

LEVELS

Sta. 547 to Sta. 846.

LEVEL BOOK

480

W21

H. S. CROCKER COMPANY

DRAWING MATERIALS AND
SURVEYING INSTRUMENTS

SAN FRANCISCO

TABLES FOR EXCAVATIONS AND EMBANKMENTS

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING

Roadway 18 Feet Wide. Side Slopes 1 to 1.
For Single Track Excavation.

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	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

314+25

4 benches

3'x5'+8'

Level Book A.

So Cal. M. Natule

Credent Fine

Dulzura to Olay.

Sep 24. 07.

Oct 12. 07.

R Wueste

MICROFILMED

JAN 8 1932

MICROFILMED

FROM

LORING'S BOOK STORE

SAN DIEGO, CAL.

Index

Pls 547 - 846+72

Swets around #2

Swets around #3

1-80

90-91

89-90

0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
MICROFILMED
22
34
35
36

1. Location Mills - Dulzura Conduit

147212

547 924

+50 928

o 10.855 1473.695 928 1462.64

548 1090

+50 1094 1/2 hour

549 1098

o 6.505 1470.31 969 1464.005

+50 783

550 787

+20 789

o 5.215 1469.555 687 1466.34

22.575 25.14

Continued from Book

Grade +4.0

9-23-07

1462.88

Waste
Water
Satur

6284

100 100

6280

6276

6272

15 85

6268

10% Gravit Blows

6264

6262

in gully

95 50

52									Commenced Sta 550+50
		1469.555							9-24-'07.
550+50				696				Grade +4.0	West
								1462.60	Waterman
551				5.1	64.5	+ 1.9		62.56	S. Pine
+50				7.04				62.52	
0	7.88	1470.395	7.04	1462.515				(75)	
552				7.92				62.47	just below bunch of Bldgs
+52				7.96	1 low			62.44	= Beginning of cur.
0	11.69	1480.385	1.70	1468.695	60	30			
<u>Bm 48D</u>				4.11	47.6275				Outcropping 1/2 Bud. on Bldg
553				9.3	71.1	+ 8.7		62.40	26 7/8 = 552+52
+50				7.3	73.1	+ 10.7		62.36	
+68				5.7	74.7	+ 12.4		62.34	
	19.57		8.74						

	1480385	
○	1168 1490.775	129 1479.095
552 + 73		
554 + 16		
554 + 50		
+ 87		
○	1029 1500.425	029 1490.185
555 + 46		
556		
+ 50		
+ 73		
+ 84		
+ 88		
	21.92	1.88

	Grade +4.0	
	125 60	
95	81.3 + 19.0	1462.34
73	83.5 + 21.2	6228
67	84.1 + 21.8	6226
	145 25	
84	1492.0 + 29.8	6220
68	93.6 + 31.4	6216
52	95.2 + 33.1	6212
48	95.6 + 33.5	6210
19	98.5	
24	98.0 + 35.9	6209

= Beginning of old cut.

Chindery
cut

= Road to Sarano

Elev. of Road out of cut	
South side	96.3
North side	95.7
108' Bet. Point	
28' Bet. base. steps	

4.

1500425

557 +50

+98

0

064 1498.015

305 1497.375

+15

558 +50

559

+50

560

+50

561

064

305

grade +4.0

31

97.3 +35.3 1462.04

37

96.6 +34.6 62.00

145

155

= wire fence

21

95.9 +33.9 61.96

36

94.4 +32.5 61.92

42

93.8 +31.9 61.88

60

92.0 +30.2 61.84

64

91.6 +29.8 61.80

87

89.3 +27.5 61.76

Halls Elev. 1497.40

= BM 150 (1495.02)?

(Sta 557+71)

5.

1498.015

Grade +4.0

0	0.715	1489.87	886	1489.158
---	-------	---------	-----	----------

160 185

561 +50

16

88.3 +26.6 1461.72

562

36

86.3 +24.6 6168

+50

39

86.0 +24.4 6164

+81

37

86.2 +24.6 6162

563 +15

7.0

82.9 +27.3 6159

564

7.1

82.2 +20.7 6152

+50
+81

7.6

82.3 +20.8 6148

= end of old cur

565

3.5

150 160

81.7 +20.3 6144

= edge of grain-field

3.435

16.24

738 1482.49

6.

148521

565 + 50

45

80.7 + 19.3

Grade + 4.0

146140

566

56

79.6 + 18.2

6136

= Be. 30 H+

0

3.055

1478.775

949

1475.72

50 160

+ 50

1.0

77.7 + 16.4

6132

Gram - full

567

27

76.1 + 14.8

6128

= 85.

+ 50

3.6

75.2 + 14.0

6124

568

5.1

73.7 + 12.5

6120

+ 50

7.8

71.5 + 10.3

6116

569

14

70.4 + 9.3

6112

+ 50

10.2

68.6 + 7.5

6108

3.055

949

7.

1478.775

BM48E3655 } 1475.12 (Wall's Elev. 1475.15) ^{Grade + 4.0} Iron Bldr 18' R.I. 568 + 84

0 0.215 1469.993 8995 1469.79

110 170

570

3.6 66.4 + 5.4 61.04

+50

4.4 65.6 + 4.6 61.00

571

5.7 64.3 + 3.3 60.96

+50

6.5 63.5 + 2.6 60.92

572

7.6 62.4 + 1.5 60.88

Grain - filled

+50

8.4 61.6 + 0.8 60.84

+90

= 3' x 3' Well (Elev of Bot 56.2 Elev of Water 57.5)

573

8.3 61.7 + 0.9 60.80

0.215

8995

8.

1469.995

4.325 1466.285 8.035 1461.96

573 + 50

574

+ 50

575

+ 50

576

B.M. 49F

+ 50

577

9.23

9.825

4.905 1469.40 1.79 1464.495

8.88

8.92

Continued 573 + 50

9-28-07

W. West, W. Waterman, S. Baker.

Grade + 40

190 230

1460.76

= End of cut

10' h + 573 + 00

60.72

60.68

60.64

60.60

60.56

Grain-field

145 120

60.52

Pt on Bed 16' h = 576 + 00

x = edge of grain field

60.48

9.

1469.40

577 +50

896

578

900

+50

904

579

908

0

7425 1467.745

908 1460.32

130

160

+50

747

580

751

+50

755

581

759

+47

763

7425

908

Commenced 576+50

9-25-07

Waste
Water
Sap

Grade +40

1460.44

60.40

60.36

60.32

60.28

60.24

60.20

60.16

60.12

skate south edge of grain field

TKs at Sept

10.

1467.745

7.0951468.81

603.1461.715

582

8.73

+24

143

+44

152

+58

142

583 +27

8.83

+75

8.87

o

8.5451466.685

1067 1458.14

130

205

584 +50

6.81

585

6.85

1 Low

15.64

16.70

Grade +4.0

90

115

1460.08

Flume begins
cluster of Rocks

54.5

- 5.5

60.06

Stake miked -1.5

53.6

- 6.4

60.04

Stake miked -2.4

grain-puff
of

South

= Road to Sarsen

59.98

Flume ends

59.94

Through brush

59.88

59.84

1466.685

585 +50

689

+78

586

693

+50

697

0

824 1467.955

697 1459.715

125

90

587

828

+50

832

588

836

+50

840

589

844

824

697

Grade +4.0

1459.80

5976

5972

5968

5964

5960

5956

5952

Grade
not plowed in 2 min fence
Cleared field

12.

589 +50

1467.955

8.48

grad +4.0

1459.48

590

8.52

594.4

+50

8.56

594.0

o

7.52 1466.925

8.56

1459.395

215

175

591

5.9

61.0

+ 1.6

593.6

+28

7.59

593.4

= stake in wash

+75

4.7

622

+ 2.9

593.0

cleared field cont.

592 +50

6.5

60.4

+ 1.2

592.4

593

7.73

592.0

+50

7.77

591.6

7.53

8.56

1466.925

594

7.1

2255

1/2 low

2350

Grade +4.0

1459.12

Commenced Sta 594+50

9-27-07.

Washed
Waterma-
saker

Bm 50

3555

1464.205

6275 1460.65 ✓

270

120

Iron Bldg

44 91

594 + 00

+50

4.2

600

+0.9

59.8

+79

5.15

59.6

cont. In wash

595 + 50

5.21

59.00

cleaned field

596

5.25

58.96

stake

+31

5.27

58.94

stake in wash

+70

5.31

1/2 low

58.90

597 + 50

5.37

58.84

3555

6275

14.

1464.205

598

+45

+50

599

+50

0

538 1464.055

553 1458.675

600

+50

601

+50

538

553

541

545

549 1/2 row

553

200

140

542 1/2 row

546

550

554

Grade +4.5

1458.80

x = 2 wire Fence

5876

5872

5868

5864

5860

5856

5852

Plowed probably less than 1/2 row

not recently plowed cleared field

15.

1464.055

602

+50

603

+55

604

+13

+43

+72

+74

+97

605

+18

+50

558

Grade

562

566

570

Low

574

577

582

586

Grade +4.0

1458.48

5844

5840

field

5836

5832

= Fence

5829

Through cor. of field

= Dam fence

Through cor.

= Fence

5824

= Dam fence

5820

Around flat gully



16.

1464.055

606

590

Grade + 4.0

1458.16

+50

594

5812

607

599

5808

+50

602

5804

608

606

5800

0

5.79

1463.795

606

1457.995

155

210

+50

593

1 hour

5796

Un cultivated fields

609

587

5792

+50

591

5788

Bm 507

579

606

435

1455.435

Pan. D. 6677

609+50

17.

1463.785

Grade + 4.0

610

595

1 low

1457.84

+50

599

1 low

5780

o

8.185

1465.97

6.00

1457.785

110

100

611

8.21

5776

+50

825

5772

Small loose Rock

612

829

1 1/2 low

5768

+22

~ 2 min jump

+50

833

5764

613

837

5760

+50

841

5756

o

10.825

1468.385

841

1457.56

120

185

614

10.87

1/2 low

5752

19.01

1441

18.

1468385

Grade + 4.0

614 +50

1091

145748

615

1095

5744

+50

1099

5740

616

1103

5736

+50

1107

5732

617

1111

5728

+50

1115

5724

0

5605 1462.94 11.15 1457235

110 240

5721

+90

563

5721

618 +26

1150

47.8 - 94

5718

State miked - 54

5605

1115

Depression

in culm

Wetmore A x
PK at 1/2

Flume begins

19.

1462.84

618 + 46

568

Em 51

504

1457.80

+ 96

572

+ 99

5712

o

7.83 1464.98

5.72 1457.2

140

45

619 + 50

7.87

5708

620

7.91

5704

+ 44

7.93

5700

waterway

621

7.99

5696

+ 50

8.03

1 1/2 hour

5692

7.83

5.72

Grade + 40

1457.16

Waterway of RK

Flume ends

From RK

18 1/2 ft

618 + 46

road to Dan Lewis

Shallow water

x

					3370	3390		Commenced Sta
20.								624+50
	1464.95						Grade +4.0	
622				8.07			1456.88	9-23-07
+50				8.11			56.84	West Water Sapling
o	740 1464.24	8.11	1456.84		120	120		
623				744			56.80	
+50				748			56.76	
624				752			56.72	
o	8.97 1465.59	752	1456.72		150	40		
+50				891	1/2 row		56.68	
625				895	1/2 row		56.64	
+40								= 10 inch oak
+55				899	1/2 row		56.60	
626				903			56.56	
	16.27		1563					

Old Mulberry ground (Clark's Timber cutting) x

21.

156559

Grade +4.0

626 +50

9.07

145652

627

9.11 1/2 Low

5648

+50

9.15 1 hour

5644 x

0

6.03 146246

9.16 145643

120

185

628

6.06

5640

+50

6.10

5636

Tree

Bm 52

3.25 1459.21

Spk on 28' W 628 + 0.0
in calyptra

629

6.14 1/2 Low

5632

+50

6.18

5628

in calyptra

630

6.22

5624

6.03

9.16

22.

146246

Grade + 40

9.80 1466.04

6.22 1456.24

170

170

630 + 50

9.0

5.70

+ 0.8

1456.20

631

9.88

56.16

+ 50

9.92

56.12

632

9.96

56.08

10.58 1466.665

9.96 1456.08

140

75

+ 50

10.63

1 hour

56.04

633

10.67

1 hour

56.00

+ 50

10.71

55.96

634

10.75

55.92

20385

16.18

are calypso trees

are cultivated
atlands
Antioquia 17

23.

1466.665

634 +50

10.79

4020

3930

Grade +4.0

1455.58

635

10.83

5584

Gully

+50

10.87

1/2 Low

5580

9855 1465.645

10.875 1455.79

135

165

636

9.89

5576

Old Mill

+50

9.93

5572

BM 53

11.98

1453.665

Prom. Quarry R 2577 ±

636 +50

+90

9.96

5560

637 +50

10.01

5564

638

10.05

5560

9855

10.875

24.

1465.645

7.71

1463.305

1005 1455.595

638 +50

7.75

639 +05

7.79

+21

18.0

+36

7.82

640

7.87

+50

7.91

641

7.95

0

1117. 1466.525

7.95 1455.355

+20

9.9

1888

1800

Grade +4.0

145

95

1455.56

55.52 Flume begins

45.3 - 10.2

55.50

Stake marked - 6.2

55.40

side - well

Flume ends.

55.44

55.40 = Trail Fanguino to Small

55.36 = Be of circular cut

55

140

566

+1.3

55.34

25.

1466525

641 + 50

7.6

58.9 + 36 1455.32

+ 75

32

63.3 + 8.0 5530

o

9.03

1473.365

2.19 1464.335

80 30

Druid's

642

6.0

67.4 + 12.1 5528

+ 18

42

69.2 + 13.9 5527

Paraguino

Amount of Saddle

+ 25

45

69.9 + 13.6 5526

Ref. 58

+ 75

77

65.7 + 10.5 5522

Carro in Villo

o

1.87

1463.845

11.39 1461.975

150 40

643 + 25

53

58.5 + 3.3 5518

+ 63

87.0

55.15 end of cut

644

87.3

55.2

1090

13.58

26.

1463.945

644 +50

8.77

Grade +4.0

1455.08

Dm 54

4.20

1459.645

Pt on Bld 14' L[±] 643 + 36

(not painted)

645

8.91

55.04

+50

9.85

55.00

0

10.895 1465.19

8.85

1454.995

200

110

646

10.93

54.96

+50

10.97

54.92

+65

647

11.01

54.88

+50

11.05

54.84

10.895

8.85

side-hill facing road

= waterway

27.

146589

4785

4510

Grade +4.0

648

1109

145480

+50

1113

5476

+17

1116

5473

stake in waterway

649 +08

1118

low

5471

Outcrop of?

+50

1121

5468

650

1125

5464

0

819 146293

1125

145464

130

200

+50

1123

5460

651

1127

5456

+50

1131

5452

819

1125

Uniform side-hill facing

28.

146283

652

935

Grade 4.0

145445

0

752 1462.00 ✓ 835 145445

140

70

+50

756

5444

facing east.

+90

759

5444

Stake in waterway.

653 +50

764

5436

with wooden slope

654

768

5432

Bm 55

1031

1451.69

From Pt 17 Pt 653+58

+50

772

5429

hill side

655

776

5424

+50

780

5420

752

835

29.

1462.00

0

599

1460.19

7.90

1454.20

656

+50

657

+50

658

+19

+50

659

599

7.80

5055

4780

220

180

603

607

611

615

619

623

627

Commenced Sta 636

9-30-07

Waste

Water

Sakre

1454.16

54.12

54.08

54.04

54.00

0

5396

5392

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1460.19

659 +50

631

Grade +4.0

1453.88

0

9.445 1463.325

631

1453.88

155

170

660

949

1 low

5384

cont.

+50

953

5380

Hillside

+95

956

5377

661 +50

961

5372

0

9.295 1461.85

10.77

1452.555

140

80

662

8.17

5368

x
A round base of
corner of solid rock

+50

8.21

5364

663 +01

8.25

2 low

5360

+50

18.74

17.04

8.29

5356

Fly side - hill facing N.

1461.85

BM 56

664

+50

665

+50

666

+50

667

+50

1123

849

1147 1450.38

833

837

841

845

849

1127

1131

1135

Grade +4.0

P on PK

1491

663 + 24

1453.52

5348

5344

5340

5336

5332

5328

5324

north

facing

Side - trees

Rocky

180

300

32.

1464.59

668

11.39

low

Grade +4.0

1453.20

+50

11.43

5316

669

11.47

5312

+50

11.51

5308

o

942 1462.50

11.51

1453.08

80

170

670

9.46

5304

+50

9.50

low

5300

671

9.54

5296

+50

9.58

5292

o

996 1462.88

9.58

1452.92

75

170

672

10.00

5288

19.38

21.09

hill-side facing north - Ferns Rocks

Above Saddle Bar Hills

1462.88

672 +50

1004

Grade +40

1452.84

673

10.08

52.80

+50

10.12

52.76

0

8895 1461.655 1012 1452.76

2.80

170

674

894 1/2 low

52.72

+50

898

52.68

675

902 1/2 low

52.64

+50

906 1 low

52.60

676

910

52.56

+50

914

52.52

8895

10.12

hill - side racing wheel

34.

1461.255

677

+49

678

+50

679

o

11335 1463.65

934 1452.315

Bm 57

+50

680

+50

11335

934

918

1 low

922

1 low

926

1/2 low

930

934

120

210

1016

1453.49

1137

1141

1145

Grade + 40

1453.49

5244

5240

5230

5232

5228

5224

5220

went

to camp

Prom PK

17 91+

678 + 79

Side-hill

35.

1463.65

681

+50

1149

1153

682

+50

1157

low

1161

0

833

1460.37

1161

1452.04

210

200

683

+50

837

841

684

+50

845

849

685

933

1161

853

Grade +4.0

1452.16

52.12

Outcrop of

52.08

x waterway

52.04

52.00

51.96

51.92

51.88

51.84

Side: hill facing west
complement bank

6305

6300

36.

1460.37

685 +50

857

+74

859

686

861

0

4.57 1460.85 4855 1455.15

15 15

+50

837

687

841

+10

97

504

+17

154

44.7

+60

227

374 - 14.2

5164 Stake miked - 10.2

+75

189

41.2

4.57

4855

Commenced 686+50

Grade +40

10-1-07

1451.80

Wester
Waterman
SARRE

51.78 = Stake in waterway

51.76

+

51.72

51.68 Flume begins

Stake Dike

37.

1460.85

687 + 95

849 1/2 hour

Grade + 4.0

1451.60 Flume ends.

688 + 50

853

5156

689

857

5152

+ 50

861

5148

⊙

126

1452.735

861

1451.473

260

130

Slate dike cont.

690

130

5144

+ 50

134

5140

691

138

5136

+ 50

142

5132

692

146

5128

126

861

Side hill facing N.E.

38.

1452.735

692 +50

150

Grade +4.0

1451.24

693

154

5120

+50

158

5116

Brushing hillside

694

162

1/2 hour

5112

+10

+50

166

5108

= fence

0

757 1458.645 166 14.51075

275

300

695

7.61

5104

+50

7.65

5100

696

7.69

2 hour

5096

+51

7.73

5092

Flame Dry Pt.

757

166

1458645

Bm 58

697

+50

698

+50

699

+49

700

+08

867

1449.975

7.77

7.81

low

7.85

low

7.89

7.93

7.97

6.00

52.6

+2.0

P.O.2

Grade + 20

Tr on Rk 8' Pt 896 + 51

145088

5084

5080

5076

5072

5068

5064

5063

Sidehill facing west

Rocky

x = stake in gulch

x facing north across point

x = hut side of gulch

40.

1458.645

700 + 50

805 — 1 low

Grade + 40

1450.60

701

809

5056

+ 50

813

5052

702

817

5048

+ 50

821

5044

703

825

5040

+ 50

829

5036

704

833

5032

+ 50

837

5028

outcrop of
with
dotted
N.E. and
Hillside facing N.E.

41.

1458.645

705

o

1064 1460.865 842 1450.225

+50

706

+50

+86

707

+50

o

7.86 1457.895 1083 1450.035

+99

708 +50

18.50

19.25

841

1200

75

320

1067

1071

1075

1078

1079

1083

790

794

Grade +40

1450.24

5020

5016

5012

5000

5008

5004

5000

4996

Common 705+50

10-2-07

White
Water
Saw

facing north

= Stake in waterway

Brushy hillside

42.

1457.895

709

+24

+50

710

+50

711

+50

712

+50

1096

8155

798

802 → 1 low

806

810 1 low

814 → 1 1/2 low

110

1098

1102

1106

Grade +40

1449.92

49.88

49.84

49.80

49.76

80

49.72

49.68

49.64

= stake in waterway
or foot of rock face

Bushy Hillside facing north

43.

1460.70

712 +70

Bm 58A

713

0 11.04 1460.69 11.00 1449.60

+50

714

+50

715

+50

716

+50

11.04

11.00

1743

1443.27

11.00

240

95

1108

1112

1116

1120

1124

1128

1132

Grade +4.0

27' Pt = Sec. Cor.

(Set 10-4'-07) Pt on edge 6' E of Sec. Cor.

1449.60

49.56

49.52

49.48

49.44

49.40

49.36

49.32

NW

facing

slope

gentle

brush

hills

side

44.

146.64

Grade + 40

717

1136

1449.28

10215 1459.405

1145 1449.19

140

195

+49

10.97

49.24

718

1021

49.20

+49

1025

low

49.16

719

1029

49.12

+50

1033

49.08

720

1037

49.04

+50

1041

low

49.00

733 1459.01

7725 1451.68

260

225

721

10.05

49.96

17.45

19.175

Steep Run Hillside facing west.

45.

1459.01

721 +50

1009

Grade +4.0

1448.92

722

1013

4888

+44

x = waterway

+50

1017

4884

723

1021

4880

Chute

+50

1025

low

4876

724

1029

4872

+50

1033

4868

725

1037

4864

46.

1459.01

725 +50

1041

Bm Sq

11.63 1447.38

726

1042

+50

1049 12.07

0

1129 1459.80 10.50 1448.51

260

245

727

11.32

+50

1136

728

1140

+38

1143

+58

290

30.8 - 17.6

4835

1129

1050

8085

7970

Commenced Sta 727

10-3-'07

Grade +4.0

1448.60

Wrest
Waterman
Salmer

Pravik 4.95 724 +17

4856

4852

4848

Shale

4844

Slaty

4840

4837

Flume begins

47.

1459.80

728 + 79

+ 98

729 + 50

730

+ 50

731

0 1120 1459.36 1164 1448.6

+ 51

732

+ 50

1120

1164

1146

1152 low

1156 low

1160

1164

85 60

1174

1184

1182

Grade + 40

1448.34 Flume ends.

Shaly Slide
waterway

4828 x

4824

4820

4816

4812

4808

4804

Goose Slaty Rock
coming up

waterway below gorge

48.

1459.36

733

+50

+68

734

Bm 60

0

1159 1459.51 1144 1447.92

+50

735

+50

+89

1159

1144

1136

1140

9.0

1144

977

11.63

11.67

11.71

504 + 2.5

1449.59

100 270

Grade + 4.0

1448.00

4796

4794

4792

4788

4784

4780

Stony

Pran RK

Four

Shale

Thin

6' R¹

733+68

X Across sharp point.
= outside of cur

= gully

49

1459.51

736

1175

Grade +4.0

1447.76

0

11405 1459.165

1175 1447.76

140

90

+50

1145

47.72

+90

1148

1 low

47.69

Flume begins
(Grade would cut valid RR)

737 +02

202

39.0

-8.7

47.68

State marked -4.7

+22

1151

47.66

Flume ends

+65

1154

47.63

weathered slaty

738

1157

1 1/2 low

47.60

+51

1161

47.56

Flume begins
(Grade would cut valid RR)

+66

214

37.8

-9.8

47.55

State marked -5.8

11405

1175

50.

1459.65

739 + 90

11.54

739 + 50

11.69

740

11.73

+50

11.77

741

11.81

o

908

1456.35

11.81

1447.355

160

235

+50

9.12

742

9.16

+32

+50

9.20

908

11.81

Grade + 40

1447.53

Flume ends

47.48

47.44

47.40

47.36

47.32

47.28

47.24

slain R/R & south

= stake in waterway

51.

1456.435

743

+50

744

Bm 61

10.15

1457.315

9.97

1464.65

+50

745

+50

+90

11.23

1468.23

03.15

1457.00

0

11.355

1478.82

07.65

1467.465

746 + 50

33485

11.05

8770

8820

Grade +40

1/2 hour

1447.20

9.24

9.28

47.16

9.32

47.12

100

120

Hand PK

101 R±

744 + 30

10.24

47.08

10.28

47.04

10.32

1/2 hour

47.00

20

70
+10.0

46.96

40

12

69.8

+22.9

46.92

Commenced

Sta 744 + 30

10-4-07

Went

Waterman
Lake

52.

147882

747

0

6415 1482.905 233 147649

+09

+50

748

0

045 1472.75 10605 147230

+50

a

0375 1461.175 1195 146080

+85

749 +50

0

869 1459.295 1157 1449.605

+80

750 +15

15930

36455

23

56

61

121

101

47

123

11.64

11.67

76.5

50

76.8

70.8

10

62.7

20

56.5

48.9

110

1/2 Low

+29.6

65

+30.0

+24.0

45

+15.9

65

+9.8

+2.2

30

1446.88

46.84

46.80

46.76

46.73

46.68

46.66

46.65

Acids +4.0

Commenced Sta 747 +09

10-5-'07.

Waste

Water

Sapre

= Summit

R.R.

No direct indication of

53.

1458.295

750 + 50

1170

751

1174

show

+ 50

1178

4656

+ 75

1180

4650

= Solid Rk in Bottom of Ravine

BM 62

4395

145390

Pran Rk 24 Rk 751 + 70

752 + 31
avr. 31

1041 1468.025

068 1457.615

20

190
+ 11.1

4646

+ 59.7

1187 1479.715

088 1467.840

9

6

+ 92.2

1184 1490.895

066 1479.055

30

22

753 + 54.2

1196 1502.15

071 1490.185

35

30

46.090

2.235

54.

1502.15

754 + 30

10.385 1509.665

287 499.28

755 + 30

11.69 1520.40

0.955 1508.71

+65.5

11.975 1532.25

0.15 1520.25

756 + 65.5

14

+60.5

0.245 1524.90

7.57 1524.655

+79.5

+86

0.99 1514.185

11.705 1513.195

757 + 07

1.58 1504.66

11.05 1503.08

+25

0.18 1493.23

11.61 1493.05

+53

0.07 1481.985

11.315 1481.915

37.115

57.260

9514

9473

Grad 40

50

40

20

55

85

15

15

10

20

15

25

15

14

20

25

15

9464 9658

Commence Sta 756 + 60.5

10-7-67

Mount

Water

Bar

Formation

- summit

Pr in R 4' h±

4' P = maximum?

Pent

55.

1481.985

757 + 80 - 0.40 1470.86 11.525 1470.46

+ 90 0.945 1460.45 11.355 1459.505

+ 98
wire #1

5.0 → 55.5 + 9.5 1446.00

Bm 63 4.80 1455.37 9.88 1450.57

100 10

Paint 5' 758 + 0.7

758 9.37

1 Low 46.00 (this hnt in 23' P of 757 + 98)

+ 50 9.41

4596

759 9.45

4592

+ 50 9.49

4588

Note: Dislance hnt.

0 11.755 1457.635 9.99 1445.88

80 70

760 11.80

4584

Rock level

759 + 50 - 760 = 49'
Compensating for
error at 758.

17800

42.250

9468 9058

Grade + 4.0

10 20

10 6

Corplum

100 10

1 Low

9.41

9.45

9.49

11.80

4596

4592

4588

4584

759 + 50 - 760 = 49'
Compensating for
error at 758.

56.

1457.25

760 + 50

1184 $\frac{1}{2}$ show

Grade + 40
1445.80

761

1188

4576

+ 34

1191 \rightarrow

4573 In waterway

762

1196

4568

+ 50

1200

4564

763

1204 \rightarrow

4560

7.01 1452.605 1204 1440.95

200 230

+ 50

706

4556

Same Rock + Earth

764

709

4552

+ 58

713 $\frac{1}{2}$ show

4548

7.01

1204

57.

1452605

764 +93 7.17

764 893 1449.915 11.62 1440.985

765 +50 4.52

766 4.56

+50 4.60

0 11385 1454.995 6305 1443.61

767 9.72

+50 9.76

768 9.80

0 10765 1455.916 9.80 1445.195

+50 10.80

31.08 27.735

9768

9992

Grade 144544

100 10

80 65

145 50

Communal 764+93

10-8-07

Went
Water
in line

Per Bdrk 11' 7" 764+93

4540

4536

4532

4528

4524

4520

4516

South - Heavy Brush - Facing West

58.

1455.96

769

+50

770

+50

o

873

1453.58

11.11

1444.65

771

+50

772

o

11.425

1456.30

8705

1444.875

+50

773

20.155

19.815

195

120

1084

1088

1092 → 2 1/2 hord

1096

50

170

862

1/2 hord

866

3 hord

870

4 hord

170

80

11.46

11.50

Grade + 4.0

1445.12

45.08

45.04

45.00

4496

4492

4488

4484

4480

Loose Rock and Earth

59.

145630

365

370

Commenced at 774

773 +50

1154 $\frac{1}{2}$ hour

Grade +40

144476

10-9-07

West
Waterway
Subur

774

1158

4472

o

11.065

1455785

1158

144472

120

80

+50

1111 $\frac{1}{2}$ hour

4468

facing south

+85

1114

4465

= Stake in waterway

775

1115

4464

+50

1119

4460

Soose Rock and South

776

1123

4456

+50

1127

4452

o

11.54

1456055

1127

1444515

105

90

777

1158

4448

22.605

22.65

60.

1456.055

777 + 50

1162

1 1/2 hour

Grade + 4.0

1444.44

Commenced Sta 779+97

10-10-'07

7778

1166

Grade

4440

West
Waterma
SAPR
E. Dwell
Jack Dalton

+ 50

1170

4436

to curbing

o

3845 1448.20 1170 1444.355

70

95

+ 75

396

4434

Rock + Earth

779 + 15

399

4431

= stake in waterway

+ 50

392

4428

200 ft

+ 97

396

4424

= stake in gulch

Bm 65

11345

1436.855

Prom Bl 41 97 779+15

o

986 1454.215 3845 1444.355

150

70

x

780 + 50

1002

4420

13705

15545

61.

1454215

781

1006

+50

1010

782 +05

1014

+50

1018

783

1022

+50

1026

784

1030

o

1075 1454.66 10305 1443.91

+50

1078

785

1082

1075

10305

810

655

grad +4.0

1444.16

44.12

44.08

44.04

44.00

43.96

43.92

43.88

43.84

1/2 hour

200 370

1 hour

grad +4.0
1444.16
44.12
44.08
44.04
44.00
43.96
43.92
43.88
43.84
Rock and Earth - Heavy Brush - being work

62.

1454.66

785 +50

+76

786

+50

787

o

3.98

1447.65

1099

1443.67

+50

788

o

10331455.21

2.77

1444.88

+50

789

14.31

13.76

1010

475

Grade +4.0

1443.86

= stake in gully

43.76

43.72

43.68

43.64

43.60

43.56

43.52

1 hour

75

90

Grade

60

60

Grade

Brush -
Rock T gully
oose

x

63.

1455.21

789 +50

1173

790

1177

+48

1181

o

784 1451.24

1181 1443.40

Bm 66

869

1442.55

791

788

4336

+50

792

6 hard

4332

o

5055 1448.27

792 1443.315

90

50

+80

508

4329

Edmore begins

+90

121

353

- 80

4329

12.895

19.735

1145

1175

Grade +40

1443.48

4344

4340

45

160

Rock and Earth - facing west

Wood

Continued 790 + 50

10-11-07

West
Waterman
Super
J. Dalton
& B. Webb

Rock and Earth

9' P±

790 + 59

64.

144.87

792 +03

509

+50

513

793

517

+55

521

794

525

0

3.14

1446.26

525

1443.12

+50

316

795

322

0

2.82

1446.86

322

1443.04

+50

311

796

310

6.96

847

1340

1335

Grade +40

1360

1443.28

Blume ends.

4324

4320

4316

4312

70

140

43.08

43.04

90

30

43.00

4296

Rock and
Point - loose
Circular

64.

144.87

792 +03

+50

793

+55

794

0

3.14

1446.26

525

1443.12

+50

795

0

3.82

1446.86

322

1443.04

+50

796

6.96

849

509

1 1/2 low

513

517

521

525

316

322

328

340

1280

1335

Grade +40

1443.28

4324

4320

4316

4312

4308

4304

4300

4296

Flume ends.
Rock and Earth
- 2000
Point
Circular

70

140

80

30

65.

1446.86

796 + 50

394

0

632

1451.19

199

1444.87

700

40

797

830

4281

+50

835

4284

Flume begins

Bm 67

1118

1440.01

Iron Pit

S' LI

797 + 87

mt granite

+92

257

255

- 17.3

4280

Solid Rock
cut

798 + 33

842

4277

Flume Ends

799

847

4272

+50

851

4268

South-Brook
Slope Pit & South-Brook

800

855

4264

632

199

1430

1505

April 14.0

1442.92

660
 1451.19
 4.625 1447.265 8.55 1442.64
800 + 50
 4.67
 801
 4.72
 +50
 4.77
 802
 4.82
 7.09 1449.535 4.82 1442.445
 +48
 7.14
 803
 7.19
 +19
 +50
 7.24
 3.45 1446.35 6.635 1442.90
 15.165 20.005

1630 1525
 55 175
 1442.60
 4255
 4250
 4245
 125 145
 4240
 4235
 4230
 80 85

Note: Beginning at
 Sta 800+50, grade
 becomes - 0.1%

Commenced Sta 800+50
 10-15-07
 West
 Watson
 S. H. Lee
 J. Dalton
 E. B. West

Soon Rock and Earth.
 = Stake in waterway

67.

1446.35

804

4.10

+50

4.15

7 low

805

4.20

0

5.27

1447.42

4.20

1442.15

+50

5.32

95

60

806

5.37

+50

5.42

1 low

+70.5

807

5.47

+50

5.52

5.27

4.30

1890

1890

Grade +4.0

1442.25

42.20

42.15

42.10

42.05

42.00

41.95

41.90

South

and

Rock

5000 =

blake in waterway

68.

1447.72

430 1446.20

552 1441.90

808

435

+50

440

809

445

+50

6.87

810

6.92 K. K. low

+50

6.97

o

4495 1446.095

699 1441.60

811

4.55 K. low

+45

4.60

15.855

17.18

1985

1950

Grade + 20

100

170

1441.85

41.80

41.75

41.70

41.65

41.60

41.55

41.50

2225

2180

Commenced at 810 + 50

10-17-'07.

Wueste
Waterman
Salter
Dalton
Webb

Fairy weather

with occasional outcrop

East hillside

= habit in gully

69.

1446.95

812 +10

4.66

+50

4.70

0

5395 1446.315

5175 1440.92

75

100

813

4.97

1 1/2 hour

41.35

+50

5.02

0

503 1447.04

4305 1442.01

55

65

814

5.79

7 1/2 hour

41.25

+52

5.84

41.20

= hut in creek
and (one branch) symmetrical
canyon

Brn 68

374 1446.58

220 1444.84

75

25

Pran Blk 145 145 814 +52

815

7.43

1 hour

41.15

clark

+40

7.45

41.11

17.165

11.680

2275

250

Grade +4.0

1441.44

41.40

2

70.

1448.58

0

10365 1457.955

0.99 1447.59

$\frac{815 + 78}{\text{Ans } \pm 2}$

11705 1468.985

0.675 1457.28

816

1196 1479.725

0.32 1468.665

+10

11075 1490.535

0.265 1479.46

+40

999 1500.055

0.47 1490.065

+57

11425 1510.785

0.645 1499.36

+78

1059 1521.075

0.30 1510.485

+94

1055 1531.375

0.25 1520.795

817 +10

11405 1542.40

0.35 1530.995

98.195

4375

2430

2370

grades

15

40

20

$\frac{10}{+16.2}$

144157

Terminal

20

15

75

15

75

20

20

20

20

15

15

20

20

15

71.

817 + 28 1090 154240 075 1541.65

+ 48 1054 156235 0875 1551.675

+ 64 10795 1572745 0225 1561.99

+ 78 1121 158364 0355 157243

+ 97 10775 1594.36 0055 1583.555

818 + 12 1124 1605.53 007 1594.29

+ 30 1094 1615.90 0665 1604.865

+ 50 1162 16305 1.12 1614.685

+ 65 1170 1636.55 146 1624.845

9101235

5575

26 10 75 40

20 20

20 20

15 15

20 15

20 15

20 15

20 20

20 20

15 20

72
81818 +90 11.525 1636.55 0.17 1636.38

819 +18 11.505 1647.905 0.17 1647.735

+41 11.935 1658.71 0.53 1658.71

+60 11.82 1649.545 1.10 1649.545

+90 11.905 1680.875 0.49 1680.875

820 +23 11.915 1692.31 0.47 1692.31

+92 1.0

821 +41 0.17 1691.695 11/63 1691.695

+68 0.09 1680.44 11.515 1680.35
60965 26.075

2780 2700

15 20

20 15

20 20

15 25

20 25

90 10

1023 = amount

10 25

8 15

73.

168044

8 821+91 0145 1669.205 1138 1669.06

8 822+13 0.91 1658.635 1138 1678.25

+35 0415 1647.15 1190 1646.735

+58 0435 1635.995 1159 1635.56

+78 072 1625.99 1072 1625.27

823 079.5 1614.92 1186.5 1614.25

+21 1035 1604.285 1167 1603.25

+41 141 1594.38 11315 1592.97

+59 052.5 1584.035 1087 1583.51

6.290

102.695

2978 285

7 15

10 10

8 15

8 15

7 12

8 15

8 15

8 13

7 13

Continued Sta 823+21

10-15-07

Q. W. West

Robt. Water

D. G. S. R. R.

Dalton

Webb

Misty

74.

1584.035

823+78

0.305

1573.115

1122.1572.81

824

0.17

1561.875

1141.1561.705

+24

0.475

1550.53

1182.1550.055

+48

0.49

1539.09

1193.1539.60

+70

0.78

1528.06

1181.1527.28

+98

0.45

1517.315

1195.1517.65

825+21

0.81

1506.58

11545.1505.77

+46

0.745

1495.85

1164.1494.74

+78

0.51

1484.27

11925.1483.76

4.735

104500

3049

2973

9

13

9

14

9

16

8

15

9

15

11

14

10

18

12

16

15

20

75.

148427

826+09 1.06 1473.645 11685 1472.585

+33 0.855 1462.80 1170. 1461.945

4 in #2

+62 1.25 1452.34 11585 1451.215

+95 4.14 1445.78 1070 1441.64

827+03 583

0 5.895 1444.845 6.83 1438.95

+45 494

828 5.00

0 4.11 1443.855 5.10 1439.745

+50 406

829 4.11

17.185 57.600

3141 3129

grade + 4.0

10 17

12 $\frac{15}{+21.9}$ 1440.02

15 $\frac{17}{+11.3}$ 39.99

7 $\frac{15}{+1.6}$ 39.95

39.95

40 $\frac{7}{(1438.95)}$

39.900

12.00 39.85

12.5 70

13.5 hand 39.80

39.75

Commenced

827+03

10-12-07

Waste

Water

Saline

Dallen

well

cloudy

clear

= Rd Prank 492 827+13

(By note page 90-91)

Gentle slope - South - Bank

76.

1443.865

829 +50

416

830

421

o

564

1443.925

557

1438.285

75

100

+50

433

831

437

+50

442

832

447

o

322

1442.675

447

1439.455

45

95

+50

321

833

333

o

404

1443.765

333

1439.345

55

55

+50

444

1330

13.31

3350 3270

Grad + 4.0

1439.70

39.65

39.60

39.55

39.50

39.45

39.40

39.35

39.30

Brush -
Rock
and
soil
Earth

77.

1443.78

834

4.78 1444.025

4.54 1439.245

4.54

+13

+50

+95

o

4.79 1443.435

4.88 1439.145

4.88

70

40

835 +50

4.34

836

o

3.56 1442.605

4.39 1439.045

4.39

80

35

+50

3.61

837

+50

19.63

13.81

3.66

3.71

~~3545~~ 3570

Grade +40

1439.25

55

50

Common ad Sta 834+95

10-21-07

clean

Wash
Water
Sands
well
Patton

= Stake in gully

39.20

Brush

39.15

In Waterway

39.10

Rock

39.05

Gravel + Stone

39.00

38.95

38.90

78.

1442.605

5575 1443.03 515 1437.455

838

4.15

3730

3695

Grade + 4.0

45 85

Low

1438.85

+45

4.23

1/2 low

3880

374 1442.78 399 1439.04

35 45

839

4.03

1 1/2 low

3875

+40

4.07

Grade

3871

462 1443.42 498 1437.80

110 55

840

3.77

Low

3865

+50

3.82

3860

841

3.87

Grade

3855

+50

3.92

3850

5945 1443.515 485 1437.57

55 120

19880

1897

Bruck
Book
1
1

79.

1443.515

842

5.07

+50

5.12

Grade

+90

5.16

1/2 Low

o

3.89

1441.565

5.84

1437.675

105

60

843 +50

3.27

1 Low

844

3.32

+50

3.37

o

8.75

1446.945

3.37

1438.195

75

60

845

8.80

+50

8.85

+87

8.88

8 hours

1264

921

3975

3950

Commenced sta 842+90

Grade +40

10-22-07

1438.45

Went
to Pine
Wash
Dallen

3840

cloudy

3836

and exterior of rock - brush

3830

and

3825

3820

3815

earth

3810

3806.5

1/2 mile begins

80.

1446.945

1815 1439.87

999 1438.055

846 + 02

+ 36

+ 72

0

151 1438.36

1815

1040

4150 4070

grade + 4.4

10

65

1438.00

71.3 + 16.7

3795

3793

80

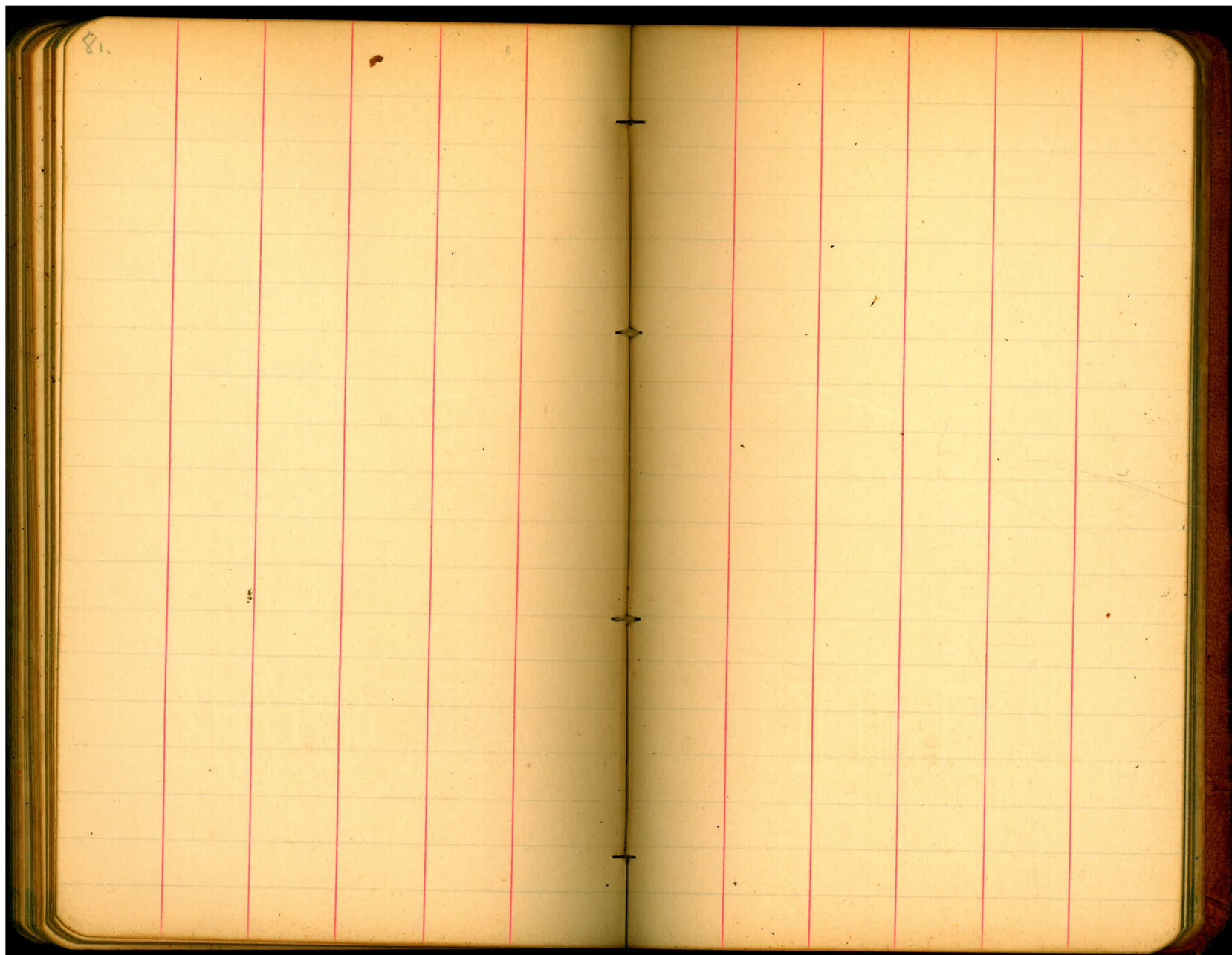
Note 845 + 8 - 846 + 72

= long chord of curved

flume across west

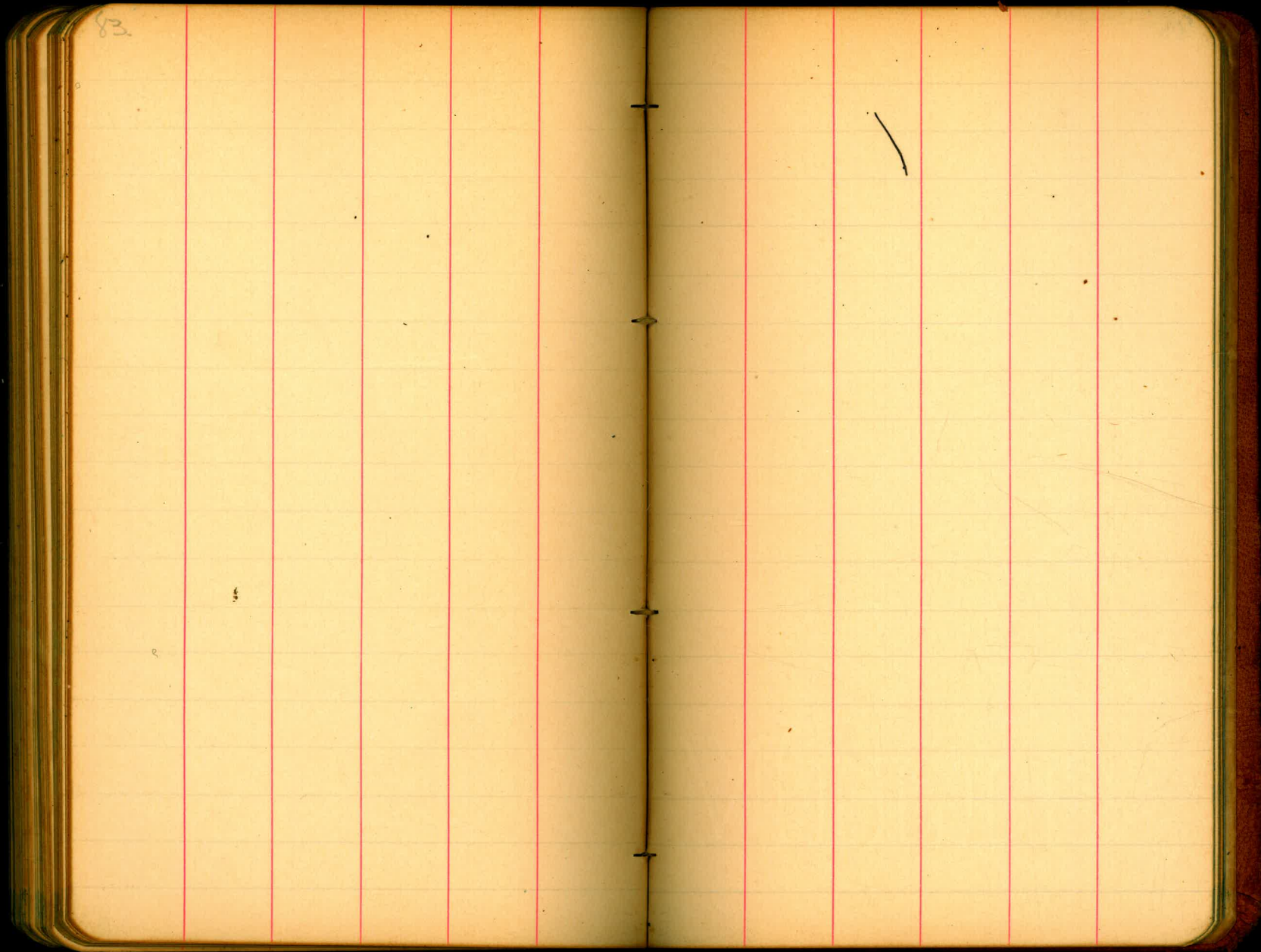
branch of Dycamore 2
later.

Flume ends



92.

✓



83

—

24.

—

85.

✓

86.

1

87

1

1443.115

o	722	1441.72	8615	1434.50
o	1184	1447.30	626	1435.46
o	1028	1450.435	7145	1440.155 Δ
o	4375	1445.85	896	1441.475 Δ
o	449	1441.855	8485	1437.365
o	1108	1449.45	3485	1438.37
o	11745	1451.385	991	1439.64
o	9535	1450.985	9935	1441.45
o	750	1448.835	965	1441.335
o	953	1451.49	6885	1441.95
o	11325	1452.12	1068	1440.80
o	8695	1450.635	1018	1441.94
o	837	1448.665	1034	1440.295
o	10965	1449.44	1014	1438.525
o	1050	1448.225	11715	1437.725
o	10345	1447.16	1141	1436.815
			971	1437.95

147.740

152905

1430 1135

370	65
150	370
760	730
300	405
16	270
135	135
120	150
180	150
210	270
120	390
250	190
85	620
135	90
450	50
140	40 360 1070
140	180
530	210

A₁₀ = P_u P_r

Δ east of divide
Δ west of divide

~~1443.115~~
~~4716a~~

continued 10-23-07

147.740
143.695
4.045

1436.95
921.5
1379.0

1443.115
5.165
379.50

152905
147.740
5.165

90.

Sevels around Tunnel #2 cont.

1453.545

4.64 1447.12 11.065 1442.48

11.7 1438.95

~~~~~

11.55 1463.525 1452.37

0.175 1452.345 11.355 1452.17

5.735 1446.61

~~~~~

Sevels around Tunnel #3

4.38 1443.725 1439.345

6.30 1437.425

3.77 1443.115 1439.345

5.715 1437.40(1)

4.18 1441.59

6.535 1440.04 8.085 1433.505

6.75 1440.015 6.775 1433.265

6.45 1437.755 8.71 1431.305

8.13 1442.64 3.245 1434.51

9.05 1443.115 8.575 1434.065

41.095

35.390

15 20

10

30

10

25

35

570

570

35

565

245

360

210

275

65

105

225

265

120

130

= Rep Pr. on Rk in gulch
death

= Rep Pr. on Rk

= Rep Pr. on Rk in gulch
death

= Sta 853 10-31-07

waste
water

91.

Levels around Tunnel # 2

3.44	1446.08	1442.64
4.54	1447.18	1442.64
5.655	1445.495	7.35 1439.85 (4)
11.015	1451.31	5.20 1440.295
7.47	1449.495	9.285 1442.025
11.045	1453.41	7.13 1442.265
11.53	1463.22	1.72 1451.69
11.08	1473.01	1.29 1461.93
10.80	1482.855	0.955 1472.055
11.845	1484.235	10.465 1472.39
9.94	1483.435	10.74 1473.495
2.04	1474.605	10.87 1472.565
11.535	1474.52	11.62 1462.965
11.71	1479.00	7.33 1467.29
4.09	1472.33	10.76 1468.24
2.90	1463.66	11.57 1460.76
11.75	1453.45	11.29 1452.27
123.530		110.125

500	
1439.83	8
8	
290	500
130	370
60	110
110	70
35	50
25	15
35	20
255	75
56	70
310	70
60	240
55	75
330	80
40	130
10	200

= Sta 800 page 66
 = pr on Rk on opposite side

10-12-07

= pr above
 Urust
 Water
 Sature

1990 137.5

Saddle 4' higher than HI

10-14-07

Urust
 Water
 Sature

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

FOR SINGLE TRACK EMBANKMENT.

ROADWAY 14 FEET WIDE. SIDE SLOPES $1\frac{1}{2}$ TO 1.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.