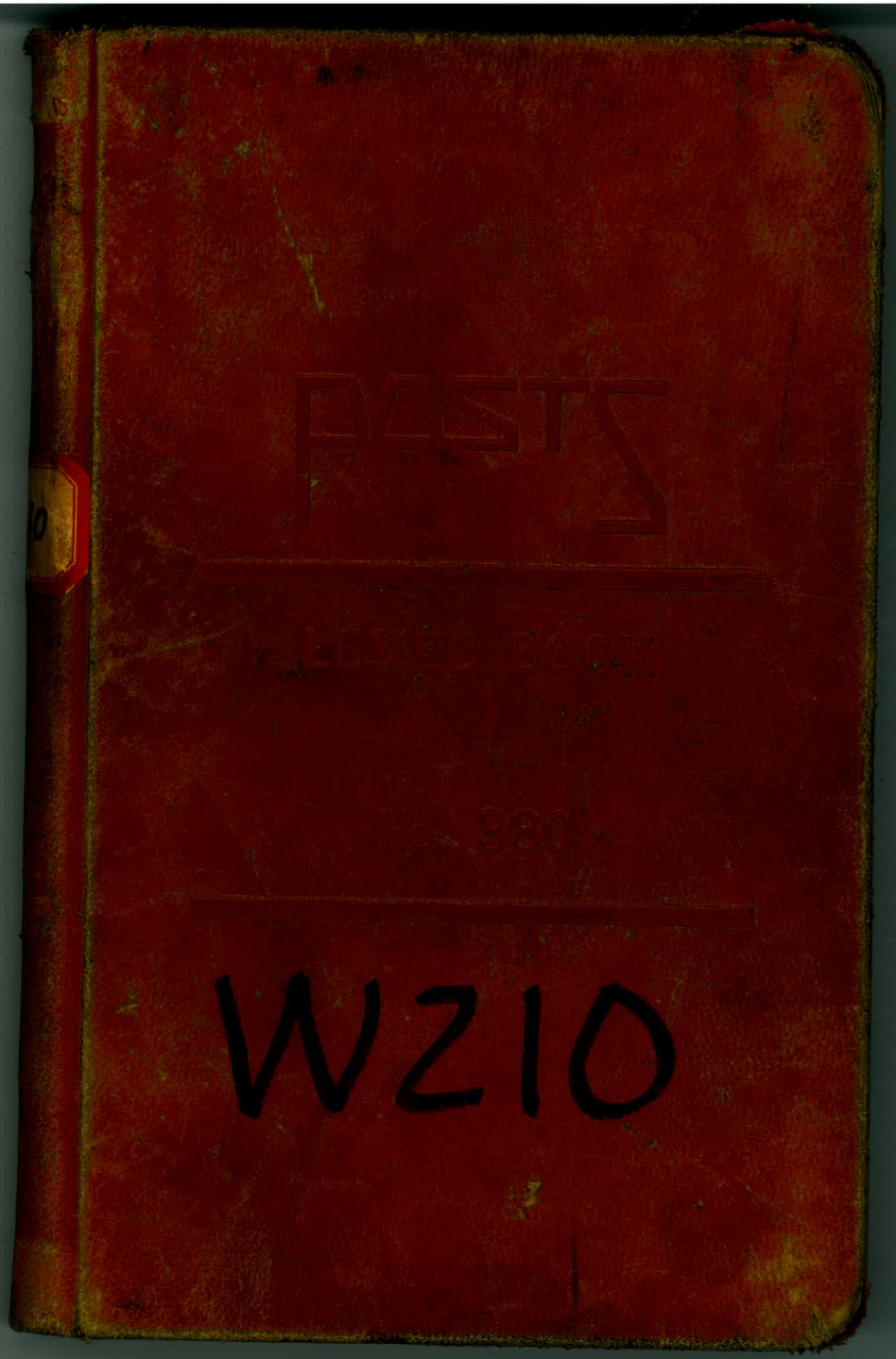

POSTS
W210

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

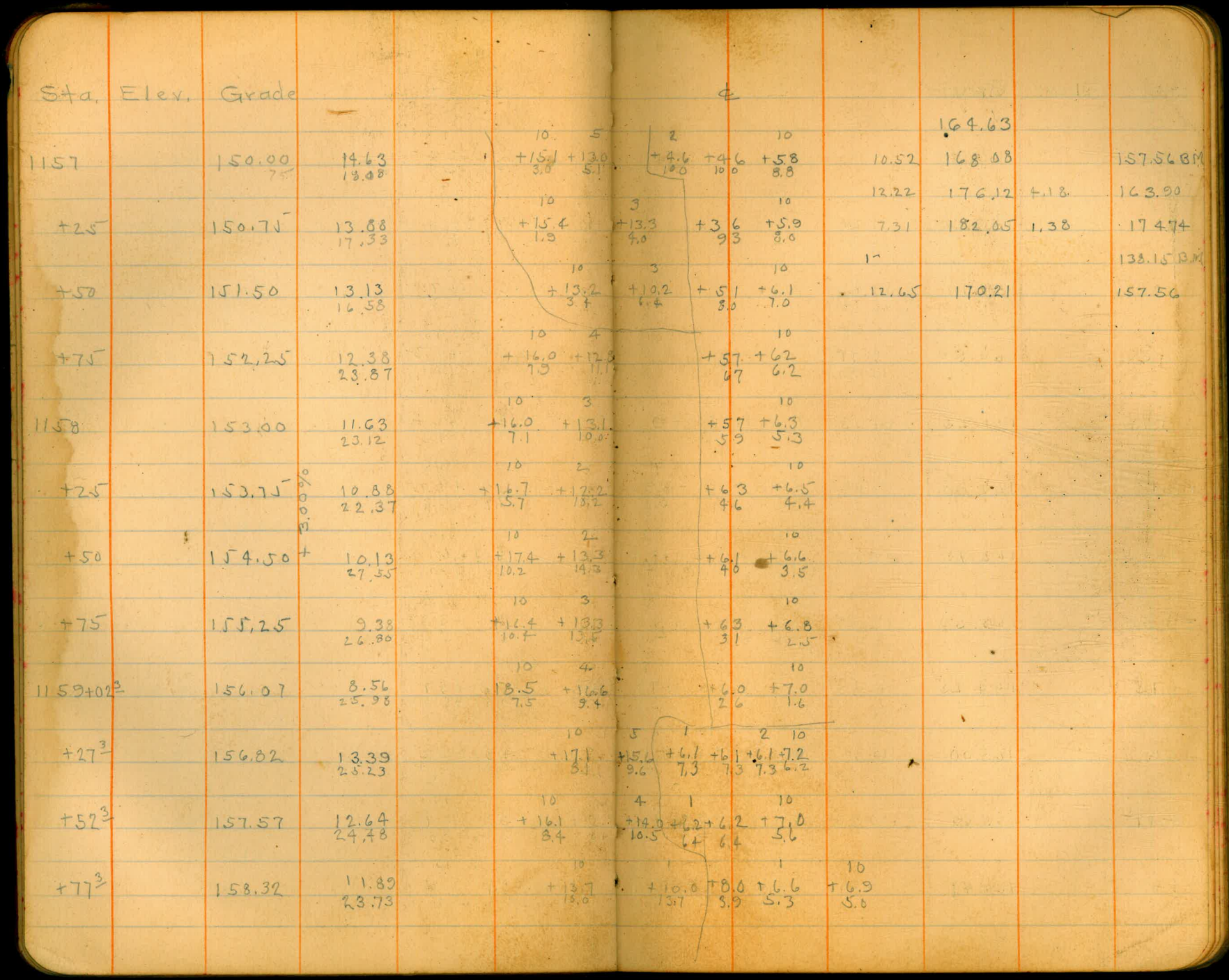
In ordering Fabri-Hide covered books, add the letter *"F"* to catalog number.

Sta.	Elev.	Grade				L	℄	R	+	H.I	−	Elev
									1.81	139.81		138.00 B.M
1148+50		126.00	X						4.43	141.96	2.28	137.53
										90' L	1149+00	138.15 B.M
+54		125.82										
										0.85	139.00	138.15
+63		125.47	4.00%				9.5			3.78 136.69	6.09	132.91
										7.72 145.28	3.83	137.86
+75	131.50	125.00	14.81			10 +7.6 7.2		3 +6.8 8.0	T 10 +10.1 4.7	10 +10.1 4.7		
1149	131.50	124.00	X 15.81			10 +6.9 8.9		7 +9.3 4.5	10 +11.1 4.7			
+25	133.10	125.00	14.81			10 +6.5 8.3		4 +10.1 4.7	10 +10.3 4.5			
+50	133.80	126.00	13.81			10 +8.0 5.8		4 +9.3 4.5	10 +9.6 4.2			
+75	134.90	127.00	12.81			10 +8.0 4.8		10 +8.9 3.9				
1150	135.70	128.00	4.00% + 11.81	8.69		10 +7.3 4.5		10 +8.6 3.2				
+25	136.30	129.00	10.81	7.69	15 +13.4 H.L	5 +11.2 H.L		10 +8.0 2.3				
+50	137.20	130.00	11.96	6.69	15 +24.8 H.L	8 +20.4 H.L	2 +7.2 4.8	10 +7.7 4.3				
+75	137.70	131.00	10.96	5.69	15 +26.7 H.L	9 +21.0 H.L	2 +6.7 4.3	10 +7.5 3.5				

Sta.	Elev.	Grade			Left	℄	Right		145.29 141.96		
1151	138.50	132.00 X	9.96	4.69	15: +20.0 H.L.; 11: +17.4 H.L.; 9: +13.5 H.L.; 4: +10.5 H.L.; 1: +6.5 3.5	+6.5 3.5	10: +7.3 2.7	∠			
+25	139.1	132.75	9.21	3.94	10: +13.8 H.L.; 3: +6.3 2.9	+6.3 2.9	10: +7.1 2.1	∠			
+50	139.70	133.50	8.46 19.19	3.19 11.78	10: 13.8 5.4; 7: +12.2 7.0; 2: +6.2 2.3	+6.2 2.3	10: +6.7 1.8	6.83 ∠	144.83		138.00
+75	140.3	134.25	10.58 18.44	11.03	10: +12.6 5.8; 4: +7.4 3.2	+6.1 4.5	10: +6.5 4.1	∠		1.57 4.13	140.39 137.83
1152	141.20	135.00	9.83 17.69	10.28	10: +16.5 2.0; 6: +10.1 7.6; 4: +8.4 9.3; 4: +8.4 1.4	+6.2 3.6	10: +6.4 3.4	∠		7.23 4.31	137.60 151+85 J'R 140.52
+25	142.0	135.75 3.00%	9.08 16.94	2.53	9: +13.9 3.0; 7: +10.9 6.0	+6.2 2.9	10: +6.5 2.6	∠			
+50	142.80	136.50 +	8.33 16.19	8.78	10: +12.6 3.6; 6: 10.9 5.3; 3: +6.1 2.2	+6.3 2.0	10: +6.4 1.9	∠ 9.25	152.69	1.39	143.44
B.C. +75	143.0	137.25	15.44	8.03	10: +14.0 1.4; 6: +10.7 4.7; 4: +8.0 7.4; 2: +5.9 9.5	+5.8 9.6	10: +6.7 8.7	∠			
1153	143.90	138.00	14.69	7.28	6: +11.0 3.6	+5.9 8.8	10: +6.7 8.0	∠			
+25	146.5	138.75	13.94	6.53	10: +18.0 H.L.; 7: +15.4 H.L.; 1: +6.1 7.8	+7.7 6.2	10: +6.8 7.1	∠			
+50	147.90	139.50	13.19	5.78	10: +19.1 H.L.; 7: +17.2 H.L.	+8.4 4.8	1: +6.3 6.9; 10: +7.2 6.0	∠			
+75	148.7	140.25	12.44	5.03	10: +19.1 H.L.	+8.5 3.9	1: +6.7 5.7; 10: +6.9 5.5	∠			

Sta.	Elev.	Grade												
												145.28		
										12.07	153.07		4.28	141.00
											152.69			
1154	147.80	141.00	11.69	4.28		10 +18.0 H.L	3 +12.3 H.L	+6.8 4.9	1 +6.2 5.5	10 +7.0 4.7	∠			
+22.2	E 149.0	141.67	11.02	3.61 11.40		10 +15.3 H.L	4 +12.7 H.L	2 8.4 5.6	+7.3 3.7	3 +5.4 4.6	10 +6.9 4.1	∠			
+50	149.10	142.50	10.19	10.57			10 +11.3 H.L	2 +6.6 3.6	+6.6 3.6	10 +6.7 3.5		∠	6.10	157.67	1.12	151.57
													7.36	162.17	2.86	154.81
+75	148.9	143.25	14.42	9.82				10 +10.3 4.1	+5.7 8.7	10 +6.3 8.1		∠			4.61	157.56
1155	149.50	144.00	13.67	9.07		8 +10.2 3.5	3 +7.3 6.4	2 +5.5 8.2	+5.5 8.2	10 +6.4 7.3		∠				
+25	150.0	144.75	12.92 17.32			10 +12.2 5.1	5 +10.8 6.5	3 +8.0 4.9	2 +5.2 7.1	+5.2 7.7	10 +6.2 6.7	∠				
+484 N		145.45	3.00%													
+50	150.70	145.50	12.17 16.67		12.9 3.8	10 +11.1 5.6	3 +8.1 4.1	2 +5.7 6.5	+5.2 7.0	10 +6.1 6.1		∠				
+75	151.7	146.25	11.42 15.92			10 +10.9 5.0	4 +7.1 4.3	2 +5.5 5.2	+5.5 5.9	10 +5.8 5.6		∠				
1156	152.30 75	147.00	10.67				10 +9.4 1.3	4 +5.6 3.1	+5.3 3.4	10 +5.7 +5.0		∠				
+25	152.7	147.75	9.92				10 +6.7 +3.2	5 +5.2 4.7	+4.9 5.0	10 +5.5 4.4		∠				
+50	153.80	148.50	9.17			10 +5.5 3.7	6 5.2 4.0	5 +4.4 4.8	+5.3 3.9	10 +5.7 3.5		∠				
+75		149.25	16.38				10 +3.3 HL	3 +5.8 10.6	+6.1 10.3	10 +6.6 7.8			7.07	164.63		157.56

↓ Notes sent to office 8-15-26.


Sta. Elev. Grade
℄
164.63
1157
150.00
14.63
18.08
+15.1 +13.0
3.0 5.1
+4.6 +4.6 +5.8
10.0 10.0 8.8
10.52 168.08 157.56 B.M.
12.22 176.12 +1.8 163.90
+25 150.75 13.88 17.33 +15.4 1.9 +13.3 4.0 +3.6 9.3 +5.9 8.0 7.31 182.05 1.38 17.474
138.15 B.M.
+50 151.50 13.13 16.58 +13.2 3.1 +10.2 6.4 +5.1 8.0 +6.1 7.0 12.65 170.21 157.56
+75 152.25 12.38 23.87 +16.0 7.9 +12.8 11.1 +5.7 6.7 +6.2 6.2
1158 153.00 11.63 23.12 +16.0 7.1 +13.1 10.0 +5.7 5.9 +6.3 5.3
+25 153.75 10.88 22.37 +16.7 5.7 +12.2 8.2 +6.3 4.6 +6.5 4.4
+50 154.50 10.13 27.55 +17.4 10.2 +13.3 14.3 +6.1 4.0 +6.6 3.5
+75 155.25 9.38 26.80 +16.4 10.7 +13.3 13.6 +6.3 3.1 +6.8 2.5
1159+02 156.07 8.56 25.98 +18.5 7.5 +16.6 9.4 +6.0 2.6 +7.0 1.6
+27 156.82 13.39 25.23 +17.1 3.1 +15.4 9.6 +6.1 7.3 +6.1 7.3 +7.2 6.2
+52 157.57 12.64 24.48 +16.1 3.4 +14.0 10.5 +6.2 6.4 +6.2 6.4 +7.0 5.6
+77 158.32 11.89 23.73 +13.7 15.0 +10.0 13.1 +8.0 5.9 +6.6 5.3 +6.9 5.0
2.00%

Sta.	Elev.	Grade							¢					
												170.20		
											8.65	175.88	2.98	167.23
										1060+50	100'R	B.M.	9.44	160.77
1159+83² E.C.		158.50												
1160		159.00		11.21 16.88				10 +12.9 4.0	+8.5 2.7	2 +6.2 5.0	10 +6.6 4.6			
+25		159.75		10.46 16.13				10 +11.1 5.0	+8.9 1.6	3 +5.9 4.6	10 +6.7 3.8			
+50		160.50		9.71 15.38				10 +10.8 4.6	+9.2 0.5	2 +6.2 3.5	10 +6.7 3.0			
+75		161.25		14.63		10 +10.8 3.8	3 +9.6 5.0	1 +6.1 8.5	+6.1 8.5	10 +6.9 7.7				
1161		162.00	+3.00%	13.88		8 +13.9 0.1	7 +8.9 5.0	4 +5.9 8.0	+6.4 7.5	10 +7.0 6.9				
+25		162.75		13.13		11 +21.4 H.L.	8 +8.4 4.7	4 +5.7 7.4	+6.5 6.6	10 +6.8 6.3				
+50		163.50		12.38		10 +19.0 H.L.	8 +8.0 4.4	5 6.0 6.4	+6.4 6.0	10 +6.5 5.9				
+75		164.25		11.63		12 +11.0 0.6	7 +7.8 3.8	6 +5.6 6.0	+6.3 5.3	10 +6.5 5.1				
1162		165.00	X	10.88		10 +7.5 3.4	6 +6.7 4.2	5 +5.4 5.5	+6.3 4.6	10 +6.8 4.1				
+17½		165.60		10.28		10 +7.3 3.8	4 +6.7 3.6	3 +5.9 4.4	+5.8 4.5	10 +6.9 3.4				
+42½		166.47	+3.5%	9.41	16 +11.2 H.L.	7 +9.2 0.2	2 +6.7 2.8	1 5.4 4.0	+5.4 4.0	10 +6.8 2.6				

Sta.	Elev.	Grade				L	℄	R	175.88	187.74	℄
1162+67 L		167.35	8.53 17.21		.9 +12.9 4.3	1 +7.1 1.4	1 +5.5 +6.0 3.0 11.2	10 +6.9 10.24 1.6	184.56	1.56	174.32
+92 L		168.22						12.32	196.54	0.34	184.22
										8.82	187.7$^{4}_{2}$ B.M
+95² E.C.		168.33									
								7.90	195.64		187.74
1163+00 92		168.50	16.06	10 +16.1 0.0	4 +13.4 2.7	1 +5.9 10.2	10 +5.9 +7.1 10.2 9.0	6.92	191.26	10.80	184.84 T.P. Rock
								10.56	198.30		187.74
+25		169.38	15.18	10 +13.4 1.8	4 +11.2 4.0	2 +5.7 9.5	10 +5.7 +6.9 9.5 8.3				
+50		170.25 +3.5%	14.31	10 +19.4 -0.1	5 +12.0 2.3	2 +5.5 8.8	10 +5.5 +6.8 8.8 7.5				
+75		171.12	13.44	10 +15.2 H.L	4 +12.6 0.8	2 +5.8 7.6	10 +5.5 +6.7 7.9 6.7				
1164		172.00	12.56	10 +17.4 H.L	3 +12.4 0.2		10 +5.4 +6.5 7.2 6.1				
+10 B.C. 25		172.35	18.91 25.95	10 +18.4 7.6	4 +15.0 11.0		2 +6.8 +5.6 12.1 13.3	10 21 +6.4 +6.9 12.5 12.0			
+35 2.5		173.22	18.04 25.08	10 +20.6 4.5	7 +12.5 5.6		2 +7.9 +6.4 10.1 11.6	16 21 +6.6 +6.9 11.4 11.1	24 30 +8.1 +5.3 9.9 12.7		
+60		174.10	17.16 24.20	10 +20.4 3.8	7 +19.9 4.3		2 +7.4 +6.3 9.8 10.9	16 22 +6.7 +7.0 10.5 10.2	27 44 +10.9 +5.4 6.3 11.8		
+82.9 E.C.		174.90	16.36 23.40	10 +17.0 6.4	6 +16.1 7.3		3 +7.4 +6.0 9.0 10.4	10 23 +6.8 +6.8 9.6 9.6	26 28 +8.0 +10.2 8.4 6.2	50 +5.6 10.8	

Sta.	Elev.	Grade		℄	
1165		175.50	15.76		
+25		176.38	14.88		
+50		177.25	14.01		
+75		178.12	13.14		
1166	BC	179.00	12.26		
+20		179.70	11.56		
+25		179.88			
+40		180.40	10.86		
+50		180.75			
+60		181.10	10.16		
+75		181.63			
+80		181.80	9.46		
1167		182.50			
+07.2	EC	182.71	8.51		
				(offset Cut.)	
+25		183.38			
+50		184.25			

3.5%

1164+82.9

℄ 191.26

Sta.	Elev.	Grade		(offset Cut)
1167+75		185.12		7.5
1168		186.00		7.6
+25		186.88		8.7
+50		187.75		7.7
+75		188.63	+3.50%	6.5
1169		189.50		10.5
+25		190.38		11
+50		191.25		11 9/10
+75		192.12		7 5/10
1170		193.00	X	7 9/10
+25		193.77		8 5/10
+50		194.53	+3.067%	9 8/10

℄	+	℄	−	El.
7 3/4 192.6				178.72
3 7/10 A	11L	189.88		
6 3/4 193.60			.08	189.80
3 5/10		A		
	10.10	199.90		
4 3/4 195.40	200.0		.28	199.62
4 2/10		B		
	9.03	208.65		
4 4/4 A5.5				
3 4/10				
195				
-4 8/10				
3 9/10				
+0 1/4 200.0				
7/10 201.5				
4 8/10				
203.1				
5 5/10				
3 7/10				
9 0/10 199.6				
3 3/10				
7 7/10 200.9				
3 2/10				
6 3/10 202.3				
3 8/10				
4 3/10 204.3				
4 0/10				

4.6

Sta.	Elev.	Grade	(Offset Cut)
1170+75		195.30	10 4/12
1171		196.07	10 0/12
+25		196.83	10.2
+50		197.60	11 0/12
+59 3/12	B.C	197.88	10.9
+84 3/12		198.65	10.0
1172+09 3/12		199.42	8.9
+34 3/12		200.19	9.7
+59 3/12		200.96	11.1
+70.4	E.C	201.29	10.1
+75		201.43	11.1
1173		202.20	12.2

3.07%

℄	+	℄	−	El.
2 9/12 3 7/12				205.7
		208.65		
			6.01	202.64
2 5/12 4 4/12				206.1
		12.77	2 C 5/12	4.1
1 1/12 4 2/12				207.5
0 0/12 4 1/12				208.6
1 6/12 3 3/12				208.8 C
6 8/12 4 0/12				208.6 C
7 1/12 5 1/12				208.3 C
5 5/12 4 4/12				209.9
3 3/12 4 1/12				212.1
4 0/12 4 5/12				211.4
2 9/12 3 8/12				212.5
1 0/12 3 4/12				214.4

Sta.	Elev.	Grade		(offset cut)	L	℄		+	⊼	−	El.
1									215.41		
1173+25		202.97		12.4	$\frac{0^{0}}{3^{6}}$ 215.4					5.22	210.19
								6.94	217.13		T.P 1173+92.2
+50		203.73		11.6	$\frac{1^{8}}{3^{9}}$ 215.3					-.42	216.71
								0.95	217.66		
+75		204.50		11.7	$\frac{0^{9}}{4^{1}}$ 216.2					2.23	215.43
								12.83	228.26		
+92.2	B.C.	205.03		11.7	$\frac{0^{4}}{3.^{6}}$ 216.17						
1174+10⁸		205.60	+3.067%	11.8	$\frac{0^{3}}{4^{0}}$ 217.4						
~~+44²~~		[illegible]									
+29.1	E.C.	206.16		10.8	$\frac{0^{7}}{3^{8}}$ 217.0						
+50		206.80		11.1	$\frac{+0^{2}}{3^{6}}$ 217.9						
+75		207.57		8.5	$\frac{1^{6}}{4^{1}}$ 216.1						
1175		208.33 ✓		5.8	$\frac{3^{6}}{7^{1}}$ 214.1						
+25		209.10		6.3	$\frac{2^{2}}{3^{7}}$ 215.4						
+50		209.87		8.8	$\frac{9^{6}}{4^{2}}$ 218.7						

Sta.	Elev. Grade	(offset cut)	℄	+ T − El.
1175+75	210.64	9.9	7 8 220.5 / 4 9	228.26
1176	211.40	10.6	6 3 222.0 / 4 5	2.25 226.01
+25	212.17	10.7	5 4 222.9 / 4 9	6.04 232.05
+50	212.94	11.7	3 7 224.6 / 4 4	
+75	213.70 +3.067%	12.7	1 9 226.4 / 3 9	
1177	214.47	11.8	2 0 226.3 / 4 9	
+25	215.24	(9.7)	3 4 224.9 / 4 8	
+34 2 BC.	215.52	8.4	4 4 223.9 / 4 1	
+50	216.00	7.4	4 1 223.4 / 5 3	
+57 5	216.18	8.0	4 1 224.2 / 5 3	
+80 6 EC.	216.73 +2.40% 36/220		3 6	
1178	217.20	11.2	+0 1 / 4 2	

Sta.	Elev.	Grade		(offset Cut)
1178+25		217.80		
+42.8	B.C.	218.23		
+69.3		218.86		
+92.8		219.43		
+95.6	E.C.	219.48		
1179		219.60	+ 2.40%	
+25		220.20		
+50		220.80		
+75		221.40		
1180		222.00		
+25		222.44	+ 1.75%	
+50		222.88		

		℄
10.8	3 4/4	228.6
10.0	3 8/40	228.2
9.6	3 5/5	228.5
9.8	2 7/4	229.3
10.8	2 2/40	229.8
10.8	1 0/40	231.0
11.3	+0 1/34	232.1
12.2	5 6/33	233.6
11.0	6 2/38	233.0
9.3	7 5/36	231.7
10.5	5 8/36	233.4

11.58 4

+	℄	−	El.
	232.05		B.M. 5.20 226.85
			226.87
12.29	239.16		

Sta.	Elev.	Grade		(offset cut)			+	℄	−	Elev.
								239.16		
1180+75		223.31		10.5	5 4 / 4 2	233.8			1.56	237.60
1181		223.75		11.0	4 4 / 4 3	234.8	7.37	244.97		B.M.
+20		224.19		11.2	3 8 / 4 3	235.4			10.61	234.36
+46		224.56	+1.75%	10.9	3 7 / 4 8	235.3				
+71		225.00		10.8	4 4 / 4 1	234.8				
+96		225.44		9.8	4 0 / 4 3	235.2				
1182+21		225.87		9.0	4 3 / 4 2	234.9				
+46		226.31		9.8	3 1 / 5 4	236.1				
+71		226.75		9.8	2 6 / 4 4	236.6				
+96		227.19		9.1	2 6 / 4 4	236.6				
1183+21		227.62		9.7	1 9 / 4 3	237.3				
+46		22806		9.4	1 7 / 7 3	237.5				

235.9
224.2
11.7

2.34.8
2 2 4.0
0 8

Sta.	Elev.	Grade	(Offset cut.)	¢	
1183+57^{0} E.C.		228.25 (+1.75%)	8.2	$\frac{2^{8}}{8^{8}}$ 236.4	
+75		228.56	10.0	$\frac{1^{6}}{7^{3}}$ 237.6	
1184+00		229.00	10.6	$\frac{5^{4}}{8^{2}}$ 239.6	
+25		229.12	13.6	$\frac{2^{3}}{6^{8}}$ 242.7	
+50		229.25	13.9	$\frac{1^{9}}{4^{2}}$ 243.1	
+65^{5} B.C.		229.45		244.4	
+75^{5}		229.50	14.9	$\frac{}{4^{0}}$	
+85^{5}		229.55	14.1	$\frac{1^{4}}{4^{0}}$ 243.6	
+95^{5}		229.60 (+0.50%)	14.6	$\frac{0^{9}}{4^{0}}$ 244.1	
1185+05^{5}		229.65	13.6	$\frac{3^{3}}{5^{0}}$ 5^{8} A 240.2	10.6
+15^{5}		229.70	11.7	$\frac{5^{1}}{5^{0}}$ 6^{1} A 240.4	10.2
+25^{5}		229.75	11.1	$\frac{5^{6}}{5^{0}}$ 6^{2} A	10.0
+45^{5}		229.85	9.8	$\frac{6^{9}}{15^{0}}$ 6^{6} A	9.5
+58^{2}		229.92	7.7	$\frac{8^{9}}{15^{0}}$ 5^{8} A 240.2	10.3
+75 $\frac{58.9}{16.1}$		229.88	7.8	$\frac{8^{8}}{15^{0}}$ 5^{2} A 240.3	10.4
1186		230.00	13.8	$\frac{2^{7}}{2^{8}}$ 5^{3} 240.7	10.7

	+	π	−	El.
	11.58	A 245.97		234.389
T.P.			.87	245.10
	7.91	B 253.01		
			2.73	250.28
	10.83	C 261.11		
			1.36	269.75
	9.75	D 269.50		
			1.95	267.55
	7.58	E 275.13		
			2.87	272.26
	10.18	F 283.44		
			2.07	280.37
	12.72	G 293.09		

Note. From Sta. 1185+05^{5} to Sta. Cuts at ¢ were taken.

Sta.	Elev.	Grade			Cut.	℄ ℄ Cut.
				↑ A 245.97		
1186+25		231.67			14.2	56 B / 12 0 45 A 241.5 9.8
+50		233.34			14.2	6 0 / 17 0 B 3 4 A 242.6 9.3
+75 B.C.		235.06			15.0	3 4 / 14 3 B 1 9 A 244.1 9.0
1186+93 1		236.21	+6.67%	T B 253.01	14.2	2 9 / 15 0 B 1 2 A 245.0 8.8
1187 +10 2 E.C.		237.35			13.2	2 9 / 14 5 B 7 2 B 245.8 8.4
+25		238.34			13.5	1 7 / 13 3 B 7 2 B 246.0 7.7
+50		240.00 X			11.3	2 3 / 12 1 B 5 7 B 247.3 7.3
+75		241.14			12.8	7 7 / 13 8 C 4 9 B 248.1 7.0
+92 3 B.C.		241.92			11.6	0 0 / 13 8 B 4 4 B 248.6 6.7
~~1188+17 2~~			4.533%			
+30 9		243.67			12.9	5 0 / 15 9 C 2 8 B 250.2 6.5
~~+42 2~~						
+69 5 E.C.		245.38			13.9	2 3 / 16 2 C 9 1 C 252.0 6.6

253.3

261.1

Sta.	Elev.	Grade	π "C" 261.11	Offset Cut	℄	℄ Cut	
1188+75		245.63		13.2	2.8 / 16.3 C 9.0 C (252.1)	6.5	
1189		246.80		10.8	4.0 / 15.7 C 8.5 C (252.6)	5.8	
+25		247.93		11.1	2.6 / 14.5 C 7.1 C (254.0)	6.1	
+50		261.84 249.07 12.77		10.8	1.7 / 13.6 C 5.9 C (255.2)	6.1	
+71.8 Δ		261.84 250.24 11.60		12.8	7.0 / 15.4 D 4.8 C (256.3)	6.1	
1190		261.84 251.33 10.51 4.533%		11.3	7.4 / 14.6 D 3.8 C (257.3)	6.0	
+25		261.84 252.47 9.37		10.6	6.9 / 14.1 D 2.7 C (258.4)	5.9	261.1
+50		261.84 253.60 8.24	π "D" 269.50	10.7	5.7 / 12.4 D 1.4 C (259.7)	6.1	
+75		254.73		10.4	4.9 / 11.8 D 8.5 D (261.0)	6.3	263.5
1191		261.84 255.87 5.97		11.5	2.6 / 13.2 D 7.4 D (262.1)	6.2	269.5 13
+25		261.84 257.00 4.84		13.0	0.9 / 14.2 D 6.0 D (263.5)	6.5	
+50		258.13		13.9	3.6 / 10.2 E 5.3 D (264.2)	6.1	

From here use Old Cross Sections

Sta.	Elev.	Grade		offset Cut.
1191+75		259.27		9.7
1192		260.40		9.5
+25		261.53		10.9
+45.8		262.48		14 2/6
+75		263.80		13 1/4
1193		264.93		10 2/4
+25		266.06		7 8/3 2
+50		267.20		7 7/3 8 S
+75		268.33		6 6/3 6 S
1194		269.47		4 3/3 6 S
+25		270.60		3 6/4 2 S
+50		271.73		2 1/3 9 S

4.533%

offset Cut offset

℄	℄ Cut.
1 0/5 4 D 5 0 D	5.2
5 7/7 2 E 3 5 D	5.6
3 2/8 9 E 2 3 D	5.7

264.5
266.0
267.2
269.5

Sta.	Elev.	Grade		Offset	Cut	℄	℄ Cut	+	⊼	−	El.
									12.72		
									293.09 ~~[illegible]~~		
1194+62² BC		272.29	4.533%								
+75		272.86									
+87²		273.42									
				Use Old Cross Sections to here-							
1194+90⁸		273.58		⊼F 283.44	9.6	9.2 / 15.5 G	3.6 F 279.8	℄ Cut.			
1195+00		274.00	X								
+19³ EC	✓	274.93		⊼G 293.09	8.2	10.0 / 15.8 G	280.2 12.9 G				
~~+25~~											
+50	3.65 ✓	276.40			7.8	8.9 / 15.3 G	282.5 10.6 G	6.1			
+75	2.45 ✓	277.60	4.80%		7.6	7.9 / 13.2 G	283.4 9.7 G	5.8	293.1	25	
1196	1.25 ✓	278.80			6.2	8.1 / 11.6 G	284.7 8.4 G	5.9			
+25	11.38 ✓	280.00			7.2	5.9 / 12.2 G	286.3 6.8 G	6.3			
+50	10.18 ✓	281.20			7.7	4.2 / 13.3 G	287.7 5.4 G	6.5			
+75	8.98 ✓	282.40			6.0	3.7 / 11.6 G	288.7 4.4 G	6.3			
1197	7.~~78~~ 69 ✓	283.60			7.4	2.1 / 11.8 G	289.8 3.3 G	6.2			

Sta.	Elev.	Grade		Offset	Cut
				π G 293.09	
1197+25	6.58 ✓	284.80	4.80%		6.0
+50	5.38 ✓	286.00 X		π H 305.01	7.3
+75	3.98 ✓	287.40			7.4
1198	2.58 ✓	288.80			7.5
+25	10.32 ✓ (1.18)	290.20			8.3
+50	8.92 ✓	291.60			8.1
+75	7.52 ✓	293.00	5.60%		9.0
1199	6.12 ✓	294.40			10.2
+25	9.46 ✓	295.80			10.6
+50	8.06 ✓	297.20			9.2
+75	6.66 ✓	298.60		π I 316.42	9.8
1200	5.26 ✓	300.00 X	5.05%		10.2

	℄	℄ Cut	+	π	−	El.
1^{3} / 12^{0} G	291.0 / 2.1 G	6.2		G 293.09	0.43	292.66
11^{7} / 11^{7} H	292.5 (293.1) / 0.6 G	6.5	12.35	H 305.01 (1.99)	0.16	304.85
10^{2} / 12^{2} H	294.0 / 11.0 H	6.6	11.57	I 316.42		
8^{7} / 13^{9}	295.1 / 9.9 H	6.3				
6^{5} / 14^{3}	296.4 ✓ / 8.6 H	6.2				
5^{3} / 13^{7} H	297.8 ✓ / 7.2 H	6.2				
4^{5} / 14^{0} H	298.9 ✓ / 6.1 H ✓	5.9				
1^{8} / 14^{6} H	300.3 / 4.7 H	5.9				
0^{1} / 15^{0} H	302.0 ✓ / 3.0 H ✓	6.2				
0^{1} / 13^{1} H	303.3 / 1.7 H	6.1				
9^{5} / 13^{1} I	305.0 ✓ / 0^{0} H	6.4				
7^{3} / 14^{0} I	306.6 / 9^{8} I	6.6				

Sta.	Elev. Grade		offset Cut.	
1200 +25	4.00	301.26		10.9
+50	2.74	302.52		10.0
+58.2 Δ	2.30	302.96	11.2	0 5/15 6 R
+75	1.47	303.79	9.5	1 1/16 6 R
1201	9.32	305.05	8.0	1 7/14 4 R
+25	8.06	306.31	8.0	0 1/15 5 R
+50	6.79	307.58	8.0	10 3/4 2 P
+75	5.53	308.84	8.5	8 6/5 1 P
1202	4.27	310.10	8.3	7 5/5 1/2 P
+25	3.01	311.36	7.9	6 6/3 6 P
+50	1.75	312.62	8.4	4 4/4 5 P
+75	11.04	313.89	8.3	3 2/5 3 P

5.05 ±0

℄	℄ Cut.	+	℄	−	El.
	307.6		I 316.42		
5 7/14 8	I 8 8 I				T.P.
				0.98	315.44
5 4/13 2	308.7 I 7.7 I				
	309.4				
	7.0 I				

12 4/5 0 4

Sta.	Elev.	Grade		offset cuts	offsets
1203	9.78 ✓	315.15		10.6	$\frac{0\ 2}{6\ 3}$ P
+25	8.52 ✓	316.41			
+50	7.25 ✓	317.68		8.6	$\frac{10\ 5}{7\ 1}$ M
+75	5.99 ✓	318.94	+5.05%	8.1	$\frac{9\ 8}{5\ 2}$ M
1204	4.73 ✓	320.20		7.6	$\frac{9\ 0}{4\ 1}$ M
+25	3.47 ✓	321.46		5.1	$\frac{10\ 2}{3\ 6}$ M
+50	2.21 ✓	322.72		6.6	$\frac{7\ 5}{3\ 2}$ M
+75	.93 ✓	324.00 ✗			
+77.8	B.C. ✓	324.06		7.5	$\frac{5\ 2}{3\ 5}$ M
+97.8	11.47 ✓	324.46	+2.00%	6.2	$\frac{6\ 1}{3\ 3}$ M
+17.8	11.07 ✓	324.86		8.4	$\frac{3\ 5}{3\ 8}$ M
+37.8	10.67	325.26		10.6	$\frac{0\ 5}{6\ 2}$ M
+57.8	10.29 ✓	325.66		12.2	$\frac{5\ 6}{8\ 0}$ K

Sta.	Elev.	Grade		offset cuts	offsets
1205+86	cc. 9.77	326.225	+2.00%	12.5	48 / 77 K
1206+02	BC 9.39	326.54		11.4	56 / 81 / 90 K
+22		326.94			
+25	8,93	327.00		12.6	112 / 142 K
+42	12.17	327.17		14.9	193 / 232 K
+52		327.27		11.1	82 / 122 K
+62	11.97	327.37		8.9	72 / 98 K
+72		327.47		6.2	58 K
+82	11.77	327.57	+1.00%	3.9	120 / 65 K
1207+032	EC.	327.791			
+20		328.00			
+50		328.671			
+70		329.33	+2.667%		
1208	12,92	330.00			
+20	11.12	331.8	+2.07%		
+33	BC. 10.18	332.49			

+	T. K	-	Elev	
			342.30	B.M.
1.23	343.53			
		9.53	334.00	
2.81	M. 336.81			
		12.97	323.84	
2.10	P 325.94			
		12.97	312.97	T.P.
1.71	R 314.68			
		11.41	303.27	
0.51	303.78			
		11.94	291.84	
0.70	292.54			
		12.01	280.53	
			4.43	
1.71	S 282.24		284.96	
			18	
			283.2	
			273.6	
			9.6	
3.26				

Sta.	Elev.	Grade		Offset cut.	L.	℄	R.	+	⊼	−	Elev.
											366.14
1208+58²	8.68 ✓	334.24			5⁰			.97	367.11		
+83²		336.04									
1209+08²		337.84									
+33² E.C.		339.64									
+38² B.C.			+7.20%								
+63											
+88											
1210+13											
+38		347.14									
+44² / +50		348.00	X								
+63		348.75									
+88		350.20	+5.80%								
1211+13		351.65									
1211+19.2		352.01 / 348.2									

℄ Cuts -

-11⁶ 355.5 — -11³/15 355.8

11⁰ 356.1 — 10⁵/15 356.6

9⁸ 357.3 — 9⁹/15 357.2

Sta.	Elev.	Grade	
1211+38		353.10	
+63		354.55	
+88		356.00	
1212+11.2 Equation		357.35	+5.80%
+13.2			
+25		358.03 / 359.10	
+43.1		353.00	X
+50		353.03	
+94.35		353.22	
1213		353.24	+0.426%
+50		353.45	
1214		353.67	
+50		353.88	
1215		354.09	

℄		Cut.	+	−	Elev.
8.4 358.7	8.9 358.2 / 15.0			367.1	
7.6 359.5	7.2 359.9 / 15.0				
6.0 361.1	5.6 361.5 / 15				
4.6 362.5	3.9 363.2 / 15				
363.0					
3.8 363.3	3.6 363.5 / 15.0				
9.6 358.8 (358.4)	9.6 358.8	5.8			359.97
			8.39	368.36	
8.6 359.8	8.5 359.9	6.7			
7.6 360.8	7.9 360.5	7.1			
7.0 361.4	6.8 361.6	7.9			
6.2	5.6 362.8	8.9			
5.3 363.1	4.8 363.6	9.5			

Sta.	Elev.	Grade	Cut.	℄	15'R	Cut.	+	⊼	-	Elev.
							-	368.36		
1215+50		354.31		5^{0}	4^{0} 364.4	10.1				
1216		354.52		4^{5} 363.9	4^{6} 364.3	9.8				
+50		354.73		4^{2}	4^{4} 364.0	9.3				
1217		354.94		4^{6} 363.8	4^{6} 364.3	9.3				
+50		355.16		4^{4}	4^{0} 364.4	9.2				
1218		355.37		4^{0} 364.4	3^{9} 364.5	9.1				
+50		355.58		3^{5}	3^{5} 364.9	9.3				
1219		355.80		3^{5} 364.9	3^{6} 364.8	9.0				BM.#
			Cut.	15'L	℄ Cut.					365.13
$+54^{35}$		356.02		4^{8} 365.7	4^{8} 365.1		4.75	369.88		
$1220+14^{35}$		355.51		4^{7} 365.2	5^{0} 364.9				4.74	365.14
$+74^{35}$		355.00		4^{6} 365.3	4^{9} 365.0					
$1221+04^{35}$		355.00		4^{1} 365.5	4^{5} 365.4					

Sta.	Elev.	Grade		Cut.	15'L	℄	+	HI	-	El.
								.369.88		
1221+64.35		356.10		8.2	4.8 (365.1)	4.6 (365.3)				
~~1222~~				8.7	4.1 (365.8)	4.2 (365.9)				
+29.35		357.18								
+50		357.29		8.7	3.9 (366.0)	3.9 (366.0)				
1223		357.50	+0.426%							
+50		357.714								
1224		357.93								
+16		358.00	X							
+50		358.03								
1225		358.06								
+50		358.10	.077%							
1226		358.14								
+50		358.18								
1227		358.22								

Sta.	Elev.	Grade		Rod
1227 + 50		358.26		
1228		358.30		
+ 50		358.33	50	
1229		358.37	77	
+ 50		358.41	.0	
1230		358.45	+	
+ 50		358.49		
+ 66		358.5	X	
1231		358.58		
+ 50		358.73		
1232		358.87	50	12.45
+ 50		359.01	28	12.31
1233		359.15	+	12.17

1233+10		359.29			12.03
1234		359.43			11.89
+50		359.57	+ .28		11.75
1235		359.71	+		11.61
+50		359.85			11.47
1236		359.99		8.6	8 2/10°
+04		360.0	X		
+50		360.42		9.0	7 9/10
1237		360.88		9.2	7 2/10
+50		361.34	+ .9239	9.4	6 4/10
1238		361.81		9.7	5 8/10
+50		362.27		10.0	5 0/10
1239		362.73		10.8	3 8/10

	+	π	- El.
			369.10
8.18	377.28		

				10' Offset	Cut
1239+50		363.19		10.1	4^{0}
1240		363.65	+ .923%	10.1	3^{6}
+50		364.11		10.2	3^{0}
1241		364.58		10.2	2^{5}
+50		365.04		10.2	2^{1}
1242		365.50		10.6	1^{7}
+50		365.96		11.3	0^{0}
$+54^{3}$		366.00	X		
1243		367.06			
+50		368.22		9.8	8^{0}
1244		369.38	+ 2.32%	9.3	7^{3}
+50		370.54		8.8	6^{7}
1245		371.70		8.4	5^{9}

℄		+	⊼	-	El
					381.96
		4.02	385.98		
				0.76	385.22
		5.11	390.33		
6^{9} 378.1					
6^{1} 378.9					
5^{4} 380.6					

		2.33%		10' offset	¢ HI=386.0				
1245+50	372.86		8.5	4^6	4^4 381.6				
+99^3	374.00 X								
1246	374.00		7.9	4^1	3^9 382.1				
+50	374.17		8.1	3^7	3^2 382.8				
1247	374.34		8.6	3^1	2^7 383.3				
+50	374.50		9.2 8' offs	2^3	2^2 383.8				
1248	374.67		9.3	2^0	1^7 384.3				
+50	374.83	+0.333%	9.7	1^5	1^3 384.7				
1249	375.00		10.2	0^8	0^8 385.2				
+50	375.17		9.7	5^4	5^1 385.2		390.33	5.22	385.11
1250	375.33		9.9	5^1	4^7 385.6				El. 386.78
+50	375.50		10.1	5^3 A	5^0 B 385.9	4.10	(B) 390.88		
1251	375.67		10.1	5^1 B	4^8 B 386.1				

Sta.	Elev.	Grade		10' offsets	
1251+50		375.83		10.2	4.9
1252		376.00		10.6	4.3
+15		376.05			
				15' offsets	
+50		376.17 ✓		10.1	6.1
1253		376.33 ✓	+0.333%	10.2	5.9
+50		376.50 ✓		10.1	5.8
1254		376.67		10.0	5.7
+50		376.83		10.1	5.5
1255		377.00 X		9.9	5.5
+50		376.94		10.8	4.7
1256		376.88	−0.125%	9.8 ✓	5.7
				5' offsets	
+50		376.81		9.7 ✓	5.9
1257		376.75		9.5 ✓	6.1

℄ 390.9		+	HI	−	El.
4 R 386.4 A	BM #175				386.78
		5.59	392.37		
4 L 386.8 A	BM #176			5.17	387.20

+	HI	−	El.
			385.11
2.89	388.00		
			386.78
2.92	389.70		
		1.90	387.80
2.06	389.86		

			Cut	5' offset	¢	¢ Cut	+	π	−	El.
										387.21
1257+50	376.69		10.2	5^{1} 386.5	5^{2} 386.6	10.1	4.38	391.59		
									5.35	386.24
1258	376.62		9.8	5^{3} 386.4	5^{0} 386.6	10.0				
+50	376.56		9.1	5^{9} 385.7	5^{8} 385.8	9.2				
1259	376.50		9.3	5^{8} 385.8	5^{8} 385.8	9.3				
+50	376.44		10.0	5^{2} 386.4	5^{1} 386.5	10.1				
				8' offsets						
1260	376.38	−0.125%	10.1	5^{1} 386.5	4^{9} 386.7	10.3				
+50	376.31		10.5	4^{8} 386.8	4^{7} 386.9	10.6				
1261	376.25		10.9	4^{5} 387.1	4^{4} 387.2	11.0				
+50	376.19		11.1	$4.^{3}$ 387.3	4^{2} 387.4	11.2				B.M. Swift St. 387.71
				10' offsets						
1262	376.12		11.4	4^{1}	4^{1} 387.5		4.54	391.65		
+50	376.06		10.7	48	4^{6}					
1263	376.00 X		10.3	5^{3}	5^{1} 386.5					

			10' offsets
1263+50	375.58	10.3	5
1264	375.16	10.1	6
+50	374.74	10.3	6
1265	374.32	10.2	7
+50	373.90	10.3	2
1266	373.48	9.8	2
+50	373.06	9.6	3.5
1267	372.64	9.7	3
+50	372.22	9.6	4
1268	371.80	9.5	4
+50	371.38	9.8	5
+95.8	371.00		
1269	370.99		

℄	E. Cut.
	391.6
5	386.1
5	385.7
6	385.2
6	384.7

391.65

386.23

+	℄	−	El.
			384.03
2.20	386.23		
		7.65	378.58
		B.M.	378.56
4.33	382.89		
		5.92	376.97
		B.M.	376.98
7.78	384.76		
		4.69	B.M. 380.07

		⊼	10' offsets		¢	
		386.23				
1269+50	370.93	✓	9.6	5^{7}		380.5
1270	370.88	✓	9.2	6^{1}		
+50	370.82	✓	8.9	6^{5}		
1271	370.77	✓	8.4	7^{0}		
+50	370.71		8.1	7^{4}		
1272	370.66		7.8	7^{7}		382.97
+50	370.60	⊼ 362.89	8.4	7^{2}	4^{3}	
1273	370.55		7.6	4^{7}	4^{4}	378.5
+50	370.49		7.4	5^{0}	4^{7}	
1274	370.44		7.3	5^{2}	4^{8}	378.1
+50	370.38		7.1	5^{4}	5^{1}	
1275	370.33		6.9	5^{7}		

					10' offsets
			↑ 382.89		
1275 +50		370.27	✓	6.9	5 7/
1276		370.22	9.98 ✓	6.8	5 9/
			0.11%		
+50		370.16	10.04 ✓	6.6	6 1/
1277		370.11	10.09 ✓	6.6	6 2/
+40		370.06	10.14 ✓	6.6	6 2/
+97½		370.0 ✓	10.20 ✓		
1278		370.01		7.0	5 9/
			↑ 384.76		
+50		370.12	10.08 ✓	7.4	7 3/
1279		370.23	9.97 ✓	7.8	6 7/
			2.24%		
+50		370.34	9.86 ✓	8.3	6 2/
1280		370.45	9.75	9.0	5 4/
			9.27 / 48		
+50		370.56	9.64	9.4	4 8/
1281		370.68		9.4	4 6/

℄		
4 6/	377.2	
7 1/		
6 5/	378.3	
5 8/		
5 2/	379.6	
4 6/		
4 5/	380.3	

			π 384.76	Cut	10' offsets	℄	+	π	-	El
1281+50		370.79		9.4	4^{6}	4^{4}				
1282		370.90		9.6	4^{3}	4^{1}				
+50		371.01		9.8	4^{0}	3^{8}				
1283		371.13		10.0	3^{7}	3^{3}				
+50		371.24		10.3	3^{3}	3^{0}				
1284		.224% 371.35		10.7	2^{8}	2^{6}				
			387.39							383.18
+67		371.50		11.0	4^{2}	4^{6}	4.21	387.39		
+89 P.I.		371.55		10.9	4^{2}	4^{2}			7.38	380.01
~~1284~~		~~371.57~~				4^{2}				
1285+17		371.61		11.0	4^{8} 387.4 4.8 382.6					
~~+50~~		~~371.69~~								
+55^6 P.I.		371.70		10.4	5^{3}	5^{0}				
1286		371.80 ✓		10.0	5^{6}					
✓+50		371.91	10.55✓	9.9	5^{6}					
✓+90		372.0 X	10.46✓							
1287 ✓		371.87	-1.30%	9.7	5^{8}					

		Grade	℄ 387.39	10' offsets	
1287+50		371.22	11.24 ✓	10.1	6
1288	X	370.57	11.89 ✓	11.3	6
+70	—	369.92	12.54 ✓	10.8	6
			12.03		
			.51		
1289		369.27	13.19	11.1	2
+50	X	368.62	✓	10.5	3
1290		367.97	✓	10.2	4
+50		367.32	✓	10.7	5
+75		367.00	X		
1291		366.51		9.3	6
+50		365.57		9.2	7
1292		364.63		9.3	8
+50		363.69	1.88	9.4	9
1293		362.75		10.0	10

+	℄	−	Elev	
			379.99	B.M.
2.73	382.72			
		10.79	371.93	
1.55	373.48			
		7.86	365.62	

380.4
379.1
378.2
377.0
375.8
374.8
373.9
373.1
372.7

382.96
12.03
370.43 El.
11.01
381.44
367.46
14.12 379.98
12.99
1.18

		Grade		offset Cut	
1293 +50		361.81		9.8	11 1/2 X 371.6
1294		360.87		9.7	12 1/2 X 370.6
+50		359.93	373.48	9.3	4 3/4 Y 369.2
1295		358.99	-1.88%	8.8	5 7/8 Y 367.8
+50		358.04		8.8	6 1/2 Y 366.8
1296		357.11		8.5	7 9/10 Y 365.6
+50		356.17		9.4	7 9/10 Y 365.6
+85.5		355.50 X			
1297		355.61		9.7	8 3/4 Y 365.2
+50		355.56		9.9	8 1/2 Y 365.5
1298		355.61	+0.094%	10.0	7 9/10 Y 365.6
+50		355.65		10.2	7 7/8 Y 365.8
1299		355.70		10.2	7 6/8 Y 365.9

		Grade		offset Cut,	
					366.0
1299+50		355.75	373.48	10.2	7⁵ Y
1300		355.80		10.4	7³ Y
+50		355.84		10.7	7⁰ Y
1301		355.89	+0.09 %		
+50		355.94			
1302		355.98			
+15		356.00			
+50		356.46			
				372.25	
1303		357.11		10.0	5⁵ 367.1
+50		357.77		9.5	4⁹ 367.3
1304		358.42	-1.31 %	9.3	4⁵ 367.7
+50		359.08		8.9	4.2 368.5
1305		359.73			3.5 368.7

5.65

+	#	T	-	El.
				366.60
	5.65	372.25		

		+1.31%	⊼ 372.25	369.8	
1305+50	360.39		9.4	2.42	
+95⁰	361.0				
				371.1	
1306	361.10		10.0	1.1	
+50	362.08				
1307	363.06				
+50	364.04				
1307+70⁰³ BC.		+1.96%			
+80⁰³					
+90					
	.98				
1308+00	365.02				
		⊼ 380.97		10' L. 6⁰ 375.0	
+09²⁷ EC					
+50	366.00				
1309	367.00				

Sept. 28, 1926.

℄	+	⊼	−	El.	
				375.34	BM #190.
	5.63	380.97			
	10' R 5¹ 375.9		offset at 8.9		

1309+50	367.05	
1310	367.09	
+50	367.14	
1311	367.18	
+50	367.23	+.091%
1312	367.27	
+50	367.32	
1313	367.36	
+50	367.41	
1314	367.46	
+50	367.50	
1315	367.55	

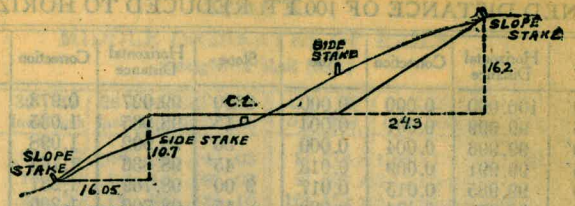
π	10' R	+	π.	-	El.
380.97		El offset	380.97	offset Cut.	
	4^{9}	376.1		9.1	
	4^{9}	376.1		9.0	
	4^{8}	376.2		9.1	
	4^{9}	376.1		8.9	
	5^{0}	376.0		8.8	
	5^{1}	375.9		8.6	
	5^{3}	375.7		8.4	
	5^{4}	375.6		8.2	
	5^{6}	375.4		8.0	
	5^{4}	375.6		8.1	
	5^{6}	375.4		7.9	
	5^{4}	375.6		8.1	

Sta.	El	Grade
1315+50		367.59
1316		367.64
+50		367.68
1317		367.73
+50		367.77
1317+61.36	B.C.	
+71.4		
+81.4		
+91.4		
1318+01.4		
+11.4		
+17.51	E.C.	

π 380.97		+	π 380.97	Offset Cut	El.
	5.4	375.6		8.0	
	6.0	375.0		7.4	
	6.4	374.6		6.9	
	6.8	374.2		6.5	
	7'	373.9		6.1	

1318+50

+71 02



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18.15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54.15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58.50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

377.3
8.7
368.6
360.0
8.6

364.9
6.1
358.8

358.8
353.0
5.8