{12}{50}$	$\frac{12}{50}$	$\frac{12}{50}$
326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓	326.5 ✓
$\frac{6}{100}$	$\frac{6}{100}$	$\frac{6}{100}$	$\frac{6}{100}$	$\frac{6}{100}$	$\frac{6}{100}$	$\frac{6}{100}$	$\frac{6}{100}$
324.0 ✓	324.5 ✓	324.5 ✓	324.5 ✓	324.5 ✓	324.5 ✓	324.5 ✓	324.5 ✓
$\frac{7}{100}$	$\frac{7}{80}$	$\frac{7}{80}$	$\frac{7}{80}$	$\frac{7}{80}$	$\frac{7}{80}$	$\frac{7}{80}$	$\frac{7}{80}$
323.5 ✓	323.8 ✓	323.8 ✓	323.8 ✓	323.8 ✓	323.8 ✓	323.8 ✓	323.8 ✓
$\frac{7}{100}$	$\frac{7}{90}$	$\frac{7}{90}$	$\frac{7}{90}$	$\frac{7}{90}$	$\frac{7}{90}$	$\frac{7}{90}$	$\frac{7}{90}$
323.9 ✓	323.9 ✓	323.9 ✓	323.9 ✓	323.9 ✓	323.9 ✓	323.9 ✓	323.9 ✓
$\frac{4}{100}$	$\frac{4}{90}$	$\frac{4}{90}$	$\frac{4}{90}$	$\frac{4}{90}$	$\frac{4}{90}$	$\frac{4}{90}$	$\frac{4}{90}$
323.6 ✓	323.6 ✓	323.6 ✓	323.6 ✓	323.6 ✓	323.6 ✓	323.6 ✓	323.6 ✓
$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$	$\frac{7}{100}$

Top of Bridge → $\frac{13}{90}$
Flow line →

Record Elev. 325.129

Sta	+	T	-	Elev.
				325.129 - B.M. #78
	3.412	328.541 ✓		
685+00			5.3	323.2 ✓
686+00			5.0	323.5 ✓
687+00			4.9	323.6 ✓
T.P.			5.143	323.398 ✓
	6.491	329.889 ✓		
688+00			6.1	323.8 ✓
689+00			6.1	323.8 ✓
690+00			4.9	325.0 ✓
T.P.			5.094	324.795 ✓
	5.386	330.181 ✓		
691+00			5.9	324.3 ✓
692+00			5.6	324.6 ✓

Lf. R Rt.

				323.7 ✓	323.8 ✓	323.1 ✓
				$\frac{4.2}{100}$	$\frac{5.7}{100}$	
				324.1 ✓	323.5 ✓	
				$\frac{4.8}{100}$	$\frac{5.0}{100}$	
				324.4 ✓	323.6 ✓	
				$\frac{4.1}{100}$	$\frac{4.9}{100}$	
				324.9 ✓	324.0 ✓	
				$\frac{5.0}{100}$	$\frac{5.9}{100}$	
				325.1 ✓	324.3 ✓	324.5 ✓
				$\frac{4.8}{100}$	$\frac{5.6}{100}$	$\frac{5.7}{100}$
				325.3 ✓	324.1 ✓	324.3 ✓
				$\frac{4.9}{100}$	$\frac{5.8}{100}$	$\frac{5.6}{100}$
				325.0 ✓	325.0 ✓	
				$\frac{4.6}{90}$	$\frac{7.9}{100}$	
				325.3 ✓	325.5 ✓	324.4 ✓
				$\frac{4.7}{100}$	$\frac{5.8}{100}$	
				324.0 ✓	324.2 ✓	
				$\frac{4.2}{100}$	$\frac{5.0}{100}$	
				324.6 ✓	324.2 ✓	
				$\frac{4.0}{100}$	$\frac{5.0}{100}$	

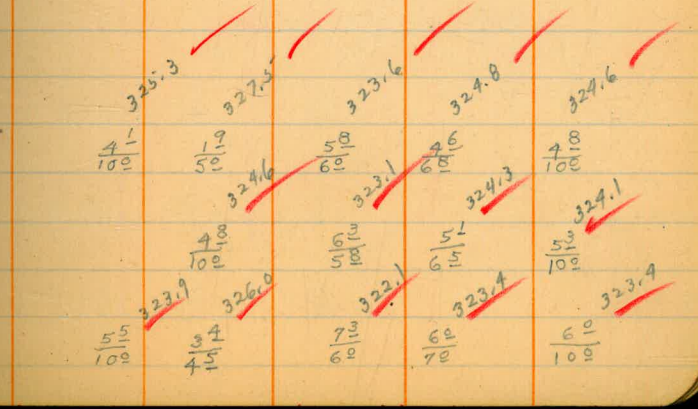
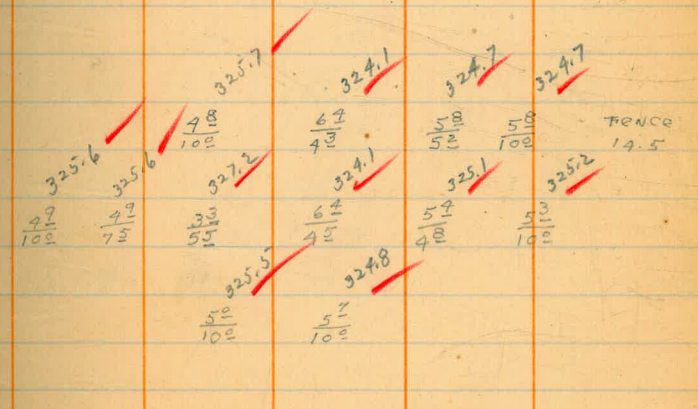
Sta	T	π	Elev.
		330.181	
692+39 ³⁰	B.C.	5.5	324.7 ✓
+64 ²		5.8	324.4 ✓
+89 ²		5.7	324.5 ✓
693+14 ²		5.2	325.0 ✓
+39 ²		5.3	324.9 ✓
+64 ²		5.6	324.6 ✓
+89 ²		4.7	325.5 ✓
694+08 ⁰⁰	E.C.	4.5	325.7 ✓
T.P. + B.M. #79		3.551	326.630 ✓ - 326.621 -
	3.933	330.554 ✓	
695+00		4.0	326.6 ✓

Left	Right
325.3	324.5
324.2	324.5
325.4	324.3
325.8	324.9
326.0	324.9
326.0	324.9
325.8	324.9
326.9	324.9
325.8	325.0
326.0	325.0
325.8	325.0
326.0	325.0
325.8	325.0
325.7	325.0
326.2	325.0
324.9	325.1
325.9	325.1
325.5	325.1
327.0	325.1
324.9	325.1
324.9	325.1
325.1	325.1

Record Elev. 326.621

Sta	+	T	-	Elev.
		330.554		
696+00			4.0	326.6
697+00			5.0	325.6
698+00			4.8	325.8
T.P.		5.473		325.081
	5.913	330.494		
699+00			5.5	325.0
700+00			4.8	325.7
701+00			5.3	325.2
T.P.		4.678		325.816
	3.602	329.418		
702+00			4.2	325.2
703+00			5.4	324.0
704+00			5.3	324.1

Ls.	Rt.
326.1	324.9
325.7	325.0
326.0	324.7
326.1	325.1
325.6	325.7
325.6	324.7
325.7	324.7
325.5	325.2
325.3	324.6
327.5	324.8
324.6	324.1
323.9	324.1
326.0	323.4



Sta	+	T	-	Elev.
				329.418
705+00			7.7	321.7 ✓
T.P. + B.M. # 80			4.140	325.278 ✓ 325.279
	1.524			326.803 ✓
706+00			6.1	320.7 ✓
+ 85 P.I.			6.6	320.2 ✓
707+00			6.6	320.2 ✓
708+00			7.2	319.6 ✓
T.P.			7.317	319.486 ✓
	4.736			324.222 ✓
709+00			5.3	318.9 ✓
710+00			5.9	318.3 ✓
711+00			6.6	317.6 ✓

L.S.	Q.	Rt.
323.8 $\frac{5.6}{100}$	324.6 $\frac{7.8}{100}$	321.0 $\frac{8.4}{60}$
321.7 $\frac{5.1}{140}$	324.3 $\frac{2.3}{80}$	320.1 $\frac{6.7}{60}$
321.2 $\frac{5.6}{140}$	322.4 $\frac{4.2}{80}$	321.4 $\frac{5.7}{80}$
321.0 $\frac{5.8}{110}$	321.8 $\frac{5.1}{100}$	320.7 $\frac{6.1}{90}$
320.2 $\frac{6.6}{160}$	320.0 $\frac{7.2}{75}$	320.5 $\frac{6.2}{100}$
319.6 $\frac{7.6}{100}$	319.4 $\frac{7.2}{75}$	320.6 $\frac{6.3}{100}$
319.1 $\frac{5.1}{100}$	319.6 $\frac{6.3}{100}$	317.9 $\frac{7.2}{100}$
318.4 $\frac{5.8}{100}$	317.2 $\frac{6.3}{100}$	317.2 $\frac{7.2}{100}$
317.6 $\frac{5.8}{100}$	316.2 $\frac{8.0}{100}$	316.2 $\frac{8.0}{100}$

Record Elev. - 325.279

Sta	+	T	-	Elev.
		324.222		
712+00		8.3		315.9 ✓
T.P.		6.587		317.635 ✓
	4.615	322.250	✓	
713+00		6.4		315.8 ✓
714+00		7.9		314.3 ✓
715+00		6.2		316.0 ✓
T.P. + B.M. # 81		3.539		318.711 ✓ — 318.699 —
	2.563	321.262	✓	
716+00		5.5		315.8 ✓
+27 ²⁸	B.C	5.7		315.6 ✓
+52 ²		5.8		315.5 ✓
+77 ²		6.2		315.1 ✓

L.S. C R.T.

317.6 ✓	317.8 ✓
$\frac{66}{100}$	$\frac{94}{100}$
317.2 ✓	317.0 ✓
$\frac{50}{100}$	$\frac{60}{100}$
316.8 ✓	315.4 ✓
$\frac{50}{100}$	$\frac{72}{100}$
317.2 ✓	315.1 ✓
$\frac{57}{100}$	$\frac{75}{100}$
316.8 ✓	312.2 ✓
$\frac{50}{100}$	$\frac{100}{100}$
317.2 ✓	313.7 ✓
$\frac{50}{100}$	$\frac{85}{100}$
316.6 ✓	315.0 ✓
$\frac{56}{100}$	$\frac{72}{100}$
316.6 ✓	316.7 ✓
$\frac{56}{100}$	$\frac{55}{100}$
316.6 ✓	316.9 ✓
$\frac{53}{100}$	

Record Elev. 318.699

316.9 ✓	315.4 ✓	316.6 ✓	316.5 ✓
$\frac{47}{100}$	$\frac{52}{100}$	$\frac{77}{100}$	$\frac{78}{100}$
316.4 ✓	315.2 ✓	316.4 ✓	316.4 ✓
$\frac{47}{100}$	$\frac{61}{100}$	$\frac{72}{100}$	$\frac{79}{100}$
316.3 ✓	315.1 ✓	316.5 ✓	316.5 ✓
$\frac{50}{100}$	$\frac{62}{100}$	$\frac{78}{100}$	$\frac{78}{100}$
316.4 ✓	316.4 ✓	316.2 ✓	
$\frac{47}{100}$	$\frac{77}{100}$	$\frac{51}{100}$	

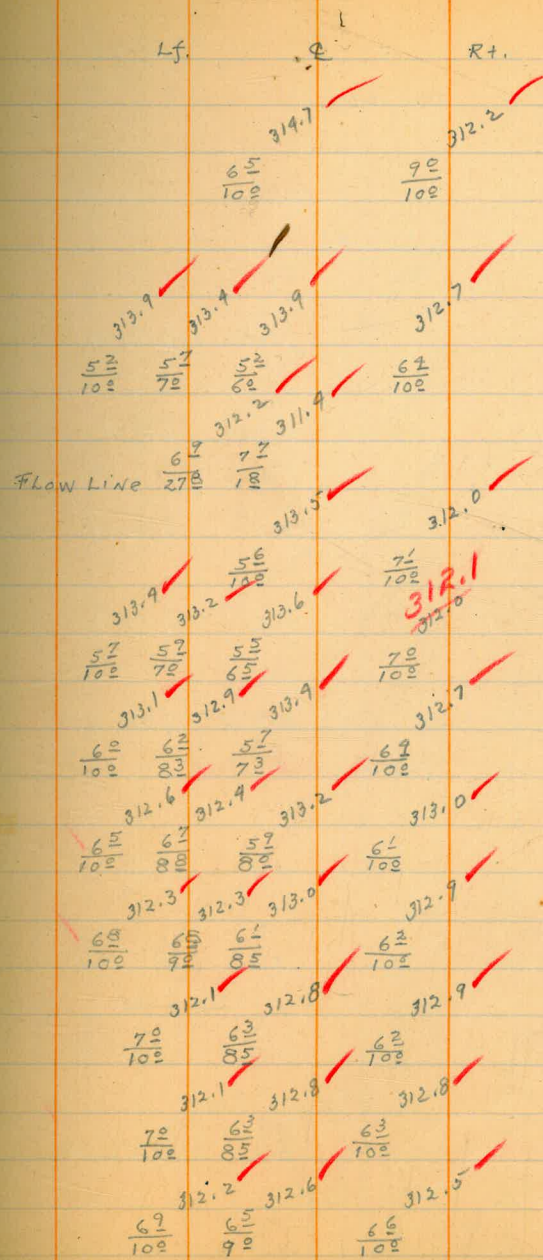
Sta	+	T	-	Elev.
		321.262		
717+02 Z			5.0	316.3 ✓
+27 Z			5.2	316.1 ✓
+52 Z			5.4	315.9 ✓
+77 Z			5.5	315.8 ✓
718+02 Z			5.5	315.8 ✓
+210 Z	E.S.		5.6	315.7 ✓
719+00			5.8	315.5 ✓
T.P		5.332		315.930 ✓
	4.288	320.218		✓
720+00			5.5	314.7 ✓
721+00			6.3	313.9 ✓
+45 S	24" C.I.P. Culvert	9.1		311.1

Lf.	±	Rt.
	316.2 ✓	315.3 ✓
$\frac{5.1}{100}$	$\frac{6.0}{20}$	$\frac{5.5}{100}$
	316.1 ✓	315.5 ✓
$\frac{5.7}{100}$	$\frac{5.7}{100}$	$\frac{5.8}{100}$
	315.9 ✓	315.6 ✓
$\frac{5.7}{100}$	$\frac{5.7}{20}$	$\frac{5.7}{60}$
	315.7 ✓	316.2 ✓
$\frac{5.7}{100}$	$\frac{5.6}{65}$	$\frac{5.7}{20}$
	315.8 ✓	316.2 ✓
$\frac{5.5}{100}$	$\frac{5.8}{20}$	$\frac{5.7}{100}$
	315.9 ✓	315.5 ✓
$\frac{5.4}{100}$	$\frac{5.6}{30}$	$\frac{5.7}{100}$
	315.9 ✓	316.1 ✓
$\frac{5.7}{100}$	$\frac{5.6}{30}$	$\frac{6.6}{100}$
	315.6 ✓	315.7 ✓
$\frac{5.7}{100}$	$\frac{5.9}{75}$	$\frac{5.6}{70}$
	315.6 ✓	315.7 ✓
	315.7 ✓	315.1 ✓
	315.0 ✓	314.7 ✓
	315.0 ✓	315.1 ✓
	315.0 ✓	314.5 ✓
	314.3 ✓	313.8 ✓
	311.2 ✓	311.0 ✓
Flow Line →	$\frac{9.0}{29}$	$\frac{9.0}{13}$

Sta	+	T	-	Elev.
		320.218		
722+00			6.2	314.0 ✓
T.P.		5.634		314.584 ✓
	5.838	320.422 ✓		
723+00			5.9	314.5 ✓
724+00			5.4	315.0 ✓
725+00			5.6	314.8 ✓
+30	P.I.		5.4	315.0 ✓
T.P. + B.M.	# 82	3.038		317.384 ✓ - 317.376 -
	3.829	321.205 ✓		
726+00			5.4	315.8 ✓
727+00			5.6	315.6 ✓
728+00			5.5	315.7 ✓

L.F.	Q	R.T.
	314.7 ✓	314.5 ✓
$\frac{5.5}{100}$		$\frac{4.5}{100}$
315.5 ✓	315.2 ✓	313.9 ✓
$\frac{4.2}{100}$	$\frac{5.5}{100}$	$\frac{6.5}{100}$
315.0 ✓	315.5 ✓	314.3 ✓
$\frac{5.4}{62}$	$\frac{4.0}{7.5}$	$\frac{6.2}{100}$
315.1 ✓	315.1 ✓	314.5 ✓
$\frac{5.10}{100}$	$\frac{5.10}{100}$	$\frac{5.9}{100}$
315.3 ✓	315.3 ✓	314.8 ✓
$\frac{5.1}{100}$	$\frac{5.1}{100}$	
Record Elev. - 317.376		
316.0 ✓	315.5 ✓	314.8 ✓
$\frac{5.2}{100}$	$\frac{5.2}{7.0}$	$\frac{6.4}{100}$
316.3 ✓	315.5 ✓	315.1 ✓
$\frac{4.9}{100}$	$\frac{5.2}{5.0}$	$\frac{6.1}{100}$
315.9 ✓	315.3 ✓	315.7 ✓
$\frac{5.10}{100}$	$\frac{5.3}{4.0}$	$\frac{5.5}{3.5}$
315.9 ✓	315.3 ✓	314.9 ✓
		$\frac{6.3}{100}$

Sta	+	X	-	Elev.
		321.205		
729+00			8.1	313.1 ✓
T.P.			5.952	315.253 ✓
	3.838	319.091 ✓		
730+00			6.1	313.0 ✓
+09	18" C.I.P. Culvert.		7.2	314.9 ✓
+40 ±			6.5	312.6 ✓
+65 ±			6.2	312.9 ✓
+90 ±			6.0	313.1 ✓
731+15 ±			6.1	313.0 ✓
+40 ±			6.1	313.0 ✓
+65 ±			6.4	312.7 ✓
+69 ±	E.C.		6.7	312.4 ✓
732+00			7.3	311.8 ✓



Sta	+ T	- T	Elev.
		319.091	
T.P.		6.993	312.098 ✓
	5.078	317.176 ✓	
733+00		7.2	310.0 ✓
734+00		5.3	311.9 ✓
735+00		5.1	312.1 ✓
736+00		7.3	309.9 ✓
T.P. + B.M. # 83		6.766	310.410 ✓
	2.492	312.902 ✓	
737+00		4.8	308.1 ✓
738+00		5.8	307.1 ✓
739+00		7.3	305.6 ✓
+60	8" C.I.P. Culvert,	7.9	305.0 ✓
740+00		7.6	305.3 ✓

Lf.	Rt.
311.6 ✓	312.2 ✓
$\frac{5.6}{100}$	$\frac{8.2}{100}$
311.3 ✓	312.3 ✓
$\frac{5.9}{100}$	$\frac{5.7}{100}$
311.5 ✓	311.3 ✓
$\frac{4.2}{100}$	$\frac{5.7}{100}$
311.1 ✓	311.9 ✓
$\frac{6.1}{100}$	$\frac{5.3}{100}$
310.9 ✓	309.9 ✓
$\frac{6.8}{100}$	$\frac{7.3}{100}$
Rec'd Elev. 310.410	
307.1 ✓	305.5 ✓
$\frac{5.0}{100}$	$\frac{7.2}{100}$
306.5 ✓	308.0 ✓
$\frac{6.7}{100}$	$\frac{7.2}{100}$
307.3 ✓	306.7 ✓
$\frac{5.5}{100}$	$\frac{6.0}{100}$
305.8 ✓	305.5 ✓
$\frac{7.1}{100}$	$\frac{7.4}{100}$
305.3 ✓	306.1 ✓
$\frac{7.5}{100}$	$\frac{6.0}{100}$
304.9 ✓	304.9 ✓
$\frac{6.0}{100}$	$\frac{7.4}{100}$
305.9 ✓	305.1 ✓
$\frac{8.5}{27.3}$	$\frac{8.0}{33}$
306.6 ✓	306.7 ✓
$\frac{7.0}{100}$	$\frac{7.0}{40}$
305.3 ✓	$\frac{6.0}{70}$
$\frac{7.0}{100}$	$\frac{6.2}{100}$

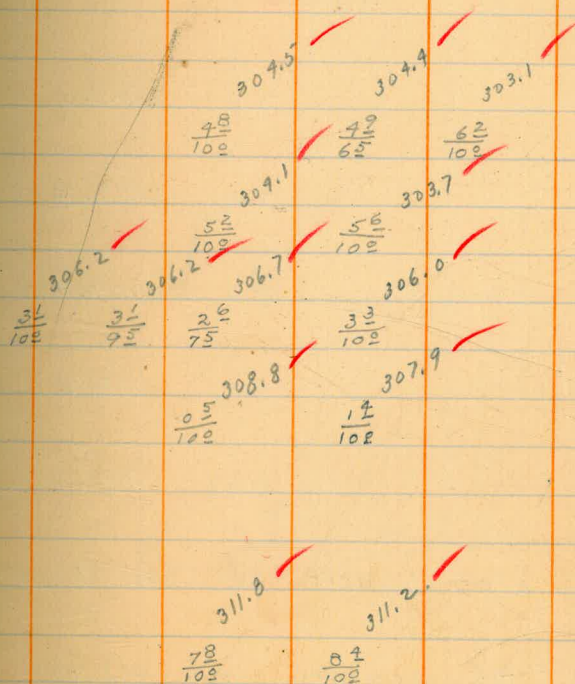
Flow Line →

Sta	+ /	X	-	Elev.
		312.902		
T.P.		6.681		306.221 ✓
	6.816	313.037 ✓		
741+00		5.8		307.2 ✓
742+00		4.6		308.4 ✓
743+00	P.I.	4.8		308.2 ✓
744+00		5.9		307.1 ✓
T.P.		5.201		307.836 ✓
	3.089	309.925 ✓		
745+00		4.3		305.6 ✓
746+00		6.2		303.7 ✓
747+00		6.6		303.3 ✓
748+00		6.2		303.7 ✓
+85	P.I.	6.1		303.8 ✓

Lf.	C	Rt.
	307.9 ✓	307.9 ✓
$\frac{56}{100}$	308.3 ✓	310.2 ✓
$\frac{47}{100}$	308.6 ✓	310.5 ✓
$\frac{47}{100}$	308.6 ✓	311.1 ✓
$\frac{47}{100}$	307.3 ✓	311.2 ✓
$\frac{57}{100}$	307.9 ✓	310.9 ✓
$\frac{57}{100}$	307.7 ✓	310.5 ✓
$\frac{71}{100}$	305.5 ✓	309.7 ✓
$\frac{71}{100}$	303.8 ✓	309.7 ✓
$\frac{61}{100}$	302.3 ✓	308.1 ✓
$\frac{76}{100}$	303.5 ✓	308.1 ✓
$\frac{59}{100}$	307.0 ✓	305.3 ✓
$\frac{59}{100}$	304.5 ✓	302.5 ✓
$\frac{54}{100}$	307.1 ✓	302.5 ✓
$\frac{54}{100}$	304.2 ✓	302.1 ✓
$\frac{59}{100}$	307.1 ✓	302.7 ✓
$\frac{59}{100}$	304.1 ✓	302.7 ✓
$\frac{58}{100}$	307.1 ✓	302.8 ✓
$\frac{58}{100}$	304.1 ✓	302.8 ✓

Sta	+	X	-	Elev.
		309.925		
T.P. + B.M. # 84			3.836	306.089 ✓ 306.095
	3.197	309.292 ✓		
7 749+00			5.0	304.3 ✓
7 750+00			5.3	304.0 ✓
7 751+00			3.3	306.0 ✓
7 752+00			1.7	307.6 ✓
T.P.			1.790	307.502 ✓
	12.071	319.573 ✓		
7 753+00			8.9	310.7 ✓
7 754+00			4.6	313.0 ✓
7 754+04 ²¹ P.I			4.5	315.1 ✓
7 755+00			3.7	315.9 ✓
7 756+00			4.1	315.5 ✓

Record Elev. 306.095.



Sta	+ T	-	Elev.
	319.573		
T.P.		3.352	316.221 ✓
	2.587	318.808 ✓	
757+00		4.4	314.4 ✓
758+00		5.6	313.2 ✓
+71	24" concrete culvert.	9.4	309.4 ✓
759+00		5.6	313.2 ✓
760+00		6.7	312.1 ✓
760+01	18" C.I. P. culvert.	6.9	311.9 ✓
T.P. + B.M. # 85		1.385	317.423 ✓ -317.442-
	6.201	323.643 ✓	
761+00		7.2	316.4 ✓
762+00		5.7	317.9 ✓
763+00		6.5	317.1 ✓

Lf.	±	Rt.
	310.8	310.1
Flow Line →	$\frac{80}{276}$	$\frac{87}{76}$
	312.6	311.5
Flow Line →	$\frac{63}{295}$	$\frac{73}{35}$
Record Elev.		317.442

Sta	+ T -	Elev.
	323.643	
763+49	5.5	318.1 ✓
764+00	3.2	320.4 ✓
+40	2.1	321.5 ✓
+75	5.1	318.5 ✓
765+00	5.1	318.5 ✓
+75	13" C.I.P. Culvert, 4.3	319.3 ✓
T.P.	2.748	320.895 ✓
	8.911	329.806 ✓
766+00	10.1	319.7 ✓
767+00	3.1	326.7 ✓
768+00	1.4	328.4 ✓
T.P.	1.368	328.438 ✓
	8.255	336.693 ✓

Lt. R Rt.
 320.1 ✓ 319.3 ✓
 Flow Line → $\frac{3.5}{298}$ $\frac{4.3}{38}$

Sta	+ T -	Elev.
	336.693	
769+00	7.4	329.3 ✓
+80 P.I.	3.9	332.0 ✓
770+00	2.9	333.8 ✓
T.P. + B.M. #86	2.696	333.997 ✓ 333.989
	7.585	341.574 ✓
771+00 P.I.	4.3	337.3 ✓
771+42	3.9	337.7 ✓
772+00	5.0	336.6 ✓
773+00	8.7	332.9 ✓
+88 12" C.I.P. Culvert.	11.7	329.9 ✓
T.P.	7.908	333.666 ✓
	3.868	337.534 ✓
774+00	7.3	330.2 ✓

Lf. 0 Rt.

Record Elev. - 333.989

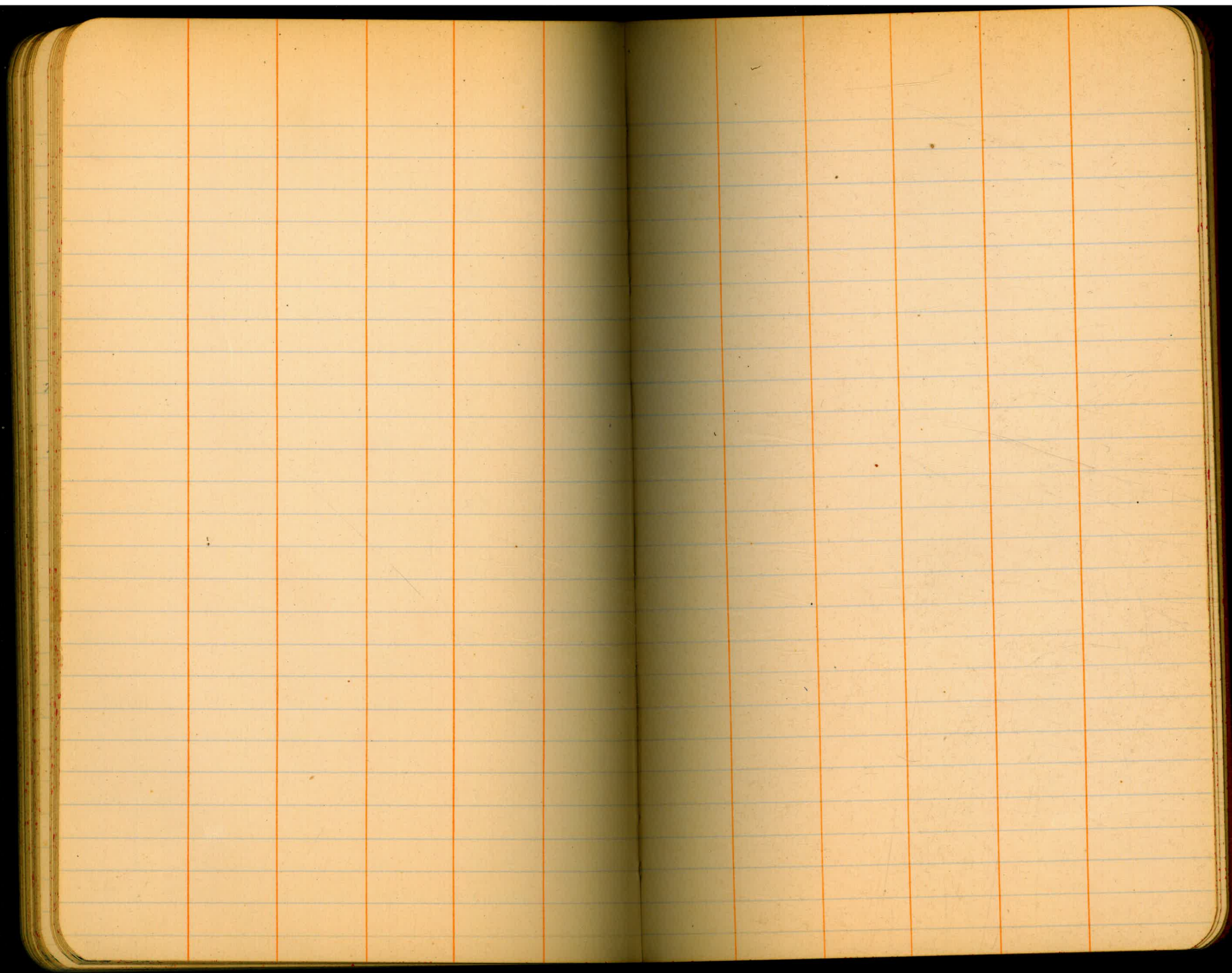
Flow Line \Rightarrow $\frac{331.2}{10\frac{1}{2}}$ $\frac{11\frac{1}{2}}{6\frac{1}{2}}$ 330.0

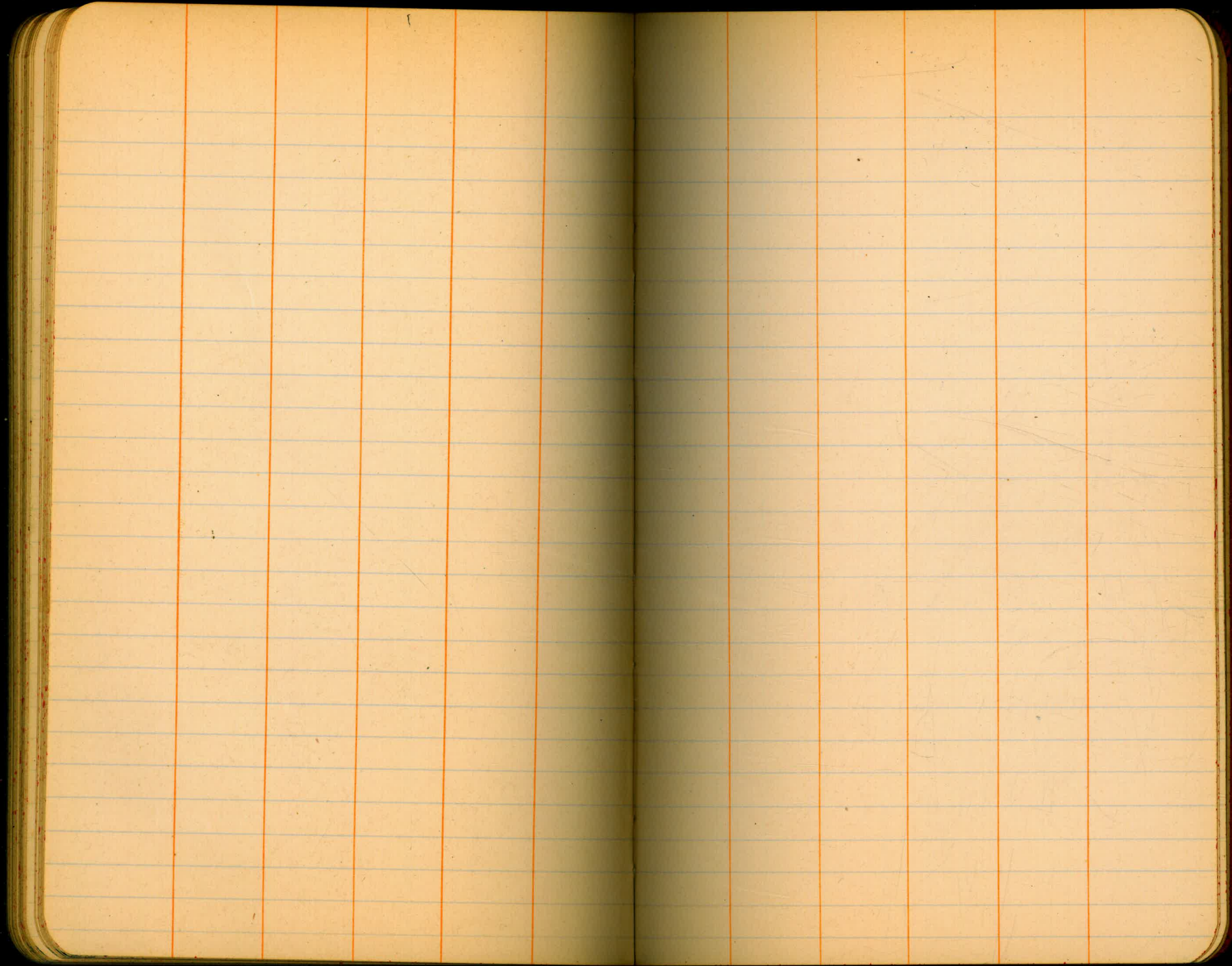
Sta	+	∓	-	Elev.
				337.534
775+00			5.2	332.3 ✓
776+00			4.3	333.2 ✓
777+00			2.7	334.8 ✓
T.P.			3.024	334.510 ✓
	7.716			342.226 ✓
778+00			6.2	336.0 ✓
779+00			4.7	337.5 ✓
780+00			2.6	339.6 ✓
T.P. + B.M. #87			0.771	341.455 ✓ - 341.454 -
	8.530			349.984 ✓
781+00			8.0	342.0 ✓
782+00			4.7	346.3 ✓

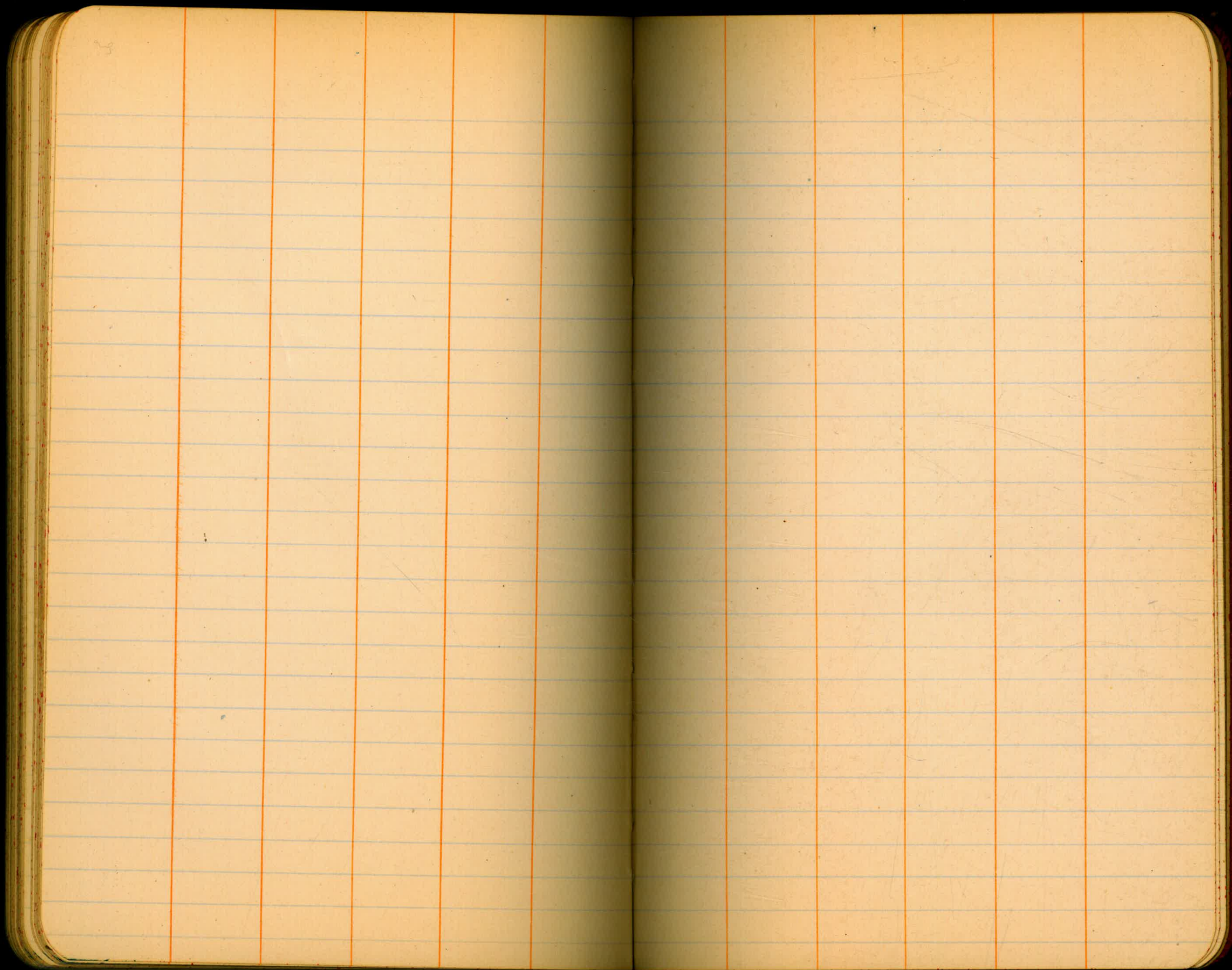
Record Elev. 341.454

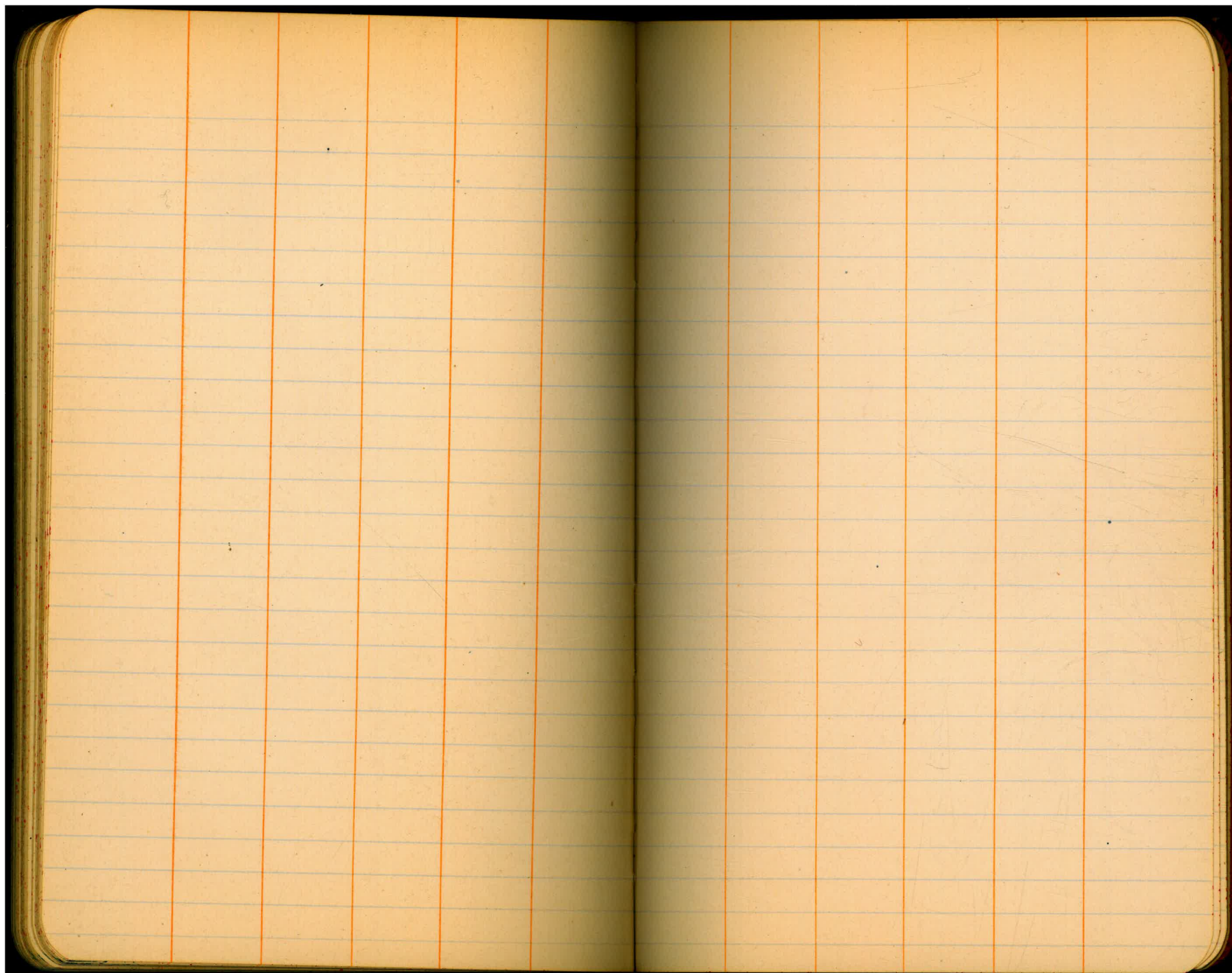
Sta	+	X	-	Elev.
		349.984		
783+00			5.0	345.0 ✓
784+00			6.4	348.6 ✓
T.P.		4.325		345.659 ✓
	7428	353.087 ✓		
785+00			7.9	345.2 ✓
786+00			6.0	347.1 ✓
787+00			4.0	349.1 ✓
788+00			2.6	350.5 ✓
T.P.		1.610		351.477 ✓
	6.609	358.086 ✓		
789+00			5.4	352.7 ✓
+40 P.I.			5.6	352.5 ✓
B.M. #88		5.326		352.760 ✓

Record Elev. 352.754









#55 379.454 Sta. 495+82. 9' L

#56 373.757 Nail in R.R. Tie.
Sta. 506+08 35' R

#57 375.360 Pole # 72413
Sta. 509+57 18' L

#58 365.469 Pole # 72410.
514+90. 10' R.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

IMPROVED TABLES

AND **INFORMATION**

level estimate the difference in elevation between the side stake and lower target by this amount if cut, elevate if fill. Add this amount to cut at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given T may be found by dividing tangent (or external) opposite T by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

322.422
317.384
31.038

348.284
6.923
342.443
347.281

317.176
6.766
310.410
349.383
6.923
342.460

342.445
321.128
1.164

309.925
3836
306.089
332.197
9.035
324.162

328.106
3.730
324.376
3.61

345.218
8866
336.352

322.250
3.539
318.711

330.791
3.738
327.053



1.660

4.792
5.587
5.451
795

325.835
3.738
322.097

6.246

328.380
3.246
325.134

330.181
3.531
326.650

5.040
4.378
.662

4.889
6.62
4.227

354.020
353.970
0.050

332.354
8.2124
324.144

330.304
6.023
324.301

342.067
341.959
340.208

324.461
324.301
.160

89.146
89.097
49

330.314
5.999
324.315

276.007
8.097
267.910

318.808
1.355
317.453

345.028
4.570
240.458

329.418
4.140
325.278

317.442
131.423
10.19

198.598
743
.853

193.024
745
192.279

339.649
4.372
335.271

362.106
362.086
0.020

336.015
3.308
332.707



339.163
3.606
335.557