

EL CAPITAN  
Pipe Line Survey  
Levels & <sup>cross</sup> sections No. 11

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LEVEL BOOK

380

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W202

MICROFILMED

JAN 24 1965

MICROFILMED

JAN 24 1965

Party  
June 4, 1926

Reynolds T  
Anderson Rod  
Bichet "

Sta	+	-	Elev	B.M.	Recd Elev
1158+75					157.561
B.M. #15+	12.709	170.270 ✓			

Left      4      Right

1159+00

8.4      161.9 ✓

18' L on next  
Page

170.3  
 $\frac{0.2}{3.2}$  ✓

162.0 ✓  
 $\frac{8.2}{7.2}$

163.0 ✓  
 $\frac{7.2}{18.2}$

+02<sup>3</sup> B.C.

8.4      161.9 ✓

170.3  
 $\frac{0.2}{3.2}$  ✓

162.0 ✓  
 $\frac{8.2}{1.2}$

163.1 ✓  
 $\frac{7.2}{10.2}$

+27<sup>2</sup>

7.4      162.9 ✓

170.3  
 $\frac{0.2}{4.2}$  ✓

163.1 ✓  
 $\frac{16.2}{1.2}$

164.8 ✓  
 $\frac{16.2}{10.2}$

+52<sup>2</sup>

6.5      163.8 ✓

170.3  
 $\frac{0.2}{3.2}$  ✓

164.2 ✓  
 $\frac{6.1}{1.2}$

164.6 ✓  
 $\frac{5.2}{10.2}$

+77<sup>3</sup>

5.1      165.2 ✓

170.3  
 $\frac{0.2}{6.2}$  ✓

168.5 ✓  
 $\frac{1.8}{1.2}$

164.5 ✓  
 $\frac{5.8}{3.2}$

165.2 ✓  
 $\frac{5.1}{10.2}$

+83<sup>2</sup> E.C.

3.5      166.8 ✓

170.3  
 $\frac{0.2}{5.2}$  ✓

167.9 ✓  
 $\frac{2.2}{1.2}$

165.1 ✓  
 $\frac{5.2}{1.2}$

164.7 ✓  
 $\frac{5.6}{6.2}$

165.2 ✓  
 $\frac{5.1}{10.2}$

91<sup>2</sup>

2.2      168.1 ✓

170.3  
 $\frac{0.2}{4.2}$  ✓

167.8 ✓  
 $\frac{2.5}{1.2}$

163.0 ✓  
 $\frac{5.3}{2.2}$

165.3 ✓  
 $\frac{5.2}{10.2}$

1160+00

2.7      167.6 ✓

170.3  
 $\frac{0.2}{6.2}$  ✓

166.9 ✓  
 $\frac{3.2}{1.2}$

165.2 ✓  
 $\frac{5.1}{2.2}$

165.5 ✓  
 $\frac{4.8}{10.2}$

Sta +  $\pi$  - Elev BM

Left  $\&$  Right

170.270

1.057

149.213 ✓

11.715

180.928 ✓

1159+00

+02<sup>3</sup>BC

+273

+523

+773

+832 - E.C.

+913

1160+00

174.1 ✓

172.1 ✓

$\frac{68}{100}$

$\frac{89}{52}$

174.3 ✓

172.5 ✓

$\frac{64}{100}$

$\frac{84}{50}$

174.1 ✓

172.4 ✓

$\frac{68}{100}$

$\frac{85}{55}$

173.8 ✓

171.5 ✓

$\frac{71}{100}$

$\frac{94}{40}$

171.9 ✓

$\frac{92}{100}$

170.9 ✓

$\frac{102}{100}$

171.5 ✓

$\frac{94}{100}$

171.8 ✓

$\frac{81}{100}$

Sta	+	π	-	Elev.	B.M.	Left	♀	Right
				180.928				
1160+08			13.5	167.4	✓	$\begin{array}{r} 172.2 \\ 82 \\ \hline 102 \end{array}$	$\begin{array}{r} 169.2 \\ 112 \\ \hline 42 \end{array}$	$\begin{array}{r} 166.0 \\ 142 \\ \hline 32 \end{array}$ $\begin{array}{r} 165.2 \\ 152 \\ \hline 42 \end{array}$ $\begin{array}{r} 165.7 \\ 152 \\ \hline 102 \end{array}$
+29			11.4	169.5	✓	$\begin{array}{r} 171.3 \\ 92 \\ \hline 102 \end{array}$		$\begin{array}{r} 169.5 \\ 114 \\ \hline 22 \end{array}$ $\begin{array}{r} 165.6 \\ 152 \\ \hline 35 \end{array}$ $\begin{array}{r} 166.5 \\ 142 \\ \hline 102 \end{array}$
+43			11.1	169.8	✓	$\begin{array}{r} 171.0 \\ 99 \\ \hline 102 \end{array}$		$\begin{array}{r} 166.3 \\ 142 \\ \hline 25 \end{array}$ $\begin{array}{r} 166.9 \\ 142 \\ \hline 102 \end{array}$
+51			11.1	169.8	✓	$\begin{array}{r} 171.6 \\ 93 \\ \hline 102 \end{array}$		$\begin{array}{r} 166.7 \\ 142 \\ \hline 22 \end{array}$ $\begin{array}{r} 167.2 \\ 132 \\ \hline 102 \end{array}$
18" concrete curb +58			13.0	167.9	✓	$\begin{array}{r} 167.4 \\ 135 \\ \hline 102 \end{array}$	$\begin{array}{r} \text{Flow line} \\ 164.6 \\ 163 \\ \hline 13 \end{array}$	$\begin{array}{r} 167.8 \\ 134 \\ \hline 102 \end{array}$ $\begin{array}{r} \text{Flow line} \\ 163.3 \\ 172 \\ \hline 272 \end{array}$
+61			12.5	168.4	✓	$\begin{array}{r} 168.4 \\ 125 \\ \hline 102 \end{array}$		$\begin{array}{r} 168.4 \\ 125 \\ \hline 33 \end{array}$ $\begin{array}{r} 167.7 \\ 132 \\ \hline 102 \end{array}$
1161+06			12.6	168.3	✓	$\begin{array}{r} 176.0 \\ 42 \\ \hline 102 \end{array}$	$\begin{array}{r} 167.8 \\ 131 \\ \hline 22 \end{array}$	$\begin{array}{r} 168.9 \\ 122 \\ \hline 102 \end{array}$
+30			11.7	169.2	✓	$\begin{array}{r} 180.9 \\ 02 \\ \hline 102 \end{array}$	$\begin{array}{r} 171.6 \\ 92 \\ \hline 72 \end{array}$ $\begin{array}{r} 168.5 \\ 122 \\ \hline 42 \end{array}$	$\begin{array}{r} 169.7 \\ 112 \\ \hline 102 \end{array}$
+50			11.2	169.7	✓	$\begin{array}{r} 180.9 \\ 02 \\ \hline 102 \end{array}$	$\begin{array}{r} 171.4 \\ 95 \\ \hline 72 \end{array}$ $\begin{array}{r} 169.4 \\ 112 \\ \hline 42 \end{array}$	$\begin{array}{r} 170.0 \\ 102 \\ \hline 102 \end{array}$

Sta + T - Elev. BM.

Sta	T	Elev.	BM.
	180328		
1162+00	9.6	171.3	✓
+17' B.C.	9.6	171.3	✓
+42'	9.5	171.4	✓
+67'	8.1	172.8	✓
+92'	6.9	174.0	✓
+95' F.C.	6.8	174.1	✓
1163+00	6.6	174.3	✓
+50	5.3	175.6	✓
1164+00	3.5	177.4	✓

172.2 ✓ $\frac{180}{100}$	171.7 ✓ $\frac{92}{100}$
172.9 ✓ $\frac{80}{100}$	172.4 ✓ $\frac{85}{100}$
177.7 ✓ $\frac{32}{100}$	173.2 ✓ $\frac{72}{100}$
180.2 ✓ $\frac{07}{100}$	174.3 ✓ $\frac{64}{100}$
10' Later 180.9 ✓ $\frac{00}{70}$ 178.1 ✓ $\frac{28}{52}$	175.2 ✓ $\frac{52}{100}$
180.9 ✓ $\frac{00}{52}$ 176.9 ✓ $\frac{40}{40}$	175.4 ✓ $\frac{53}{20}$
180.9 ✓ $\frac{00}{32}$ 174.4 ✓ $\frac{62}{10}$	176.3 ✓ $\frac{44}{100}$
180.9 ✓ $\frac{00}{32}$ 175.5 ✓ $\frac{52}{10}$	<del>175.5</del> ✓ $\frac{54}{100}$
180.9 ✓ $\frac{00}{32}$ 178.4 ✓ $\frac{00}{10}$	177.0 ✓ $\frac{39}{100}$
180.9 ✓ $\frac{00}{10}$	178.4 ✓ $\frac{25}{100}$

Sta	+	π	-	Elev	BM
		180.928			
Rock TP.			0.793	180.135	✓
	11.955	192.090			✓

1162+92+

+95± B.C.

1163+00

+50

1164+00

+10 B.C.

+35

+60

133

160

106

178.8 ✓

181.1 ✓

181.5 ✓

182.7 ✓

$\frac{9.5}{10.2}$

182.6 ✓

$\frac{9.5}{10.2}$

183.6 ✓

$\frac{8.5}{10.2}$

184.1 ✓

$\frac{8.0}{10.2}$

189.1 ✓

$\frac{3.0}{10.2}$

189.9 ✓

$\frac{2.2}{10.2}$

10' Later 192.1 ✓

$\frac{0.2}{7.0}$

192.1 ✓

$\frac{0.2}{5.8}$

182.1 ✓

$\frac{10.0}{4.2}$

182.4 ✓

$\frac{9.2}{5.2}$

185.4 ✓

$\frac{6.2}{4.5}$

187.4 ✓

$\frac{4.2}{5.2}$

178.8 ✓

$\frac{13.3}{10.2}$

179.6 ✓

$\frac{12.5}{2.2}$

180.4 ✓

$\frac{11.2}{2.2}$

179.9 ✓

$\frac{12.2}{1.0.2}$

180.8 ✓

$\frac{11.3}{1.0.2}$

Sta	T	Elev	B.M.
	192.090		
+ 82 <sup>nd</sup> E.C.	10.4	181.7	✓
1165+00	10.3	181.8	✓
+17	10.3	181.8	✓
+50	9.0	183.1	✓
1166+00 B.C.	7.2	184.9	✓
+10	7.0	185.1	✓
41 CIP			
+18	6.9	185.2	✓
+20	6.9	185.2	✓
+30	6.4	185.7	✓

$$\begin{array}{r} 191.2 \\ 02 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 190.0 \\ 12 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 180.7 \\ 11 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 181.7 \\ 10 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 187.5 \\ 44 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 187.0 \\ 51 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 182.3 \\ 98 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 182.3 \\ 98 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 182.9 \\ 92 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 182.9 \\ 92 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 181.3 \\ 108 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 183.4 \\ 82 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 182.9 \\ 92 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 185.2 \\ 69 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 185.2 \\ 69 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 183.0 \\ 85 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 185.7 \\ 64 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 185.7 \\ 64 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 180.3 \\ 118 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 179.7 \\ 124 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 180.4 \\ 112 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 180.5 \\ 114 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 185.0 \\ 71 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 186.2 \\ 59 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 182.0 \\ 92 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 183.0 \\ 92 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 185.7 \\ 64 \\ \hline 102 \end{array}$$

$$\begin{array}{r} 186.7 \\ 54 \\ \hline 102 \end{array}$$



Sta	+	π	-	Elev	B.M.
		192.090			
+40			6.1	186.0	
+50			5.8	186.5	
+60			4.1	188.0	
+70			3.3	188.8	
T.P.			1.833	190.257	
	8.674	198.931			
			11.199	187.732	Record Elev 187.73
	11.199	198.935			
1164+35					
+60					
1166+80			9.7	189.2	

185.8 ✓	187.2 ✓
$\frac{62}{102}$	$\frac{49}{102}$
188.0 ✓	187.3 ✓
$\frac{44}{102}$	$\frac{42}{102}$
189.5 ✓	187.7 ✓
$\frac{22}{102}$	$\frac{42}{102}$
186.5 ✓	188.11 ✓
$\frac{54}{102}$	$\frac{42}{102}$
191.5 ✓	186.7 ✓
$\frac{06}{102}$	$\frac{54}{102}$
190.8 ✓	188.3 ✓
$\frac{13}{25}$	$\frac{32}{102}$
193.9 ✓	192.9 ✓
$\frac{52}{102}$	$\frac{62}{82}$
194.4 ✓	193.4 ✓
$\frac{45}{102}$	$\frac{55}{62}$
192.6 ✓	191.7 ✓
$\frac{63}{102}$	$\frac{72}{102}$
187.5 ✓	188.5 ✓
$\frac{112}{102}$	$\frac{104}{102}$

Sta + T Elev BM

198.935  
+90 8.8 190.1 ✓

1167+072 E.C. 8.3 190.6 ✓

1168+00 6.5 192.4 ✓

+50 5.0 193.9 ✓

1169+00 4.1 194.8 ✓

T.P. 1.835 197.100 ✓

10.872 207.972 ✓

1168+00

+50

1169+00

194.1 ✓  
 $\frac{48}{100}$   
192.2 ✓  
 $\frac{62}{20}$   
187.8 ✓  
 $\frac{111}{12}$   
188.8 ✓  
 $\frac{101}{100}$

196.8 ✓  
 $\frac{22}{100}$   
194.7 ✓  
 $\frac{42}{50}$   
193.8 ✓  
 $\frac{51}{15}$   
188.8 ✓  
 $\frac{101}{12}$   
189.5 ✓  
 $\frac{94}{100}$

198.9 ✓  
 $\frac{02}{65}$   
197.1 ✓  
 $\frac{18}{15}$   
193.0 ✓  
 $\frac{59}{100}$

198.9 ✓  
 $\frac{00}{52}$   
197.3 ✓  
 $\frac{14}{12}$   
194.5 ✓  
 $\frac{44}{100}$

198.9 ✓  
 $\frac{02}{12}$   
195.2 ✓  
 $\frac{32}{12}$   
196.3 ✓  
 $\frac{26}{100}$

199.9 ✓  
 $\frac{81}{100}$

200.5 ✓  
 $\frac{75}{100}$

202.2 ✓  
 $\frac{50}{100}$

Sta	T	Elev	RM
	207.972		
+43	10.7	197.3 ✓ <del>207.3</del>	
1170+00	9.4	198.6 ✓	
+06	9.0	199.0 ✓	
+17	8.2	199.8 ✓	
+32	7.7	200.3 ✓	
1171+00	5.4	202.6 ✓	
+593 B.C.	3.8	204.2 ✓	
T.P	16.28	206.344 ✓	
11.477	217.821 ✓		
1170+00			

204.2 ✓ $\frac{38}{102}$	202.4 ✓ $\frac{54}{24}$	197.5 ✓ $\frac{105}{12}$	198.2 ✓ $\frac{98}{102}$
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105.5 ✓ 208.0 ✓ $\frac{02}{92}$	205.8 ✓ 198.7 ✓ $\frac{93}{12}$	200.0 ✓ $\frac{82}{102}$
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208.0 ✓ $\frac{02}{72}$	205.7 ✓ $\frac{23}{22}$	201.2 ✓ $\frac{78}{102}$
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208.0 ✓ $\frac{02}{42}$	199.8 ✓ $\frac{82}{12}$	200.7 ✓ $\frac{73}{102}$
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208.0 ✓ $\frac{02}{33}$	200.4 ✓ $\frac{74}{05}$	201.1 ✓ $\frac{62}{102}$
----------------------------	----------------------------	-----------------------------

208.0 ✓ $\frac{02}{42}$	203.7 ✓ $\frac{43}{22}$	203.0 ✓ $\frac{52}{102}$
----------------------------	----------------------------	-----------------------------

208.0 ✓ $\frac{02}{22}$	204.3 ✓ $\frac{32}{15}$	204.6 ✓ $\frac{32}{102}$
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209.1 ✓ $\frac{82}{102}$
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Party Reynolds X  
 Junes. Anderson Rod  
 Clearwork Bicket Rod

Sta + T - Elev BM

217.821

+06

+17

+32

1171+00

+593 B.C.

morning June 5.

T.P.

4.001

213.828 ✓

4.065 217.885 ←

+843

13.2

204.7 ✓

1172+093

12.6

205.3 ✓

18" C.I.P.

+103

12.3

205.6 ✓

208.8 ✓  
 $\frac{90}{100}$

210.6 ✓  
 $\frac{78}{100}$

213.3 ✓  
 $\frac{45}{100}$

215.6 ✓  
 $\frac{22}{100}$

217.7 ✓  
 $\frac{01}{100}$

214.6 ✓  
 $\frac{33}{42}$

216.0 ✓  
 $\frac{12}{100}$

212.5 ✓  
 $\frac{52}{55}$

204.7 ✓  
 $\frac{132}{100}$

211.3 ✓  
 $\frac{66}{100}$

207.6 ✓  
 $\frac{103}{26}$

210.7 ✓  
 $\frac{73}{100}$

204.0 ✓  
 $\frac{139}{12}$

205.2 ✓  
 $\frac{122}{100}$

206.0 ✓  
 $\frac{112}{100}$

206.1 ✓  
 $\frac{112}{100}$

204.1 ✓  
 flow time  
 $\frac{1384}{23}$

Sta + T - Elev. BM

		217.885	
+343	12.4	205.5 ✓	
+593	11.4	206.5 ✓	
+70 <sup>±</sup> E.C.	10.9	207.0 ✓	
+85	8.9	209.0 ✓	
1173+00	9.2	208.7 ✓	
+50	8.1	209.8 ✓	
+92 <sup>±</sup> B.C.	6.7	211.2 ✓	
1174+022	7.2	210.7 ✓	
+122	6.8	211.1 ✓	

213.8 ✓ 209.5 ✓ 206.9 ✓ 206.9 ✓

$\frac{41}{102}$	$\frac{84}{32}$	$\frac{112}{22}$	$\frac{112}{102}$
217.7 ✓	216.2 ✓	206.7 ✓	207.7 ✓
$\frac{02}{102}$	$\frac{12}{52}$	$\frac{112}{15}$	$\frac{102}{102}$
217.8 ✓	216.4 ✓	209.9 ✓	208.1 ✓
$\frac{02}{102}$	$\frac{15}{62}$	$\frac{82}{32}$	$\frac{98}{102}$
217.9 ✓	209.9 ✓	208.1 ✓	208.7 ✓
$\frac{02}{65}$	$\frac{82}{32}$	$\frac{98}{22}$	$\frac{92}{102}$
217.9 ✓	208.6 ✓	209.1 ✓	
$\frac{02}{65}$	$\frac{92}{32}$	$\frac{82}{102}$	
217.9 ✓	216.7 ✓	210.2 ✓	
$\frac{02}{52}$	$\frac{12}{32}$	$\frac{72}{102}$	
217.9 ✓	210.5 ✓	211.5 ✓	
$\frac{02}{22}$	$\frac{74}{32}$	$\frac{64}{102}$	
217.9 ✓	210.7 ✓	211.8 ✓	
$\frac{02}{22}$	$\frac{72}{22}$	$\frac{64}{102}$	
217.9 ✓	211.3 ✓	212.2 ✓	
$\frac{02}{22}$	$\frac{62}{12}$	$\frac{52}{102}$	

Sta	+	X	Elev	BM
		217.885		
+223		4.1	211.8 ✓	
+294 E.C.		5.3	212.6 ✓	
+79		4.8	213.1 ✓	
1175+00		4.3	213.6 ✓	
T.P.		4065	213.820 ✓	
12328		226.148 ✓		
1172+85				
1173+00				
+50				
+922 B.C.				

$$\begin{array}{r} 217.9 \checkmark \\ 00 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 211.5 \checkmark \\ 60 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 212.3 \checkmark \\ 50 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 217.9 \checkmark \\ 00 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 211.8 \checkmark \\ 60 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 212.5 \checkmark \\ 50 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 214.8 \checkmark \\ 30 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 213.5 \checkmark \\ 40 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 215.5 \checkmark \\ 20 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 214.2 \checkmark \\ 30 \\ \hline 80 \end{array}$$

$$\begin{array}{r} 214.0 \checkmark \\ 30 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 220.4 \checkmark \\ 50 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 219.9 \checkmark \\ 60 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 219.5 \checkmark \\ 60 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 219.5 \checkmark \\ 60 \\ \hline 100 \end{array}$$

Sta + π - Elev BM

226.148

+ 022

+ 122

+ 222

+ 292 E.C.

1175+50

11.2 214.9 ✓

1176+00

10.0 216.1 ✓

+ 13

9.2 216.9 ✓

+ 50

7.1 219.0 ✓

+ 77

6.7 219.4 ✓

220.6 ✓  
 $\frac{55}{102}$

220.9 ✓    219.3 ✓  
 $\frac{52}{102}$      $\frac{62}{42}$

220.6 ✓    218.9 ✓  
 $\frac{55}{102}$      $\frac{72}{35}$

220.0 ✓    217.9 ✓  
 $\frac{64}{102}$      $\frac{82}{32}$

219.8 ✓    217.6 ✓    215.6 ✓    215.6 ✓  
 $\frac{63}{102}$      $\frac{85}{22}$      $\frac{105}{52}$      $\frac{105}{102}$

223.8 ✓    221.3 ✓    216.6 ✓    216.7 ✓    217.3 ✓  
 $\frac{23}{102}$      $\frac{48}{32}$      $\frac{95}{12}$      $\frac{94}{32}$      $\frac{82}{102}$

224.7 ✓    222.7 ✓    217.1 ✓    217.4 ✓    217.8 ✓  
 $\frac{14}{102}$      $\frac{34}{52}$      $\frac{90}{12}$      $\frac{82}{32}$      $\frac{83}{102}$

226.1 ✓    219.6 ✓    218.6 ✓    219.2 ✓  
 $\frac{00}{52}$      $\frac{65}{12}$      $\frac{75}{32}$      $\frac{60}{102}$

226.1 ✓    219.1 ✓    220.1 ✓  
 $\frac{00}{22}$      $\frac{70}{32}$      $\frac{60}{102}$

Party { Reynolds K  
Anderson Red  
Bichet }

Sta	x	T	Elev. B.M.
			226.148
1177+80		3.9	222.2 ✓
+20		4.8	221.3 ✓
+34 <sup>2</sup> B.C.		5.1	221.0 ✓
12" C.M.A. +43 <sup>2</sup>		4.7	221.4 ✓
+57 <sup>2</sup>		4.6	221.5 ✓
+80 <sup>2</sup> E.C.		4.0	222.1 ✓
T.P.		0.792	225.356 ✓
12.305			237.661 ✓
#156 B.M. 50 Monday morn. June 7.		10.768	226.893 ✓ 226.870
12.312			239.182 ✓

226.1 ✓ $\frac{0e}{3e}$	223.4 ✓ $\frac{2e}{2e}$	220.4 ✓ $\frac{5e}{4e}$	220.7 ✓ $\frac{5e}{10e}$
226.1 ✓ $\frac{0e}{4e}$	221.2 ✓ $\frac{4e}{10e}$		
225.8 ✓ $\frac{0e}{10e}$	223.4 ✓ $\frac{2e}{2e}$	221.5 ✓ $\frac{4e}{10e}$	
220.3 ✓ Flow Line $\frac{5e}{1e}$		219.4 Flow Line $\frac{6e}{2e}$	
225.6 ✓ $\frac{0e}{10e}$		222.2 $\frac{3e}{10e}$	
226.1 ✓ $\frac{0e}{4e}$	225.5 $\frac{0e}{2e}$	222.7 $\frac{3e}{10e}$	



Sta + T - Elev BM

239.182

1176+50

+77

1177+00

+20

+80<sup>4</sup>E.C.

1178+00

+30

+42<sup>B</sup>B.C.

+69<sup>3</sup>

16.4

15±

13.9

14.2

222.8 ✓

223.8 ✓

225.3 ✓

225.0 ✓

227.4 ✓  
 $\frac{118}{102}$

230.7 ✓  
 $\frac{85}{102}$

230.2 ✓  
 $\frac{92}{102}$

227.8 ✓  
 $\frac{11±}{102}$

226.3 ✓  
 $\frac{129}{52}$

229.5 ✓  
 $\frac{92}{52}$

229.0 ✓  
 $\frac{102}{45}$

226.7 ✓  
 $\frac{125}{42}$

227.6 ✓  
 $\frac{116}{100}$

229.5 ✓  
 $\frac{92}{102}$

228.0 ✓  
 $\frac{112}{32}$

222.9 ✓  
 $\frac{163}{02}$

229.6 ✓  
 $\frac{94}{102}$

227.5 ✓  
 $\frac{112}{32}$

229.5 ✓  
 $\frac{92}{102}$

228.1 ✓  
 $\frac{11±}{22}$

229.7 ✓  
 $\frac{95}{102}$

228.0 ✓  
 $\frac{112}{22}$

223.7 ✓  
 $\frac{160}{102}$

224.0 ✓  
 $\frac{152}{102}$

224.2 ✓  
 $\frac{150}{102}$

224.9 ✓  
 $\frac{143}{102}$

Sta	+	π	-	Elev	BM
				239.182	
+95±	E.C.		13.7	225.5 ✓	
1179+00			13.2	226.0 ✓	
+50			11.1	228.1 ✓	
+60			8.6	230.6 ✓	
1180+00			9.6	229.6 ✓	
+50			8.4	230.8 ✓	
+60			8.2	231.0 ✓	
1181+00			9.2	230.0 ✓	
+46±	B.C.		8.0	231.2 ✓	

230.9 ✓ $\frac{83}{102}$	229.7 ✓ $\frac{95}{32}$	225.4 ✓ $\frac{138}{102}$
232.2 ✓ $\frac{70}{102}$	230.1 ✓ $\frac{91}{25}$	225.3 ✓ $\frac{139}{12}$
225.4 ✓ $\frac{138}{102}$		
234.6 ✓ $\frac{40}{102}$	232.9 ✓ $\frac{63}{28}$	226.6 ✓ $\frac{124}{15}$
226.8 ✓ $\frac{72}{102}$		
235.7 ✓ $\frac{35}{102}$	<del>233.6</del> $\frac{54}{25}$	227.0 ✓ $\frac{122}{12}$
227.1 ✓ $\frac{121}{102}$		
235.8 ✓ $\frac{34}{102}$	232.5 ✓ $\frac{62}{22}$	227.7 ✓ $\frac{115}{22}$
227.9 ✓ $\frac{113}{102}$		
236.8 ✓ $\frac{22}{102}$	234.2 ✓ $\frac{52}{32}$	228.4 ✓ $\frac{108}{22}$
229.1 ✓ $\frac{101}{102}$		
230.2 ✓ $\frac{90}{102}$	226.6 ✓ $\frac{124}{28}$	229.0 ✓ $\frac{103}{15}$
229.4 ✓ $\frac{98}{102}$		
238.0 ✓ $\frac{12}{102}$	235.1 ✓ $\frac{41}{32}$	230.4 ✓ $\frac{88}{102}$
237.0 ✓ $\frac{22}{102}$	235.2 ✓ $\frac{40}{25}$	231.4 ✓ $\frac{78}{102}$

S+2 + T - Elev. BM

239.182  
 +71± 6.7 232.5 ✓  
 +96± 7.8 231.4 ✓  
 1182±21± 6.3 232.9 ✓

#  
 B.M. 156 226.670

12.746 239.636 ✓  
 B.M. 157 5.242 234.394 234.389 ✓  
 12.703 247.092 ✓

12" C.I.P.  
 +36± 14.3 232.8 ✓

+46± 14.1 233.0 ✓

+71± 13.7 233.4 ✓

+96± 13.6 234.1 ✓

237.1 ✓  
 $\frac{21}{102}$   
 233.4 ✓  
 $\frac{58}{05}$   
 231.0 ✓  
 $\frac{82}{02}$   
 231.8 ✓  
 $\frac{74}{102}$

236.7 ✓  
 $\frac{25}{102}$   
 234.7 ✓  
 $\frac{45}{22}$   
 232.1 ✓  
 $\frac{71}{102}$

236.6 ✓  
 $\frac{26}{102}$   
 234.9 ✓  
 $\frac{43}{42}$   
 232.2 ✓  
 $\frac{70}{12}$   
 232.5 ✓  
 $\frac{62}{102}$

233.8 ✓  
 $\frac{132}{102}$   
 232.9 ✓  
 $\frac{142}{52}$   
 231.4 ✓  
 $\frac{152}{02}$   
 232.7 ✓  
 $\frac{142}{102}$   
 230.8 ✓  
 $\frac{162}{232}$

236.8 ✓  
 $\frac{102}{102}$   
 235.6 ✓  
 $\frac{115}{32}$   
 233.2 ✓  
 $\frac{132}{102}$

236.7 ✓  
 $\frac{102}{102}$   
 234.7 ✓  
 $\frac{122}{12}$   
 233.7 ✓  
 $\frac{132}{102}$

237.8 ✓  
 $\frac{92}{102}$   
 236.3 ✓  
 $\frac{102}{32}$   
 234.5 ✓  
 $\frac{126}{102}$

Sta	T	Elev	B.M.
	247.092		
1183 +21±	12.5	234.6 ✓	
+46±	12.4	234.7 ✓	
+57± E.C.	12.1	235.0 ✓	
1184 +00	11.2	235.9 ✓	
+45	9.8	237.3 ✓	
455	5.4	241.7 ✓	
+65± B.C.	4.1	243.0 ✓	
+75±	3.8	243.3 ✓	
+85±	4.6	242.5 ✓	

239.3 ✓ $\frac{70}{100}$	236.6 ✓ $\frac{105}{150}$	235.1 ✓ $\frac{120}{100}$
238.3 ✓ $\frac{80}{100}$	236.4 ✓ $\frac{102}{150}$	235.6 ✓ $\frac{115}{100}$
	234.9 ✓ $\frac{122}{150}$	
	236.9 ✓ $\frac{103}{100}$	235.8 ✓ $\frac{113}{100}$
240.3 ✓ $\frac{60}{100}$	238.0 ✓ $\frac{91}{150}$	236.9 ✓ $\frac{102}{100}$
	236.1 ✓ $\frac{110}{150}$	
243.5 ✓ $\frac{36}{100}$	242.8 ✓ $\frac{43}{150}$	238.1 ✓ $\frac{90}{100}$
246.2 ✓ $\frac{02}{100}$	242.7 ✓ $\frac{44}{150}$	237.6 ✓ $\frac{95}{150}$
		238.2 ✓ $\frac{82}{100}$
	247.1 ✓ $\frac{00}{100}$	237.9 ✓ $\frac{92}{150}$
		238.4 ✓ $\frac{82}{100}$
	247.1 ✓ $\frac{00}{100}$	243.0 ✓ $\frac{41}{150}$
		238.2 ✓ $\frac{82}{150}$
		238.6 ✓ $\frac{85}{100}$
	246.6 ✓ $\frac{05}{100}$	242.3 ✓ $\frac{48}{150}$
		238.5 ✓ $\frac{86}{150}$
		238.7 ✓ $\frac{84}{100}$

Sta	+	T	-	Elek. BM
		247.092		
+95 <sup>±</sup>		6.0	241.1 ✓	
1185+05 <sup>±</sup>		6.9	240.2 ✓	
+15 <sup>±</sup>		7.2	239.9 ✓	
+25 <sup>±</sup>		7.4	239.7 ✓	
+35 <sup>±</sup>		7.8	239.3 ✓	
+45 <sup>±</sup>		7.8	239.3 ✓	
+55 <sup>±</sup>		7.1	240.0 ✓	
+582 E.C.		7.2	239.9 ✓	
36" C.I.P. +699		6.3	240.8 ✓	

246.0 ✓ $\frac{11}{100}$	244.8 ✓ $\frac{23}{50}$	241.6 ✓ $\frac{55}{20}$	238.7 ✓ $\frac{84}{50}$	238.8 ✓ $\frac{83}{100}$
244.5 ✓ $\frac{24}{100}$	241.0 ✓ $\frac{61}{35}$	239.0 ✓ $\frac{81}{100}$		
243.4 ✓ $\frac{32}{100}$	241.1 ✓ $\frac{60}{55}$	239.2 ✓ $\frac{79}{100}$		
	241.8 ✓ $\frac{53}{100}$	239.5 ✓ $\frac{76}{100}$		
	240.2 ✓ $\frac{69}{100}$	239.7 ✓ $\frac{74}{100}$		
	238.0 ✓ $\frac{91}{100}$	239.9 ✓ $\frac{73}{100}$		
237.6 ✓ $\frac{95}{100}$	238.3 ✓ $\frac{80}{40}$	240.0 ✓ $\frac{74}{100}$		
237.0 ✓ $\frac{101}{100}$	237.4 ✓ $\frac{92}{50}$	240.0 ✓ $\frac{71}{100}$		
	238.6 ✓ $\frac{85}{40}$	240.0 ✓ $\frac{71}{100}$		
235.2 ✓ $\frac{113}{100}$	234.9 ✓ $\frac{123}{42}$	239.4 ✓ $\frac{72}{38}$	240.2 ✓ $\frac{69}{100}$	233.6 ✓ $\frac{135}{295}$

Sta + N - Elev BM

247.092

1186+00 6.5 240.6 ✓

240.6 ✓  
 $\frac{65}{100}$

241.1 ✓  
 $\frac{60}{100}$

T.P. 0.352 246.740 ✓

12.952 259.692 ✓

1186+19 18.5 241.2 ✓

244.8 ✓  
 $\frac{140}{100}$

244.2 ✓  
 $\frac{155}{85}$

241.7 ✓  
 $\frac{180}{80}$

241.7 ✓  
 $\frac{180}{100}$

+37 17.3 242.4 ✓

249.7 ✓  
 $\frac{100}{100}$

247.2 ✓  
 $\frac{130}{80}$

244.0 ✓  
 $\frac{150}{100}$

242.7 ✓  
 $\frac{170}{100}$

+58 13.3 246.4 ✓

254.8 ✓  
 $\frac{40}{100}$

250.7 ✓  
 $\frac{90}{80}$

242.6 ✓  
 $\frac{170}{100}$

243.3 ✓  
 $\frac{160}{100}$

+75<sup>0</sup> B.C. 14.8 244.9 ✓

255.4 ✓  
 $\frac{40}{100}$

252.9 ✓  
 $\frac{60}{40}$

250.6 ✓  
 $\frac{90}{30}$

243.5 ✓  
 $\frac{160}{100}$

243.9 ✓  
 $\frac{150}{100}$

+93<sup>-</sup> 15.2 244.3 ✓

256.8 ✓  
 $\frac{80}{100}$

254.1 ✓  
 $\frac{50}{50}$

249.4 ✓  
 $\frac{100}{40}$

244.5 ✓  
 $\frac{150}{100}$

244.9 ✓  
 $\frac{140}{100}$

1187+10<sup>0</sup> E.C. 13.8 245.9 ✓

258.1 ✓  
 $\frac{10}{100}$

255.4 ✓  
 $\frac{40}{40}$

244.9 ✓  
 $\frac{140}{100}$

245.4 ✓  
 $\frac{140}{100}$

Sta	+	π	-	Elev
		259.692		
1187+33 <sup>2</sup>		13.1		246.6 ✓
+50		12.5		247.2 ✓
+67		13.3		246.4 ✓
T.P.		4.040		255.652 ✓

11475 267.327 ✓

+66		20.9		246.4 ✓
+92 <sup>2</sup> B.C.		19.8		247.5 ✓
1188+172		19.1		248.2 ✓
+42 <sup>2</sup>		18.0		249.3 ✓

259.4 ✓  
 $\frac{0^2}{10^2}$

256.6 ✓  
 $\frac{3^2}{5^2}$

254.6 ✓  
 $\frac{5^2}{4^2}$

245.3 ✓  
 $\frac{14^2}{0^2}$

246.5 ✓  
 $\frac{13^2}{10^2}$

259.6 ✓  
 $\frac{0^2}{10^2}$

256.5 ✓  
 $\frac{3^2}{4^2}$

245.8 ✓  
 $\frac{13^2}{0^2}$

247.0 ✓  
 $\frac{12^2}{10^2}$

258.6 ✓  
 $\frac{1^2}{10^2}$

256.6 ✓  
 $\frac{3^2}{5^2}$

247.5 ✓  
 $\frac{12^2}{10^2}$

258.9 ✓  
 $\frac{8^2}{10^2}$

256.3 ✓  
 $\frac{11^2}{4^2}$

247.5 ✓  
 $\frac{19^2}{10^2}$

259.9 ✓  
 $\frac{7^2}{10^2}$

257.3 ✓  
 $\frac{10^2}{5^2}$

248.6 ✓  
 $\frac{18^2}{10^2}$

261.7 ✓  
 $\frac{5^2}{10^2}$

258.7 ✓  
 $\frac{8^2}{5^2}$

249.8 ✓  
 $\frac{17^2}{10^2}$

263.3 ✓  
 $\frac{4^2}{10^2}$

261.5 ✓  
 $\frac{5^2}{7^2}$

249.5 ✓  
 $\frac{17^2}{1^2}$

250.8 ✓  
 $\frac{16^2}{10^2}$

Sta	+ T -	Elev
	267.327	
1188+69 <sup>5</sup> EC	16.7	250.6 ✓
1189+00	14.6	252.7 ✓
+82	13.2	254.1 ✓
+90	12.7	254.6 ✓
+50	12.7	254.6 ✓
+75	11.7	255.6 ✓
+90	10.6	256.7 ✓
1190+00	10.5	256.8 ✓

L	¢	R+
264.3 ✓ $\frac{3^2}{10^2}$	262.7 ✓ $\frac{4^2}{6^2}$	251.7 ✓ $\frac{15^2}{10^2}$
265.7 ✓ $\frac{1^2}{10^2}$	263.4 ✓ $\frac{3^2}{6^2}$	252.8 ✓ $\frac{14^2}{10^2}$
264.7 ✓ $\frac{2^2}{10^2}$	262.9 ✓ $\frac{4^2}{7^2}$	252.8 ✓ $\frac{14^2}{10^2}$
265.2 ✓ $\frac{2^2}{10^2}$	261.9 ✓ $\frac{5^2}{5^2}$	253.9 ✓ $\frac{13^2}{10^2}$
263.7 ✓ $\frac{3^2}{10^2}$	262.5 ✓ $\frac{4^2}{4^2}$	254.9 ✓ $\frac{12^2}{10^2}$
265.1 ✓ $\frac{2^2}{10^2}$	263.0 ✓ $\frac{4^2}{4^2}$	256.1 ✓ $\frac{11^2}{10^2}$
264.6 ✓ $\frac{2^2}{10^2}$	258.7 ✓ $\frac{8^2}{1^2}$	256.4 ✓ $\frac{10^2}{10^2}$
264.2 ✓ $\frac{3^2}{10^2}$	261.5 ✓ $\frac{5^2}{3^2}$	257.1 ✓ $\frac{10^2}{10^2}$
262.1 ✓ $\frac{5^2}{4^2}$	259.7 ✓ $\frac{7^2}{1^2}$	257.5 ✓ $\frac{9^2}{10^2}$



Reynolds  
Painty Anderson Road  
June 6 (Sick)

Sta	+	T	-	Elev
		267.327		
1190+43			5.5	261.8 ✓
T.P.		2988		264.333 ✓
	11.868	276.207		True morning
1190+43				
+48		15.4		260.8 ✓ <del>276.8</del>
+49		16.1		260.1 ✓
+60		15.9		260.3 ✓
+70		15.6		260.6 ✓
+93		14.5		261.7 ✓
+95		11.4		264.8 ✓

H	E	Rt.
267.3 ✓ $\frac{0^{\circ}}{7^{\circ}}$	265.3 ✓ $\frac{2^{\circ}}{5^{\circ}}$	264.8 ✓ $\frac{2^{\circ}}{3^{\circ}}$
258.5 ✓ $\frac{0^{\circ}}{1^{\circ}}$	259.5 ✓ $\frac{7^{\circ}}{10^{\circ}}$	
269.2 ✓ $\frac{7^{\circ}}{10^{\circ}}$	267.5 ✓	
270.4 ✓ $\frac{5^{\circ}}{10^{\circ}}$	<del>267.5</del>	258.9 ✓ $\frac{17^{\circ}}{1^{\circ}}$
270.5 ✓ $\frac{5^{\circ}}{10^{\circ}}$	267.9 ✓ $\frac{8^{\circ}}{6^{\circ}}$	259.7 ✓ $\frac{16^{\circ}}{10^{\circ}}$
266.5 ✓ $\frac{9^{\circ}}{10^{\circ}}$	263.6 ✓ $\frac{12^{\circ}}{5^{\circ}}$	258.9 ✓ $\frac{17^{\circ}}{1^{\circ}}$
271.4 ✓ $\frac{18^{\circ}}{10^{\circ}}$	269.6 ✓ $\frac{12^{\circ}}{5^{\circ}}$	259.7 ✓ $\frac{16^{\circ}}{10^{\circ}}$
272.1 ✓ $\frac{4^{\circ}}{10^{\circ}}$	267.8 ✓ $\frac{14^{\circ}}{3^{\circ}}$	260.7 ✓ $\frac{15^{\circ}}{10^{\circ}}$
272.5 ✓ $\frac{3^{\circ}}{10^{\circ}}$	261.7 ✓ $\frac{15^{\circ}}{1^{\circ}}$	260.4 ✓ $\frac{15^{\circ}}{10^{\circ}}$
		259.5 ✓ $\frac{16^{\circ}}{1^{\circ}}$
		270.4 ✓ $\frac{15^{\circ}}{10^{\circ}}$
		260.7 ✓ $\frac{15^{\circ}}{10^{\circ}}$
		262.0 ✓ $\frac{14^{\circ}}{10^{\circ}}$
		260.7 ✓ $\frac{15^{\circ}}{1^{\circ}}$
		262.1 ✓ $\frac{14^{\circ}}{10^{\circ}}$

Sta	+	T	Elev	Box
		276.207		
1181+00		10.7	265.5 ✓	
+18		11.9	264.3 ✓	
+29		13.2	263.0 ✓	
+50		13.2	263.0 ✓	
1192+00		10.4	265.8 ✓	
+35		9.0	267.2 ✓	
+36		10.1	266.1 ✓	
+45B		10.1	266.1 ✓	
+71		8.1	268.1 ✓	

272.8 ✓ $\frac{34}{102}$	261.0 ✓ $\frac{152}{12}$	262.4 ✓ $\frac{138}{102}$
273.1 ✓ $\frac{31}{102}$	269.9 ✓ $\frac{62}{52}$	261.5 ✓ $\frac{142}{12}$
272.8 ✓ $\frac{34}{102}$	269.2 ✓ $\frac{70}{32}$	267.3 ✓ $\frac{139}{102}$
273.2 ✓ $\frac{32}{102}$	266.7 ✓ $\frac{95}{22}$	263.7 ✓ $\frac{125}{102}$
272.8 ✓ $\frac{32}{102}$	268.4 ✓ $\frac{78}{62}$	264.6 ✓ $\frac{112}{102}$
269.5 ✓ $\frac{62}{102}$	267.9 ✓ $\frac{83}{52}$	266.4 ✓ $\frac{98}{102}$
274.7 ✓ $\frac{15}{102}$	269.3 ✓ $\frac{62}{92}$	267.7 ✓ $\frac{85}{102}$
269.8 ✓ $\frac{64}{102}$	269.1 ✓ $\frac{71}{82}$	267.4 ✓ $\frac{88}{12}$
276.2 ✓ $\frac{0268}{6255}$	268.0 ✓ $\frac{82}{32}$	267.9 ✓ $\frac{83}{102}$
269.4 ✓ $\frac{88}{32}$	266.7 ✓ $\frac{95}{22}$	266.2 ✓ $\frac{102}{15}$
267.4 ✓ $\frac{88}{32}$	267.0 ✓ $\frac{92}{12}$	267.9 ✓ $\frac{83}{22}$
		268.3 ✓ $\frac{72}{102}$
		269.3 ✓ $\frac{62}{102}$

S+T + T - Elev BM.

276.207

T.P. 0.948 275.259 ✓

12.337 287.596 ✓

1192+71

1193+60

19.1 268.5 ✓

+12

15.7 271.9 ✓

+25

14.6 273.0 ✓

+50

12.6 275.0 ✓

+82

13.8 273.8 ✓

1194+00

13.0 274.6 ✓

278.6 ✓  
 $\frac{9^{\circ}}{10^{\circ}}$

279.1 ✓  $\frac{8^{\circ}}{10^{\circ}}$  271.8 ✓  $\frac{15^{\circ}}{12^{\circ}}$  268.7 ✓  $\frac{18^{\circ}}{12^{\circ}}$  269.8 ✓  $\frac{17^{\circ}}{2^{\circ}}$  270.6 ✓  $\frac{17^{\circ}}{10^{\circ}}$

281.5 ✓  $\frac{6^{\circ}}{10^{\circ}}$  277.7 ✓  $\frac{9^{\circ}}{5^{\circ}}$  269.6 ✓  $\frac{18^{\circ}}{0.5^{\circ}}$  269.5 ✓  $\frac{18^{\circ}}{2^{\circ}}$  271.2 ✓  $\frac{1.6^{\circ}}{10^{\circ}}$

282.1 ✓  $\frac{5^{\circ}}{10^{\circ}}$  280.3 ✓  $\frac{7^{\circ}}{2^{\circ}}$  271.0 ✓  $\frac{16^{\circ}}{12^{\circ}}$  271.9 ✓  $\frac{15^{\circ}}{10^{\circ}}$

285.2 ✓  $\frac{2^{\circ}}{10^{\circ}}$  281.3 ✓  $\frac{6^{\circ}}{3^{\circ}}$  272.4 ✓  $\frac{15^{\circ}}{1^{\circ}}$  273.2 ✓  $\frac{17^{\circ}}{10^{\circ}}$

287.0 ✓  $\frac{0^{\circ}}{10^{\circ}}$  284.6 ✓  $\frac{3^{\circ}}{5^{\circ}}$  274.7 ✓  $\frac{18^{\circ}}{10^{\circ}}$

287.0 ✓  $\frac{0^{\circ}}{10^{\circ}}$  283.6 ✓  $\frac{4^{\circ}}{4^{\circ}}$  275.3 ✓  $\frac{12^{\circ}}{10^{\circ}}$

Sta +  $\pi$  - Elev B.M.

287.596

1194+30 11.0 276.6 ✓

+50 11.2 276.4 ✓

+62<sup>2</sup> BC. 10.9 276.7 ✓

B.M. 1.070 286.526 286.521 ✓

12.043 298.569 ✓

+90<sup>0</sup> 20.3 278.3 ✓

1195+10<sup>5</sup> EC. 19.3 279.3 ✓

1196+00 15.2 283.4 ✓

+35 12.1 286.5 ✓

4

E

34

283.2 ✓  
 $\frac{9^{\circ}}{10^{\circ}}$

276.6 ✓  
 $\frac{11^{\circ}}{10^{\circ}}$

286.7 ✓  
 $\frac{0^{\circ}}{10^{\circ}}$

284.2 ✓  
 $\frac{3^{\circ}}{7}$

281.8 ✓  
 $\frac{5^{\circ}}{5^{\circ}}$

280.4 ✓  
 $\frac{7^{\circ}}{3^{\circ}}$

276.5 ✓  
 $\frac{11^{\circ}}{1^{\circ}}$

287.3 ✓  
 $\frac{0^{\circ}}{10^{\circ}}$

283.3 ✓  
 $\frac{4^{\circ}}{3^{\circ}}$

278.2 ✓  
 $\frac{9^{\circ}}{2^{\circ}}$

276.7 ✓  
 $\frac{10^{\circ}}{1^{\circ}}$

278.3 ✓  
 $\frac{9^{\circ}}{10^{\circ}}$

287.3 ✓  
 $\frac{11^{\circ}}{10^{\circ}}$

280.3 ✓  
 $\frac{18^{\circ}}{8^{\circ}}$

279.7 ✓  
 $\frac{18^{\circ}}{10^{\circ}}$

288.7 ✓  
 $\frac{9^{\circ}}{10^{\circ}}$

286.3 ✓  
 $\frac{18^{\circ}}{4^{\circ}}$

280.6 ✓  
 $\frac{18^{\circ}}{2^{\circ}}$

281.4 ✓  
 $\frac{17^{\circ}}{10^{\circ}}$

297.0 ✓  
 $\frac{1^{\circ}}{10^{\circ}}$

291.0 ✓  
 $\frac{7^{\circ}}{3^{\circ}}$

285.3 ✓  
 $\frac{13^{\circ}}{2^{\circ}}$

283.8 ✓  
 $\frac{14^{\circ}}{4^{\circ}}$

285.0 ✓  
 $\frac{13^{\circ}}{10^{\circ}}$

296.8 ✓  
 $\frac{1^{\circ}}{10^{\circ}}$

294.8 ✓  
 $\frac{3^{\circ}}{6^{\circ}}$

291.6 ✓  
 $\frac{7^{\circ}}{5^{\circ}}$

290.9 ✓  
 $\frac{7^{\circ}}{3^{\circ}}$

287.4 ✓  
 $\frac{11^{\circ}}{10^{\circ}}$

Sta + T - Elev

298.569

1194 T.P. 1.198 297.371 ✓

11.775 309.146 ✓

1197+00 18.0 291.1 ✓

+13 19.2 289.9 ✓

1198+00 15.0 294.1 ✓

+77 11.7 297.4 ✓

1199+00 9.3 299.8 ✓

T.P. 0.331 308.815 ✓

11.879 320.694 ✓

1199+00

304.4 ✓  
 $\frac{47}{10^2}$   
 300.4 ✓  
 $\frac{82}{5^2}$   
 293.5 ✓  
 $\frac{15^6}{3^2}$

289.7 ✓  
 $\frac{10^4}{2^2}$   
 290.1 ✓  
 $\frac{19^2}{10^2}$

302.2 ✓  
 $\frac{6^2}{10^2}$   
 299.2 ✓  
 $\frac{9^2}{5^2}$   
 291.5 ✓  
 $\frac{17^2}{1^2}$

290.9 ✓  
 $\frac{18^2}{10^2}$

303.1 ✓  
 $\frac{6^2}{10^2}$   
 301.1 ✓  
 $\frac{8^2}{4^2}$   
 294.4 ✓  
 $\frac{14^2}{1^2}$

295.1 ✓  
 $\frac{14^2}{10^2}$

302.7 ✓  
 $\frac{6^2}{10^2}$   
 298.2 ✓  
 $\frac{18^2}{2^2}$

298.8 ✓  
 $\frac{10^2}{10^2}$   
 10.2

309.1 ✓  
 $\frac{0^2}{9^2}$

300.7 ✓  
 $\frac{8^2}{10^2}$

310.0 ✓  
 $\frac{10^2}{10^2}$   
 10

Sta	T	X	Flev
		320.694	
12'' C.I.P.	+14	19.6	301.1 ✓
	+87	15.4	305.3 ✓
12.00+00		14.7	306.0 ✓
	+50	12.2	308.5 ✓
		1.8	
12.01+00		10.4	310.3 ✓
		312.5	
12.02+00		5.6	315.7 ✓
		5.4	
T.P.		1.534	319.160 ✓
		11.189	330.349 ✓
12.00+50			
12.02+00			

305.8 ✓ $\frac{14.2}{10.2}$	300.1 ✓ Flowline $\frac{20.6}{3.0}$	301.7 ✓ $\frac{19.0}{10.2}$	298.5 ✓ Flowline $\frac{22.2}{21.2}$
316.5 ✓ $\frac{4.2}{10.2}$	313.7 ✓ $\frac{7.0}{6.2}$	306.1 ✓ $\frac{14.4}{2.2}$	304.7 ✓ $\frac{16.2}{1.2}$
317.1 ✓ $\frac{3.6}{10.2}$	315.5 ✓ $\frac{5.2}{7.2}$	309.7 ✓ $\frac{11.0}{2.0}$	306.5 ✓ $\frac{14.2}{10.2}$
320.7 ✓ $\frac{0.2}{4.2}$	308.5 ✓ $\frac{12.2}{0.5}$	309.1 ✓ $\frac{11.6}{10.2}$	
320.6 ✓ $\frac{0.1}{10.2}$	311.2 ✓ $\frac{9.2}{3.2}$	311.0 ✓ $\frac{9.7}{10.2}$	
320.7 ✓ $\frac{0.2}{6.2}$	316.2 ✓ $\frac{4.5}{4.2}$	316.0 ✓ $\frac{4.2}{10.2}$	
323.9 ✓ $\frac{6.2}{16.2}$	321.2 ✓ $\frac{9.1}{6.2}$		
326.8 ✓ $\frac{3.2}{10.2}$			

S+B + T - Elev BM

330.349

#11 CIP  
12.03+31.5

8.6 321.7 ✓

T.P.

0.724 329.575 ✓

12.238 341.813 ✓

B.M. #159

9.802 332.011 332.011 ✓

366.088 BM

2.128 368.266 ✓

1212+113 EC

5.6 362.7 ✓

1211+88<sup>e</sup>

7.3 361.0 ✓

+63<sup>e</sup>

8.9 359.4 ✓

+38<sup>e</sup>

9.7 358.6 ✓

319.3 ✓  
Flow Line  
 $\frac{11.2}{5.5}$

317.4 ✓  
Flow Line  
 $\frac{12.8}{2.0}$

362.7 ✓  
 $\frac{5.4}{10.2}$

363.0 ✓  
 $\frac{5.3}{10.2}$

361.2 ✓  
 $\frac{7.1}{10.2}$

361.3 ✓  
 $\frac{7.2}{10.2}$

359.7 ✓  
 $\frac{9.2}{10.2}$

359.7 ✓  
 $\frac{8.6}{10.2}$

358.2 ✓  
 $\frac{10.1}{10.2}$

358.3 ✓  
 $\frac{10.2}{10.2}$

Sta +  $\pi$  - Elev

348.266

1 12 +13e 11.0 357.3 ✓

1210+88 12.2 356.1 ✓

T.P. 11.872 356.394 ✓

1.55B 357.952 ✓

1210+63e 2.5 355.5 ✓

+52e 1.8 356.2 ✓

1 12 +38e 7.0 351.0 ✓

Between 120B+83e - 1210+63-Piets

T.P. 12.262 345.690 ✓

0.73B 346.428 ✓

357.1 ✓  
11.2  
10e

356.3 ✓  
12.0  
10e

355.8 ✓  
2.2  
10e

355.6 ✓  
2.4  
10e

355.1 ✓  
2.2  
5.3

356.0 ✓  
2.2  
3.5

349.4 ✓  
8.2  
10e

357.0 ✓  
11.2  
10e

356.3 ✓  
12.0  
10e

355.7 ✓  
2.3  
10e

345.6 ✓  
12.4  
10e

354.8 ✓  
3.2  
10e



Sta	+	-	Elev	BM
			346.428	
T.P. + BM #160		4.134	342.292	342.20
	4.136		346.437	
1208+832		1.45	335.9	
+58.2		9.6	<del>336.8</del>	
1208+332 B.C.		9.9	<del>336.5</del>	
		12.246	334.191	
	3.328		337.519	
1208+00		5.7	331.8	
T.P.		10.298	327.229	
	1.173		328.402	
1207+532		8.8	319.6	

332.3 ✓  
 141  
 102

332.9 ✓  
 135  
 100

332.8 ✓  
 134  
 102

340.0 ✓  
 62  
 102

341.3 ✓  
 51  
 102

341.2 ✓  
 53  
 102

326.8 ✓  
 102  
 102

337.0 ✓  
 05  
 100

320.3 ✓  
 84  
 102

322.7 ✓  
 52  
 102

Sta + T Elev

328.402

+03<sup>2</sup> Ec.

9.4

319.0 ✓

1206+92<sup>e</sup>

4.6

323.8 ✓

T.P.

1.173

327.229 ✓

9.241

330.470 ✓

1206+82<sup>e</sup>

10.0

326.5 ✓

+72<sup>e</sup>

6.6

329.9 ✓

T.P.

1.818

334.652 ✓

10.595

345.247 ✓

1206+72<sup>e</sup>

337.6 ✓  
 $\frac{7.6}{10.2}$

+62<sup>e</sup>

14.5

330.7 ✓

337.9 ✓  
 $\frac{7.9}{10.2}$

327.1 ✓  
 $\frac{18.1}{5.9}$

326.0 ✓  
 $\frac{2.4}{10.2}$

318.0 ✓  
 $\frac{10.4}{10.2}$

328.4 ✓  
 $\frac{0.2}{9.2}$

318.7 ✓  
 $\frac{9.2}{10.2}$

333.3 ✓  
 $\frac{3.2}{10.2}$

320.9 ✓  
 $\frac{15.4}{10.2}$

322.6 ✓  
 $\frac{13.9}{10.2}$

$\frac{10.2}{10.2}$

Sta + T - Elev BM e

345247

+52e 13.3 331.9 ✓

337.6 ✓  
 $\frac{7.6}{10e}$

327.7 ✓  
 $\frac{17.5}{10e}$

+42° 7.8 337.4 ✓

337.3 ✓  
 $\frac{7.9}{10e}$

331.0 ✓  
 $\frac{14.2}{10e}$

T.P. 10.595 334.652 ✓

6.438 341.090 ✓

BM + TP 9.075 332.015 332.021 ✓ Record

9.075 341.095 ✓

12.06+32e 3.7 337.4 ✓

336.8 ✓  
 $\frac{4.3}{10e}$

337.2 ✓ 333.4 ✓ 328.6 ✓  
 $\frac{3.9}{1.5}$   $\frac{7.2}{3.4}$   $\frac{12.5}{10e}$

+22e 4.6 336.5 ✓

336.2 ✓  
 $\frac{4.2}{10e}$

336.8 ✓ 333.9 ✓ 330.9 ✓  
 $\frac{4.7}{4.5}$   $\frac{7.2}{5.5}$   $\frac{31.0}{10e}$

+12e 4.9 336.2 ✓

341.0 ✓ 335.7 ✓  
 $\frac{0.4}{10e}$   $\frac{5.4}{8.2}$

336.9 ✓ 335.5 ✓  
 $\frac{4.2}{8e}$   $\frac{5.2}{10e}$  Flow Line  
 12" x 8"  
 Woodenculvert

+02e B.C. 53 335.8 ✓

340.8 ✓ 335.4 ✓  
 $\frac{0.2}{10e}$   $\frac{5.5}{7.5}$

336.0 ✓ 334.1 ✓ 331.9 ✓  
 $\frac{5.1}{6.1}$   $\frac{7.2}{10e}$   $\frac{9.2}{13.2}$

Sta + T - Elev

341.095

1205+86+EC

5.9

335.2 ✓

+77.2

6.1

~~335.0~~  
335.0 ✓

+67.2

6.5

334.6 ✓

+57.2

7.1

334.0 ✓

+47.2

7.7

333.4 ✓

+37.2

8.2

332.9 ✓

T.P.

9.522

331.573 ✓

1.828

333.401 ✓

1205+27.2

1.0

332.4

±

339.3 ✓  
 $\frac{18}{100}$

334.9 ✓  
 $\frac{62}{82}$

335.7 ✓  
 $\frac{52}{100}$

340.0 ✓  
 $\frac{11}{100}$

334.5 ✓  
 $\frac{44}{82}$

335.4 ✓  
 $\frac{52}{100}$

338.1 ✓  
 $\frac{32}{100}$

334.2 ✓  
 $\frac{62}{92}$

335.0 ✓  
 $\frac{61}{100}$

339.1 ✓  
 $\frac{22}{100}$

333.7 ✓  
 $\frac{74}{75}$

334.3 ✓  
 $\frac{68}{100}$

339.1 ✓  
 $\frac{22}{100}$

333.4 ✓  
 $\frac{72}{65}$

334.0 ✓  
 $\frac{71}{92}$

333.3 ✓  
 $\frac{72}{100}$

340.0 ✓  
 $\frac{11}{100}$

335.8 ✓  
 $\frac{52}{70}$

332.8 ✓  
 $\frac{82}{62}$

333.5 ✓  
 $\frac{74}{100}$

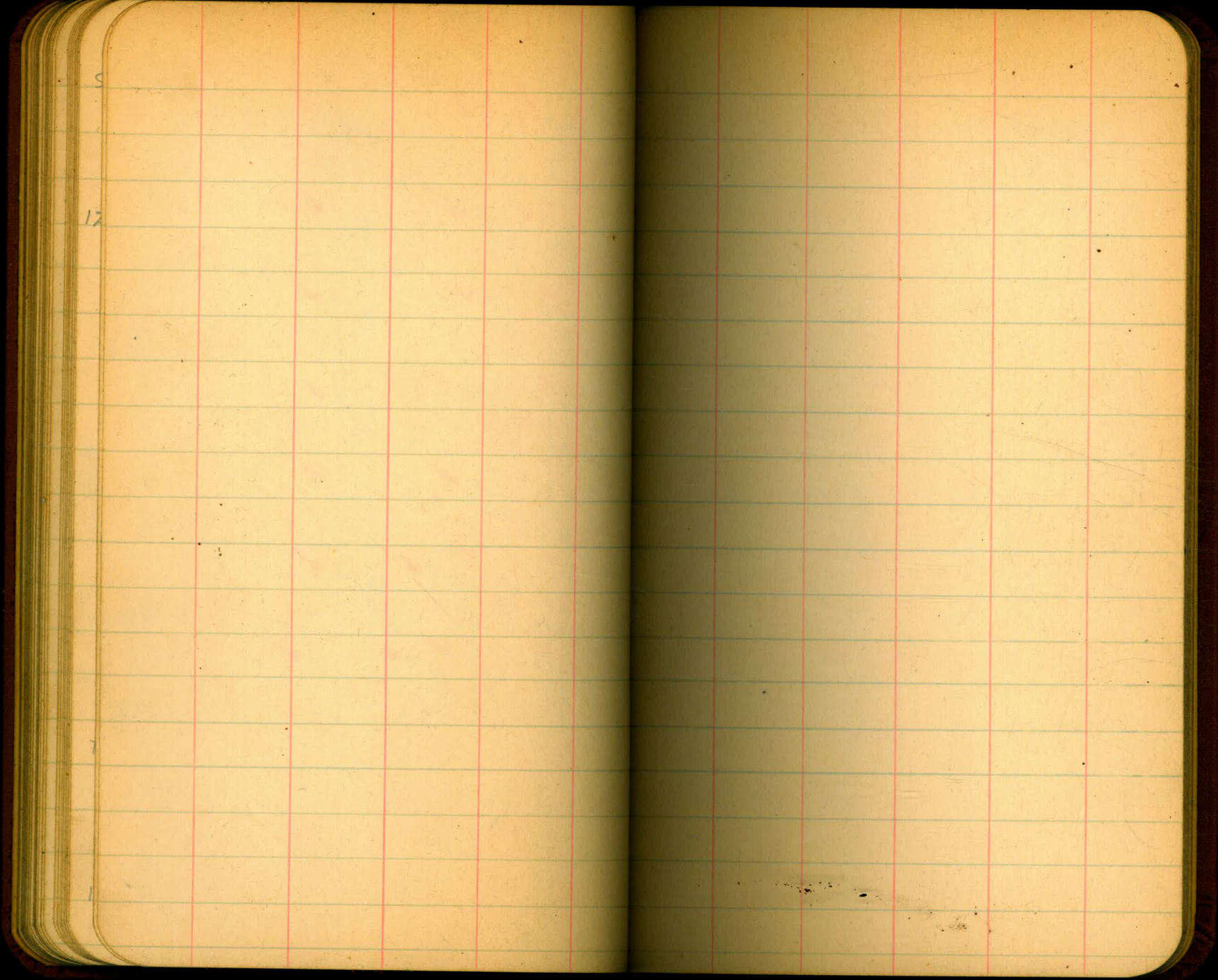
333.4 ✓  
 $\frac{02}{52}$

332.2 ✓  
 $\frac{12}{42}$

332.9 ✓  
 $\frac{02}{100}$

St	Sta	+	T	-	Elev
			333.401		
	+17 <sup>e</sup>		1.6		331.8 ✓
120	+07 <sup>e</sup>		2.4		331.0 ✓
	1204+97 <sup>e</sup>		9.2		330.2 ✓
	+87 <sup>e</sup>		3.8		<del>329.4</del> 329.6 ✓
	+77 <sup>e</sup>		4.4		329.0 ✓
	1204+00		8.6		<del>324.0</del> 324.8 ✓
	1203+00		12.6		320.8 ✓
TF			11.613		321.788 ✓

333.4 0.2 3.2	331.8 1.6 3.2	332.2 1.2 10.2
333.4 0.2 3.2	330.9 2.5 2.2	331.6 1.0 10.2
333.4 0.2 3.2	330.2 3.2 2.2	330.9 2.5 10.2
333.4 0.2 3.2	329.4 4.2 2.2	330.2 3.2 10.2
333.4 0.2 2.2	329.4 4.2 2.2	329.5 3.2 10.2
333.1 0.2 10.2	328.0 5.4 5.2	324.5 8.2 7.2 10.2
327.0 6.2 10.2	326.0 7.4 7.2	321.2 12.2 5.2
		320.3 13.2 10.2



Sta	+	π	-	Elev
B.M. #132				329.782
	5.881	335.663		
		12.072	323.591	
	12.082	335.673		
		5.886	329.787	
		323.591		

Stn	+ X	- Elev
135A		324.156
3.773	327.929	
	2.478	325.451
	327.929	
	11.333	316.594
0.871	317.467	
	4.30	313.17
	6.14	311.33
	5.09	312.38
	5.08	312.39
	6.88	310.59
	8.27	309.20
	8.18	309.29
	7.28	310.19
	8.50	308.97
	7.26	310.21
	8.52	308.95
	6.90	310.57
	6.46	311.01

+ X	- Elev
	317.467
5.93	311.54
5.65	311.82
7.29	310.18
5.76	311.71
5.63	311.84
5.35	312.12
5.49	311.98
0.871	316.596
11.190	327.786
2.337	325.449



Sta	+	∩	-	Elev
B.M. #143				342.301
	1.026			343.327
		1.43		341.90
		2.07		335.26
		3.48		339.85
		9.92		333.41
B.M. #147				298.507
G.O.L. 1134100	12.228			316.727
B.M. #147 B		3.349		307.378
B.M. #147 A				298.507
	1.085			299.592 ✓
		12.314		287.278 ✓
	4.632			291.910 ✓
		6.33		285.58

Sta	+	∩	-	Elev
				291.910
		5.93		286.08
		7.22		284.79
		8.55		283.46
		7.73		284.28
		7.45		284.56
		6.56		285.45
		5.56		286.45
		9.58		282.33
		2.05		289.86

Sta	+	π	-	Elev
		291.910		
		3.02		288.89
		12.09		279.82
		3.06		288.85
		11.23		280.68
		2.26		289.65
		9.81		282.10
		0.639		291.271
		<del>8.642</del>		<del>299.913</del>
				337.929
		1.312		339.241
		12.512		326.729

BM #146

Sta	+	π	-	Elev
		0.558		327.287
				12.581 314.706
		0.601		315.307
				4.02 317.29
				7.73 307.58
				2.31 313.00
				9.78 305.53
				10.56 304.75
				9.12 306.19
				11.12 304.19
				6.13 309.18
				11.065 304.242
		3.033		307.275
				3.50 303.78
				9.14 298.14
				5.59 301.69

Sta + T - Elev  
304.242

12.422 316.664

0.786 315.878

11.954 327.832

1112 326.720

12.330 339.050

1130 337.920

337.929

4.808 342.737

4050 338.687

BM #141 104.918

7.542 112.460

1102 111.358

112.460

9.22 103.24

7.77 104.69

9.96 102.50

9.01 103.45

Sta + T - Elev  
112.460

8.21 104.25

7.09 105.37

8.36 104.10

7.19 105.27

7.51 104.95

6.38 106.08

8.23 104.23

6.99 105.47

BM 111.358

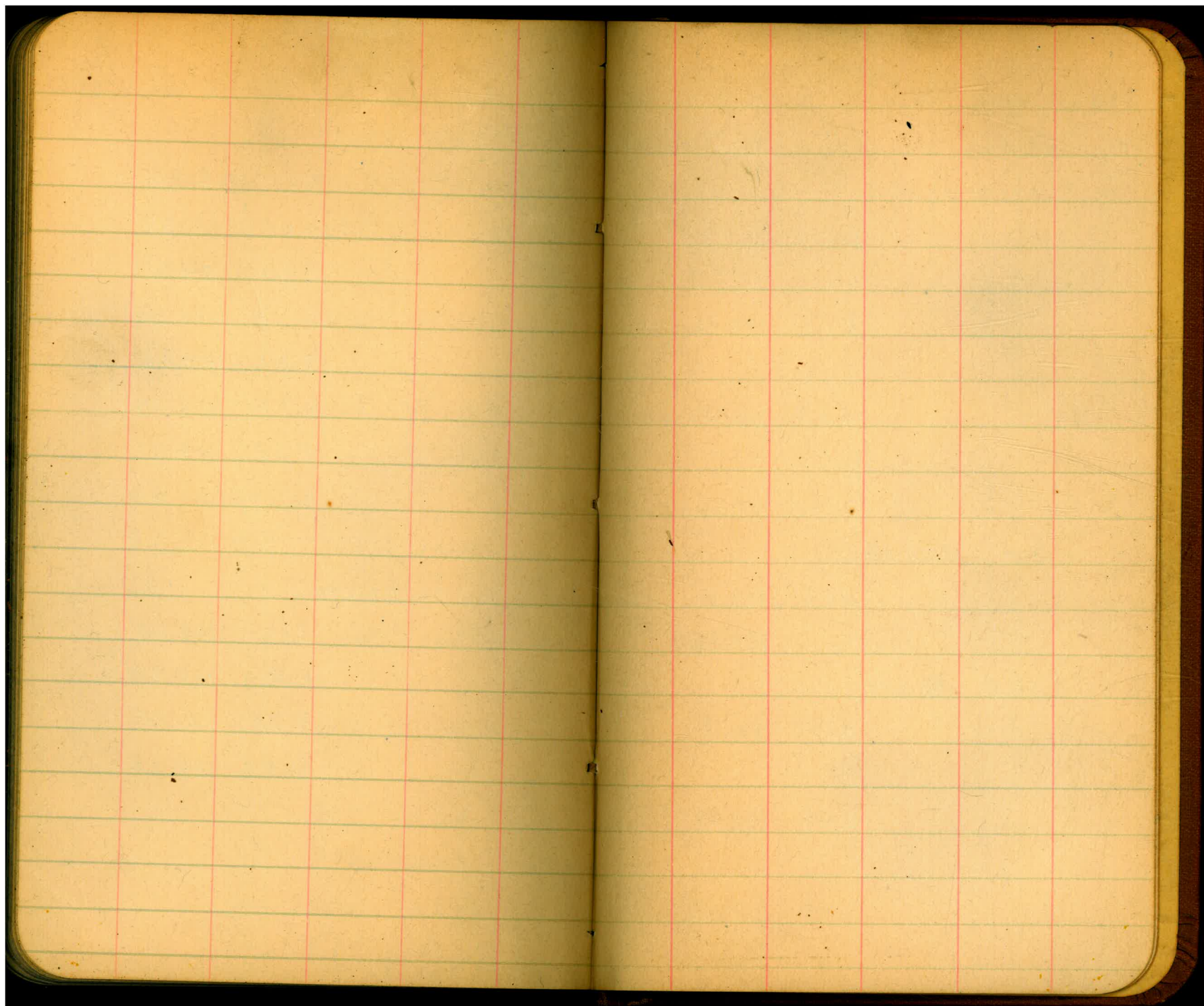
6.882 118.240

9.76 108.48

4.51 113.73

3.20 115.04

8.51 109.73



Sta.	+	π	-	Elev
BM				193.324

0.550 193.882

2.064 191.818

~~9.13 184.75~~

~~12.38 181.50~~

T.P. 12.349 181.533

12.65 182.798

7.29 175.51

184.988

3.286 188.274

8.14 180.13

6.48 181.79

11.05 177.22

Sta.	+	π	-	Elev
119B				324.156

(1) (2)  
3773

Sta	+	π	-	E lev
		1882.74		
		3.25		185.02
		4.75		183.52
T.P.		12.458		175.816
	0.921	176.737		
		1.98		174.76
		5.09		171.65
		5.22		171.52
		11.42		165.32
		12.23		164.51
T.P.		12.320		164.417
	1.522	165.939		

Sta	+	π	-	E lev
		165.939		
		7.91		158.03
		8.02		157.92
		6.19		159.75
		12.21		153.73
		13.66		152.28
		5.60		160.34
		9.65		156.29

Sta

77

T.P.

11

7

(1245)

3 10.720  
12.220  
398.500

72  
233  
200.000  
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