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LEFAX FILING INDEX

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LEFAX, PHILADELPHIA, PA. 42

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(5022)



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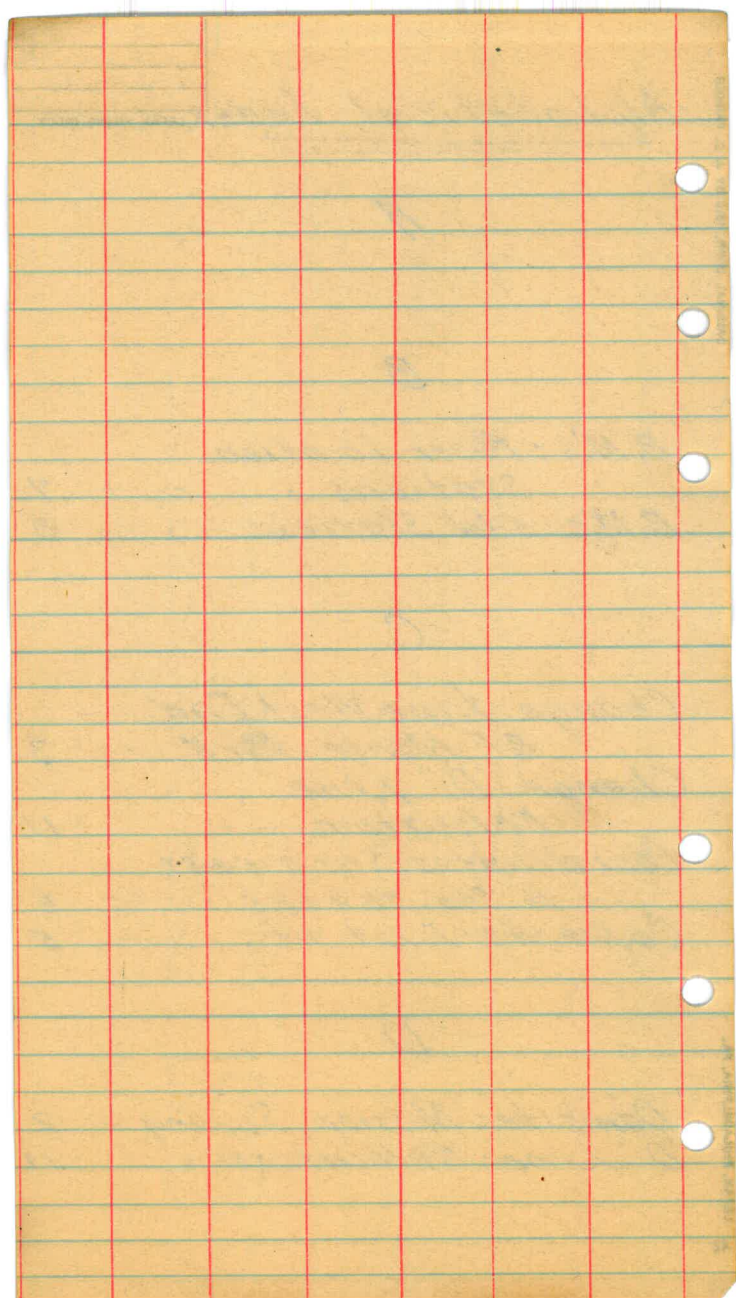
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F

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G

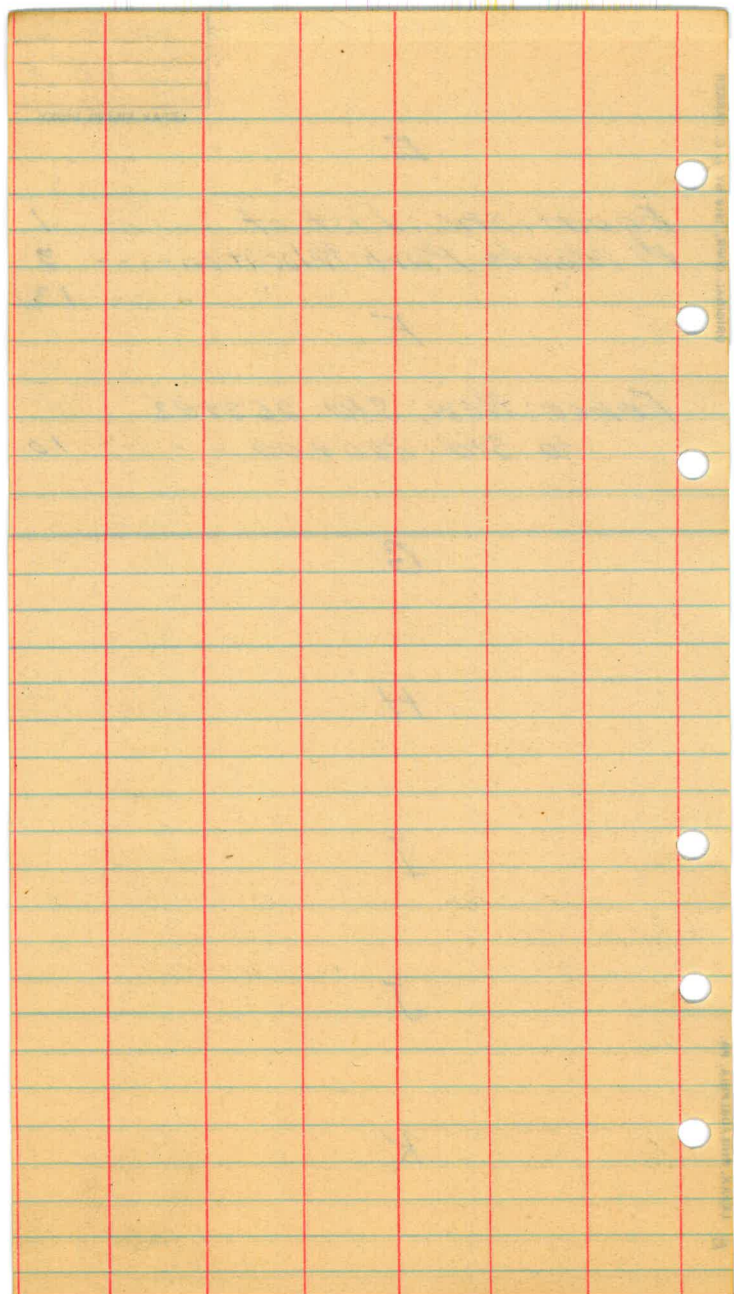
H

I

J

K





L

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 El Monte Park - - - 3  
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M

Mission Dam site Survey - - 2

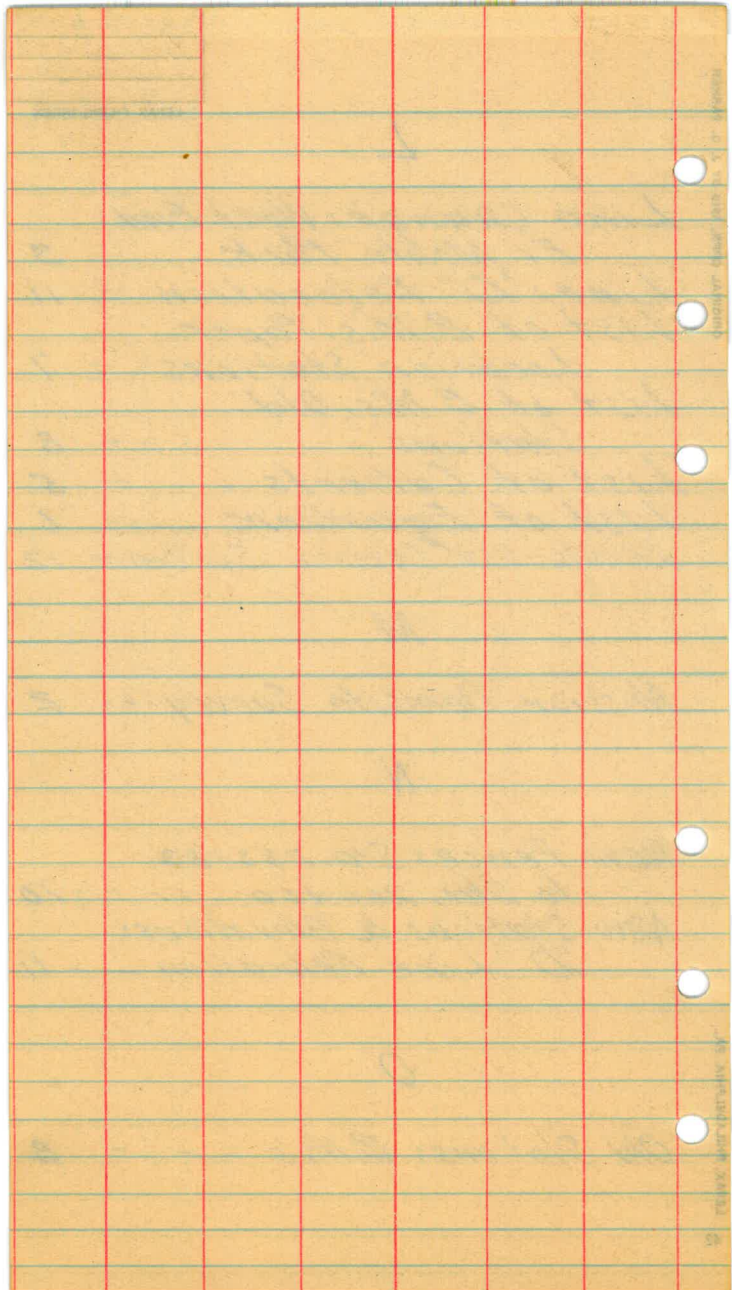
N

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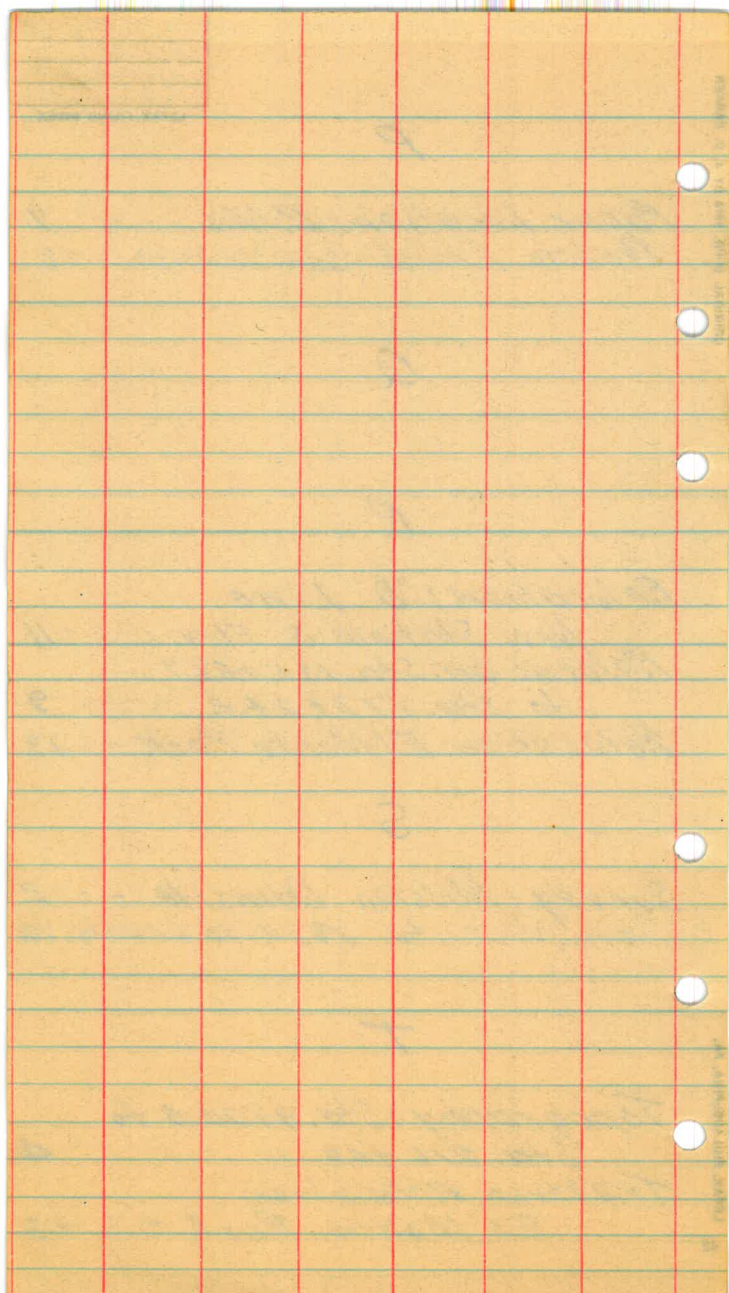
S

Survey: Mission Dam site --- 2  
 San Vicente - Profile Levels 12

T

Topography: Sta. 9+28.8 to  
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 Traverse Relocation:  
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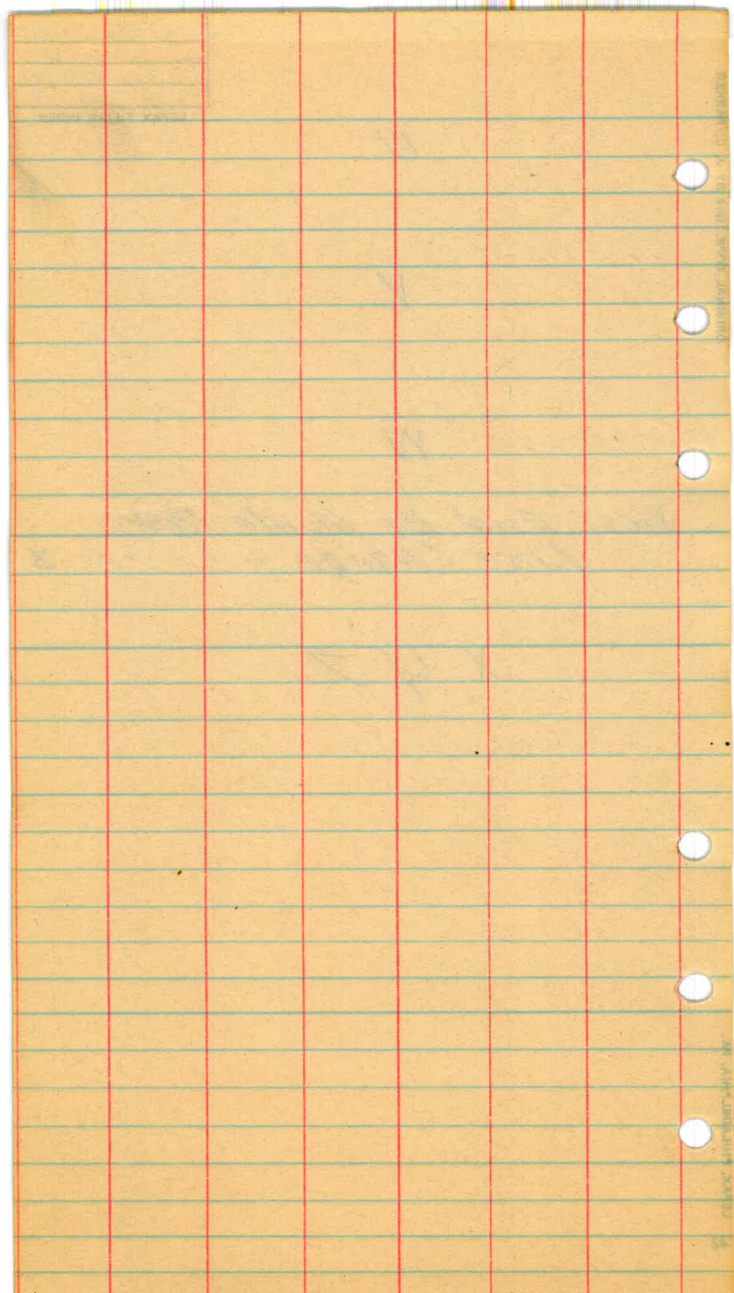
U

V

W

West End El Monte Park:  
Line Change - - - - - 3

X Y Z

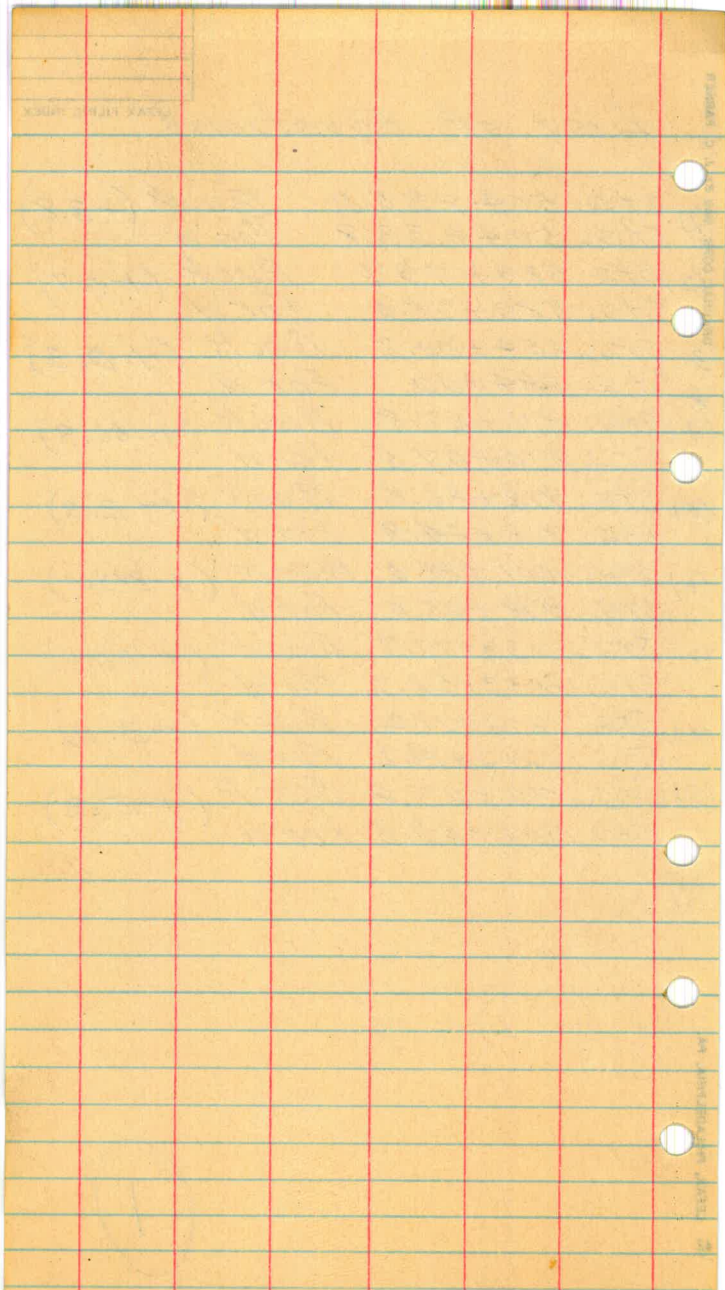




## List of Equations

- (1) Sta. 504 + 30.0 Back (-3.8)  
Sta. 504 + 33.8 For'd
- (2) Sta. 589 + 79.7 Back (+1.7)  
Sta. 589 + 78.0 For'd
- (3) Sta. 684 + 00.3 Back (+0.3)  
Sta. 684 + 00 For'd
- \* (4) Sta. 811 + 67.8 Back (+160.3)  
Sta. 810 + 07.5 For'd
- (5) Sta. 918 + 86.6 Back (+2.3)  
Sta. 918 + 84.3 For'd
- (6) Sta. 1001 + 88.0 Back (+383.0)  
Sta. 998 + 05.0 For'd
- (7) Sta. 1139 + 72.7 Back (+20.0)  
Sta. 1139 + 52.7 For'd
- (8) Sta. 1212 + 11.2 Back (-3.0)  
Sta. 1212 + 14.2 For'd
- (9) Sta. 802 + 25.8 Back (+5.3)  
Sta. 802 + 20.5 For'd

(1)



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Dec =  $-11^{\circ}43'$   
Alt =  $29^{\circ}53'$  Hor. L =  $41^{\circ}30'L$   
Lat. =  $32^{\circ}50'$

Log sec. alt =  $0.06196$   
" " Lat =  $0.07559$   
0.13755

Co =  $27^{\circ}15'$

Sin Co.  $45839$   
Sin Dec.  $20307$

$25532$   $0.13755$   
Log =  $9.40708$

Log vers. sin =  $9.54463$

Az. =  $49^{\circ}29.6$

$49$   $29.6$   
 $41$   $30.0$   
 $N7^{\circ}59'.6W$

Bearing  ~~$N7^{\circ}59'.6W$~~   
 $N8^{\circ}00'W$

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Thurs. Feb. 18  
Observation at Cor. 8,  
Ranch El Cajon, to  
determine course from  
Cor. 8 to Cor 7,

Sun Watch Vert L Hor. L

$\phi$  9-07-25 29-30 42-48L

$\delta$  9-11-14 29-31 41-15

$\phi$  9-13-21 30-27 41-34

$\delta$  9-15-27 30-10 40-23

Time = 9<sup>h</sup> 11.5 A.M.

Alt = 29° 54.5

Ref =  $\frac{1.5}{29^{\circ} 53'.0}$

①

Survey South along  
East Line Lot 13  
Rancho Ex Mission  
to establish Cor # 14  
Lot 70

---

Converse.

Traverse from Cor # 9  
Rancho El Cajon to  
Establish So Line Lot 73.

---

Converse.  
Feb - 1926

Lot 13. Cor. 9. Cor # 8.

Cor # 7. Rancho El Cajon.

②

South Along East Line  
Lot 73 Rancho Ex Mission to  
Establish Cor. #19. Lot. 70

4+76<sup>3</sup>

19+78<sup>8</sup> P.O.T.

5+85

5+10 P.O.T.

4+20 P.O.T.

5.53°42'E

0+29

0+00 45°42'E

58°0'E



2

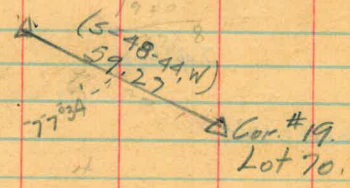
420

63.7

Property of Mrs Fitzherbert West.

16°20'

Slope Dist. = 63.2  
Vert. Δ = 16°20'



Nail.

77	34
53	42
180	16
131	
48	42

(Stadia Vert. Δ - 16°20' Dist. 460.)  
Corr. Dist. 423.6  
~~See chained Dist.~~

Stake on 340 Contour.

Cor. # 8. Rancho El Cajon (Lot 13, Cor. 9.)

Cor. #7 Rancho El Cajon.

Traverse from Cor. #8 Rancho  
El Cajon To Estab. So. Line Lot 73.

846+112 L. 7°36' ✓

5.8°57'E ✓

844+87 L. 6°11' ✓

5.1°21'E ✓

842+54 L. 22°17' ✓

5.4°50'N ✓

841+92 P.O.T. ✓

5.27°07'W ✓

838+33 L. 10°0' ✓

5.37°07'W ✓

835+83 L. 133°49' ✓

N. 9°06'N ✓

0+00 1°06' L ✓

N. 8°0'W ✓

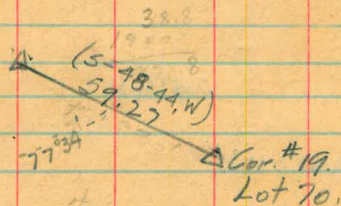
420

63.7

②

Property of W<sup>m</sup> Fitzherbert West.

16°20'

Slope Dist. = 63.2  
Vert. Δ = 16°20'

Nail.

(Stadia Vert. Δ = 16°20' Dist. 460.)  
Corr. Dist. 423.6  
~~See Stadia Dist.~~

Stake on 340 Contour.

Cor. # 8. Rancho El Cajon. (Lot 13, Cor. 9.)

Cor. #7 Rancho El Cajon.



Traverse from Cor. 8 Rancho  
El Cajon To Estab. 50 Line Lot 73.

5.8°51'E

846+172 L. 7°36' ✓

5.1°21'E ✓

844+187 L. 6°11' ✓

5.4°50'W ✓

842+154 L. 27°17' ✓

841+92° P.O.T. ✓

5.27°07'W ✓

838+338 L. 10°0' ✓

5.37°07'W ✓

835+183 L. 133°47' ✓

N. 9°06'W ✓

0+001°06' L ✓

N. 8°0'W ✓

3

Old Sta. 846+12.

124.8 ✓

$$\begin{array}{r} 27 \cdot 07 \\ 22 \cdot 17 \\ \hline 45 \cdot 0 \end{array}$$

Old Sta. 844+87

$$\begin{array}{r} 46+11.8 \\ 44+87 \\ \hline 124.8 \end{array} \quad \begin{array}{r} 842+54 \\ 41+92 \\ \hline 62 \end{array}$$

232.8 ✓

$$\begin{array}{r} 6 \cdot 7 \\ 4 \cdot 50 \\ \hline 1 \cdot 21 \end{array}$$

Old Sta. 842+54

$$\begin{array}{r} 9 \cdot 06 \\ 133 \cdot 47 \\ \hline 142 \cdot 53 \end{array}$$

62.0 ✓

$$\begin{array}{r} 359.1 \\ 62 \\ \hline 421.1 \end{array} \quad \begin{array}{r} 37 \cdot 07 \end{array}$$

Old Sta. 841+92.1

$$\begin{array}{r} 841+92.1 \\ 838+33.0 \\ \hline 359.1 \end{array}$$

359.1 ✓

Old Sta. 838+33.1

$$\begin{array}{r} 9 \cdot 06 \\ 133 \cdot 47 \\ \hline 142 \cdot 53 \end{array}$$

250.1 ✓

$$\begin{array}{r} 37 \cdot 07 \end{array}$$

Old Sta. 835+83.

117.6 ✓

Cor. #8. Rancho El Cajon.

Cor. #7.

"G" ✓

5.62°0' ✓

90  
62  
28

"F" L.10°0' ✓

5.72°0' ✓

"E" R.11°47' ✓

5.60°13' ✓

"D" R.13°50' ✓

5.46°23' ✓

"C" R.21°30' ✓

5.25°03' ✓

"B." R.23°03' ✓

5.2°0' ✓

"A" L.26°30' ✓

5.28°30' ✓

843+45 R.37°27' ✓

5.8°57' ✓

846+12 ✓



(4)

46 23  
13 50  
60 13

19° 44'  
95.4

9.973916  
1.979548  
7.53267

89.8

37 27  
8 57  
28 30  
340  
52 10

G 621.0 ✓

F 165.0 ✓

F 727.0 ✓

D" App. Axis of Dam. 100' West 7.53267

" 570 ✓

C" ✓

313.9 ✓

B" ✓

170.0 ✓

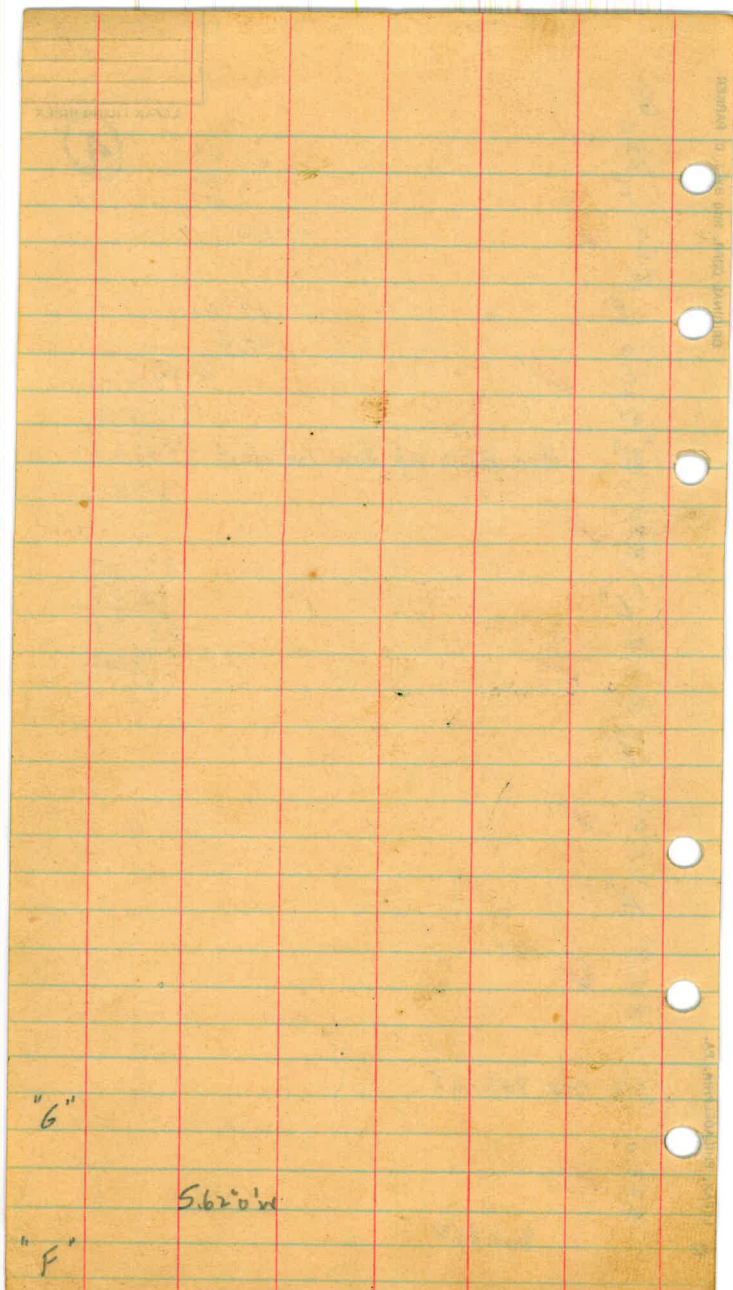
A" ✓

89.8 ✓

Old Sta. 848+45

233.0 ✓

846+12



"6"

5.62.0'w

"F"

Line Change -  
W. End El Monte Park.

Converse  
2/25/26

③



Line Change W. End El Monte  
("B" Line) Park.

$\Delta$   
140+21.7 L. 13° 0'

$\frac{3}{2}$   
139+67 B.C.

E = 31  
R = 477.47  
T = 54.4  
L = 108.3  
D = 12°

5.44° 33' W  
135+00 E.C.

$\Delta$   
134+76 L. 5° 46'

$\frac{2}{2}$   
134+52 B.C.

E = 0.6  
T = 24.05  
R = 477.47  
D = 12°  
L = 48.05

5.50° 19' W  
133+50 E.C.

$\Delta$   
133+27 R. 5° 40'

$\frac{2}{2}$   
133+00 B.C.

E = 0.6  
T = 23.6  
D = 12°  
R = 477.47  
L = 47.2

$\Delta$   
126+90

5.44° 39' W

P.I.  $\frac{3}{2}$   
126+90

Feb. 25.



173+45<sup>2</sup> B.C.

3.59°52'W 0.7

173+44<sup>2</sup> E  
168+53<sup>2</sup> E.C.

P.I.  
168+33<sup>2</sup> 19°23'R

168+14<sup>2</sup> B.C.

E =  
R = 114.59  
T = 19.6  
D = 50°  
L = 38.8

5.40°21'W

144+6<sup>2</sup> E.C.

A  
144+09<sup>2</sup> R 8°56'

E = 2.2  
T = 55.9  
R = 716.2  
D = 80  
L = 111.7

143+53<sup>2</sup> B.C.

5.31°33'W  
140+15<sup>2</sup> E.C.

A  
140+2<sup>2</sup>



E.C. 173+44.5° Ahead  $\Delta$   
 E.C. 168+53° Back  $\Delta$

183.4  
 145+38.0  
 1+83.4  
 144+02.6

 $\Delta$ 

$\left\{ \begin{array}{l} 144+58.5 \text{ "A" POT} \\ 144+65.3 \text{ "B" E.C.} \end{array} \right\} = 15.2 \Delta$

 $15.2 \Delta$ 

$\left\{ \begin{array}{l} 144+02.6 \text{ "A" POT} \\ 144+09 \text{ "B" R.I.} \end{array} \right\} =$

 $\Delta$ 

24'

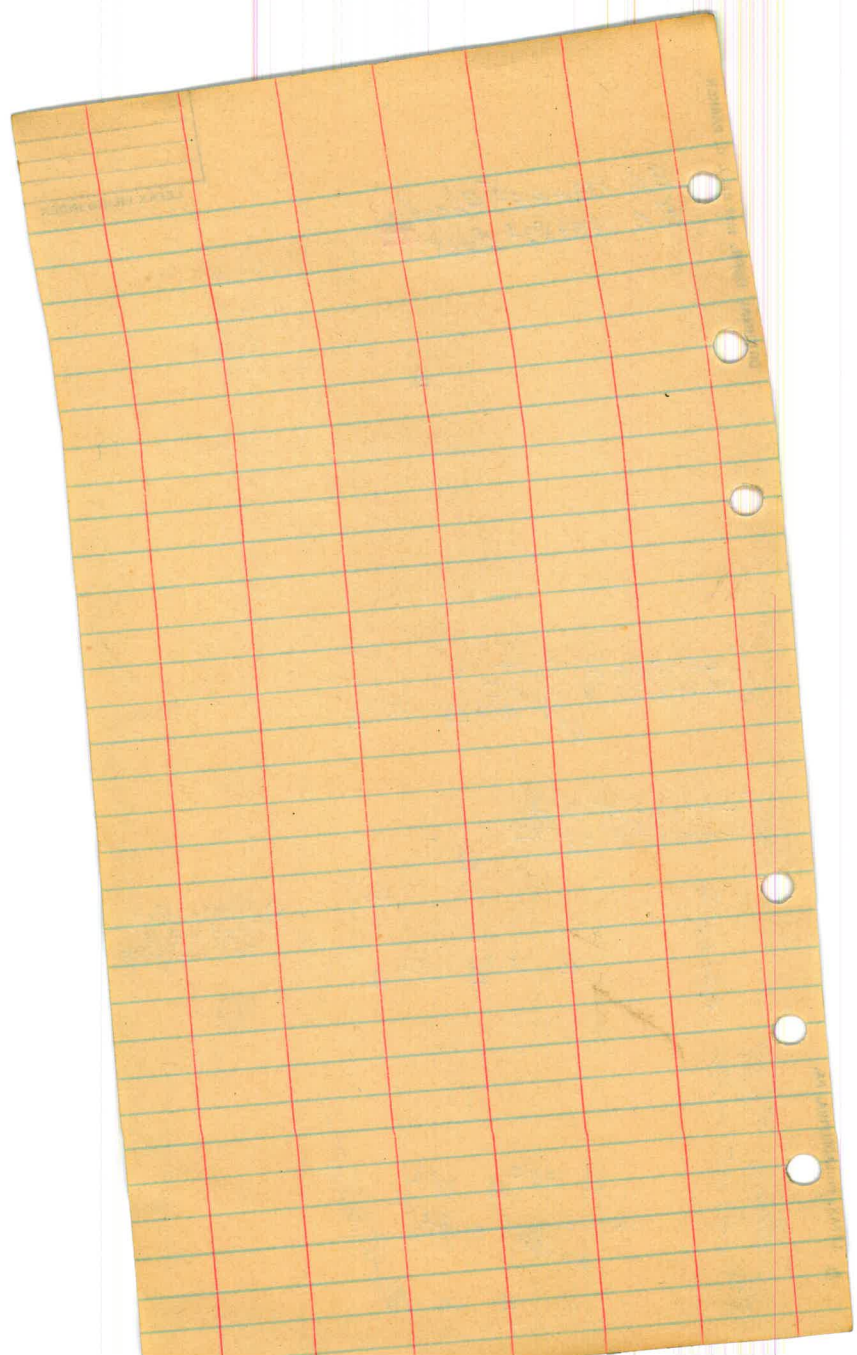
Large Oak  
 Tree 24' R.  
 Sta. 143+85

 $\Delta 15.2 \Delta 15.2 \Delta$ 

Grain Field.  
 Sta. 140+58 - Sta. 144+65.3

$\Delta 35.2 \Delta 25.2 \Delta$   
 x x x x x x x  
 140+58 x x 24' x  
 $\Delta 10'$

Board Fence.



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E.C. 173+44<sup>2</sup> Ahead  $\Delta$   
E.C. 168+53<sup>2</sup> Back  $\Delta$

183.4  
145786.0  
1+83.4  
144702.6

$\Delta$

$\left\{ \begin{array}{l} 144+58.5 \text{ "A" P.O.T.} \\ 144+65.3 \text{ "B" E.C.} \end{array} \right\} = 15^\circ \Delta$   
R.P.

$\left\{ \begin{array}{l} 144+07.6 \text{ "A" P.O.T.} \\ 144+09.5 \text{ "B" P.I.} \end{array} \right\} = \Delta$

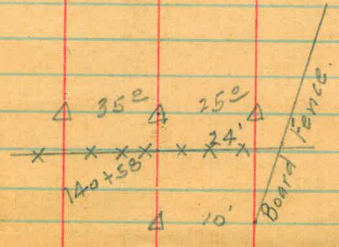
24'

Large Oak  
Tree 24' R  
Sta. 143+85

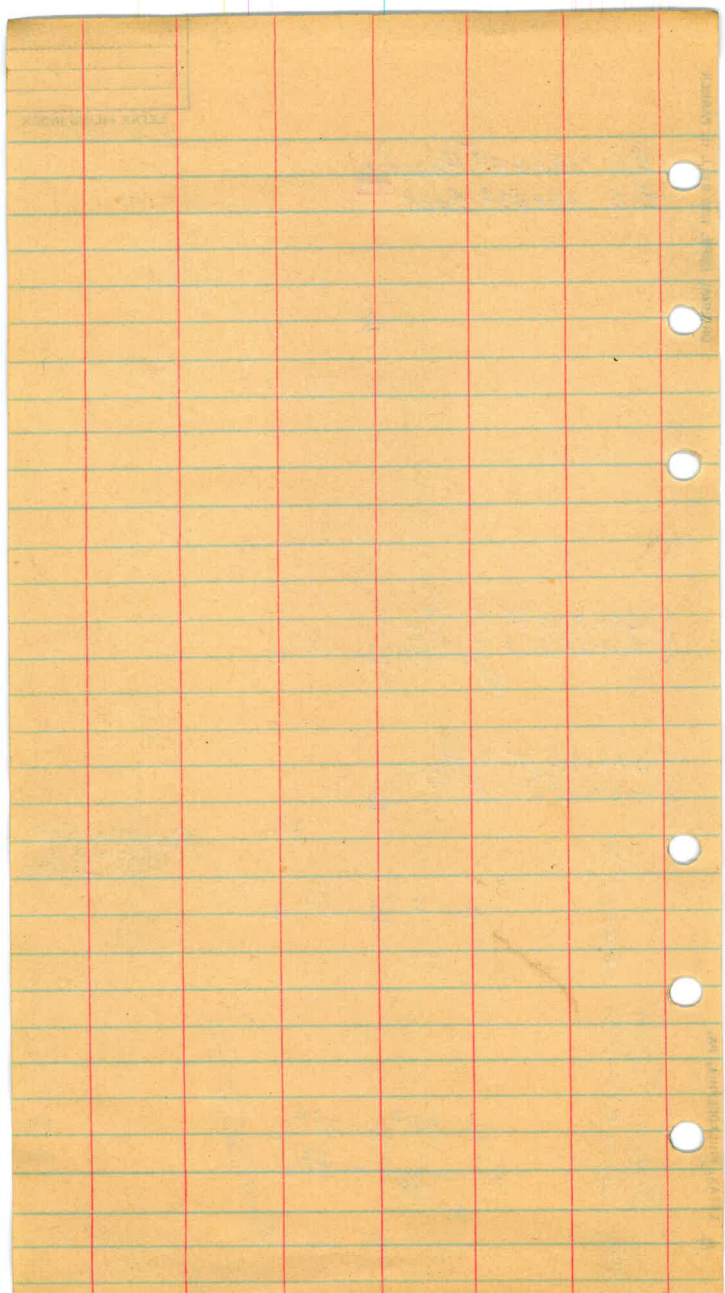
Sta. 140+58 - Sta. 144+65<sup>3</sup>  
Grain Field.

$\Delta$  15.2<sup>2</sup>  $\Delta$  15.2<sup>2</sup>  $\Delta$

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$$\text{Log. Cos. } 12^{\circ} 26' = 9.989693$$

$$\text{Log. } 59.27 = 1.772817$$

$$\text{Log. } 57.88 = 1.762510$$

$$\text{Log. Sin. } 12^{\circ} 26' = 9.333051$$

$$\text{Log. } 59.27 = 1.772817$$

$$\text{Log. } 12.76 = 1.105868$$

$$\text{Log. } 57.88 = 1.762510$$

$$\text{Log. } 4063.5 = 3.608900$$

$$\text{Log. Tan. } 0^{\circ} 49' = 8.153610$$

$$\text{Log. } 57.88 = 1.762510$$

$$\text{Log. } 2084.7 = 3.319044$$

$$\text{Log. Tan. } 1^{\circ} 35.4' = 8.443466$$

$$\frac{57.88}{\sin 49'} = \frac{4063.5}{\cos A}$$

$$\begin{array}{r} 633 \quad 603 \\ 526 \quad 526 \\ \hline 107 \quad 770 \end{array}$$

$$1.762510$$

$$8.153907$$

$$\frac{3.608603}{\phantom{000000}} = 4060.7$$

$$\begin{array}{r} 3.608900 \\ 9.999956 \\ \hline 3.608944 = 4064. \end{array}$$

Pop. Co. 2.12.25 = 7.772817

Pop. 27.27 = 1.772817

Pop. 27.88 = 1.772810

Pop. 27.15.25 = 7.553021

Pop. 27.27 = 1.772817

Pop. 15.76 = 1.102868

Pop. 27.88 = 1.772810

Pop. 40.3.2 = 3.608100

Pop. Tan. 0.74 = 8.123610

Pop. 27.88 = 1.772810

Pop. 20.84.7 = 3.314044

Pop. Tan. 1.324 = 8.443466



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"B" Line				Party Leach T Reynolds Rod Todd Feb. 25 "
Sta.	+	π	-	Elev.
B.M. # 16				503.054
	4.830	507.884		
133+03.6				
133+03.6	Post "A"			
133+03.6	BC "B"		5.1	502.8
133+27.3			5.1	502.8
+50.8			5.2	502.7
134+00			5.3	502.6
+76.4			5.3	502.6
135+00.4			5.4	502.5
136+00			5.4	502.5
137+00			6.5	501.9
138+00			6.8	501.1
			6.413	501.971
	4.773	506.299		
B.M. # 17			4.036	502.208
				502.184
138+84.5			2.4	503.8
139+00			3.3	502.9
T.P.			5.498	500.796
	5.421	506.167		
+67.3			5.6	500.6

"B" Line

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$$\frac{49}{100} 503.0$$

$$\frac{47}{100} 503.2$$

$$\frac{49}{100} 503.0$$

$$\frac{53}{100} 502.6$$

$$\frac{53}{100} 502.6$$

$$\frac{53}{100} 502.7$$

$$\frac{55}{100} 502.4$$

$$\frac{63}{100} 501.7$$

$$\frac{66}{100} 501.3$$

$$\frac{65}{100}$$

$$\frac{52}{100} 500.5$$

$$\frac{48}{100} 501.4$$

$$\frac{55}{100} 500.7$$

30 rd.

50 rd.

20 rd.

18 rd.

Left edge rd.

Rt. edge rd.

$$\frac{42}{20} 503.2$$

$$\frac{49}{100} 503.0$$

$$\frac{50}{100} 502.9$$

$$\frac{51}{100} 502.8$$

$$\frac{53}{100} 502.7$$

$$\frac{52}{100} 502.9$$

$$\frac{48}{100} 503.1$$

$$\frac{51}{100} 502.8$$

$$\frac{59}{100} 502.0$$

$$\frac{62}{100} 501.2$$

$$\frac{49}{100} 502.2$$

$$\frac{42}{100} 502.0$$

$$\frac{52}{100} 500.5$$

PCC



Sta	+	π	-	"B" Line Elev.
		506.67		
139+92.3			6.2	500.0
140+17.3			5.7	500.5
+42.3			5.0	501.2
+67.3			5.1	501.1
+75.6			5.1	501.1
141+00			5.2	501.0
142+00			5.1	501.1
143+00			5.4	500.8
<del>144+00</del>			<del>6.0</del>	
T.P			5.510	500.657
	4.415	505.072		
B.M.			6.475	498.597
143+53.6			5.0	500.1
143+78.3			5.2	499.9
144+03.3			5.1	500.0
144+21.6			7.1	498.0

"B" line

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$$\frac{58}{100} 500A$$

$$\frac{54}{100} 500B$$

$$\frac{54}{100} 501.1$$

$$\frac{54}{100} 501.1$$

$$\frac{54}{100} 501.1$$

$$\frac{54}{100} 501.1$$

$$\frac{50}{100} 501.2$$

$$\frac{55}{10}$$

$$\frac{42}{100} 500.2$$

$$\frac{50}{100} 500.1$$

$$\frac{49}{100} 500.2$$

$$\frac{47}{100} 500.4$$

$$\frac{64}{100} 500.1$$

$$\frac{59}{100} 500.8$$

$$\frac{54}{100} 501.1$$

$$\frac{50}{100} 501.2$$

$$\frac{48}{100} 501.4$$

$$\frac{52}{10} 501.0$$

$$\frac{53}{10} 500.9$$

$$\frac{54}{10} 500.8$$

$$\frac{50}{100} 500.1$$

$$\frac{42}{100} 500.2$$

$$\frac{62}{100} 498.9$$

$$\frac{75}{100} 497.5$$

"B" Line

Sta +  $\pi$  - Elev.

505.072

144+28.5 7.4 497.7

+53.5 8.0 497.1

+65.3 7.9 497.2

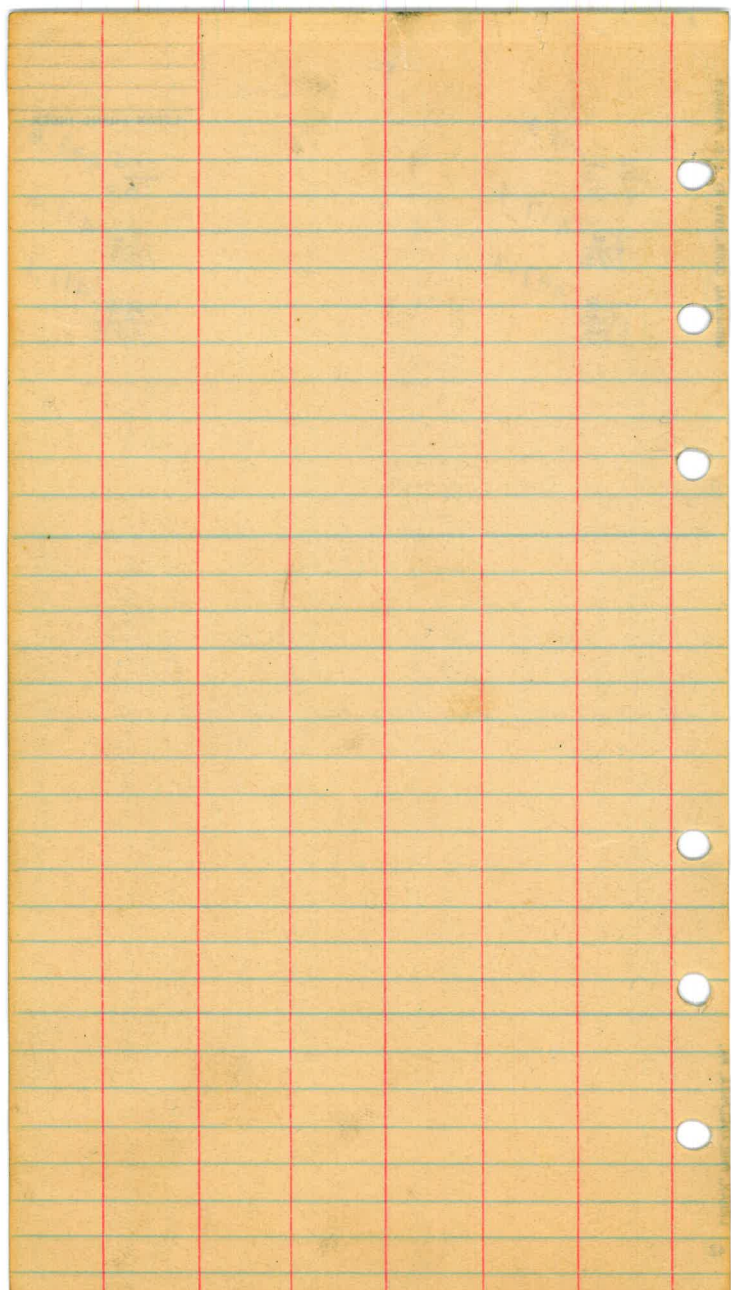


2 B Line

$$\begin{array}{r} 52499.4 \\ 100 \\ \hline 22497.4 \\ 100 \\ \hline 78497.3 \\ 100 \end{array}$$

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$$\begin{array}{r} 25497.6 \\ 100 \\ \hline 78497.2 \\ 100 \\ \hline 80497.1 \\ 100 \end{array}$$



Topography from  
Sta. 9728.8 to Sta.  
216+00

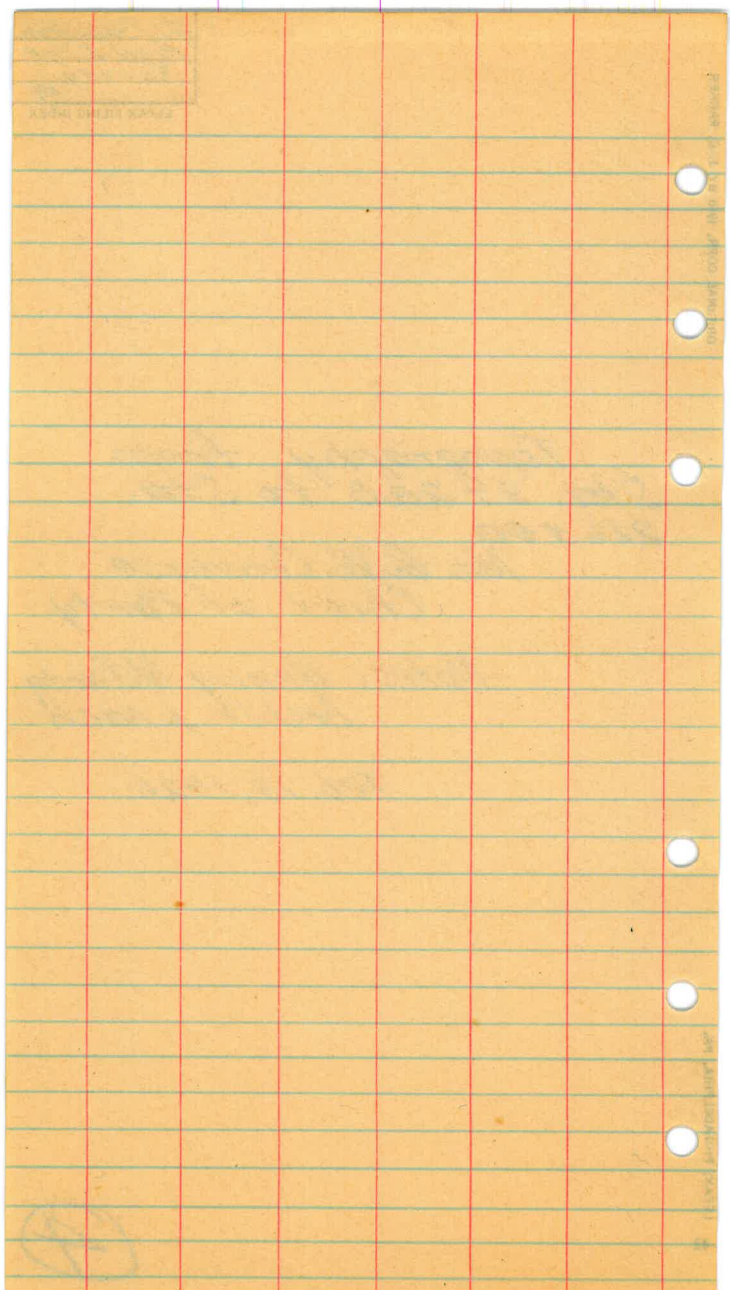
Mr. G. W. Converse  
Chief of Party

Notes: Henry McCarty  
Archie Leach

Feb. 18, 1926

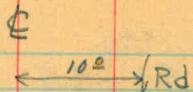
(4)



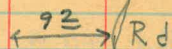


Sta.  $\text{C}$   
 9+28.8 18" tree  $\odot$  25  $\rightarrow$  ✓  
 9+40.4 12" tree  $\odot$  10  $\rightarrow$  \* 85  $\rightarrow$  Edge of road ✓  
 9+58.8  $\leftarrow$  90  $\rightarrow$  Edge of Road  
 9+83.8  $\leftarrow$  75  $\rightarrow$  Rd ✓  
 10+08.5 8" tree  $\odot$  9  $\rightarrow$  50  $\rightarrow$  Rd  
 10+44.8 30" tree  $\odot$  32  $\rightarrow$   
 10+58.8  $\leftarrow$  50  $\rightarrow$  Rd  
 10+83.8  $\leftarrow$  50  $\rightarrow$  Rd  
 10+95.3 6" tree  $\odot$  14  $\rightarrow$   
 11+08.8  $\leftarrow$  70  $\rightarrow$  Rd  
 11+20.8 6" tree  $\odot$  45  $\rightarrow$   
 11+58.8  $\leftarrow$  90  $\rightarrow$  Rd  
 11+68.0  $\leftarrow$  100  $\rightarrow$  Rd  
 11+72.2  $\leftarrow$  95  $\rightarrow$   
 11+97.2  $\leftarrow$  80  $\rightarrow$  Rd

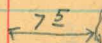
Sta.  
12+22.2



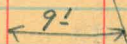
12+47.2



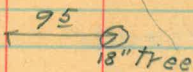
12+72.2



12+97.2

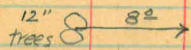


13+81.4

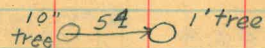


142.4  
4.7  
2.7

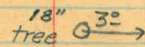
14+29.4



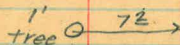
14+64.4



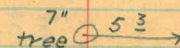
14+93.7



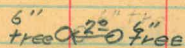
15+10.2



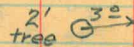
15+24.2



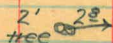
15+74.4



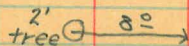
15+90.3



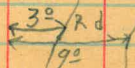
16+06.9



16+16.5



17+00



18+00





Sta  
18+69E  
Rd 62 / Rd

19+00

Road 12°  
8°

19+27.5

Rd 52 10° / Rd

19 42.2

Rd  
65 / Rd

20+773

10° / Rd

21+031

6° / Rd

21+903

45° / Rd

22+964

45° / Rd

22+164

45° / Rd

22+264

45° / Rd

22+364

45° / Rd

22+464

5° / Rd

22+564

6° / Rd

22+664

65° / Rd

22+721

72° / Rd

23+00

10° / Rd

Sta	⊕
25+01.6	← 8° → Rd
25+17.3	← 7° → Rd
25+42.3	← 5° → Rd
25+67.3	← 7° → Rd
28+05	2' tree ⊕ 5° →
28+72.3	← 9° → Rd
28+97.3	← 5° → Rd
29+10.9	1' tree ⊕ 4° → ⊕ 7° →
29+25.3	← 4° → Rd
29+41.3	2' tree ⊕ 3° →
29+47.3	← 4° → Rd
29+72.3	← 3° → Rd
29+97.3	← 4° → Rd
30+22.3	← 4° → Rd
30+47.3	← 5° → Rd
30+61.7	← 4° → Rd

Stg  
30 + 61.2

← 48 → Rd

30 + 72.7

1.5 tree  $\odot$  7.3 5.5  
2' stump

30 + 85.8

← 42 → Rd

31 + 10.8

← 42 → Rd

31 + 35.8

← 52 → Rd

31 + 60.8

← 70 → Rd

31 + 73.3

2.5 tree  $\odot$ 

31 + 85.8

← 72 → Rd

32 + 10.8

← 76 → Rd

32 + 22.8 EC

← 80 → Rd.

32 + 55

← 48  $\odot$  2' tree

33 + 14

3' tree  $\ominus$  95 →

33 + 18

 $\odot$  1' tree

33 + 65.1

2' tree  $\ominus$  30 →

34 + 11.5

← 52  $\odot$  1.5 stump

34 + 48.3

← 62  $\square$  4x4 sign post



Sta  
34+80.9

€  
5' stump  
and 8" tree

35+60.4

← 7L → Rd

35+85.4

← 7Z → Rd

36+10.4

← 70 → Rd

36+35.4

← 95 → Rd

37+188

8" tree ⊖ 80 →

37+37.2

3' tree ⊖ 103 → 2" tree

37+91.1

← 100 → Rd

38+00

← 90 → Rd

38+22.1

← 100 → Rd

38+45

15" tree ⊖ 7 →  
18" tree ⊖ 5Z →

38+59

← 43 ⊖ 18" stump

38+74

← 25 ⊖ 2' stump

40+625

← 65 → Rd

41+41.4

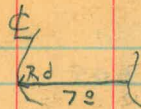
← 75 ⊖ 30 ⊖ 18" tree ⊖ 2' tree

45+84.5

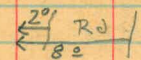
← 85 ⊖ 6" tree

Sta	
46+05	← 7 <sup>0</sup> ○ 2' tree
46+17	← 2 <sup>0</sup> ○ 6" tree
46+28	← 5 <sup>0</sup> ○ 1' tree
47+00	← 9 <sup>5</sup>   Rd
47+49	← 1 <sup>6</sup>   Rd   62
47+74	← 1 <sup>2</sup>   Rd   72
47+99	← 5 <sup>0</sup>   Rd
48+24	← 6 <sup>7</sup>   Rd
48+66.5	○ 18" tree
48+84.5	← 5 <sup>0</sup> ○ 6" tree
49+20	1' tree ○ 1 <sup>2</sup> →
49+29	2' tree ○
49+43.5	← 9 <sup>0</sup> ○ 6" tree
49+45.8	2' clump ⊗ 3 <sup>5</sup> →
49+74.1	← 10 <sup>0</sup>   Rd
50+00	← 0 <sup>5</sup>   Rd   6 <sup>0</sup>

Sta  
50+60

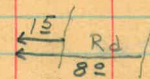


52+00

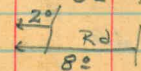


52+17.5 18" tree ⊙ 9° →

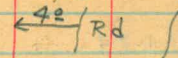
52+69.9



52+94.9



53+19.9



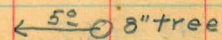
53+44.9



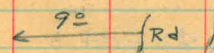
53+57

5° ⊙ 6" trees

53+59.5



53+69.9



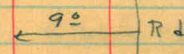
53+80 6" trees ⊙ 9° →

53+81 1' tree ⊙ 9 1/2° →

53+82.9



54+00



54+28.5 1' tree ⊙ 4° →



54+85 Tree 0 2' →

55+00 Tree 0 6 5' → ← 9 5' Rd. }

55+02 Stump 0 6 5' →

55+07.7 Tree 0 9' Tree 0 7' →

55+11 Tree 0 2 2' 2' 0 Tree

+16.5 Tree 0 4 8' →

+35.5 Tree 0 9' →

+80.4 4 Trees 0 0 6 5' →  
1' Deach 0 0

56+19.4 6' Rd }

+44.9 4' Rd }

+59.9 5' Rd }

+70.4 2 Trees 0 1' → 0 8' →  
1' → 0

+99.9 5' Rd }

57+19.9 6' Rd }

+39.7 6' Rd }

+81.2 2' Tree 0 10.4 5' Tree

58+05

9.5' 2' Tree

+11

18" Tree 0 2' 00 2' 1' Trees

59+00

10' Rd

+44.5

18" Tree 0

+75 Two fallen trees

(18" Tree) 7'

2' (Tree)

61+11.3

Four Trees

6" (D)

0.0 1.2

61+52

9' 10" Tree

62+00

10' Rd

63+00

6' Rd

64+00

10'

+61

8' 8" Tree

+79.5

7.5' 0" Tree

+85

1.3 10' Trees

+89

7.5 0" Trees

65+27.5

1' Tree 0 4 5 4

2.2 6" Tree

Clump Trees  
one 1' Tree  
Three 4" Tree

65+38 8" Tree 6'  
 +40 8" Tree 7'  
 +50 18" Tree  
 +69 8" Tree 15'  
 +74.3 8' (rd.)  
 +88 8" Tree 26'  
 +89 1' Tree 52'  
 66+05 18" Tree 10' 2' Tree edge line  
 66+06 7" Tree 9'  
 +24.3 5' (rd.)  
 +32.6 1' Tree 0'1'  
 +49.3 5.5 (rd.)  
 +63.3 1' Tree 5'  
 +74.3 8" Tree 10' 8' (rd.)  
 +94.3 18" Tree edge tree  
 +99.3 10' (rd.)



67+42      clump of  
 6' <sup>000</sup> shomache  
 +53.7      1' 8" tree  
 +60.2      1' 0" tree  
 +75      1' tree 6' 2' 0"  
 +78      6' 18" tree  
 +79      2' 2' tree  
 68+00      8' (Rd.)  
 69+00      4' (Rd.)  
 70+00      10' (Rd.)  
 71+00      9' (Rd.)  
 72+00      8' (Rd.)  
 71+00      (5' 1' / Rd.)  
 +18<sup>2</sup>      (6' 1' / Rd.)  
 +43.2      (5' 2' / Rd.)  
 +68<sup>2</sup>      (1' 6' / Rd.)

71+93 =

8' } Rd.

74+00

3' } 10' } Rd.

+37

6x6 Post 4' } 8' } Rd.

75+00

6' } Rd.

+87.5

3' Tree O

76+07 =

6' } Rd.

+27.1

4' } Rd.

76+29

3' Tree O

77+00

3' 2' } Rd. Fee

77+78 =

6' } 75' } Rd.

78+03

4' 2' } Rd.

+28

6' } Rd.

+53

2' 8' } Rd.

+78

4' } 10' } Rd.

79+03

3' } 10' } Rd.

±

Sta

79+28

4 | 10'  
Rd.

+932

4.5 | 10'  
Rd.

+725

7' | Rd.

80+20

Trees 1' 0.85

+52

18" Tree 10'

+775

Trees (1" D) 0.75

81+225

14" Tree 7'

+33

12" Tree 2.5

+448

000 9 Trees  
000 9 Howing out  
000 of 3' base

82+47

2' Tree 0.35

83+00

0.5 | 5'  
Rd.

+16

3' Tree 8'

+575

1' | 7'  
Rd.

+775

3' | 10'  
Rd.

+975

5' | Rd.

84+00

6' | Rd.



Sta.  
84+50

Large Boulder 2' 5' 2' Tree

84+81

2' Tree 4'

85+15

Large Boulder  
on line

85+28

7' 15" Dead tree

86+97

7' 6' 0' Two Trees

87+265

2' Tree 5'

87+94

3' 2' stump

88+54

5' 18" Tree

88+63

5' 2' stump

89+32

12" Tree 3'

89+79

18" Tree 95

91+83

4' 6" Tree

+89

5' 8" stump

+94

10" Tree 95

92+49

18" Tree 2

93+375

10' rd

39  
47  
86

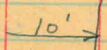
4

Sta.

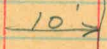
93+48 1/2



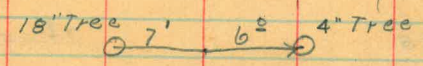
95+48 1/2



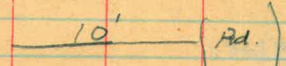
+ 73 1/2



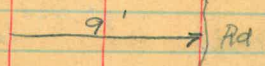
96+35



+ 46 1/2



+ 68



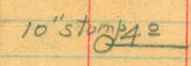
+ 86



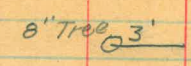
97+00



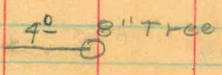
+ 07



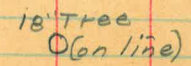
+ 56



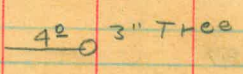
+ 77



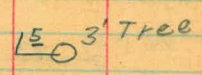
98+38



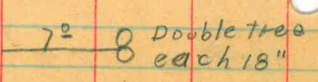
+ 48



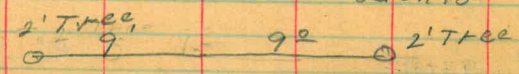
+ 61



+ 78



+ 95



Sta  
99+40

6° 0 2' Tree

99+69

7° 0 5' Tree

+74

3° 0 6" Tree

+78

5° 0 5" Tree

+90

3° 0 8" Tree

+94

8° 0 12" Tree

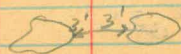
100+00 12" stump 2 trees growing out

+15 2' stump 4 trees growing out

+36

3° 0 12" Tree

100+75

 Boulders 4' high

101+37

18" stump 2 trees growing out

102+74

4° 0 2' stump 3 trees growing out

103+07

1° 0 10" Tree

103+87


10° 0 3° stump

104+70

4° 0 2' stump

42

105+15

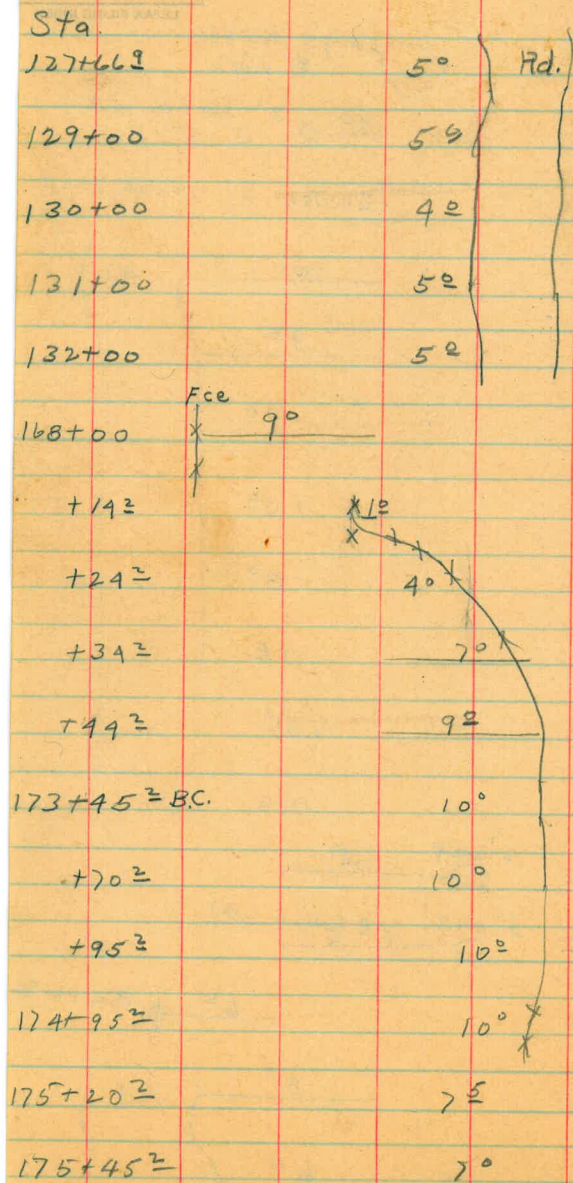
 large uprooted stump



Sta.	Notes
105+82	7° 2' stump (sprouted)
106+ab	5° 6" stump (sprouted)
+56	2' stump 2° 9° 2' stump (sprouted)
+67	7° 2' stump (sprouted)
+69	2' sprouted stump 6°
+96	8° 3' sprouted stump
107+09	2' stump 5°
+11	12" tree 10°
+21	8" tree 7° 2° 2' stump
+37	6" tree 3°
+58	2° 12" stump
+97	7° 8" tree
108+06Z	9° Rd.
+31Z	6° Rd.
+56	6°
110+4	3° 6" tree

Sta.	Notes
112+00	Large Boulder 8' high
113+70	4° 3' base with 3 18" limbs
115+12	center of cross road.
116+00	10° Rd.
116+129	9°
+32	9°
117+00	10°
118+00	8°
119+00	9°
120+00	10°
121+00	10°
+733	6' oak 10°
123+94 <sup>2</sup>	5' oak 9° (edge of)
126+27	6° Power Pole
127+16	8° Rd.
+41	6°

2





Fcc

175+59<sup>1</sup>

7<sup>0</sup>

176+00

7<sup>0</sup>

177+00

6<sup>0</sup>

178+00

6<sup>0</sup>

+62<sup>1</sup>

5<sup>0</sup>

87<sup>2</sup>

5<sup>0</sup>

179+02<sup>1</sup>

6<sup>0</sup>

+37<sup>2</sup>

6<sup>0</sup>

+62<sup>1</sup>

7<sup>0</sup>

+87<sup>2</sup>

7<sup>0</sup>

180+12<sup>2</sup>

6<sup>0</sup>

737<sup>2</sup>

6<sup>0</sup>

+62<sup>1</sup>

3<sup>0</sup>

+87<sup>2</sup>

2<sup>0</sup>

181+03<sup>2</sup>

2<sup>0</sup>

182+00

6<sup>0</sup>

Σ

Sta			Fce
183+00 / Rd.	10'	10'	X
184+00	9°	9°	
185+00	9°	8°	
186+00	8°	7°	
187+00	10°	5°	
188+00	10°	2°	
189+00	10	3°	
190+00	8°	6°	
191+00	7°	6°	
192+00	6°	6°	
193+00	5°	7°	
194+00	3°	8°	
195+00	3°	8°	
196+00	3°	6°	
197+00	3°	8°	

Sta.		
198+00	30	40
Ad		
199+00	20	40
204+00	30	
+37	50	
+62	70	
205+624	90	
+874	90	
206+098	80	
207+00	80	
208+00	80	
209+00	80	
210+00	90	
211+00	90	
212+00	80	
213+00	90	
214+00	50	



2

2014-01-21

215700 6°

216 6°

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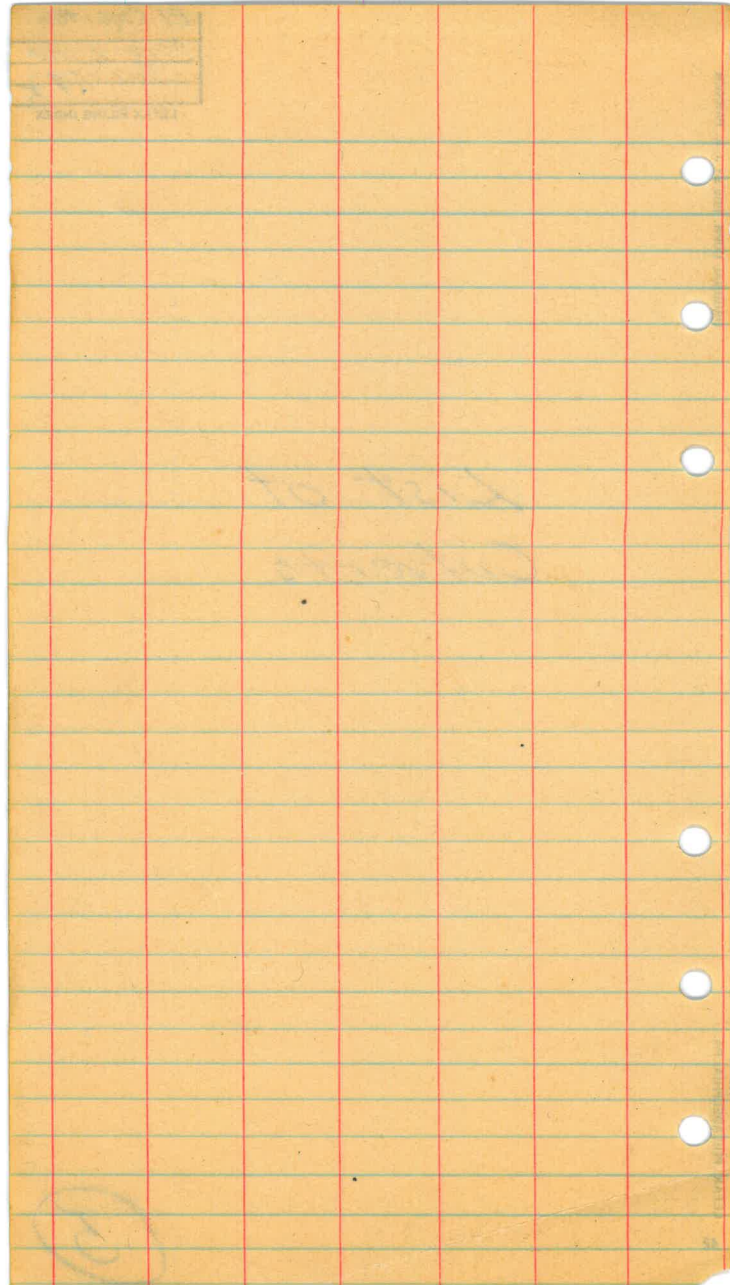
LEFAX, PHILADELPHIA, PA.

42

LEFAX FILING INDEX  
Pipe Line  
Survey 5

List of  
Culverts

5





214+37 (approx) 12" Conc 14' Left

BM # 13 480.700

4.796 485.510

FlowLine 4.3 481.3

Sewer from Cow Barn south of Rd

St. 169+13 - 12" Conc 8.5' L

BM # 16 504.635

1.263 505.898

FlowLine 11.9 494.0

165+26 - 10" Iron pipe ~~enters~~  
under line draining Barn on south  
North end is 8' N. of Q

Same HI above

FlowLine 11.1 494.8

182+40 (See Transit book)

is a 12" conc pipe xing line on  
surface of the ground. Think  
not in use now. Probably  
is from old barn wrecked  
on south side of Rd.

LEFAX FILING INDEX


469+05-2x6 Conc. cul 5.2' L

B.M. #33 383.857

4.050 387.907

Flow Line 8.0 379.9

452+13 -12" Conc 3.6 L

B.M. #31 393.949

3.230 397.179

Flow Line ~~8.5~~ 8.5 388.7

446+22 12" C.M.P. 9.7' L

397.179

Flow Line 5.2 392.0

439+15-3.3' X 1.5' Conc Br 8' Left

Flow Line 395.1

See transit notes

430+07 12" cul L 5.7

B.M. #30 400.227

5.820 406.047

Flow Line 5.8 400.6

355+ 3' X 2d Br

Set levels Sta 355+12

" + 20'

" + 50'

also set transit notes Sta 355-356



331+78 12" C.M.P. 2' R

B.M. near 56336 (on any pole) 441.278

7.470 448.748

South end 11.7 437.0

North end 12.8 435.9

Note actual Rods were 1017 & 1017 but  
were taken on top of pipe

285-76 ~ 16" conc out South end is  
directly under line. It extends north  
under Rd

B.M. near 296+70 446.620

11.580 458.200

Flow Line intake 5.0 453.2

Outfall 6.2 452.0

~~284+85~~  
384+85 on Line (apparently) an old stone

Drain has collapsed.

Same HI as above

Flow line approx 5.5 452.7

277+28 12" conc pipe 7.5 R

B.M. #22 455.815

2.065 457.880

Flow Line intake T. 7.6 450.2

" " Outfall 8.4 449.4

249+96 18" conc 1' left.

B.M. near 253+95 466.397

7.360 468.707

Out fall 6.6 462.1



Sta 559+39 12" CMP 5' L  
B.M. #41 369.052  
1.430 370.462  
Flow Line 8.5 362.0

559+55 12" CONC Pipe 5.7 L  
Same HJ as above 11.5 Lopot opening  
Flow Line 12.5 358.0

536+02 - 5' Left 36" CMP 362.588 551.91  
B.M. #40 HCO, 537 369.032  
4.100 373.150  
Flow Line 366.989 9.2 357.8  
364.2

514 +67 - 12" Conc 2' L  
B.M. #38 365.570  
4.690 370.200  
Flow Line 6.4 363.8

493+14 - 2.5' X 6' Conc ONLY 3' L to road wing  
6' L to Rd. wall  
Co B.M. #17 379.508  
3.140 382.648  
Flow Line 8.5 374.1 ✓

486+38 12" Conc 1.8' Left  
Co B.M. #18 381.717  
2.860 384.577  
Flow Line 9.3 376.3 ✓

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760+48 - 18" CIP 5.7' L 311.7

759+17 - 24" Conc Pipe 9.5' L 310.6

B.M. Rt 761+ 317.569

1.027 318.596

5.9 311.7

8.0 310.6

740+06 8" C.I.P. 3.8' L

B.M. # 726+50 310.545

2.001 312.546

Flow Line cdy 7.5 305.0

733+24 8" Conc 4' L

B.M. # 440 Near 736+50 310.545

6.440 316.985

Flow Line 7.3 309.7

730+55 18" CIP 8.6' L

Flow line 316.985 (Same HI as above)

5.9 311.6

721+9A - 24" C.M.P. 15.0' L

T.P. Near sta 723 314.485

4.580 319.065

Flow Line 8.0 311.1

701+77 6"x12" wood <sup>9' left</sup> ~~7'~~

B.M. Near 705 325.363

4.070 329.433

Flow Line 5.6 323.8



650+32 12" C.M.P. 17' LxH

B.M. near st. 650+00 335.677

3.550 338.227

Flow Line 7.0 331.2

631+21 12" C.M.P. 5' L

B.M. near st. 635 339.393

3A30 342.823

Flow Line 6.5 336.3

617+91 -12" C.M.P. 4.3' L

B.M. near st. 618 = 343.593

3.700 347.293

Flow Line 5.8 341.5

596+99 - 8" C.M.P. 1.5' L

B.M. near 596 364.525

3.250 367.755

Flow Line 6.9 360.9

587+33 (2 -12" C.M.P.) 5.3' L

TP near 583 365.120

4.040 369.160

Flow Line 8.3 360.9

571+48 12" C.M.P. extend under  $\phi$  T.S.R

B.M. #12 365.762

4.970 373.732

10.7 363.0



766+21 - 12" CMP 8' L

B.M. near sta 720+28 335.057

1.010 336.67

(2 Rods held together) 16.1  
18.1

320.0

~~210.0~~

774+35 - 12" CMP 14' L

B.M. near sta 770+28 335.057

6.780 341.837

Flow Line 10.8 331.0

794+38 12" CMP 17' L

B.M. near 800+50 333.181

4.430 337.611 ←

TP

0.835 336.774

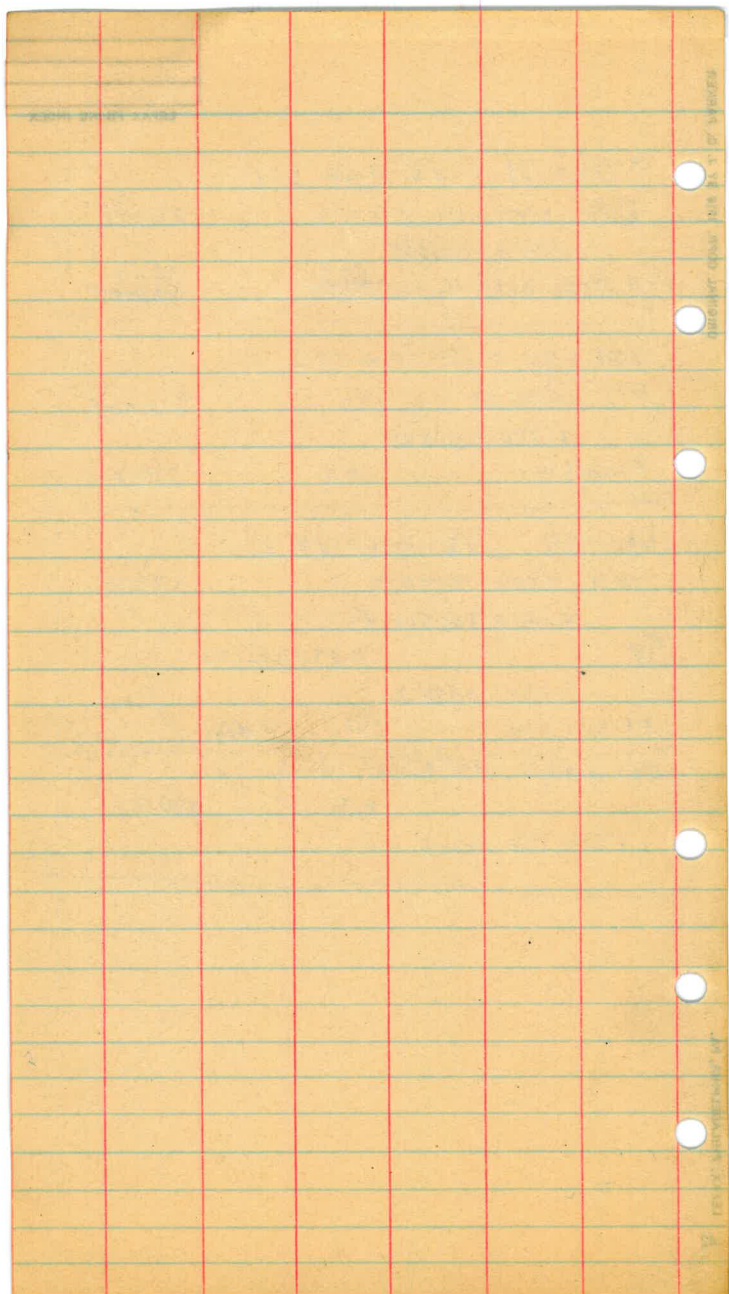
8.390 345.166

Flow Line 9.7 340.5

800+400 12" Comp 13' L

2.8 328.8

From HI above

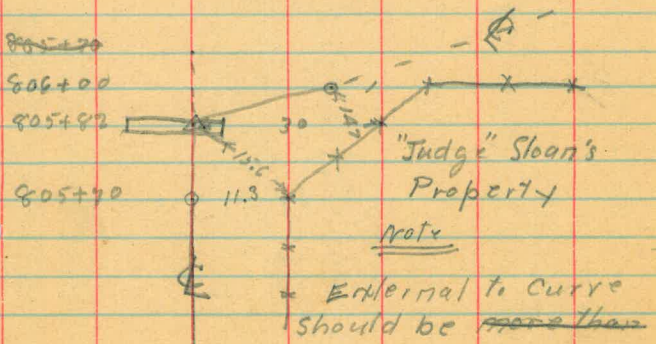


Dec 10

BM NEAR ST. 800 333.181  
 5.965 339.146  
 10.070 329.096  
 2.640 331.736

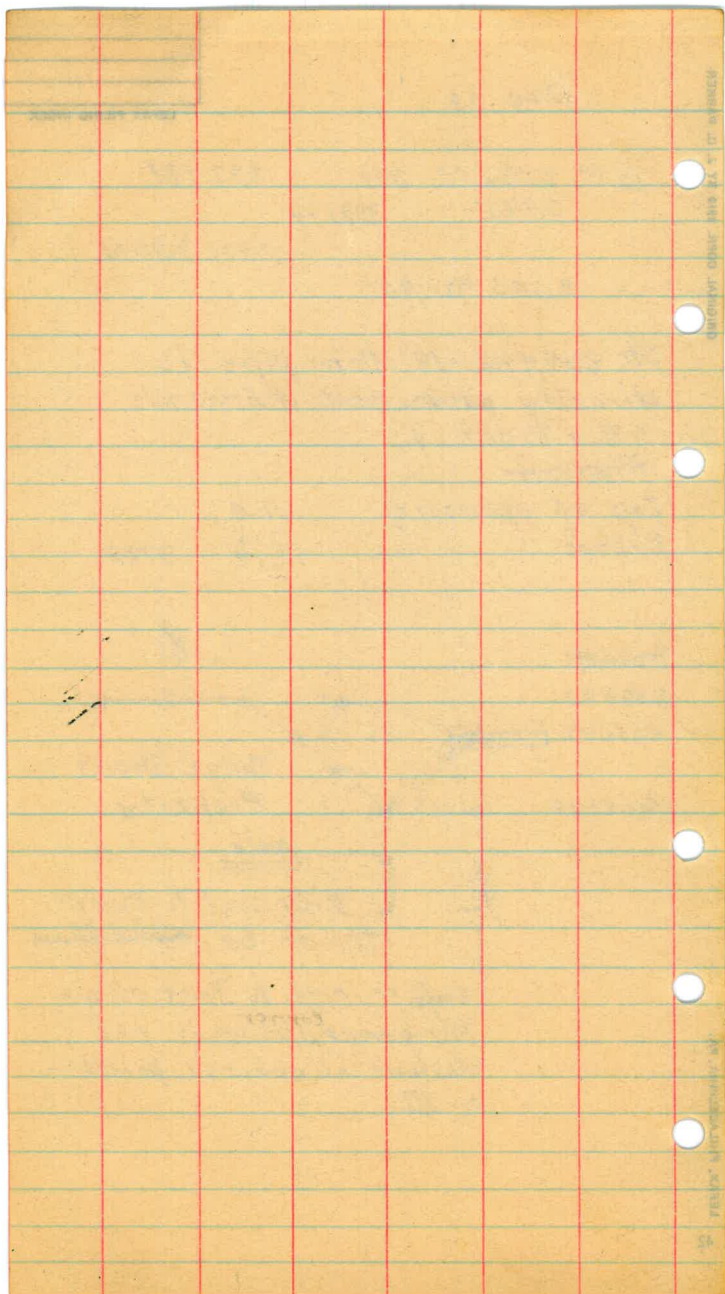
Stc 805+82 - 18" Conc pipe is  
 directly under road. & Extends  
 to the Right 6'  
 Flow Lite

Top of opening 11.9  
 Bottom 1.5  
 12.9 318.8



sufficient to Just clear  
 the fence <sup>corner</sup> which is 15.6  
 distant at nearest point  
 to P.I.






LEFAX FILING INDEX

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817+22                      12" Cond cul - 5' + P  
 (Inlet end covered up)

out fall

B.M. near 815+85

2.060 302.531

out fall

7.4

~~25.1~~

790  
 500.471

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~~486+38~~

~~70 760+78 1200~~

Dec 10

LEFAX FILING INDEX

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St 825+00 12" Conc 8' R

BM Near 824+00

7.95

309.431

1.450

310.881

Intake

10.6

300.3

out fall 2' Lower

822+20 - 12" Conc 26' R

HI above

310.881

Top of opening

12.2

Bottom

1.0

intake

13.2

297.7

828+20 5" Conc pipe 27' R

BM Near 824+00

309.431

5.500

314.931

intake

10.1

304.8

out fall

10.5

304.4

830+20 apparently has a pipe  
about 5' R. But we were unable  
to uncover it.

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832+82 - 12" Conc pipe - 51' R

T.P. nail in Post near 833

323.032

0.138 323.170

T.P.

8.470

314.700

5.635 320.335

intake

11.6

308.7

out fall

12.7

302.6

42



314.505

B.M. N.C. 836 ±

~~328.431~~

0.690 330.121

T.P. 8.605 321.516

1.038 322.554

841+43

16" C.M.P. - 14' - Right

Inlet (on top)

11.9

M.V.

out Fall

~~1.3~~

13.2

309.4 Flow Line

T.P.

10.555 311.999

2.345 314.344

M.V.

out Fall

6.2

~~308.1~~ out Fall

845+90 - 16" C.M.P. 26' ± To Right

T.P. ± B.M. 846+10

300.609

~~310.575~~

0.00 310.575

T.P. 11.023 299.552

1.393 300.945

T.P. 10.175 290.770

2.065 292.835

T.P. (Peg in Roadside) 7.875 284.960

0.160 285.120

Inlet 4.3 280.8

out Fall 5.5 ~~279.6~~

9.926

Dec 10

285.120

LEFAX FILING INDEX

T.P. Nail in Quill Club S. post

8550 276.570

848+75 12" Conc Pipe 30' R

4970 281.540

inlet = 6.9 276.45

out fall 7.8 273.7

855+55 about 4'x6' - 1.5' R

Flow Line 275.3

861+90 - 18" CMP 10.6' R

287.9

B.M. near 863+80

277.868

2780 270.649

inlet = ~~5.9~~ 7.7 262.0

out Fall 8.0 252.6

864+85 - 16" CMP 6' R

B.M. near 863+80

287.9

2.175 270.043

inlet = 6.7 263.3

out Fall 5.9 253.1

868+70 - 16" CMP 32' R

Same HI as above 270.043

inlet = 9.7 200.3

out Fall 11.3 208.7

Sta 873-17 12" Conc 25' Right

From old TP 873+10 elev 287.612  
0.991 288.603

TP 11.280 277.323  
0.442 277.765

TP at Road side 9.080 268.185  
4.180 272.865

In take 4.3 265.5

out Fall 8.9 264.7

---

891+25 - 12" Conc pipe 25' R  
 BM on Block near 889+52 = 251.493  
 1.085 262.578

Inlet 9.80 252.8  
 outfall 11.2 244.4

St 892+17 - 16" CMP 22' R

BM near 889+52 251.499  
 0.835 262.328

Inlet 5.5 246.8  
 outfall

896+05 16" CMP 36' R

BM near 897+75 265.742  
 0.842 266.584

Inlet 6.4 260.2  
 outfall 7.2 259.1

St 899+68 12" Conc Pipe 29' Right

Same HI as above 264.584

Inlet 7.7 258.7



Dec 11

B.M. on Boulder near 8722 - 258.361

1.780 270.091

TP 10.690 259.401

0.769 260.170

TP 11.030 249.140

2.650 251.790

Sta 879+25 12" Concpipe 30' R

Inlet 6.7 6.7 245.1

out fall 8.1 243.7

251.790

TP 4.240 247.550

7.780 255.330

Sta 889+02 16" C.M.P. 6' R

Inlet 5.4 249.9

out Fall 7.0 248.3

Sta 889+36 12" Concpipe 10' R

B.M. on Boulder near 889+52 - 251.493

4.062 265.555

Inlet 6.8 258.8

out Fall 7.4 258.2

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LEFAX FILING INDEX

S to 900+50 18" CIP 25' R

B.M. near 903+30 261.553

9.750 271.303

Inlet 9.3 262.0

out fall 10.2 261.1

900+90 12" conc pipe 21' T right

same HI as above

Inlet 8.8 8.1 269.2

B.M. near s/c 903+30 261.553

6.525 268.078 ✓

B.M. 0.600 262.478 ✓

S 903+19 18" CIP

~~Extends~~ upper end 5' L of line  
Extends toward R.

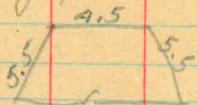
H.I. 268.078

Inlet 9.4 258.7

out Fall 12.5 5.6

911+26 Dog Sp Canon 153' Right

Section



BM Near 912+90 = 302.577

0.372 302.949

TP

11.405 = 291.544

1618 293.162

TP

11.740 281.422

2.110 283.532

Nail on S.E. X Post of Wing wall

5.772 277.760

2.725 280.485

Out Fall

11.9 268.6

in take

10.9 269.6

☒ Pub Rd on cul.

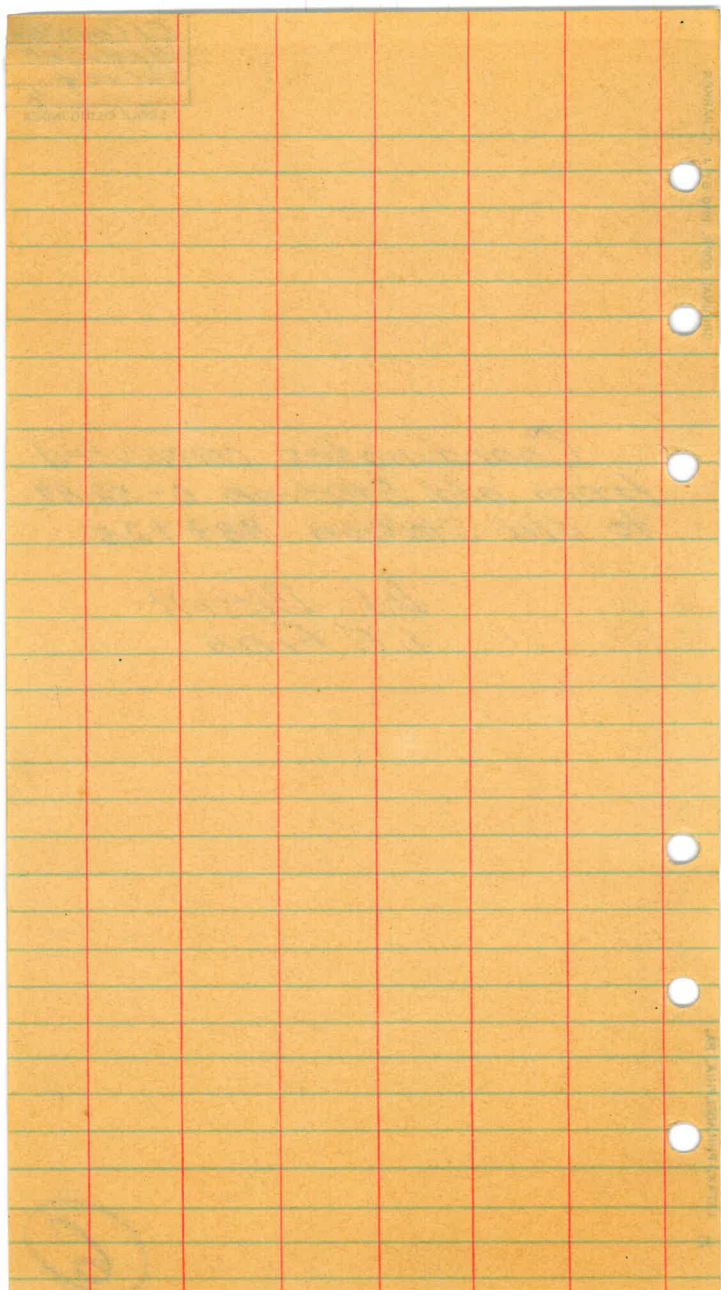
4.4 276.1




Coordinates computed  
from old Station 0-52.87  
to old Station 984+25.

D.L. Bissell  
I. E. Fish

6



73

LEFAX, PHILADELPHIA, PA.

ORIGINAL CORR. 1810 BY J. O. PARKER

Sta	Bear	Dist	Cos	Sin	N	S	E	W	Co-ordinates	Original	Final
0-52.87											
1474.1	N72°26'W	226.97	.302	.953	68.54			216.30	216.30	0	0
3+51.3	S85°44'W	177.2	.083	.996		14.71		176.69	176.69	0	0
6+00.3	S88°18'W	249.0	.030	.999		7.47		248.75	248.75	0	0
7+99.8	S84°23'W	199.5	.098	.998		19.55		198.50	198.50	0	0
9+99.5	S82°49'W	199.7	.125	.992		24.96		197.10	197.10	0	0
11+98.1	N88°08'W	198.6	.120	.993	23.83			197.21	197.21	0	0
13+73	N78°29'W	174.9	.251	.968	43.90			168.64	168.64	0	0
					43.72			169.30	169.30	0	0
					156.69			168.64	168.64	0	0
								170.58	170.58	0	0
								170.4.83	170.4.83	0	0

N = -  
 S = +  
 W = +  
 E = -

5/ Cor Typo Line  
 Co-ordinates  
 Original Final  
 TAM  
 LEFAX FILING INDEX





$N = -$   
 $S = +$   
 $E = +$   
 $W = +$

Sta	Bear	Dist	Cos	Sin	N	S	E	W	W
24+25	S88°35'W	120.0	.025	.999				22.05	2438.20
25+45	N81°45'W	255.0	.143	.990		3.00		199.88	2638.88
28+00	S83°49'W	200.0	.108	.994	84.46			252.45	-11.4 / 2890.53
30+00	N77°31'W	475.0	.216	.976		21.60		198.80	+10.19 / 3089.33
34+75	N71°46'W	139.0	.313	.950	102.60			463.60	-92.4 / 3552.93
37+14	N77°46'W	86.0	.212	.977	74.81			227.05	-167.22 / 3777.98
38+00	N65°45'W	95.0	.442	.897	18.23			84.02	-185.45 / 3864.00
38+95					41.99			85.22	-227.44 / 3949.22 ✓

El Cap. Top Line  
 Co-ordinates  
 Original Line  
 T.A.M. (2)  
 LEFAX FILING INDEX

Sta	Bear	Dist	Cor	Sin	N	S	E	W	S	W
38+95	N54°0'W	183.2	.882	.813	106.62 ✓ 106.44 ✓	148.94 ✓ 149.17 ✓			-227.14 ✓ -334.06 ✓	3949.22 ✓ 4098.16 ✓
40+78.2	N49°3'W	157.5	.662	.750	104.26 ✓ 104.10 ✓	118.12 ✓			-438.32 ✓	4226.28 ✓
44+35.7	N64°20'W	35.3	.482	.902	15.25 ✓ 15.21 ✓	31.84 ✓			-453.57 ✓	4248.12 ✓
42+71	N74°2'W	84.0	.268	.963	22.51 ✓ 22.34 ✓	80.89 ✓			-476.08 ✓	4329.01 ✓
43+55	N77°08'W	234.0	.223	.975	52.18 ✓ 51.71 ✓	893.45 ✓ 728.15 ✓			-528.26 ✓	4557.16 ✓
45+89	N82°08'W	301.0	.137	.991	41.24 ✓ 40.43 ✓	298.29 ✓			-569.50 ✓	4855.95 ✓
48+90	N79°38'W	155.0	.180	.984	27.90 ✓ 27.29 ✓	152.52 ✓			-597.40 ✓	5007.97 ✓
50+45						16.70 ✓				



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Sta	Bear	Dist	Cos	Sin	N	S	E	W	S	W
50+AK	N70°58'W	230.0	.326	.945	74.98 <del>74.75</del>			217.35 <del>215.75</del>	-591.40	5007.91
52+78	N63°58'W	327.0	.439	.899					-672.38	5225.32
56+02	N44°08'W	413.0	.718	.696	143.55			293.97	-815.93	5519.29
60+15	N54°28'W	535.0	.581	.814	296.53			287.45	-1112.46	5806.74
65+50	N75°40'W	133.0	.281	.960	310.84			43.549	-1423.34	6272.23
66+83	N78°20'W	97.0	.202	.979	37.37			127.68	-1460.67	6369.91
67+80	579°54'N	120.0	.175	.984	19.59			94.96	-1420.26	6764.87
69+00						21.00		118.08 119.19	-1459.26	6582.95

El. Cap/pipe line  
Coordinates  
Original Lines  
T.A.M. (3)  
LEFAX FILING INDEX



Sta	Bear	Dist	Cor	Sin	N	S	E	W	S	W	W	
69+00	S73°25'W	206.0	.285	.958					-1459.26	6582.96	✓	
71+06	N87°07'W	108.0	.047	.999		58.71		197.35	-1422.55	6782.30	✓	
72+14	N82°35'W	264.0	.129	.992	5.08			107.89	-1405.63	6888.19	✓	
74+78	N88°55'W	300.0	.019	1.000	<del>29.57</del> 34.06			261.89	262.47	-1439.19	7152.08	✓
77+78	N52°25'W	202.0	.581	.814	5.70			300.00	-1448.89	7462.08	✓	
79+80	N76°16'W	303.0	.237	.971	117.36			164.43	-1522.76	7614.51	✓	
82+83	N62°05'W	184.0	.437	.899	71.81			294.21	-1634.58	7928.12	✓	
84+67					80.41			165.42	165.41	-1714.97	18094.14	✓
								1401.71			✓	

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ORIGINAL COPY, 1910 BY J. O. PARKER

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Co-ordinates  
Original Line  
T.A.M. (4)  
LEFAX FILING INDEX

Sta	Bear	Dist	Cos	sin	N	S	E	W	S	W
84+67	N50°21'W	69.8	.638	.770	44.53				-1714.97	8074.14
85+56.8	N65°21'W	663.2	.417	.909	276.56				53.75	-1769.50
92+00	N46°45'W	200.0	.685	.728	137.00				602.85	-2036.06
94+00	N55°15'W	285.0	.570	.822	162.45				145.60	-2175.06
96+85	N53°37'W	67.0	.593	.805	39.73				2342.7	-2335.5
97+52	N68°12'W	183.0	.371	.928	67.89				53.94	-2270.24
99+35	N79°24'W	415.0	.184	.983	76.36				169.82	-2443.13
103+50									4079.14	-2579.99

9110.61  
9164.65  
9334.39  
9742.31

Sta	Bear	Dist	Gas	Sin	N	S	E	W	S	W
103+00	N75°46'W	119.0	.246	.969					-2519.99	9742.31
104+69	S81°14'W	77.0	.066	.998	29.27			115.31	-2548.76	9857.62
105+46	N72°28'W	251.0	.301	.954		5.08		76.85	2522.88	9934.41
107+97	N84°14'W	481.1	.827	.563	75.55			239.45	2619.23	10178.92
112+76.1	N88°32'W	194.2	.779	.628	397.87			170.86	3017.10	10444.78
114+72.3	N87°06'W	127.7	.051	.999	151.28			121.96	3168.38	10566.74
116+00	S85°32'W	615.0	.113	.994	6.51			127.57	3124.89	10694.21
122+15						69.50		611.31	3105.89	11305.62

FLYK WYNS HOKR

PLANT COMM 1018 81 1 0 100000

PLANT COMM 1018 81 1 0 100000



F 164, P 100, 100  
 Co-ord  
 Orig. Time  
 No. (5)  
 LEFAX FILING INDEX

Sta	Beer	Dist	Cre	bin	N	S	E	W	S	W
122+N	579-2W	416.0	.314	.949		120.62		394.98	-3108.39	1205.62
126+31									2974.77	1700.44
129+00	344-31W	769.0	.713	.701		191.60		188.57	2082.97	1888.97
132+00	343-01W	300.0	.730	.687		219.00		204.90	2568.97	1809.387
134	546-21W	200.0	.689	.724		137.80		144.80	2426.17	12238.67
137+08	544-24W	308.0	.714	.700		219.91		215.60	2206.26	12455.27
139+50	56-52E	242.0	.913	.170		240.31	29.04		1965.95	2425.23
141+	do	150.0	"	"		148.95	18.00		1817.00	2407.23





	Ben	Dist	000	Lin	N	S	E	W	S	W
162+	540-40W	281.0	.759	.652		713.78		5328.83	13649.86	13649.86
164+81	564-35W	2520	.429	.903		108.11		227.56	7.44	13962.63
167+33	507-44W	3350	.673	.740		<del>225.46</del> 215.45		247.90	218.02	14208.53
170+68	107-23W	139.0	.539	.842	7492			117.04	143.10	14325.57
172+09	1089-11W	93.0	.014	1.000	1.20			93.00	141.80	14418.57
173+	559-52W	168.0	.502	.865		84.34		105.32	226.14	14563.89
174+68	542-40W	5320	.735	.678		391.02		360.70	617.16	14924.59
180+										

16.10

Bar	Dist	Co	Time	N	S	E	W	S	W
180+									
533-01W	3000	.838	.546		207.40		163.80	677.16	14924.59
183+								888.56	15088.39
536-19W	6000	.806	.592		483.60		355.20	1352.16	15443.59
189+									
538-02W	16340	.788	.616		1287.59		1006.54	2639.73	14450.13
205734									
206734					101.24				
585-08W	11910	.085	.996		104.23		1186.22	2892.99	17626.37
218725									
149-32W	4570	.629	.761	296.59			347.78	2444.40	17984.15
222782									
170-13W	850	.338	.941	28.73			74.98	2415.67	18064.13
222467									
563-00W	3140	.043	.897		139.10		281.66	2554.77	18245.79
226781									

TRAVEL RECORD 1948 SA Y 9 NYRICK

2. TRAVEL RECORDSHEET NO.







	Ben	Dist	Co	Lin	N	S	E	W	S	W
29150	566-38N	310.0	397 300	918		138.95 100.00			4089.13	22389.99
279+	573-42N	300.0	592	806		177.60		241.80	4405.68	22953.69
282+	517-43N	267.0	953	304		204.05		81.17	4660.13	23034.26
28467	552-40N	373.0	634	773		236.08		282.32	4896.61	23322.67
28440	542-49N	666.0	734	650		486.54		452.88	5385.45	23775.47
295406	570-01N	257.0	342	940		87.89		241.58	5473.34	24017.05
297463	576-38N	437.0	191	982		83.47		429.12	5556.81	24446.18
302+						108.12				

S W

105.11





Ben	Dist	Co	fin	N	S	E	W	S	W
372+	582-27W	600.0	133	991	79.80	79.80	1594.60	9598.83	29413.20
378+	580-59W	2400.0	157	988	376.80	376.80	2371.20	9618.63	30007.80
402+	580-40W	1342.0	162	989	217.40	217.40	1324.55	10055.93	32349.00
415+42	14-45W	178.0	986	170	175.51	175.51	3076	10222.83	33703.55
417+20	14-37W	140.0	724	640	101.36	101.36	96.60	9995.92	33830.41
418+60	168-18W	93.0	370	924	36.41	36.41	86.40	9961.55	33916.81
419+53	180-24W	282.0	097	995	27.35	27.35	280.59	9934.20	34197.40
422+35									

9





B D

Co

in

r

s

E

W

495758

575-57N 7375

24

970

✓

179.95

✓

225.09

✓

344.43

✓

10431.35

41316.21

✓

10616.30

42031.59

507107

586-49W 411.5

547

837

✓

480.34

✓

533.77

✓

537.19

✓

11316.73

42910.21

✓

1264.54

12521.88

✓

44174.75

53171.6

546-23W 1746.6

690

724

✓

1205.15

✓

3971.41

✓

4190.76

16493.29

48365.51

✓

589444

546-33W 572.4

688

776

✓

84.43

✓

124.83

16408.86

48500.34

✓

591103

575-57N 159.2

531

808

✓

104.44

✓

57970.16

63442

53997.34

✓

646100

575-53W 5297.0

218

1

✓

98.95

✓

S W

B	D	Co	fin	N	S	E	W	SW
6A6+	589-43N 4768.0	005	1-		23.84		4768.0	180942 53997.34
693+68	569-33N 3367.0	349	937		826.08		2,217,881 154,346 983,22	163024 58765.34
717+35	583-48N 1438.0	108	994		155.30		1429.39 11309.64 62412.59	
731+73	186°N 3800.0	070	998	269.85			3897.29 17039.19 66259.88	
770+78	179-38N 1951.0	175	985	341.42			1921.74 16683.39 68181.62	
789+79	180-44N 1603.0	161	987	258.08			1582.16 16440.29 69763.78	
807+82	173-5W 718.0	202	302	68425			216.84 1556.04 69980.62	
813+			958					

PROPERTY OF THE U.S. GEOLOGICAL SURVEY

FIELD INVESTIGATION BY





Bear	Dist	Co	Su	N	S	E	W	S	W
84457	51-31E	076	1—		125.0	3.25	17202.91	72497.64	
84642	233	987	158		124.96	3.81	17327.91	72494.39	
84844	29-07E	158	967		247.75	49.13	17391.0	72491.22	
84885	22.5	998	069		247.75	49.13	17391.0	72491.22	
85070	53-18W	069	948		229.97	36.81	151.53	73564.02	
85353	2830	915	403		254.55		1140.5	73564.02	
85757	2830	404	915		238.94		1140.5	73564.02	
85975	404.0	740	672		254.0		1140.5	73564.02	
86721	404.0	672	740		298.96		49	72841.56	
86975	718.0	655	756		249.12		164.78	72841.56	
87198	706.0	513	819		.79		640.56	72841.56	

7 BEARS APPROXIMATELY BY DISTANCE GROUP DATE SET BY W. W. WILSON

	Ben	Dist	Ass	fin	N	S	E	W	S	W
867421	36-20W	287.0	732	104		167.69	.59	348.87	18.53	732.215
871408	38-24W	227.0	783	487		177.69	.74	141.76	19.11	732.216
873735	36-21W	218.0	508	559		176.78	.44	178.27	19.53	732.217
875753	33-23W	247.0	911	240		229.79	.84	57.27	19.57	732.218
878+	50-25E	327.0	1.007	007		327.00	.29	3.38	14.23	732.219
88427	35-57W	335.0	962	275		322.45	.27	92.06	20.17	732.220
884762			745	961		152.00	.79	24.75	20.17	732.221
886716			987	987						

12

B	D	Co	dir	N	S	E	W	S	W
886+16	88-09E 1760	990	142		24	99		850.19	744.36
887+2	88-09E 1760	142	970		24.25	24.95		80.21	144.27
890+34	88-09W 2620	875	484		76		.13	117.02	74.33
892+91	88-09W 2620	483	875		11.89		68	174.33	150
894+29	88-09W 2570	971	240		53				
896+03	88-09E 1380	1	018		249.49	61.67		61.67	74.00
894+29	88-09E 1380	018	1		138.0	48			
896+03	88-09W 2650	915	404		137.98	2.45			
896+03	88-09W 2650	404	915		81		46		
896+03	88-09W 2650	927	376		195.80		86.76		
896+03	88-09W 2650	376	927		2741.14		111.83		
896+03	88-09W 2650	927	376		2739.77		117.50		
896+03	88-09W 2650	376	927						
896+03	88-09W 2650	641	967		788.45				
896+03	88-09W 2650	641	967						



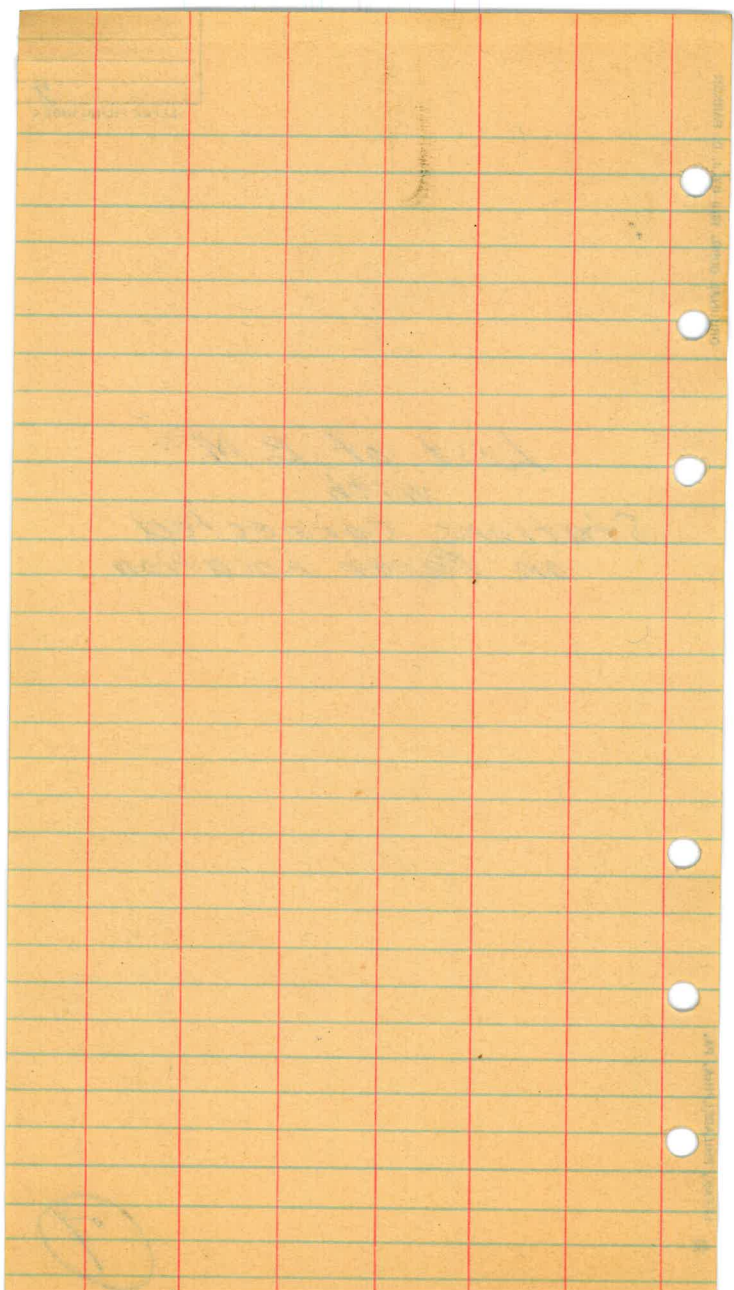




List of B. M.'s  
With  
Stations Corrected  
on Paper Location

⑦





B.M.#1 571.460 Nail in tree  
3' L.1 + 09

B.M.#2 570.564 Nail in syc-  
tr. 20'R.10+05

B.M.#3 570.171 Pt. on Bldr.  
40' R. 19+50

B.M.#4 568.844 Oak tr. 3' R.  
31+65

B.M.#5 543.678 Pt. on bldr.  
15'R.40+85

B.M.#6 539.618 Nail in Oak  
30' R.52+50

B.M.#7 546.027 Nail in Oak  
5' L. 60+42

B.M.#8 547.161 Pt. of Bldr.  
20' R.69+80

B.M.#9 529.904 Nail in Oak  
6' L.76+78

B.M.#10 547.366 Nail in Oak  
4' L.84+40

B.M.#11 545.997 Leaning tree  
2'L. 96+85

B.M.#12 548.340 Pt. on rock  
2'L. 97+40





B.M.#13 520.891 Round peg at ft.  
of post north  
of rd. 103+80

B.M.#14 574.366 Nail in 12" Oak  
20'L. 112+78

B.M.#15 508.445 Power pole 100'L  
121+00

B.M.#16 503.054 Power pole 25' 104  
6'L. 134+00

B.M.#17 502.184 Oak tree 6' R.  
137+70

B.M.#18 509.255 Nail in fence  
50'L. 149+00

B.M.#19 500.758 Cycamore 15'R  
158+00

B.M.#20 504.635 Oak 20'L 167+40

B.M.#21 492.472 Hub in fence  
4'R. 177+63

B.M.#22 491.366 Pole 40'L. 183+50

B.M.#23 491.419 Peg on line  
189+00

B.M.#24 490.912 Nail in pole  
#73938 30'L.  
198+10

220.891 Round peg at E.  
 of post north  
 at rd. 123+82  
 E.M. 413

274.266 Nail in 12" Oak  
 60' E. 112+78  
 E.M. 414

298.225 Lower pole 100' E.  
 181+00  
 E.M. 415

302.681 Power pole 210'  
 5' E. 134+00  
 E.M. 416

302.104 Oak tree 5' E.  
 187+70  
 E.M. 417

308.252 Nail in fence  
 20' E. 149+00  
 E.M. 418

309.722 Gyron 15' E.  
 138+00  
 E.M. 419

309.632 Oak 20' E. 167+70  
 E.M. 420

408.472 Sap in fence  
 4' E. 177+00  
 E.M. 421

431.302 Pole 40' E. 183+00  
 E.M. 422

461.412 Peg on line  
 189+00  
 E.M. 423

480.912 Nail in pole  
 173+00  
 100+10  
 E.M. 424

B.M.#25

486.282 Nail in tel.pole  
30' L. 205+00

B.M.#26

484.342 Nail in power  
pole #73929  
30'L. 212+65

B.M.#27

480.800 Oak 15'L 221+40

B.M.#28

486.482 Corner fence post  
55' L. 226+80

B.M.#29

485.125 Hub on pole 5'R  
237+10

B.M.#30

465.854 Nail in post 2'R  
247+40

B.M.#31

461.347 Nail in fence  
20'R.of gate  
253+75

B.M.#32

463.134 Nail in sycamore  
40'R. 262+00

B.M.#33

455.815 Syca.tree 15'L.  
275+65

B.M.#34

446.620 Nail in 12" cott-  
onwood 80'R.  
286+70

B.M.#35

448.876 Nail in sycamore  
25'R. 298+00

~~B.M.#36~~

~~446.101 Power pole #~~





B.M.#36  
446.101 Power pole 72749  
10' L 302+00

B.M.#37  
443.824 Syca.tr.30'R.303+00

B.M.#38  
U.S.C.S. Conc. Hub at  
438.932 Pump Sta.

B.M.#39  
441.278 Nail in Guy pole  
40' R. 335+10

B.M.#40  
450.117 On pole #74387  
338+25

B.M.#41  
466.272 Pole #74389 3'R.  
351+16

B.M.#42  
458.035 Nail in tel. pole  
#025099-30'R.  
363+00

B.M.#43  
432.996 Hub nailed on  
Eucy.tr.6'L  
378+45

B.M.#44  
403.777 Nail in root of  
slump 393+10

B.M.#45  
430.396 Nail Guy pole  
28'R 400+60

B.M.#46  
421.954 Hub nailed to  
fence post 30'R  
408+45

E.M. 436  
442.101 Power pole 78743  
to J. 402+00

E.M. 437  
443.284 Power pole 78740

E.M. 438  
U.S.C.S. Camp at  
437+00

E.M. 439  
441.278 Rail in cut pole  
to R. 388+10

E.M. 440  
440.117 On pole 47487  
336+82

E.M. 441  
440.272 Pole 47488 2' R.  
341+12

E.M. 442  
442.033 Rail in cut pole  
to R. 302+00

E.M. 443  
442.089 Rail in cut pole  
to R. 378+42

E.M. 444  
442.777 Rail in post of  
camp 302+10

E.M. 445  
442.388 Rail cut pole  
to R. 400+00

E.M. 446  
441.024 Rail in cut pole  
to R. 402+00



B.M.#47 417.160 No.11 in Power  
pole #25773 2'L  
415+92

B.M.#48 407.212 Nail in pole  
#25780 5'L  
423+40

B.M.#49 400.256 Co.B.M. on tree  
6'R 436+12

B.M.#50 393.949 Co.B.M.Pole 72479  
20'R 449+70

B.M.#51 393.440 Pole #72476 40'L  
457+50

B.M.#52 383.857 Pole #72947  
474+30

B.M.#53 381.717 Co.B.M.Pole 72468  
40'L 480+40

B.M.#54 379.508 Pole #24982 2'R  
496+01

B.M.#55 374.021 End of Ry.switch  
50'R. 506+25

B.M.#56 376.461 Pole #72413 4'L  
509+75

B.M.#57 365.510 Pole #72410 Co.BM  
10'R 515-05

B.M. 427  
 417.100 No. 11 in front  
 pole 782712 2' 1/2  
 418-78

B.M. 428  
 407.212 Well in pole  
 782710 2' 1/2  
 428-40

B.M. 429  
 400.000 Co. R. N. on tree  
 8' N 428-12

B.M. 430  
 398.000 Co. R. N. Pole 782710  
 20' N 429-70

B.M. 431  
 395.100 Pole 782710 40' L  
 431-30

B.M. 432  
 392.887 Pole 782707  
 432-00

B.M. 433  
 391.717 Co. R. N. Pole 782609  
 40' L 433-43

B.M. 434  
 379.708 Pole 782602 N' N  
 434-01

B.M. 435  
 376.001 End of N. section  
 20' N 435-23

B.M. 436  
 378.401 Pole 782613 4' S  
 436-75

B.M. 437  
 368.210 Pole 782610 Co. R. N.  
 10' N 437-00

B.M.#58 366.203 Concrete pillar  
70'L. 521+00

B.M.#59 362.585<sup>8</sup> Culvert N.E.  
post 20'R  
537+45

B.M.#60 361.779 15'R 545+00

B.M.#61 369.032 Co.B.M.Pole #  
72384 15'R  
556+42

B.M.#62 365.762 Pole #72379  
Co.B.M.#12, 10'R  
571+50

B.M.#63 365.369 Co.B.M.Pole#  
72376 15'R  
580+50

B.M.#64 369.682 Co.B.M.#11 tree  
at fork or road  
to El Cajon opp.  
589+00, 100'L

B.M.#65 364.525 Nail on pole  
50'L 595+85

B.M.#66 354.749 8'R Pole#23530  
606+35

B.M.#67 343.593 Pole #72289 40'L  
617+70



B.N. 468  
 308.303 Concrete pillar  
 70' L. 521-00

B.N. 469  
 308.308 Driver N.E.  
 post 20' R  
 527-45

B.N. 470  
 301.779 15' R 568-00

B.N. 461  
 309.022 Co. B.N. 461  
 72884 15' R  
 500-48

B.N. 462  
 308.703 Pole 72879  
 Co. B.N. 462 10' R  
 571-50

B.N. 463  
 308.309 Co. B.N. 463  
 72870 15' R  
 500-50

B.N. 464  
 309.682 Co. B.N. 464  
 at left of road  
 to El Cajon ave.  
 500+00, 100' L

B.N. 465  
 304.325 Nail on pole  
 50' L 505-85

B.N. 466  
 304.749 8' R Pole 52520  
 508-55

B.N. 467  
 304.893 Pole 52520 40' L  
 517-70

B.M.#68 ✓  
342.432 Pole #72292 40'L  
626-37 ✓

B.M.#69 ✓  
339.393 Pole #72295 40'L  
635+65 ✓

B.M.#70 ✓  
336.827 Pole #72297 40'L  
641-00 ✓

B.M.#71 ✓  
335.677 Pole #23566 8'R  
650-12 ✓

B.M.#72 ✓  
335.392 Pole 50'L 659-0 ✓

B.M.#73 ✓  
327.201 Pole #75591 50'L  
675-40 ✓

B.M.#74 ✓  
325.277 Pole 23594 3'R  
694-06 ✓

B.M.#75 ✓  
326.761 Nail pepper tree  
50'L 694-00 ✓  
*684+06*

B.M.#76 ✓  
325.363 Hub in fence 50'L  
*705+60 714-70*

B.M.#77 ✓  
318.821 Hub 60'L fence  
post 715-50 ✓

B.M.#78 ✓  
317.530 Nail in tree 30'L  
725-30 ✓

B.M.#79 ✓  
310.545 On post 8'R  
736-50 ✓

B.M. 468  
 322.422 Pole 472222 40' L  
 622-7

B.M. 469  
 322.322 Pole 472222 40' L  
 622-62

B.M. 470  
 322.227 Pole 472227 40' L  
 621-00

B.M. 471  
 322.677 Pole 422222 8' H  
 622-12

B.M. 472  
 322.322 Pole 20' L 622-0

B.M. 473  
 327.201 Pole 472221 50' L  
 672-20

B.M. 474  
 322.277 Pole 22224 2' H  
 621-00

B.M. 475  
 322.701 Half pepper tree  
 60' L 624-00

B.M. 476  
 322.222 Sap in fence 20' L  
 722-20

B.M. 477  
 318.221 Sap 20' L fence  
 post 712-20

B.M. 478  
 317.222 Nail in tree 20' L  
 722-20

B.M. 479  
 310.222 on post 8' H  
 722-20



B.M.#80 <sup>390</sup>  
306.229 40'L 749+75  
B.M.#81  
317.570 Hub on fence  
10'R 761+00  
B.M.#82  
334.131 Lathe on fence  
post 10'R 770+38  
B.M.#83  
341.613 Hub nailed to  
fence post 10'R  
780+86  
B.M.#84  
352.910 Hub nailed to  
fence post 8'R  
789+79  
B.M.#85  
332.255 Eucy. tree 50'L  
~~800+70~~  
800+70  
B.M.#86  
308.236 Nail in post 30'  
L. 810+85  
B.M.#87  
290.471 Hub nailed in  
fence post 30'R  
815+90  
B.M.#88  
309.431 Hub nailed to  
post 3' L.  
824+40  
B.M.#89  
308.179 Nail in post 2'L  
825+88

B.N.480 306.289 40' E 745+78  
 B.N.481 317.070 80' S on fence  
 10' N 741+00  
 B.N.482 324.121 120' S on fence  
 post 10' N 740+22  
 B.N.483 341.013 120' S on fence  
 fence post 10' N  
 736+88  
 B.N.484 352.010 120' S on fence  
 fence post 8' N  
 739+79  
 B.N.485 352.022 120' S on fence  
 fence post 8' N  
 739+79  
 B.N.486 358.222 120' S on fence  
 fence post 8' N  
 740+88  
 B.N.487 360.471 120' S on fence  
 fence post 30' N  
 812+00  
 B.N.488 369.421 120' S on fence  
 fence post 3' N  
 824+40  
 B.N.489 368.172 120' S on fence  
 fence post 3' N  
 824+88

B.M.#90 319.505 Nail in post 2'L  
836+00

B.M.#91 300.649 Paganxline  
Pt. on boulder  
on line 846+10

B.M.#92 285.202 Pt. of rock 1'L  
851+98

B.M.#93 257.942 High pt. of bldr  
20' R. 863+80

B.M.#94 272.341 Nail in oak tr.  
8' R. 869+75

B.M.#95 258.435 On bldr. 15'L.  
877+28

B.M.#96 251.567 On pt. of bldr.  
30' R. 889+52

B.M.#97 255.816 On oak tr. 20'R  
897+75

B.M.#98 251.627 Spot on boulder  
4' from road  
culvert 903+30

B.M.#99 257.478 Pt. of bldr.  
37'L 902+88

(Note: 99 replaces  
98



E.M. 100  
219.505 Well in post 2' L  
00-500

E.M. 101  
200.519 Examination  
pc on Boulder  
on line 040-10

E.M. 102  
222.202 Pt. of rock 1' L  
021-00

E.M. 103  
227.242 High pt. of Bluff  
20' N. 023-00

E.M. 104  
227.241 Well in oak tr.  
9' N. 023-75

E.M. 105  
228.433 On side. 15' L.  
023-75

E.M. 106  
221.227 On pt. of Bluff  
20' N. 023-00

E.M. 107  
225.212 On oak tr. 20' N.  
027-75

E.M. 108  
221.227 Spot on Boulder  
22' N. from road  
cylinder 005-00

E.M. 109  
227.476 Pt. of Bluff  
27' L. 023-00

(Note: 00 replaces  
00)

B.M.#100	269.660	Pt. of boulder 50' L 905+50
B.M.#101	298.182	Top of hub 908+00
B.M.#102	292.651	Pt. of boulder 10' L 912+90
B.M.#103	313.849	Lathe driven by Sumac bush 18' R 918+70
B.M.#104	323.414	Lathe driven beside rock 60' L 924+00
B.M.#105	297.268	Small pt. of stone 35' R. 930+70
B.M.#106	301.670	Lathe driven in ground 2' R 938+85
B.M.#107	309.132	Hub Lathe 15' R 942+25
B.M.#108	308.678	Hub 20' R. 953+00
B.M.#109	340.341	Lathe driven 25' L 956+40
B.M.#110	383.670	Hub in ground 959+85

388.660	Top of bench	50' L 202460	E.N. 4100
388.182	Top of bed	508+00	E.N. 4101
388.681	Pl. of bench	10' L 912-80	E.N. 4102
312.889	Lath driven by same tool in E	912+70	E.N. 4103
382.414	Lath driven bedrock	60' L 924+00	E.N. 4104
387.608	Small pt. of stone E	280+70	E.N. 4105
301.679	Lath driven in ground E	928+88	E.N. 4106
388.122	Lath in E	948+88	E.N. 4107
388.678	Bed 20' E	852+00	E.N. 4108
340.241	Lath driven	85' L 852+80	E.N. 4109
388.670	Bed in ground	852+00	E.N. 4110



B.M.#111 395.111 Hub 18' R 962+60  
B.M.#112 376.936 Pt. on boulder  
18' L 968+00  
B.M.#113 371.562 Hub 10' L 974+00  
B.M.#114 333.390 Hub 10' L. 984+00  
"A" Line  
B.M.#115 218.543 P.I. Hub 15+056 *Bisselle's list*  
B.M.#116 335.974 P.I. Hub 25+55  
B.M.#117 322 354.037 Hub 30' L 45+55  
B.M.#118 329.807 Hub 30' R 55+00  
B.M.#119 336.381 Hub 20' L 66 B  
B.M.#120 326.652 Hub 20' L 87+55  
B.M.#121 268.017 Hub 20' L 98+10  
B.M.#122 202.655 Rock 30' R.  
100+20  
B.M.#123 149.817 Hub 30' L 102+80  
B.M.#124 89.144 Syc. tr. 122+00  
B.M.#125 104.781 Nail in 8" tr.  
1' L. 128+97



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9

Relocation  
between  
Sta. 135 + 83.7  
    &  
Sta. 173 + 24.2

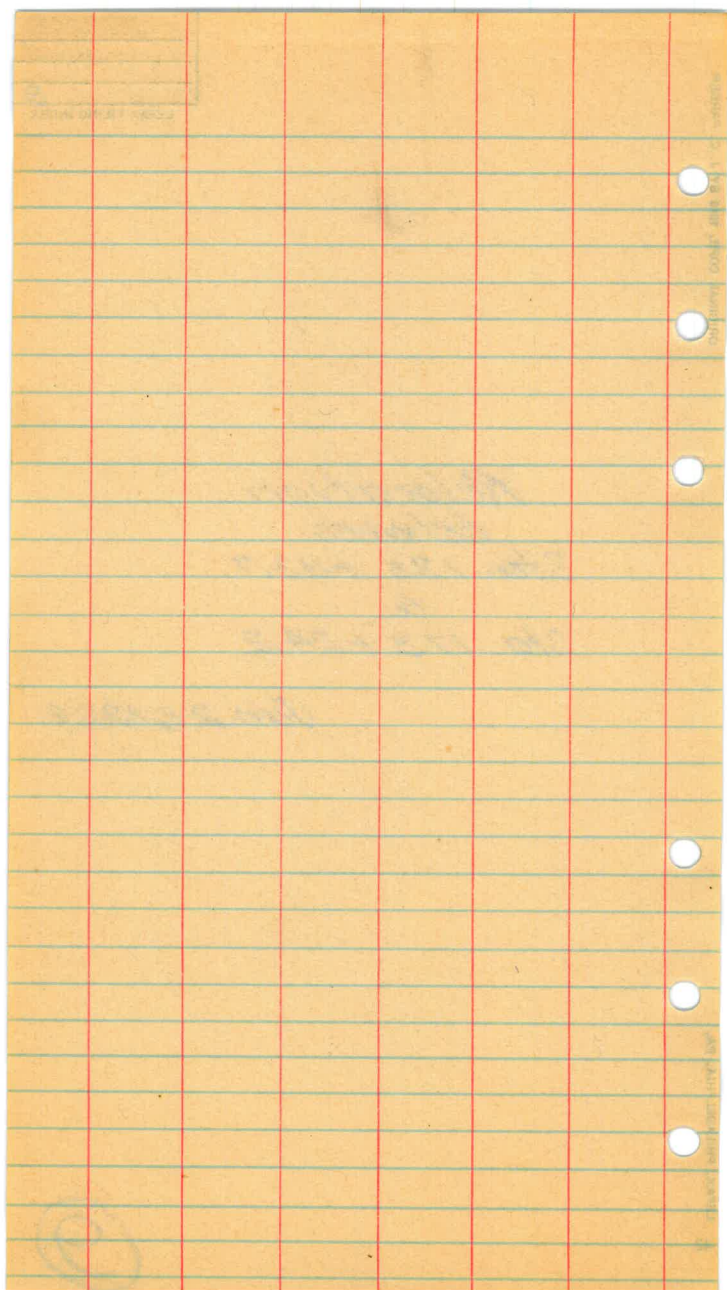
Jan. 21, 1926.

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⑨





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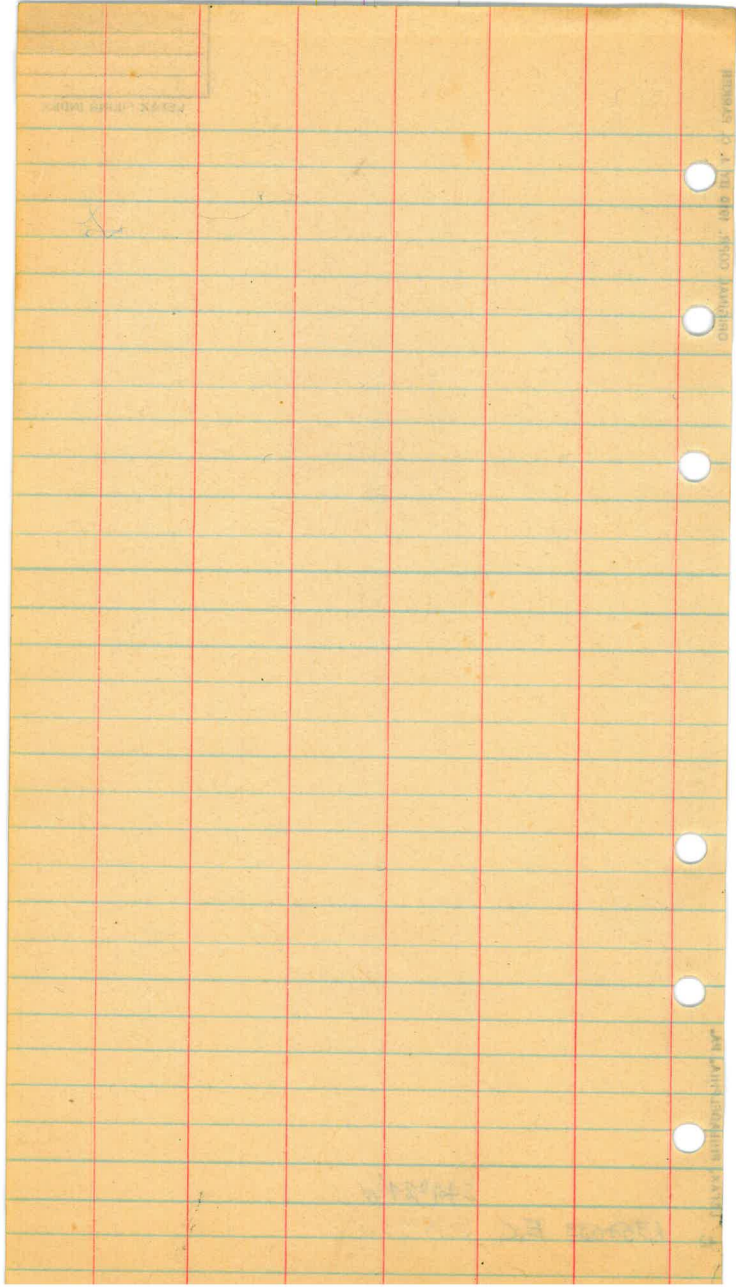
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135703<sup>o</sup> E.C.

S44<sup>o</sup>24'W

S44<sup>o</sup>24'W





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Relocation bet. Sta. 135+83.7  
Sta. 173+24.2

152+60<sup>±</sup> P.O.T.

145+91 P.O.T.

145+89<sup>±</sup> P.O.T.

Land Tie

140+60 P.O.T.

5.40<sup>±</sup>2'W

135+83.7  
135+83.2 = 4'0.2'L.

5.44<sup>±</sup>2'W

134+64<sup>±</sup> P.I.

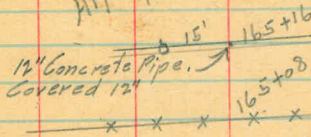
5.59° 52' W

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173+24<sup>3</sup> E.C.  
168+36<sup>2</sup> P.I. =

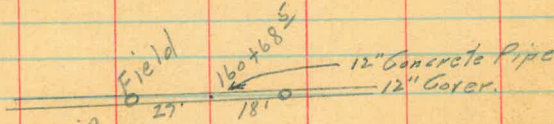
15° 26'  
5.59° 52' W  
40 32  
190° 30' R.

Alfalfa Field.



49  
70) 920.5  
80  
180  
180

Grain Field

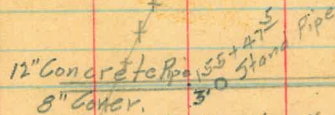


159+72.0

674.2 Land Tie  
N 35° 49' W → Cor.

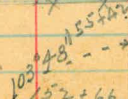
Alfalfa

Alfalfa



10348  
207'36"

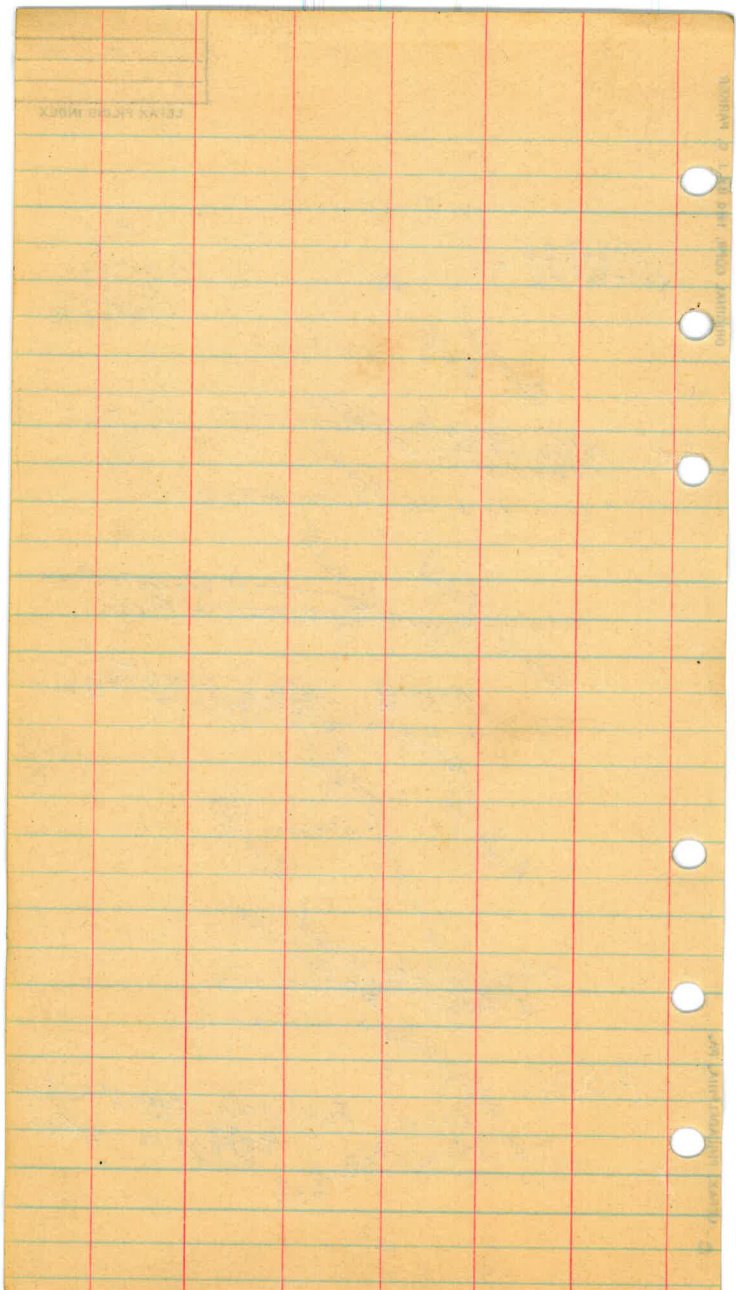
Alfalfa



423.7  
N 35° 50' W → Cor.

632





RELAY FACTORY INDEX

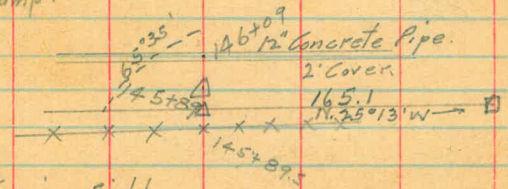
CONTINUED FROM PAGE 101 OF 1000000

101 OF 1000000

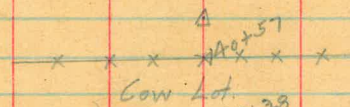
Jan. 21. 1926.

149+60 7' 12" or 14" Concrete Pipe  
Grain Field Buried 2'

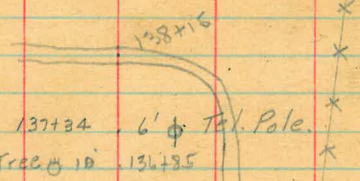
148+00 12' Large Oak Stump  
Large Oak Stump. 15' 147+90



Grain Field.



6" Iron Pipe 139+12 10' Stand Pipe  
Buried 3' 138+91 20' Concrete Sump 10' in Diameter



135+83.7 P.I. =  
135+83.7 Pott. =

18' Rd. 39'

173+45<sup>±</sup> B.C.

F.C.

539°52'W  
55949W

173+24<sup>±</sup>  
168+36<sup>B</sup> 19°27'R

E:  
T=  
R=  
D: 50°  
L=

B.C.

159+80° P.O.T.  
159+77° P.O.T.

Land Tie

152+63<sup>L</sup> P.O.T.

540°22'W

Land Tie

152+60° P.O.T.



Bottom Ditch

Pipe Line. 12" Concrete Pipe. 8" Cover.

12" Concrete Pipe. 12" Cover.

Pipe Line. 12" Concrete Pipe. 12" Cover.

B.M. #20		504.64
2.35	506.99	
T.P.		11.05 495.94
6.35	502.29	
166		10.4 491.9 ✓
167		11.3 491.0
168		11.7 490.6
+10		11.8 490.5
+36 <sup>2</sup> =		5.6 496.7
173+24 <sup>2</sup>		

Levels from Sta. 146. to Determine  
Difference in Elev. bet. River and  
~~146~~ lowest point on Line.

146		497.60
5.35	502.95	
		4.18 498.77
3.90	502.67	
		5.90 496.77
4.02	500.79	
		4.5 496.3 Top Bank
		9.7 491.1 River Bottom

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Levels on Relocation  
Sta. 135+83.2 to Sta. 173+24.2

B.M. #17		502.18
4.47	506.65	
135+83.2		4.5 502.2 ✓
136		4.5 502.2
137		4.5 502.2
138		5.0 501.7
+05		6.0 500.7
+15		5.0 501.7
+70		4.5 502.2
+75		5.7 501.0
+90		14.4 492.3
139		4.8 495.7
+12		4.8 501.9
+20		4.6 502.1
140		4.4 502.3
+60		5.0 501.7
141		5.6 501.1
142		5.4 501.3
T.P.		5.17 501.48
1.05	507.53	
143		2.0 500.5
144		2.4 500.1
+20		4.7 497.8
145		5.5 497.0
146		4.9 497.6
+09		5.0 497.5
147		6.2 496.3
148		6.7 495.8
+40		3.8 498.7
149		3.5 499.0
+50		3.4 499.1
150		4.1 498.4

Jan. 21, 1926.

Edge Road.

Edge Hole.  
Bottom

6" Iron Pipe, Covered 3'

Edge Bank

12" Concrete Pipe, 2' Cover.

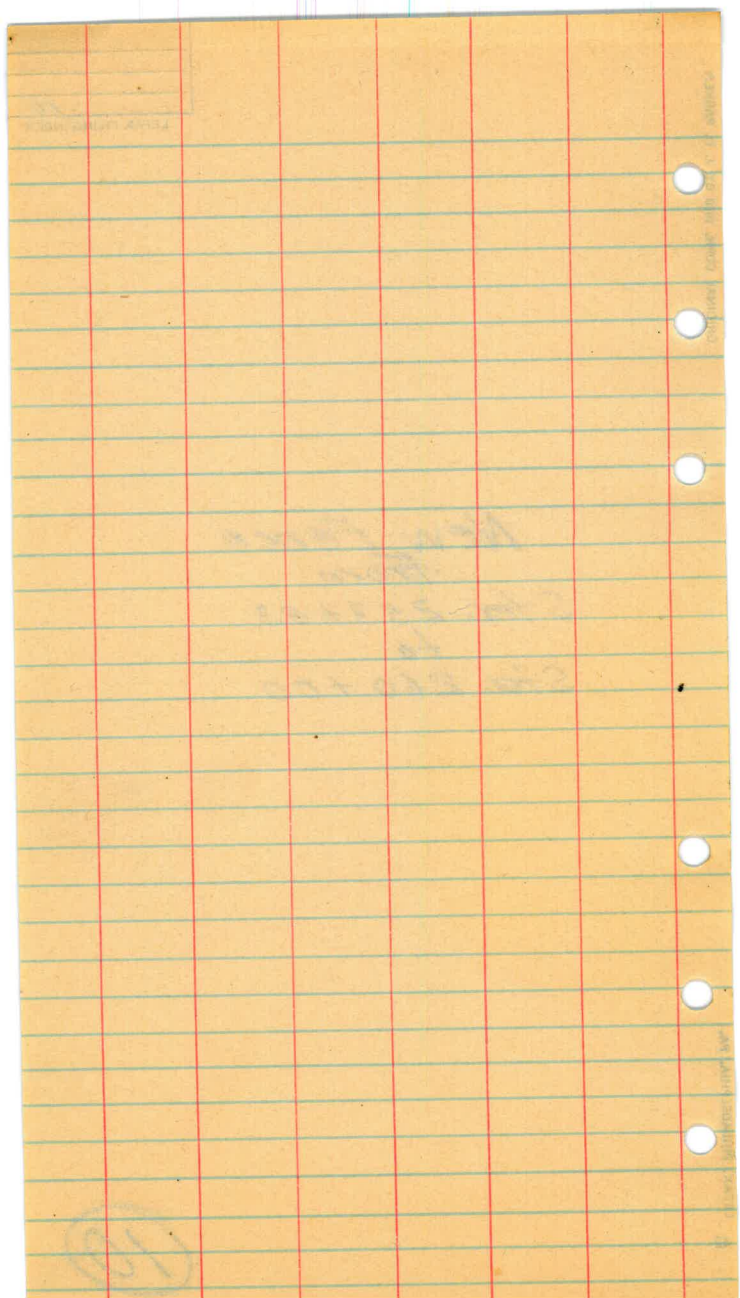
Edge Bank.

	502.53		
T.P.		3.97	498.56
	2.16	500.72	
151		2.8	497.9
152		3.3	497.4
+60		3.3	497.4
+66		4.2	496.5
+68		3.3	497.4
153		4.0	496.7
154		4.8	495.9
155		5.2	495.5
+47		5.4	495.3
156		5.1	495.6
157		5.9	494.8
158		6.6	494.1
T.P.		6.47	494.25
	3.32	497.57	
159		3.6	494.0
+77		3.2	494.4
+80		4.0	493.6
160		4.3	493.3
+68		4.3	493.1
161		4.6	493.0
162		4.8	492.8
163		5.2	492.4
164		5.8	491.8
165		5.8	491.8
+16		6.0	491.6
166		5.7	491.9
T.P.		5.65	491.92



New Fence  
From  
Sta. 253+83  
to  
Sta. 260+00

10

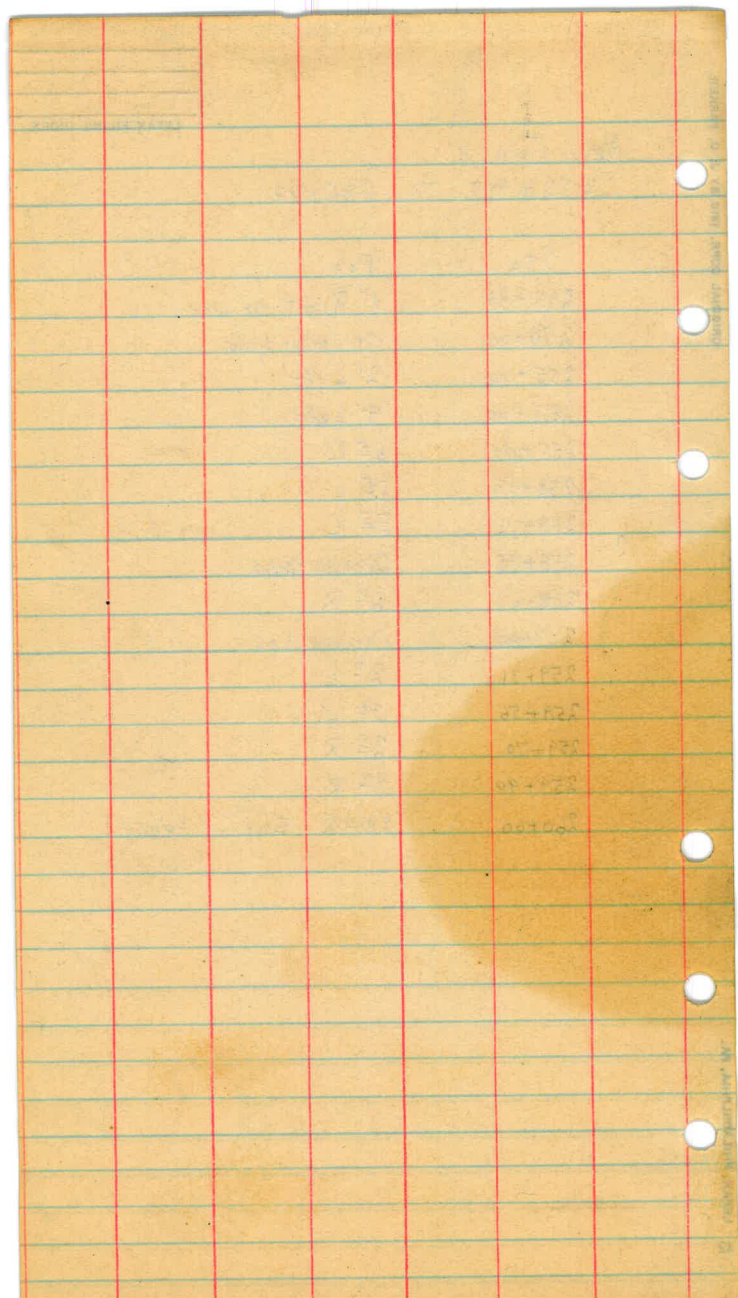


## New Fence

253+83 to 260+00

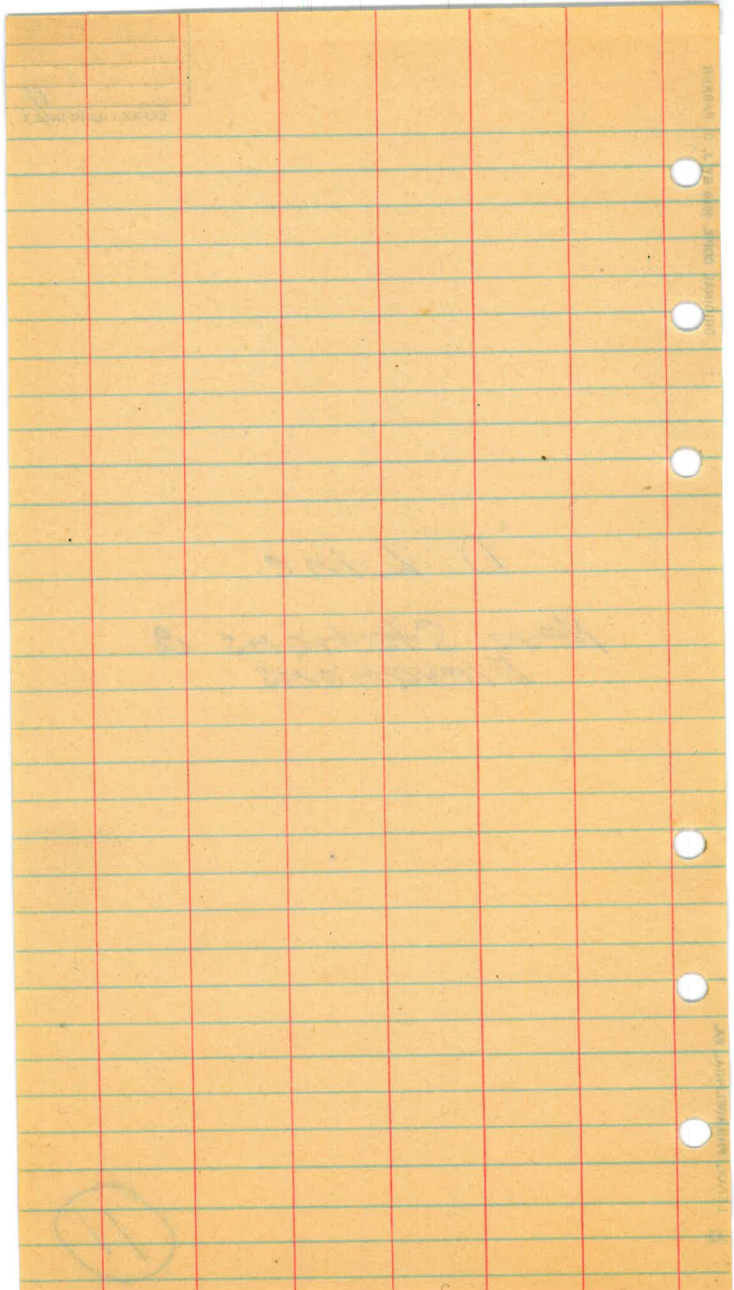
Sta	Fce
253+83	1' Right of Line
254+00	On Center Line
255+00	2' Left
256+00	4' Left
257+00	6 $\frac{1}{2}$ L
258+00	7 $\frac{1}{2}$ L
258+12	5 $\frac{1}{2}$ L
258+35	Crosses line
258+63	6 $^{\circ}$ R
259+00	Crosses line
259+31	7 $^{\circ}$ L
259+56	2 $^{\circ}$ L
259+70	2 $\frac{1}{2}$ R
259+90	9 $^{\circ}$ R
260+00	20 $^{\circ}$ R End of fence





"D" Line  
New Stations &  
Elevations

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D-Line

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Sta.	+	∇	-	Elev.
				104.781
		116.883		
129+22.7	1111+05 <sup>4</sup>	PC	12.0	104.9
+47.7	1111+30 <sup>4</sup>		13.1	103.8
+72.7	+55 <sup>4</sup>		12.2	104.7
97.7	+80 <sup>4</sup>		11.4	105.5
130+22.7	1112+05 <sup>4</sup>		9.9	107.0
47.7	+30 <sup>4</sup>		1.8	115.1
T.P.	12.300		1.365	115.518
		127.918		
130+72.7	1112+55 <sup>4</sup>		6.6	121.2
T.P.	11.873		0.939	126.879
		138.752		
130+92.7	+80 <sup>4</sup>		11.0	127.8
131+22.7	1113+05 <sup>4</sup>		6.4	132.4
+47.7	+30 <sup>4</sup>		3.2	135.6
+72.7	+55 <sup>4</sup>		1.4	137.4
T.P.	11.091		.608	138.144
		149.235		
+97.7	+80 <sup>4</sup>		9.7	139.5
132+22.7	1114+05 <sup>4</sup>		6.8	142.4
47.7	+30 <sup>4</sup>		4.2	145.0
T.P.	11.444		.719	148.516
		159.960		
72.7	EG = 1114+55 <sup>4</sup>		7.9	152.1
133+00	1114+82 <sup>4</sup>		2.0	158.0
T.P.	11.527		1.080	158.880
		170.407		.961 169.446
T.P.	12.124		.961	169.446
		181.570		.829 180.741

## D-Line

Sta	+ T	- Elev	B.M.
	11.628	192.369	180.741
134+00	11.15782 <sup>7</sup>	4.4	188.0
T.P	11.867	.934	191.435
		203.302	
T.P	12.469	1.845	201.457
		213.926	
T.P	11.909	1.401	212.525
		224.434	
135+00	11.16787 <sup>7</sup>	1.6	222.8
T.P	12.467	1.257	223.177
		235.644	
T.P	11.754	1.194	234.450
		246.804	
T.P	9.098	1.132	245.072
		254.170	
T.P	6.111	1.155	253.015
		259.131	(B.M. 253.002)
		259.113	(Sta. 1120+00)
136+00	11.17722 <sup>7</sup>	12.6	246.5
+42 B.C.	11.1876 <sup>7</sup>	2.8	256.3
T.P	11.636	.868	258.245
		267.899	
		267.881	
136+77	11.1651 <sup>7</sup>	8.2	261.7
+92	11.1876 <sup>7</sup>	2.0	267.9
T.P	11.464	.637	269.244
		280.716	
		280.708	
137+00	11.18784	11.1	269.6
+17	11.19701	6.8	273.9
+42	1.26	1.2	279.5
T.P	11.499	.651	280.57
		291.574	
		291.556	

# D-Line

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Sta.	+ T	-	Elev
	291.574		B.M.
	291.556		
137+67	1119+51	7.2	284.4
+92	+76	2.8	288.8
T.P.	11.829	1.187	290.369
	302.216		
	302.178		
138+17	1120+01	9.2	293.0
+92	+26	5.3	296.9
+67	+51	1.2	301.0
T.P.	11.299	.975	301.223
	312.540		
	312.522		
+92	+76	6.4	306.1
139+22	E.C. 1121+05	.9	311.6
T.P.	11.724	.983	311.539
	323.263		
T.P.	11.772	1.083	322.180
	333.972		
	333.952		
		.763	333.189
			333.317

(B.M.)  
Sta. 1125+00



Sta.	+	$\bar{A}$	-	Elev. B.M.
				333.317
.764		334.081		
			11.508	322.273
.799		323.071		
			11.824	311.247
.822		312.069		
			10.833	301.236
.607		301.843		
			11.372	290.471
1.248		291.719		
			11.410	280.309
.639		280.948		
			11.612	269.336
1.198		270.534		
			11.225	259.309
1.306		260.615		
			7.512	253.103

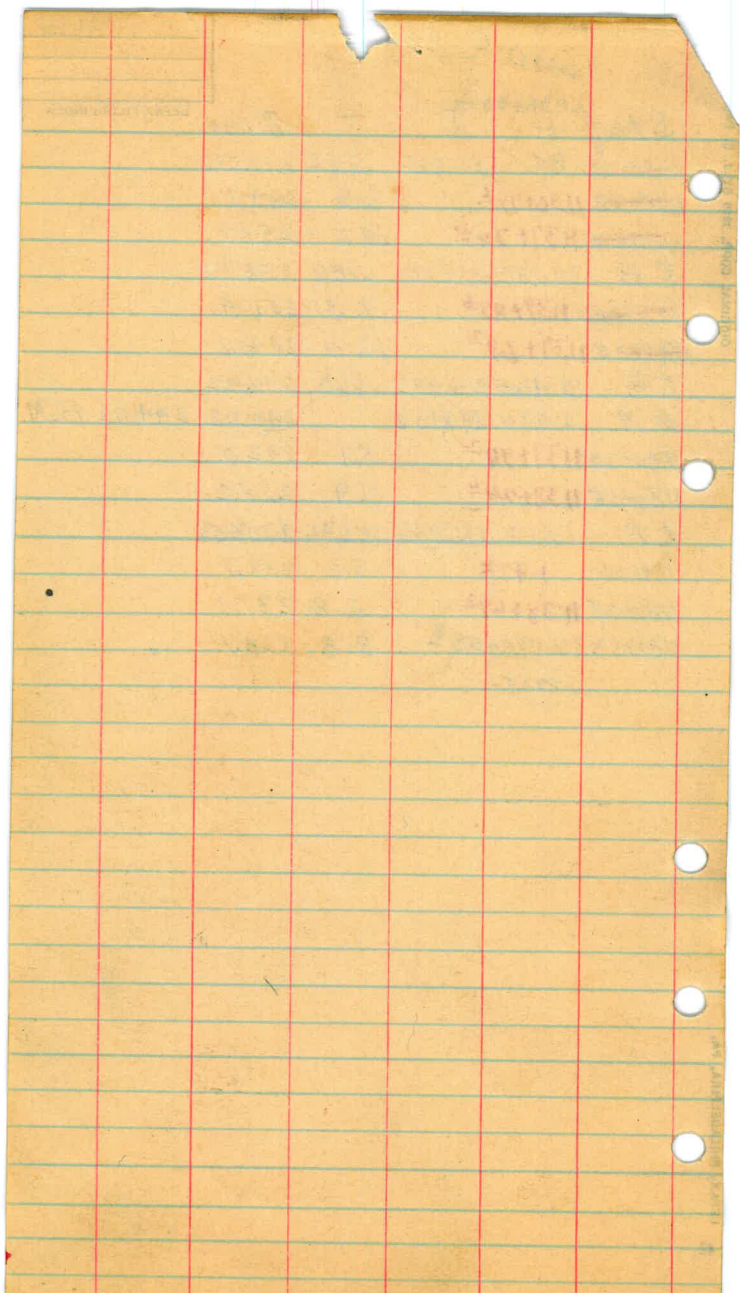
-205.8 CURVE

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Sta	+ 1136+69 <sup>6</sup>	- Elev
<del>1139+054</del> B.C.	270.862	.652 270.210
1139+30	1136+99 <sup>6</sup>	6.8 264.1
1139+55	1137+24 <sup>6</sup>	13.0 257.9
T.P.	12.132 258.730	.180 258.910
1139+80	1137+49 <sup>6</sup>	7.3 251.4
1140+05	1137+69 <sup>2</sup>	12.0 246.7
T.P.	12.468 246.442	.660 247.102
B.M.	2.990 247.102	244.112 244.112 B.M.
1140+30	1137+74 <sup>2</sup>	5.1 242.0
1140+55	1138+24 <sup>6</sup>	11.9 235.2
T.P.	1.450 236.706	11.646 235.456
1140+80	+49 <sup>6</sup>	3.2 233.7
1141+05	1138+69 <sup>2</sup>	5.8 231.1
1191+39.3 = 1139+09 <sup>8</sup>		8.8 228.1
	235.5	

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Station	Elev	Sta.	Elev
1120+00	250.8	1133 <sup>20+63</sup> +00	337.5
+35	255.9	1130 <sup>81</sup> +18	338.5
+50	260.3	1131 <sup>09</sup> +46	337.6
+85	264.6	" <sup>19</sup> +56	336.7
1121+00	267.8	1134 <sup>31+63</sup> +00	327.2
+40	275.4	+95 +32	319.7
1122+00	287.2	1132 <sup>33</sup> +70	306.3
1123+00	303.8	1135 <sup>2+63</sup> +00	299.7
+70	316.9	+78 +15	297.2
1124 <sup>1121+63</sup> +00	320.5	1136 <sup>3+63</sup> +00	286.6
1122 <sup>1121+13</sup> +50	327.5	1134 <sup>105</sup> +42	284.2
1125 <sup>1122+62</sup> +00	335.8	+07 +44	283.1
1123 <sup>1123+13</sup> +50	339.7	+09 +46	284.2
" <sup>1123+43</sup> +80	342.3	1133 <sup>33</sup> +70	286.2
1126 <sup>1123+63</sup> +00	342.7	1137 <sup>4+63</sup> +00	286.4
1123 <sup>1123+83</sup> +80	342.7	1135 <sup>23</sup> +60	290.0
1127 <sup>1124+63</sup> +00	341.9	1138 <sup>5+63</sup> +00	287.5
1125 <sup>1125+33</sup> +70	340.0	1135 <sup>7</sup> +28	285.0
1128 <sup>1125+63</sup> +00	336.8	1136 <sup>14</sup> +51	281.9
1126 <sup>1126+7</sup> +50	331.5	1136 <sup>48</sup> +85	273.9
1126 <sup>1126+63</sup> +00	324.5	1139+00	271.6
+88	321.4	+60	256.8
1127 <sup>1127+38</sup> +75	311.9	1140+00	
1120 <sup>1127+63</sup> +00	307.3	Curve from	
+93	300.8	1139 to 1141 - see	
1128 <sup>1128+43</sup> +80	311.0	extra sheet	
1131 <sup>1128+28</sup> +00	313.5	1139 <sup>69.5</sup> +00	225.2
1132 <sup>1131+39</sup> +00	328.8	+90 <sup>5</sup> +25	223.1
1130 <sup>1132+13</sup> +50	333.3	1140 <sup>55</sup> +00	220.8
		(over) 1140+200	

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Sta.	Elev		
<del>1143+00</del>	217.7	<del>1140+65.5</del>	1140+50
+10	217.3	+75.5	+60
<del>1143+70</del>	211.7	<del>1141+35.5</del>	1141+20
+90	211.3	<del>1141+55.5</del>	+40
1144+00	210.3	1141+65.5	+50
+15	208.4	+80.5	+65
+50	206.0	1142+10.5	+95
+80	204.8	1142+45.5	1142+30
1145+00	202.1	1142+65.5	+50
+10	197.3	+75.5	+60
+77	154.9	1143+42.5	1143+27
+82	150.9	+47.5	+32
+85	153.8	+50.5	+35
+92	154.9	+57.5	+42
1146+00	158.4	1143+65.5	+50
+40	184.0	+44+65.5	+90
+50	189.1	44+15.5	1144+00
+59.5	192.6	+25.0	+10
+75	189.4	+40.5	+25
1147+00	184.3	1144+65.5	+50
+75	175.4	45+40.5	1145+25
1148+00	171.4	1145+65.5	+50
+20	165.7	+85.5	+70
1149+00	165.9	1146+45.5	1146+50
+20	167.3	+85.5	+70
+36.1	162.3	1147+01.6	+86
1150+00	146.4	1147+65.5	1147+50
+25	143.8	+90.5	+75
1150+34.6	140.1	1148+00.1	1147+85
+55	135.7	1148+20.5	1148+00



El Capitan Pipe Line Survey.  
March, 1926.

Stadia Traverse from  
Sta. 15+05<sup>6</sup> Bissell's "H" Line  
to Sta. 812+31<sup>3</sup> Final Location  
Line,

G.W. Converse - Field Engr.  
H. M<sup>c</sup>Carty - Inst.  
W<sup>m</sup> Simpson - Rod  
H. Reynolds - Rod.

Set from top

Set from top  
of 6' high bench

475

1000 1/15

Small wash

A line 15. 15. 3



Sta	Hor L	Bear Vert L	H. I	Rod	Elev
M	Δ				275.1
		N.36°57.5E + 4°06'		2.94	21.0
L	Δ	18°6'30"R	4.72		254.1
		N.18°51'E + 3°51'		2.92	133.3
K	Δ	58°11'R	5.01		<del>234.5</del> 19.6
		-9°35'		6.83	112.3
J	P.O.T				130.5
		-13°20'		5.11	115.1
I16+35	P.O.T				191.1
		-14°02'		4.87	114.5
H14+98	P.O.T				221.9
		N.39°20'W - 16°19'		4.53	122.4
I17+6	Δ	10°17'L	4.745		<del>305.6</del> 122.1
		-11°18'		2.23	<del>344.3</del> 42.9
F10+60	P.O.T		4.94		<del>389.5</del> 4.2
		-2°03'		1.18	4.2
E14+61	P.O.T				251.5
		-10°57'		5.18	97.0
B3+71	P.O.T				251.3
		-8°47'		6.04	251.3
		-8°35'		6.15	348.5
B171A	P.O.T		5.16		373.7
		+6°45'		11.14	130.1
		+6°43'		15.05	175.0
R2+19	P.O.T				190.4
		-16°34'		1.11	190.4
Q+62	P.O.T				292.7
		+4°25'		9.67	301.3
A+16	Δ P.O.T		4.78		221.6
		N.29°03'W + 1°15'		1.15	201.6
O+0.0	Δ 105°00'R		5.0		218.5
		S.45°57'W			2.5
124					



Sta.	Hor. $\Delta$	Bear.	Vert. $\Delta$	H.I	Rod	Elev.
A,						311.2
		N 2° 42.5' E	+ 0° 28'	0.93		0.8
Z	$\Delta$ 56° 09' 30" R			5.25		310.4
		N 52° 27' W	+ 3° 49'	3.16		20.9
Y	$\Delta$ 47° 39' 32"			5.00		289.5
		N 57° 51' W	+ 1° 12'	0.74		1.5
X	$\Delta$ 94° 59' 30" L			5.12		288.0
		N 89° 12' E	- 0° 17'	3.12		1.5
W	$\Delta$ 27° 32' R			5.24		289.6
		N 61° 40' E	- 1° 09'	0.74		1.5
V	$\Delta$ 37° 01' R			5.19		291.1
		N 24° 39' E	- 0° 40'	2.53		2.9
U	$\Delta$ 10° 49' L			5.18		294.0
		N 35° 28' E	- 1° 10'	1.83		3.7
T	$\Delta$ 15° 19' L			5.04		297.7
		N 50° 47' E	- 0° 49'	3.74		5.3
S	$\Delta$ 12° 27' 30" R			5.25		303.0
		N 38° 12.5' E	- 1° 02'	6.70		12.1
R	$\Delta$ 30° 23' 30" R			5.14		315.1
		N 8° 16' E	- 2° 26'	2.16		9.1
Q	$\Delta$ 60° 02' 30" L			4.98		324.7
		N 68° 55' E	- 2° 43'	1.32		6.3
P	$\Delta$ 12° 26' R			5.10		330.5
		N 55° 52.5' E	+ 2° 57'	3.90		20.0
O	$\Delta$ 31° 12' R			5.10		310.5
		N 24° 49.5' E	+ 4° 14'	4.00		29.4
N	$\Delta$ 13° 0' R			5.23		281.1
		N 11° 46.5' E	+ 3° 21'	1.03		6.0
M	$\Delta$ 25° 17' L			5.11		275.1
		N 36° 57.5' E				



Hor. Dist. Dist.

③  
LEFAX FILING INDEX

	5.63
	4.60
	<u>10.3</u>
Fwd. from Sta "Y"	5.11
	5.23
	3.23
	<u>20.0</u>
Fwd. from Sta "X"	7.50
	7.05
Fwd. from Sta "W"	5.10
	1.95
	<u>3.90</u>
Fwd. from Sta "V"	5.76
	1.32
Fwd. from Sta "U"	6.06
	3.90
	<u>2.16</u>
Fwd. from Sta "T"	5.14
	1.79
	<u>3.35</u>
Frd. from Sta "S"	6.70
	5.25
	3.38
	<u>1.87</u>
Frd. from Sta "R"	5.95
	4.12
	<u>1.83</u>
Frd. from Sta "Q"	6.45
	5.18
	<u>1.27</u>
Frd. from Sta "O"	2.54
	6.45
	3.92
Frd. from Sta "N"	2.53
	6.79
	3.67
	<u>3.12</u>
Frd. from Sta "M"	6.58
	3.42
	<u>3.16</u>

Sta	Hor Ang	Bear	Vert Ang	H.I.	Rod	Elev
B.M.						313.775
			-3°28'		0.91	5.5
N <sub>1</sub>						321.3
			N7°04'E-3°40'		6.66	42.5
M <sub>1</sub>	0°48'L			5.42		363.8
			N7°52'E-1°55'		3.15	10.5
L <sub>1</sub>	30°15'30"L			5.09		374.3
			N38°07'SE+2°15'		2.83	11.1
K <sub>1</sub>	23°11'30"L			4.95		363.2
			N61°19'E+2°27'		5.78	23.9
J <sub>1</sub>	39°28'L			5.18		339.3
			S79°93'E+3°20'		6.38	37.0
I <sub>1</sub>	13°20'30"L			5.08		302.3
			S65°52'SE-3°20'		3.56	20.6
H <sub>1</sub>	29°08'L			5.03		322.9
			S36°44'SE-4°06'		2.11	15.1
G <sub>1</sub>	50°50'R			5.25		338.0
			S87°34'SE-3°38'		1.59	10.1
F <sub>1</sub>	35°12'L			5.22		348.1
			S52°22'SE-3°42'		2.16	13.9
E <sub>1</sub>	30°29'30"R			5.19		362.0
			S82°52'E-1°20'		3.66	8.5
D <sub>1</sub>	36°39'R			5.32		370.5
			N60°29'E+0°31'		0.80	.72
C <sub>1</sub>	21°43'R			5.19		369.8
			N38°46'E+3°22'		6.92	40.5
B <sub>1</sub>	14°16'30"R			5.22		329.3
			N24°29'SE+1°56'		5.36	18.1
A <sub>1</sub>	21°47'R			5.22		311.2
			N2°42'SE			

Hor Dist Slope Dist

From Sta "N,"

Frd. from Sta. "M,"

Frd. from Sta. "L,"

Frd from Sta. "K,"

Frd from Sta. "J,"

Frd from Sta. "I,"

Frd from Sta. "H,"

Frd from Sta. "G,"

Frd from Sta. "F,"

Frd from Sta. "E,"

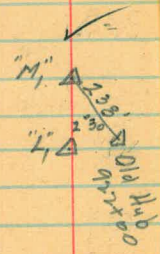
Frd from Sta. "D,"

Frd from Sta. "C,"

Frd from Sta "B,"

Fwd from Sta. "H,"

Fwd from Sta "Z"



+19  
 211  
 ---  
 681  
 325  
 356  
 8.27  
 508  
 319  
 ---  
 638  
 8.07  
 518  
 289  
 ---  
 478  
 637  
 354  
 ---  
 283



Sta Hor Δ Bear Vert Δ HI Rod Elev

U <sub>1</sub>		-0°08'	5.19	6.56
T <sub>1</sub>	14°16'30" R	+3°02'	5.03	0.68
S <sub>1</sub>	68°57' L	-0°58'	5.31	6.60
R <sub>1</sub>	36°36'30" R	-1°18'	5.07	1.18
Q <sub>1</sub>	70°24' R	-0°05'	5.19	4.79
P <sub>1</sub>	22°20' L	-2°26'	5.02	2.30
O <sub>1</sub>	26°05'30" L			

Slope  
Dist      Hor.  
                 Dist.

LEFAX FILING INDEX

202530

6.18
<u>3.87</u>
2.30
5.19
<u>2.80</u>
2.39
<u>2</u>
4.78
5.66
<u>4.48</u>
1.18
8.61
<u>5.31</u>
3.30
<u>2</u>
5.37
4.69
0.68
5.19
<u>1.91</u>
3.28
<u>2</u>
6.56

Fwd from Sta. T,

Fwd. from Sta. S,

Fwd. from Sta R,

Fwd. from Q,

Fwd. from P,

Fwd. from O,

Fwd. from N,

Sta HorA Bear VertA H.I. Rod Elev

N,

N7:13



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LEFAX, PHILADELPHIA, PA.

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LEFAX FILING INDEX

6.13  
4.42  

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1.71

Sta	Hor Δ	Bear	Vert Δ	H.I.	Rod
			+1°33'		5.78
H <sub>2</sub>	25°26' L		-0°45'	5.21	3.15
G <sub>2</sub>	22°05' L		+1°03'	5.29	5.36
F <sub>2</sub>	13°19'30" L		+0°39'	5.12	5.38
E <sub>2</sub>	6°48'30" L		-0°41'	5.10	6.38
D <sub>2</sub>	27°39' R		+0°32'	5.19	4.28
C <sub>2</sub>	18°45'30" R		+3°14'	5.27	3.46
B <sub>2</sub>	28°27'30" R		+0°47'	5.22	1.99
A <sub>2</sub>	22°57' L		-1°31'	5.01	5.30
Z <sub>1</sub>	17°35'30" R		-0°49'	5.25	2.19
Y <sub>1</sub>	36°48' L		+1°34'	5.31	2.29
X <sub>1</sub>	15°57' R		+0°28'	5.35	1.49
W <sub>1</sub>	13°40' R		-2°03'	5.19	2.33
V <sub>1</sub>	27°23' L		+0°50'	5.18	1.71
U <sub>1</sub>	8°06'30" R		-0°08'	5.28	6.56
T <sub>1</sub>	14°16'30" R			5.19	

Elev. Slope D Hor. Dist

LEFAX FILING INDEX

510

241

2.69

2

1.78

7.80

Fwd from Sta. F<sub>2</sub>

5.12

2.68

Fwd from Sta. E<sub>2</sub>

5.36

6.86

Fwd from D<sub>2</sub>

3.71

3.15

Fwd from Sta. C<sub>2</sub>

5.29

3.71

Fwd from Sta. B<sub>2</sub>

1.18

5.29

3

1.18

Fwd from Sta. A<sub>2</sub>

5.21

2.32

Fwd from Sta. 2<sub>1</sub>

5.89

2.78

Fwd from Sta. Y<sub>1</sub>Fwd from Sta. X<sub>1</sub>Fwd from Sta. W<sub>1</sub>Fwd from Sta. V<sub>1</sub>Fwd from Sta. U<sub>1</sub>Fwd from Sta. T<sub>1</sub>Fwd from Sta. S<sub>1</sub>



Sta Hor Δ Bear Vert Δ H.I. Rod

BM#87		+0°35'	2.32
S <sub>2</sub>	51°20'	to 802 + 7.8 - S 45°36'E	
		+1°15'	5.22
R <sub>2</sub>	29°26'30"R		5.27
		-0°33'	7.86
Q <sub>2</sub>	34°11'L		5.21
		-2°24'	0.95
P <sub>2</sub>	32°58'30"R		5.11
		+0°30'	4.18
O <sub>2</sub>	17°21'30"L		5.28
		-0°57'	3.39
N <sub>2</sub>	25°56'R		5.22
		-2°56'	1.65
M <sub>2</sub>	10°11'30"R		5.21
		+0°01'	3.64
L <sub>2</sub>	31°08'R		5.35
		+2°01'	2.17
K <sub>2</sub>	19°48'30"L		5.34
		+1°55'	1.09
J <sub>2</sub>	24°35'R		5.29
		+3°34'	2.88
I <sub>2</sub>	13°01'30"R		5.06

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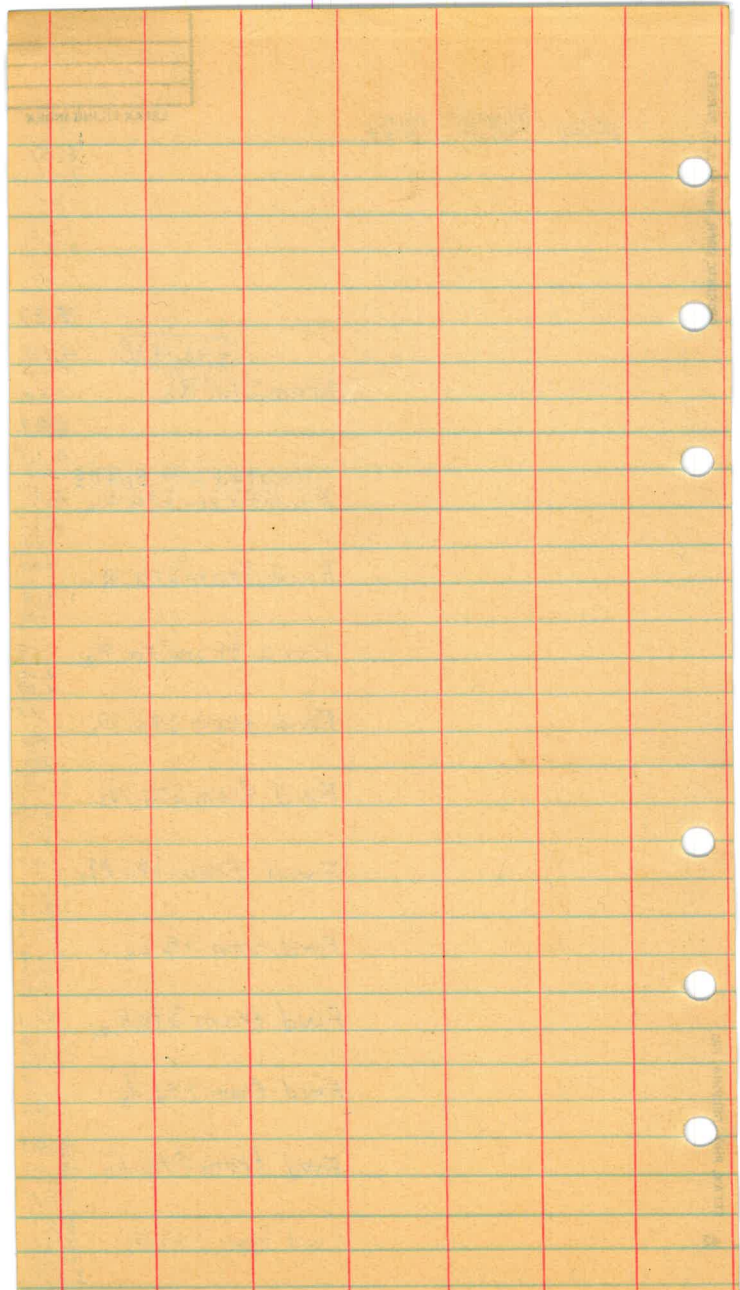
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42

Elev	Slope Dist	Hor. Dist.
------	---------------	---------------

LEFAX FILING INDEX

		6.51
		5.26
		1.95
		5.06
		3.67
		1.43
		5.83
	(290.471)	4.74
From	From Sta. "R <sub>2</sub> "	1.09
		6.42
		4.25
	Located Line 811+115	
	Fwd from Sta R <sub>2</sub>	2.17
		5.35
		3.52
	Fwd. from Sta. Q <sub>2</sub>	1.83
		7.18
		1.82
		2
	Fwd. from Sta. P <sub>2</sub>	3.64
		6.02
		4.37
	Fwd. from Sta. O <sub>2</sub>	1.65
		7.09
		3.22
	Fwd. from Sta. N <sub>2</sub>	3.39
		5.28
		3.19
	Fwd. from Sta M <sub>2</sub>	1.09
		2
		4.18
	Fwd. from Sta. L <sub>2</sub>	5.59
		4.64
		9.2
	Fwd. from Sta. K <sub>2</sub>	5.21
		1.26
		3.93
	Fwd from Sta J <sub>2</sub>	2
		7.86
	Fwd from Sta I <sub>2</sub>	6.43
		4.11
		23.2
	Fwd from Sta H <sub>2</sub>	5.27
		2.66
		2.01
		5.22

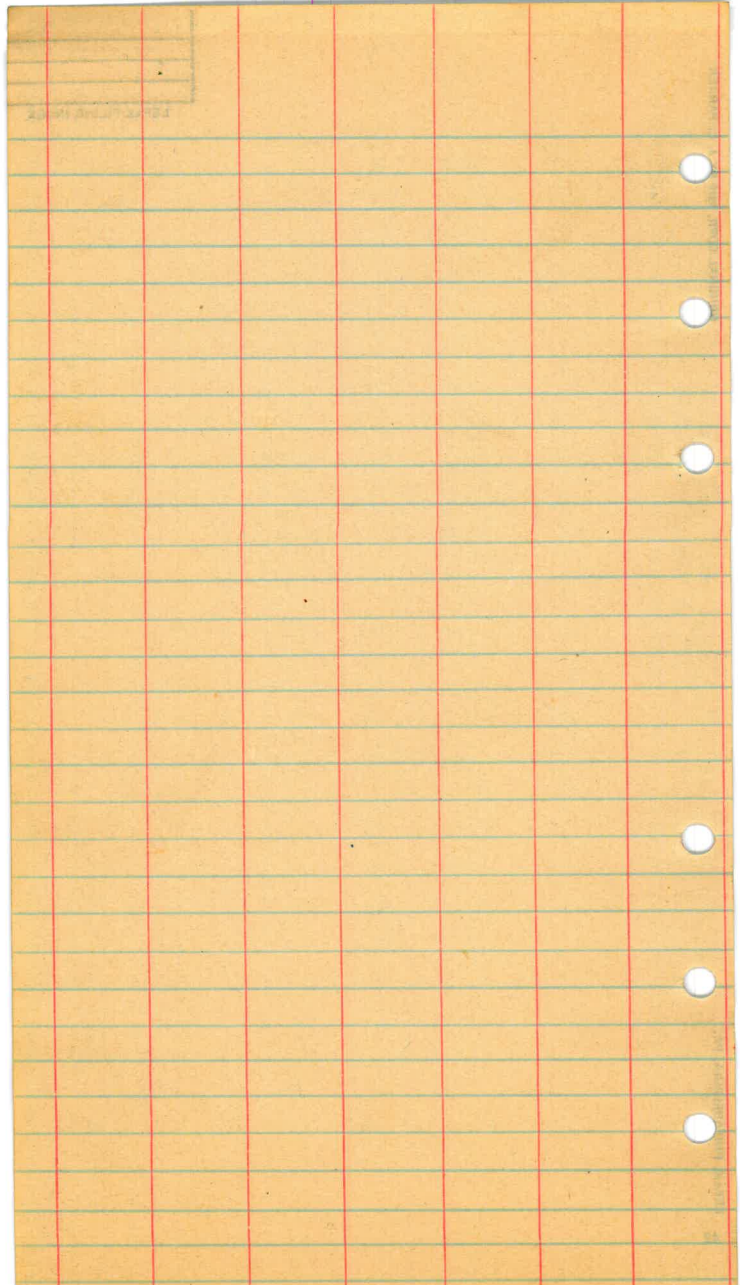




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LEFAX FILING INDEX

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Sta.	Bear Dist	Cos	Sin	N	S	E	W
116132.5	S 88° 32' N	615.0	.11263	.99364	69.27		611.09
122742.3	S 71° 42' N	444.0	.31399	.94943	139.41		421.55
A	N 70° 24' E	447.3	.33516	.94206	152.01	421.45	
B	N 64° 31' E	614.0	.09556	.99542	58.67	611.19	
116132.5					208.68	208.68	1032.64

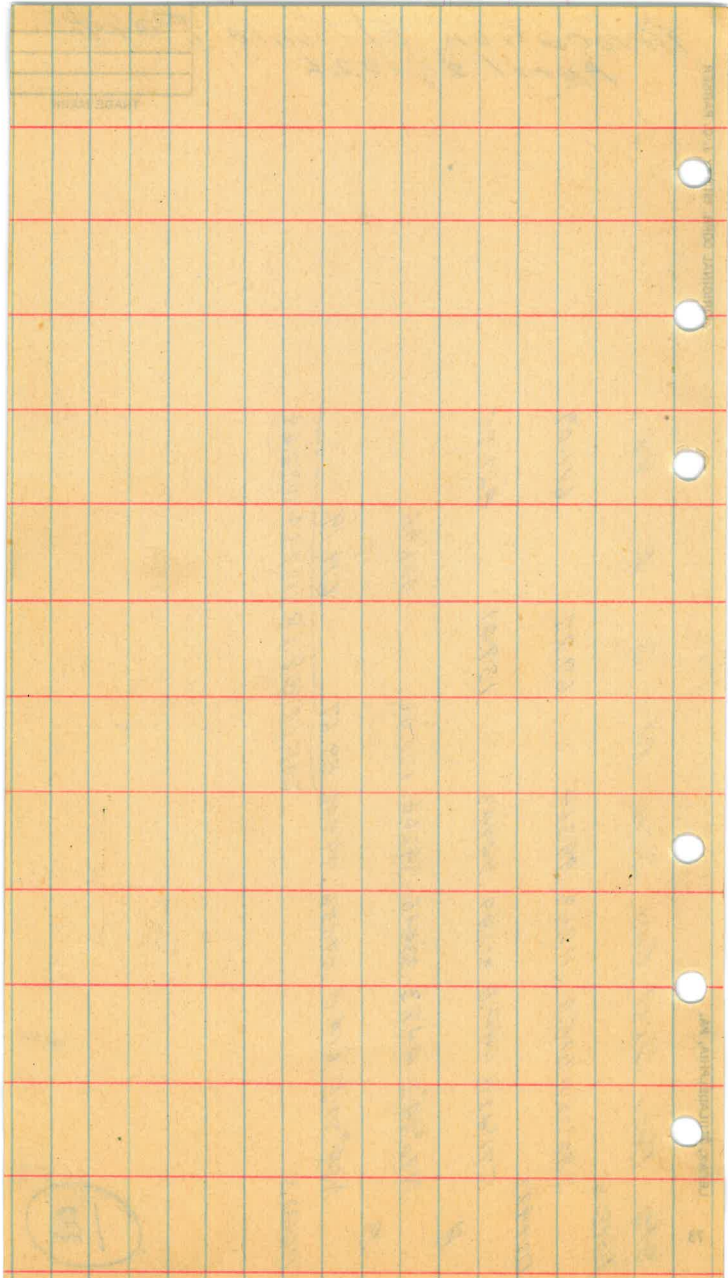
1032.64  
 1032.64  
 1032.64

(10)

Relocation El Monte  
 April 21, 1926

TRADE MARK





①

LEFAX FILING INDEX\*

El Capitan Pipe Line Survey.  
Feb. 1, 1926.

Tie to Bowens Line at  
Sta. 77+968. Equation of  
Bearing and Station to  
Continue along Old Line as  
Figured in Paper Location.

G. W. Converse. Chief of Party.  
Harold Soper Hd. Chain  
W<sup>m</sup> Simpson R. Chain.

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42

①4

79+47<sup>5</sup> B.C.

^

3.8 N. 54° 45' W =  
N. 54° 28' W =

79+43<sup>7</sup> P.O.S.T. = ✓  
79+40<sup>5</sup> E.C.

77+96<sup>8</sup> P.O.S.T.  
78+61<sup>9</sup> P.I. 35° 45' R

E = 13.2  
T = 83.9  
R = 260.44  
D = 22°  
L = 162.5

77+78<sup>0</sup> B.C.

^

150.9

589° 30' W

76+27<sup>1</sup> E.C. ✓



183.7

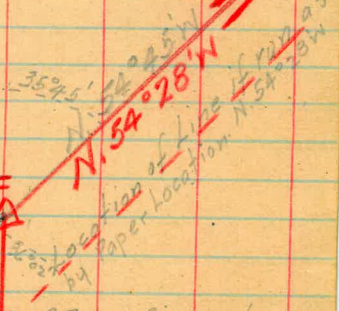
254.6

== Paper Location P.O. ST 79+43.7  
New Location E.C. 79+40.5

Bowens Line P.O. ST 77+96.8  
New Line P.I. 78+61.9

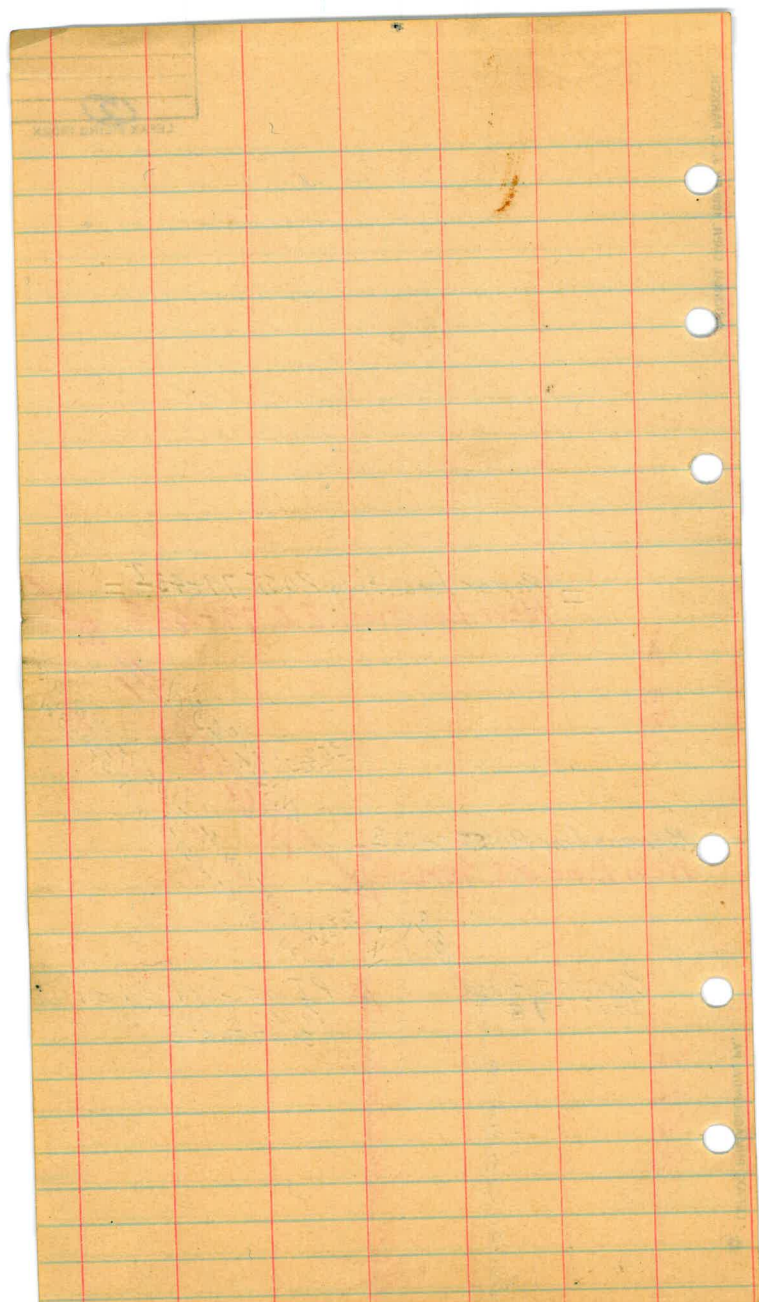
Bowens Hub  
Sta 77+78

P.I. as figured on  
Paper Location  
Sta. 78+47.5



Bowens Line →

New Location



El Capitan Pipe Line Survey.  
March 1-4. 1926.

Notes of Final Location between  
Sta. 392+70<sup>2</sup> and Sta. 480+03<sup>2</sup>  
Showing Ties to Bissells Lakeside  
change at Sta. 44+14<sup>1</sup> and Borens  
Line at his Sta. 431+01<sup>2</sup>.

Also Equation in Stationing between  
Section One and Section Two.

Also change in Angles and  
Equation of Bearing west of  
Lake side at Stations 441+77<sup>2</sup> and  
455+14<sup>2</sup>

G. W. Converse - Chief of Party.  
Harold Soper - Hd. Chain  
Wm Simpson - Rr. Chain.



423+65<sup>3</sup> E.C.

E=10.9  
T=145.0  
R=954.93  
D=6°  
L=287.8

PI 422+22<sup>4</sup> 17°16'R

420+77<sup>1</sup> B.C.

N.70°48'W 602.8

414+74<sup>2</sup> E.C.

E=9.2  
T=73.2  
R=286.48  
D=20°  
L=143.2

PI 414+04<sup>2</sup> 28°39'R

413+31<sup>1</sup> B.C.

N.80°33'W 2061.2

PI 392+70<sup>3</sup> 0°35'L

2134.4

821.0

673.9

New location as run.

Upper location as figured

24" TPC 5' L.H. 422+235  
Sta 422+20

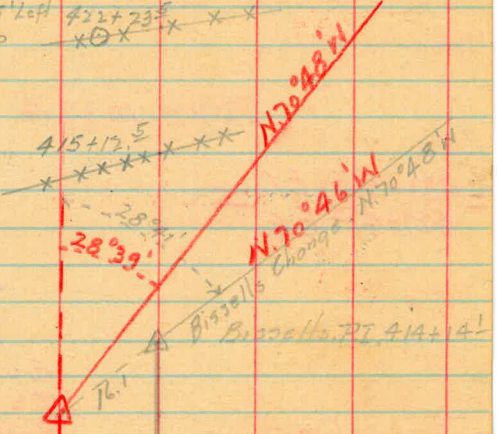
415+12.5  
XXXXXX

28°39'

N.70°46'W

N.70°48'W

Bissells Change  
Bissells RT 414+14'



P.L. 441+77° 0' 51" L.

S. 81° 11' W 1038.4

= 431+38<sup>1/2</sup> E.C. =  
429+47<sup>1/2</sup> E.C. =

Section #1

X

P.L. 428+94<sup>1/2</sup> 45° 17' L.

E = 12.0

T = 59.7

R = 143.24

D = 40°

L = 113.2

Section #2

428+34<sup>1/2</sup> B.C.

N. 53° 32' W 469.2

423+65<sup>1/2</sup> E.C.



1098.1

673.9

E.G.

B.G.

Highway Pavement  
County  
Bovens

X 428+887  
No. Edge Pavement

428+544  
So. Edge Pavement

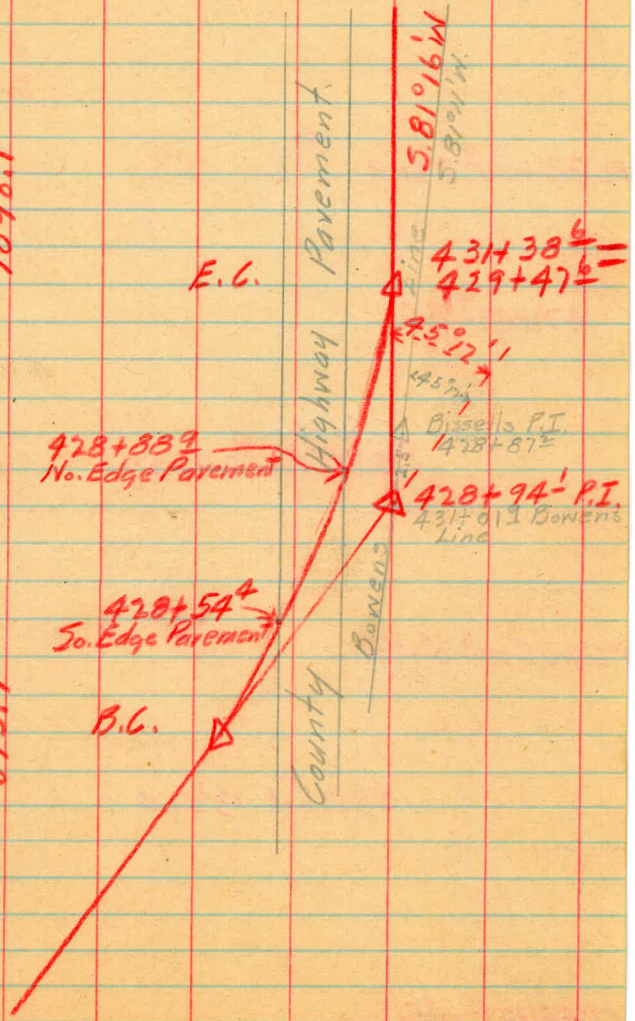
5.81° 16' W  
5.81° 16' W

431+386  
429+476

2.5° 12' 11"

A Bissella P.I.  
428+872

428+941 P.I.  
431+011 Bovens Line



PI 480+03° 83' R.

479+49° B.C.

$5.8058^{\circ} W =$   
 $5.8103^{\circ} W \quad 2435.7$

PI 455+19° 043' R.  
(0° 47' R)

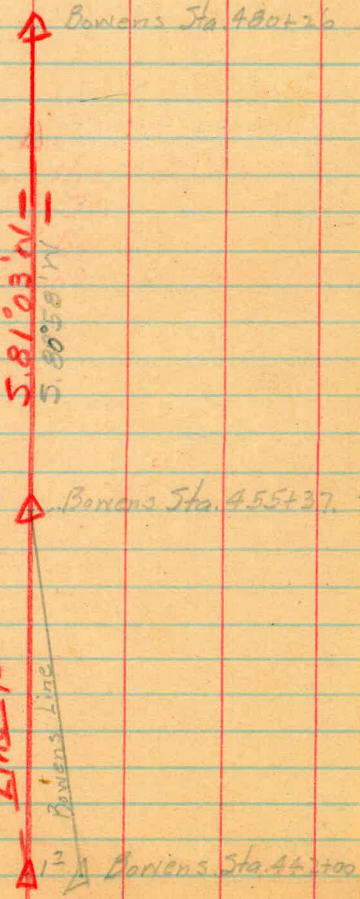
5.8020° W 1337.0

PI 441+77° 0° 51' L.  
(1° 01' L)

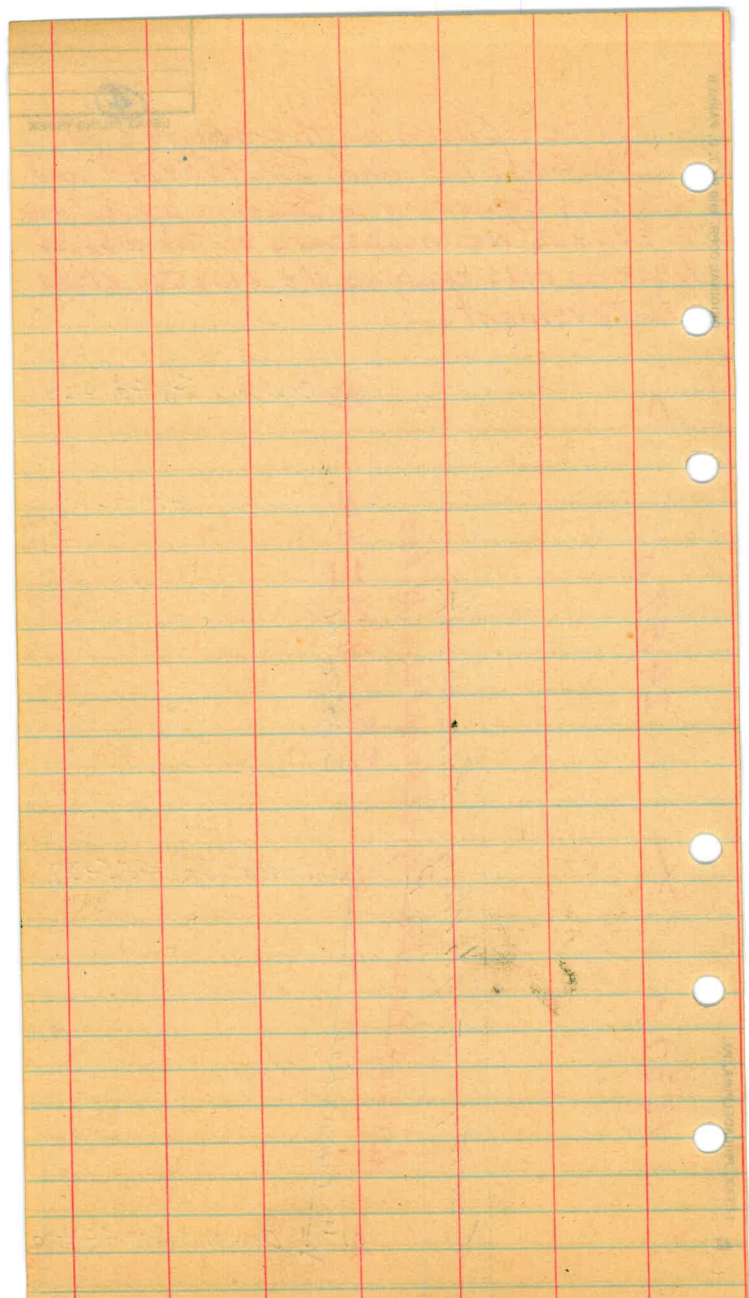
Note - Changing the angles at Sta. 441+77 and Sta. 455+14 and Making Equation in Bearing bet. 455+14 to 480+03 was necessary as the diff. of Bearing was running the Line too close to Pavement.

← 1337.0 X 2489.0 →

County Highway Pavement.  
Line if Run by Paper Location Notes.







B.M.#1 571.460  
Nail in tree  
3' L.1 + 09 ✓

B.M.#2 570.564 Nail in syc-  
tr. 20' R. ~~10+05~~  
20' R 11+50

B.M.#3 570.171 Pt. on Bldr.  
~~40' R. 19+50~~  
23' R 19+95

B.M.#4 568.844 Oak tr. 3' R.  
~~31+65~~  
20' L 32+22

B.M.#5 543.678 Pt. on bldr.  
~~15' R. 40+05~~  
14' R 41+33

B.M.#6 539.618 Nail in Oak  
~~30' R. 32+50~~  
18' R 53+05

B.M.#7 546.027 Nail in Oak  
~~5' L. 60+42~~  
15' L 60+85

B.M.#8 547.161 Pt. of Bldr.  
~~20' R. 69+80~~  
5' L 70+70

B.M.#9 529.904 Nail in Oak  
~~6' L. 76+78~~  
11' L 77+50

B.M.#10 547.366 Nail in Oak  
~~4' L. 84+40~~  
16' L 84+96

B.M.#11 545.997 Leaning tree  
~~2' L. 96+85~~  
15' L 97+40

B.M.#12 548.340 Pt. on rock  
~~2' L. 97+40~~  
15' L 97+92

571.460 B.M.#1  
 Nail in tree  
 3' L.I. + 09 ✓  
 570.564 B.M.#2  
 Nail in eyes -  
 tr. 20' R. 10+05  
 20' R. 11+70  
 570.171 B.M.#3  
 Pt. on Blk.  
~~40' R. 10-50~~  
 23' R. 13+92  
 568.844 B.M.#4  
 Oak tr. 3' R.  
 31-05  
 20' L. 22+22  
 545.378 B.M.#5  
 Pt. on Blk.  
~~25' R. 40-05~~  
 14' R. 41+53  
 538.018 B.M.#6  
 Nail in Oak  
~~30' R. 52-50~~  
 18' R. 53+03  
 546.037 B.M.#7  
 Nail in Oak  
~~31' R. 60+03~~  
 17' R. 60+52  
 547.161 B.M.#8  
 Pt. of Blk.  
~~20' R. 62-90~~  
 21' L. 70+70  
 529.904 B.M.#9  
 Nail in Oak  
~~31' L. 70+78~~  
 11' L. 77+50  
 547.300 B.M.#10  
 Nail in Oak  
~~41' L. 84+40~~  
 16' L. 84+50  
 545.997 B.M.#11  
 Leaning tree  
~~21' R. 90+05~~  
 15' L. 97+40  
 548.340 B.M.#12  
 Pt. on rock  
~~21' L. 97-10~~  
 15' L. 97+31



copy  
BY PER

2

- B.M.#13 520.891 Round peg at ft. of post north of rd. ~~103+80~~ *104+45*
- B.M.#14 574.366 Nail in 12" Oak 20'L. ~~112+78~~ *20'L 113+21*
- B.M.#15 508.445 Power pole 100'L ~~121+00~~ *100'L 121+30*
- ∩ B.M.#16 503.054 Power pole ~~25104~~ *6'L 134+00*
- -B.M.#17 502.184 Oak tree 6' R. ~~137+70~~ *6'R 137+90*
- B.M.#18 509.255 Nail in fence ~~50'L 149+00~~ *130'L 147+45*
- √ B.M.#19 500.758 Cycamore 15'R ~~158+00~~ *15'R 156+00*
- √ B.M.#20 504.635 Oak ~~20'L 167+40~~ *12'L 165+45*
- √ B.M.#21 492.472 Hub in fence 4'R. ~~177+63~~ *4'R 177+50*
- ↓ B.M.#22 491.366 Pole 40'L. ~~183+50~~ *40'L 183+32*
- √ B.M.#23 491.419 Peg on line ~~189+00~~ *8'L 188+80*
- √ B.M.#24 490.912 Nail in pole #73938 30'L. ~~198+10~~ *25'L 197+95*

188-10  
 W3238 30' L.  
 480.912 Nail in pole  
 8' L. 188-80  
 189-00  
 491.412 Peg on line  
 40' L. 185+32  
 491.366 Pole 40' L. 185+50  
 4' R. 177+50  
 4' R. 177-63  
 492.472 Hub in fence  
 12' L. 182+42  
 504.632 Oak 20' L. 187+40  
 12' R. 126+00  
 500.758 Gyasmore 15' R.  
 130' L. 147+42  
 50' L. 149-80  
 509.252 Nail in fence  
 8' R. 137+20  
 137-70  
 502.184 Oak tree 6' R.  
 10' L. 134+30  
 503.024 Power pole 2104  
 109' L. 121+30  
 181-00  
 508.442 Power pole 100' L.  
 20' L. 112+78  
 20' L. 112+78  
 574.366 Nail in 12" Oak  
 104+42  
 of rd. 103+80  
 of post north  
 520.891 Round peg at ft.  
 B.M.#13  
 B.M.#14  
 B.M.#15  
 B.M.#16  
 B.M.#17  
 B.M.#18  
 B.M.#19  
 B.M.#20  
 B.M.#21  
 B.M.#22  
 B.M.#23  
 B.M.#24

- ✓ B.M.#25 486.282 Nail in tel.pole  
30' L. 205+00
- ✓ B.M.#26 484.342 Nail in power pole #73929  
30' L. 212+65  
30' L 203+82
- ✓ B.M.#27 480.800 Oak 15' L 231+40  
30' L 211+25
- ✓ B.M.#28 486.482 Corner fence post  
55' L. 226+60  
20' L 219+60
- ↓ B.M.#29 485.125 Hub on pole 5' R  
237+10  
65' L 225+30
- ✓ B.M.#30 465.854 Nail in post 2' R  
5' R 235+55  
247+40
- ✓ B.M.#31 461.347 Nail in fence  
3' L 245+60  
20' R. of gate  
253+75
- ↓ B.M.#32 463.134 Nail in sycamore  
20' R 251+95  
40' R. 262+00
- ✓ B.M.#33 455.815 Syca.tree 15' L.  
48' R 260+10  
275+65
- ✓ B.M.#34 446.620 Nail in 12" cott-  
onwood 80' R.  
20' L 275+65  
80' R 286+70
- B.M.#35 448.876 Nail in sycamore  
25' R. 298+00  
80' R 286+65
- ~~B.M.#36 446.101 Power pole #~~  
25' R 297+90



B.M.#26 446.101 Power pole #  
 25' R. 297+30  
 B.M.#25 448.876 Nail in sycamore  
 25' R. 298-00  
 288-70  
 onwood 80' R.  
 B.M.#24 446.620 Nail in 12" cut-  
 20' L. 297-57  
 B.M.#23 455.818 Syc. tree 15' L.  
 48' R. 280+10  
 40' R. 282-00  
 B.M.#22 463.134 Nail in sycamore  
 25' R. 281-72  
 B.M.#21 461.347 Nail in fence  
 20' R. of gate  
 283-78  
 B.M.#20 468.854 Nail in post 2' R.  
 247-40  
 2' R. 282+22  
 B.M.#19 488.128 Hub on pole 5' R.  
 237-19  
 27' L. 282+30  
 25' L. 282-30  
 488.482 Corner fence post  
 20' L. 219+00  
 480.800 Oak 15' L. 281-40  
 20' L. 211+27  
 B.M.#18 484.342 Nail in power  
 pole #73829  
 30' L. 212-82  
 B.M.#17 486.282 Nail in tel. pole  
 30' L. 202-00  
 20' L. 203+22

B.M.#36

446.101 Power pole 72749  
10' L 302+00

B.M.#37

12' L 301+90

443.824 Syca.tr. 30'R. 303+00

B.M.#38

30'R 302+90

U.S.G.S. Conc. Hub at  
Pump Sta.

B.M.#39

316+60

441.278 Nail in Guy pole

40' R. 335+10

B.M.#40

5' R 334+95

450.117 On pole #74387

338+25

B.M.#41

338+18

466.272 Pole #74389 3'R.

38' L 351+16

B.M.#42

351+08

458.035 Nail in tel. pole

#025099 30'R.

363+00 20'R

B.M.#43

362+50

432.996 Hub nailed on

Eucy.tr. 6' L 12' L

378+45

377+95

B.M.#44

403.777 Nail in root of

stump 393+10

392+60

B.M.#45

430.396 Nail Guy pole

28'R 400+80

B.M.#46

24'R 400+10

421.954 Hub nailed to

fence post 30'R

408+45

407+96

468-45  
 481.924 Hub nailed to  
 fence post 30'R  
 27'R 400'10  
 28'R 400-60  
 430.398 Nail Guy pole  
 B.M.#45  
 403.777 Nail in roof of  
 stump 303-10  
 317-92  
 378-45  
 432.998 Hub nailed on  
 Encl. tr. 0'2'11"  
 B.M.#43  
 362-50 20'R  
 #025099 30'R.  
 458.025 Nail in tel. pole  
 321-98  
 301-251-16  
 466.278 Pole #74389 3'R.  
 338-18  
 338-25  
 450.117 On pole #74387  
 2 R 334-92  
 401.278 Nail in Guy pole  
 401 R. 333-10  
 314-60  
 B.M.#39  
 U.S.G.S. Bench. Hub at  
 Pump Sta.  
 301 R 302-90  
 443.824 Vec. tr. 30'R. 302-00  
 12' L 301-90  
 10' L 302-00  
 446.101 Power pole 78748  
 B.M.#36



B.M.#47

417.160 No.11 in Power  
pole #25773 ~~2<sup>L</sup>~~  
*4'R 415+92*  
*415+08*

B.M.#48

407.212 Nail in pole  
#25780 ~~5<sup>L</sup>~~ *115'A*  
*423+40*  
*421+67*

B.M.#49

400.256 Co.B.M. on tree  
~~6'R 436+12~~  
*435+85*

B.M.#50

393.949 Co.B.M.Pole 72479  
~~20'R 449+70~~

B.M.#51

*449+45*  
393.440 Pole #72476 40'L  
~~457+50~~  
*457+27*

B.M.#52

383.857 Pole #72947,  
~~474+30~~  
*474+04*

B.M.#53

381.717 Co.B.M.Pole 72468  
~~40'L 480+40~~  
*480+15*

B.M.#54

379.508 Pole #24982 ~~2<sup>R</sup>~~  
*9'L 496+01*  
*495+82*

B.M.#55

374.021 End of Ry.switch  
~~50'R. 506+25~~  
*35'R 506+08*

B.M.#56

376.461 Pole #72413 ~~4<sup>L</sup>~~  
*509+75 18 L*  
*509+57*

B.M.#57

365.510 Pole #72410 Co.BM  
~~10'R 515+05~~  
*514+90*

B.M.#47  
 417.180 No. 11 in Power  
 pole #23778 2' 1/2  
 418-92  
 412-08

B.M.#48  
 407.212 Nail in pole  
 #25780 5' 1/2  
 423-40  
 421-27

B.M.#49  
 400.256 Co. B.M. on tree  
 6' R 426-18  
 427-82

B.M.#50  
 383.949 Co. B.M. Pole 72479  
 20' R 446-70  
 441-42

B.M.#51  
 383.440 Pole #72478 40' L  
 427-20  
 427-27

B.M.#52  
 383.827 Pole #72947  
 474-30  
 474-27

B.M.#53  
 381.717 Co. B.M. Pole 72468  
 40' L 488-40  
 480-12

B.M.#54  
 379.508 Pole #24982 2' R  
 47 488-01  
 492-81

B.M.#55  
 374.021 End of Ry. switch  
 20' R. 202-22  
 23' R. 202-08

B.M.#56  
 376.461 Pole #72413 4' L  
 202-4212  
 209-427

B.M.#57  
 362.610 Pole #72410 Co. B.M.  
 10' R 618-08  
 618-10

6

B.M.#58 366.203 Concrete pillar  
70'L. ~~521+00~~  
*520+85*

B.M.#59 362.585 <sup>B</sup> Culvert N.E.  
post 20'R  
~~537+45~~  
*537+30*

B.M.#60 361.779 15'R ~~545+00~~  
*544+85*

B.M.#61 369.032 Co.B.M.#pole #  
72384 15'R  
~~556+42~~  
*556+28*

B.M.#62 365.762 Pole #72379  
Co.B.M.#12, 10'R  
~~571+50~~  
*571+33*

B.M.#63 365.369 Co.B.M.Pole#  
72376 15'R  
~~580+50~~  
*580+33*

B.M.#64 369.682 Co.B.M.#11 tree  
at fork or road  
to El Cajon opp.  
~~589+00, 100'L~~  
*588+85, 107'L*

B.M.#65 364.525 Nail on pole  
50'L ~~595+85~~  
*595+45*

B.M.#66 354.749 8'R Pole#23530  
~~606+35~~  
*605+98*

B.M.#67 343.593 Pole #72289 40'L  
~~617+70~~  
*617+32*



B.M.#67 243.893 Pole #72289 40' L  
 617-70  
 B.M.#68 354.749 8' R Pole #23530  
 606-25  
 B.M.#65 354.222 Nail on pole  
 50' L 592-88  
 B.M.#64 359.682 Co. B.M. #11 tree  
 at fork on road  
 to El Cajon opp.  
 389-00 100' L  
 B.M.#63 385.369 Co. B.M. Pole #  
 72376 15' R  
 580-50  
 B.M.#62 368.762 Pole #72379  
 Co. B.M. #12 10' R  
 571-50  
 B.M.#61 361.779 15' R 545-60  
 B.M.#59 362.585 Driver N.L.  
 Post 20' R  
 557-45  
 B.M.#58 366.202 Concrete pillar  
 70' L 521-00  
 517-24

7

B.M.#68 342.432 Pole #72292 40'L  
~~626+7~~  
625+70

B.M.#69 339.393 Pole #72295 40'L  
635+85

B.M.#70 336.827 Pole #72297 40'L  
635+25  
~~641+00~~

B.M.#71 335.677 Pole #23566 8'R  
640+60  
650+12

B.M.#72 335.392 Pole 50'L 659+00  
649+72

B.M.#73 327.201 Pole #75591 50'L  
658+60  
675+40

B.M.#74 325.277 Pole 23594 3'R  
675+00  
~~694+06~~

B.M.#75 326.761 Nail pepper tree  
683+68  
50'L 694+00

B.M.#76 325.363 Hub in fence 50'L  
45'L 693+60  
~~705+60~~ 714+70

B.M.#77 318.821 Hub 60'L fence  
705+18  
post 715+50

B.M.#78 317.530 Nail in tree 30'L  
715+05  
~~725+30~~

B.M.#79 310.545 On post 8'R  
724+85  
736+50  
736+00

B.M.#68  
 342.432 Pole #72222 40'L  
 626-7  
 625+70  
 B.M.#69  
 339.393 Pole #72222 40'L  
 625-82  
 626+22  
 B.M.#70  
 336.827 Pole #72227 40'L  
 641-00  
 640+00  
 B.M.#71  
 332.677 Pole #22222 8'R  
 620-12  
 647+72  
 B.M.#72  
 332.392 Pole 50'L 620-00  
 628+00  
 B.M.#73  
 327.201 Pole #72221 50'L  
 675-40  
 675+00  
 B.M.#74  
 322.277 Pole 22224 3'R  
 624+02  
 622+02  
 B.M.#75  
 322.761 Nail pepper tree  
 50'L 624-00  
 622+00  
 B.M.#76  
 322.362 Hub in fence 50'L  
 714-70  
 702+12  
 B.M.#77  
 318.821 Hub 60'L fence  
 post 712-20  
 712+02  
 B.M.#78  
 317.220 Nail in tree 30'L  
 722-30  
 712+02  
 B.M.#79  
 310.242 On post 8'R  
 726+20  
 726+00



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B.M.#80 390  
306.229 40'L ~~749+75~~  
749+23

B.M.#81 317.570 Hub on fence  
10'R ~~761+00~~  
760+47

B.M.#82 334.131 Lathe on fence  
post 10'R ~~770+38~~  
769+88

B.M.#83 341.613 Hub nailed to  
fence post 10'R  
780+86  
780+38

B.M.#84 352.910 Hub nailed to  
fence post 8'R  
~~789+79~~  
789+35

B.M.#85 332.255 Eucy. tree 50'L  
~~800+70~~  
800+70

B.M.#86 308.236 Nail in post 30'  
L. ~~810+85~~  
100'L 808+90

B.M.#87 290.471 Hub nailed in  
fence post 30'R  
~~815+90~~  
49'R 813+90

B.M.#88 309.431 Hub nailed to  
post 3'L.  
~~824+40~~  
5'L 822+40

B.M.#89 308.179 Nail in post 2'L  
~~825+88~~  
823+88

B.M.#80 308.229 40' L 749-75  
 B.M.#81 317.570 Hub on fence  
 10' R 761-00  
 B.M.#82 334.131 Lath on fence  
 post 10' R 770-38  
 B.M.#83 341.613 Hub nailed to  
 fence post 10' R  
 780-86  
 B.M.#84 352.910 Hub nailed to  
 fence post 8' R  
 789-79  
 B.M.#85 332.255 Ency. tree 50' L  
 800-70  
 B.M.#86 308.236 Nail in post 30'  
 L. 810-82  
 B.M.#87 320.471 Hub nailed in  
 fence post 30' R  
 818-90  
 B.M.#88 309.431 Hub nailed to  
 post 3' L.  
 824-40  
 B.M.#89 308.179 Nail in post 2' L  
 828-88

9

B.M.#90 319.505 Nail in post ~~2'L~~  
*1'L 836+00*  
*836+00*

B.M.#91 300.649 ~~Paxxonline~~  
Pt. on boulder  
~~on line 846+10~~  
*2'L 846+05*

B.M.#92 285.202 Pt. of rock 1'L  
~~851+98~~  
*851+98*

B.M.#93 257.942 High pt. of bldr  
20' R. ~~863+80~~  
*863+70*

B.M.#94 272.341 Nail in oak tr.  
8' R. ~~869+75~~  
*869+60*

B.M.#95 258.435 On bldr. 15'L.  
~~877+28~~  
*13'L 877+12*

B.M.#96 251.567 On pt. of bldr.  
30' R. ~~889+52~~  
*889+28*

B.M.#97 255.816 On oak tr. 20'R  
~~897+75~~  
*897+78*

B.M.#98 251.627 Spot on boulder  
~~48~~ 4' from road  
culvert ~~903+30~~  
*903+07*

B.M.#99 257.478 Pt. of bldr.  
37'L ~~902+88~~  
*902+65*

(Note: 99 replaces 98  
98)



(Note: 99 replaces

37' L 902-88  
Pt. of bldr.

B.M.#99

Spot on boulder  
4' from road  
elevator 903-30

B.M.#98

251.816 On oak tr. 30' R  
897-75

B.M.#97

251.567 On pt. of bldr.  
30' R. 899-52

B.M.#96

258.435 On bldr. 15' L.  
877-29

B.M.#95

278.361 Nail in oak tr.  
8' R. 899-75

B.M.#94

257.948 Right pt. of bldr.  
20' R. 893-80

B.M.#93

285.202 Pt. of rock 1' L  
851-98

B.M.#92

on line 846-10

Pt. on boulder  
300.649 Paganxixina

B.M.#91

319.505 Nail in post 2' L  
836-00

B.M.#90

10

B.M.#100	269.660	Pt. of boulder 50' L <del>905+50</del>
B.M.#101	298.182	Top of hub <del>908+00</del> <i>905+27</i>
B.M.#102	292.651	Pt. of boulder 10' L <del>912+90</del> <i>907+77</i>
B.M.#103	313.849	Lathe driven by Sumac bush 18' R <del>918+70</del> <i>912+67</i>
B.M.#104	323.414	Lathe driven beside rock 60' L <del>924+00</del> <i>918+47</i>
B.M.#105	297.268	Small pt. of stone 35' R. <del>930+70</del> <i>923+77</i>
B.M.#106	301.670	Lathe driven in ground 2' R <del>938+85</del> <i>20' R 930+30</i>
B.M.#107	309.132	Hub <del>938+40</del> <del>Lathe 15' R</del> <i>16' R 942+25</i>
B.M.#108	308.678	Hub 20' R. <del>953+00</del> <i>15' R 941+75</i>
B.M.#109	340.341	Lathe driven 25' L <del>956+40</del> <i>952+38</i>
B.M.#110	383.670	Hub in ground <del>959+85</del> <i>955+75</i> <i>959+20</i>

959-82	Hip in ground	383.670	B.M.#110
953-40	25' L lathe driven	340.341	B.M.#109
953-00	Hip 20' R.	308.678	B.M.#108
943-25	Latina 15' R Hip	309.132	B.M.#107
938-85	Ground 2' R Lathe driven in	301.670	B.M.#106
930-70	stone 25' R. Small pt. of	297.268	B.M.#105
924-00	80' L beside rock Lathe driven	323.414	B.M.#104
913-70	Sumac bush 18' R Lathe driven by	313.849	B.M.#103
912-30	10' L Pt. of boulder	292.621	B.M.#102
908-00	Top of hip	298.182	B.M.#101
903-50	50' L Pt. of boulder	299.660	B.M.#100



- B.M.#111 395.111 Hub 18' R 962+60
- B.M.#112 376.936 Pt. on boulder  
18' L 968+00  
*19' R 964+85*
- B.M.#113 371.562 Hub 10' L 974+00  
*967+31*
- B.M.#114 333.390 Hub 10' L. 984+00  
*9' L 973+28*
- B.M.#115 "A" Line 218.543 P.I.Hub 15+056  
*27' L 983+33*  
Bissell's List  
*48' Left 996+93*
- B.M.#116 335.974 P.I.Hub 25+55  
*22' R 1007+40*
- B.M.#117 ~~32~~ 354.037 Hub 30' L 45+55
- B.M.#118 329.807 Hub 30' R 55+00  
*1027+35*
- B.M.#119 336.381 Hub 20' L 66 B  
*1036+80*
- B.M.#120 326.652 Hub 20' L 87+55  
*1047+80*
- B.M.#121 268.017 Hub 20' L 98+10  
*1069+34*
- B.M.#122 202.655 Rock 30' R.  
~~100+20~~  
*1079+90*
- B.M.#123 149.817 Hub 30' L 102+80  
*1082+00*
- B.M.#124 89.144 Syc.tr. 122+00  
*1084+60*
- B.M.#125 104.781 Nail in 8" tr.  
1' L. 128+97  
*1103+65*  
*1109+65*

104.781 B.M.#125  
 J. I. 128+24 Well in 8" tr.  
 89.144 B.M.#124  
 Syc. tr. 122+00  
 149.817 B.M.#123  
 Hrb 30' L 102+80  
 302.655 B.M.#122  
 Rock 30' R. 100+20  
 268.017 B.M.#121  
 Hrb 30' L 98+10  
 326.652 B.M.#120  
 Hrb 30' L 87+52  
 336.381 B.M.#119  
 Hrb 30' L 66 B  
 329.807 B.M.#118  
 Hrb 30' R 55+00  
 322.384.027 B.M.#117  
 Hrb 30' L 43+52  
 325.974 B.M.#116  
 P. I. Hrb 22+52  
 218.643 B.M.#115  
 P. I. Hrb 15+02  
"A" Line  
 323.390 B.M.#114  
 Hrb 16' L. 984+00  
 371.562 B.M.#113  
 Hrb 10' L 974+00  
 376.926 B.M.#112  
 18' L 968+00  
 376.926 Pt. on postiger  
 392.111 B.M.#111  
 Hrb 18' R 962+80  
 B.M.#111

ORIGINAL COPY, 1910 BY J. C. PARKER

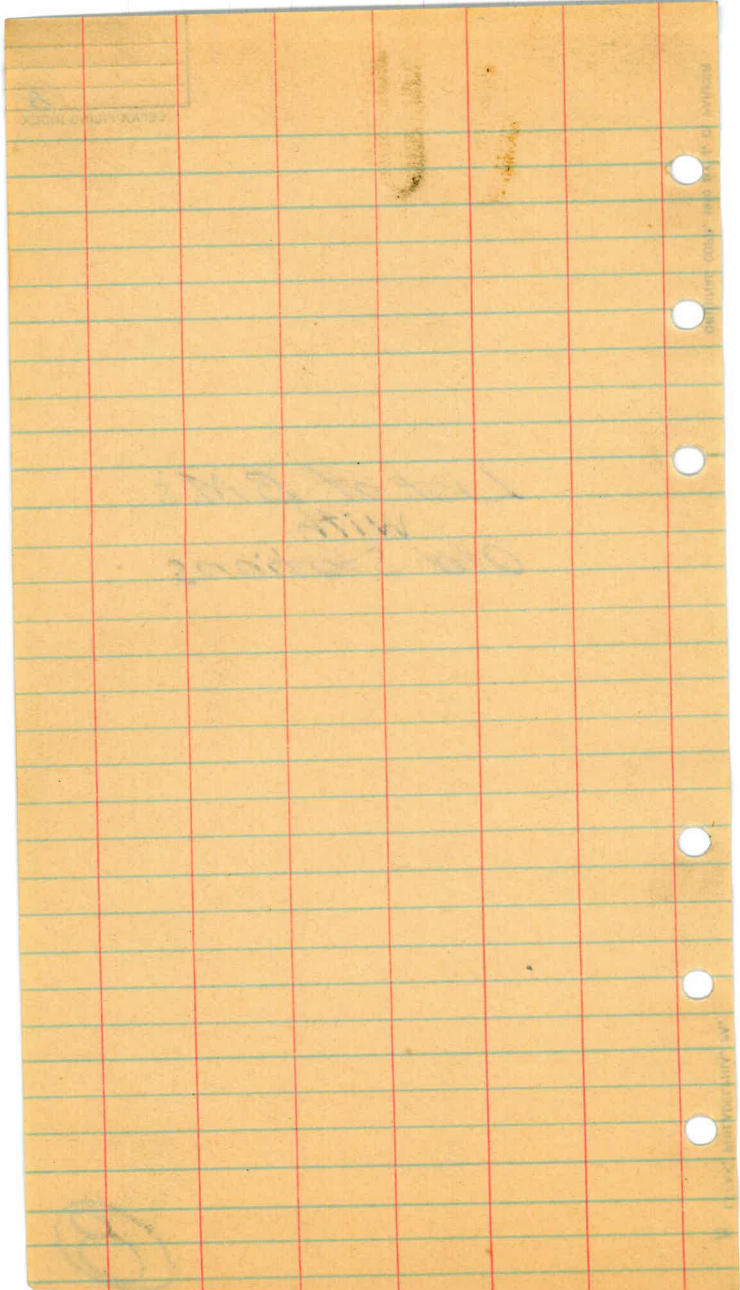
LEFAX FILING INDEX 8

List of B.M.'s  
With  
Old Stations

LEFAX, PHILADELPHIA, PA.  
42

8





Small rectangular stamp or marking in the top left corner, containing illegible text.

Dark smudges or markings near the top center of the page.

Vertical text along the right edge of the paper, possibly a page number or reference code, which is mostly illegible due to the paper's age and the binding holes.

Line Change

$$492+68^1 \text{ to } 504+30^2 (=504+338)$$

June 2, 1926 (McCarty)

= 504+33<sup>2</sup>  
504+30<sup>2</sup> E.C.

503+04<sup>2</sup> 20°19' L

E=11.4  
T=128.33  
R=716.20  
D=8°00'  
L=253.96

501+76<sup>2</sup> B.C.

495+44<sup>2</sup> P.O.T.

576°26' W

494+84<sup>2</sup> E.C.

E=6.2  
T=108.80  
R=954.93  
D=6°00'  
L=216.67

493+76<sup>2</sup> 13°00' L

492+68<sup>2</sup> B.C.

589°26' W

487+00 P.O.T.



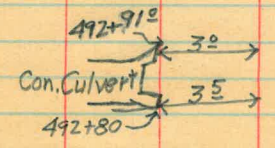
ORIGINAL COPY, 1910 BY J. C. PARKER

Δ 13° Δ 15° Δ

Δ 39° Δ 16° Δ

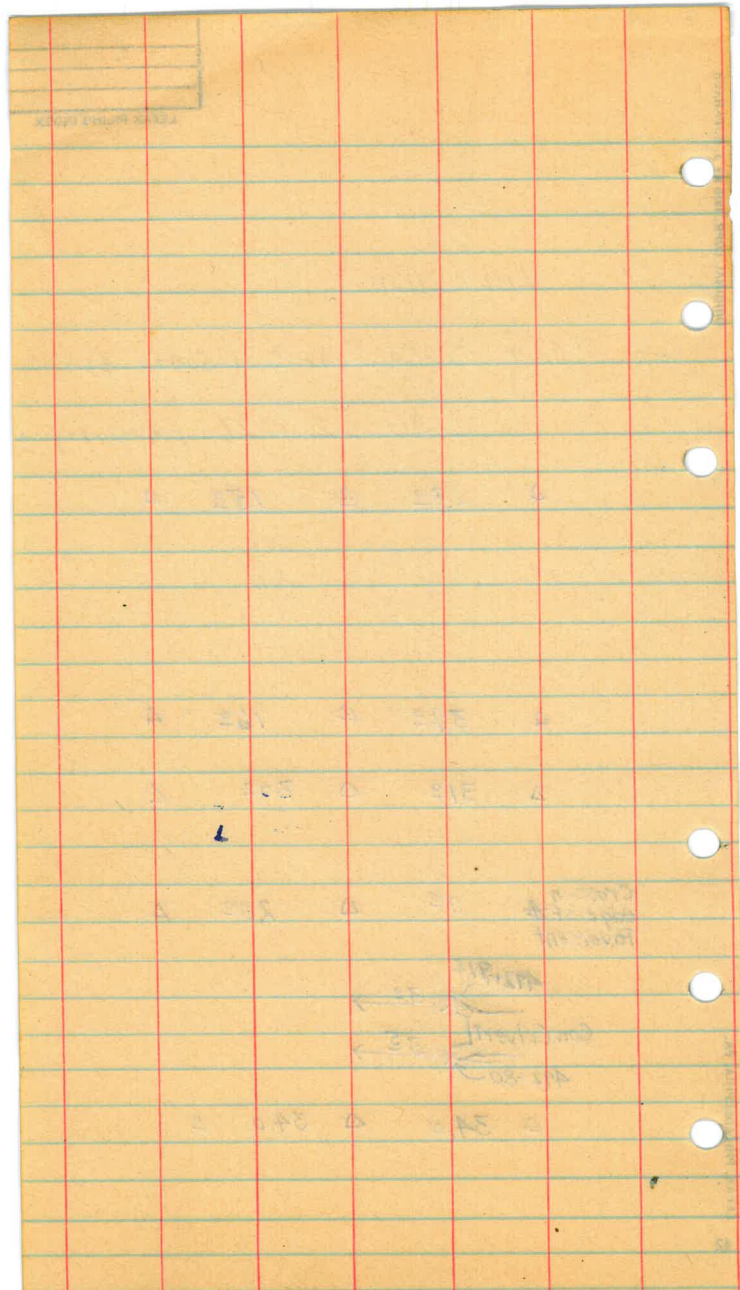
Δ 31° Δ 30° Δ

Cross in edge of Pavement 11° Δ 20° Δ



Δ 34.0 Δ 34.0 Δ

LEFAX, PHILADELPHIA, PA.



Topog.

LEFAX FILING INDEX

492+68<sup>1</sup> Pavement 10<sup>o</sup> L  
492+80 Guy pole 4<sup>o</sup> R  
492+98 Tel. pole 7<sup>o</sup> R  
494+84<sup>8</sup> Pavement 11<sup>o</sup> L  
495+51 Guy pole 1<sup>o</sup> R  
495+75 Tel. pole 1<sup>5</sup> R  
497+00 Tel. pole 5<sup>o</sup> R  
" " Pavement 12<sup>5</sup> L  
497+35 Con. Culvert 6<sup>5</sup> L  
498+39 Tel. pole 5<sup>5</sup> R  
" " Pavement 15<sup>5</sup> L  
499+89 Tel. pole 9<sup>9</sup> R  
501+02 Guy pole 5<sup>o</sup> L  
" " Pavement 15<sup>7</sup> L  
501+20<sup>5</sup> Tel. pole 12<sup>5</sup> R  
501+76<sup>3</sup> Pavement 16<sup>8</sup> L  
502+09 Tel. pole 15<sup>o</sup> R  
502+26<sup>3</sup> Pavement 19<sup>o</sup> L

ORIGINAL CORR. 1010 BY J. C. PARKER

LEFAX, PHILADELPHIA, PA.



Tape

REARFLING BOOK

492+66 Pavement 12 L  
 492+80 Guy pole 4 R  
 492+78 Tel pole 7 R  
 494+84 Pavement 11 L  
 492+51 Guy pole 1 R  
 492+75 Tel pole 1 R  
 491+00 Tel pole 5 R  
 " " Pavement 12 L  
 497+55 Con Culvert 6 L  
 498+37 Tel pole 2 R  
 " " Pavement 12 L  
 499+87 Tel pole 9 R  
 501+02 Guy pole 2 L  
 " " Pavement 12 L  
 501+30 Tel pole 1 R  
 501+75 Pavement 12 L  
 502+07 Tel pole 1 R  
 502+24 Pavement 12 L

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El Capitan Pipe Line Survey.  
March 5, 1926.

Tie to Borens Line at Santee.

G. W. Converse - Chief of Party.  
Harold Soper. Hd. Chain  
W<sup>m</sup> Simpson Rr. Chain.

16

590+62<sup>2</sup> P.I.

589+70<sup>2</sup> B.C.

N. 57° 57' W 12.7

589+78<sup>2</sup> P.O. ST =

589+79<sup>2</sup> E.C.

PL 589+24<sup>1</sup> 75° 30' R

588+44<sup>2</sup> B.C.

S 46° 33' W 5689.9

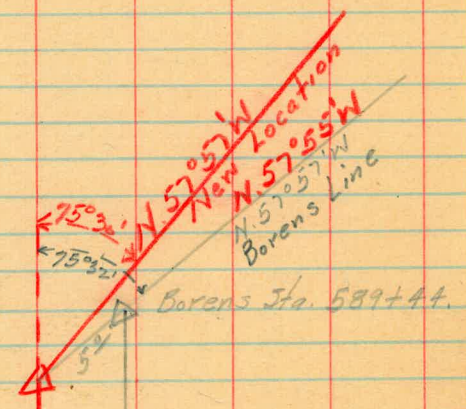
531+55<sup>2</sup> P.I.

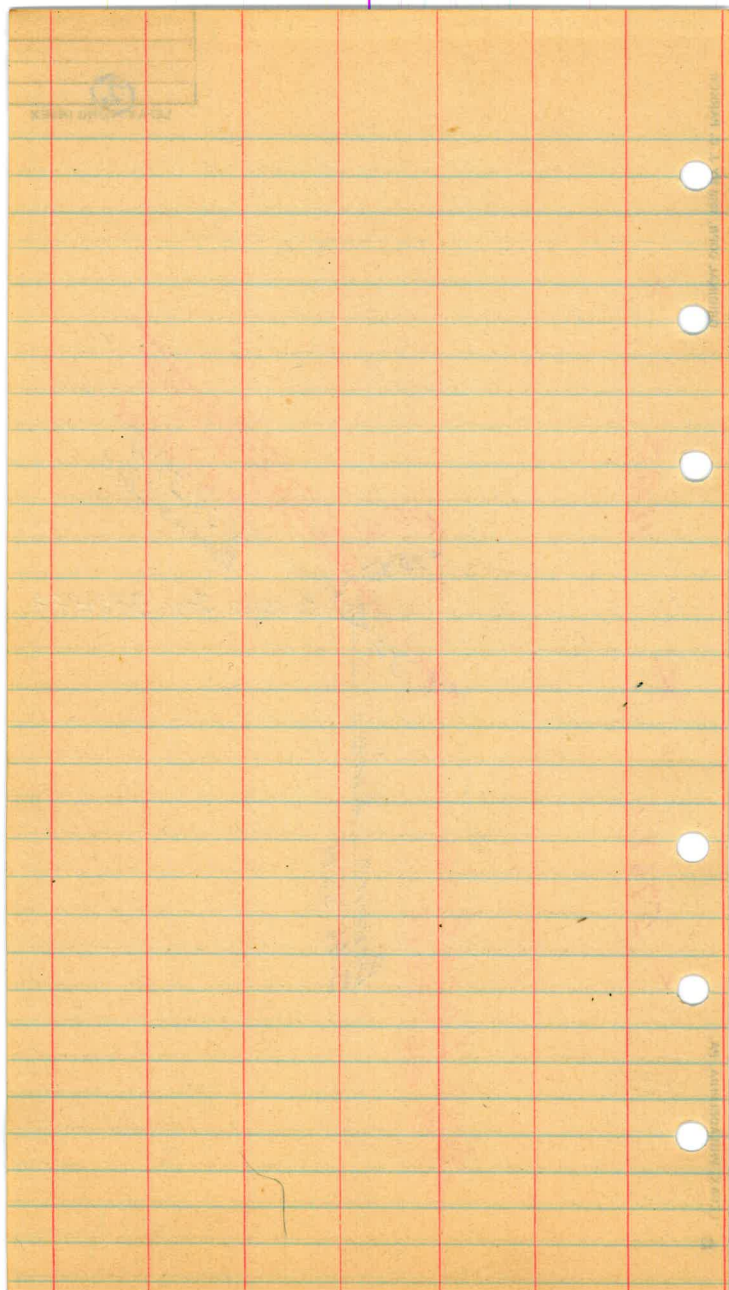


5769.1 X 164°

New Location  
S. 46° 33' N

Borens Line  
S. 46° 33' N





El Capitan Pipe Line Survey  
March 9. 1926.

Line Change from Station  
674+00 to Station 684+00 to  
miss downstream Wing Walls  
of County Highway Bridge.

Mr. T. A. Mills.

G. W. Converse - Chief of Party.

H. C. McCarty - Inst.

H. Soper Hd. Chain.

Wm Simpson R. Chain.



693+24<sup>2</sup> P.I.

692+22<sup>2</sup> B.C.

5.89°43'W 822.3

PI. 684+00 =  
PI. 684+00 = 0°57'R.

5.88°46'W 305.3

PI. 680+95 1°22'L.

11.89°52'W 695.0

PI. 674+00 0°25'R

5.89°43'W 2843.8

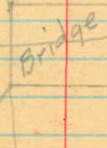
645+56<sup>2</sup> P.I.

← 2043.8 X 695<sup>0</sup>

305.3

X 924.2 →

Downstream  
King Mills of  
Bridge.



County

Highway

△ 645+56<sup>2</sup>

△ 674+00 P.I =  
674+00 P.O.T.

← ○ Tel. Pole.  
4<sup>5</sup>

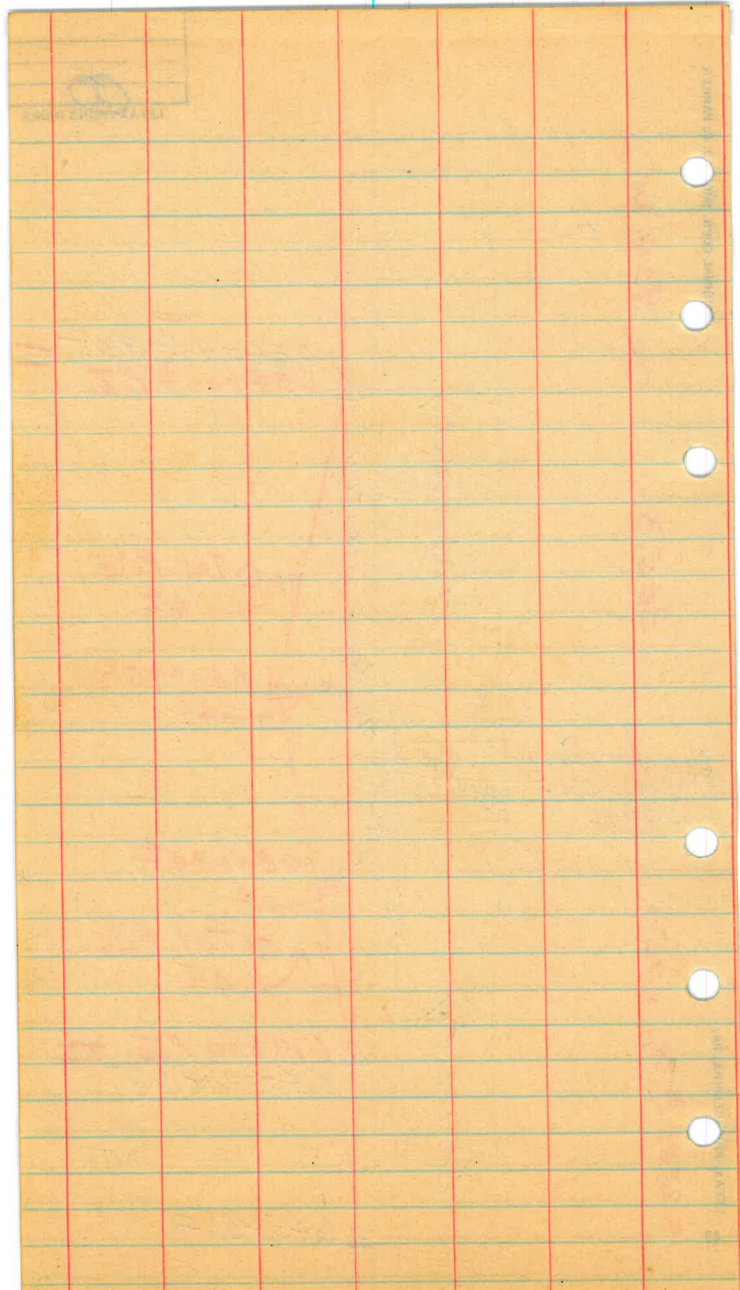
← 680+34<sup>4</sup>  
2<sup>5</sup>

← △ 680+95<sup>0</sup>  
4<sup>1</sup>

← ○ Tel. Pole  
4<sup>4</sup>

△ 684+00<sup>0</sup> P.O.T. =  
684+00<sup>0</sup> P.I. =

Paper Location





①  
LEFAX FILING INDEX  
El Capitan Pipe Line Survey.  
March. 9. 1926.

Line Change at Sta. 724+00  
To miss 18" Culvert at Sta.  
730+07.

G. W. Converse - Chief-of-Party.  
H. G. Mc Carty. Inst.  
H. Soper. Hd. Chain.  
W<sup>m</sup> Simpson Rr. Chain.

N86°0'W

P.I 731+26<sup>±</sup> 10°12'R

T=127.8

729+98<sup>±</sup> B.C.

5.83°48'W 198.7

P.I 728+00 1°15'L

5.85°03'W 400.0

P.I 724+00 1°15'R

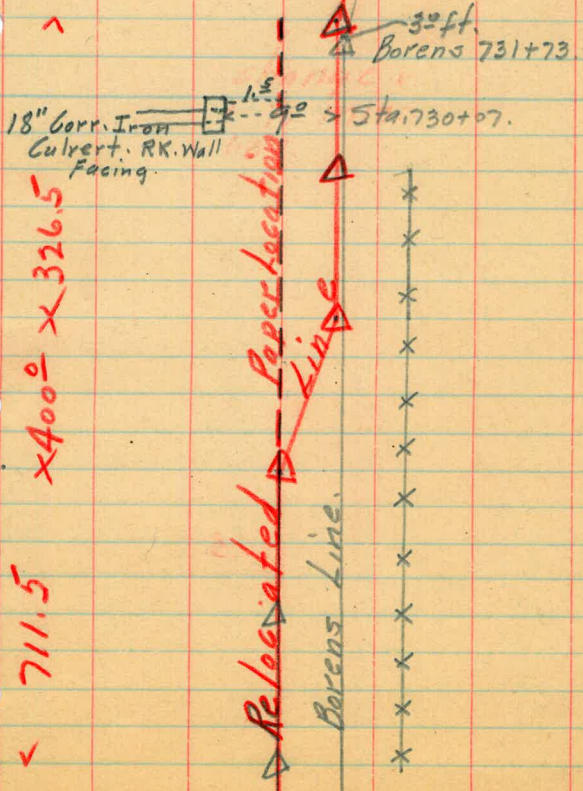
5.83°48'W 651.8

717+48<sup>±</sup> B.C.

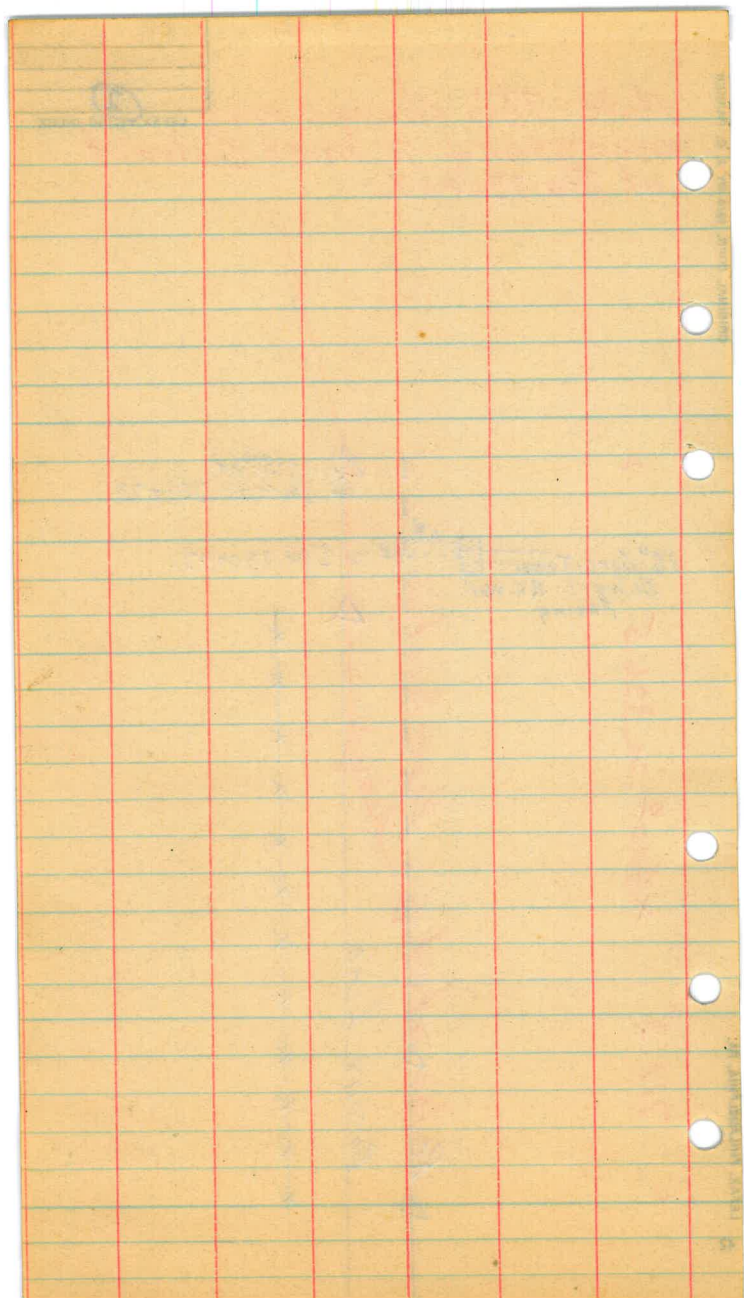
T=59.7

P.I 716+89<sup>±</sup> 14°15'R

Note - This change was necessary to miss Culvert at Sta. 730+07.







El Capitan Pipe Line Survey.  
March 11, 1926.

Line change from Paper  
Location to Tie into Borens Line,  
with Equasion of Stations and  
Bearing.  
Sta. 770130<sup>±</sup> to Sta. 800199<sup>±</sup>

(19)

P.I. 802+17<sup>8</sup>

T=118.6

800+99<sup>8</sup> B.C. =  
801+02<sup>8</sup> B.C. =

= N. 80° 44' W =  
N. 80° 42' W = 1167.3

789+34<sup>8</sup> 1° 07' L.

834.8

N. 79° 35' W (934.8)

781+00 0° 21' R

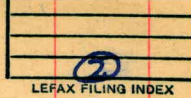
N. 79° 56' W 1068.6

770+34<sup>8</sup> E.C.

P.I. 769+80<sup>8</sup>

T=50.6





< 1179.2 ✓ x 9342 x 1285.9 >

Relocation

Borens Line

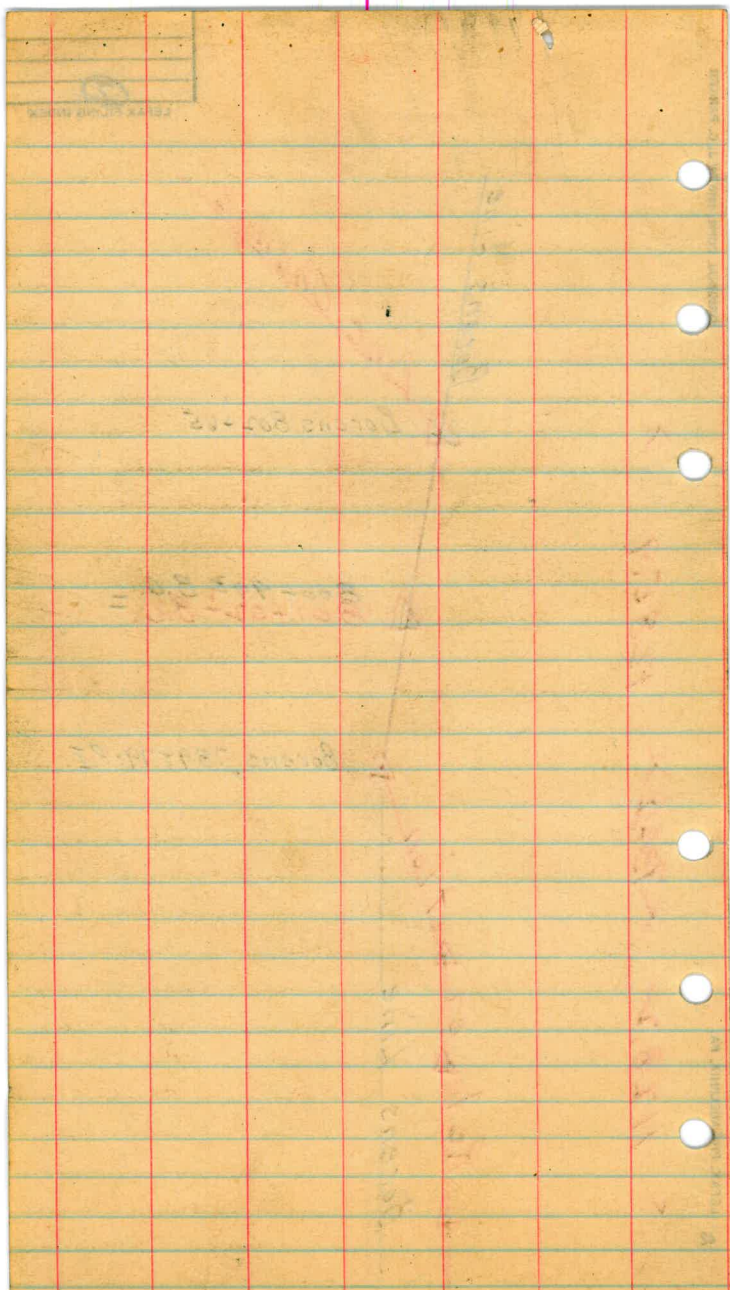
$800 + 99 \approx B.C. =$   
 $801 + 02 - B.C. =$

Borens 802+65

Borens 789+79 P.I.

Borens Line

Line Change



El Capitan Pipe Line Survey.  
Jan. 30, 1926.

Equasion in Stationing to take  
care of 14 ft. mistake in  
chaining on Bowens Line between  
Sta. 92+00 - Sta. 94+00.

20



PI 95+47.2 7°56' L

94+48<sup>5</sup> B.C. =  
94+34<sup>6</sup> B.C. =

~~94+40.2 P.O.T. =~~ 85.9  
~~94+51.9 P.O.T. =~~ 99.9

46°45' W

93+48<sup>5</sup> E.C.

PI 92+56<sup>5</sup> 18°36' R

^ "B"

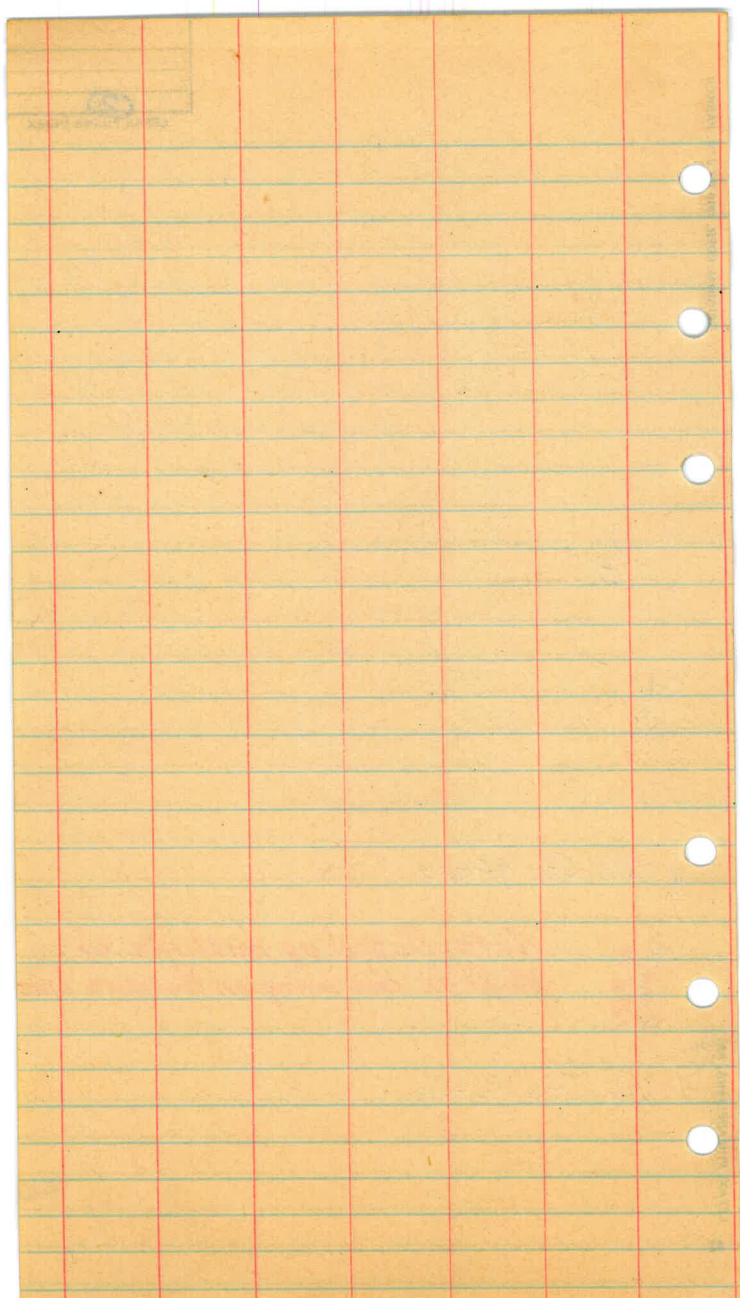
93.2

x Old Sta 94+00

~~93.2~~  
186.2

Note Picked up mistake of 14 ft. in chaining on Bonens Line

x Old Sta. 92+00





El Capitan Pipe Line Survey.  
Feb. 10. 1926.

Tie to Bowens Line at Sta. 258+55.  
Equasion of Bearing and Station  
to Continue along Old Line as  
Figured in Paper Location.

P.I. 260+14<sup>9</sup> 59°17'

259+76<sup>1</sup> B.C.

= N 53°36' W 250.7  
N 53°30' W

257+25<sup>4</sup> 2057  
257+31<sup>4</sup> E.C. =

P.I. 256+70<sup>2</sup> 49°20' R

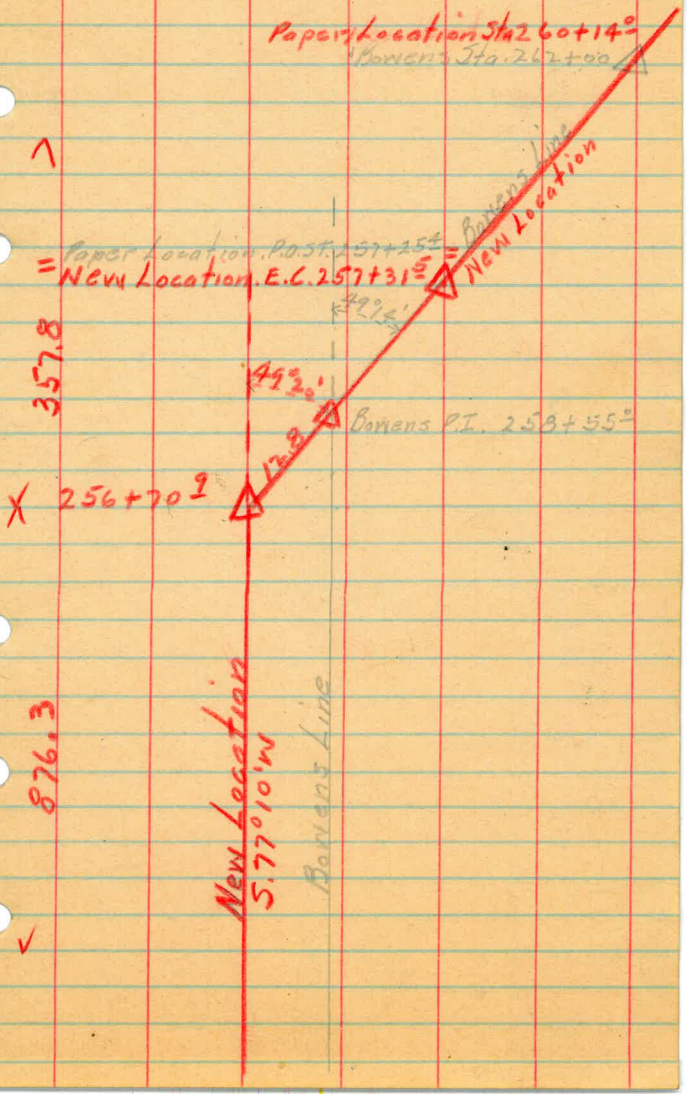
E=15.1  
T=69.2  
R=150.78  
D=38°  
L=129.7

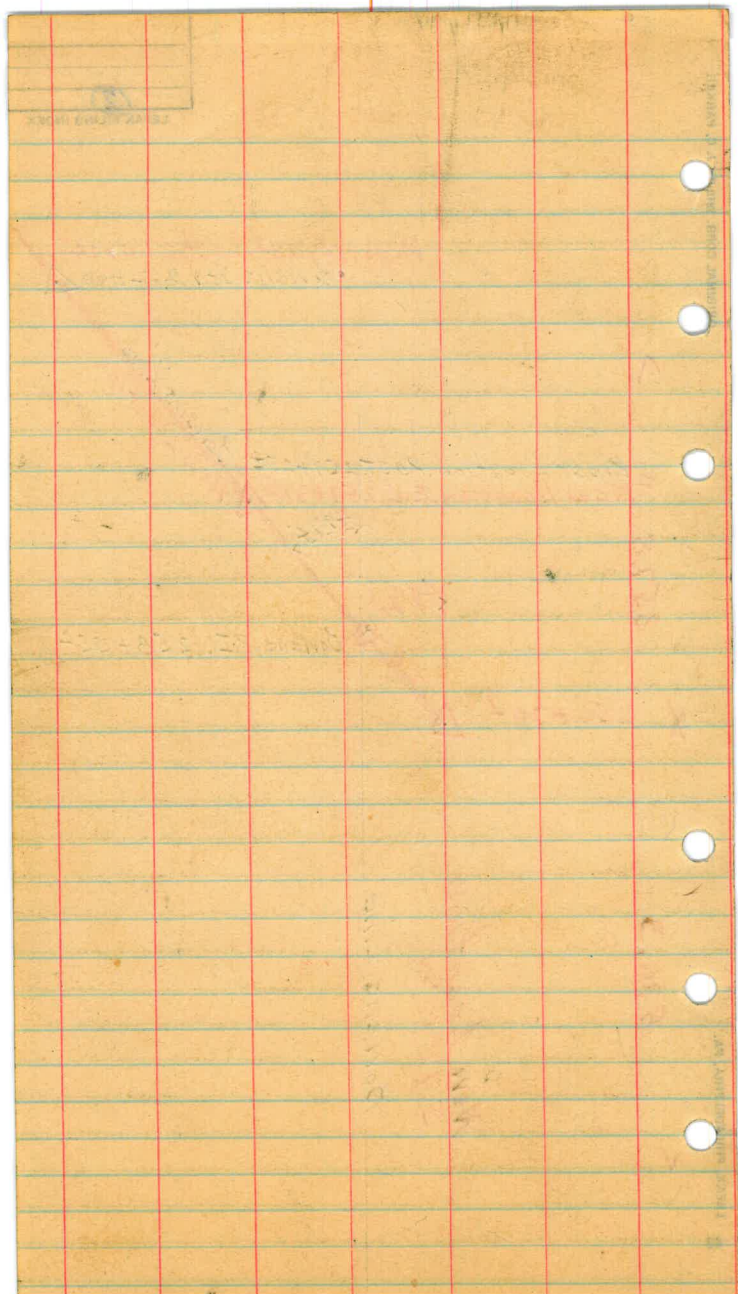
256+01<sup>2</sup> B.C.

5.77101<sup>1</sup> 724<sup>1</sup>

248+77<sup>6</sup> E.C.

P.I. 247+94<sup>6</sup> 638' R







Profile Levels and Cross  
Sections on Line Change.  
from Sta. 912+93.1 to  
Equation.

= Sta. 918+86.63 Back =  
= Sta. 918+84.29 Ahead =

Page 1-4.

W<sup>m</sup> Simpson - Level.

May 26. 1926.

22

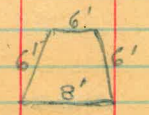
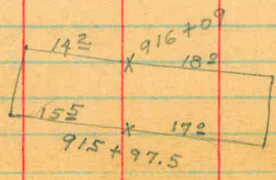
Relocation.

Sta	+	π	-	Elev.
				267.352 B.M. #109
	0.632	267.984		
			4.247	263.737
	7.168	270.905		
912+931			8.3	262.6
913+00			8.2	262.7
+27 <sup>2</sup>			7.7	263.2
+91 <sup>63</sup>			5.9	265.0
914+16 <sup>E</sup>			4.9	266.0
+41 <sup>E</sup>			4.8	266.1
+66 <sup>E</sup>			4.6	266.3
+91 <sup>E</sup>			4.5	266.7
915+16 <sup>E</sup>			4.7	266.2
+41 <sup>E</sup>			4.9	266.0
+66 <sup>E</sup>			4.9	266.0

25 2 2.5

$\frac{6.7}{100}$	$\frac{7.4}{100}$	$\frac{9.1}{100}$	$\frac{8.2}{100}$
$\frac{6.1}{100}$	$\frac{7.4}{100}$	$\frac{9.1}{100}$	$\frac{8.0}{100}$
$\frac{6.1}{100}$	$\frac{6.4}{100}$	$\frac{8.0}{100}$	$\frac{7.5}{100}$
$\frac{8.1}{100}$	$\frac{3.0}{4.0}$	$\frac{6.1}{1.0}$	$\frac{5.4}{100}$
$\frac{2.7}{100}$	$\frac{8.2}{100}$	$\frac{6.1}{3.0}$	$\frac{5.0}{100}$
$\frac{3.0}{100}$	$\frac{3.0}{100}$	$\frac{5.4}{4.0}$	$\frac{4.0}{100}$
	$\frac{2.0}{100}$	$\frac{5.1}{7.0}$	$\frac{4.7}{100}$
		$\frac{9.0}{100}$	$\frac{4.8}{100}$
		$\frac{2.6}{100}$	$\frac{5.1}{100}$
		$\frac{4.5}{100}$	$\frac{5.4}{100}$
		$\frac{4.4}{100}$	$\frac{5.5}{100}$

Wooden Culvert.



Sta	+	π	-	Elev.
		270.905		
915+91E			4.8	266.1
915+97E	Wooden culvert.		4.9	266.0
916+09	Wooden culvert.		4.7	266.2
T.P.			4.524	266.381
		7.850	274.231	
916+16E			7.5	266.7
+41E			6.6	267.6
+66E			5.2	269.0
+91E			3.2	271.0
917+16E			1.9	272.8
			1.067	273.164
		12.896	286.060	



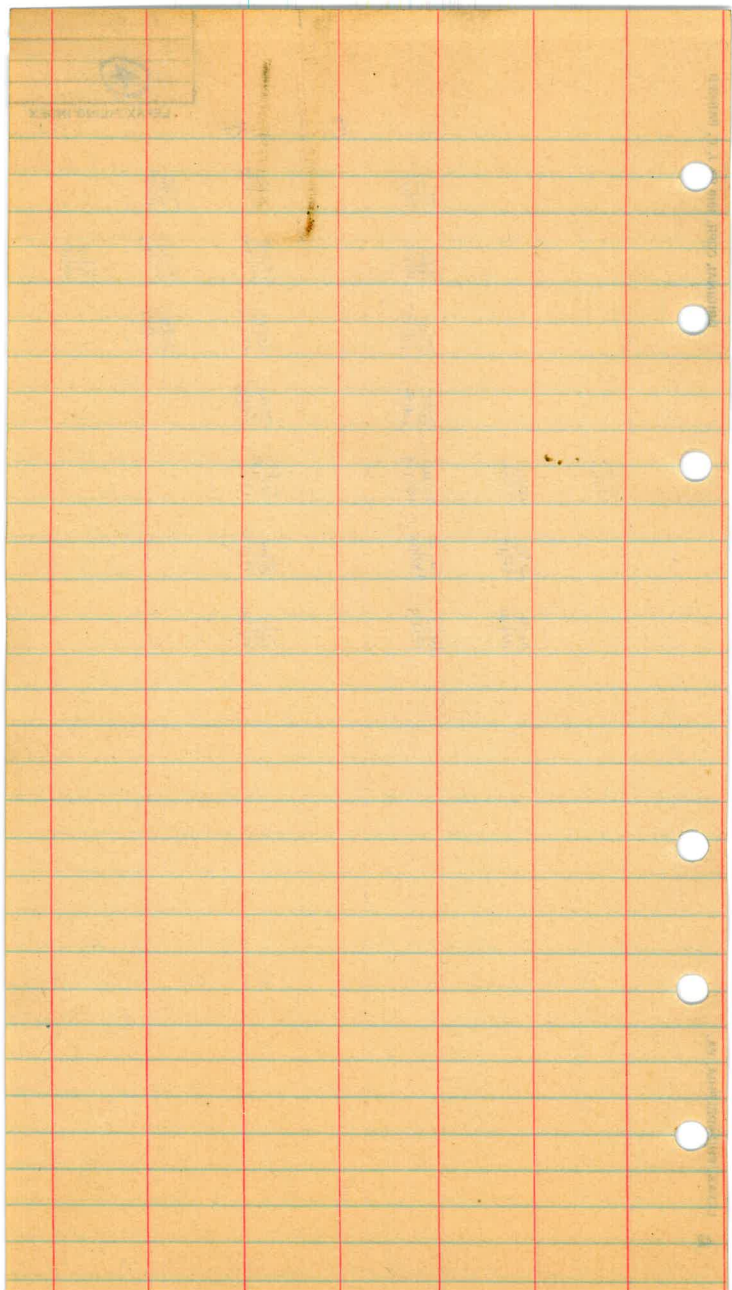
L.F.      R      R.T.

	$\frac{46}{70}$	$\frac{51}{80}$	$\frac{5}{100}$
Top →	$\frac{51}{153}$	$\frac{62}{190}$	← Top R.T.
	$\frac{113}{153}$ <sup>259.6</sup>	$\frac{123}{190}$ <sup>258.6</sup>	
Floor →		$\frac{123}{190}$	← Floor culvert.
	$\frac{115}{153}$ <sup>259.4</sup>	$\frac{140}{170}$ <sup>256.9</sup>	
Ground →		$\frac{140}{170}$	← Ground at END culvert.
2.5	$\frac{51}{143}$	$\frac{62}{182}$	← Top
	$\frac{112}{143}$ <sup>259.5</sup>	$\frac{123}{182}$ <sup>258.6</sup>	← Floor
Floor →		$\frac{134}{182}$ <sup>257.5</sup>	← Ground
	$\frac{112}{143}$ <sup>259.7</sup>		
Ground →			

	$\frac{76}{100}$	$\frac{72}{70}$	$\frac{10}{100}$
	$\frac{65}{100}$	$\frac{73}{100}$	
	$\frac{5}{100}$	$\frac{5}{100}$	
$\frac{10}{100}$	$\frac{26}{100}$	$\frac{30}{100}$	
	$\frac{11}{100}$	$\frac{21}{100}$	

Sta	+	$\pi$	-	Elev.
		286.060		
917+91 <sup>6</sup>			11.3	274.8
+66 <sup>6</sup>			9.3	276.8
+91 <sup>5</sup>			7.3	278.8
918+16 <sup>6</sup>			5.5	280.6
441 <sup>6</sup>			3.6	282.5
+66 <sup>6</sup>			2.2	283.9
918+86 <sup>63</sup> = 918+84 <sup>29</sup>			0.7	285.4







Profile Levels and  
Cross Sections on Line  
Change from Sta. 801+12  
to Equation.

Sta. 811+67.75 - Back  
Sta. 810+07.49 - Ahead.

Page 1-4.

W<sup>m</sup> Simpson - Level.

May 26, 1926.

MAY. - 26.

Simpson - Inst.  
Revoix - Rod  
Isbell - "Sta. +  $\pi$  - Elev.  
332.102 B.M. #89

6.757 338.860

801+12 3.6 335.3 ✓

802+00 4.2 334.7 ✓

+50 4.1 334.8 ✓

803+00 5.7 333.2 ✓

T.P. 5.428 333.432

2.073 335.505

804+00 5.9 329.6 ✓

+37 7.0 328.5 ✓

805+04<sup>83</sup> B.C. 2.6<sup>A</sup> 322.3

T.P. 12.934 323.071

1.863 324.934<sup>B</sup>805+14<sup>B</sup> 3.0 321.9+24<sup>B</sup> 3.6 321.3+34<sup>B</sup> 4.0 320.9+36<sup>B</sup> 18' concrete  
Culvert. 4.1 320.8



Sta +  $\pi$  - Elev.  
324.934

805+49<sup>B</sup> 4.7 320.2

+54<sup>B</sup> 5.5 319.4

+64<sup>B</sup> Center of Road, 5.5 319.4

805+74<sup>B</sup> 5.6 319.3

+84<sup>B</sup> 6.9 318.0

+94<sup>B</sup> 7.9 317.0

806+04<sup>B</sup> 7.9 317.0

+14<sup>B</sup> 8.2 316.7

+24<sup>B</sup> 8.7 316.2

+35<sup>B</sup> E.C. 9.2 315.7

807+00 11.9 313.0

T.P. 9.438 315.496

2.206 317.502

808+00 6.9 310.8



Lf. C. Rt.

$$\frac{37}{100} \quad \frac{65}{100} \quad \frac{60}{100}$$

$$\frac{47}{150} \quad \frac{67}{150}$$

$$\frac{47}{150} \quad \frac{57}{110} \quad \frac{48}{100} \quad \frac{65}{150}$$

30" sycamore tree sta. 805+58<sup>00</sup> - 5' Rt.

$$\frac{79}{150} \quad \frac{66}{90} \quad \frac{57}{80} \quad \frac{65}{150}$$

$$\frac{80}{150} \quad \frac{80}{90} \quad \frac{67}{30} \quad \frac{68}{150}$$

$$\frac{86}{150} \quad \frac{67}{70} \quad \frac{67}{150}$$

$$\frac{87}{150} \quad \frac{81}{60} \quad \frac{65}{90} \quad \frac{68}{150}$$

$$\frac{85}{150} \quad \frac{81}{80} \quad \frac{69}{110} \quad \frac{77}{150}$$

$$\frac{90}{150} \quad \frac{82}{80} \quad \frac{76}{120} \quad \frac{76}{150}$$

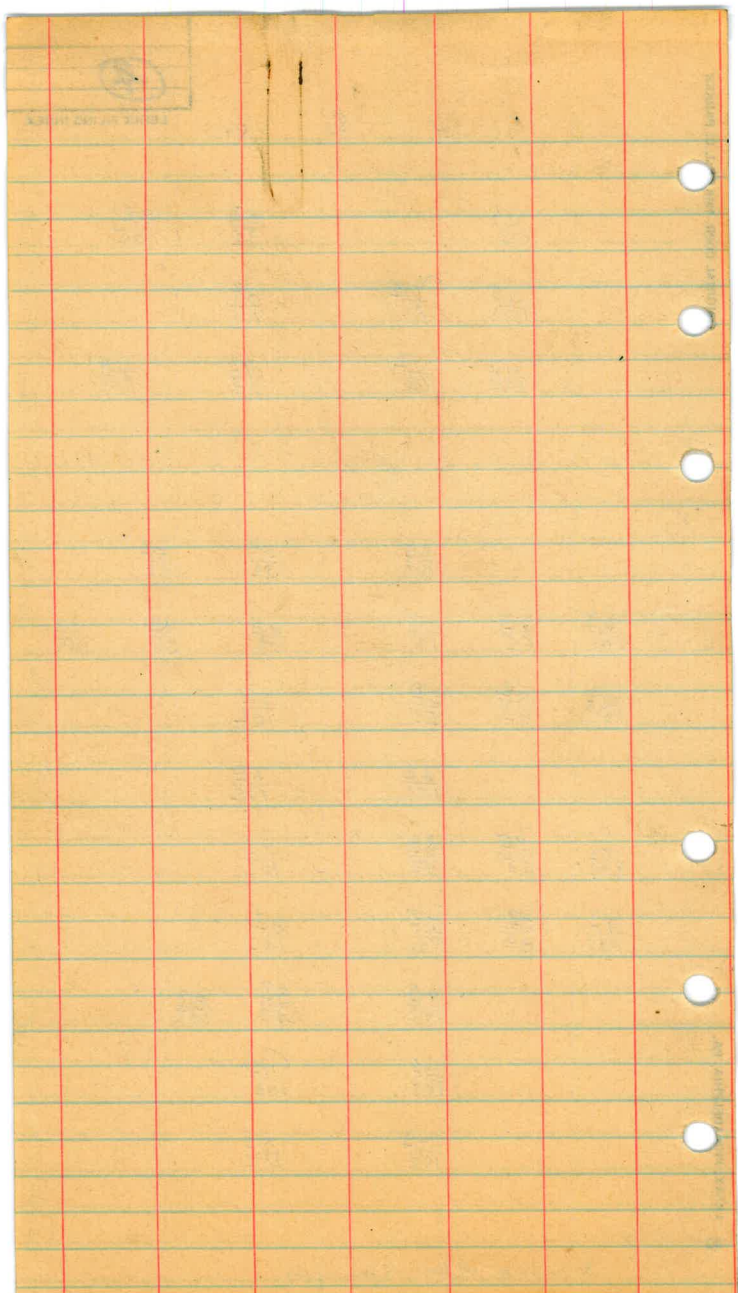
$$\frac{90}{150} \quad \frac{90}{60} \quad \frac{75}{100} \quad \frac{81}{150}$$

$$\frac{114}{150} \quad \frac{100}{120} \quad \frac{120}{30} \quad \frac{110}{15} \quad \frac{90}{40} \quad \frac{90}{150}$$

$$\frac{76}{150} \quad \frac{80}{100} \quad \frac{70}{80} \quad \frac{60}{20} \quad \frac{64}{150}$$

Sta	+ π	-	Elev.
	317.702		
808+82		9.8	307.9
+85		8.3	309.4
809+00		9.7	308.0
T.P.		9.370	308.332
	1.350	309.682	
810+00		5.7	304.0
+83 <sup>5</sup>		4.8	304.9
+27° B.C.		5.7	304.0
+52 <sup>0</sup>		6.1	303.7
+77 <sup>0</sup>		7.0	302.7
811+02 <sup>0</sup>		7.8	301.9
+27 <sup>0</sup>		10.2	299.5
+52 <sup>0</sup>		9.3	300.4
810+07 <sup>19</sup> = 811+67 <sup>12</sup> E.C.		10.0	299.7
T.P.		9.873	299.809
	1.791	301.600	
B.M. # 70.		11.130	290.470







1986

RP  
△ 20' △ 20' △  
- 90°  
R.P.

old Sta. 9+99.5

1992

R.P. △ 20' △ 20' △ R.P.  
90°

old Sta. 7+99.2

A = 102.7

559.1

Opp. B.

1911.9

On Axis N. 1° 28' E. 18' from old Sta  
- 52.87

20+15<sup>2</sup> ✓

17+12<sup>2</sup> B.C. ✓

17+50<sup>3</sup> P.O.T. ✓  
5.82°03'N 177°

15+100<sup>3</sup> P.O.T. ✓  
5.82°03'N 250°

14+78<sup>3</sup> E.C. ✓  
5.82°03'N 21.3

Tues. 1/19/26

14+52<sup>2</sup> 24° ✓

E=2.9  
T=27.7  
R=130.37  
D=44°  
L=54.5

14+24<sup>2</sup> B.C. ✓

N.73°51'W 79.1

13+26<sup>2</sup> E.C. ✓

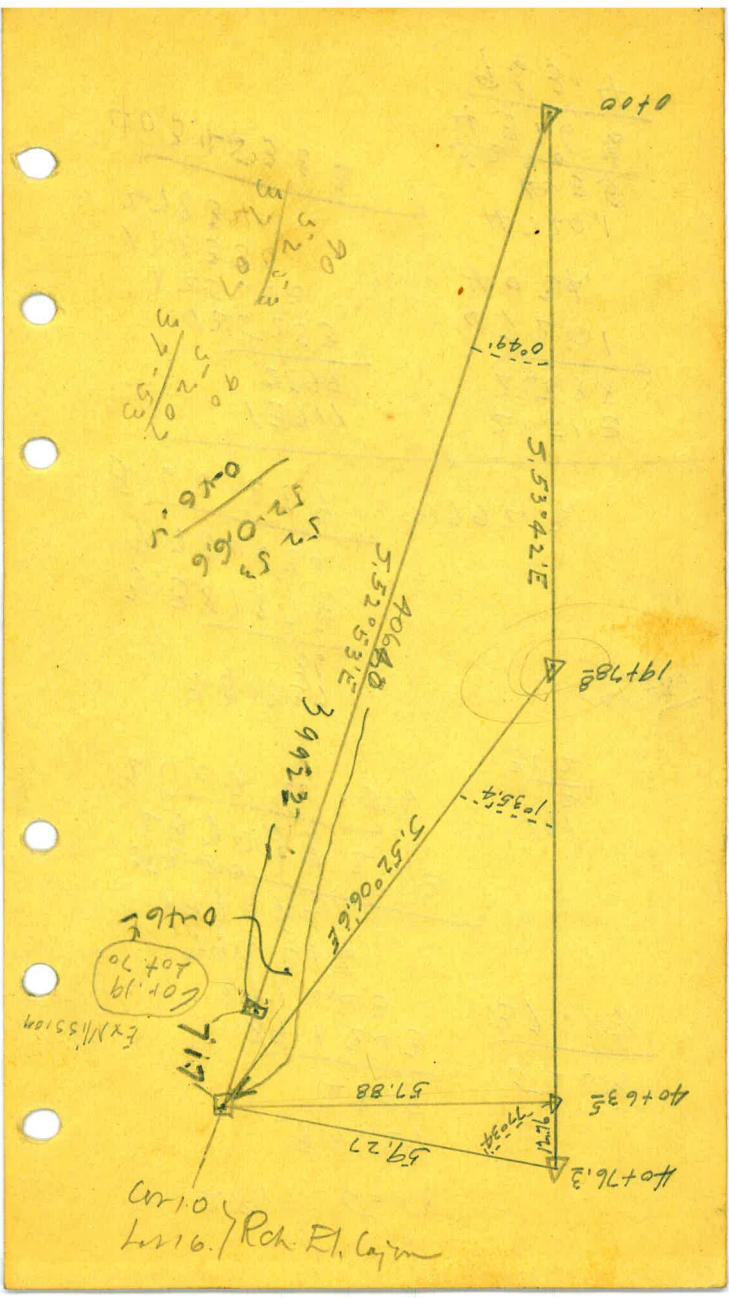
12+48<sup>2</sup> 9°11' RV

E=3.1  
T=76.7  
R=95.73  
D=6°  
L=153.1

11+72<sup>2</sup> B.C. ✓

N.83°08'W 4.2

11+68<sup>2</sup> E.C. ✓



2.513  
 2568.8  
472.01  
 4034.  
 472.01  
4034  
 5280.8  
4316.6  
 963.14

13917  
 2899  
125253  
 125253  
 11336  
 27834  
40345383

381837  
 36  
3381873  
 9780634  
3601239  
 = 3992.3

109/480

181  
362

99027  
 2899  
891243  
 891243  
 792216  
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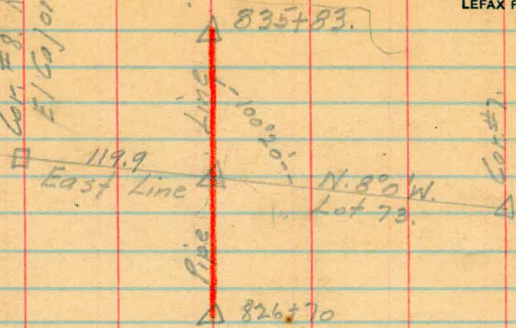
2899 Cos 8°



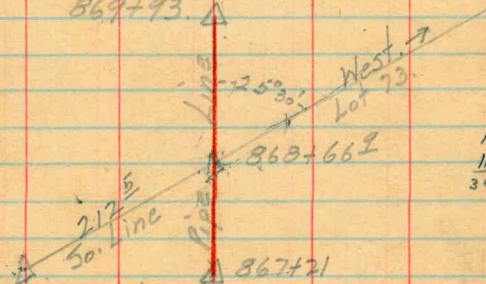
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LEFAX FILING INDEX

Cor. # 8 Rancho  
El Cajon.



869+93.



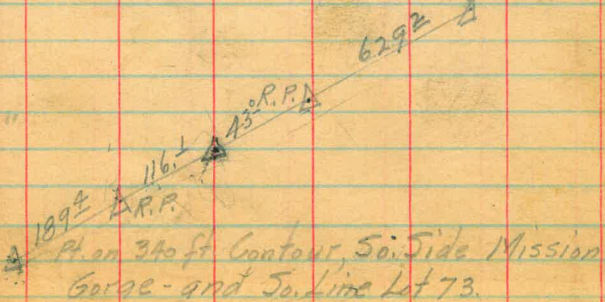
189.4
116.1
305.5

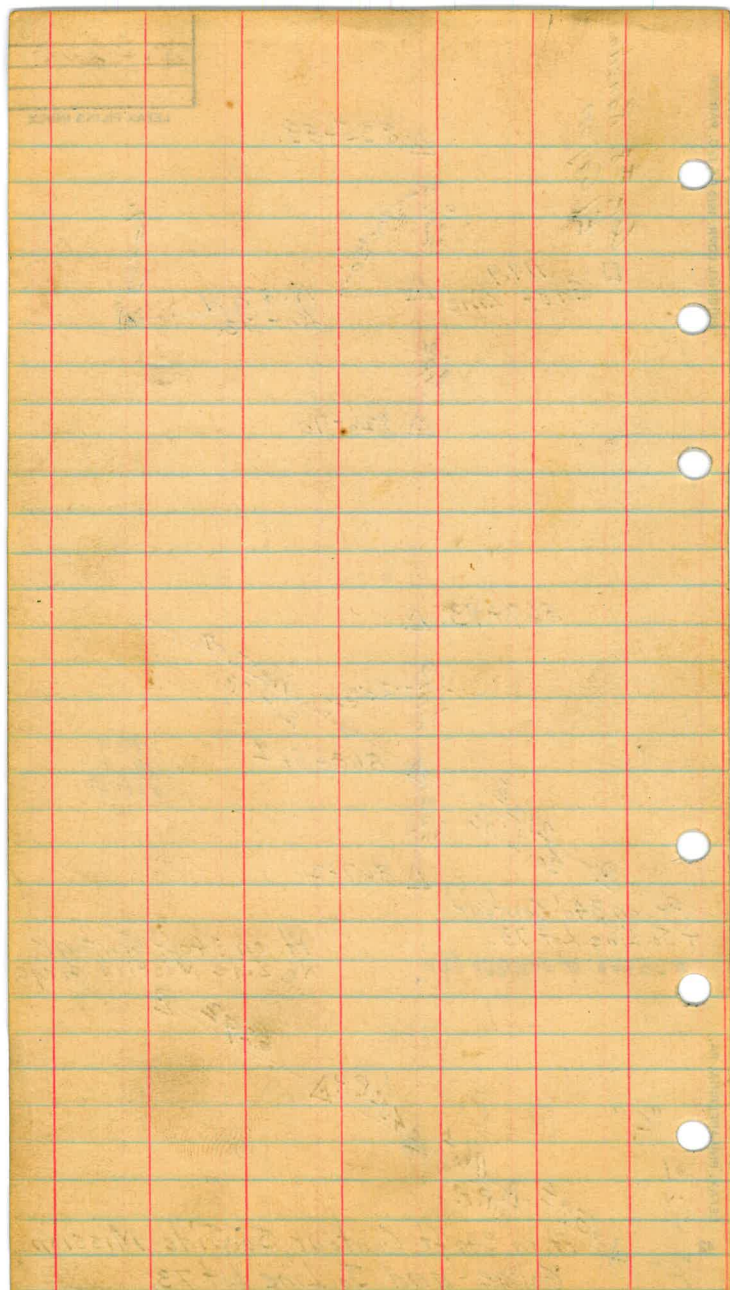
Pt. on 340' Contour  
+ So. Line Lot 73.  
= 00+00 of contour sur.

Pt. on 340' Contour  
No. Side Mission Gorge.

LEFAX, PHILADELPHIA, PA.

42





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Meander of 340 ft. Contour  
in Mission Gorge. Lot 73. Ex ①  
Mission Rancho. Property of  
Wm F. West.

Feb. 23-24.

G. W. Converse, Chief of Party.

H. Soper Hd. Chain.

Wm Simpson Rr. Chain.

Jas. Todd Rr. Chain.

LEFAX, PHILADELPHIA, PA.

42



6+67<sup>5</sup> ✓

N.53°20'E ✓

5+78<sup>7</sup> ✓

5°19' L N.51°22'E ✓

5+57<sup>3</sup> ✓

0°51' R N.57°32'E ✓

5+29<sup>1</sup> ✓

28°16' R N.84°57'E ✓

4+79<sup>0</sup> L.3°21' ✓

N.56°41'E ✓

Feb. 23

4+51<sup>5</sup> ✓

8°55' L N.54°55'E ✓

45.5 ✓

40.5 ✓

4+11<sup>0</sup> ✓

15°31' R N.79°21'E ✓

28.4 ✓

3+82<sup>6</sup> L.7°09' ✓

N.63°50'E ✓

21.1 ✓

3+61<sup>5</sup> ✓

2°39' R N.64°50'E ✓

36.3 ✓

3+25<sup>3</sup> ✓

8°28' R N.70°39'E ✓

65.1 ✓

2+80<sup>1</sup> R.1°39' ✓

N.62°11'E ✓

136.3 ✓

1+23<sup>8</sup> R.1°21' ✓

N.60°44'E ✓

123.8 ✓

0+0<sup>0</sup> L.2°9'6" ✓

East



ORIGINAL COPY, 1910 BY J. C. PARKER

TRADE MARK

Profile of S. p. River due  
W. from Pipe Line.

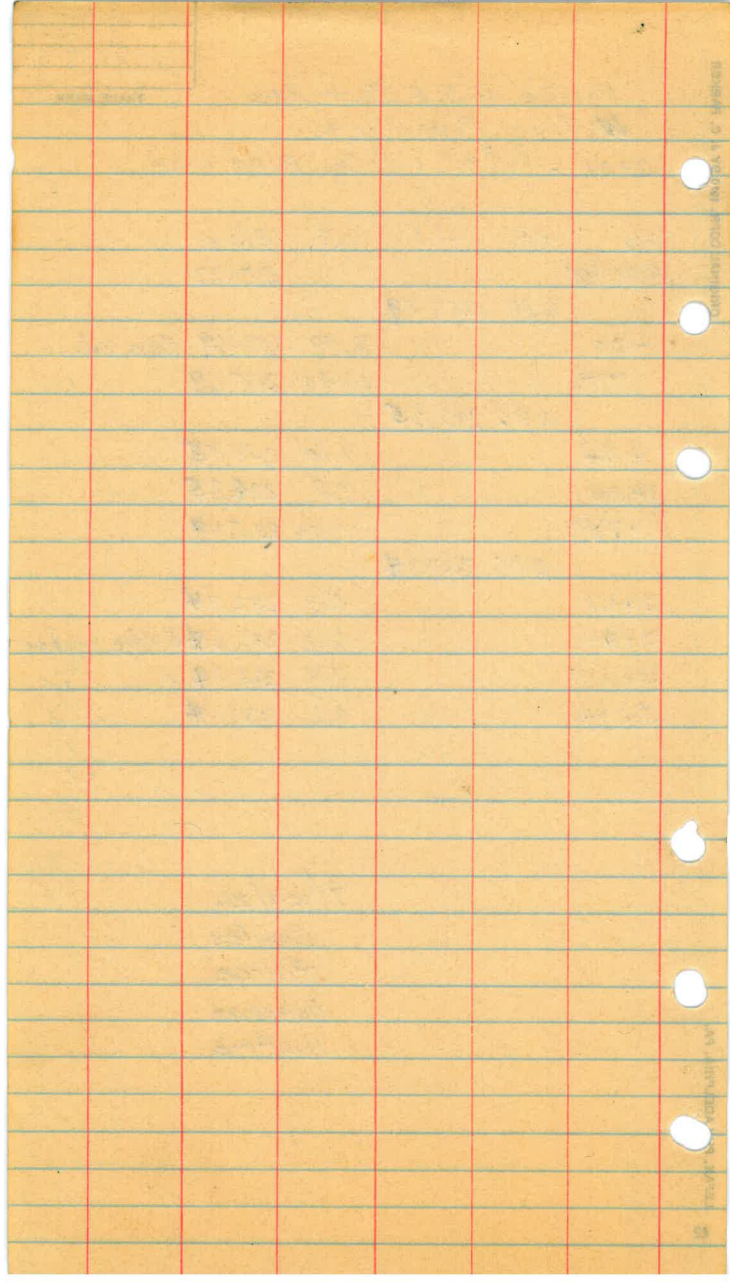
0+00 = 868 + 77.8 E/Cap. Pipe Line

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	6.32		257.59
+20		2.90	254.69 Edge rd.
T.P.		11.90	245.69
	0.96		246.65
+64		1.10	245.55
+39		9.8	236.85
T.P.		11.56	235.09
	2.85		237.94
2+14		5.7	232.24
2+94		6.2	231.64 E. edge water
3+45		4.9	233.04 W "
3+94		0.1	237.84

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7/23/26  
Cowles  
Pierce  
Osborne  
Moultrie

LEFAX, PHILADELPHIA, PA.



1880-1881

Continued from page 1 of 1

1880-1881

3425.2

2

88.8 ✓

21.4 ✓

28.2 ✓

32.1 ✓

60.44

1.27

62.11

1.39

63.50

7.09

56.41

499.8

451.3

48.5

451.5

41.5

411.0

382.6

28.4

382.6

261.5

21.1

382.6

261.5

21.1

361.5

325.2

36.3

325.2

260.1

65.1

260.1

123.8

136.3

Pt. on So. Line Lot 73 Ex Mission Rancho and  
Contour 340. So. Side Mission Gorge.

15+70<sup>+</sup> ✓ 15°27'R N.28°32'E ✓  
15+45<sup>+</sup> ✓ 11°47'R N.24°52'E ✓  
14+83<sup>+</sup> ✓  
14+22<sup>+</sup> ✓ N13°5E ✓  
81°22'L N.11°0'E ✓  
13+63<sup>+</sup> ✓ 81°50'L N.10°42'E ✓  
12+43<sup>+</sup> ✓ 29°0'R.5.58°28'E ✓  
11+82<sup>+</sup> ✓ L.79°27' ✓  
4 ✓ 5.87°28'E ✓  
11+43<sup>+</sup> ✓ R.19°15' ✓  
10+76<sup>+</sup> ✓ R.23°18' ✓  
9+51<sup>+</sup> ✓ N73°17'E ✓  
8°09'L N.49°02'E ✓  
8+77<sup>+</sup> ✓ 4°41'L N.52°30'E ✓  
8+54<sup>+</sup> ✓ 24°35'R N.81°46'E ✓  
8+27<sup>+</sup> ✓ L.7°12' ✓  
7+44<sup>+</sup> ✓ R.6°10' ✓  
6+93<sup>+</sup> ✓ N.57°11'E ✓  
N.51°01'E ✓  
10°52'R N.64°12'E ✓  
6+67<sup>+</sup> ✓ L.2°19' ✓  
N.53°26'E ✓



3

24.5 ✓

62.2 ✓

60.5 ✓

59.1 ✓

120.5 ✓

60.9 ✓

39.3 ✓

66.7 ✓

124.8 ✓

74.3 ✓

23.3 ✓

26.4 ✓

83.2 ✓

50.2 ✓

51.2 ✓

76.3 ✓

6°10'R

73 17  
19 15  
92 32

87 28  
79 27  
180 55  
166 55  
23 05

49 59  
23 18

73 17  
19 15  
92 32

87 28  
79 27  
180 55  
166 55  
13 05

28+89 <sup>3</sup>	
Δ	N. 25° 51' E
27+52 <sup>6</sup>	R. 19° 14'
Δ	N. 6° 37' E
25+22 <sup>8</sup>	R. 11° 04'
Δ	N. 42° 27' W
23+98 <sup>3</sup>	R. 4° 59'
Δ	N. 9° 26' W
22+41 <sup>3</sup>	R. 8° 52'
Δ	N. 18° 18' W
21+35 <sup>8</sup>	36° 52' L N. 15° 37' W
20+86 <sup>3</sup>	21° 37' R N. 42° 52' E
20+72 <sup>4</sup>	10° 33' R N. 31° 48' E
Δ	N. 21° 15' E
20+50 <sup>5</sup>	L. 39° 33'
19+20 <sup>2</sup>	8° 19' R N. 21° 24' E
18+15 <sup>2</sup>	10° 42' R N. 23° 47' E
17+97 <sup>3</sup>	11° 45' R N. 24° 50' E
17+80 <sup>4</sup>	10° 35' R N. 23° 40' E
16+38 <sup>3</sup>	10° 57' R N. 24° 02' E
15+70 <sup>1</sup>	
Δ	N. 13° 05' E
14+83 <sup>4</sup>	R. 8° 10'





51+04<sup>2</sup> ✓  
51+00<sup>1</sup> ✓ 5.35°34'W ✓  
R. 20°39' S. 36°22'W ✓  
50+52<sup>2</sup> ✓  
R. 22°57' S. 38°40'W ✓  
48+73<sup>1</sup> ✓ R. 19°51' ✓  
5.15°43'W ✓  
48+09<sup>2</sup> ✓ R. 8°55' ✓  
5.6°48'W ✓  
46+49 ✓ 9°10' R. 5.86°08'W ✓  
45+14<sup>3</sup> ✓ L. 70°10' ✓  
5.76°58'W ✓  
43+82<sup>2</sup> ✓ 64°07' R. N. 36°21'W ✓  
43+04<sup>1</sup> ✓ L. 2°34' ✓  
5.79°32'W ✓  
42+30<sup>1</sup> ✓ R. 26°19' ✓  
5.53°13'W ✓  
40+66<sup>4</sup> ✓ L. 118°45' ✓

Feb. 24.

P.O.T.  
33+07<sup>6</sup> ✓ N. 8°02'W ✓  
R. 44°54' ✓  
32+78<sup>5</sup> ✓ N. 52°56'W ✓  
L. 103°13' ✓  
31+17<sup>2</sup> ✓ N. 50°17'E ✓  
R. 14°46' ✓  
28+69<sup>2</sup> ✓ N. 35°31'E ✓  
R. 9°40' ✓  
N. 25°51'E ✓



24
55
53
57
04

72.6
85
160

LEFAX FILING INDEX

5

Not on 340 Contour

48 ✓

28+69.3
247.3
31+17.0
161.6
32+78.6
29
33+07.6

25-51
9 40
35-31
14 46
50 17
103-13
50-17
52-56
44 44
8 02

47 ✓

179 ✓

63 ✓

160 ✓

134 ✓

131.8 ✓

78 ✓

74.0 ✓

163 ✓

↑

758.8 ✓

↓

29 ✓

161 ✓

249 ✓

118 45
40+66.4
1+63.0
42+30.0
1 2 5
43+82.5
1 31 8
45+14.8
13+3
46+49
160.6
43 07 7
63 7
48 7 3 6
179
50+52.8

118 42
80 2
110 43
80 02
118 45
180 47
126 47
53 10
26 19
79 32
2 34
76 50

Pl. on E. Line Lot. 73 and 340ft Contour on No. Side Gorge.

34+27 7

Cor. #8. Rancho El Cajon

Pl. on E. Line Lot 73 Ex Mission Rancho and 340' Contour on So. Side Mission Gorge.

66+57 <sup>8</sup>		18°07'R 5.19-32W
66+15 <sup>8</sup>		38°15'R 5.39-40W
65+80 <sup>8</sup>		
62+02 <sup>8</sup>	5.1°25'W	14°45'R 5.5°03'W
61+51 <sup>5</sup>		28°0'R 5.18°18'W
60+59 <sup>7</sup>	R.11°0'	
59+85 <sup>5</sup>	L.28°08'	5.9°42'E
59+45 <sup>5</sup>		5.13°26'W
59+33 <sup>4</sup>		16°03'L 5.19°31'W
56+67 <sup>2</sup>		15°21'L 5.20°13'W
55+72 <sup>2</sup>		7°35'L 5.27°59'W
55+13 <sup>2</sup>		5°17'L 5.30°17'W
53+41 <sup>2</sup>		2°08'R 5.37°42'W
53+05 <sup>2</sup>		4°36'R 5.40°10'W
52+09 <sup>2</sup>		8°08'R 5.43°42'W
51+04 <sup>2</sup>	L.17°08'	8°13'R 5.43°47'W
		5.35°34'W

68.0  
23.0  
91.0

LEFAX FILING INDEX

38  
58.9  
96.9  
78.0  
80.9  
72.0  
15.2  
265.2  
53+41.0  
172.8  
58+13.8  
58.6  
55+72.4  
95.5  
56+67.9  
265.2  
59+33.1  
39.5  
57+25.5  
59.8  
5.0  
74.7  
77.0  
60+59.7  
91.9  
92.1  
61+51.4  
50.6  
87  
11  
62+02.2

6

36<sup>0</sup> ✓

35<sup>0</sup> ✓

378<sup>6</sup> ✓

50<sup>6</sup> ✓

91<sup>2</sup> ✓

Not on Contour ✓

74<sup>2</sup> ✓

39<sup>5</sup> ✓

12<sup>4</sup> ✓

265.2 ✓

95<sup>5</sup> ✓

58<sup>6</sup> ✓

172<sup>8</sup> ✓

35<sup>1</sup> ✓

96<sup>2</sup> ✓

104<sup>1</sup> ✓

N. 87° 11' W  
46.4  
θ A

35 3.2  
17 0.8  
18 26.6  
38 0.8  
18 26.6  
94.2

11 0.7  
9 0.0  
1 2.5



82+51 <sup>2</sup> ✓		L. 8°44' S. 65°58' W ✓
80+67 <sup>2</sup> ✓		L. 6°49' S. 67-22 W ✓ S 67°53' W ✓
79+84 <sup>2</sup> ✓		R. 6°06' S. 80-18 W ✓ S 80°48' W ✓
78+92 <sup>3</sup> ✓		R. 47°13' N. 58-05 W ✓
77+63 <sup>2</sup> ✓		
75+77 <sup>2</sup> ✓	R. 8°25'	5.74°42' W ✓
74+98 <sup>5</sup> ✓	R. 13°22'	5.66°17' W ✓
72+97 <sup>2</sup> ✓		5.52°55' W ✓
71+82 <sup>2</sup> ✓	R. 6°44'	17°15' R. 563-26 W ✓
70+20 <sup>5</sup> ✓	R. 15°22'	5.46°11' W ✓
69+05 <sup>2</sup> ✓		5.30°59' W ✓
67+83 <sup>5</sup> ✓		17°26' R. 533-59 W ✓
67+91 <sup>2</sup> ✓	R. 14°26'	22°26' R. 538-59 W ✓
66+81 <sup>2</sup> ✓		5.16°32' W ✓
66+51 <sup>8</sup> ✓		24°06' R. 525-31 W ✓
65+80 <sup>5</sup> ✓	R. 15°08'	
		5.1°25' W ✓



7

181<sup>5</sup> ✓

852 ✓

71<sup>2</sup> ✓

128.2 ✓

186.9 ✓

138<sup>5</sup> ✓

140<sup>6</sup> ✓

115<sup>5</sup> ✓

162.4 ✓

115<sup>5</sup> ✓

121.4 ✓

51.8 ✓

49.9 ✓

30.1 ✓

Pl. on Opp. Side  
Gorge.

Pl. on Opp. Side  
Gorge.

6920'

10830'

○

○

○

△

○

△

△

○

○

○

○

○

△

66+81.9  
49.9

67+37.8

67+83.6  
1 21.4

67+65.0  
1 15.5

70+20.5  
1 62.4

71+82.9  
1 15

72+97.7  
1 40.6

74+58.5  
1 38.5

75+77.0  
1 86.9

77+63.9  
1 28.9

78+92.8  
91.2

79+84.0  
85.7

80+69.7  
1 81.5

82+51.2

80.00  
77.28

109.82

110  
110.50

69.70

88+64 <sup>2</sup> <del>+</del>		24° 13' R S 67-29 W <del>+</del>
88+43 <sup>2</sup> <del>+</del>		19° 41' R S 89-59 W <del>+</del>
88 <sup>A</sup> 703 <sup>1</sup> <del>+</del>		<del>+</del>
87+68 <sup>3</sup> <del>+</del>	5.40° 16' W	25° 22' L S 39-54 W <del>+</del>
87+38 <sup>3</sup> <del>+</del>		23° 25' L S 41-51 W <del>+</del>
87+12 <sup>2</sup> <del>+</del>		17° 37' L S 47-39 W <del>+</del>
86+85 <sup>5</sup> <del>+</del>		20° 21' L S 44-55 W <del>+</del>
86+36 <sup>4</sup> <del>+</del>		10° 59' L S 59-17 W <del>+</del>
85+61 <sup>2</sup> <del>+</del>		25° 0' R N 89-44 W <del>+</del>
85+10 <sup>3</sup> <del>+</del>		28° 02' R N 86-42 W <del>+</del>
84+72 <sup>3</sup> <del>+</del>		14° 18' R N 70-26 W <del>+</del>
84 <sup>A</sup> +34 <sup>5</sup> <del>+</del>	2.250'	<del>+</del>
83+44 <sup>2</sup> <del>+</del>	5.65° 16' W	9° 16' L S 65-26 W <del>+</del>
82+91 <sup>3</sup> <del>+</del>		
82+51 <sup>2</sup> <del>+</del>		→
77+63 <sup>9</sup> <del>+</del>	L. 9° 26'	
	5.74° 42' W	

LEFAX FILING INDEX

20.8 ✓

40.3 ✓

34.8 ✓

29.5 ✓

26.1 ✓

27.1 ✓

49.3 ✓

74.6 ✓

51.5 ✓

38. = ✓

37.2 ✓

90.2 ✓

52.6 ✓

40.6 ✓

△

△

△

8

82+91.8  
52.6

88+44.4  
40.2

84 3 4 6  
25 30

65 58  
90 88

71 28  
88 32

84+54.6  
37.7

84+72.3  
38.

88+0.3  
51.5

85+61.8  
76.6

86+36.4  
49.2

86+85.6  
25.1

87+12.7  
26.1

87+38.8  
29.5

87+68.3  
34.8

88+03.1  
20.3

88+23.4  
20.8

88+64.2  
74 42  
9 26  
65 16

188° 32' W. ✓  
40.2 ✓

0+00 =  
99+03 =

89+25 = 1.132' 34"

88+64 =

88+03 = R. 2' 18"

East

5.42' 34" W ✓

5.40' 16" W ✓



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LEFAX FILING INDEX

9

132 3d  
42 2d  
90 00

88+64 =  
61 3  
89+28.5

40-16  
2-18  
42 34

LEFAX, PHILADELPHIA, PA.

42

977.7

61 3 ✓

Δ Starting Point.

Δ No. Side Gorge,  
Pt. on 340 ft. Contour +  
So. Line Lot 73 Ex Mission  
Rancho

○

Δ

4959.0

4959.5  
305.5  
4654.0

189.4  
116.1  
305.5

B.C. 9+33 <sup>8</sup>	- Def 30°45'	25	
9+58 <sup>8</sup>	1°30'	50	
9+83 <sup>8</sup>	2°15'	74.98	
10+08 <sup>8</sup>	3°0'	99.96	
10+33 <sup>8</sup>	3°45' ✓		0.71
10+58 <sup>8</sup>	4°30'		2.30 30
10+83 <sup>8</sup>	5°15'		
11+08 <sup>8</sup>	6°		4.9
11+33 <sup>8</sup>	6°45'		27.7
11+58 <sup>8</sup>	7°30'		21.3
11+68 <sup>0</sup>			13.7
			1312 4.5
			4.5 6.8 5
			0.48
			67.6 5
B.C. 11+72 <sup>2</sup>			99.1
12+97 <sup>2</sup>	25 - 45'		27.7
12+22 <sup>2</sup>	50 1°30'		14+24 ✓
12+47 <sup>2</sup>	74.98 - 2°15'		14+49 ✓
12+72 <sup>2</sup>	99.96 - 3°		+7.0
12+97 <sup>2</sup>	3°45'		78.9
13+22 <sup>2</sup>	4°30'		
13+25 <sup>3</sup>	4°35' 30"		
E.C. 13+25 <sup>3</sup>			
14+24 <sup>4</sup>	12°		10.0
14+32 <sup>4</sup>	2°12' - 9°48'		19.98
14+44 <sup>4</sup>	4°24' - 7°36'		29.93
14+54 <sup>4</sup>	6°36' - 5°24' On Rock		39.84
64 <sup>4</sup>	8°48' - 3°12' On Side Tree		
74 <sup>4</sup>	11° - 1° On Rock		
E.C. 78.9	12° - 1'		

82°03'	P.I 20+15.5	19+28
10°28'	87.5	174.5
<u>97 35</u>	19+28.0	21+02.5
87 29	+53	0°45'

$\Delta = 10^{\circ}28'$	+78	-1°30'	-3°44'
$\frac{1}{2}\Delta = 5^{\circ}14'$	20+03	-2°15'	-2°59'
D = 6°	+28	3°01'	-2°14'
R = 954.93	+53	-3°45'	1°29'
T = 87.5	+78	-4°30'	-44'
E = 3.9	21+02.5	-5°14'	
L = 174.5			

954.93	
.09159	
<u>859437</u>	
477465	
95493	
9437	
<u>87.462038</u>	
95493	
.00419	
<u>859437</u>	
95493	
381972	
<u>390 1567</u>	
17447	
6) 10,4667	
6	
44	
4	
26	
24	
26	
24	
27	

<del>19+28.0</del>	
<del>21+02.5</del>	
<del>74.5</del>	
T = 88.0	

19+27.5 B.C.	
+52.5	-45'
√ +77.5	-1°30' -3°46'
√ 20+02.5	-2°15' 3°01'
√ +27.5	3° -2°46'
+52.5	3°45' -1°31'
+77.5	4°30' -4°46'
21+03.1	-5°16'

0.2	
27.5	
<u>75.6</u>	



4"

265.0

R.P.  $\Delta$  20'  $\Delta$  20'  $\Delta$  R.P.  
90°

Old Sta. 16+98.3

186.3

Old Sta. 14+48.

47.0

R.P.  $\Delta$  15'  $\Delta$  25'  $\Delta$  R.P.  
90°  
RT. Side Rd.

A.

203.5

R.P.  $\Delta$  8.7  $\Delta$  11.55  $\Delta$  R.P.  
90°

90°  
5' 15'  $\Delta$  13'  $\Delta$

Old Sta. 11+98.2

198.6

$\Delta$   
25+77<sup>3</sup> 14°18'K

E=3.7  
T=59.9  
R=477.47  
D=12°  
L=119.2

25+19<sup>3</sup> B.C.

5.88°35'W 15.7

25+01<sup>6</sup> E.C.

E=1.2  
T=24.4  
R=288.75  
D=14°  
L=48.7

$\Delta$   
24+77<sup>3</sup> 11°41'L

24+52<sup>3</sup> B.C.

~~11°41'W~~  
N 11°41'W 180.8

23+49<sup>3</sup> P.O.T.

22+71<sup>2</sup> E.C.

E=4.9  
T=38.6  
R=150.78  
D=38°  
L=25.7

~~22+35° 28° 15'K~~  
~~22+35° 28° 15'K~~

~~21+91<sup>2</sup>~~

~~21+16<sup>2</sup>~~ B.C.

~~5.71°31'W~~ 93.3

21+03<sup>4</sup> E.C.

wed. 1/20/20

20+15<sup>5</sup> 10°32'L

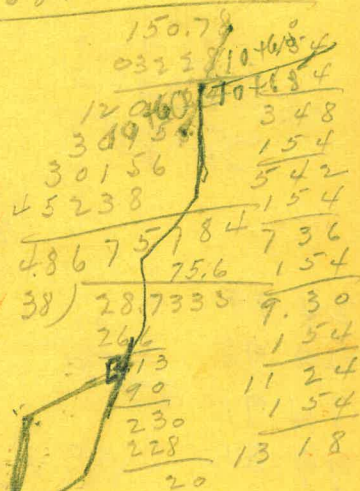
E=4.0  
T=38.0  
R=92.93  
D=6°  
L=175

$\Delta = 28^{\circ} 44'$       25614      12.23  
 $\frac{1}{2}\Delta = 14^{\circ} 22'$       15078      57.27

$D = 38^{\circ}$       20491.2      23.46  
 $R = 150.78$       17.9298      28  
                  1280700  
 $T = 38.6$       25614      22+34.7  
 $E = 4.9$       38.6 207892      33.1  
 $L = 75.6$       21+96.1  
                  75.6

$P.I = 22+34.7$       25614  
                  03228      22+71.7  
 $B.C = 21+96.1$       20491.2      71.7  
                  51228      66.1  
                  51228      5.6  
                  768/42

22+21.1  
 +46.1  
 +71.1  
 21+96.1 B.C.  
 22+06.1 - 1054 ✓  
 +16.1 - 3048 ✓  
 +26.1 - 5042 ✓  
 +36.1 - 7036 ✓  
 +46.1 - 9030 ✓  
 +56.1 - 11024 ✓  
 +66.1 - 13018 ✓  
 +71.7 - 14022 ✓



150.78  
 03228 10+68.4  
 12060 10+68.4  
 30954      348  
 30156      154  
 45238      542  
 48675784      154  
 75.6      736  
 154  
 38) 287335      9.30  
 242      154  
 113      1124  
 90      154  
 230  
 228      131.8  
 20  
 11.4 104  
 5.6  
 684  
 570  
 63.84

23+38  
 10.65 71.7  
 23+48.636.1  
 57.4  
 57.35.6





Old Sta 25+25

1000

R.P. Δ 14 Δ 17 Δ

R.P. Δ 15 Δ 18 Δ R.P.

Old Sta 24+25

23+48.6 P.O.T.

3843

71 35

R.P. Δ 15' Δ 25' Δ 100 18

243.8

900

R.P. 79 42

90°

R.P. Δ 12.6 Δ 17.4 Δ R.P.

Old Sta 21+81

2199

R.P. Δ 15' Δ 15' Δ R.P.

90°

90°

R.P. Δ 17' Δ 17' Δ R.P.

A

32+22<sup>2</sup> ✓ E.C.

E = 2.5  
T = 68.6  
R = 954.93  
D = 6°  
L = 136.9  
C = 186.88

<sup>A</sup> 31+54<sup>2</sup> ✓ 8°13'R

30+85<sup>2</sup> B.C.

14.81°38'N 24.1

30+61<sup>2</sup> E.C.

<sup>A</sup> 29+55<sup>2</sup> ✓ 17°09'R

E = 8.1  
T = 108.0  
R = 716.20  
D = 8°  
L = 216.4

28+47<sup>2</sup> B.C.

5.81°13'N 29.7

28+17<sup>2</sup> E.C.

<sup>A</sup> 27+97<sup>2</sup> ✓ 21°40'L

E = 1.9  
T = 20.3  
R = 106.10  
D = 54°  
L = 401

1/20/26

27+77<sup>2</sup> ✓ B.C.

27+00 P.O.T

N 77°20'W 141.0

26+36<sup>2</sup> ✓ E.C.

<sup>A</sup> 25+77<sup>2</sup> ✓

90°  
Δ 20' Δ 18' Δ

\* Note: Large Oak Tree  
2.5 in Diam. 16 h. Lin. Sta.  
31+72.

11"

200.7

R.P. Δ 20' Δ 20' Δ R.P.

90°

90°

Δ 20' Δ Δ

Note - Large Oak Tree 24

Old Sta 29+00

Sta. 29+42.

158.0

Δ 15' Δ 21' Δ

90°

Δ 15' Δ 21' Δ

11"

221.2

R.P. Δ 14' Δ 22' Δ R.P.

90°

90°

R.P. Δ 15' Δ 30' Δ R.P.

H.

4  
38+53<sup>8</sup> 15°07'R

E = 2.1  
T = 31.7  
R = 288.73  
D = 24°  
L = 63.0

38+12<sup>1</sup> B.C.

N.85°34'W 31.0

37+91<sup>1</sup> E.C.

4  
37+66<sup>5</sup> 21°58'L

E = 2.4  
T = 25.3  
R = 130.24  
D = 44°  
L = 47.2

37+41<sup>2</sup> B.C.

N.63°36'W 35.4

37+05<sup>8</sup> E.C.

4  
36+33<sup>2</sup> 17°27'R

E = 5.6  
T = 79.3  
R = 472.47  
D = 12°  
L = 145.4

35+60<sup>4</sup> B.C.

N.81°03'W 108.1

34+52<sup>3</sup> E.C.

4  
33+57<sup>1</sup> 7°38'L

E = 3.2  
T = 95.6  
R = 1432.4  
D = 4°  
L = 190.2

Jan. 25.

32+61<sup>5</sup> B.C.

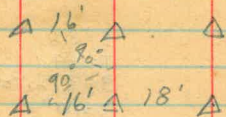
N.73°25'W 38.8

32+22<sup>2</sup> E.C.



A

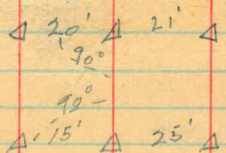
880



$$\begin{array}{r} 358 \\ 37 \\ \hline 1230 \end{array}$$

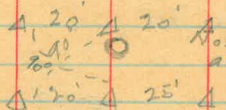
B

1340



C

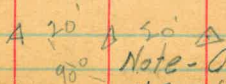
270



Note - Dead Oak Stump  
at Sta. 34+80.

D

2030



Note - Oak Tree 1.0 in Diam  
on Line. Sta. 33+18

Note - Oak Tree 1.8 in Diam  
4'R. Sta. 32+55

46+52<sup>8</sup> BC

N77°09'W 177.3

44+75<sup>5</sup> EC

E=3.6  
T=64.1  
R=572.96  
D=10°  
L=127.7

44+41<sup>9</sup> 12°46'L

43+47<sup>8</sup> BC

N64°23'W 254

43+22<sup>4</sup> EC

E=2.7  
T=39.8  
R=286.48  
D=20°  
L=79.2

42+83<sup>3</sup> 15°48'L

42+43<sup>4</sup> BC

41+73<sup>6</sup> P.O.T. N48°35'W 88.4

41+55<sup>2</sup> EC

E=0.7  
T=29.3  
R=572.96  
D=10°  
L=58.5

41+25<sup>8</sup> 5°51'R

Jan. 26.

40+96<sup>5</sup> BC

N54°26'W 96.3

40+00.2 EC

E=4.0  
T=57.6  
R=409.26  
D=14°  
L=119.4

39+43<sup>4</sup> 16°01'R

38+85<sup>8</sup> B.C.

N70°27'W 0.7

38+85<sup>1</sup> E.C.

38+53<sup>8</sup>

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57.6  
11.0  
46.6  
4.0  
6.6

RP A 15' Δ 24' Δ RP  
20°

117.3

129.3

Old Sta. 42+35.7 Δ - 5.2 Δ Old Sta. 42+35.2

157.5 P.O.T. on Rocky Point.

Old Sta. 40+78.2 Δ - 5.0 Δ Old Sta. 40+78

183.2

Old Sta. 38+95 Δ  
2.2 Δ - 3.5 Δ Old Sta. 38+95

Δ 5.0 Δ 20' Δ  
30°

90.0

LEFAX, PHILADELPHIA, PA.

42

Line should be run along old points

N44°08'W 282.2

57+34<sup>1</sup> EC

E = 7.2  
T = 83.5  
R = 477.47  
D = 12.0  
L = 165.3

56+52<sup>2</sup> 19°50'R

55+69<sup>4</sup> BC

N63°58'W 186.5

53+82<sup>7</sup> E.C.

E = 4.5  
T = 57.0  
R = 358.1  
D = 16°  
L = 113.0

53+26<sup>2</sup> 18°05'R

52+69<sup>2</sup> BC

N82°03'W 127.0

51+42<sup>7</sup> 2°43'L

N79°20'W 168.8

49+74<sup>1</sup> EC

E = 1.0  
T = 19.2  
R = 179.05  
D = 32°  
L = 38.3

49+55<sup>2</sup> 12°15'L

49+35<sup>2</sup> BC

N67°05'W 107.5

48+28<sup>2</sup> EC

E = 4.5  
T = 40.3  
R = 179.05  
D = 32°  
L = 79.3

47+89<sup>2</sup> 25°22'R

47+49<sup>2</sup> BC

S87°33'W 56.9

46+92<sup>1</sup> EC

E = 1.3  
T = 19.8  
R = 150.78  
D = 38°  
L = 39.3

46+72<sup>2</sup> 14°57'L

4

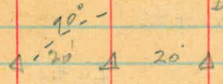
Jan 27



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LEFAX FILING INDEX

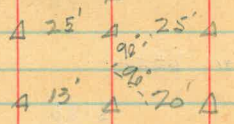
Note Oak Tree 15' in Diam. 1' L. Sta. 57+42.



Old Sta 56+02

Old Sta 56+02

327.0



Note Oak Tree 15' in Diam. 1' L. Sta. 54+85

Old Sta 52+75

Old Sta 52+75

134.0



A



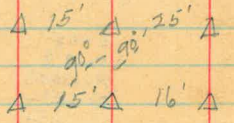
188.0



Note Oak Tree 3' in Diam. on Line Sta. 49+30 Oak Tree 12" Diam 1' L. Sta. 49+20

"B"

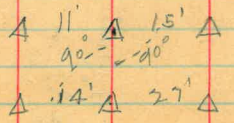
167.0



Note Oak Tree 14" in Diam. 1' R Sta. 48+67

"C"

117.0



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2612 "J"

72+35<sup>±</sup> EC N87°17'W 48.2

E=8.0  
T=59.8  
R=220.37  
D=26°  
L=116.9

71+78<sup>±</sup> 30°23'R

71+18<sup>±</sup> B.C.

70+20<sup>±</sup> EC

E=2.6  
T=20.0  
R=75.39  
D=76°  
L=39.1

70+00<sup>±</sup> 29°41'L

69+80<sup>±</sup> B.C.

67+38<sup>±</sup> E.C.

E=14.5  
T=97.3  
R=318.31  
D=18°  
L=188.9

66+46<sup>±</sup> 34°00'L\*

65+49<sup>±</sup> B.C.

61+55<sup>±</sup> EC

N53°59'W 394.2

Jan. 28.

E=1.5  
T=19.9  
R=130.22  
D=44°  
L=39.5

61+35<sup>±</sup> 17°24'L\*

61+15<sup>±</sup> B.C.

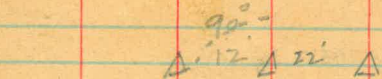
61+11<sup>±</sup> EC

N36°35'W 4.3

E=1.6  
T=47.3  
R=716.2  
D=8°  
L=94.4

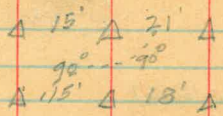
60+64<sup>±</sup> 7°33'R\*

60+16<sup>±</sup> BC



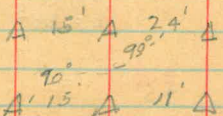
Old Sta 71+06  
 Old Sta 71

178.0 ✓



"A"

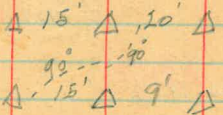
360.0 ✓



Oak 12" in Diam. on  
 Line 66+30  
 Oak 2' in Diam. on  
 Line Sta 66+05.

"B"

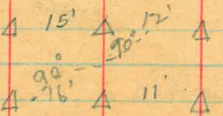
511.4 ✓



Note Oak Tree 14"  
 in Diam. 1/2 Sta 65+50

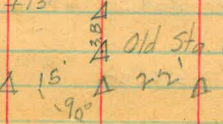
"C"

71.5 ✓



Old Sta 60+15

413.0 ✓



Old Sta 60+15



85+93<sup>3</sup> 3°06'L

N62°15'W 196.0

83+97<sup>3</sup> E.C.

E=1.0  
T=20.0  
R=204.63  
D=28°  
L=39.8

83+77<sup>5</sup> 11°09'R

83+57<sup>5</sup> B.C.

N73°24'W 220.7

81+36<sup>9</sup> E.C.

E=7.9  
T=95.5  
R=572.96  
D=10°  
L=189.3

80+43<sup>9</sup> 18°56'L

Feb. 2

79+47<sup>5</sup> B.C.

79+42<sup>7</sup>  
79+44<sup>5</sup> E.C.

N54°28'W  
N54°45'W

3.8  
3.0

78+61<sup>9</sup> 35°45'R

78+47<sup>9</sup> 36°02'R

E=16.4  
T=103.5  
R=318.31  
D=18°  
L=200.2

E=13.2  
83.9

269.44  
29.

162.5

77+78<sup>9</sup>

77+44<sup>3</sup> B.C.

389°30'W 150.9  
117.2

Feb. 1

76+27<sup>1</sup> E.C.

E=0.7  
T=19.8  
R=286.48  
D=20°  
L=39.6

76+07<sup>3</sup> 7°55'L

75+87<sup>5</sup> B.C.

N82°35'W 40.2

75+37<sup>0</sup> P.O.T.

N82°35'W 264.0

72+83<sup>3</sup> 4°42'R

72+35<sup>1</sup> E.C.

48.2



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$\Delta$   
80+43°

T=75.5

79+67° B.C.

N.54°28'W 3.8

79+43° = E.C.  
79+40° = P.O.S.T

$\Delta$   
78+61° 35'45" R  
77+96° P.O.S.T

E=  
T=83.9  
R=318.31  
D=22°  
L=162.5

77+78° B.C.

S.89°30'W

71° 29'	36	02
35° 45'	35	45
	<hr/>	
	17	

Old Sta. 79+80

New Line P.I 78+61.9 =  
 Old Line P.O. 77+96.8

202.0
<hr/>
180.8
21.2

77+78.8  
Old Sta

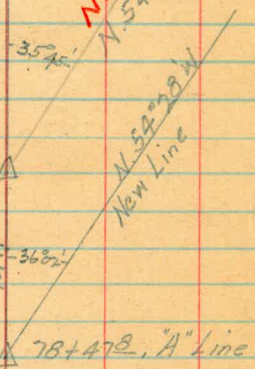
Old Sta. 77+96.8

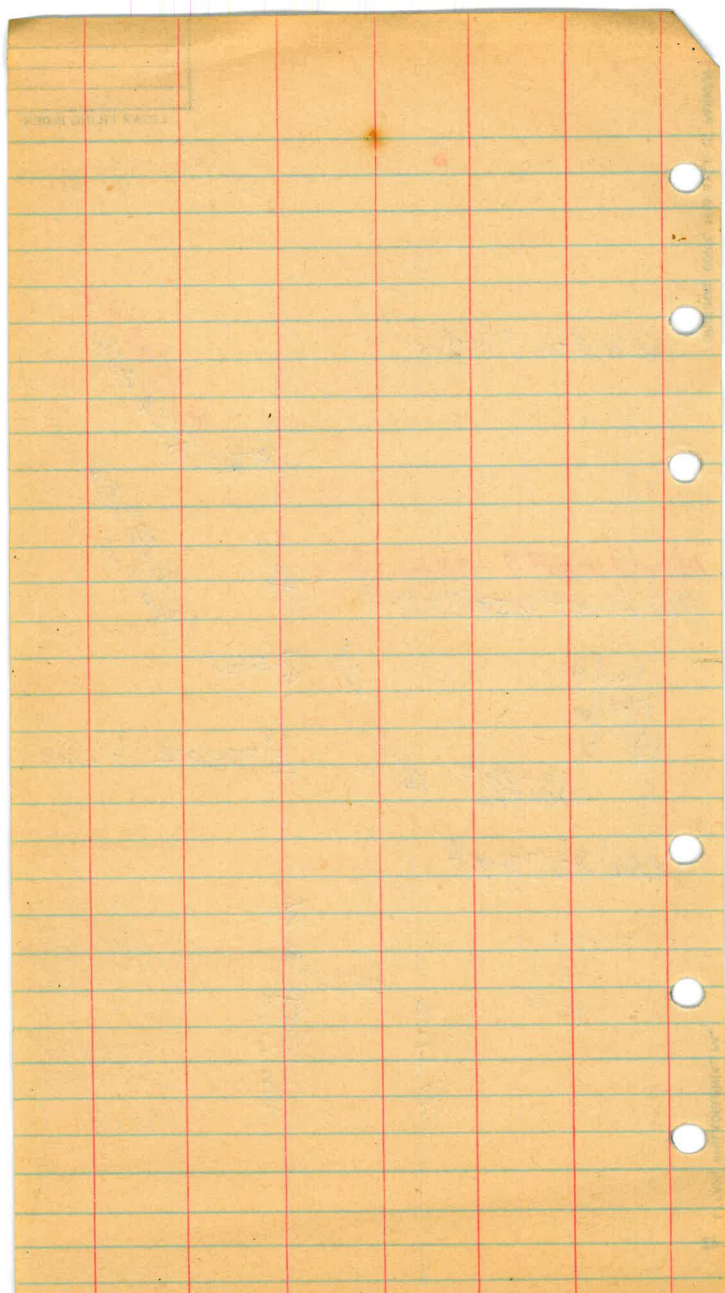
77+78
1 18.8
<hr/>
77 96.8

Old Line

4 R.I. 720° 30' W.  
 New Line

89	30
35	20
<hr/>	
54	10
<hr/>	
54	45
	<hr/>
78+47.8	
	14.1
	<hr/>
78+61.9	









91+62.7			25	
+87.7	1°15'		49.99	
92+12.7	2°30'		74.94	
+37.7	3°45'		99.88	
+62.7	5°	4°18'	5°33'	
+87.7	6°15'	3°03'	148	
93+12.7	7°30'	1°48'	115	
+37.7	8°45'	0°33'	303	
93+48.7	9°18'		115	

$\frac{277}{11.0}$        $\frac{33}{33}$   
 533

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Old Sta 85+36.8

216.0

"H" R.P. Δ 20' Δ 20' Δ R.P.  
92°

336.2

Δ 20.0 Δ 48.0 Δ

50.5  
19.8  
70.3

Old Sta 79+80

202.0

Δ 17.0 Δ 18.0 Δ In Road  
Δ 15.0 Δ 17' Δ In Road

Old Sta 77+78 11.8

240.5

Δ 20' Δ 20' Δ In Road  
90° - 90°  
R.P. Δ 14' Δ 16' Δ Note E.C. Oak Tree 30" in Diam  
on Rock

"H"

60.0

Δ 12' Δ 21' Δ  
-90°

Note B.C. in Crotch.  
Oak Tree 36" in Diam

Old Sta 74+78

264.9

Old Sta 72+14 R.P. Δ 20' Δ 21' Δ R.P.  
48.2  
-90°

108.0

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106+49<sup>5</sup> EC

E=1.8  
T=45.3  
R=572.96  
D=10°  
L=90.5

106+04<sup>9</sup> 9°03'R

105+59<sup>1</sup> B.C.

N81°31'W 268.3

102+90<sup>8</sup> 2°07'L

N79°24'W 295.0

99+95<sup>8</sup> P.O.T.

N79°24'W ~~362.5~~ 67.3

99+28<sup>5</sup> E.C.

E=7.5  
T=69.7  
R=318.31  
D=18°  
L=137.3

98+60<sup>2</sup> 24°43'L

97+91<sup>2</sup> B.C.

N54°41'W 144.3

96+46<sup>7</sup> E.C.

E=3.4  
T=99.3  
R=1482.40  
D=4°  
L=198.3

95+97<sup>3</sup> 7°56'L

94+48<sup>8</sup> BC = 94+34<sup>6</sup>

94+40<sup>7</sup> P.O.T. =

94+54<sup>9</sup> P.O.T. =

93+48<sup>2</sup> EC

N46°45'W 97.9 85.9

E=7.6  
T=98.8  
R=572.96  
D=10°  
L=186.0

92+56<sup>5</sup> 18°36'R

91+62<sup>3</sup> BC.

90+0<sup>4</sup> P.O.T. N65°21'W 569.4

85+92<sup>3</sup> 3°06'L

Jan. 30.



Δ 11' Δ 13' Δ

Old Sta 105+46

Old Hub 1.1 Rt.  
Sta. 106+00 ±

312.6

Δ 15' Δ 17' Δ

Old Hub 0.7 Rt.  
Sta. 102+90 ±

Old Sta 102+30 Δ 19.6 Δ 24.0 Δ

295.0

Old Sta. 99+35

137.0

Δ 15' Δ

Note Oak Tree 18"  
Diam. I.R. Sta. 98+30.  
Oak Tree 30"  
in Diam. I.R. Sta. 98+60

"H"

Δ 12.1 Δ 15' Δ

313.3

Δ 15' Δ 20' Δ

"B"

93.0

Δ 15' Δ 12' Δ

Old Sta 94+00

Note. Mistake of 14 ft. in  
Chaining on Bowens Line

200.0  
~~186.0~~

Δ 15' Δ 20' Δ

Old Sta 92+00

663.2

Δ 15' Δ Δ

Δ 10' Δ 15' Δ

126+90<sup>3</sup> 17°03' L

E=11.7  
T=98.4  
R=409.26  
D=14°  
L=193.2

125+91<sup>3</sup> B.C.

5.7142W 197.2

123+94<sup>2</sup> E.C.

E=7.7  
T=148.4  
R=1632.40  
D=4°  
L=395.8

122+97<sup>3</sup> 11°50' L

120+98<sup>2</sup> B.C.

5.8332W 447.0

116+51<sup>3</sup> E.C.

E=0.8  
T=19.6  
R=238.73  
D=24°  
L=39.0

116+32<sup>5</sup> 9°22' L

116+12<sup>3</sup> B.C.

N.87°06'W 16.5

115+96<sup>4</sup> E.C.

E=19.6  
T=91.6  
R=204.63  
D=23°  
L=172.3

115+15<sup>2</sup> 48°14' L

114+24<sup>4</sup> B.C.

N.38°52'W 102.6

113+21<sup>5</sup> 4°38' L

N.34°14'W 282.5

110+39<sup>2</sup> E.C.

E=33.4  
T=198.6  
R=572.96  
D=10°  
L=582.3

108+55<sup>3</sup> 38°14' R

Feb. 4.

106+56<sup>7</sup> B.C.

N.72°28'W 7.1

106+49<sup>6</sup> E.C.

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Old Sta 85+36.8

216.0

"H" R.P.  $\Delta$  20'  $\Delta$  20'  $\Delta$  R.P.

336.2

 $\Delta$  20.0  $\Delta$  30.0  $\Delta$ 50.5  
19.0  
70.3

Old Sta 79+80

202.0

 $\Delta$  13.0  $\Delta$  18.0  $\Delta$  In Road $\Delta$  15.0  $\Delta$  17'  $\Delta$  In Road

Old Sta 77+78.11.2

240.5

 $\Delta$  20'  $\Delta$  20'  $\Delta$  In Road

90° - 90°

R.P.  $\Delta$  14'  $\Delta$  16'  $\Delta$   
on RockNote E.C. 1/8" Oak  
Tree 30" in Diam

"H"

60.0

 $\Delta$  12'  $\Delta$  21'  $\Delta$ 

90°

Note E.C. in Crotch  
Oak Tree 36" in Diam

Old Sta 74+78

264.0

Old Sta 72+14 R.P.  $\Delta$  20'  $\Delta$  21'  $\Delta$  R.P.

105.0

 $\Delta$  8.2  $\Delta$  90°

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106+495 E.C.

E=1.8  
T=45.3  
R=572.96  
D=10°  
L=90.5

106+041 9°03'R

105+591 B.C.

N81°31'W 268.3

102+908 2°07'L

N79°24'W 295.0

99+958 P.O.T.

N79°24'W ~~262.3~~ 67.3

99+285 E.C.

E=7.5  
T=69.7  
R=918.31  
D=18°  
L=137.3

98+602 24°43'L

97+912 B.C.

N54°41'W 144.3

96+462 E.C.

E=8.4  
T=99.9  
R=1482.40  
D=4°  
L=198.3

95+472 7°56'L

94+482 BC = 94+342

94+402 P.O.T. =

94+542 P.O.T. =

93+482 E.C.

N46°45'W 77.9 85.9

E=7.6  
T=93.8  
R=572.96  
D=10°  
L=186.0

92+565 18°36'R

91+622 B.C.

90+202 P.O.T. N65°21'W 569.4

85+923 3°06'L

Jan. 30.



Old Sta 85+36.8

216.0

"H" R.P.  $\Delta$  20'  $\Delta$  20'  $\Delta$  R.P.  
90°

336.2

 $\Delta$  20.0  $\Delta$  20.0  $\Delta$ 50.5  
19.8  
70.3

Old Sta 79+80

202.0

 $\Delta$  13.0  $\Delta$  18.0  $\Delta$  In Road $\Delta$  15.0  $\Delta$  17'  $\Delta$  In Road  
90°

Old Sta 77+78 11.2

240.5

 $\Delta$  20'  $\Delta$  20'  $\Delta$  In Road  
90° - 90°R.P.  $\Delta$  14'  $\Delta$  16'  $\Delta$   
on RockNote E.C. I.R. Oak  
Tree 30" in Diam

"H"

60.0

 $\Delta$  12'  $\Delta$  21'  $\Delta$   
-90°Note E.C. in Crotch  
Oak Tree 36" in Diam

Old Sta 74+78

264.0

Old Sta 72+14 R.P.  $\Delta$  20'  $\Delta$  21'  $\Delta$  R.P.  
4.82

105.0

90°

106+49<sup>2</sup> EC

E=1.8

T=45.3

106+044 9°03'R

R=572.96

D=10°

L=90.5

105+59<sup>2</sup> B.C.

N81°31'W 268.3

102+90<sup>2</sup> 2°07'L

N79°24'W 295.0

99+95<sup>2</sup> P.O.T.

N79°24'W ~~362.5~~ 67.3

99+28<sup>2</sup> EC

E=7.5

T=69.7

98+60<sup>2</sup> 24°43'L

R=318.31

D=18°

L=137.3

97+91<sup>2</sup> B.C.

N54°41'W 144.3

96+46<sup>2</sup> EC

E=3.4

T=99.3

95+47<sup>2</sup> 7°56'L

R=1482.40

D=4°

L=198.3

94+48<sup>2</sup> BC = 94+34<sup>2</sup>

94+40<sup>2</sup> P.O.T. =

94+54<sup>2</sup> P.O.T. =

93+48<sup>2</sup> EC

N46°45'W 77.9

E=7.6

T=93.8

92+56<sup>2</sup> 18°36'R

R=572.96

D=10°

L=186.0

94+62<sup>2</sup> B.C.

90+94<sup>2</sup> P.O.T.

N65°21'W 569.4

85+93<sup>2</sup> 3°06'L

Jan. 30.

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444.0

△ 20' △ 20' △

116+12.9

△ 20' △ 20' △

19.5

32.4

Old Sta. 122+15

Old Hub

△ 20' △ 25' △

615.0

Old Hub 2.8' back of new Hub.

Old Sta. 116+00

△ 20' △ 30' △

127.7

127.0 on Old Line.

△ 25' △ 35' △

Old Sta. 114+72

△ 15' △ 15' △

194.2

1.8 Rt. New Hub

Old Sta. 112+78

△ 17' △ 36' A.R.P. on Rock

451.1

△ 15' △ 20' △

Old Sta. 107+97

1.5 Rt. New Hub

Old Hub 1.5 Rt.  
10.8+5.5=3

251.0

△ 15' △ 12' △

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148+90<sup>2</sup> 240'R

E=5.3  
T=50.8  
K=238.73  
D=2A°  
L=100.1

143+47<sup>2</sup> E.C.

5.2903N 633.8

142+14<sup>2</sup> E.C.

E=16.3  
T=103.7  
K=318.81  
D=18°  
L=177.5

141+17<sup>2</sup> 3555'R

140+14<sup>2</sup> B.C.

5.652'E 190.6

138+12<sup>2</sup> E.C.

E=22.3  
T=98.2  
K=204.63  
D=28°  
L=183L

137+39<sup>2</sup> 5176'L

136+40<sup>2</sup> B.C.

5.4434N 137.9

135+103<sup>2</sup> E.C.

E=1.1  
T=38.9  
K=516.2  
D=8°  
L=77.7

134+64<sup>2</sup> 673'R

134+25<sup>2</sup> B.C.

5.3811N 75.0

133+50<sup>2</sup> E.C.

E=0.7  
T=23.1  
K=409.26  
D=14°  
L=46.2

133+27<sup>2</sup> 628'L

133+04<sup>2</sup> B.C.

5.4439N 519'

127+85<sup>2</sup> E.C.

126+90<sup>2</sup>

FEB 5,



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LEFAX, PHILADELPHIA, PA.

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145+86<sup>2</sup> P.O.T

5.40<sup>29</sup>W

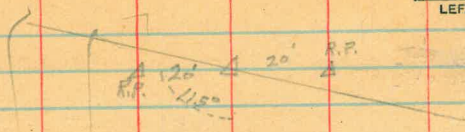
<sup>A</sup>  
136+01<sup>2</sup> L 3.55'

135+03<sup>2</sup>

5.47<sup>24</sup>W 98.0

135+03<sup>2</sup>

134+64<sup>2</sup> P.I



P.I. 136+01 = New Line  
 R.A.T. 136+04 = Old Sta. =

R.P. 18' 30' R.P.  
 90°

Old Sta. 135+83.7 FT



159474<sup>2</sup> P.O.T.

152460<sup>2</sup> P.O.T.

5.40<sup>2</sup> 29m

152457<sup>2</sup> P.O.T.

145486<sup>2</sup> P.O.T.



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42

R.P.  
A 20' A 20' R.P.  
- 20 - 20 -

173+45<sup>2</sup> B.C. =  
168+53<sup>2</sup> B.C. 0.7  
173+44<sup>2</sup> P.O.T. =  
168+53<sup>2</sup> E.C. =

P.I.  
168+33<sup>2</sup> 1723R

E=114.59  
R=19.6  
D=50°  
L=38.8

168+14<sup>2</sup> B.C.

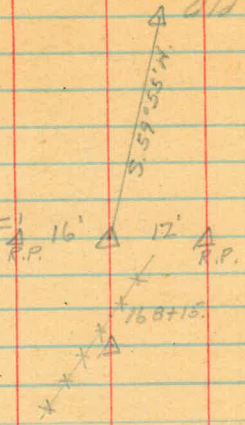
159+77<sup>2</sup> P.O.T.

540<sup>2</sup> in

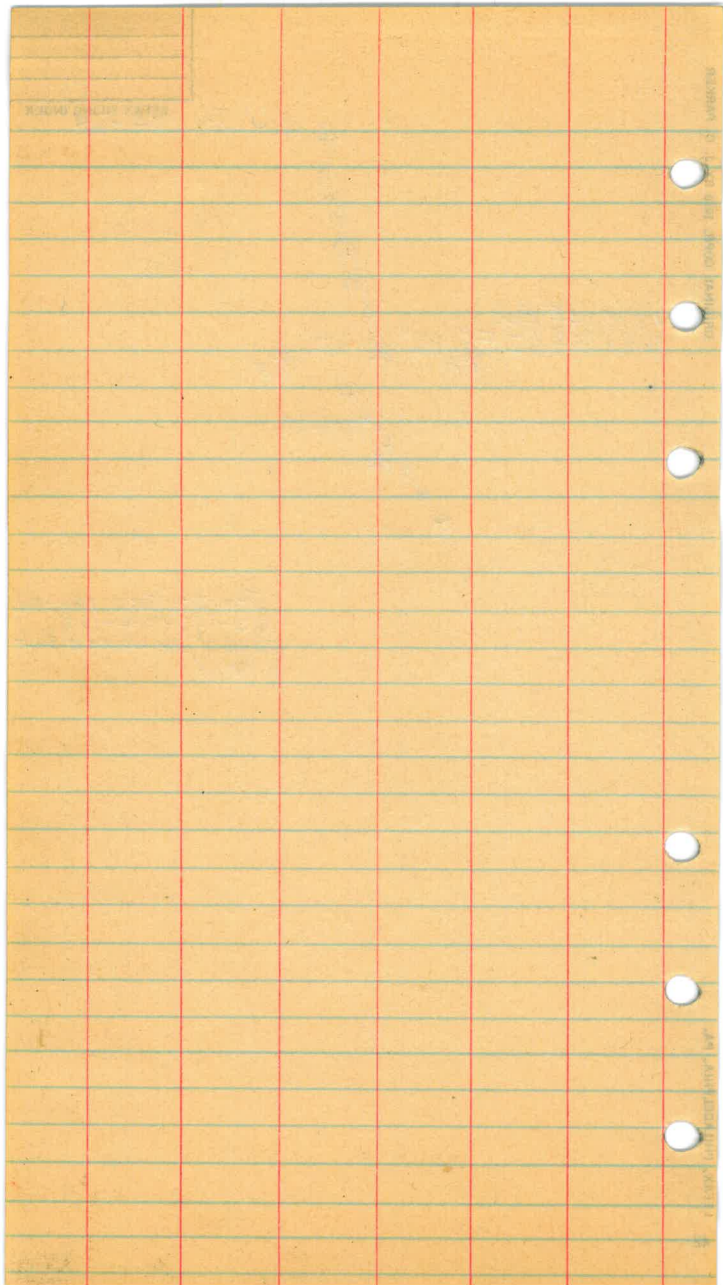
159+74<sup>2</sup> P.O.T.

Old Sta. 160-161

173+24<sup>9</sup> E.C.  
168+33<sup>2</sup> P.T.



Sta. Sta. Res. 160-161  
162-163-164-165  
Should be moved 3 ft  
ahead.





Old Sta. 150+85.

187.8

Old Sta. 141+00

372.0

Old Sta. 137+08.

275.0

△ 15' △ 35' △

Old Sta. 134+33 P.O.T

137.0

△ 20' △ 35' △

A.

△ 15' △ 23' △

640.5

△ 20' △ 20' △

161+15<sup>±</sup> B.C.

5.33°37'W 50.9

160+64<sup>±</sup> E.C.

E = 4.0  
T = 57.3  
R = 409.26  
D = 14°  
L = 113.8

160+08<sup>±</sup> 15°56'L

157+50<sup>±</sup> B.C.

5.49°33'W 232.6

157+18<sup>±</sup> E.C.

E = 4.6  
T = 42.1  
R = 190.77  
D = 30°  
L = 82.8

156+17<sup>±</sup> 24°51'R

156+35<sup>±</sup> B.C.

5.24°42'W 264

156+08<sup>±</sup> E.C.

E = 2.6  
T = 40.5  
R = 318.31  
D = 18°  
L = 80.6

155+68<sup>±</sup> 14°31'L

155+28<sup>±</sup> B.C.

5.39°13'W 118.5

154+09<sup>±</sup> 3°36'L

5.42°39'W 345.6

150+64<sup>±</sup> E.C.

E = 2.4  
T = 52.2  
R = 572.16  
D = 10°  
L = 104.2

150+12<sup>±</sup> 10°25'L

149+60<sup>±</sup> B.C.

5.53°04'W 12.0

149+48<sup>±</sup> E.C.

148+98<sup>±</sup>

Old Sta. 762+00

332.0

Old Sta. 158+68

109.0

Old Sta. 152+59

157.0

Old Sta. 156+00

397.8

Old Sta. 152+00

115.0

✓  
173+24<sup>9</sup> E.C.  
168+338 P.I. =

E=5.4  
T=39.7  
R=143.24  
D=40°  
L=77.4

172+87<sup>2</sup> 30°57'

172+47<sup>5</sup> B.C.

N.89°11'N 2.3

172+45<sup>2</sup> E.C.

E=7.1  
T=51.0  
R=179.05  
D=32°  
L=97.4

171+96<sup>8</sup> 31°48'

171+45<sup>8</sup> B.C.

N.57°23'N 27.1

171+18<sup>2</sup> E.C.

E=20.6  
T=60.9  
R=79.58  
D=72°  
L=104.0

170+75<sup>6</sup> 74°53'R

170+14<sup>2</sup> B.C.

5.47°44'N 168.0

168+46<sup>2</sup> E.C.

166+46<sup>2</sup> E.C.

E=7.8  
T=106.1  
R=716.2  
D=8°  
L=210.6

165+42<sup>2</sup> 16°51'L

164+36<sup>4</sup> B.C.

5.64°35'N 99.5

163+36<sup>6</sup> E.C.

E=15.4  
T=113.4  
R=409.26  
D=14°  
L=221.2

162+28<sup>8</sup> 30°50'R

161+15<sup>4</sup> B.C.



221.6 A

319.0

Old Sta. 167+33

335.0

Old Sta. 170+68

139.0

Old Sta. 172+07

93.0

Old Sta. 173+00

221+41<sup>B</sup> B.C.

N49°32'W 378.9

217+62<sup>A</sup> E.C.

216+96<sup>A</sup> 45°20'R

E=15.0  
T=74.8  
R=179.05  
D=32°  
L=141.7

216+21<sup>B</sup> B.C.

S85°08'W 1011.4

206+09<sup>B</sup> E.C.

205+17<sup>B</sup> 47°23'R

E=22.0  
T=104.8  
R=238.73  
D=24°  
L=197.4

Feb. 8.

204+12<sup>A</sup> B.C.

192<sup>Top</sup> P.O.T. S37°45'W 1829.4

185+83<sup>B</sup> 1°26'R

S36°19'W 300.0

182+83<sup>B</sup> 3°15'R

S33°04'W 179.1

181+03<sup>B</sup> E.C.

179+83<sup>B</sup> 9°39'L

E=5.1  
T=120.9  
R=1432.4  
D=4°  
L=241.2

178+62<sup>A</sup> B.C.

S42°43'W 303.1

175+59<sup>B</sup> E.C.

174+53<sup>B</sup> 17°09'L

E=8.1  
T=108.0  
R=716.2  
D=8°  
L=214.4

Feb. 6

173+45<sup>B</sup> B.C.

168+53<sup>B</sup> B.C. S59°52'W 20.3

173+24<sup>B</sup> E.C.

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Line to Close RR  
Revestment at this Pt.

△ 31' △ 10' △

△ 25' △ 14' △

Old Sta 218+25

POT 209+00  
POT 213+00

1191.0

△ 25' △ 12'

△ 27' △ 10' △

Old Sta 206+34

P.O.T. 199+00  
199+00  
205+00

1934.2

△ 26' △ 10' △

△ 32' △ 9' △

Old Sta 186+00  
33' △ 10' △

Old Hub 1.3 ft. Rt.

Old Sta 183+00  
10' △ 10' △

Old Hub 1.0 ft. Rt.

300.0

△ 11' △ 8' △

Old Sta 180+00

Old Hub 2.6 ft. Rt.

532.0

△ 15' △ 8' △

△ 10' △ 10' △

Old Sta 174+68

168.0

△ 10' △ 11' △

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42

234+183 B.C.

532°28'N 37.9

233+80<sup>2</sup> E.C.

E = 5.5  
T = 79.8  
R = 572.16  
D = 10  
L = 158.5

233+02<sup>2</sup> 15°51' L

232+22<sup>2</sup> B.C.

548°9'N 13.7

232+08<sup>2</sup> E.C.

E = 3.1  
T = 38.5  
R = 143.24  
D = 40  
L = 75.3

231+71<sup>2</sup> 30°07' L

231+33<sup>2</sup> B.C.

578°26'W 259.9

228+73<sup>2</sup> E.C.

E = 9.9  
T = 52.8  
R = 126.64  
D = 42  
L = 100.7

228+125<sup>2</sup> 42°18' L

Feb. 9

227+72<sup>2</sup> B.C.

459°16'W 187.4

225+85<sup>2</sup> E.C.

E = 13.2  
T = 51.8  
R = 95.49  
D = 60  
L = 95.0

225+42<sup>2</sup> 57°0' R

224+90<sup>2</sup> B.C.

563°44'W 225.0

222+65<sup>2</sup> E.C.

E = 20.9  
T = 62.9  
R = 106.1  
D = 54  
L = 123.6

222+11<sup>2</sup> 66°44' L

221+41<sup>2</sup> B.C.



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LEFAX FILING INDEX

120  
57  
123

195

Δ 35 Δ 9' Δ  
Δ 30' Δ 11' Δ

Old Sta. 234+55 Old Hub. 6.5' Rt.

132

Δ 27' Δ 12' Δ  
Δ 24' Δ 12' Δ

Old Sta 233+23 P.O.T.

351.2

Δ 28.5 Δ 10' Δ  
Δ 10' Δ 10' Δ

Note: 12" On K 5' Rt  
Sta. 228+73<sup>E</sup>

A

292.0

Δ 15' Δ 15' Δ  
Δ 15' Δ 21' Δ

Old Sta 226+81

3467

Δ 30' Δ 13' Δ  
Δ 32' Δ 12' Δ

" H "

5236

LEFAX, PHILADELPHIA, PA.

42

256+01<sup>2</sup>

~~256+01~~ B.C.

577°10'W 730.9

724

248+77.6 E.C.

E=2.4 ✓  
T=83.0 ✓  
R=1432.40 ✓  
D=4° ✓  
L=165.8 ✓

247+94.2 E 6°38'R

247+11.8 D.C.

570°32'W 87.4

246+29<sup>2</sup> E.C.

E=5.3 ✓  
T=61.6 ✓  
R=358.7 ✓  
D=16° ✓  
L=122.1 ✓

245+63.2 19°32'R

Feb. 10

245+62<sup>2</sup> B.C.

551°0'W 372.0

241+30<sup>2</sup> E.C.

(8)  
E=8.0 ✓  
T=81.4 ✓  
R=409.22 ✓  
D=14° ✓  
L=160.7 ✓

240+51<sup>2</sup> 22°30'L

239+61<sup>2</sup> B.C.

523°30'W 151.4

238+18<sup>2</sup> E.C.

E=20.0 ✓  
T=62.2 ✓  
R=86.81 ✓  
D=66° ✓  
L=107.9 ✓

237+72<sup>2</sup> 71°14'R

237+10<sup>2</sup> B.C.

52°16'W 140.5

235+69<sup>2</sup> E.C.

(17)  
E=10.2 ✓  
T=77.3 ✓  
R=286.78 ✓  
D=20° ✓  
L=151.0 ✓

234+96<sup>2</sup> 30°22'L

234+188 B.C.

883  
876.3

△ 20' △ 9' △

Old Sta. 249+72

Old Hub. 18.5 ft. Rt.

232

△ 23' △ 15' △

△ 30' △ 20' △

Old Sta. 247+40

Old Hub. 8.1 ft. Rt.

515

△ 20' △ 10' △

△ 15' △ 15' △

Old Sta. 242+25

295

△ 23' △ 22' △

△ 17' △ 20' △

Old Sta. 239+30

280

△ 20' △ 21' △

△ 31' △ 10' △

Old Sta. 236+50

Old Hub. 6.7 ft.

195

△ 15' △  
SX



S53°42'W 1819

279+44<sup>3</sup> E.C

③  
E=2.3  
T=40.6  
R=358.10  
D=16°  
L=80.8

279+04'1256 L

278+63<sup>5</sup> B.C

S66°38'W 221.2

276+42<sup>3</sup> E.C

②  
E=6.7  
T=88.2  
R=372.72  
D=10°  
L=175.00

275+55<sup>5</sup> 1730R

Feb. 16.

274+67<sup>3</sup> B.C

S49°08'W 121.1

273+46<sup>3</sup> E.C

①  
E=7.1  
T=90.7  
R=572.96  
D=10°  
L=179.8

272+57'17°59' L

271+66<sup>4</sup> B.C

S67°07'W 921.4

260+45<sup>3</sup> E.C

④  
E=10.0  
T=37.9  
R=66.62  
D=86°  
L=68.9

262+45°

260+14°59'17' L

259+76<sup>4</sup> B.C

N63°36'W 238.0

257+31<sup>6</sup> E.C

N53°30'W

⑤  
E=15.1  
T=69.1  
R=150.78  
D=38°  
L=129.6

15.1

69.2

150.78

38°

129.6

257+38<sup>5</sup> E.C

256+72.6 49'14R

256+01<sup>2</sup> B.C

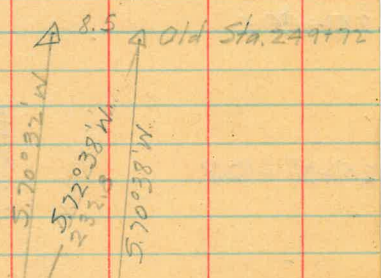
256+08.5 B.C



$$\begin{array}{r}
 51 \\
 21^{\circ} 38' \\
 \hline
 72^{\circ} 38'
 \end{array}$$

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247+94.8



245+63.9

8.1 Old Sta. 247+40

N. 53° 30' W

257+31<sup>A</sup>E.C.

~~PT~~  
256+70<sup>B</sup> 492<sup>A</sup>R.

E =  
T = 69.2  
R = 130.78  
D = 30°  
L = 129.7

256+01<sup>B</sup> B.C

N. 77° 10' W

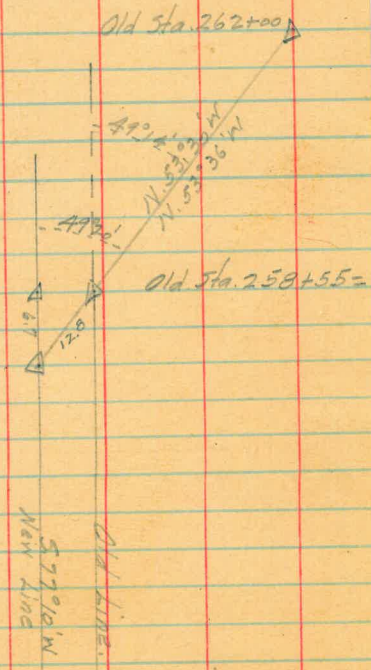
69.2	7	10
12.8	49	20
<u>56.4</u>	180	
	126	30
238.0	53	30

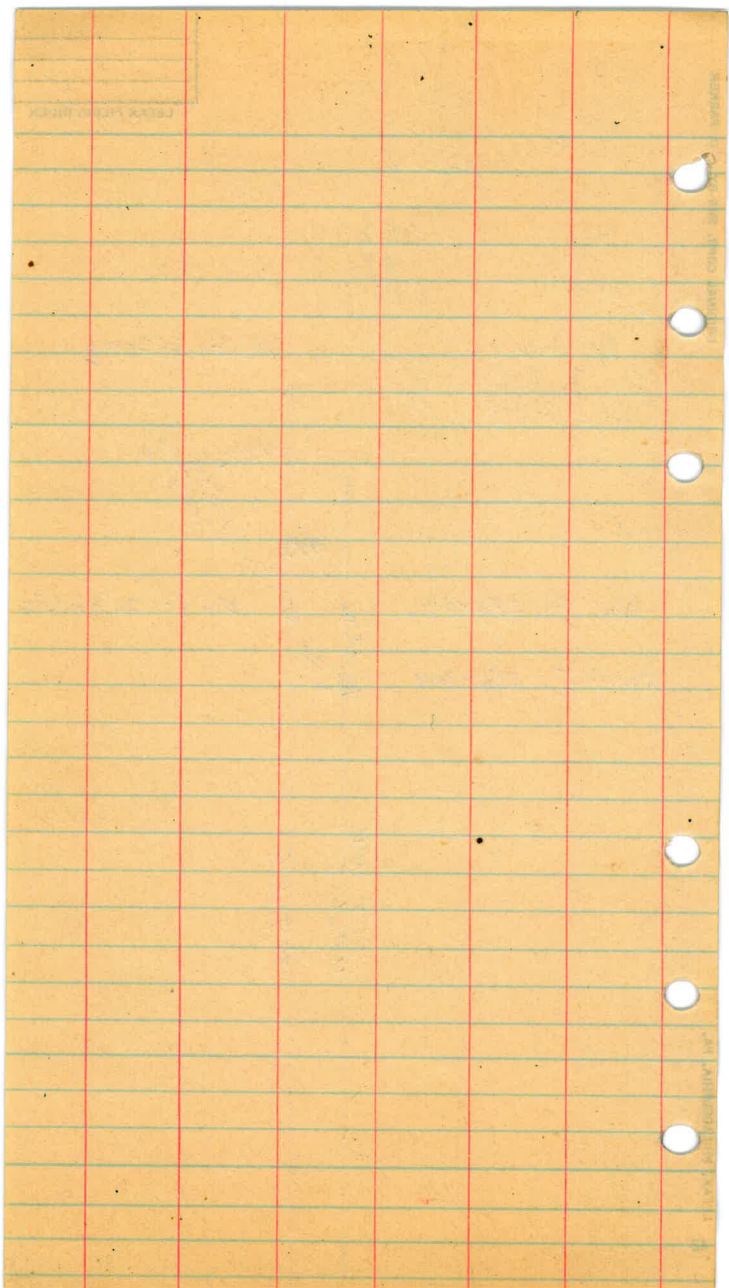
77.6
6.7
70.9

345	357.8
12.8	69.1
<u>357.8</u>	288.7

260+14.0
2 88.7
<u>257 25.3</u>

New Sta. 256+77.6  
 New P.I. 256+70.9







300.0

Nail in Rock Wall  
8.14 Δ 17.0 Δ

Old Sta 279+00 Δ 8.0 Δ 18.0 Δ

Nail in R.R. Wall  
86.4'

350.0

Δ 20' Δ 11.0 Δ

Old Sta. 275+50

300.0

Δ 20' Δ 19' Δ

Δ 11.0 Δ 25' Δ

Old Sta. 272+50

Nail in Rock Wall  
14.7 Δ 22' Δ Hub.  
74<sup>00</sup> Δ

1050.0

Old Sta. 262+00

R.P.A. Nail in Rock Wall  
19.9 Δ 25' Δ R.P.  
90.8'

257+25.4 P.O.S.T.  
257+31.4 EC -

345.0  
357.8

Δ 43' Δ Δ

Old. 25B+55

Δ 9.9

Old Sta 258+55

883.0  
876.3

Δ 27' Δ 20' Δ

297199° E.C. S78°58'W 331.6

E=1.8 ✓

T=44.8 ✓

R=572.96 ✓

D=10° ✓

L=89.5 ✓

297154° 857'R

297109° B.C.

S70°01'W 142.9

295166° E.C.

E=8.3 ✓

T=69.3 ✓

R=286.48 ✓

D=20° ✓

L=136.0 ✓

294197° 2712'R

294130° B.C.

S42°49'W 568.6

288162° E.C.

E=1.0 ✓

T=28.1 ✓

R=409.25 ✓

D=14° ✓

L=56.1 ✓

288134° 751'L

288105° B.C.

S50°40'W 260.2

285145° E.C.

E=12.3 ✓

T=84.7 ✓

R=286.48 ✓

D=20° ✓

L=164.8 ✓

284165° 3257'R

283180° B.C.

S17°43'W 104.8

282176° E.C.

E=12.3 ✓

T=77.5 ✓

R=238.73 ✓

D=24° ✓

L=149.9 ✓

282103° 3559'L

281126° B.C.

S53°42'W 181.9

Feb. 17.

437.0

Δ 15.0 Δ 18.0 Δ

Old Sta. 297+63 Old Hub. 0.15 ft. RT.

257.0

Δ 11.0 Δ 20.0 Δ

Δ 13 Δ 21 Δ

Old Sta. 295+06 Old Hub. 0.1 ft. RT.

666.0

Δ 11.0 Δ 20' Δ

Old Sta. 288+40 Δ 15.0 Δ 20. Δ  
90'

373.0

Δ 16 Δ 20 Δ

Old Sta. 284+67 Old Hub. 0.1 RT.

267.0

Δ 16' Δ 22' Δ

Δ 15' Δ 26' Δ

Old Sta. 282+00

300

Δ 12' Δ 15' Δ



315+41<sup>3</sup>

315+42<sup>3</sup> E.C.

A ↓ 25°59' L.

314+50<sup>2</sup>

313+55<sup>2</sup>  
313+54<sup>2</sup> B.C.

312+95<sup>2</sup> E.C.

A ↓  
312+53<sup>2</sup> 16°44' L.

312+11<sup>5</sup> B.C.

310+03<sup>2</sup> E.C.

A ↓  
309+29<sup>2</sup> 11°45' R.

308+56<sup>2</sup> B.C.

306+05<sup>2</sup> E.C.

A ↓  
305+46<sup>2</sup> 7°07' L.

304+86<sup>2</sup> B.C.

302+51<sup>2</sup> E.C.

A ↓  
301+91<sup>2</sup> 7°16' R.

301+30<sup>6</sup> B.C.

297+99<sup>2</sup> E.C.

E=11.1  
T=93.93  
R=409.22  
D=14°  
L=188.5 185.6

60.5  
54.0

E=3.1  
T=42.1  
R=286.48  
D=20°  
L=83.7

E=3.8  
T=73.7  
R=716.20  
D=8°  
L=146.9

E=1.8  
T=59.4  
R=754.93  
D=6°  
L=113.6

E=1.9  
T=60.6  
R=954.93  
D=6°  
L=121.1

5.74°08'W 54.0

1189°08'N 208.4

579°07'N 250.9

586°14'N 235.0

5.78°58'W 331.6

Fch. 26.

x



197.0 H<sup>2</sup> 21030175  
Δ 10.0 Δ 15.0 Δ

Δ 19.2 Δ 16.0 Δ

Nail in  
Rk. Wall  
89.57'  
Δ 21.2 Δ 15.0 Δ73.7  
59.6  
250.9  
384.0Old Sta. 312+63<sup>2</sup> P.O.T.

324.2

Nail in Face Rock Wall.  
Δ 14.7 Δ 13.0 Δ75.24'  
Δ 15.0 Δ 22.0 Δ

Old Sta. 309+39

384.0

Δ 21 Δ 21 Δ

old Hub.

Old Sta. 305+55 Δ 16' Δ 19' Δ

355.0

Δ 10.0 Δ 20.0 Δ

Old Sta. 302+00 Old Hub 0.5' Rt.

437.0

Δ 15.0 Δ 18.0 Δ

414+746

414+81 E.C.

414+046

414+11 28°39'R

414+046

413+314

413+38 B.C.

404+00 P.O.T. 5.80°35'W 2067.8

398+15 P.O.T.

392+70 5°35'L

E = 9.2  
T = 73.2  
R = 286.48  
D = 20°  
L = 143.2

2061.8

384+00 P.O.T.

372+00 P.O.T. 5.81°08'W 3092.7

361+77 E.C.

361+07 54°41'R

360+25 B.C.

5.26°27'W 1871.1

341+62 3°14'R

336+72 523°13'W 492.4

336+70 E.C.

335+49 24°56'L

335+49 24°32'L

334+12

334+25 B.C. 5.48°09'W

315+41 547°45'W 1882.5

315+42 E.C.

1881.8

E = 13.4  
T = 124.6  
R = 572.96  
D = 10°  
L = 245.3

Mar. 1, 1926.

Feb. 27.

2103.0

"B"

△ 33°	△ 12°	△
-------	-------	---

617.0

"C"

△ 20°	△ 11°	△
-------	-------	---

1953.4

"D"

△ 33°    △ 15°  
 Guy Pole.    4 9A  
 Bridge.    355+55  
 16 x 16    1.5

△ 20°	△ 15°	△
-------	-------	---

3175.0

"E"

Jack 10'    △ 12°  
 Dead stump    Dead stump

△ 20'	△ 28'	△
△ 27°	△ 13°	△
△ 15°	△ 21°	△

2141.0

"F"

414+04 = 416  
 66

△ 8°	△ 33°	△
△ 15'	△ 29'	△
△ 15'	△ 27'	△
△ 12°	△ 30°	△

821.0

"G"

38° 41' N 70° 26' W  
 Bissell's Change. PI  
 414 + 141

544.538 to 549.543

In Road

Line of Trees  
10' L.Line of Trees  
10' L.



S7a L B D C.D.

478+87° B.C. 384.7

579°26'N 392.3

494+94° E.C. 495+02

E=4.9 5.5 Mch. 1

T=48.4 125.9

R=1432.40

D=4°00'

L=236.2 251.2

493+76° 0°03'L

492+58° B.C. 492+51

481+09 P.O.T. 5.89°29'N 1202.3

480+56° E.C. 1194.7

E=2.0

T=53.3

R=716.20

D=8°00'

L=106.5 Mch. 3

480+03° 8°31'A

479+99° B.C.

465+00 P.O.T. 5.80°58'N 2435.7

455+14° 0°43'R 5.81°03'N

5.80°20'W 5.80°11'N 1337.0

441+77° 0°51'L

431+40° 5.81°11'N 1039.3

429+40° E.C. 429+47

451+44°

E=12.0

T=59.7

R=143.24

D=40°

L=113.2

428+27° 45°17'L = 428+94

428+34

428+27° B.C.

N.53°32'W 469.2

423+65° E.C.

E=10.9 Mch. 2

T=145.0

R=954.93

D=60

L=287.8

422+22° 17°6'R

420+97° B.C.

414+74° N.70°48'W 596.2

414+51° E.C.

602.8



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LEFAX FILING INDEX

"A"  
622.0

495+00  
495+00 =

15°  
R.P. 51° Δ 13° Δ R.P.

Old Sta. 494+00 old Hub. 2<sup>o</sup> Back

1374.0

Δ 72° Δ 17° Δ  
Δ 39° Δ 16° Δ  
Δ 38° Δ 15° Δ

P.O.T.  
485+00

Old Sta. 480+26 old Hub 1.7 Back

P.O.T. 460+00  
463+85  
467+00

1337.0

580°58W  
581°03W

Δ 36° Δ 11° Δ  
Δ 35° Δ 8° Δ  
Δ 47° Δ 37° Δ  
Δ 11° Δ 15° Δ

Old Sta. 455+37 P.O.T.  
447+00 P.O.T.

Old Sta. 442+00 old Hub 1.3 R.P.

1096

431+38  
429+47 =

R.P. 43° Δ 17° Δ

Old Sta. 431+04 P.O.T. 437+00

667.0

R.P. Δ 15° Δ 53° R.P.  
x x x 42+55 3: Proc A.R.  
x x x 427+28 fence  
Δ 20° Δ 24° Δ

"A"

x x x 426+235  
24<sup>o</sup> Proc 5<sup>o</sup> L.

821.0

Δ 20° Δ 20° Δ  
415+18  
Δ 40° Δ 35° Δ

589+24<sup>1</sup>

589+27 75° 30' R

588+44<sup>2</sup>

588+48<sup>2</sup> B.C

E = 27.1  
T = 79.2  
R = 102.31  
D = 56°  
L = 134.8

531+55<sup>0</sup> 10' R

523+9<sup>0</sup> R.O.T S 46° 23' W 1689.5

514+65<sup>2</sup> E.C

514+08<sup>6</sup> 51' R

513+51<sup>3</sup> B.C

510+95<sup>4</sup> 3° 04' L

507+81<sup>2</sup> E.C

506+68<sup>2</sup> 13° 34' L

505+54<sup>2</sup> B.C

504+26<sup>2</sup> E.C

503+66<sup>2</sup> 14° 23' L

501+86<sup>2</sup> B.C

501+09<sup>1</sup> E.C

499+98<sup>2</sup> 8° 53' L

498+87<sup>2</sup> B.C

S 46° 33' W 5693.2  
5689.9

S 39° 32' W 255.9

S 42° 36' W 314.4

S 56° 10' W 128.9

S 70° 35' W 77.2

E = 1.7  
T = 57.1  
R = 954.93  
D = 6°  
L = 114.2

E = 6.7  
T = 113.6  
R = 954.93  
D = 6°  
L = 226.1

E = 7.6  
T = 120.5  
R = 954.93  
D = 6° 00'  
L = 239.7

E = 4.3  
T = 111.3  
R = 1432.4  
D = 4° 00'  
L = 222.1

Mch. 5

54.9  
26.1  
81.0

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LEFAX FILING INDEX

Old Sta 589+44

$\Delta 44^\circ \Delta 16^\circ \Delta$   
 $\Delta 39^\circ \Delta 15^\circ \Delta$   
 $\Delta 7^\circ \Delta 15^\circ \Delta$

581700  $\Delta 33^\circ \Delta 22^\circ \Delta$   
 573700  $\Delta 33^\circ \Delta 20^\circ \Delta$   
 562700  $\Delta 38^\circ \Delta 15^\circ \Delta$   
 550700  $\Delta 34^\circ \Delta 15^\circ \Delta$   
 540700  $\Delta 35^\circ \Delta 15^\circ \Delta$

Old Sta 531+71

Old Hub 2<sup>1</sup> Back

$\Delta 39^\circ \Delta 15^\circ \Delta$   
 $\Delta 7^\circ \Delta 15^\circ \Delta$

R.P.  $\Delta 34^\circ \Delta 15^\circ \Delta$   
 P.O.T.

Old Sta 514+25

Old Hub 15 Ht.

$\Delta 9^\circ \Delta 15^\circ \Delta$   
 $\Delta 15^\circ \Delta 15^\circ \Delta$   
 $\Delta 18^\circ \Delta 12^\circ \Delta$

Power Pole 3' R.P.  
 512+57  
 497 94.7

$\Delta 15^\circ \Delta 15^\circ \Delta$   
 $\Delta 12^\circ \Delta 19^\circ \Delta$

$\Delta 20^\circ \Delta 12^\circ \Delta$   
 $\Delta 14^\circ \Delta 16^\circ \Delta$

$\Delta 21^\circ \Delta 20^\circ \Delta$

LEFAX, PHILADELPHIA, PA. 42

622.0 "A"  
 309.0 "B"  
 363.0 "C"  
 428.0 "D"  
 313.0  
 1746.6  
 5777  
 57691 ✓



X N.86°W  
732+53<sup>2</sup> E.C

E=5.7 ✓  
T=127.8 ✓  
R=1432.4 ✓  
D=4 ✓  
L=255.0 ✓

Mch. 11.

X  
731+26<sup>5</sup> 10°12'R

X  
727+98<sup>3</sup> B.C  
72A+00 5.83°48'N 1250.5 ✓  
717+48<sup>2</sup> E.C

E=3.7  
T=59.7  
R=477.47  
D=12°  
L=118.8

X  
716+89<sup>1</sup> 14°15'R

X  
716+29<sup>4</sup> B.C  
70A+00 5.67°33'N 2205.4 ✓  
694+24<sup>0</sup> E.C

E=9.0  
T=101.9  
R=572.96  
D=10°  
L=201.7

X  
693+24<sup>2</sup> 20°10'L

X  
692+22<sup>3</sup> B.C  
694+00  
65A+00 5.89°43'N 1466.1 ✓

Mch. 9.

X  
645+56<sup>2</sup> 1°24'L  
633+00  
62A+00

Mch. 8.

X  
591+31<sup>3</sup> E.C  
N.88°53'N 5424.9 ✓

E=9.8  
T=72.1  
R=260.44  
D=22°  
L=140.6

Mch. 6.

X  
590+62<sup>8</sup> 30°56'L

X  
589+90<sup>1</sup> B.C  
589+49<sup>3</sup> N.57°57'N 7.7 ✓  
589+83<sup>0</sup> E.C

X  
589+24<sup>1</sup>  
589+27<sup>4</sup> 75°30'R



Old Sta. 770+28

3855-

R.P.  $\Delta$  12°  $\Delta$  49°  $\Delta$

LEFAX FILING INDEX  
P.O.T. 742+50  
754+00  
761+00  
766+00  
748+00

Old Sta. 731+73

1438-

R.P.  $\Delta$  14°  $\Delta$  8°  $\Delta$  4RP

P.O.T. 723+00  
728+00

R.P.  $\Delta$  18°  $\Delta$  13°  $\Delta$  4RP

Old Sta. 717+35

P.O.T. 698+00  
703+00  
713+00

R.P.  $\Delta$  6°  $\Delta$  11°  $\Delta$  4RP

R.P.  $\Delta$  55°  $\Delta$  9°  $\Delta$  4RP

Old Sta. 693+68

4768.0

Old Hub 6.8 NE  
P.O.T. 661+00  
656+00  
666+00  
676+00  
686+00  
691+00

R.P.  $\Delta$  10°  $\Delta$  14°  $\Delta$  R.P.

Old Sta. 646+00

5497.0

Old hub 32 NE  
P.O.T. 601+00  
611+00  
621+00  
631+00  
641+00

$\Delta$  40°  $\Delta$  29°  $\Delta$

Old Sta. 591+03

164.0

$\frac{589+780}{15} =$   
 $\frac{589+792}{15} =$

$\Delta$  57°  $\Delta$  38°  $\Delta$   
 $\Delta$  60°  $\Delta$  29°  $\Delta$   
 $\Delta$  75°  $\Delta$  29°  $\Delta$

Old Sta. 589+44

$\Delta$  817+68<sup>2</sup> 7°30' L  
E=1.0 ✓  
T=31.3 ✓  
R=477.47 ✓  
D=12° ✓  
L=62.5 ✓

817+36<sup>2</sup> B.C.  
57°41' W 6.0 ✓

817+30<sup>2</sup> E.C.  
 $\Delta$  816+88<sup>2</sup> 20°45' L  
E=4.0 ✓  
T=43.7 ✓  
R=238.73 ✓  
D=24° ✓  
L=86.5 ✓

816+44<sup>2</sup> B.C.  
N.88°39' W 367.4 ✓

812+77<sup>2</sup> E.C.  
 $\Delta$  812+31<sup>2</sup> 70°59' L  
E=19.8 ✓  
T=67.9 ✓  
R=86.81 ✓  
D=66° ✓  
L=107.6 ✓

811+69<sup>2</sup> B.C.  
N.17°35' W 552.5 ✓

806+16<sup>2</sup> E.C.  
 $\Delta$  805+34<sup>2</sup> 63°09' R  
E=29.2 ✓  
T=29.3 ✓  
R=103.6 ✓  
D=34° ✓  
L=185.7 ✓

804+31<sup>2</sup> B.C.  
N.80°44' W 1499.4 ✓

789+318<sup>2</sup> 0°48' L  
N.79°36' W 1900.4 ✓

770+31<sup>2</sup> E.C.  
 $\Delta$  769+80.9<sup>2</sup> 6°04' R  
E=1.3 ✓  
T=50.6 ✓  
R=954.93 ✓  
D=6° ✓  
L=101.1 ✓

769+30<sup>2</sup> B.C.  
N.86°01' W 3676.6 ✓

732+53<sup>2</sup> E.C.

Line Change of Riverview  
Farms. Sta. 492+68.0 to  
Equation at Sta.  
= E.C. 504+30.0 Back =  
= E.C. 504+33.8 Ahead =

June 2, 1926.



505+54.9 B.C.

T=113.6

5.56°07'N 121.1

504+33.8  
= 504+30.0 = E.C.

P.I.  
503+04.3 20°19'N

E=11.4  
T=128.33  
R=716.20  
D=8°00'  
L=254.0  
253.96

501+76° B.C.

5.76°26'N 691.3

494+84.2 E.C.

P.I.  
493+76.9 13°0'N

E=6.2  
T=108.80  
R=754.93  
D=6°00'  
L=216.67

492+68° B.C.

5.89°26'N 1211.8

480+56.2 E.C.

T=53.3



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502+263 Pave 19° L

502+09 Tel pole 15° R

501+20<sup>E</sup> Tel pole 12<sup>E</sup> R

501+02 Guy pole 5° L Pave 15<sup>L</sup> L

499+89 Tel pole 9° R

498+39 Tel pole 5<sup>E</sup> R Pave 15<sup>E</sup> L

497+35 Con. Culvert 6<sup>E</sup> L

497+00 Pavement 12<sup>E</sup> L

497+00 Tel pole 5' R

LEFAX FILING INDEX

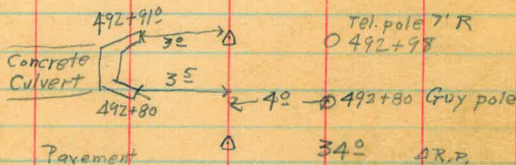
Δ 13° Δ 15° Δ

495+75 Tel pole 1<sup>E</sup> R

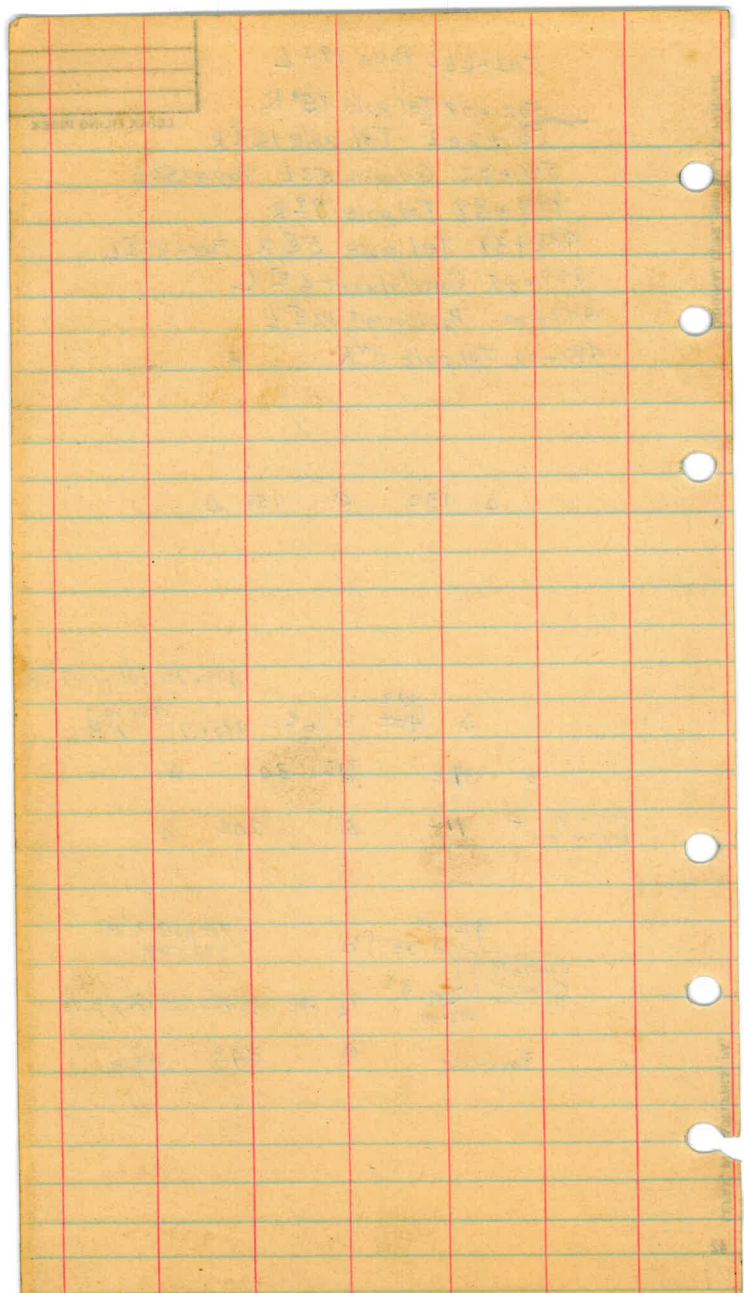
Δ 39° Δ 40° Δ 16° Δ 495+57 Guy pole 1' R

Δ 31° Δ Pot. 30° Δ

Gross in Edge of Pave. + 11° Δ 20° Δ



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Σ


LEFAX FILING INDEX

Δ

342

342

ΔR1

LEFAX, PHILADELPHIA, PA.

42

Pavement

$-504+33^B$   
 $504+30^B$  E.C.

$+04^B$   
 $503+04^B$   $20^{\circ}19' L$

$76^B$   
 $501+76^B$  B.C.

$495+44^B$  P.O.T.  
 $494+84^B$  E.C.

$493+76^B$   $13^{\circ}00' L$

$492+68^B$  B.C.

$487+00$  P.O.T.

$589^{\circ}26' W$

$E=11.4$   
 $T=128.33$   
 $R=716.20$   
 $D=8^{\circ}00'$   
 $L=253.96$

$16^B L$

$11^B L$

$E=6.2$   
 $T=108.8$   
 $R=954.93$   
 $D=6^{\circ}00'$   
 $L=216.67$

$10^B L$

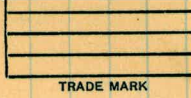


3-113

El Capitan Pipe Line.  
 Cross Sections on  
 Center Line. Sta. 754+00  
 to Sta. 802+25

$$\begin{array}{r} 318.720 \\ 1.205 \\ \hline 317.515 \end{array}$$





Lf. E Rt.

$$\frac{37}{102}$$

$$\frac{4}{102}$$

FENCE  
9.6

$$\frac{32}{102}$$

$$\frac{37}{102}$$

$$\frac{4}{102}$$

$$\frac{3}{102}$$

FENCE  
9.6

$$\frac{36}{102}$$

$$\frac{2}{102}$$

$$\frac{6}{102}$$

FENCE  
9.6

$$\frac{37}{102}$$

$$\frac{31}{102}$$

$$\frac{2}{102}$$

$$\frac{10}{102}$$

FENCE  
9.6

$$\frac{3}{102}$$

Sta	#	π	-	Σ/Σ
		318.720		
757+00				
758+00				
759+00				
760+00				
761+00				
		1.285		317.435
				317.442
9.305		326.747		



Lf. R Rt

$$\frac{3.9}{100}$$

$$\frac{7.4}{100}$$

$$\frac{3.9}{100}$$

$$\frac{7.7}{100}$$

$$\frac{4.7}{100}$$

$$\frac{5}{100}$$

$$\frac{4.5}{100}$$

Fence  
10.0

$$\frac{5.10}{100}$$

$$\frac{5}{100}$$

Fence  
 $\frac{6.10}{100}$

$$\frac{4.5}{100}$$

$$\frac{5}{100}$$

$$\frac{6.5}{100}$$

Fence  
 $\frac{6.9}{100}$

$$\frac{3.10}{100}$$

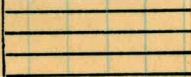
$$\frac{3.3}{60}$$

$$\frac{2.5}{40}$$

Fence  
 $\frac{2.5}{100}$

Record Elev - 317.442

Sta	+	K	-	Elev.
		326.747		
762+00				
763+00				
	+40		8.8	
764+00				
	+40		6.8	
	+75		7.2	



LF

⊕

RT

$$\frac{9.3}{10.0}$$

$$\frac{9.6}{5.0}$$

$$\frac{10.0}{4.0}$$

$$\frac{9.0}{10.0}$$

$$\frac{8.0}{7.0}$$

$$\frac{8.5}{5.0}$$

$$\frac{8.0}{4.0}$$

$$\frac{10.0}{10.0}$$

$$\frac{7.6}{10.0}$$

$$\frac{7.5}{4.0}$$

$$\frac{9.6}{10.0}$$

$$\frac{6.5}{10.0}$$

$$\frac{6.9}{4.5}$$

$$\frac{6.1}{2.5}$$

$$\frac{7.0}{10.0}$$

$$\frac{6.1}{10.0}$$

$$\frac{6.3}{6.0}$$

$$\frac{6.7}{5.0}$$

$$\frac{6.9}{10.0}$$

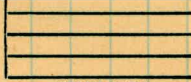
$$\frac{5.0}{10.0}$$

$$\frac{5.0}{6.0}$$

$$\frac{5.0}{10.0}$$

Sta	+ T	- Elev
	326.747	
765+00		
766+00		
T.P.	1.976 <del>1.953</del>	324.771 324.794
	10.780	335.551
767+00		
768+00		
769+00		





Lf,

E

Rt,

$$\frac{57}{102}$$

$$\frac{57}{65}$$

$$\frac{87}{102}$$

$$\frac{44}{102}$$

$$\frac{47}{82}$$

$$\frac{43}{72}$$

$$\frac{71}{102}$$

$$\frac{103}{102}$$

$$\frac{107}{52}$$

$$\frac{87}{102}$$

$$\frac{73}{102}$$

$$\frac{76}{52}$$

$$\frac{69}{32}$$

$$\frac{72}{102}$$

$$\frac{4}{10100}$$

$$\frac{4}{60100}$$

$$\frac{65}{10100}$$

Sta. +  $\pi$  - Elev.  
335.554

769+80 P.I.

770+00

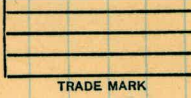
T.P. + B.M. # 86 1.555 334.996  
- 333.989 -

7.682 341.671

771+00

+42 4.0

772+00



$$\frac{20}{100}$$

$$\frac{33}{100}$$

$$\frac{15}{100}$$

$$\frac{22}{100}$$

Record Eler - 333.989

$$\frac{52}{100}$$

$$\frac{42}{50}$$

$$\frac{51}{100}$$

$$\frac{51}{100}$$

$$\frac{52}{92}$$

$$\frac{46}{80}$$

$$\frac{49}{100}$$

$$\frac{54}{100}$$

$$\frac{59}{100}$$

Sta	+	X	-	Elev
		341.671		
773+00				
774+00				
T.P.		9.059		332.612
		8.322		340.934
775+00				
776+00				
777+00				





L.F.

¢

R.L.

$$\frac{73}{100}$$

$$\frac{73}{80}$$

$$\frac{89}{100}$$

$$\frac{95}{100}$$

$$\frac{93}{80}$$

$$\frac{110}{40}$$

$$\frac{117}{100}$$

$$\frac{82}{100}$$

$$\frac{86}{100}$$

$$\frac{73}{100}$$

$$\frac{75}{100}$$

$$\frac{60}{100}$$

$$\frac{63}{100}$$

Sta.	+ $\pi$ -	Elev.
	340.934	
778+00		
779+00		
780+00		
T.P.	0.961	339.973
	9.770	349.743
B.M. # 87	8.281	341.462 341.454
	8.281	349.735
781+00		

Lf.

E

Rt.

TRADE MARK

$$\frac{47}{102}$$

$$\frac{48}{85}$$

$$\frac{45}{45}$$

$$\frac{53}{102}$$

$$\frac{34}{102}$$

$$\frac{37}{102}$$

$$\frac{07}{102}$$

$$\frac{05}{75}$$

$$\frac{14}{102}$$

Record Elev 341.454.

$$\frac{71}{102}$$

$$\frac{82}{102}$$

Sta +  $\lambda$  - Elev  
349.735

782+00

783+00

784+00

785+00

786+00

T.P. - 1.413 348.322

7.970 356.292



Lf.

Q

Rt.

$$\frac{49}{100}$$

$$\frac{43}{85}$$

$$\frac{51}{100}$$

$$\frac{38}{100}$$

$$\frac{37}{80}$$

$$\frac{52}{100}$$

$$\frac{41}{100}$$

$$\frac{38}{81}$$

$$\frac{64}{100}$$

$$\frac{30}{100}$$

$$\frac{30}{75}$$

$$\frac{37}{55}$$

$$\frac{53}{100}$$

$$\frac{18}{100}$$

$$\frac{14}{60}$$

$$\frac{23}{40}$$

$$\frac{34}{100}$$

Sta +  $\pi$  - Elev.  
356.292

787+00

788+00

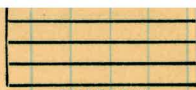
789+00

+40 P.I

T.P. + B.M. # 88 -3.548 352.744  
352.754

3.548 356.302

790+00



Lf.                      ♀                      Rt.

$$\frac{62}{100}$$

$$\frac{61}{70}$$

$$\frac{83}{100}$$

$$\frac{45}{100}$$

$$\frac{41}{63}$$

$$\frac{64}{100}$$

$$\frac{31}{100}$$

$$\frac{32}{83}$$

$$\frac{27}{72}$$

$$\frac{39}{100}$$

$$\frac{33}{100}$$

$$\frac{35}{90}$$

$$\frac{30}{75}$$

$$\frac{36}{100}$$

Record Elev. - 352.754

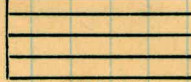
$$\frac{44}{100}$$

$$\frac{42}{80}$$

$$\frac{5}{100}$$

Sta	+	-	Elev.
		356.302	
791+00			
792+00			
T.P. -		9.335	346.967
	0.895	347.862	
793+00			
794+00			
795+00			





14. R

$$\frac{71}{100} \quad \frac{69}{80}$$

$$\frac{83}{100}$$

$$\frac{94}{100}$$

$$\frac{114}{45}$$

$$\frac{128}{100}$$

$$\frac{33}{100}$$

$$\frac{35}{82}$$

$$\frac{48}{45}$$

$$\frac{59}{100}$$

$$\frac{55}{100} \quad \frac{70}{72} \quad \frac{76}{72}$$

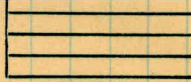
$$\frac{93}{100}$$

$$\frac{69}{100}$$

$$\frac{89}{45}$$

$$\frac{95}{100}$$

Sta	+	X	-	Elev
		347.862		
796+00				
	+16		7.6	
797+00				
			10.855	337.007
		2.543	339.550	
798+00				
799+00				



$$\frac{85}{100}$$

$$\frac{79}{65}$$

$$\frac{84}{100}$$

$$\frac{89}{100}$$

$$\frac{83}{75}$$

$$\frac{89}{100}$$

$$\frac{112}{100}$$

$$\frac{118}{85}$$

$$\frac{112}{55}$$

$$\frac{127}{100}$$

Fence  
9.8

$$\frac{56}{100}$$

$$\frac{71}{100}$$

Fence  
8.0

$$\frac{82}{100}$$

$$\frac{78}{100}$$

Fence  
7.5

Sta	+	X	-	Elev.
		339.550		
800	+00			
	+20 <sup>5</sup>		12.1	
	+80		6.7	
801	+00			
	+16 <sup>5</sup>		9.2	
	+56 <sup>5</sup>		5.1	



Lf.

C

Rt.

TRADE MARK

$$\frac{95}{100}$$

$$\frac{102}{70}$$

$$\frac{114}{70}$$

$$\frac{125}{100}$$

Fence  
7.5

$$\frac{86}{100}$$

$$\frac{110}{60}$$

$$\frac{117}{30}$$

$$\frac{126}{100}$$

Fence  
7.8

$$\frac{70}{100}$$

$$\frac{65}{70}$$

$$\frac{72}{100}$$

Fence  
8.2

$$\frac{60}{110}$$

$$\frac{46}{80}$$

$$\frac{59}{100}$$

Fence  
8.2

$$\frac{53}{110}$$

$$\frac{34}{80}$$

$$\frac{47}{100}$$

Fence  
8.2

$$\frac{51}{100}$$

$$\frac{53}{100}$$

Fence  
80

Sta + K - Elev

339.550

802+00

802+25  $\frac{81}{2}$  = 802+20  $\frac{53}{2}$

B.M. # 89

7.452-332.098



Lf.

£

Rt.

$$\frac{45}{100}$$

$$\frac{53}{100}$$

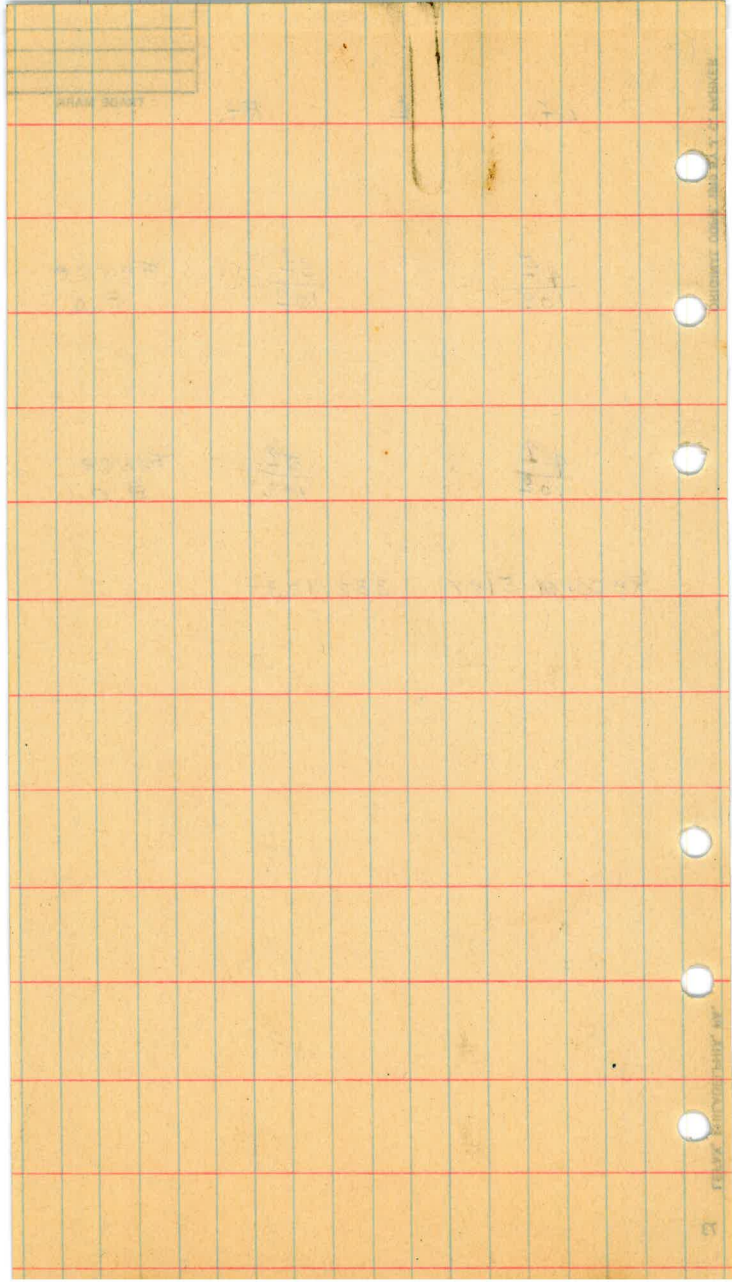
Fence  
8.0

$$\frac{44}{100}$$

$$\frac{52}{100}$$

Fence  
8.0

Record Elev. 332.103-




WRAN 35487

BRIDGEMAN COMPANY, NEW YORK, N.Y.

BRIDGEMAN COMPANY, NEW YORK, N.Y.



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①

LEFAX FILING INDEX

*El Capitan Pipe Line.*

*Transit Notes on line  
Change from Sta.  
642+00 to Sta.*

LEFAX, PHILADELPHIA, PA.

693+25

693+02

684+00

681+30 P.O.T.

680+91

680+35

674+00

671+35 P.O.T.

664+00

661+50 0°02'L

654+25 0°10'R

654+00 P.O.T.

645+56 P.O.T.

642+00 1°25'L

591+31<sup>3</sup> E.G.

N. 88° 48' W

589° <sup>47'</sup> ~~48'~~ W 3089.4 ✓

589° <sup>49'</sup> ~~50'~~ W 725.0 ✓

589° <sup>39'</sup> ~~40'~~ W 1225.0 ✓

N. 88° 36' <sup>5</sup> W 6068.7

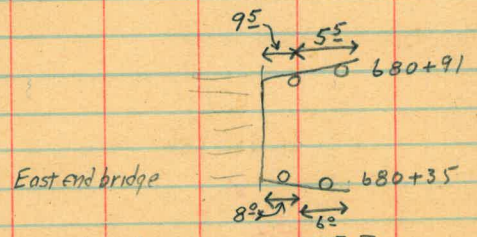
ORIGINAL COPY - 1910 BY J. C. PARKER

Old hub 693+24<sup>±</sup> is 15<sup>±</sup>R

4x4 Sign post 3'R

Old hub 689+00<sup>±</sup> is 3<sup>±</sup>R

Δ 40° Δ 17° Δ



East end bridge

Old hub 674+00 is 47'R

Δ 46° Δ 17° Δ

Old P.O.T. 664+00 11°R

Δ 43° Δ 20° Δ

Δ 40° Δ 22° Δ

Old P.O.T. 654+00 is 93'R

Old P.I. 645+56<sup>±</sup> is 9°R

Δ 38° Δ 15° Δ

LEFAX, PHILADELPHIA, PA.



718+21<sup>07</sup> E.C.

584°~~56~~<sup>55</sup> W

E=6.6 ✓  
T=97.26 ✓  
R=716.20 ✓  
D=8°00' ✓  
L=193.33 ✓

717+25 15°28'R

716+27<sup>74</sup> B.C.

569°~~28~~<sup>27</sup> W 942.7

706+85 0°15'R

569°~~28~~<sup>27</sup> W 820.0

698+65 0°15'L

569°~~28~~<sup>27</sup> W 456.2

694+08<sup>82</sup> E.C.

E=7.6 ✓  
T=85.62 ✓  
R=477.47 ✓  
D=12° ✓  
L=169.44 ✓

693+25 20°20'L

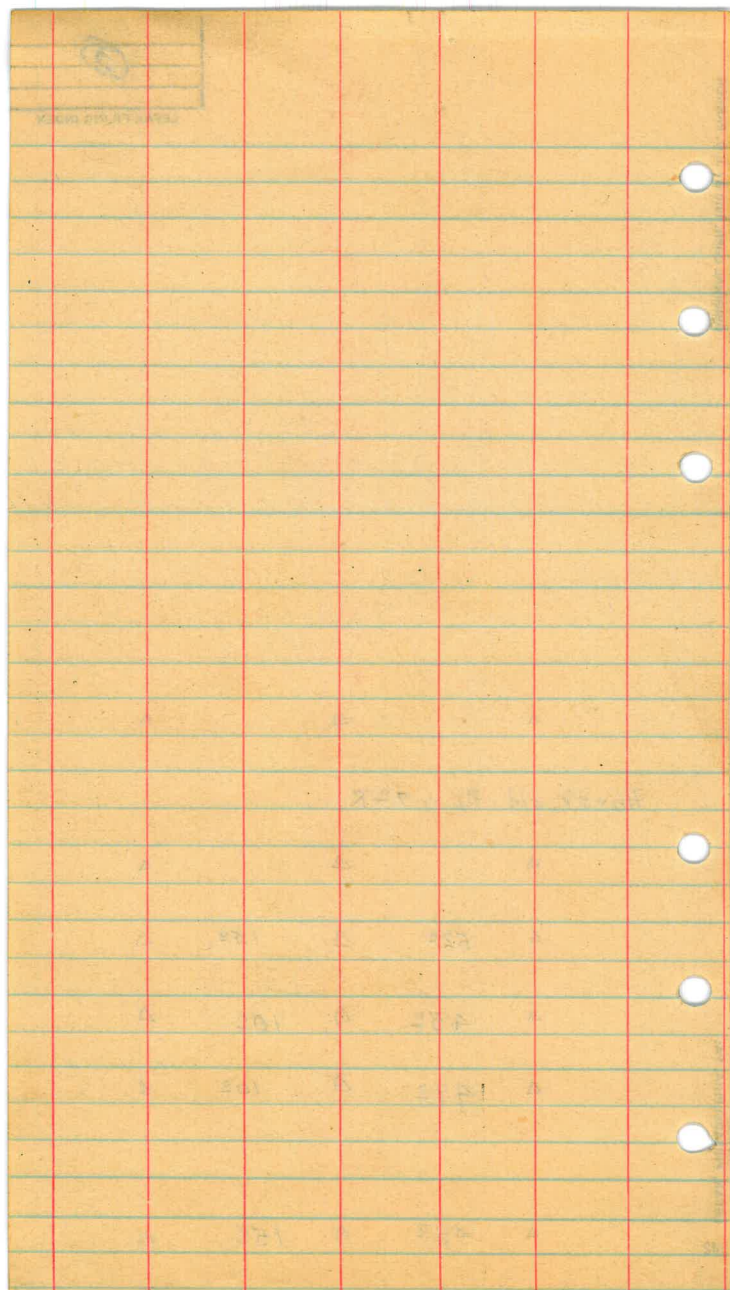
692+39<sup>38</sup> B.C.

589°~~48~~<sup>47</sup> W 3089.4



716+89, old P.I. is 7°R

△		△		△
△		△		△
△	52°	△	15°	△
△	45°	△	10°	△
△	49°	△	10°	△
△	45°	△	15°	△



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769+80 5°0'R

N. 86°06'W 1575.8  
~~1576.0~~

754+04<sup>29</sup> 0°55'L

N. 85°11'W 519.2

748+85 1°45'R

N. 86°56'W 585.0

743+00 1°05'L

N. 85°51'W 1130.8

731+69<sup>29</sup> E.C.

E=2.9 ✓  
T=64.55 ✓  
R=716.20 ✓  
D=8° ✓  
L=128.75 ✓

731+05 10°18'R

730+40<sup>29</sup> B.C.

S. 83°51'W 510.4

725+30 1°04'L

S. 84°55'W 708.9

718+21<sup>07</sup> E.C.

E=6.6 ✓  
T=97.26 ✓  
R=716.20 ✓  
D=8°00' ✓  
L=193.33 ✓

717+25 15°28'R

716+27<sup>24</sup> B.C.



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42

760+02 3'L 18" Gal. Iron Culvert

758+70 8'L 24" Concrete Culvert

Old POT 754+00

739+60 8" Gal. Iron 3'L

Δ 38° Δ 12° Δ

Δ 40° Δ 15° Δ

730+08<sup>5</sup> 18" Culvert 2'L

Δ 45° Δ 14° Δ

721+45 24" C.I. Culvert 1'L

Δ 39° Δ 25° Δ

Δ 54° Δ 17° Δ

805+04.8 B.C.

N.80°45'W 284.3 ✓

~~802+20.53~~  
802+2581 0°40'L = 802+20<sup>53</sup> P.I.

N.80°05'W 1285.8 ✓

789+40 0°08'R

N.80°13'W 1840.0 ✓

771+00 0°53'R

N.81°06'W 120.0 ✓

769+80 5°0'R

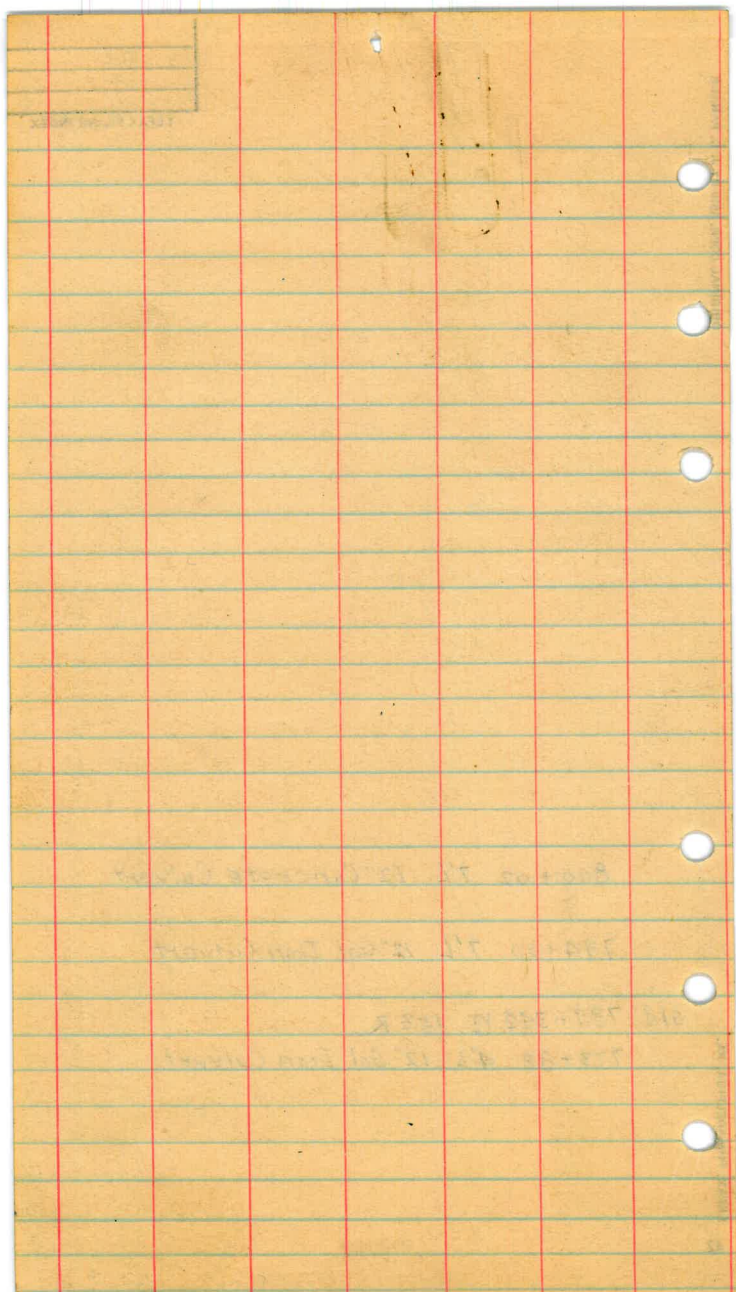
1575.8  
N.86°06'W 1576.0

800+02 7'L 12" Concrete Culvert

794+00 7'L 12" Gal. Iron Culvert

old 789+348 PI. 15<sup>2</sup> R

773+88 4'L 12" Gal. Iron Culvert





Bearing	Dist	Co. S	Sin	N	S	E	W
N12°00'W	587.0	.97815	.20791	574.2	—	—	122.0
East	310.8	0.00	1.0000	—	—	310.8	—
S58°10'E	1858.4	.59949	.80038	—	1114.1	1487.4	—
S78°40'E	830.8	.19652	.98050	—	163.3	814.6	—
S54°30'E	759.0	.58070	.81412	—	440.8	617.9	—
S78°10'E	689.9	.20507	.97875	—	141.0	625.2	—
S84°11'E	776.3	.10135	.99483	—	78.7	772.3	—
N82°36'E	792.1	.12880	.99167	102.0	—	785.5	—
S88°11'E	1617.1	.03170	.99950	—	51.3	1616.3	—
S1°28'W	159.0	.99987	.02660	—	158.9	—	4.1
N72°26'W	227.0	.30182	.95337	168.5	—	—	216.4
S85°14'W	177.2	.08310	.99654	—	14.7	—	176.6
S88°18'W	249.0	.02867	.99956	—	7.4	—	248.9
S84°23'W	199.5	.09787	.99520	—	19.5	—	198.5
S82°47'W	199.7	.12504	.99215	—	25.0	—	198.1
Sub-Total							

Bearing	Dist	cos	sin	N	S	E	W
Sub-Totals Forward →							
N83°08'W	198.6	.11956	.99283	23.7	-	-	197.2
N75°09'W	174.9	.25066	.96807	43.8	-	-	169.3
N83°12'W	34.6	.1840	.98297	4.1	-	-	34.4
N87°03'W	40.4	.09159	.99914	1.7	-	-	40.4
S82°03'W	250.3	.13831	.99039	-	34.6	-	247.9
S77°08'W	151.6	.22410	.97457	-	29.5	-	128.3
S77°32'W	124.4	.21567	.97642	-	26.9	-	121.5
S77°16'W	226.9	.22041	.97541	-	50.0	-	221.3
N79°04'W	243.8	.17823	.98399	43.6	-	-	239.9
S88°35'W	120.0	.02472	.99969	-	3.0	-	120.0
N81°45'W	255.0	.14349	.98965	36.6	-	-	252.4
S83°49'W	200.0	.10771	.99418	-	21.5	-	198.8
N77°03'W	478.0	.21616	.97636	102.7	-	-	463.8
Sub-Totals →							

Sheet #2 - El Monte Ranch Tic

Bearing Dist cos Sin

Sub Totals - Forward

	N	S	E	W	Tic
N7°41'W	1239.0	31289	94979	748	227.0
N77°46'W	86.0	21189	97729	18.2	84.0
N63°45'W	95.0	44229	89687	42.0	85.2
N54°26'W	183.2	58165	81344	106.6	149.0
N48°33'W	157.5	66153	74992	104.2	118.1
N64°23'W	35.3	43235	90171	15.3	31.8
N74°28'W	84.0	26780	96347	22.5	80.9
N77°08'W	234.0	22268	97489	52.1	228.1
N82°08'W	301.0	13682	99059	41.2	298.2
N79°38'W	155.0	17995	98368	27.9	152.5
N70°58'W	130.0	32612	94533	75.0	217.4
N69°58'W	327.0	43889	89854	143.5	293.8
N44°08'W	413.0	77972	69633	296.4	287.6
N54°28'W	535.0	58118	81328	310.9	435.4
N78°40'W	133.0	28123	95964	37.4	127.6
Sub Totals					



Bearing	Dist	cos	Sin	N	S	E	W
Sub Totals Forward →							
N78°20'W	97.0	20222.97934	19.6	—	—	—	95.0
S79°54'W	120.0	17537.98450	—	21.0	—	—	118.1
S73°45'W	206.0	28541.95841	—	58.8	—	—	197.4
N87°17'W	108.0	14746.99588	5.1	—	—	—	107.9
N82°35'W	153.5	12908.99163	19.8	—	—	—	152.8
			2413.3	246.5	7,080.0	7,087.0	7087.0
			2,460.5				
N82°26'E	47.7		47.2			7.0	
(N12°W	18.0)						



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①  
LEFAX FILING INDEX

# El Capitan Pipe Line.

Profile Levels and  
Cross Sections on  
Line Change from  
Sta. 492+68 B.C. to  
Equation  
Sta. 504+30.3 Back  
Sta. 504+33.8 Ahead

June 3, 1926,  
Simpson.

LEFAX, PHILADELPHIA, PA.  
42

JUNE-3 - RELOCATION.

Sta.		Elev.
492+61 <sup>8</sup>		375.9
+85 <sup>1</sup>	6'x2' CONCRETE CULVERT.	374.3
+93 <sup>1</sup>		375.0
493+18 <sup>1</sup>		374.8
+43 <sup>1</sup>		374.4
+68 <sup>1</sup>		374.7
+93 <sup>1</sup>		374.6
494+18 <sup>1</sup>		374.9
+43 <sup>1</sup>		375.3
+68 <sup>1</sup>		375.8

$\frac{377.8}{100}$        $\frac{377.9}{90}$        $\frac{375.8}{100}$   
 $\frac{374.4}{322}$        $\frac{374.3}{92}$        $\nabla$  Flow Line

$\frac{377.9}{100}$        $\frac{377.6}{50}$        $\frac{374.2}{100}$

$\frac{377.9}{100}$        $\frac{377.8}{50}$        $\frac{375.8}{100}$

$\frac{377.9}{100}$        $\frac{377.4}{50}$        $\frac{374.8}{100}$

$\frac{377.9}{100}$        $\frac{377.3}{50}$        $\frac{375.4}{100}$

$\frac{377.9}{100}$        $\frac{377.4}{50}$        $\frac{375.0}{100}$

$\frac{377.9}{100}$        $\frac{377.4}{50}$        $\frac{375.1}{100}$

$\frac{378.0}{100}$        $\frac{377.6}{50}$        $\frac{374.5}{100}$

$\frac{378.0}{100}$        $\frac{377.7}{42}$        $\frac{375.4}{100}$

FORM 100-100-100

1.7  
1.7  
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Flow Link

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FORM 100-100-100

FORM 100-100-100





Sta		Elev.
494+84 <sup>B</sup>	E.C.	376.5
495+28 <sup>3</sup>		377.5
+60 <sup>B</sup>		381.0
496+00		376.6
497+00		375.2
498+00		376.1
499+00		377.6
500+00		383.3
501+00		386.6
+76 <sup>3</sup>	B.C	388.3

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Lf. £ Rt.

$\frac{378.0}{100}$	$\frac{377.4}{32}$	$\frac{376.5}{100}$
---------------------	--------------------	---------------------

$\frac{377.9}{100}$	$\frac{376.4}{100}$
---------------------	---------------------

$\frac{378.0}{100}$	$\frac{378.0}{80}$	$\frac{381.3}{50}$	$\frac{381.9}{25}$	$\frac{377.9}{55}$	$\frac{377.3}{100}$
---------------------	--------------------	--------------------	--------------------	--------------------	---------------------

$\frac{378.1}{100}$	$\frac{377.9}{85}$	$\frac{378.4}{70}$	$\frac{376.1}{100}$
---------------------	--------------------	--------------------	---------------------

$\frac{379.1}{100}$	$\frac{378.3}{65}$	$\frac{379.6}{100}$
---------------------	--------------------	---------------------

$\frac{380.7}{100}$	$\frac{380.5}{80}$	$\frac{375.5}{100}$
---------------------	--------------------	---------------------

$\frac{382.8}{100}$	$\frac{382.9}{90}$	$\frac{375.7}{60}$	$\frac{375.0}{100}$
---------------------	--------------------	--------------------	---------------------

$\frac{387.3}{100}$	$\frac{380.4}{100}$
---------------------	---------------------

$\frac{389.3}{100}$	$\frac{389.2}{55}$	$\frac{384.3}{100}$
---------------------	--------------------	---------------------

$\frac{391.6}{100}$	$\frac{391.6}{55}$	$\frac{381.6}{100}$
---------------------	--------------------	---------------------

LEFAX, PHILADELPHIA, PA. 42

RT	0	21
2.20 100	A.70 20	0.80 100
A.20 100	P.70 100	
C.P. 100	P.70 20	P.10 20
1.20 100	A.80 10	P.70 20
2.20 100	C.80 20	1.80 100
2.20 100	2.80 100	1.80 100
0.20 100	1.20 10	P.80 100
A.00 100	C.70 100	0.50 100
C.40 100	A.80 100	C.80 100
2.10 100	2.10 100	2.10 100



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LEFAX, PHILADELPHIA, PA.

LEFAX FILING INDEX

5

1.000	1000
2.000	2000
3.000	3000
4.000	4000
5.000	5000
6.000	6000
7.000	7000
8.000	8000
9.000	9000
10.000	10000
11.000	11000
12.000	12000
13.000	13000
14.000	14000
15.000	15000
16.000	16000
17.000	17000
18.000	18000
19.000	19000
20.000	20000

Sta	Elev.
502+01 <sup>3</sup>	389.5
+26 <sup>3</sup>	388.0
+51 <sup>3</sup>	388.4
+76 <sup>3</sup>	388.2
503+01 <sup>3</sup>	386.7
+26 <sup>3</sup>	384.1
+51 <sup>3</sup>	383.1
+76 <sup>3</sup>	380.7
504+01 <sup>3</sup>	378.8
+26 <sup>3</sup>	377.8

Lf.

Q

Ry.

$$\frac{392.6}{100}$$

$$\frac{391.9}{95}$$

$$\frac{386.6}{50}$$

$$\frac{385.2}{100}$$

$$\frac{392.8}{100}$$

$$\frac{392.6}{90}$$

$$\frac{385.1}{100}$$

$$\frac{392.7}{100}$$

$$\frac{392.5}{80}$$

$$\frac{385.1}{100}$$

$$\frac{392.8}{100}$$

$$\frac{384.7}{73}$$

$$\frac{381.4}{100}$$

$$\frac{391.3}{100}$$

$$\frac{383.4}{100}$$

$$\frac{388.5}{100}$$

$$\frac{381.3}{100}$$

$$\frac{386.0}{100}$$

$$\frac{380.0}{100}$$

$$\frac{383.7}{100}$$

$$\frac{379.4}{55}$$

$$\frac{375.8}{100}$$

$$\frac{381.0}{100}$$

$$\frac{378.2}{35}$$

$$\frac{374.7}{100}$$

$$\frac{380.2}{100}$$

$$\frac{376.9}{70}$$

$$\frac{375.1}{100}$$

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1913  
2778  
204338 = 2041302

Sta

Elev.

$$504+33^8 = 504+30^3 \quad 377.6$$

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Lf.

Q

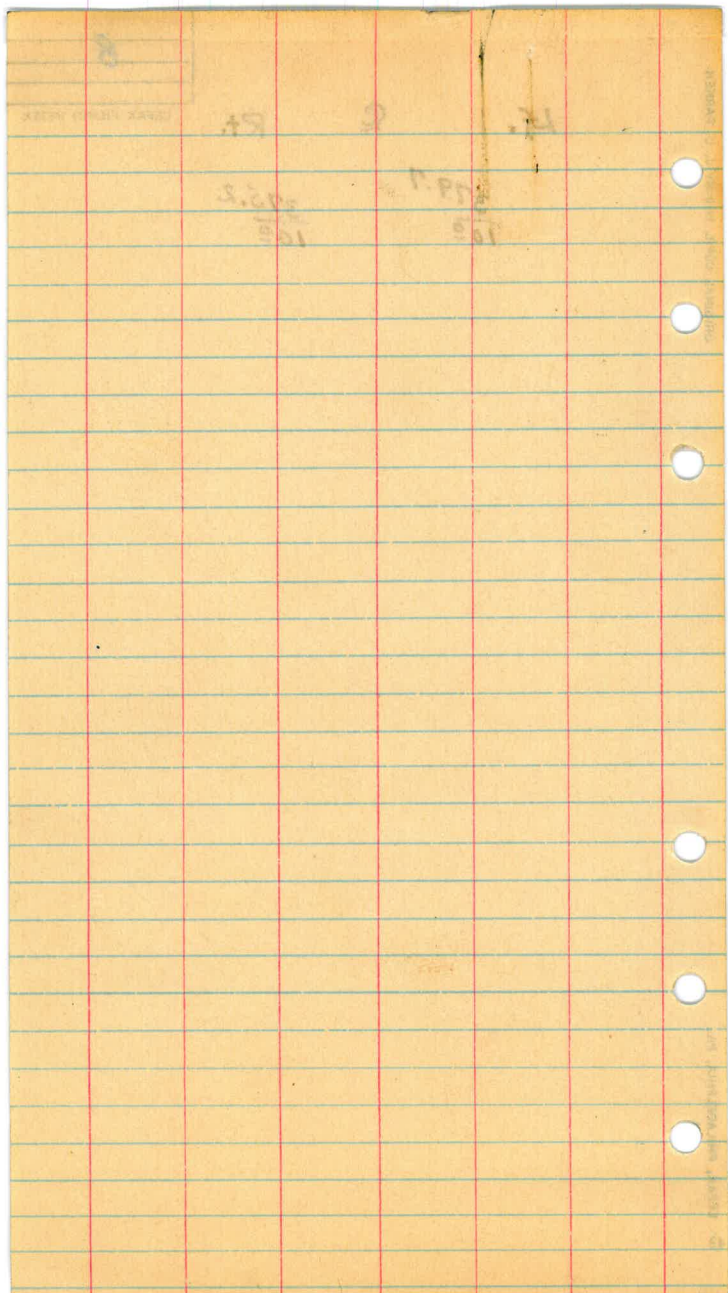
Rt.

$$\frac{379.7}{10^2}$$

$$\frac{375.2}{10^2}$$

LEFAX FILING INDEX

8





Sta	Course	Ang	Mag	Brngs		
0+0	N72°26'W					
	S88°21'W	93°07'	N87°30'W	174.1	✓	X
	S85°14'W					CHAS. M. BOREN
1+74.1	S66°01'W	22°20'L	S69°45'W	179.2	✓	
	S88°18'W					
3+75.3	S67°05'W	3°04'R	S72°35'W	249.0	✓	
	S89°23'W					
6+00.3	S65°10'W	3°55'L		199.5	✓	
	S82°49'W					
7+99.8	S63°36'W	1°34'L	S67°25'W	199.7	✓	
	N83°08'W					
9+99.5	S77°37'W	14°08'R	S81°30'W	198.6	✓	
	N75°30'W					
11+98.1	S85°17'W	7°38'R	S89°00'W	<del>175.7</del> 174.9	✓	
	N83°13'W					
13+73	S77°34'W	7°43'L		74.6	✓	
	N87°38'W					
14+07.6	S73°09'W	4°25'L	S77°00'W	40.4	✓	X
	S82°02'W					
14+48	S62°47'W	10°20'L	S67°00'W	250.3	✓	
	S77°02'W					
16+98.3	S57°49'W	5°01'L	S62°10'W	131.6	✓	
	S77°30'W					
18+22.9	S58°17'W	00 28'R	S62°35'W	124.4	✓	X
	S77°14'W					
19+54.3	S58°01'W	00 16'L	S62°20'W	225.7	✓	X
	N79°46'W					
22+00	S80°01'W	23°00'R	S84°50'W	225.0	✓	
	S88°34'W					
24+25	S67°11'W	11°40'L	S73°10'W	120.0	✓	
	N81°46'W					
25+45	S77°01'W	9°40'R	S82°45'W	255.0	✓	
	S83°48'W					
28+00	S64°35'W	14°26'L	S68°20'W	200.0	✓	
	N71°32'W					
30+00	S83°51'W	18°40'R	S86°50'W	102.0	✓	
34+02	N71°41'W			73.0	✓	Boundary of Forest
	P.O.T.					
34+75	S89°01'W	5°45'R	N86°30'W	239.0	✓	
	N77°47'W					
37+14	S83°00'W	6°00'L	S88°00'W	82.0	✓	
	N63°46'W					
38+00	S82°31'W	4°01'R	N78°00'W	93.0	✓	
	N54°27'W					
38+95	S73°00'W	9°19'R	N68°35'W	183.2	✓	
	N48°37'W					
40+78.2	S67°50'W	5°50'R	N62°45'W	157.5	✓	
	N64°28'W					
42+35.7	S83°41'W	15°51'L	N78°35'W	35.3	✓	
	N74°33'W					
42+71	S84°10'W	10°5'L	N89°15'W	84.0	✓	
	N77°13'W					
43+55	S83°34'W	2°40'L	S88°00'W	237.0	✓	
	N82°13'W					
45+89	S78°34'W	5°00'L	S83°15'W	302.0	✓	
	N79°45'W					
48+90	S81°04'W	2°30'R	S84°26'W	155.0	✓	
	N71°08'W					
50+45	S84°41'W	9°40'R	N87°00'W	238.0	✓	
	N64°03'W					
52+75	N85°16'W	7°00'R	N80°10'W		✓	

ORDER NO.



Station	1st track	2nd track	Creek Bed
0.00			
0.00	1.74		
1.74	17	26	
2.00	17	26	
3.00	17	26	
3.40	Cross fence right angles		
3.90	Wash drainage right		
4.00	14	23	
5.00	7	17	
6.00	13	22	
6.00	13	22	
7.10	14	25	
7.99	4	11	
9.00	7	15	
9.99	10	20	
11.00	10	20	
11.45	Wash drains to right		
11.98	7	16	
13.00	18	27	
13.73	20	27	
14.07	22	31	
14.48	12	20	
15.00	15	23	
16.00	16	25	
18.00	12	20	
18.29	7	16	
18.90	Big wash drains to right		
19.00	17	<sup>26</sup> 21	?
19.54	37	46	
20.44	20	30	



Station	1st track	2nd track	Creek Bed
21.81	7	16	
22.00	5	<sup>13</sup> 8 ?	
24.25	10	20	
25.25	5	13	
25.45	18	28	
26.00	28	35	
26.91	28	35	
28.00	14	23	
30.00	30	40	From sta. 0 to sta. 30 dense brush and large boulders.
31.95	33	43	
33.00	42	50	From sta. 30 to sta. 38 large scattered live oaks and under brush.
34.02	35	44	
34.75	34	42	From sta. 38 to sta. 43.55 solid rock cliff. Line should be benched in to this solid rock.
35.00	33	41	
36.00	16	25	From sta. 45 to sta. 52 large boulders above surface of ground and oak trees and manzanita brush.
<del>37.00</del>	<del>22</del>	<del>31</del>	
37.14	33	41	
38.00	30	37	
38.95	14	23	
39.52	7	15	Creek Bed
40.00	<sup>14</sup> 3	9 ?	25
40.78	7	<sup>16</sup> 11 ?	28
41.00	10	18	31
42.35	6	17	36
42.71	21	30	45
43.55	26	34	50
45.89	31	40	
47.00	4	12	
48.00	9	20	





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LEFAX, PHILADELPHIA, PA.

42

160' Contour

Sta	Ht.	A	L	E	C
0	0	0			
			270'	1,601,438	13,162
2+70	65'	11,862.5			
		36,325	100'	1,716,250	12,000
3+70	95'	24,462.5			
		54,125	70'	1,894,375	10,500
4+40	105'	29,462.5			
		71,225	70'	2,492,875	12,075
5+10	125'	41,562.5			
		86,412	100'	4,320,600	19,125
6+10	130'	44,850.0			
		86,412	90'	3,888,540	17,212
7+00	125'	41,562.5			
		47,525	210'	7,366,375	26,775
9+10	45'	5,962.5			
			40'	119,250	1,350
9+50	0	0		23,399,763	112,199

LEFAX FILING INDEX

150' Contour					
Sta	Ht	A	L	E	C
0	0		230	966,188	9,488
2+30	55	8,662.5 28,425	100	1,421,250	10,500
3+30	85	19,762.5 44,225	70	1,547,875	9,450
4+00	95	24,462.5 59,825	70	2,092,875	11,025
4+70	115	35,362.5 73,762	100	3,688,100	17,625
5+70	120	38,400 73,762	90	3,319,290	15,862
6+00	115	35,362.5 44,025	170	3,742,125	26,675
8+30	55	8,662.5	60	2,598,75	2,475
8+90	0				
			<hr/>		
			17,038,575	98,100	

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# 140' Contour

LEFAX FILING INDEX

Sta	H	A	L	E	C
0					
			190	566,438	3,562
1+90	45	5912.5			
		21,525	100	1,076,250	9,000
2+90	75	15,562.5			
		35,325	70	1,236,375	8,400
3+90	85	19,762.5			
		49,425	170	1,729,875	9,975
4+30	105	29,662.5			
		62,112	100	3,105,600	16,125
5+30	110	32,450.0			
		62,112	90	2,795,940	14,572
6+20	105	29,662.5			
		35,425	170	3,028,125	19,125
7+90	45	5912.5			
			65	193,781	2,194
8+55	0				
				<u>13,731,484</u>	<u>82,893</u>



130' Contour					
Sta	H	A	L	E	C
0	0	0	150	282,188	3,938
1+50	35	3,762.5			
	6	15,425	100	781,250	7,500
2+50	65	11,862.5			
		27,425	70	959,875	7,350
3+20	75	15,562.5			
		40,025	70	1,400,875	8,925
3+90	95	24,462.5			
		51,462	100	2,573,100	14,625
4+50	100	27,000.0			
		51,462	90	2,315,790	13,162
5+50	95	24,462.5			
		28,225	170	2,399,125	16,575
7+50	35	3,762.5			
			60	112,875	525
8+10	0	0			
			10,825,078	72,600	





110' Contour					
Sta	H	A	L	E	C
0	0	0			
0+68	15	862.5	68	29,325	765
		6,825	100	341,250	4,500
1+68	45	5962.5			
		14,625	70	511,875	5,250
2+38	55	8662.5			
		24,225	70	847,875	6,825
3+08	75	15,512.5			
		33,162	100	1,658,100	11,425
4+08	80	17,600.0			
		33,162	90	1,492,290	10,462
4+98	75	15,562.5			
		16,425	170	1,394,125	11,475
6+68	15	862.5			
			34	14,662	382
7+02	0	0			
				<u>6,291,502</u>	<u>51,284</u>

1001 Contour

Sta	H	A	L	E			
0	0				30	2,438	112
0+30	5	162.5					
		3925	10	0	196,250	3,000	
1+30	35	3762.5					
		9,725	70	340,375	4,200		
2+00	45	5962.5					
		17,825	70	623,875	5,775		
2+70	65	11,862.5					
		25,512	100	1,275,000	10,125		
3+70	70	13,650.0					
		25,512	90	1,148,040	9,112		
4+60	65	11,862.5					
		12,025	170	1,022,125	8,925		
6+30	5	162.5					
			12	975	45		
6+42	0	0					
					<u>4,609,678</u>	<u>41,294</u>	

DATE	DESCRIPTION	AMOUNT	BALANCE
10/1	...	...	...
10/2	...	...	...
10/3	...	...	...
10/4	...	...	...
10/5	...	...	...
10/6	...	...	...
10/7	...	...	...
10/8	...	...	...
10/9	...	...	...
10/10	...	...	...
10/11	...	...	...
10/12	...	...	...
10/13	...	...	...
10/14	...	...	...
10/15	...	...	...
10/16	...	...	...
10/17	...	...	...
10/18	...	...	...
10/19	...	...	...
10/20	...	...	...
10/21	...	...	...
10/22	...	...	...
10/23	...	...	...
10/24	...	...	...
10/25	...	...	...
10/26	...	...	...
10/27	...	...	...
10/28	...	...	...
10/29	...	...	...
10/30	...	...	...
10/31	...	...	...



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Sta	Ht	Area	L	Evol
4167	15	862.5		
		1025	25	12,812
4192	5	162.5		375
			13	1,056
5705	0	0		49
				1,956,146
				24,326

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Vol 90 Contour = 110,460  
Coronwall = 1,200

Sta	Ht	Area	L	E	Vol C	Vol
0	0	0				
			12		975	45
0112	5	162.5				
		1025.0	30		15,375	450
0142	15	862.5				
		2925	40		58,500	1,200
0182	25	2,062.5				
		5925	70		203,875	3,150
1152	35	3,762.5				
		12425	70		434,875	4,725
2122	55	8,662.5				
		18862	100		943,100	8,625
3122	60	10,200.0				
		18862	90		848,790	7,762
4112	55	8,662.5				
		12425	62		385,175	4,185
4174	35	3,762.5				
		5825	23		66,988	1,035
4197	25	2,062.5				
		2925	25		54,562	750
5122	15	862.5				
			48			
			32		20,700	540
5170	0	0				
					3,014,915	32,467

LEFAX, PHILADELPHIA, PA.  
42

100,000

Contour	W.S.	Max. Ht. of corn above Ground Surf	Flooded Area - Acres	Cap. Res. Acres Feet	Cap. Res. Million Gallons
Core Wall = 97000					
Vol. 60' Contour = 2					
Sta.	Ht.	Area	L.	Vol Earth	Core
0	0	0	✓		
			35'	2,810	130
0+35	5'	162.5	✓		
			70'	77,875	1,575
1+05	25'	2062.5	✓		
			100'	245,625	4,125
2+05	30'	2850	✓		
			90'	221,062	3,712
2+95	25'	2062.5	✓		
			73'	75,281	1,369
3+48	0	0	✓	623,653	10,911
Vol 80' Contour = 7					
Core Wall =					
Sta	Ht	Area	L	Vol Earth	Core
0	0	0	✓		45
			12'	975	<del>450</del>
0+12	5'	162.5	✓		
		102.5	40'	20,500	600
0+52	15'	862.5	✓		
		292.5	70'	102,375	<del>2100</del>
1+22	25'	2062.5	✓		
		802.5	70'	280,875	3,675
1+92	45'	5962.5	✓		
		<del>6075</del>	100'	660,400	7,125
2+92	50'	7250	✓		
		13,212	90'	594,540	6,412
3+82	45'	5962.5	✓		
		<del>6075</del>	62'	248,775	3,255
4+44	25'	2062.5	✓		
		292.5	28	27,638	690

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LEFAX, PHILADELPHIA, PA.

42

Sto Def Bear Dist. N.S.

63+00

30

38

55

62+60

Wash-R

62+00

61+00

37

45

47

60+15

10°20' L

3/6

10°10' L N54°33' W

21

29

32

60+00

59+22

Wash-R

59+01 P.O.T.

9

18

30

59+00

30

58+00 P.O.T.

8

16

35

58+00

15

26

57+00

7

19

56+02 19°30' R N44°13' W

4/3

13

25

+16 POT

8-6

11

14

?

55+0

12

19

53+0

57.03

8

17

271

 Rice Line Survey  
 Transit Notes  
 5788+0  
 P.S. P.T.  
 LEFAX FILING INDEX  
 Creek  
 Bank



Sta	Defl.	Bear.	Dist.	N.S	F.S.	Remarks
72100			108			Creek Bank
71+06	19°18' R	N89°22' W		16	24	
70+98						
70+00				25	34	
69+42	Cross wagon trail to house					South -
			206			
69+00	6°29' L	S73°20' W		40	50	54
68+00				12	21	
			120			
67+80	21°46' L	S79°41' W		9	17	
67+30				33	42	
			97			
66+83	4°40' L	N78°25' W				
66+00				38	41	65
	19°12' L	N63°45' W	133			
65+50	9°12' L	N73°45' W		32	39	
65+00				40	48	53
64+00				35	43	48 West R
			219			
63+31	P.O.T.			29	38	55



El Cañon  
 Pipe Line Survey  
 Transit Notes  
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LEFAX FILING INDEX

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LEFAX, PHILADELPHIA, PA.

42

Sta	Defl.	Bear.	Dist.	N.S.	F.S.	
81+00				30	38	40
80+00				12	20	28
79+80						
79+00	21°48'L	N76°48'W	260.	6'	14'	20
78+00				14'	22'	27
77+78	34°00'R	N55°00'W	122.0	20	27	33
77+00				6	14	20
76+75				10	20	14
76+00				14	22	32
75+00				23	32	36
74+78	6°20'L	N89°00'W	300.0			
74+00				14	23	36
73+675	P.O.T.	El Monte Ranch line	110.5			
73+00				16	24	
72+14	4°42'R	N82°40'W	153.5	19	28	

40  
 20  
 28  
 33  
 20  
 14  
 20  
 14  
 22  
 32  
 36  
 36  
 24  
 28

Sta.	Defl.	Beat.	Dist.	N.S.	F.S.	Fense Creek
91+00						
90+03			275			
89+25	P.O.T.			43	51	54
88+00			188			
87+37	P.O.T.			33	42	45
87+00						
86+00						
85+36	15°00' L	N65°53' W	200.2	21	33	41' 43"
85+00			69.8			
84+62	12°44' R	N50°53' W		25	31	38
84+00	P.O.T.		67	25	31	37
83+00				13	21	33
82+83	12°11' R	N61°37' W	117	14	23	35
82+00				14	22	37
81+60	P.O.T.		123	22	30	37

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Sta.	Defl.	Beah	Dist	N.S	F.S.	U
102+00				35	49	48
			114			
101+16	P.O.T.		181	17	25	37
101+00				14	23	34
100+00				9	17	27
			181			
99+35	11° 12' L	N79° 56' W		15'	27'	35'
99+00						
98+00				36'	43'	54' 56'
			183			
97+52	14° 35' L	N68° 44' W		33	40	45 48
97+00						
			67			
96+85	1° 38' R	N54° 09' W		34	43	48 50
96+00						
95+00				21	28	33 35
			285			
94+00	8° 30' L	N65° 47' W		20	27	30
93+00						
			200			
42 92+00	18° 36' R	N47° 17' W		23	30	34

E.L. 1001007

Pipe Line Survey

Transit Notes

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LEFAX FILING INDEX



Sta.	Defl.	Beat.	Dist	N.S	F.S.	Fence Creek
114+00						
113+00						
112+78.1	4°08' L	N38°54' W	194.2	Point of hill	185'	R-
110+00				41	49	58
109+00				36	48	62
108+00				35	43	61
107+77.2	38°14' R	N34°46' W	481.1			
107+00				26	35	50
106+77.2						
106+00				28	35	50
105+46.2	21°18' R	N73°00' W	267			
105+00						
104+69.1	18°00' L	S85°42' W	77	15	27	41
103+50.3	3°38' R	N76°18' W	119	23	31	47
103+00				21	28	45
102+30.1	P.O.T.		120	37	45	50



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LEFAX, PHILADELPHIA, PA.

Sta.	Defl.	Beat.	Dist.	N.S.	F.S.	4	0
125+00				57	65	75	
124+00				53	60		
123+73	5'	oak	10' L				
123+00				33	40		
122+75	6'	oak	10' to R.				
122+15	11°50' L	S 71° 42' W	416	11	19		
122+00				11	19		
121+00				12	20		
120+00				10	18		
119+00	P.O.T.		315	9	18		
118+00				9	16		
117+00				10	18		
116+00	9°20' L	S 83° 32' W	300	7	15		
115+00		El Monte Park	1277				
42 114+723	48° 14' L	N 87° 08' W		10	19		

 EL CORREO  
 Pipe Line Survey  
 Transit Notes  
 4

LEFAX FILING INDEX

Sta.	Detl.	Beat.	Dist.	N.S.	F.S.	Fence	Creek
129700	1°26' L				18	26	35
128700					18	26	35
127789	6' oak	6' L					
127700					17	26	31
126731	27°11' L		269		17	25	32
126700					30	38	45
125799	Power Pole	2' R					

S43°05'W

S43°05'W

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LEFAX, PHILADELPHIA, PA.

Sta.	Defl.	Bear	Dist.	N.S.	F.S.
138100				45'R	53'R
137173	36"	oak	6' R		
			242		
137108	51°16'2"	S	6°52' E		
137102	Power Pole		4' L		
136152	30"	oak	18' L		
136100					
135100				16'R	21'R 39'R
134122	30"	oak	12' R		
			308		
134100	2°01'	S	41°24' W	21'R	29'R 40'R
133100	2-24"	oaks	one each side sta.		
			200		
132100	3°20'	S	46°25' W	21'R	29'R 40'R
131100				21'R	29'R 41'R
130100				20'R	28'R 37'R
129150					
			300		
42 129100	1°26'	S	43°05' W	18'R	26'R 35'R

E.I. CARTER  
Pipe Line Survey  
Transit Notes  
5

LEFAX FILING INDEX

Fence



Sta.	Detl.	Beat.	Dist	N.S.	F.S.	fence
			553			
145100	225°28R	SE 129W		12'L	22'L	5'R-37'L
145100				11'L	19'L	3'R-35'L
144100				5'L	14'L	4'R-35'L
			164			
143168	62°19'R	S 29°01'W		6'L	14'L	8'R-35'L
				Entered lane -		
143156				15'L	24'L	8'L-35'L
				← Is in corner of field.		
143100				10'L	20'L	
142156				In Fence line -		
142100				In center of road -		
			268			
141100	26°26'L	S 33°18'E		5'R	13'R	18'R
				West edge of Park -		
140100				28'R	36'R	42'R
			150			
139150				P.O.T.		
139152	24" 09K	5'R 33'R		40'R	73'R	
139144	2-24" 09K	5'R				
139100						
138177	30" 09K	13'L		36'R	44'R	80'R



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LEFAX, PHILADELPHIA, PA.

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E.I. COADITION  
Fine Line Survey  
Transit Notes

LEFAX FILING INDEX

Sta.	Defl.	Beat.	Dist.	N.S.	F.S.		
156+00							
155+63				17'L	32'L	2'R-38'L	
153+00				16'L	30'L	3'L-35'L	
154+40		cross fence					
154+00				15'L	28'L	15'R-35'L	
				S40°38'W 459			
153+00	135°L	S39°13'W?		27'L	41'L	4'R-48'L	
152+00							
157+00							
150+89		Entrance way 15' wide -					
				215'			
→ 150+85	1°25'L S53°14'W						
150+00							
149+00				12'L	30'L	13'R-44'L	
148+00							
147+00							
146+00				12'L	24'L	7'R-38'L	

← fence and shaft →

Sta.	Detl.	Beac.	Dist.	N.S.	F.S.	Fence
166700				8'L	27'L	3'R-50'L
165700				6'L	21'L	6'R-50'L
			252			
164491	23°55'R	56'33"W		4'L	21'L	5'R-50'L
164445						cross fence into lane-
164400				10'L	28'L	5'L-50'L
163488						cross fence turns to R.
163436						cross fence - leave lane
163400				4'L	23'L	2'R-43'L
			281			
162400	8°53'L	59°38'W		4'L	23'L	5'R-38'L
161400				2'L	23'L	8'R-48'L
160400				11'L	33'L	5'R-48'L
159400				10'L	31'L	7'R-46'L
			332			
158408	21°49'R	54°31'W		3'L	25'L	10'R-38'L
158400						
			109			
157459	14°31'L	52°42'W		16'L	36'L	8'R-41'L
157400						

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LEFAX, PHILADELPHIA, PA.

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 EL COPY 17  
 Pipeline Survey  
 Transit Notes  
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LEFAX FILING INDEX

Sta.	Defl.	Bear.	Dist.	N.S.	F.S.	Fe
176+00						
175+00				22'L	35'L	7'R-32L
174+68	17°09'L	S42°37'W	332	25'L	39'L	9'R-53L
174+00				15'L	38'L	9'R-44L
173+00	30°57'L	S59°16'W	168	22'L	43'L	2'R-50L
172+07	31°52'L	N89°17'W	93			
172+00				24'L	39'L	3'R-53L
171+00				3'L	19'L	14'R-32L
170+68	<del>14°03'44"</del> 14°03'44"	N57°23'W?	139	5'R	22'L	16'R-32L
170+00	P.O.T.		68	8'L	28'L	16'R-32L
169+00				15'L	30'L	3'R-39L
168+91		10' Driveway to R				
168+00				8'L	22'L	4'R-43L
167+33	16°51'L	S47°42'W	267	11'L	29'L	6'R-50L
167+00				10'L	25'L	6'R-30L



Sta.	Detl.	Bear.	Dist.	N.S.	F.S.	Fence
190+00						10'R-25'L
			500			
189+00		1°43'R	S38°25'W			
188+00						center of 10' driveway to R.
187+00						
186+00	P.O.T.					
185+00						
184+00			300			
183+00		3°15'R	S36°42'W	15'L	28'L	10'R-35'L
182+90	}	10' driveway to R-				
182+80						
182+40						12" concrete pipe crosses road
181+00						
			300			
180+00		9°10'L	S33°27'W	20'L	35'L	2'R-45'L
179+00						
			200			
178+00	P.O.T.					
177+00				15'L	30'L	6'R-40'L

(Fence continuous on each side along power poles along left fence)



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LEFAX. PHILADELPHIA, PA.

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EL. COL. 11+00  
Pipe Line Sur.  
View: Transit  
Notes 8 (8)

LEFAX FILING INDEX

Sta.	Defl.	Beat.	Dist.	N.S.	F.S.	ℓ
204+00				5'L	15'L	3'R-30'L
203+00				5'L	15'L	3'R-30'L
202+00						3'R-25'L
201+00						3'R-25'L
200+00						3'R-25'L
199+00	P.O.T.		600			3'R-25'L
198+10		Form entrance				10'R-25'L
198+00						10'R-25'L
197+00						10'R-25'L
196+00						10'R-25'L
195+00						10'R-25'L
194+00	P.O.T.		500			10'R-25'L
193+00						10'R-25'L
192+00						10'R-25'L
191+00						10'R-25'L

Sta.	Defl.	Beat	Dist.	N.S.	F.S.	Fence
217+00	P.O.T.			6'L	22'L	6'R-34'L
216+00						Fences road contiguous
215+00						
214+00				8'L	23'L	5'R-37'L
213+00	P.O.T.		400	7'L	22'L	4'R-37'L
212+20						Cross fence
212+00				14'L	25'L	3'L
211+00				12'L	20'L	3'L
210+00				11'L	25'L	3'L
209+00	P.O.T.		400	8'L	26'L	3'L-30'L
208+00				7'L	23'L	2'L-32'L
207+00				In fence line	4'L 19'L	32'L
206+15				10' Driveway to R-		
206+34			266	97° 6'R S85° 31'W	00'L	12'L 9'R
206+00					4'L	16'L 6'R-30'L
205+00	P.O.T.		134	5'L	17'L	3'R-30'L

E.L. ADLTON  
 Pipe Line Survey  
 Transit Notes  
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Sta.	Defl.	Bear.	Dist.	N.S.	F.S.	
221100				12'L	28'L	
			204			
221481	57°00'R	N58°53'W		5'L	17'L	2'R
221600				9'L	20'L	5'R
2215100				11'L	23'L	7'R
221198 221136	} 12' Drive to R					
221400				15'L	30'L	4'R
			314			
2213167	160°31'L	S64°01'W		15'L	30'L	2'R
2213100				6'L	32'L	
			85			
221182	20°41'L	N69°50'W		8'L	33'L	
2212100				8'L	33'L	
221400				8'L	33'L	
219100				8'L	33'L	
			457			
218125	95°20'R	N49°09'W		6'L	25'L	33'L
218100						
217170				6'L	23'L	6'R-35'L
			125			

Fence discontinued



Sta.	Defl.	Bear.	Dist.	N.S.	F.S.	Fence
233715	27°36' L	S48°13' W		11' L	37' L	44' L
233700			80			
232725	6°32' L	S73°9' W		33' L	48' L	
232700						
231700			210			
230725	19°6' L	S79°51' W		35' L	48' L	
230700			83			
229747	22°00' L	N80°53' W		27' L	43' L	
229700			57			
228785	P.O.T.					
228700				26' L	43' L	



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Sta.	Defl.	Beck.	Dist.	N.S.	F.S.	
241+0				8'L	21'L	
240+0				2'A	10'L	
+30	71°15'R	573°34'W	295	5'R	18'R	
239+0	(in Rd)			4'R	17'L	
+70'	Farm Bldgs & sites			30'R		
238+0				15'L	26'L	
237+0				19'L	35'L	41'L
+50	38°12'L	52°39'W	280	26'L	39'L	47'L
236+0				15'L	30'L	
235+0				16'L	35'L	40'
+55	155°2'L	532°51'W	195	15'L	30'L	39'L
234+0				19'L	36'L	45'L
233+15	243°6'L	548°43'W	140	11'L	36'L	↑ Fence
233+0				11'L	36'L	
232+35	6°32'L	573°19'W	80	33'L	48'L	

Road

El Capitan  
Mag Line Survey  
Transit Notes  
(10)

LEFAX FILING INDEX

Stk	Defl	Bring	Dist	NS.	FS.	Fence
+47				9'L	27'L	20'R
248				8'L	25'L	45'L 15'R
+82				7'L	23'L	44'L 13'R
+70				6'L	22'L	43'L 11'R
+58				5'L	20'L	38'L 10'R
+43				4'L	19'L	38'L 3'R
			S 71° 52' W 232			
+40	20° 28' R			4'L	18'L	27'L - 5'R
7				4'L	19'L	27'L 5'R
6				6'L	20'L	36'L
245	< Fence begins on left 36' from line			5'L	30'L	6'R
+30				4'L	16'L	15'R
+10			Private drive to Rt 10' wide 90° angle			
4				4'L	17'L	17'
243				4'L	16'L	10'R
			S 51° 24' W 515			
+25	22° 30' L			15'L	24'L	4'R
242				14'L	26'L	

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LEFAX, PHILADELPHIA, PA.

sto	Defl	bring	dist	NS.	EL 001704 Paco Lima Survey Transit Notes FS (11) LEFAX FILING INDEX Fence
259+0				5'L	32'L 47'L
		N52°16'W	345'		
+55	49°14'R			00'	25'L 34'L 25'R
258				11'L	32'L 36'L 60'R
257+0				9'L	30'L 40'L 29'R
6+0				12'L	26'L 40'L 4'R
255+0	Cross near fence			13'L	28'L 40'L
+10	P. Rivato DRIVE 10' wide			15'L 30'L 40'L 9'L	10'R
254				19'L	36'L 40'L 9'R
253+0				16'L	72'L 16'L 37'L
252				13'L	27'L 5'L 38'L
251+0				10'L	24'L 2'L 30'L
+07	LINE crosses fence				017'R
250				5'L	20'L 27'L 2'R
		S78°30'W	88.3		
+72	6°38'R			5'L	19'L 24'L 5'R
42 249+0				8'L	24'L 27'L



Sta	Defl	Bying DIST	NS	FS	Fence
274			06R	14'R	35' R cliff
273	S 50° 28' W	300	4'R	30'R	40' R cliff
250	17° 59' L		10'L	22'R	
2			5'L	25'R	
1			5'L	22'R	
270			9'L	22'R	
9			5'L	22'R	
8			15'L	11'R	
7			18'L	9'R	
6			10'L	17'R	
5			15'L	24'R	
4			1'L	34'R	
3			00L	34'R	
2	S 68° 27' W	1050	17'L	26'R	
1	59° 14' L (Not over 10' External-sec.)		15'L	26'R	
260			00	20'L	35' L



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LEFAX. PHILADELPHIA, PA.

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Sto	Defl	bring	Dist	NS	FL	112	LEFAX FILING INDEX
5				4'R	20'R	30'R	Fence
			552°00'W 373	9'R	30'R	39'R	
+67	32°54'R						
4				3'R	21'R	30'R	
3				3'R	21'R	44' <sup>R</sup>	
			519°03'W 267	4'R	20'L		
2	35°39'L			0'R	20'L	4'R	
1				0'R	13'R	17'R	
280				1'R	15'R	18'R	
			555°02'W 300				
9	12°56'L			0'R	14'R	14'R	
278				13'R	26'R	33'R	
+37 (Pot)				5'R	21'R	26'R	
+28				3'R	21'R	27'R	
7				0'R	20'R	28'R	
276				11'L	11'R	4' Fence R	
			567°58'W 350			R	
+50	17°30'R			2'R	18'R	24' Fence	
42	275			1'R	18'R	47' Cliff R	

Sta	Defl	bearing	DIST	NS	FS.	Fence
<del>16</del>	<del>8°57'R</del>					
7				2'R	19'R	
296				3'R	19'R	
		S71°21'W	257			
+06	27°12'R			12'R	31'R	
5				10R	30R	
4				4'R	20R	
3				4'R	20R	
2				4'R	20'R	
1				2'R	20'R	
290				3'R	20'R	
9				5'R	21'R	
		S44°09'W	666			
+A0	7°51'L			2'R	19'R	
8				3'R	19'R	
7				3'R	18'R	Fence Right 400 approx
6				3'R	17'R	40'R
285777				4'R	17'R	41'R

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LEFAX, PHILADELPHIA, PA.

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Stk	Defl	bear	Dist	NS	(13)
310+0				3'R	19'R
			N 87° 48' W <sup>398.2</sup>		
+37	11° 45' R			6'R	20'R
9				1'R	19'R
8				1'R	15'R
7				3'R	18'R
6				1'R	20'R
			S 80° 27' W <sup>382</sup>		
+55	7° 07' L			1'R	15'R
5				3'R	19'R
309+0				1'R	19'R
303+0				1'R	19'R
			S 87° 34' W <sup>355</sup>		
302+00	7° 16' R			5'R	18'R
1				1'R	15'R
300+0				1'R	15'R
9				1'R	17'R
298+0				0'R	15'R
			S 80° 18' W <sup>437</sup>		
297+63	8° 37' R			4'R	19'R

FLS 991700  
 Def Lina Survey  
 Transit Notes  
 FLS Fenc  
 LEFAX FILING INDEX

St	Defl	brng	DIST	NS	FS	Fence
180	20 L to Corner of Power H					
+60	" " " "			17'R	35'R	11'L 50'R
+27	Pump H. 12'L					
	Extends back about 50'					
+21	Pump House 11'L					
316 to	Tank 10' Left joins Pump house					
+94	Tank 9' Left					
+74	Tank "					
315	High voltage plant					
	to left 15'					
+837 (Pot)						
	8' 6.3					
				9'R		
314						
				5'R	9'L	
+84						
				00'L	12'L	
+352	549°34' W 42°38' L					
				20'L	32'L	
313						
				15'L	27'L	
+50						
				00'L	11'L	
312	in Rd					
				5'L	7'R	
311						
				1'R	15'R	

Road being widened



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Sta	Defl	bearing	Dist	N.S.	12 L	33 R
328	(Pot)		710			
7					11 L	33 R
6	↓ 6'			20 R	46 R	45 R
5	Pipe 4' R			18 R	32 R	10 L 47 R
324+0				15 R	35 R	10 L 49 R
+25				14 R	35 R	10 L 49 R
3				13 R	35 R	10 L 49 R
2						
1				15 R	37 R	10 L 50 R
320				15 R	37 R	10 L 50 R
319				18 R	38 R	10 L 50 R
318+0	Water pipe 5' R (6" dia)			17 R	37 R	10 L 50 R
+73	" " 5' R			17 R	37 R	10 L 50 R
+60	bunk N. 15' L			17 R	37 R	10 L 50 R
+25	bunk N. 15' left			17 R	37 R	10 L 50 R
						10 L
42				19 R	37 R	45 R

(14)

31740  
 Profile  
 Transit Notes  
 F.S. F.P.C.C.  
 LEFAX FILING INDEX

Stk	Defl	Brng	Dist	NS	FS	Fence
1	POT		482	12' R	32' R	53' R
340						
+15	Powderpot	2' R				
8	fence	Car 2' L				
+68		15' P.Drive on left				
7						
6						
		526° 31' W	590	9' R	27' R	43' R
+10	22° 43' L	Not over	12' Eil/Prnal			
5				10' R	27' R	
4				11' R	21' R	
333				12' R	20' R	42' R
+70		Pipeline 2' R	turns 20° R			42' R
2		↑ Crosses the lane				42' R
331		Pipeline 2' R				42' R
330						13' L 42' R
329		Pipeline 3' R				13' L 42' R

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LEFAX, PHILADELPHIA, PA.

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 EL (cont'd)  
 2nd Line Survey  
 Transit Notes

LEFAX FILING INDEX

Sta.	Defl.	Beat.	Dist.	M.S.	F.S.	Fence
3				17'R	40'R	$\frac{3'}{2}$ $\frac{60'}{R}$
2	+15°	Power pole	2'R			
1		Pot	5-00			
					DIRECT	
	350					
	+92	10' Drive	Left Ring			
					↓	
9				5'R	24'R	$\frac{3'}{2}$ $\frac{53'}{R}$
					↑	
8						
					DIRECT	
7						
					↓	
6			527°20'45"18			
	+82	0°29'18"		5'R	25'R	$\frac{3'}{2}$ $\frac{53'}{R}$
	+15	Power pole	2'R			
5				7'R	26'R	$\frac{3'}{2}$ $\frac{53'}{R}$
4				9'R	27'R	$\frac{3'}{2}$ $\frac{53'}{R}$
3				9'R	28'R	$\frac{3'}{2}$ $\frac{53'}{R}$
42	34270			72'R	30'R	$\frac{3'}{2}$ $\frac{53'}{R}$
				12'R	30'R	$\frac{3'}{2}$ $\frac{53'}{R}$

Sta. Defl. Beat. Dist. N.S. F.S. Fence

+92 Pepper tree 7' R End of Row  
 1'  $\frac{4'}{L}$

+50 telephon pole 3' left

360

+81 15' drive left  $\frac{5'}{L} \frac{55'}{R}$

9

8

7

+50 Row of Pepper trees 7' R

356 POT 492 25' R 35' R 4' L 53' R

+55 Power pole 2' R

+28 Bridge in Rd  $2\frac{1}{2} \times 16$  openings

5  $\frac{16'}{R}$  43' R  $\frac{2'}{L} \frac{60'}{R}$

354  $\frac{2'}{L} \frac{60'}{R}$

Row of trees direct

DIRECT





Sta	Defn	bear	Dist	NS	FS	FR
380				2'R	22'R	37'R
9		030°18'5				
8	1-22°E	581°06'W	500	3'R	23'R	35'R
7				4'R	25'R	37'R
6				5'R	24'R	36'R
5				8'R	23'R	35'R
4				Line	24'R	36'R
373				4'R	16'R	38'R
+43	NW Cor of Grove	on Left	15'			
		582°28'W	600			
372	1°41'R			3'R	23'R	
1	Pot		100			
+83	Property Line Stake	4x4	RS 57.5'			
370						
9						
8						
367				7' R	25' R	45'R

Sta. Dept. Bear. Dist. N.S.

396

395

394

393 P.O.T.

392

391

390

389

388 P.O.T.

387

386

385

384

383 P.O.T.

382

381

581-06W  
900581-06W  
500

581-06W 500

581-06W

(17)  
 Line is on left side of road along fence.  
 From 392 - 396; borders and yard on left of road.  
 Fence about 15' left of line from 381 to 393

El Capitan  
 Base Line Survey  
 Transit Notes  
 F. S. Pence  
 LEFAX FILING INDEX

Fence and trees intermingled along here  
 at 10' from ft. side of road.  
 Road continues 20' wide along fence.  
 Telephone line runs about 5' ft. of roadside.

Outline 20'R 30'R

2'R 22'R 37'R









Sta	Defl	Bear	Dist	NS	FS	Force
2	Pat.			10	28	
1						
430				Concrete Pavement.		
+94						
9				10	28	
+94		581°4'W				
+14	51°48'L		Concrete Pavement 10' R.	10	28	
8						in vacant Block
7				"	"	"
6				10	10	
5				10'R	24'R	
+95			End of fence on left			
+30			Mibbey's well - 20' L x 1'			
+22			Power pole G.L.			
			N46°58'40" 398			
+16	12°41'W					
4				9'R	24'R	
423				5'R	21'R	





Sta	+	-	∇	Elev	Hyd. Grd.
Top Hub		4.924		518.533	
6+86 <sup>1</sup>		5.21		518.247	
6+00 <sup>3</sup>		3.34		580.117	594.0
T.P.	5.888	0.618	583.457	511.509	
4+98		3.40		514.98	
4+00		5.70		511.35	594.2
3+85		8.00		510.87	
3+51 <sup>2</sup> A		1.63		516.557	
T.P.	3.755	10.148	518.787	514.432	on Rock
3+00		5.89		518.79	594.4
2+00		4.43		580.25	594.6
1+74 <sup>1</sup> A		3.52		581.16	
1+51		2.2		582.48	
1+29		5.350		519.33	
T.P.	12.520	1.516	584.680	512.160	on Rock
1		0.00		519.736	594.8
+68 <sup>2</sup>		3.3		516.436	
0+00		8.600		511.136	595.00
	8.276		519.736		
B.M. Nail in tree	SS. Road			511.460	



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LEFAX, PHILADELPHIA, PA.

LEFAX FILING INDEX

2

El Capitan Pipe Line			Survey	Hyd.	Keeler
Sta	+	Levels #1	Elev	Grd.	Leach Simpson Oct 1935
18+29 <sup>9</sup>		3.853	569.778		
18+00		4.14	568.89	591.8	
16+98 <sup>3</sup>		4.25	568.98	592-	
+62 Bottom Bank		9.65	563.38		
+23 Bank of Wash		10.55	562.48		
+16 1/2 Wash		11.0	562.03		
+10 Bank of Wash		9.1	563.93		
16+00		7.56	565.47	592.2	
T.P. or rock	5.808	10.302	573.631	567.223	
15+00		8.22	569.3	592.4	
14+48		6.15	571.37		
T.P.	2.84	6.494	571.525	574.665	
14+00		1.16	580.62	592.6	
13+73 <sup>8</sup>		2.63	578.55		
13+00		2.65	598.53	592.8	
11+98 <sup>1</sup>		4.25	576.93	593-	
T.P. L.Rd. Lath Hub	11.530	6.94	581.783	569.653	
11+00		4.10	571.993	593.2	
Top Hub T.P.	5.803	6.100	576.993	570.690	
9+99 <sup>5</sup>		3.62	573.98	593.4	
+15		5.4	571.99		
+07		7.3	569.79		
9+00		5.16	571.63		
Top Hub	6.092	11.713	576.870 576.790	570.798	
7+99 <sup>8</sup>		11.91	570.65	593.8	
7+10		6.93	575.48		
T.P. Top Hub	3.878	49.24	582.511 582.411	578.623 578.533	
6+86-					

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3  
LEFAX FILING INDEX



El. Capitan Pipe Line Survey				14	Oct 1928	Keeler Heach Simpson
Levels #1				4	Hqd.	
Sta	+	-	∩	Elev.	Grd.	
T.P.						
30+25	7.520	10.302	570.913	563.253		
29+63 P.O.T.		6.52		561.63		
29+00		4.3		569.25	589.8	
T.P.	2.447	11.668	573.555	561.108		
28+90		9.433		573.343	B.M.	
T.P.	0.309	9.309	582.776	582.467		
28+00		10.8		580.9	590-	
T.P.	4.810	12.653	591.776	586.966		
27+50		6.80		592.82		
27+25		2.00		597.62		
26+91		0.2		599.42	590.2	
T.P. on rock	6.304	7.467	599.619	593.315		
26+00		0.95		599.22	590.4	
25+45		1.0		599.78		
T.P. on rock	12.753	3.219	600.982	588.629		
24+25		2.86		588.4		
23+98		2.1		589.25	590.6	
23+00		6.35		584.9	590.8	
T.P. on rock	11.576	0.755	591.248	579.672		
22+00		10.27		570.25	591-	
21+00		6.74		573.68	591.2	
20+44 P.O.T.		6.28		574.74		
+18				571.3		
20+00		4.11		576.31		
T.P.	3.55	0.437	580.427	576.877		
19+54		1.00		576.31		
19+00		11.1		566.3	591.6	
+92		12.31		565.4		
+52		12.71		564.7		
18+47 Top Bank		8.55		568.96		
18+29	8.136	3.853	577.314	569.78		



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LEFAX FILING INDEX

Sta	+	-	∧	Elev	H grd
T.P.	7.409	1.668	561.344	553.935	
+71		5.22		550.38	
+35		7.25		548.35	
42+00		4.31		551.29	
+55				542.46	
41+00		4.37		551.23	
B.M.	0.786	9.002	555.603	554.867	
T.P.	4.603	8.771	563.869	559.266	
40+82		8.2			
40+58		14.34		553.897	
40+38		22.6		547.437	
40+00		21.83		546.207	
38+95		1.58		566.457	
T.P.	3.670	1.021	568.537	564.367	
38+00		4.78		560.6	
37+00		2.78		562.6	
T.P.	4.895	1.448	565.388	560.493	
36+00		8.65		553.29	
35+00		5.22		556.69	
34+75		3.96		557.98	
T.P.	1.97	12.153	561.941	559.971	
34+00		10.86		561.26	
33+00		3.64		568.48	
32+95		3.28		568.84	
T.P.	3.676	2.425	572.124	568.536	
B.M.		1.78		569.98	
30+65		2.16		568.71	
31+95		4.65		566.22	
31		4.51		566.36	

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sta	+	-	∧	Elev	Hyd Grd
T.P		5.503		535.315 ✓	
54+00		4.6		<del>535.7</del> 536.7	
53+00		4.5		536.35 ✓	
52+00		4.16		536.69 ✓	585.4
T.P	4.158	12.1163	540818	536.60 ✓	
B.M.		5.034		544.089 ✓	
51+00		5.35		543.77 ✓	585.6
50+45		5.66		543.46 ✓	
T.P	4.292	8.109	549173	544.831 ✓	
50+00		7.82		545.12 ✓	585.8
49+75		9.91		543.03 ✓	
+90		4.35		548.59 ✓	
48+00		14.42		538.52 ✓	586-
47+00		16.12		536.92 ✓	586.2
46+00		3.57		549.37 ✓	586.4
T.P	4.099	12.503	552.940	548.841 ✓	
45+89		9.9		551.44 ✓	
45+00		9.92		551.42 ✓	
44+00		4.65		556.69 ✓	
+55		3.75		557.59 ✓	
43+00		6.9		554.44 ✓	587-



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10	10	10	10
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93	93	93	93
94	94	94	94
95	95	95	95
96	96	96	96
97	97	97	97
98	98	98	98
99	99	99	99
100	100	100	100

Sta	+	-	∧	Elev.	Hyd Grd
El Capitan Pipe Line Survey					
+60		0.1		549.1 ✓	
68+20		12.5		536.7 ✓	
68		12.9		536.3 ✓	592.4
T.P.	13.095	1.019	549.198 ✓	536.103 ✓	
67+80		7.5		535.6 ✓	
68+32		7.5		535.6 ✓	
T.P. <sup>in oak</sup>	0.972	12.815	543.122 ✓	542.150 ✓	
67		6.0		549.9 ✓	
66		2.4		552.5 ✓	
T.P.	5.010	0.290	554.965 ✓	549.955 ✓	
+50		0.2		550.5 ✓	
65		3.7		546.3 ✓	
64		16.6		533.6 ✓	
+45		18.4		531.8 ✓	
+40		14.6		535.6 ✓	
+31		15.1		535.1 ✓	
63		16.3		533.9 ✓	
T.P.	12.185	10.255	550.245 ✓	538.060 ✓	546.345 ✓
60+42	B.M. on Oak C.L. &	1.970		548.315 ✓	549.3 ?
62		9.0		538.3 ✓	
61		6.5		541.8 ✓	
60		2.7		545.6 ✓	
T.P.	11.705	2.583	548.315 ✓	536.610 ✓	
+84		6.1		533.1 ✓	
58		3.3		525.9 ✓	535.9
57		3.8		535.4 ✓	
56+02		3.9		535.3 ✓	
+16	.607			539.8 ✓	
55+00		1.5		537.7 ✓	
T.P.	3.878	5.503	539.193 ✓	535.315 ✓	58
54+00		4.6	540.818 ✓	526.2 ✓	536.2

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Sta	+	-	←	Elev.	Hyd Grd
El Capitan Pipeline Survey					
T.P.	12.442	0.190	539.434	526.992	✓
83+00		1.2		526.0	591.2 ✓
82+93		0.6		526.6	✓
T.P.	3.024	10.731	527.182	524.158	✓
82+10		8.3		526.1	✓
+60		7.2		527.2	✓
81		3.8		530.6	✓
80		1.9		537.5	✓
T.P.	1.926	2.354	534.389	532.463	✓
79		2.9		531.9	✓
78		3.0		531.8	✓
77		1.5		527.3	✓
BM on Oak 76+75		4.558		530.259	✓
76+75		7.9		526.9	✓
T.P.	6.458	12.447	534.818	528.359	✓
76		1.6		529.2	✓
T.P.	1.868	8.070	540.806	538.938	✓
75		7.7		539.3	✓
74+78		6.6		540.4	✓
74		7.8		539.2	✓
+615		1.3		539.7	✓
73		2.2		544.8	592.1 ✓
T.P.	3.120	11.729	547.008	543.888	✓
+14		6.7		548.9	✓
72		1.3		548.3	✓
T.P.	2.621	2.249	555.617	552.996	✓
+98		5.0		550.2	✓
70		4.6		550.6	✓
69		3.2		552 -	✓
	7.010	0.963	555.715	548.735	✓



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LEFAX FILING INDEX

Sta	+	-	∧	Elev	Hyd Grd
El Capitan Pipe Line Survey					
T.P.	9.116	3.943	570.302	561.186	✓
91			13.2	551.9	589.4 ✓
90+03			15.9	549.2	✓
+95			4.5	560.6	✓
T.P. 89+80	3.452		565.229	561.677	✓
U.S. Geo B.M.		6.304		571.151	U.S. Elev = 529.85
T.P.	2.543	11.157	533.455	530.912	✓
T.P.	1.038	12.953	542.070	541.032	✓
90+03 T.P.	2.253	12.455	553.965	551.732	✓
T.P. 89+95	2.510	0.598	561.187	561.677	556.3 ✓
		3.5		558.8	✓
T.P.	12.093	4.703	562.275	550.182	✓
88		4.2		550.6	589.7 ✓
8737		5.1		549.9	
T.P.	11.278	1.743	551.885	543.607	✓
87		2-		543.3	589.8 ✓
86		7.9		537.4	589.9 ✓
B.M. Oak Tree 84+00 = 7L				541.421	
T.P.	10824	6.288	545.350	544.266	✓
85+366		6.3		544.2	✓
85.5		6.4		544.7	591 ✓
+67		2.2		548.3	
84		10.8		539.8	✓
T.P.	11.932	0.812	550.554	538.622	✓



Sta	+	-	Σ	Elev	Hyd Grd
El Capitan Pipe Line Survey					
T.P	3.099	7.913	529.310	526.211	✓
+53		8.1		526-	✓
+20		4.8		529.3	✓
102		3.1		531-	✓
+65		4.8		529.3	✓
+41		8.6		525.5	✓
+16		4.6		529.5	✓
101		6.1		528-	✓
T.P	2.678	0.919	534.124	531.446	✓
+18		5.1		527.3	✓
100		4.5		527.9	✓ 588.5
99+35		7.0		525.4	✓
T.P.	4.709	12.060	532.365	527.656	✓
99		10.0		527.9	529.7 ✓
98		1.8		537.9	✓
T.P.	0.759	10.820	539.716	538.957	✓
+52		5.4		544.4	✓
97		2.7		547.1	✓
B.M. nail in oak 22' 96+85 Hole		2.420		547.357	✓
96+85	4.695	7.972	549.777	545.082	✓
+85		8.1		544.9	✓
96		4.9		548.1	✓
T.P.	2.110	10.770	553.054	550.944	✓
95		9.5		556.2	552.2 ✓
T.P.	2.354	8.212	561.714	559.360	✓
T.P. RW Hole 94	2.542	5.272	567.572	565.030	589.1 ✓
93		11.1		559.2	✓
92		2.6		567.7	589.3 ✓
			570.302		





Sta	+	-	∧	Elev.	Hyd. Grd.
El Capitan Pipeline Survey					
T.P.	0.206	11.684	568.698	568.492	✓
113		11.8		568.4	✓
BM Nail in oak 20' to 113 + 00 + 78'		5.484		574.692	✓
		4.1		576.1	✓
112 + 66		4.8		575.4	✓
T.P.	11.309	1.247	580.176	568.867	✓
T.P.	11.179	1.198	570.114	558.935	✓
112		9.9		550.2	✓
T.P.	12.650	1.445	560.133	547.483	✓
T.P.	12.400	1.989	548.928	536.528	✓
T.P.	11.683	0.917	538.517	526.834	✓
111		6.7		521.1	✓
+ 75		10.8		517	✓
110		12.3		515.5	✓
T.P.	7.985	12.595	527.751	519.766	✓
109		12.6		519.8	✓
+ 58		13.0		519.4	✓
108		2.7		529.7	✓
107 + 97		2.0		530.4	✓
T.P.	3.566	1.949	532.361	528.795	✓
107		5.2		525.5	✓
106		0.4		530.3	✓
T.P.	2.296	0.044	530.744	528.448	✓
+ 46		0.3		528.2	✓
105		5.4		523.1	✓ 588-
104 + 69		4.6		529	523.9
T.P.	10.937	11.755	528.492	517.555	✓
104		5.9		523.4	✓
+ 50		3.3		526	✓
103		2.5		526.8	✓

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LEFAX FILING INDEX

Faint, illegible handwritten entries on a grid background, possibly representing a filing index or ledger. The text is mostly obscured by bleed-through from the reverse side of the page.

Sta + -  $\times$  Elev Hyd. Grd.  
 El Capitan Pipe Line Survey

120		3.9		508.7	586.5
119		3.6		509	
118 T.P.	3.218	5.713	512.559	509.340	
117		4.9		510.2	
116		4.3		510.8	
115		4.3		510.8	587-
114+49		3.9		511.2	
T.P.	2.773	12.782	515.053	512.260	
114		5.0		520.1	
T.P.	0.764	11.287	525.062	524.298	
T.P.	1.272	12.135	535.585	534.313	
T.P.	0.863	11.205	546.448	545.585	
T.P.	0.862	12.770	556.790	555.928	



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Sta + - T Elev  
El Capitan Pipe line

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LEFAX FILING INDEX

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Sta	+	-	T	Elev
140		4.0		502.4 ✓
139+50		4.4		502.0 ✓
139		4.7		501.7 ✓
138		4.5		501.9 ✓
T.P.	4.560	6.492	506.390	<del>501.830</del> 501.830 ✓
137		5.2		502.1 ✓
136		5.0		502.3 ✓
135		4.9		502.4 ✓
B.M. Nail in Gas Co Pole #71104		3.902		<del>503.405</del> 503.410 ✓
134		4.4		502.9 ✓
133		3.6		503.7 ✓
132		3.4		503.9 ✓
T.P.	3.030	6.083	507.312	<del>504.290</del> 504.292 ✓
131		5.9		504.5 ✓
130		5.4		505.0 ✓
129		4.7		505.7 ✓
128		4.8		505.6 ✓
127		4.6		505.8 ✓
126+31		4.1		<del>506.3</del> 506.3 ✓
T.P.	4.996	6.569	510.365	<del>505.367</del> 505.367 ✓
126		5.5		506.4 ✓
125		4.5		507.6 ✓
124		4.3		507.6 ✓
123		4.1		507.8 ✓
T.P.	4.224	4.844	511.938	507.714 ✓
122		4.6		508 — 586.3 ✓
121+00		4.6		508 — 586.2 ✓
B.M. Nail in Gas Co Pole #73502		3.792		508.766 ✓
			512.558	

FRANK LITER BOOK

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100	100	100	100	100	100

FRANK LITER BOOK

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Sta	+	-	⌞	Elev.	
160	.	8.5		500.3	
159		8.2		500.6	
158+69		4.4		504.4	
B.M.		7.657		501.133	Mail in Sky Tree o.R. 158+00
158		4.5		504.3	
157+89		5.9		502.9	
157		5.9		502.9	
T.P.	5.563	6.624	508.790	503.227	
156		8.2		501.7	
155		11.3		598.6	
154		12.0		497.9	
153		10.7		499.2	
152		9.0		500.8	
T.P.	6.575	12.042	509.881	503.276	= Sta 151+00
150		9.6		505.7	584.5
149		9.1		506.2	
148		7.1		508.2	
T.P.	1.335	12.740	515.318	513.983	
147		12.8		513.9	
146		6.4		520.3	
145+32		3.3		523.4	
145		3.1		523.6	
143+68		3.2		523.5	
T.P.	4.032	1.060	526.723	522.611	
143		6.0		517.8	
T.P.	11.918	1.092	523.751	511.833	
142		.4		512.5	
141		6.4		506.5	
+68		4.1		508.8	
140+30		9.5		505.4	
T.P.	0.295	6.830	512.925	506.095	-?

13

LEFAX FILING INDEX

Hyd. Gnd = 583.5

Mail in Sky Tree  
o.R. 158+00

= Sta 151+00

584.5

1	2	3	4	5	6
1.00	1.00	1.00	1.00	1.00	1.00
2.00	2.00	2.00	2.00	2.00	2.00
3.00	3.00	3.00	3.00	3.00	3.00
4.00	4.00	4.00	4.00	4.00	4.00
5.00	5.00	5.00	5.00	5.00	5.00
6.00	6.00	6.00	6.00	6.00	6.00
7.00	7.00	7.00	7.00	7.00	7.00
8.00	8.00	8.00	8.00	8.00	8.00
9.00	9.00	9.00	9.00	9.00	9.00
10.00	10.00	10.00	10.00	10.00	10.00
11.00	11.00	11.00	11.00	11.00	11.00
12.00	12.00	12.00	12.00	12.00	12.00
13.00	13.00	13.00	13.00	13.00	13.00
14.00	14.00	14.00	14.00	14.00	14.00
15.00	15.00	15.00	15.00	15.00	15.00
16.00	16.00	16.00	16.00	16.00	16.00
17.00	17.00	17.00	17.00	17.00	17.00
18.00	18.00	18.00	18.00	18.00	18.00
19.00	19.00	19.00	19.00	19.00	19.00
20.00	20.00	20.00	20.00	20.00	20.00
21.00	21.00	21.00	21.00	21.00	21.00
22.00	22.00	22.00	22.00	22.00	22.00
23.00	23.00	23.00	23.00	23.00	23.00
24.00	24.00	24.00	24.00	24.00	24.00
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27.00	27.00	27.00	27.00	27.00	27.00
28.00	28.00	28.00	28.00	28.00	28.00
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33.00	33.00	33.00	33.00	33.00	33.00
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35.00	35.00	35.00	35.00	35.00	35.00
36.00	36.00	36.00	36.00	36.00	36.00
37.00	37.00	37.00	37.00	37.00	37.00
38.00	38.00	38.00	38.00	38.00	38.00
39.00	39.00	39.00	39.00	39.00	39.00
40.00	40.00	40.00	40.00	40.00	40.00
41.00	41.00	41.00	41.00	41.00	41.00
42.00	42.00	42.00	42.00	42.00	42.00
43.00	43.00	43.00	43.00	43.00	43.00
44.00	44.00	44.00	44.00	44.00	44.00
45.00	45.00	45.00	45.00	45.00	45.00
46.00	46.00	46.00	46.00	46.00	46.00
47.00	47.00	47.00	47.00	47.00	47.00
48.00	48.00	48.00	48.00	48.00	48.00
49.00	49.00	49.00	49.00	49.00	49.00
50.00	50.00	50.00	50.00	50.00	50.00

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LEFAX, PHILADELPHIA, PA.

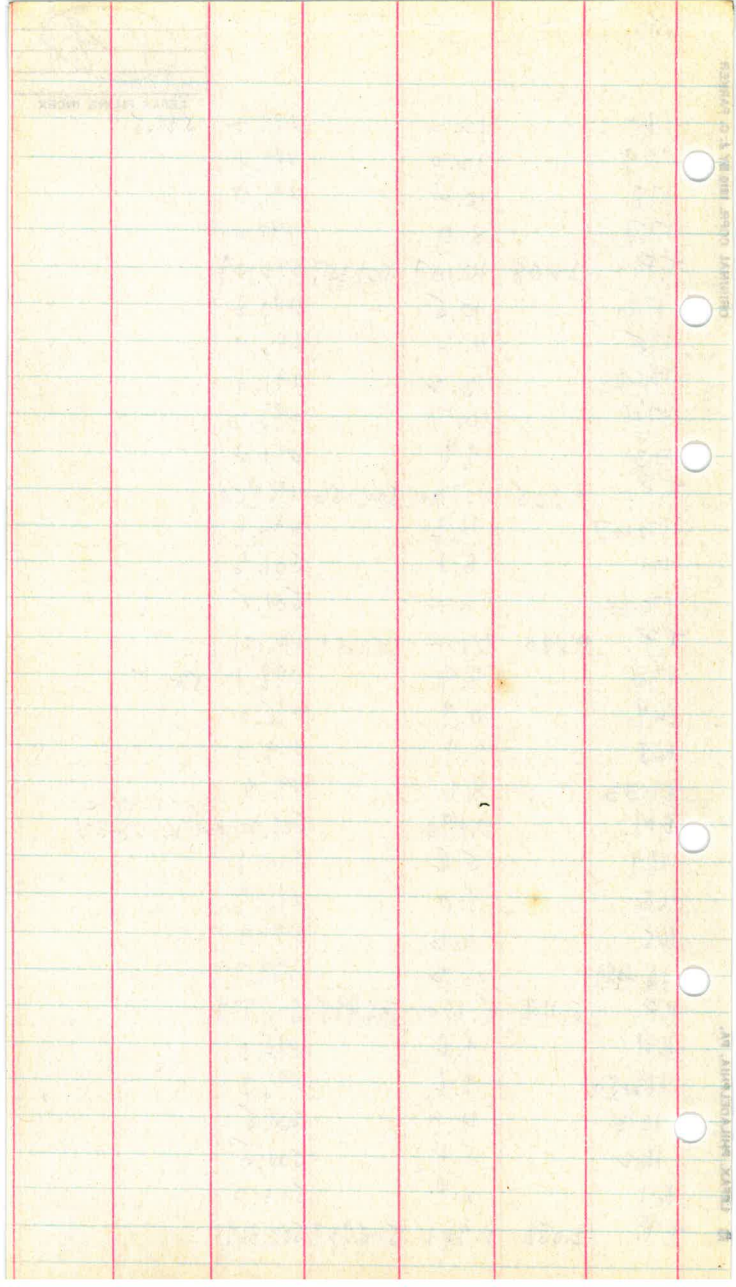
42

Sta	+	-	T	Elev.
180		12.2		489.2
179		12.0		489.4
178		10.4		491.0
177		8.0		493.4
T.P.	7.208	10.107	501.357	494.149
176		10.5		493.8
175		11.6		492.7
174+68		13.2		491.1
174		10.7		493.6
173		9.9		494.4
T.P.	8.305	11.700	504.256	495.951
172+07		11.6		496.1
171		6.1		501.6
170+68		6.2		501.5
T.P.	9.480	7.724	507.651	498.171
170		7.8		498.1
169		10.9		495.0
168		7.9		498.0
167+33		8.1		497.8
B.M.		0.890		505.000
167		5.8		500.1
166		9.0		496.9
165		6.6		499.3
164+81		6.2		499.7
T.P.	5.118	5.150	505.895	500.777
164		9.6		496.3
163+50		9.6		496.3
163		4.4		501.5
162		5.4		500.5
161		2.9		503.0
T.P.	2.058	4.921	505.927	503.869

(14)

Hud Ord  
LEFAX FILING INDEX  
581.5

Mail in Case  
581.5 L 167+33



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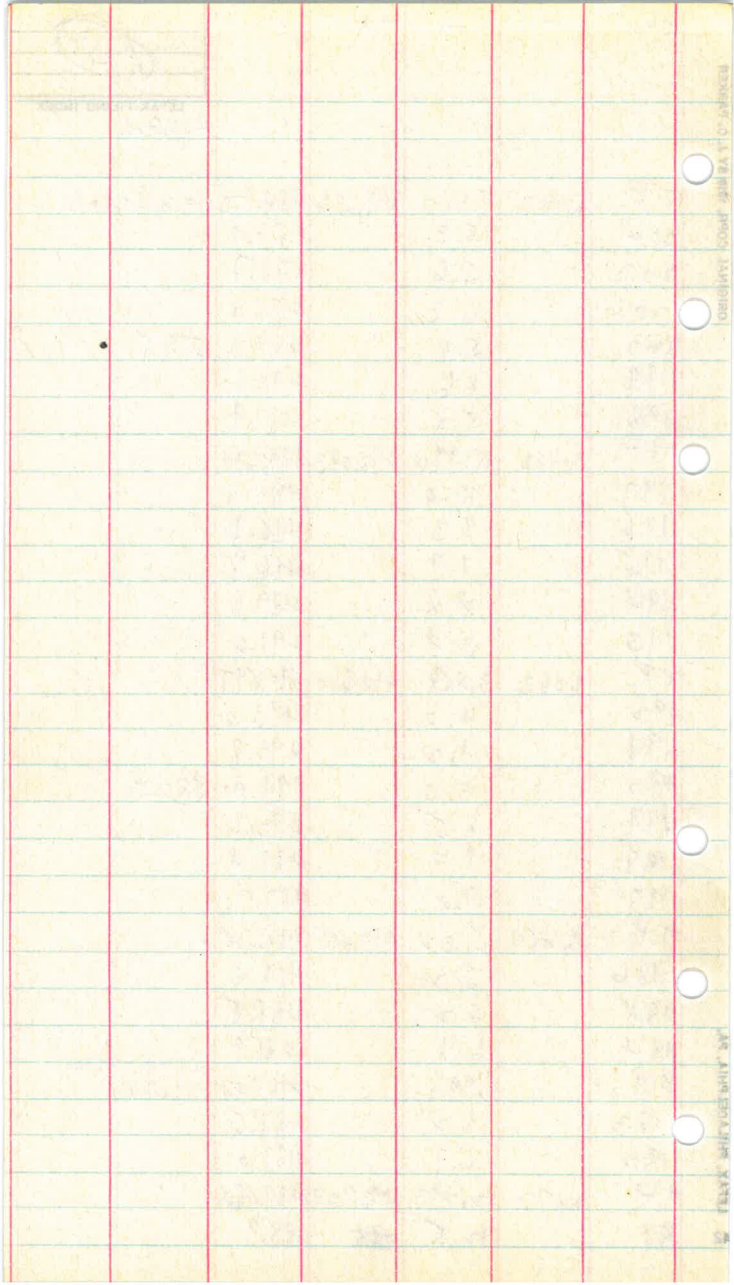
42

Sta	+	-	X	Elev	
T.P.	6.183	7.310	491.156	484.973	= 205100
204		5.3		487.0	
203		5.6		486.7	
201		6.3		486.0	
200		5.0		487.3	579.5
199		1.6		490.6	
198		5.5		487.9	
T.P.	3.613	5.990	492.283	488.670	
197		10.0		484.6	
196		9.3		485.3	
195		7.7		486.9	
194		4.8		489.8	
193		3.4		491.2	
T.P.	1.063	3.458	494.660	493.597	
192		4.0		493.0	
191		4.2		492.8	
190		3.0		494.0	580.5
189		4.5		492.6	
188		8.7		488.4	
187		9.4		487.7	
T.P.	8.450	5.132	497.055	488.605	
186		5.2		488.5	
185		5.2		488.5	
184		6.9		486.8	
B.M.		1.990		491.747	Mail Tel Note #73948
183		6.2		487.5	
182		6.7		487.0	
T.P.	4.673	12.293	493.737	489.064	
181		12.5	<del>493</del>	488.9	

LEFAX FILING INDEX

Hyd. Gvd.

15





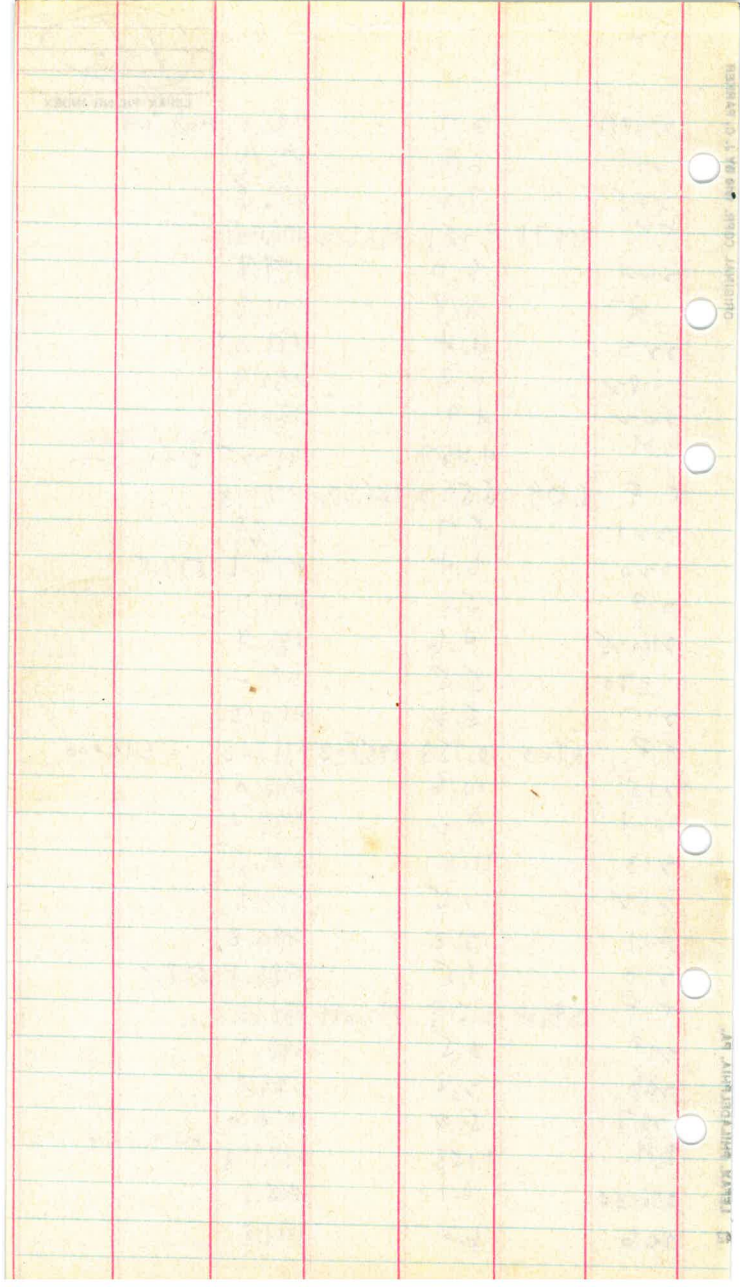
ORIGINAL COPY. #10 BY J. C. PARKER

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Sta	+	-	X	Elev	
226+81		3.7		480.0	Hyd. Gvd
226		6.8		476.9	
225		7.2		476.5	
T.P.	7.271	9.251	483.672	476.401	
224		8.0		476.8	
+67		8.9		476.8	
223		4.4		481.3	
+82		4.8		480.9	
222		4.9		480.8	
B.M.		4.427		481.225	Nail in Oak Sta 221+00
T.P.	5.679	5.570	485.652	479.973	
221		5.7		479.8	
220		6.4		479.1	577.5
219		5.8		479.7	
218+25		4.6		480.9	
+70		5.5		480.-	
217		5.2		480.3	
T.P.	3.700	10.758	485.543	481.843	= 216+00
215		10.6		482.0	
214		9.2		483.4	
213		11.1		481.5	
212		12.5		480.1	
211		12.3		480.3	
210		9.5		483.1	578.5
T.P.	3.964	2.519	492.601	488.637	
209		2.5		488.7	
208		2.8		488.4	
207		5.2		486.0	
B.M.		3.158		487.998	Point on route
206+34		6.1		485.1	
206		6.4		484.8	

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42

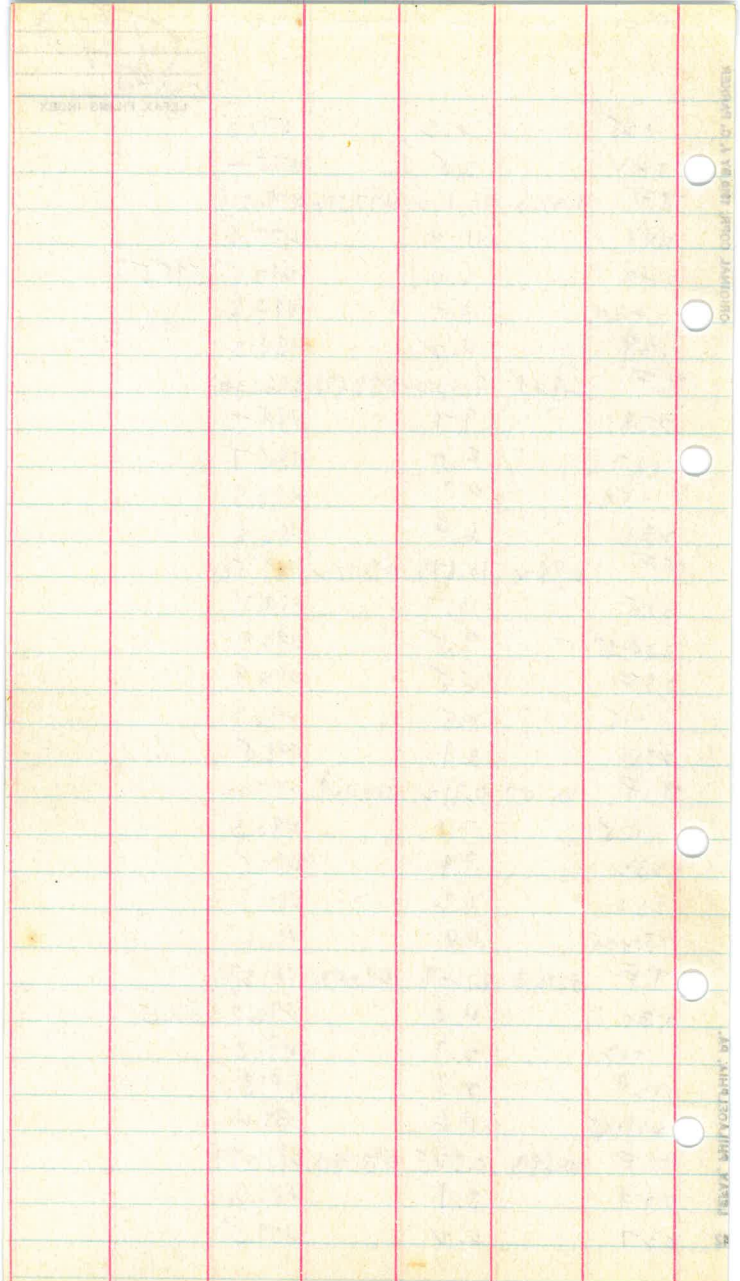
Sta	+	-	K	Elev
245		4.2		473.3
242		2.5		475-
T.P.	1.000	12.162	477.516	476.316
241		11.4		477.1
240		6.0		482.5
+30		3.9		484.6
239		4.2		484.3
T.P.	2.848	8.102	488.478	485.630
238		9.7		484-
237		8.0		485.7
+50		9.9		483.8
236		6.9		486.8
T.P.	3.982	10.679	493.732	489.750
235		10.7		489.7
234+55		9.5		490.9
234		5.5		494.9
+15		3.5		496.9
233		3.9		496.5
T.P.	10.707	0.712	500.429	489.722
+35		7.1		483.3
232		9.9		480.5
231		6.6		483.8
230+25		4.8		485.6
T.P.	3.063	6.609	490.434	487.371
230		4.0		490.0
+42		2.7		491.3
229		2.9		491.9
228+85		4.6		489.4
T.P.	10.683	0.375	493.980	483.297
228		3.1		480.6
227		4.2		479.5

Hud. Div.

LEFAX FILING INDEX

575.5

576.5





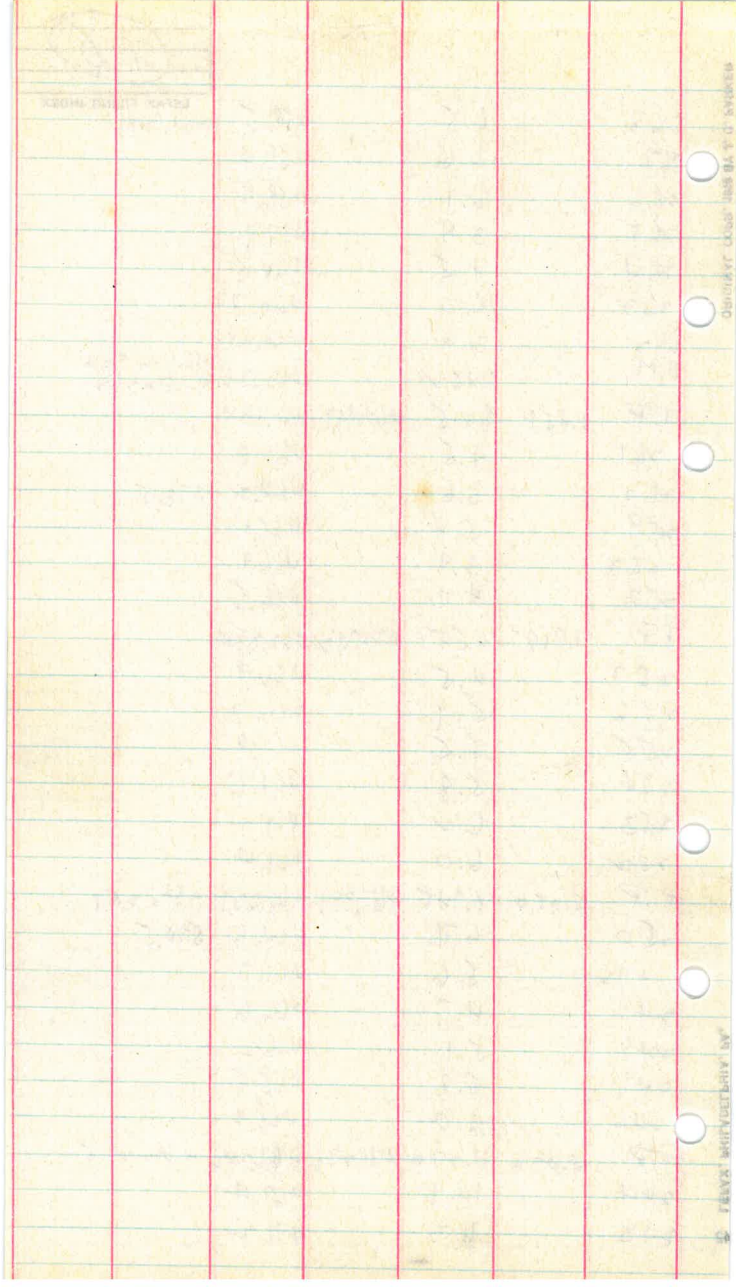
ORIGINAL COPY, 1916 BY J. C. PARKER

LEFAX, PHILADELPHIA, PA.

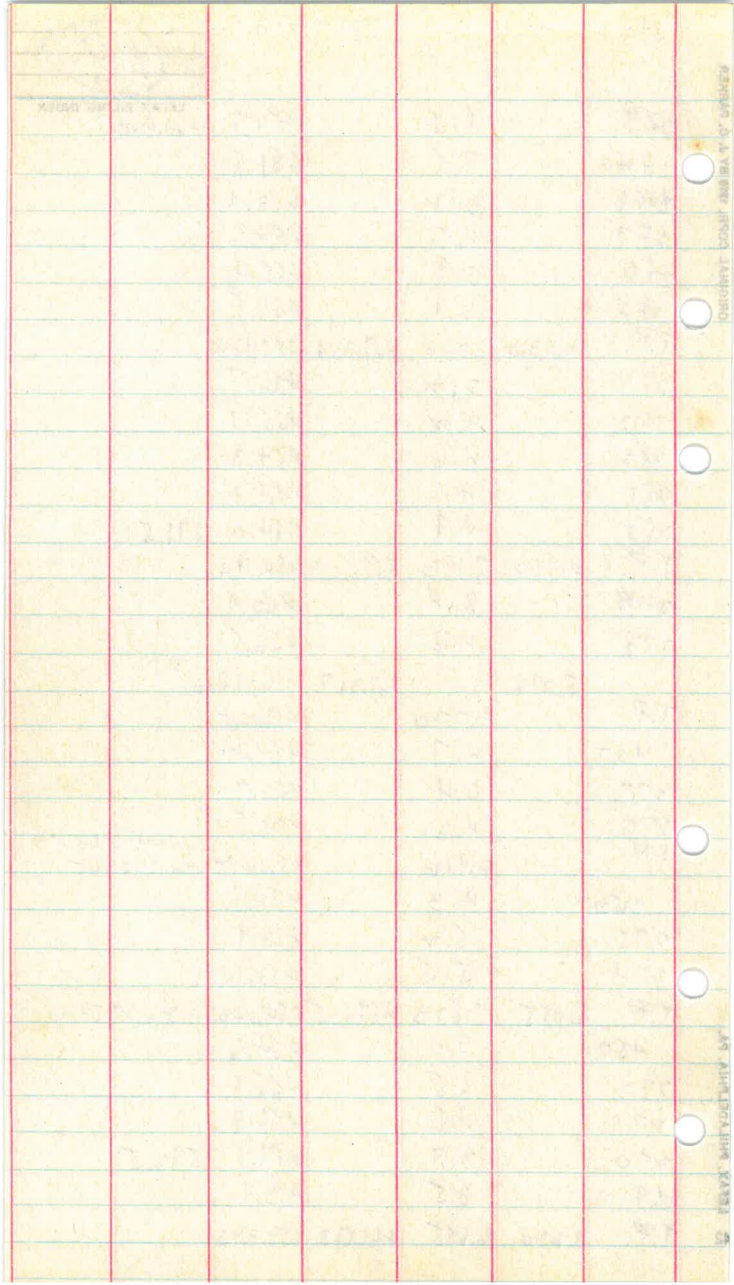
Sta	+	-	Σ	Elev.	
268		6.5		458.5	Hyd. Grd.
267		6.6		458.4	
266		6.1		458.9	
265		3.9		461.1	
264		4.5		460.5	
263		4.3		460.7	
262		3.9		461.09	
B.M.		1.452		463.536	Nail in Sky R. Sta 262
T.P.	3.451	9.215	464.988	461.537	
261		8.5		462.3	
260		6.6		464.2	573.5
259		5.4		465.4	
253		3.9		466.9	
258		4.3		466.5	
T.P.	7.918	4.547	470.752	462.834	
257		4.5		462.9	
256		5.1		462.3	
255		5.5		461.9	
254		5.8		461.6	
253		6.2		461.2	
252		6.0		461.4	
T.P.	5.050	8.945	467.381	462.331	= Sta 251
250		6.76		464.6	574.5
+72		5.6		465.7	
249		4.7		466.6	
248		5.1		466.2	
247		5.8		465.5	
246		6.0		465.3	
T.P.	5.030	11.270	471.276	466.246	= Sta 245
244		10.1		467.4	
243		6.3		471.2	

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LEFAX FILING INDEX









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LEFAX, PHILADELPHIA, PA.

Sta	+	-	π	Elev	
					20
					LEFAX FILING INDEX
+352		9.8		434.8	Hyd. Gnd
313		9.3		435.3	
312+81		5.2		439.4	
B.M.		2.234		442.316	Nail in Secy Tree Sta. 317
T.P. Sta 311	5.170	7.195	444.550	439.430	
310		5.9		440.7	568.5
309		5.0		441.6	
308		4.9		441.7	
307		4.1		442.5	
306		3.8		442.8	
T.P. B.M.	3810	5.893	446.675	442.815	Nail in Secy Tree Opp. 300 too
		4.465		441.243	
+55		5.9		442.9	
305		5.6		443.2	
304		6.3		442.5	
303		5.2		443.6	599.5
302		3.7		444.9	
T.P.	2.843	6.648	448.708	445.825	
301		6.7		445.8	
300		7.0		445.5	
299		6.3		446.2	
298		5.1		447.4	
297		5.0		447.5	
296		4.2		448.3	
T.P.	0.970	1.115	452.473	451.503	= Sta 295+06
294		3.5		449.1	
293		4.7		457.9	
292		4.4		448.2	
291		4.0		448.6	
T.P.	2.030	6.746	452.618	450.588	
290		8.0		451.3	570.5

DATE	DESCRIPTION	AMOUNT	BALANCE
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DATE: 10/1/2023

10/1/2023

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42 LEFAX, PHILADELPHIA, PA.

Sta	+	-	X	Elev
335		4.8		442.6
334		2.1		445.3
333		5.1		442.3
332		8.1		439.3
T.P.	8.564	1.150	447.44	438.877
331		1.1		438.9
330		1.7		438.3
329		4.1		435.9
328		4.4		435.6
327		4.9		435.1
326		5-		385-
T.P.	4.964	5.901	440.027	435.163
325		5.5		435.6
324		5.7		435.4
323		4.7		436.4
322		4.4		436.7
321		4.6		436.5
T.P.	3.522	4.755	441.064	437.522
320		4.9		437.4
319		4.3		438-
318		4.3		438-
317		4.1		438.2
U.S. BM.		2.913		439.384
T.P.	2.910	4.130	442.297	439.387
316		8.2		439.3
315		2.5		445-
314+67		1.4		446.1
T.P.	7.940	4.973	442.517	439.577
314+54		5.0		
313+79		4.8		
313+63		9.7		

(21)

LEFAX FILING INDEX  
Hyd. Gnd

U.S. Elev. 439.83





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Sta + - x ELEV

22  
LEFAX FILING INDEX

T.P.	341		3.189		461.487
	340		7.8		456.9
	339		11.3		453.4
T.P.	12.914	0.736	464.676	451.762	
B.M.		1.895		450.603	
	338		3.0		449.5
	337		6.3		446.2
T.P.	8.251	3.194	452.498	444.247	
	336		3.2		444.2

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Nail in Pole #74397



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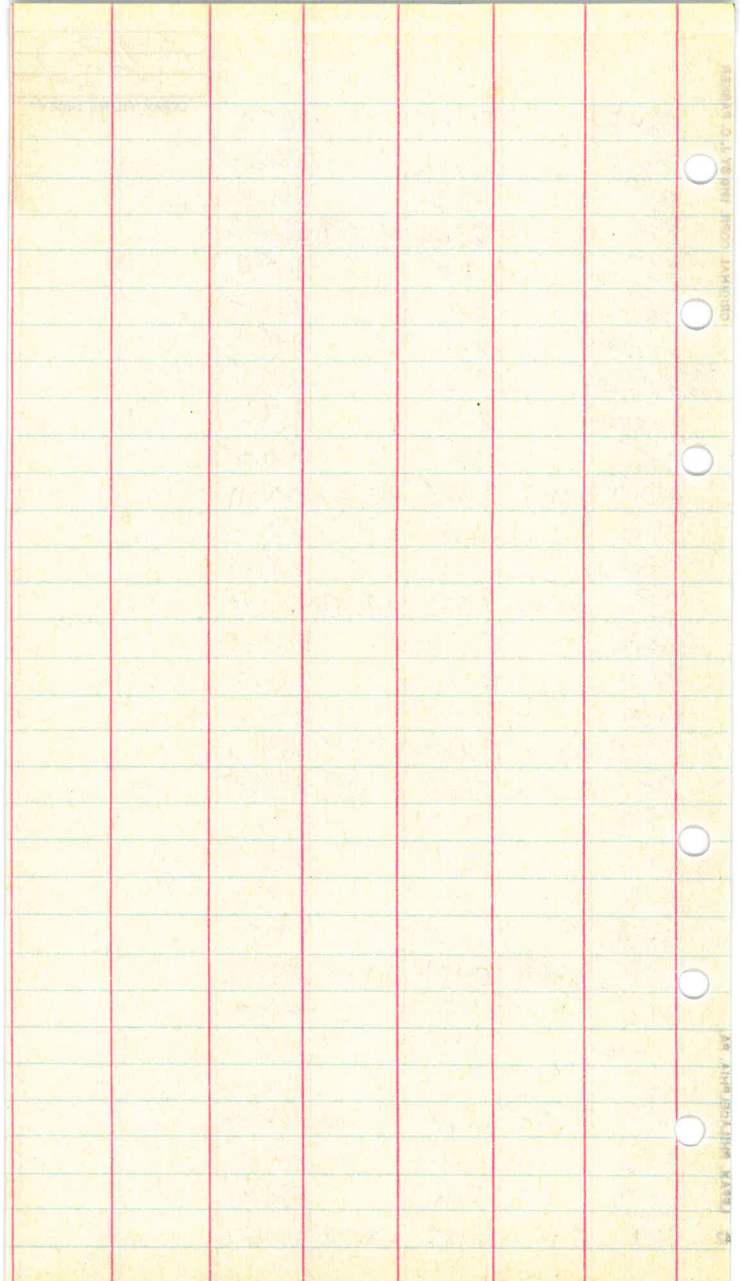
R2

Sta	+	-	Δ	Elev
360+9v		1.2		465.5
360		2.5		464.2
359		4.3		462.4
T.P. 358	5.154	<del>2.330</del>	466.650	461.496
357		4.0		459.8
356		3.8		460-
+44		4.9		458.9
Flow Lin Culvert+24		7.3		465.5
+12		4.2		459.6
355		3.6		460.2
354 T.P.	3.215	7.445	463.826	460.611
353		6.5		461.6
352v		3.0		465.1
T.P.	2.412	6.151	468.056	466.644
B.M. Nail Gas 366*74389		5.672		466.123
351		5.5		466.3
350		5.2		466.6
T.P. 349	2.682	7.846	471.795	469.113
T.P.	1.500	7.659	476.959	475.459
348		10.3		472.8
347		6.7		476.4
346		3.7		479.4
345+6v		3.4		479.7
T.P.	2.253	0.959	483.118	480.865
345		1.8		480.0
+12		6.76		475.1
344		9.6		474.2
T.P.	12.520	1.424	481.824	469.354
343		1.4		469.3
342v		5.6		465.1
T.P. 341	9.241	3.189	470.728	461.487

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351+16



СЕРИЯТ ЛОЖИ ИМАБАТИО ШИДЕШ

СЕРИЯТ ШИДЕШ ИМАБАТИО ШИДЕШ



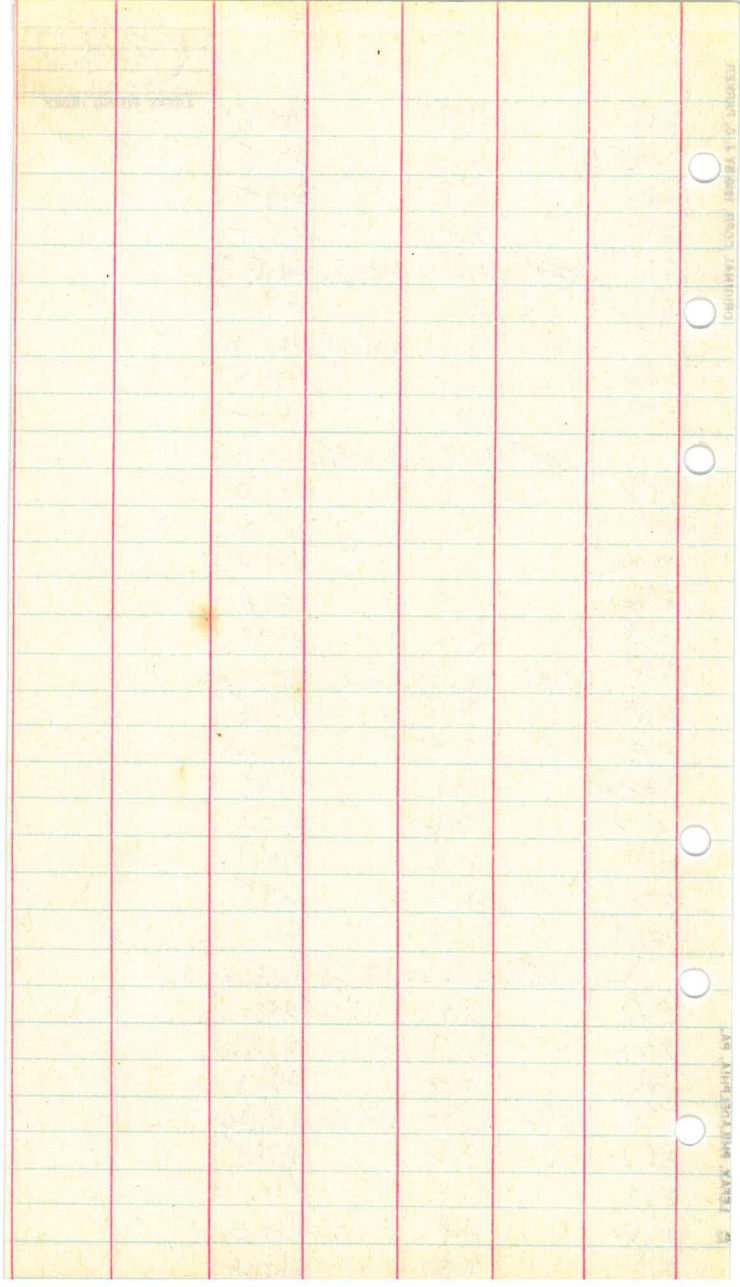
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Sta	+	-	T	EV.
386		7.9		399.9
385		6.3		411.5
384		4.8		413-
383		2.8		415-
382 T.P.	1.328	6.490	417.855	416.527
381		4.0		419.0
T.P.	1.296	10.131	423.017	421.721
380		6.6		425.2
379		1.8		430-
T.P.	1.047	12.276	431.852	430.805
378		11.1		432.0
377		5.9		437.2
376+45		3.7		439.4
376		3.5		439.6
375		5.2		437.9
T.P.	1.741	12.028	443.081	441.340
374		11.9		441.5
373		3.2		450.2
372+30		2.1		451.3
372		7.6		450.8
371		4.3		449.1
370		3.9		449.5
369		3.3		450.1
T.P. 368	2.058	6.946	453.368	451.310
367		5.2		453.1
366		3.7		454.6
365		2.2		456.1
T.P.	1.116	9.510	458.256	457.140
364		8.2		458.5
363		6.6		460.1
362		4.4		462.3
361		4.3		465.4

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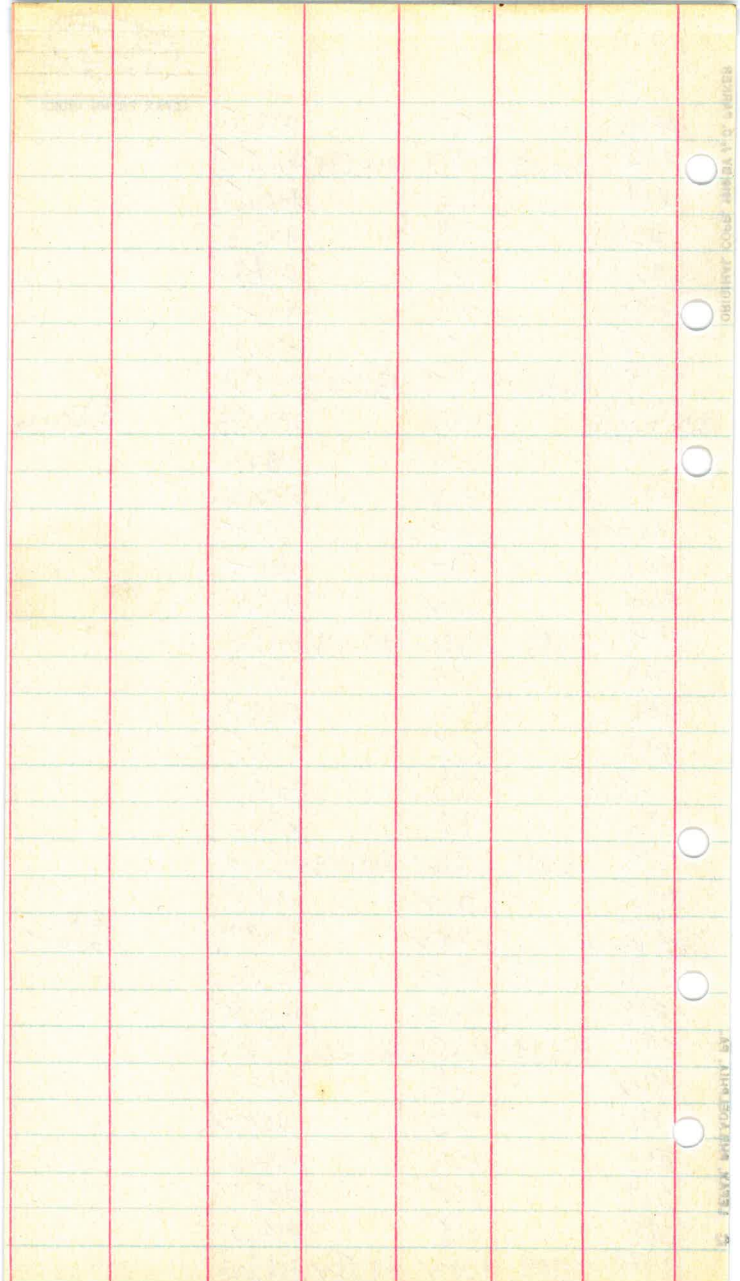
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Sta	+	-	✓	Flv.	
410		5.1		H18.5	
T.P.	3.023	10.959	H23.589	H20.565	
409		11.0		H20.5	
408		7.9		H23.6	
407		4.7		H26.8	
406		2.5		H21	
405		0.7		H30.8	
T.P.	0.430	4.917	H31.524	H31.094	
B.M. Nail Bolt 761206		2.618		H33.593	S.L. Sta 400+60
404		3.4		H32.6	
403		3.8		H32.2	
402		4.1		H32	
401		5.1		H31	
400		6.2		H29.8	
T.P.	9.098	1.090	H36.011	H26.913	
399		0.3		H27.7	
398		3.3		H24.7	
397		5.5		H22.5	
+53		5.3		H22.7	
396		9.4		H19.6	
T.P.	12.299	0.916	H28.003	H15.704	
395		2.2		H14.4	
B.M. Nail in T.P. 25084		1.642		H14.978	24 R Sta 394+75
394		9.1		H07.6	
393		13.0		H03.5	
T.P.	9.209	4.151	H16.620	H07.411	
392		7.6		H03.9	
391		7.3		H04.2	
390		4.9		H06.6	
389		3.4		H08.1	
388		3.5		H08.0	
387 T.P.	2.739	9.032	H11.562	H08.823	

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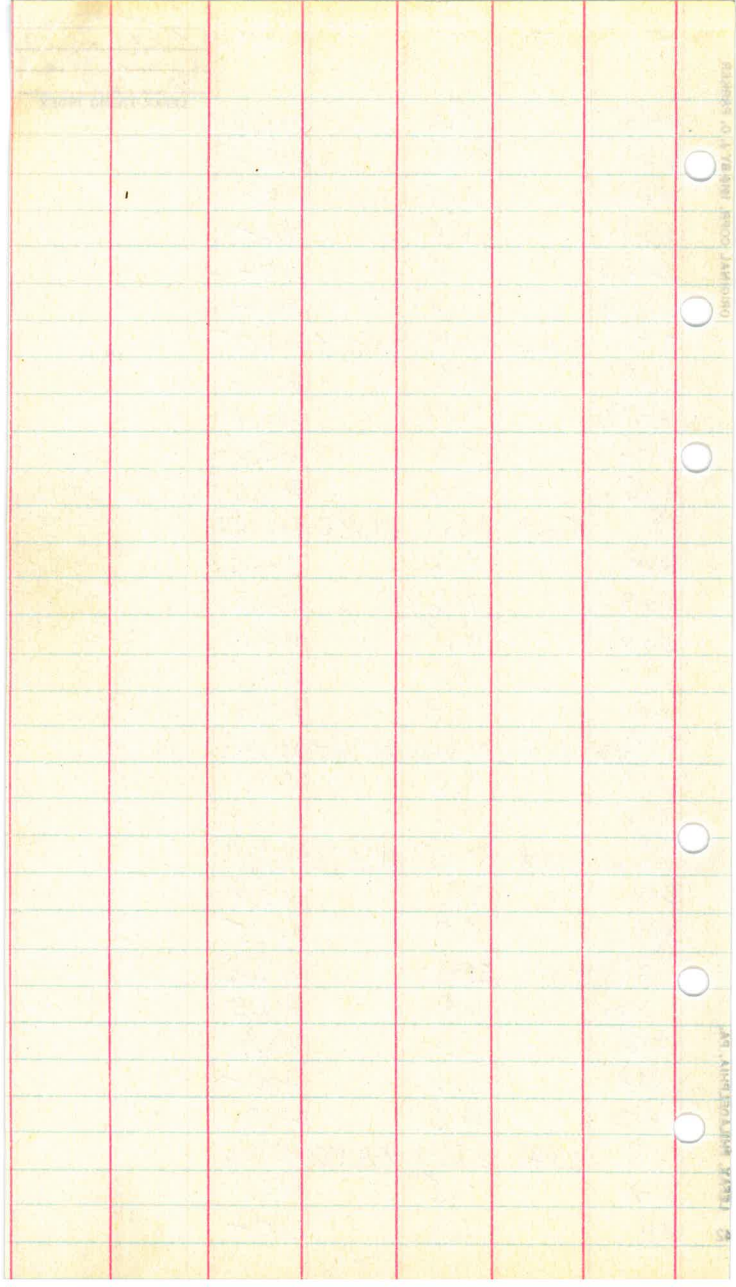
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2

Sta	+	-	X	Elv.
H32		7.6		400.8
H31		7.0		401.4
H30		6.5		419-
H29		2.4		406-
H28+64		1.4		407-
H28+14		1.4		407-
T.P.	0.220	3.298	408.375	408.55
H28		4.9		406.6
H27		6.7		404.8
H26		5.7		405.2
H25		5.2		406.3
T.P.	5.069	4.501	411.453	406.384
H24		4.6		406.3
H23		4.6		406.3
H22		4.5		406.4
H21		4.4		406.5
H20		3.9		407.2
T.P. 53	3.825	10.313	410.585	407.060
H19		9.3		408.1
H18		7.4		410-
T.P.				
H17+20	3.544	9.345	417.373	413.829
H17		5.8		414.4
H16		5.7		417.5
BY H11 Pole 025 13T.		5.526		417.646
H15		6.9		416.3
H15		6.3		416.9
H14		3.2		420-
H13		4.5		418.7
T.P.	3.448	3.862	423.174	419.726
H12		7.5		416.1
H11		6.6		417-

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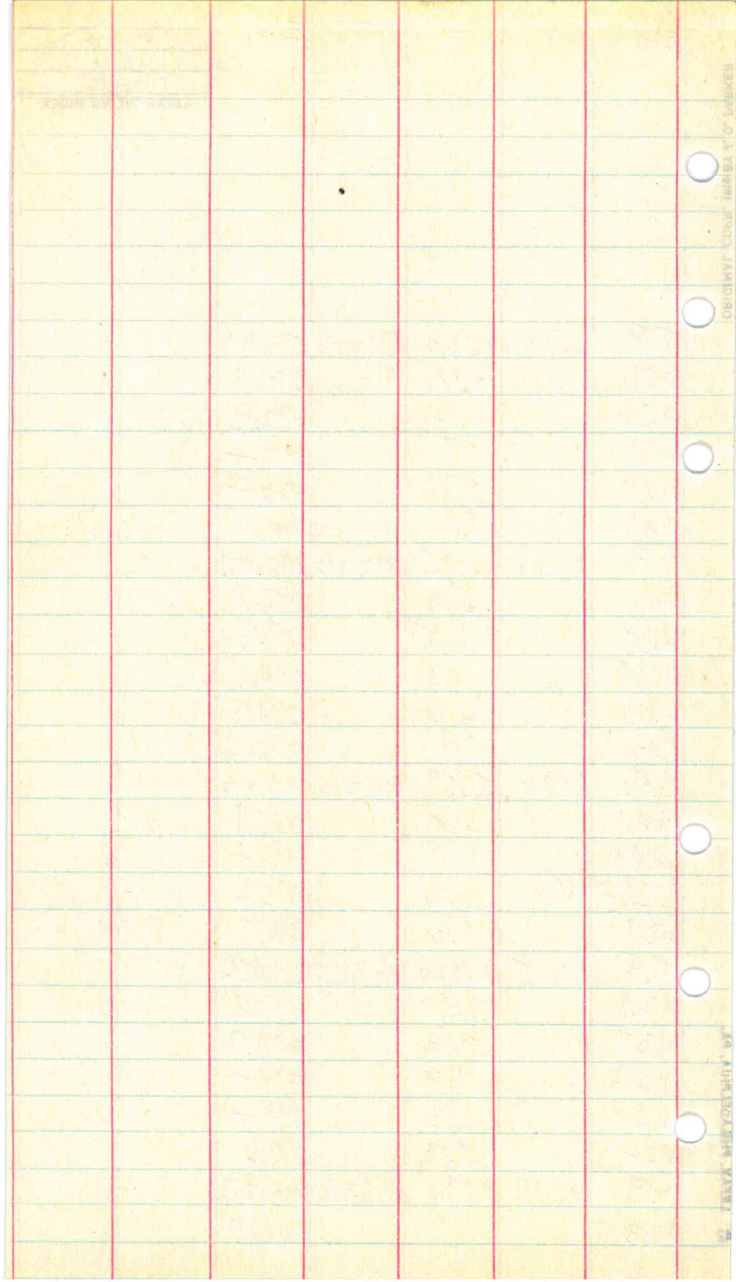
LEFAX, PHILADELPHIA, PA.

12

Sta	+	-	⌈	Elv.
T.P.	6.510	8.160	397.227	390.717
H51.	6.510	8.160	396.117	390.717
H50		6.6		392.3
H49		5.9		393.1
H48		5.9		393.7
H47		5.1		393.8
T.P.	2.690	4.895	398.877	396.197
H46		5.2		395.9
H45		6.5		394.6
H44		6.6		394.5
H43		6.3		394.8
H42		5.8		396.3
T.P.	5.770	5.559	401.082	395.312
H41		5.0		395.9
H40		4.9		396.1
Flow Line +15		5.3		395.6
H39		4.2		396.7
T.P.	1.815	6.260	400.871	399.056
H38		7.9		397.4
H37		7.6		397.7
H36		7.3		398.1
H35		6.3		399.1
H34		5.7		399.6
T.P.	4.539	7.599	405.316	400.777
H33		7.7		408.7

LEFAX FILING INDEX

27





Sta.

115  
 518.6  
 +7.8  
 65  
 510.9  
 +0.1  
 47  
 510.8  
 510A  
 -0.4  
 8  
 510.9  
 +0.1  
 27  
 511.2  
 +0.4  
 50

114+29  
 522.1  
 +10.9  
 50  
 511.7  
 511.0  
 -0.2  
 50  
 Rd.  
 511.3  
 +0.1  
 68

11A  
 530.1  
 +10.0  
 50  
 520.1  
 511.4  
 -8.7  
 37  
 510.7  
 -2.4  
 79  
 Rd.  
 511.1  
 -2.0  
 102  
 Rd.

55A.7  
 +16.8  
 65  
 548.7  
 +10.5  
 31  
 537.9  
 536.8  
 -1.1  
 18  
 531.0  
 -6.9  
 39  
 515A  
 -22.5  
 78  
 510.5  
 -27.1  
 107  
 Rd.

113+65

113+12

113  
 576.6  
 +8.2  
 700  
 574.2  
 +5.8  
 50  
 568.4  
 562.2  
 -6.2  
 80  
 504.0  
 -64.4  
 148  
 503.9  
 -64.5  
 158  
 499.3  
 -69.1  
 175.5

582.8  
 +6.7  
 40  
 580.6  
 +4.5  
 68  
 581.0  
 +4.9  
 83  
 588.1  
 +12.0  
 117

112+781  
 576.1  
 0.0  
 10  
 576.1  
 562.1  
 -14.0  
 100  
 Break  
 543.6  
 -32.3  
 130  
 Break  
 509.6  
 -66.5  
 166  
 Rd.  
 509.8  
 -66.3  
 177  
 Rd.

Sta.	Q				
122		507.8 -0.2 50 508.0	507.6 -0.4 9 508.2	508.2 +0.2 25 508.4	508.2 +0.2 50 508.4
121		508.4 +0.4 50 508.0	507.8 -0.2 7 508.0	508.0 0.0 23 508.3	508.3 +0.3 50 508.6
120		508.4 -0.3 50 508.1	508.2 -0.5 8 508.7	508.3 -0.4 25 508.7	30 fence 508.7
119 POT.		509.1 +0.1 50 509.0	508.9 -0.2 7 509.1	509.1 +0.1 25 509.2	509.5 +0.5 50 509.0
118		509.5 +0.2 50 509.7	509.2 -0.1 4 509.3	509.4 +0.1 19 509.5	509.7 +0.4 50 509.3
117		510.3 +0.1 50 510.2	509.7 -0.5 7 510.2	510.2 0.0 23 510.2	510.2 0.0 5 510.2
116		510.5 -0.3 50 510.8	510.0 -0.8 5 510.8	510.3 -0.5 23 510.8	510.7 -0.1 50 510.7

Sta

529.5 548.9  
 594 554.0 523.9 521.6 521.9 521.7  
 10A+69 +156.7 25.0 52.0 -2.3 -2.0 -2.2  
 155 20 15 22 30

575.8 544.4  
 10A +52.1 +11.0 52.3 51.9 520.2 519.7  
 150 57 19 27 50

539.0 566.6  
 +33.0 +40.6  
 12A 150

537.0 528.5 523.4 523.7 522.8  
 103+50 +11.0 +2.5 52.0 -2.6 -2.3 -3.2  
 50 27 23 32 50  
 538.6 Rd. Rd.

+31.8  
 780

552.0 532.8 524.1 523.7 522.6  
 103 +25.2 +6.0 52.0 -2.7 -3.1 -4.2  
 155 93.0 24 33 50

552.7 524.3 524.5 516.2 508.5  
 102 +21.7 53.0 -6.7 -6.5 -14.8 -22.5  
 150 34 41 100 125  
 541.3 Rd. Rd.

+19.3  
 150

539.8 534.6 526.0 526.0 522.8  
 101 711.8 76.5 528.0 -2.0 -2.0 -5.2  
 117 50 15 22 30  
 Rd. Rd.

563.2  
 +25.3  
 200

544.9 541.9 526.6 526.3 519.9 509.7  
 100+10 +17.0 +14.0 52.0 -1.3 -1.6 -8.0 -18.2  
 150 100 9.0 18 72 107  
 Rd Rd



Sta.	e						
112	587.2 ✓ +37.0 123	580.2 ✓ 8.2 115	530.2 ✓ -20.0 8.2	511.5 ✓ -38.7 115	511.8 ✓ -38.4 133	512.4 ✓ -37.8 144	
111	587.1 ✓ +66 162	542.5 ✓ +21.4 73	511.1 ✓ 511.3 ✓ -9.8 37	511.9 ✓ 511.7 ✓ -9.2 46	511.6 ✓ 511.6 ✓ -9.5 60	511.5 ✓ 512.3 ✓ -9.6 80	512.3 ✓ -8.8 97
110	587.5 ✓ +22.0 182	515.5 ✓ 0.0 8.0 Rd.	515.5 ✓ +0.0 0 Ad.	515.5 ✓ -2.0 44	513.3 ✓ -2.2 51	512.7 ✓ -2.8 61.0	
109	520.6 ✓ +0.8 14 Rd.	520.3 ✓ +0.5 5 Rd.	519.8 ✓ 588.8 ✓ +38.0 124	516.6 ✓ -3.2 30	516.0 ✓ -3.8 42	515.7 ✓ -4.1 50	
107+97	588.5 ✓ +63.0 129	530.3 ✓ 525.5 ✓ -8.3 28	516.4 ✓ 517.2 ✓ -8.3 28	515.4 ✓ 517.2 ✓ -8.3 35	515.4 ✓ 516.2 ✓ -9.3 50	515.4 ✓ -13.0 62	
106	588.3 ✓ +58.0 135	530.3 ✓ 516.0 ✓ -14.3 28	516.4 ✓ 515.7 ✓ -14.6 38	515.4 ✓ 515.3 ✓ -15.0 51	515.4 ✓ -15.0 51	515.3 ✓ -15.0 51	
105+116	588.2 ✓ +60.0 135	528.2 ✓ 515.3 ✓ -12.9 33	515.3 ✓ 515.4 ✓ -12.8 41	515.4 ✓ 515.3 ✓ -12.9 50	515.3 ✓ -12.9 50	515.3 ✓ -12.9 50	

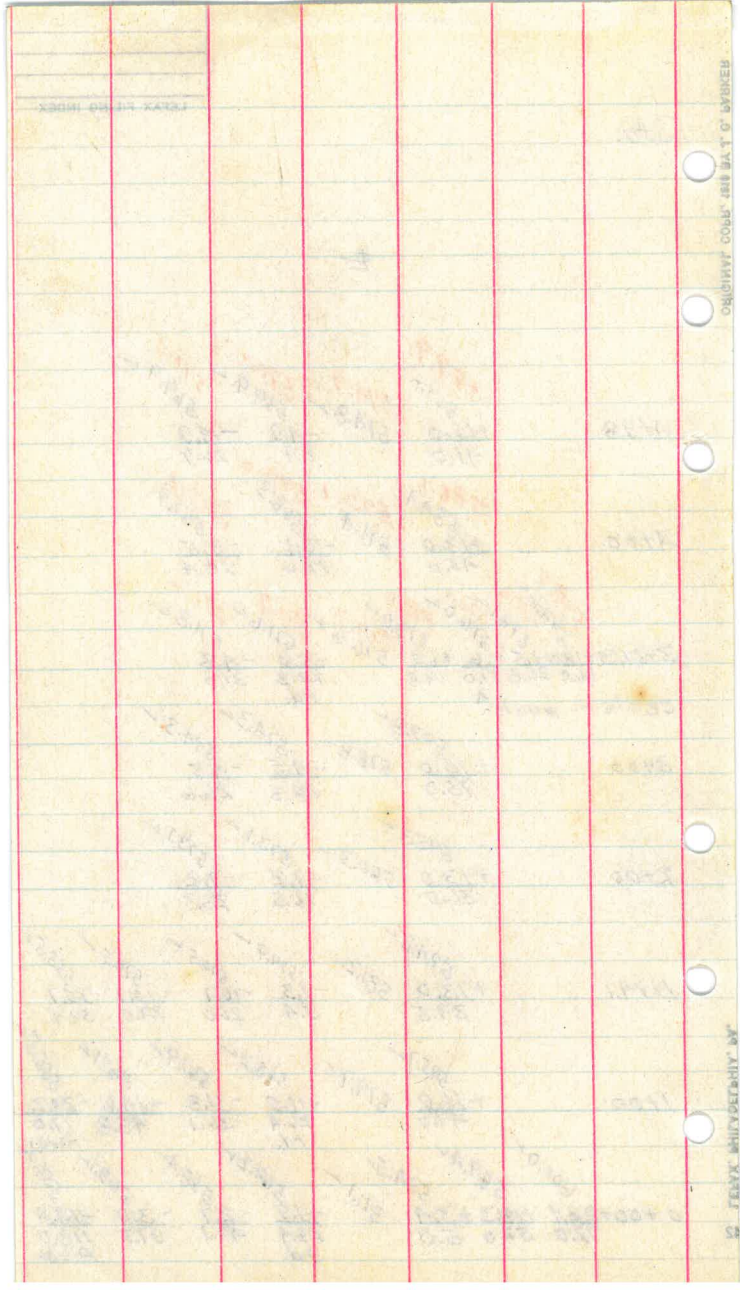




E Sta.	ϕ
130	505.0 ✓ $\frac{0.2}{50}$ 505.0 ✓
129	505.7 ✓ $\frac{0.3}{50}$ 505.7 ✓
128	505.8 ✓ $\frac{0.2}{50}$ 505.6 ✓ 0.11 Pile
127	505.8 ✓ $\frac{0.2}{50}$ 505.8 ✓
+31	506.1 ✓ $\frac{0.2}{50}$ 506.3 ✓
126	505.9 ✓ $\frac{0.5}{50}$ 506.4 ✓
125	507.4 ✓ $\frac{0.2}{50}$ 507.6 ✓
124	507.1 ✓ $\frac{0.5}{50}$ 507.6 ✓
123	507.3 ✓ $\frac{0.5}{50}$ 507.8 ✓
122	507.4 ✓ $\frac{0.2}{50}$ 508.0 ✓ 508.2 ✓









Sta.

LEFAX FILING INDEX

13+73.3 A	+15.0 10.0 Hyd. Gr.	578.6	-1.9 11.2 Bank	-11.1 22.8 rd.	-12.0 29.8	-13.5 42.0 Creek bed
13+00	+15.0 38.0 Hyd. Gr.	578.5	-3.7 8.8 Bank	-9.7 17.0	-9.6 24.0	
11+98.1	+17.0 55.5 Hyd. Gr.	576.7	-8.0 11.9	-8.3 18.9		
11+00	22.0 78.0 Hyd. Gr.	577.8	-3.8 9.7	-3.8 19.5		
9+99.5 A	+20.0 46.9 Hyd. Gr.	573.2	-5.7 11.5	-5.1 19.9		
9+00	+22.0 70.0 Hyd. Gr.	571.6	-2.7 8.7	-2.9 16.3		
7+99.8 A	+23.0 73.9	570.5	0.0 0.0 Edge of road	0.0 10.0	-16.5 54.6 Rivet	
7+10	19.0 37.5 Hyd. Gr.	575.5	-1.2 14.2 rd.	-1.2 21.9	-22.2 65.0	
6+86.1	+16.0 32.2 Hyd. Gr.	578.3	-8.9 14.5 rd.	-9.2 25.8	-25.2 60.0	
6+00.3	+14.0 50.0 Hyd. Gr.	580.1	-2.2 14.4 rd.	-7.4 21.5		

593.6

593.8

593.9

593.7

593.5

578.3

580.1

573.1

578.5

576.7

577.8

573.2

571.6

570.5

575.5

578.3

573.1

572.9

572.7

572.1

571.9

571.7

567.2

571.8

568.1

568.0

568.1

569.9

570.5

569.3

569.1

569.1

568.8

568.7

568.6

568.5

566.6

569.0

568.7

568.0

568.1

568.1

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568.1

565.1

565.1

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565.1

565.1

565.1



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LEFAX FILING INDEX

Sta.

27+25.6

597.6  
-11.7  
21.0  
Edge of bank  
30.0  
-16.7  
30.0  
-16.8  
39.0  
-16.5  
12.0  
Bank

26+91

594.5  
-14.3  
25.0  
Bank  
-21.6  
30.0  
-21.6  
36.0  
-21.7  
40.0  
-53.1  
40.0  
-56.0  
110.0  
-58.8  
115.0  
-60.8  
147.0  
Edge of bank  
Top of slope  
Toe of slope  
Center of stream

26+00

599.8  
-9.0  
21.0  
Bank  
-15.0  
26.0  
-14.7  
35.5  
-14.3  
11.6  
-61.1  
129.9  
Top of slope  
Center of stream

25+45

599.8  
-4.5  
10.5  
Bank  
-9.0  
16.5  
-9.4  
25.1  
-9.0  
31.1  
-31.4  
66.1  
-38.2  
82.9  
-56.3  
101.9  
-59.7  
136.7  
Top of slope  
Center of stream

24+25A

590.5  
+5.0  
11.8  
Hyd. Gt.  
-2.5  
3.5  
-6.3  
9.5  
-6.1  
16.5  
-6.6  
21.1  
-4.6  
27.6  
-12.6  
106.0  
Top of bank  
Top of slope  
Center of stream

23+98

594.2  
+5.0  
14.5  
Hyd. Gt.  
-3.7  
10.0  
-8.5  
13.9  
-8.0  
21.0  
-6.0  
24.0  
-18.0  
85  
-48.0  
97.0  
Top of bank  
Top of slope  
Center of stream

23+00

591.0  
+6.0  
14.0  
Hyd. Gt.  
-3.3  
8.0  
-10.3  
3.7  
-10.3  
21.0  
-10.2  
31.0  
Top of bank  
Top of slope  
Center of stream

22+00

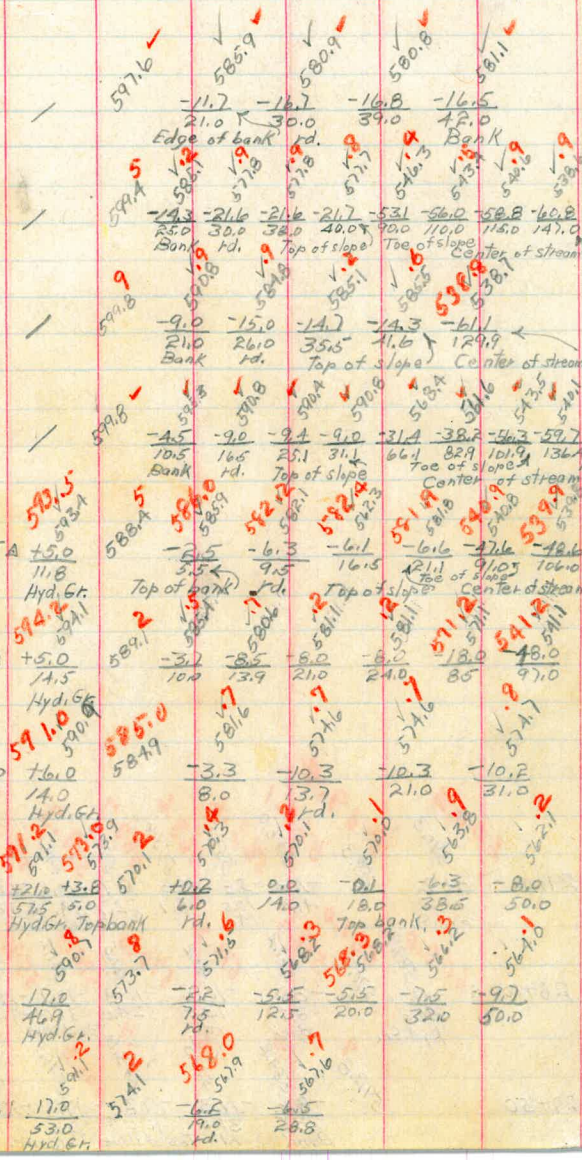
591.2  
+21.0  
+3.8  
57.5  
51.0  
Hyd. Gt. Top bank  
+0.2  
6.0  
0.0  
14.0  
-0.1  
18.0  
-6.3  
38.5  
-8.0  
50.0  
Top bank  
Center of stream

21+00

590.1  
+17.0  
16.9  
Hyd. Gt.  
-2.2  
7.5  
-5.5  
12.5  
-5.5  
20.0  
-7.5  
32.0  
-9.7  
50.0  
Top of bank  
Center of stream

20+44B

591.2  
+17.0  
53.0  
Hyd. Gt.  
-1.5  
7.0  
-6.5  
28.8  
-1.5  
28.8  
Top of bank  
Center of stream





Station	Top of Slope	Bank	Top of Slope	Bank	Top of Slope	Bank	Top of Slope	Bank	Top of Slope	Bank
29+00	570.3	13	569.3	13	568.1	10.0	563.6	18.7	559.3	10.1
	570.3	4.2	568.1	10.0	563.6	18.7	559.3	10.1	555.9	16.7
	Hyd. St.									
28+00	570.3	13	569.3	13	568.1	10.0	563.6	18.7	559.3	10.1
	570.3	4.2	568.1	10.0	563.6	18.7	559.3	10.1	555.9	16.7
	Hyd. St.									
27+50	570.3	13	569.3	13	568.1	10.0	563.6	18.7	559.3	10.1
	570.3	4.2	568.1	10.0	563.6	18.7	559.3	10.1	555.9	16.7
	Hyd. St.									

SHERMAN CONSTRUCTION COMPANY

SHERMAN CONSTRUCTION COMPANY



Sta.

LEFAX FILING INDEX

37+00	+36.0 128.0	+19.9 77.0	+9.9 36.0	562.6	561.2 9.0	548.6 32.0	548.7 39.0
36+00	+15.0 86.0	+10.0 77.0	553.3	553.3	550.6 16.0	550.5 23.0	541.7 61.5
35+00	+33.0 67.0	556.7	551.5	551.5	551.3 32.0	540.5 56.0	
34+00	+38.0 75.0	561.3	553.6	552.9	549.3 46.0		
33+00	+31.0 91.0	568.5	555.5	555.7	555.1 48.3		
31+95	+31.0 205.0	+29.9 167.0	+10.1 69.0	560.7	561.5 24.0	561.5 31.0	562.7 39.0
31+00	+33.0 82.0	561.2	561.1	558.8	558.7 18.5	553.2 24.5	546.6 33.0
30+00	+34.0 90.4	+8.0 31.9	564.4	560.3	560.1 38.0	547.7 110.0	543.1 126.0
29+63	+33.0 106	+17.5 55	567.1	561.2	561.2 28.0	550.4 91.0	542.9 116.0

Sta	597.3 ✓	539.2 ✓	539.1 ✓	532.7 ✓
42+00	+46.0 59.0	551.3 -12.1 11.0	11.9 15.0	-15.6 29.0
44+00	597.7 ✓ +41.0 89.0	556.0 ✓ 536.8 ✓ -19.9 4.0	536.5 ✓ -20.2 47.0	
43+55	596.6 ✓ +39.0 55.0	557.6 ✓ 538.2 ✓ -19.4 25.0	538.1 ✓ -19.5 32.0	531.4 ✓ 26.2 57.0
43+00	597.1 ✓ +43.0 95.0	554.1 ✓ 538.3 ✓ -16.1 16.0	538.1 ✓ -16.3 24.0	531.6 ✓ -22.8 39.0
42+71	597.1A ✓ +47.0 75.0	550.4 ✓ 536.8 ✓ -13.6 18.0	536.6 ✓ -13.8 25.0	531.8 ✓ -15.6 35
42+35	597.4 ✓ 49.0 64.0	548.1 ✓ 537.1A ✓ -11.0 11.0	537.1A ✓ 537.1A ✓ 11.4 18.0	532.2 ✓ -16.2 25.0
41+00	597.2 ✓ +46.0 33.0	551.2 ✓ 542.9 ✓ -8.3 10.0	543.0 ✓ -8.2 7.0	531.9 ✓ -19.3 26.0
40+58	597.7 ✓ +52.0 35.0	553.7 ✓ 545.1 ✓ -8.6 7.0	544.9 ✓ -8.8 14.0	
40+00	546.2 ✓ +52.0 53.0	549.2 ✓ 545.5 ✓ -0.4 3.0	545.0 ✓ -0.6 9.0	545.3 ✓ -0.9 13.0
38+95	546.5 ✓ +32.0 41.0	546.5 ✓ 546.6 ✓ -17.9 16.0	546.8 ✓ -17.7 21	546.3 ✓ -18.2 25.0
38+00	546.6 ✓ +35.0 53.0	547.0 ✓ 547.5 ✓ -13.0 22.0	547.5 ✓ -13.1 29.0	547.9 ✓ -19.1 30.0 113.0

ORIGINAL COPY 1910 BY J. C. PARKER

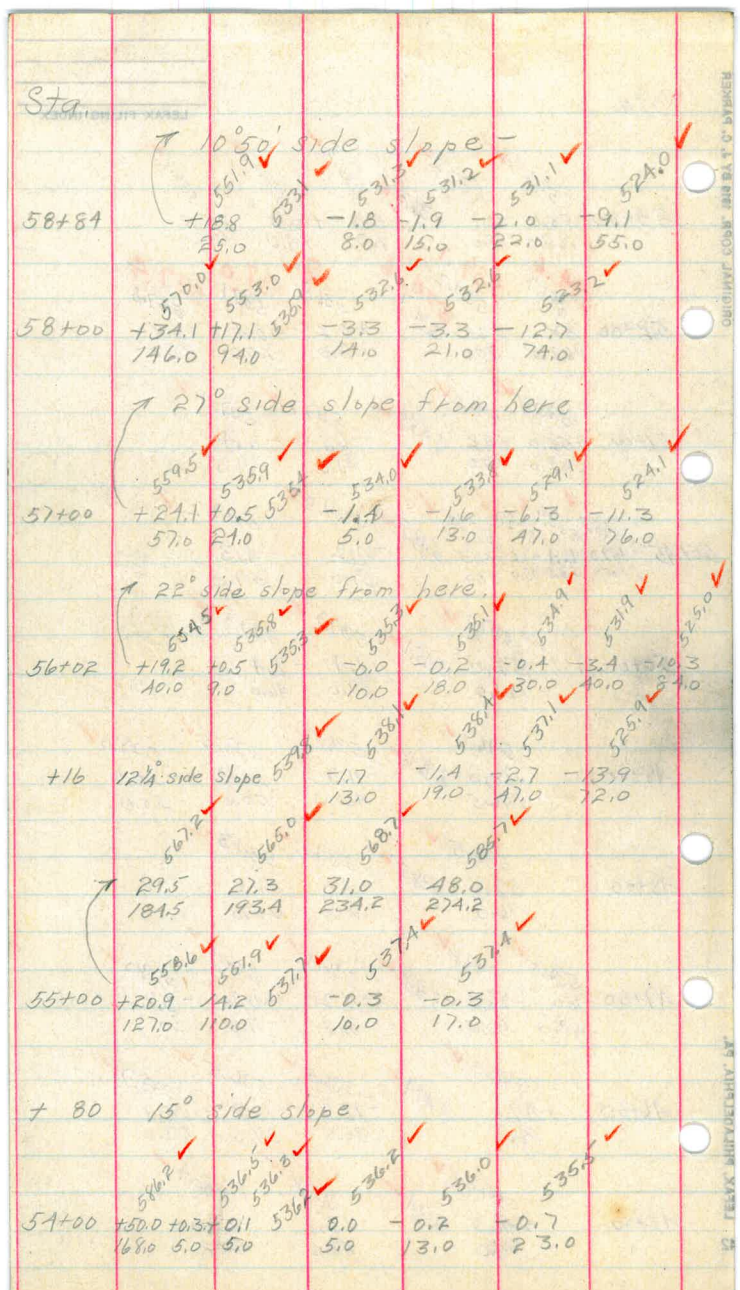
LEFAX, PHILADELPHIA, PA.

LEFAX FILING INDEX

Sta.

53+00	58.0 163.0	-0.1 15.0	536.3 536.5	0.0 7.0	+0.2 14.0	+0.5 25.0
52+00	58.0 162.0	+2.5 30.0	539.1 539.2 536.6	+0.2 13.0	+0.1 20.0	+0.8 36.0
51+00	595.8 162.0	546.0 40.0	5A38	537.7 41.0	537A 49.0	
50+45	595.8 160.0	538.9 53.0	538.5 45.0	539.3 51.0	539.2 59.0	
50+00	597.1 161.0	5A5.1	537.7	537.7 39.0	537.7 46.0	
48+90	596.6 146.5	546.6	536.9	527.3 40.0	528.0 58.0	
48+00	596.5 76.0	538.5	534.5	534.3 18.0		
47+00	596.5 103.0	544.8 10.0	536.1	536.2 3.0	533.0 3.0	
46+00	596A 98.0	549A	536.5	536.5 30.0	533.7 52.0	
45+00	597A 94.0	556A	536.8	536A 28.0		







ORIGINAL COPR. 1919 BY J. C. PARKER

LEFAX FILING INDEX

5° 10' slope from here

66+00	575.5 +15.0 127.0	577.8 -9.7 27.0	582.5 525.9 -6.6 18.0	581.3 -21.2 36.0	581.2 726.3 42.0	529.5 -23.0 66.0	523.5 -29.0 89.0
-------	-------------------------	-----------------------	--------------------------------	------------------------	------------------------	------------------------	------------------------

65+50	586.0 +18.0 150.0	550.0	587.1 -2.9 13.0	581.4 -18.6 32.0	581.4 -18.6 59.0
-------	-------------------------	-------	-----------------------	------------------------	------------------------

8° 36.5' slope

65+00	546.5	535.1 -11.2 36.0	532.3 -14.0 40.0	532.2 -11.1 47.0	524.9 -21.4 64.0
-------	-------	------------------------	------------------------	------------------------	------------------------

14° 30' slope

64+00	533.6	536.6 -2.0 37.0	531.2 -2.4 44.0	523.1 -10.5 75.0
-------	-------	-----------------------	-----------------------	------------------------

13° 10' side slope from here

63+00	567.3 33.4 169.0	581.1 +20.2 122.0	533.9 -2.4 23.0	531.5 -2.4 36.0	531.6 -3.0 47.0	522.1 -11.8 78.0
-------	------------------------	-------------------------	-----------------------	-----------------------	-----------------------	------------------------

62+00	584.3 +45.0 161.0	539.3	531.4 -7.9 30.0	581.4 -7.9 37.0	522.7 -16.6 62.0
-------	-------------------------	-------	-----------------------	-----------------------	------------------------

61+00	576.8 33.0 118.0	551.4 +9.6 15.0	541.8 -6.4 33.0	535.4 -13.6 39.0	528.2 -13.7 47.0	528.1 -19.7 57.0
-------	------------------------	-----------------------	-----------------------	------------------------	------------------------	------------------------

5° 3.5' slope

60+00	566.6 +21.0 100.0	538.0 +38.0 145.0
-------	-------------------------	-------------------------

60+00	56 3.5 76.0	556.9 +11.3 64.0	546.6 -4.0 10.0	524.0 -21.6 20.0	523.8 -21.8 26.0	518.9 -26.7 41.0
-------	-------------------	------------------------	-----------------------	------------------------	------------------------	------------------------

LEFAX, PHILADELPHIA, PA. 42

73	549.1 +14.3 194.0	545.7 +0.9 16.0	544.8	544.1 -0.7 15.0	543.6 -1.2 24.0	528.3 -16.5 227.0	519.0 -20.8 206.0
72+00	543.3 +16.0 272.0	542.5 +14.2 100.0	540.3	546.3 -2.0 20.0	545.9 -2.4 25.0	528.6 -19.7 219.0	521.2 -27.1 224.0
70+98	578.1 +27.9 150.0	550.2	544.8 -5.4 14.0	544.2 -6.0 22.0			
70	544.4 +33.8 20.0	550.6	547.0 -3.6 17.0	543.0 -7.6 27.0	543.0 -7.6 35.0	533.0 -17.6 76.0	
70					531.1 -30.9 169.0	529.8 -22.2 149.0	530.5 -21.5 77.0
69+00	578.2 +21.2 200.0	557.0	546.1 -5.9 35.0	542.0 -10.0 41.0	541.6 -10.4 52.0	541.8 -10.2 56.0	
68+20	539.4 +2.8 50.0	536.6	534.3 -2.4 75.0	534.3 -2.4 85.0	531.6 -8.1 116.0	519.6 -17.1 130.0	
67+80	586.5 +5.0 320.0	557.7 +20.1 219.0	535.1	534.8 -0.8 8.0	534.6 -1.0 16.0	531.8 -3.8 74.0	522.8 -12.8 106.0
67+32	546.1 +12.5 100.0	540.6 +5.0 50.0	538.1	534.3 -1.3 18.0	534.0 -1.6 25.0	531.9 -3.7 91.0	527.1 -13.5 111.0
67+00	700 +0.0 0.0	518.9	545.9 -3.0 10.0	531.9 -17.0 30.0	528.2 -16.7 37.0	521.5 -17.4 95.0	521.4 -2.5 121.0

COURTESY COBB COUNTY BOARD OF SUPERVISORS

COURTESY COBB COUNTY BOARD OF SUPERVISORS

Sta.

LEFAX FILING INDEX

83	540A +14.4 50.0	528.6 +2.6 14.0	523.5 -2.5 13.0	523A -2.6 21.0	523.0 -3.0 23.0	515.6 -10.4 51.0
----	-----------------------	-----------------------	-----------------------	----------------------	-----------------------	------------------------

82+10	528.5 +11.4 50.0	524.1 52.1	523.9 -2.2 14.0	522.9 -2.2 23.0	523.8 -2.3 19.0	516.6 -10.5 61.0
-------	------------------------	---------------	-----------------------	-----------------------	-----------------------	------------------------

81	542.6 +12.0 50.0	532.6 +2.0 26.0	528.1 -2.5 29.0	527.1A -3.2 39.0	526.9 -4.7 37.0	514.3 -14.3 39.0
----	------------------------	-----------------------	-----------------------	------------------------	-----------------------	------------------------

80	539.1 +6.6 50.0	532.5 52.5	530.2 -2.3 11.0	529.7 -2.8 19.0	526A -6.1 50.0
----	-----------------------	---------------	-----------------------	-----------------------	----------------------

79	542A +11.5 50.0	531.0 53.0	530.9 -1.0 5.0	530.4 -1.5 13.0	527.3 -4.6 50.0
----	-----------------------	---------------	----------------------	-----------------------	-----------------------

78	541.1 +9.3 50.0	532.3 +0.5 13.0	532.5 -0.7 14.0	532.6 -0.8 22.0
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77	540.8 +13.5 50.0	527.3 52.3	527.3 -0.0 6.0	527.3 -0.0 14.0	526.8 -0.5 50.0
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76+00	540.2 +21.0 50.0	529.2 52.2	527.9 -1.3 15.0	527.8 -1.4 22.0	527.0 -2.2 50.0
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75	540.3 +21.0 51.0	537.2 53.2	537.2 -5.1 13.0	531.0 -8.3 23.0	531A -7.9 30.0	530A -8.9 50.0
----	------------------------	---------------	-----------------------	-----------------------	----------------------	----------------------

74+00	540.3 +19.1 50.0	539.2 53.2	537.6 -1.6 9.0	537.5 -1.7 17.0	536.5 -2.7 50.0
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Sta.							
89+25	586.3 +30.0 52.0	516.5 -15.8 25.0	516.4 -34.9 35.0	516.4 -39.9 42.0	502.8 -53.5 59.0		
89	590.8 +37.0 37.0	526.5 -6.3 8.0	522.0 -31.8 27.0	526.8 -32.0 34.0	511.7 -44.1 33.0		
88+00	589.6 +39.0 46.0	550.7 -10.0 18.0	540.6 -26.1 26.0	524.5 -26.1 33.0	513.3 -37.3 48.0		
87+37	37.20's slope 549.8 +37.0 64.0	549.8 -6.2 8.0	543.5 -25.0 18.0	524.7 -25.2 28.0	513.4 -36.3 42.0		
87	590.3 +47.0 64.0	543.2 -3.1 3.0	523.3 -20.0 18.0	523.2 -20.1 24.0	513.7 -29.6 41.0		
86+00	35.20's slope 531.1 +39.0 67.0	531.1 -8.8 13.5	528.0 -17.6 22.0	519.8 -17.9 29.0	513.0 -24.9 34.0		
85+36.8	583.2 +39.0 67.0	544.3 -14.0 19.0	530.2 -24.4 26.0	519.8 -24.6 32.0	518.9 -25.3 43.0	505.1 -25.7 82.0	
85	593.1 +28.6 71.0	544.2 -11.3 16.0	532.8 -24.0 27.0	520.1 -24.7 33.0	514.0 -30.1 32.0	511.1 -29.4 83.0	
84	589.8 +50.0 121.0	540.8 -13.0 20.0	526.8 -18.3 25.0	511.6 -18.2 32.0	511.9 -24.9 49.0	511.5 -25.3 70.0	
83+36	511.1 +20.1 50.0	523.1 -2.6 15.0	523.2 -2.8 24.0	522.1 -3.9 31.0	516.5 -10.5 47.0		

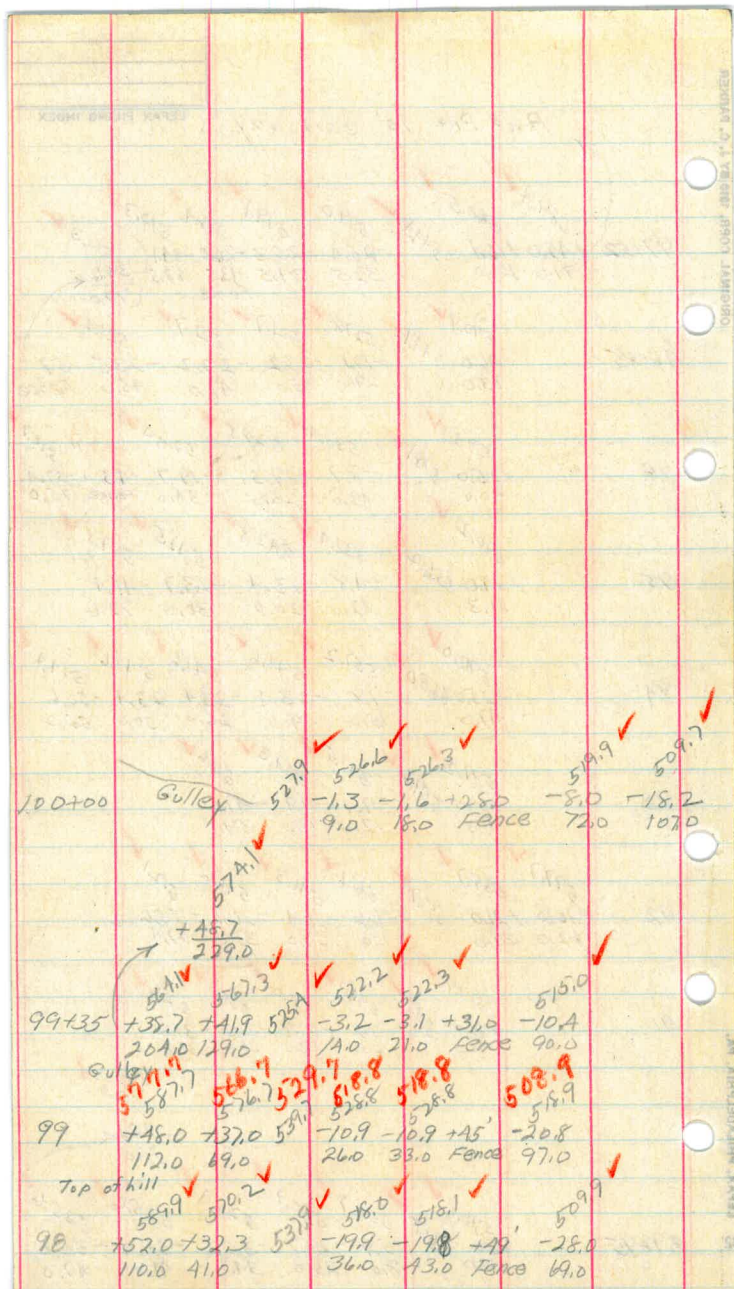
ORIGINAL COPY AND B.A.T.C. NUMBER

BY FEAKS UNIVERSITY



Rock Pile 15' each way

97+52	589A +15.0 91.0	560.5 24.0	519.0 -25.4 32.5	519.1 -25.3 39.5	519.4 -26.0 43.5	510.3 -34.1 62.5	510.3 -34.6 77.0
96+85	590.9 +16.0 93.0	519.9 24.0	527.8 -17.1 29.0	521.7 -23.2 35.0	521.7 -23.2 42.0	521.4 -23.5 48.0	Fence
96	573.1 +25.0 90.0	519.1 24.0	539.7 -8.7 13.0	528.8 -19.3 25.0	528.8 -19.7 34.0	510.7 -37.4 Fence 75.0	
95	590.2 +24.0 61.3	556.2 24.0	551.4 -1.8 12.0	542.8 -13.4 20.0	542.5 -13.7 30.0	519.3 -41.4 72.6	
94	590.0 +25.0 97.0	566.6 24.0	551.2 -7.8 15.0	541.6 -23.4 19.0	541.6 -23.4 26.0	541.6 -23.4 30.0	514.4 -50.6 58.2
93	589.2 +30.0 47.5	559.8 24.0	549.6 -9.7 12.0	549.8 -9.9 19.0	511.6 -17.6 59.1		
92	597.7 +30.0 62.0	556.7 +21.0 39.0	567.7 24.0	561.1 -6.6 11.0	541.3 -26.4 27.0	541.6 -26.1 37.0	512.1 -55.6 67.4
91	587.9 +36.0 46.0	551.9 24.0	540.7 -11.2 16.0	530.0 -21.9 23.0	530.3 -21.6 30.0	526.6 -39.3 50.0	
89+95	590.6 +30.0 48.0	560.6 24.0	554.7 -5.9 8.0	530.9 -27.7 25.0	526.4 -35.2 34.0	526.6 -35.0 41.0	526.6 -35.0 47.0



Road Road

LEFAX FILING INDEX

Fence

$$\begin{array}{r} 506.0 \\ -0.0 \\ \hline 17 \end{array} \quad \begin{array}{r} 506.2 \\ +0.2 \\ \hline 31 \end{array}$$

37

$$\begin{array}{r} 506.5 \\ -0.2 \\ \hline 15 \end{array} \quad \begin{array}{r} 506.0 \\ +0.3 \\ \hline 31 \end{array}$$

35

$$\begin{array}{r} 506.0 \\ -0.6 \\ \hline 16 \end{array} \quad \begin{array}{r} 506.2 \\ -0.1 \\ \hline 31 \end{array}$$

34

$$\begin{array}{r} 506.2 \\ -0.6 \\ \hline 14 \end{array} \quad \begin{array}{r} 506.7 \\ -0.4 \\ \hline 29 \end{array}$$

34

$$\begin{array}{r} 506.0 \\ -1.3 \\ \hline 15 \end{array} \quad \begin{array}{r} 506.7 \\ -0.6 \\ \hline 30 \end{array}$$

35

$$\begin{array}{r} 506.2 \\ -1.2 \\ \hline 29 \end{array} \quad \begin{array}{r} 506.9 \\ -0.5 \\ \hline 46 \end{array}$$

50

$$\begin{array}{r} 506.6 \\ -2.2 \\ \hline 59 \end{array} \quad \begin{array}{r} 506.4 \\ -1.2 \\ \hline 24 \end{array}$$

77

$$\begin{array}{r} 506.9 \\ -0.2 \\ \hline 52 \end{array} \quad \begin{array}{r} 507.0 \\ -0.6 \\ \hline 71 \end{array}$$

$$\begin{array}{r} 507.7 \\ -0.1 \\ \hline 29 \end{array} \quad \begin{array}{r} 508.1 \\ +0.3 \\ \hline 45 \end{array} \quad \begin{array}{r} 508.2 \\ +0.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 507.6 \\ -0.1 \\ \hline 90 \end{array} \quad \begin{array}{r} 508.2 \\ +0.3 \\ \hline 25 \end{array} \quad \begin{array}{r} 508.2 \\ +0.2 \\ \hline 50 \end{array}$$

R.O.  
Pole



1	Sta.	Σ
	+50	501.9 ✓ -0.1 ✓ 50
	139	501.9 ✓ +0.2 ✓ 50
	138	502.1 ✓ +0.2 ✓ 50
	137	502.3 ✓ +0.2 ✓ 50
	136	502.1 ✓ -0.2 ✓ 50
	135	502.3 ✓ -0.1 ✓ 50
	134	502.2 ✓ -0.2 ✓ 50
	133	502.8 ✓ -0.2 ✓ 50
	132	503.0 ✓ -0.2 ✓ 50
	131	504.3 ✓ -0.2 ✓ 50
		0.5' pole
		0.6' pole
		0.3' pole
		502.0 ✓
		501.7 ✓
		501.9 ✓
		502.1 ✓
		502.1 ✓
		502.3 ✓
		502.4 ✓
		502.9 ✓
		503.7 ✓
		503.9 ✓
		504.5 ✓



Road Road

$$\begin{array}{r} 501.7 \\ -03 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 501.7 \\ -03 \\ \hline 46 \end{array}$$

$$\begin{array}{r} 501.4 \\ -03 \\ \hline 31 \end{array}$$

$$\begin{array}{r} 501.7 \\ -00 \\ \hline 48 \end{array}$$

$$\begin{array}{r} 501.6 \\ -03 \\ \hline 44 \end{array}$$

$$\begin{array}{r} 502.0 \\ +04 \\ \hline 59 \end{array}$$

$$\begin{array}{r} 501.0 \\ -14 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 502.1 \\ -00 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 501.9 \\ -04 \\ \hline 80 \end{array}$$

$$\begin{array}{r} 502.3 \\ 00 \\ \hline 27 \end{array}$$

$$\begin{array}{r} 502.7 \\ +03 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 502.9 \\ +05 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 503.1 \\ +02 \\ \hline 16 \end{array}$$

$$\begin{array}{r} 503.5 \\ +06 \\ \hline 31 \end{array}$$

$$\begin{array}{r} 503.2 \\ -05 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 503.1 \\ -06 \\ \hline 32 \end{array}$$

$$\begin{array}{r} 503.3 \\ -06 \\ \hline 19 \end{array}$$

$$\begin{array}{r} 503.7 \\ -02 \\ \hline 34 \end{array}$$

$$\begin{array}{r} 504.6 \\ +01 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 504.7 \\ +02 \\ \hline 33 \end{array}$$

LEFAX FILING INDEX

Fence

70

85

40

40

40

39

41

44

41

Sta.					
147	514.2 +0.3 50	43	513.9 0.0 35 Rd	514.3 0.4 15 Rd	513.9
146	522.8 +2.5 50	42 Fence	520.7 +0.4 33 Rd	520.7 +0.4 12.7 Rd	520.3
132	526.9 +3.5 50	42 Fence	524.5 +1.1 23	523.6 +0.2 42 Rd	523.4
145	527.4 +3.8 50	44 Fence	524.6 +1.0 29 Rd.	523.9 +0.3 8 Rd	523.6
168			524.9 +3.4 50	522.4 -1.1 29 Rd	523.5
143	523.7 +5.2 50	517.9 +0.1 31 Rd	518.1 +0.3 18 Rd	517.8 10 Fence	517.8
142		526.4 ✓ +13.2 50	521.9 ✓ +2.7 16	518.1 ✓ -0.4 9 Rd.	518.5 ✓
141			524.0 ✓ +17.5 50		506.5 ✓
168			523.6 ✓ +4.8 50		508.8 ✓
140			514.6 ✓ +12.2 50	503.3 ✓ +0.2 10	502.9 ✓

Road Road

Fence

$$\begin{array}{r} 512.2 \\ -17 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 512.8 \\ -25 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 520.0 \\ -34 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 520.2 \\ -34 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 522.2 \\ -12 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 516.2 \\ -16 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 511.4 \\ -11 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 504.8 \\ -12 \\ \hline 20 \end{array}$$

31

52

00

$$\begin{array}{r} 512.5 \\ -00 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 506.2 \\ -03 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 505.2 \\ -3.6 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 502.5 \\ -0.1 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 00 \\ -15 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 505.3 \\ -35 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 502.2 \\ -03 \\ \hline 42 \end{array}$$



Sta

Road Road

£

	526.8	520.3	504.8	505.1	
157	$\frac{+23.9}{50}$	$\frac{+17.2}{32}$	$\frac{+1.2}{26}$	$\frac{+2.2}{5}$	502.9

	519.6	511.9	503.3	503.4	
156	$\frac{+17.2}{50}$	$\frac{+10.2}{38}$	$\frac{+1.6}{26}$	$\frac{+1.2}{3}$	501.7

Fence

	505.0	500.6	500.5		
155	$\frac{+6.4}{50}$	$\frac{+2.2}{34}$	$\frac{+1.2}{14}$		498.6

Fence

	503.7	502.5	502.5	501.9	598.1
154	$\frac{+5.8}{50}$	$\frac{+4.6}{42}$	$\frac{+4.6}{18}$	$\frac{+2.2}{11}$	$\frac{+0.2}{7}$

Ad.

	514.2	504.9	505.5	499.5	
153	$\frac{+15.2}{55}$	$\frac{+5.5}{46}$	$\frac{+6.3}{22}$	$\frac{+0.3}{8}$	499.2

Fence

	510.8	510.6	505.0	505.2	501.8
152	$\frac{+10.2}{50}$	$\frac{9.2}{47}$	$\frac{+4.2}{39}$	$\frac{+4.4}{15}$	$\frac{+1.2}{7}$

	505.1	505.0	504.7		
150185	$\frac{+2.1}{50}$	48	$\frac{+1.2}{36}$	$\frac{+1.4}{14}$	503.3

	508.3	505.8	506.1		
150	$\frac{+3.4}{50}$	47	$\frac{+0.6}{32}$	$\frac{+0.2}{14}$	505.2

	509.6	507.0	506.9		
149	$\frac{+3.1}{50}$	46	$\frac{+0.8}{34}$	$\frac{+0.2}{15}$	506.2

Fence

	510.6	508.9	508.8		
148	$\frac{+2.4}{50}$	45	$\frac{+0.5}{35}$	$\frac{+0.6}{17}$	508.2

Fence



Fence

LEFAX FILING INDEX

7	$\begin{array}{r} 497.5 \\ -54 \\ \hline 443.5 \end{array}$	$\begin{array}{r} 497.3 \\ -56 \\ \hline 441.3 \end{array}$
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	$\begin{array}{r} 498.2 \\ -32 \\ \hline 466.2 \end{array}$	$\begin{array}{r} 497.8 \\ -32 \\ \hline 465.8 \end{array}$	Plowed ground
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0.0	$\begin{array}{r} 498.2 \\ -0.4 \\ \hline 497.8 \end{array}$		
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4	$\begin{array}{r} 498.5 \\ +0.6 \\ \hline 504.1 \end{array}$		
---	--	--	--

3	$\begin{array}{r} 498.8 \\ -0.4 \\ \hline 498.4 \end{array}$		
---	--	--	--

3	$\begin{array}{r} 499.4 \\ -1.4 \\ \hline 498.0 \end{array}$	Plowed - Ground	
---	--	--------------------	--

5	$\begin{array}{r} 501.9 \\ -1.1 \\ \hline 500.8 \end{array}$		
---	--	--	--

4	$\begin{array}{r} 502.3 \\ -2.2 \\ \hline 500.1 \end{array}$	$\begin{array}{r} 501.4 \\ -3.8 \\ \hline 497.6 \end{array}$	
---	--	--	--

2	$\begin{array}{r} 503.2 \\ -3.0 \\ \hline 500.2 \end{array}$	$\begin{array}{r} 502.1 \\ -4.1 \\ \hline 498.0 \end{array}$	
---	--	--	--

3	$\begin{array}{r} 506.0 \\ -3.2 \\ \hline 502.8 \end{array}$		
---	--	--	--

10						
Sta			Road	Road		\$
		500.9	499.7	500.0		
164	$\frac{+16}{58}$	$\frac{+34}{40}$	$\frac{+32}{23}$	7	496.3	
				Fence		
	500.5	501.1	501.5			
163+50	$\frac{+12}{50}$	53	$\frac{+18}{38}$	$\frac{+52}{24}$	3	496.3
				Fence	Top of slope	
	519.4	518.4	501.4			
163	$\frac{+17}{50}$	$\frac{+11}{43}$	$\frac{-01}{25}$	$\frac{00}{0.0}$		501.5
	520.8	515.3	501.5	501.3		
162	$\frac{+20}{50}$	$\frac{+14}{43}$	$\frac{+10}{38}$	$\frac{08}{25}$	$\frac{08}{6}$	500.5
	525.2	518.7	503.4			
161	$\frac{+22}{50}$	$\frac{+13}{41}$	$\frac{+04}{35}$	$\frac{00}{22}$	$\frac{00}{00}$	503.0
		512.3	503.1	503.6		
160		$\frac{+20}{49}$	$\frac{+22}{34}$	$\frac{+32}{9}$		500.3
	519.9	516.6	504.4	504.5		
159	$\frac{+19}{50}$	$\frac{+16}{47}$	$\frac{+38}{44}$	$\frac{+31}{32}$	$\frac{7}{7}$	500.6
	521.5	516.7	503.9			
168	$\frac{+17}{50}$	$\frac{+12}{42}$	$\frac{-05}{38}$	$\frac{00}{27}$	$\frac{00}{10}$	504.4
	517.5	512.3	504.5	504.7		
158	$\frac{+13}{50}$	$\frac{+8}{42}$	$\frac{+02}{36}$	$\frac{+02}{29}$	$\frac{+01}{6}$	504.3
	525.8	513.3	506.3	505.1		
157+59	$\frac{+22}{50}$	$\frac{+20}{42}$	$\frac{+34}{30}$	$\frac{+23}{30}$		502.9
		Fence				

Fence

LEFAX FILING INDEX

$$\begin{array}{r} 503.3 \\ 03 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 10 \\ 496.9 \\ -36 \\ \hline 7 \end{array}$$

$$\begin{array}{r} 497.6 \\ -54 \\ \hline 44 \end{array}$$

$$\begin{array}{r} 497.6 \\ -27 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 497.2 \\ -34 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 511.8 \\ +74 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 498.8 \\ -58 \\ \hline 11 \end{array}$$

$$\begin{array}{r} 497.1 \\ -58 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 496.9 \\ -36 \\ \hline 7 \end{array}$$

$$\begin{array}{r} 497.6 \\ -54 \\ \hline 44 \end{array}$$

$$\begin{array}{r} 497.6 \\ -27 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 497.2 \\ -34 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 511.8 \\ +74 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 498.8 \\ -58 \\ \hline 11 \end{array}$$

$$\begin{array}{r} 497.1 \\ -58 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 495.3 \\ -10 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 496.4 \\ -10 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 495.6 \\ -59 \\ \hline 77 \end{array}$$

$$\begin{array}{r} 495.6 \\ -60 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 495.4 \\ -51 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 496.4 \\ -65 \\ \hline 45 \end{array}$$

$$\begin{array}{r} 496.3 \\ -40 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 496.9 \\ -37 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 496.6 \\ -78 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 496.8 \\ -75 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 496.9 \\ -60 \\ \hline 50 \end{array}$$



Sta	Fence	Road	Road	Σ
172	$\frac{+216}{50}$	46	$\frac{+102}{36}$	493.6
173	$\frac{+247}{51}$	38	$\frac{+122}{36}$	494.4
172+67	$\frac{+233}{50}$	47	$\frac{+122}{36}$	496.1
168	$\frac{+34}{50}$	17	$\frac{+04}{10}$	501.5
170	$\frac{+35}{50}$	35	$\frac{+11}{80}$	498.1
169	$\frac{+33}{50}$	41	$\frac{+09}{16}$	495.0
168	$\frac{+79}{50}$	45	$\frac{+12}{80}$	498.0
167	$\frac{+78}{55}$	24	$\frac{+28}{85}$	500.1
166	$\frac{+63}{50}$	35	$\frac{+25}{6}$	496.9
181	$\frac{+125}{50}$	32	$\frac{+04}{10}$	499.7



Fence

$$\begin{array}{r}
 490.8 \\
 -28 \\
 \hline
 12
 \end{array}
 \qquad
 \begin{array}{r}
 490.5 \\
 -36 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 491.4 \\
 -30 \\
 \hline
 50
 \end{array}
 \qquad
 \begin{array}{r}
 491.1 \\
 -53 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 492.6 \\
 -35 \\
 \hline
 90
 \end{array}
 \qquad
 \begin{array}{r}
 492.0 \\
 -41 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 501.1 \\
 -06 \\
 \hline
 21 \\
 Pd
 \end{array}
 \qquad
 \begin{array}{r}
 41 \\
 -93 \\
 \hline
 64
 \end{array}$$

$$\begin{array}{r}
 493.8 \\
 -18 \\
 \hline
 78
 \end{array}
 \qquad
 \begin{array}{r}
 493.1 \\
 -50 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 494.5 \\
 -02 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 494.1 \\
 -33 \\
 \hline
 13
 \end{array}
 \qquad
 \begin{array}{r}
 493.2 \\
 -18 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 494.1 \\
 -52 \\
 \hline
 15
 \end{array}
 \qquad
 \begin{array}{r}
 494.1 \\
 -62 \\
 \hline
 40
 \end{array}$$

$$\begin{array}{r}
 496.3 \\
 -16 \\
 \hline
 7
 \end{array}
 \qquad
 \begin{array}{r}
 495.7 \\
 -22 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 496.7 \\
 -30 \\
 \hline
 7
 \end{array}
 \qquad
 \begin{array}{r}
 495.6 \\
 -41 \\
 \hline
 50
 \end{array}$$

Sta.	Fence Road Road				Σ
184	491.5 $\frac{+12}{50}$	34 $\frac{+18}{34}$	401.6 $\frac{+22}{29}$	489.0 $\frac{+21}{12}$	488.8
183	492.9 $\frac{+12}{50}$	34 $\frac{+23}{31}$	489.8 $\frac{+15}{16}$	489.3	487.5
182	492.9 $\frac{+53}{50}$	39 $\frac{+28}{32}$	489.8 $\frac{+23}{16}$	487.3	487.0
181	493.7 $\frac{+18}{50}$	42 $\frac{+23}{33}$	490.9 $\frac{+12}{17}$	490.8	488.9
180	503.7 $\frac{+143}{50}$	45 $\frac{+102}{39}$	491.2 $\frac{+18}{35}$	494.2 $\frac{+52}{19}$	499.2
179	502.7 $\frac{+153}{50}$	38 $\frac{+86}{32}$	491.0 $\frac{+18}{30}$	494.2 $\frac{+52}{16}$	489.4
178	508.1 $\frac{+176}{50}$	38 $\frac{+102}{33}$	496.2 $\frac{+58}{29}$	497.0 $\frac{+62}{13}$	491.0
177	514.6 $\frac{+212}{50}$	39 $\frac{+141}{34}$	501.7 $\frac{+72}{30}$	501.1 $\frac{+72}{14}$	493.4
176	516.0 $\frac{27.2}{50}$	39 $\frac{+182}{36}$	509.0 $\frac{+89}{31}$	502.6 $\frac{+86}{15}$	493.8
175	514.8 $\frac{+224}{50}$	40 $\frac{+161}{39}$	507.6 $\frac{+102}{35}$	502.7 $\frac{+102}{21}$	492.7

Fence

LEFAX FILING INDEX

8		4855
		$\frac{-12}{50}$
10°		4862
		$\frac{-12}{50}$
5°		4865
		$\frac{-0.5}{50}$
0	4866	4867
	$\frac{-22}{11}$	$\frac{-22}{50}$
2°	4872	4896
	$\frac{-20}{90}$	$\frac{-16}{50}$
5°	4870	4881
	$\frac{-14}{120}$	$\frac{-13}{50}$
6°	4876	4884
	$\frac{-24}{14}$	$\frac{-26}{50}$
6°	4888	4888
	$\frac{-15}{19}$	$\frac{-46}{50}$
7°	4895	4891
	$\frac{-10}{16}$	$\frac{-14}{50}$
6°	4897	4895
	$\frac{-30}{16}$	$\frac{-32}{50}$



Sta.	Fence	Road	Road	E
194	$\frac{+32}{50}$ 493.0	$\frac{+22}{29}$ 492.0	$\frac{+01}{22}$ 489.9	489.8
193	$\frac{+28}{50}$	$\frac{+22}{30}$ 493.9	$\frac{+05}{25}$ 491.9	481.7 491.2
192	$\frac{+22}{50}$ 495.8	$\frac{+22}{29}$ 495.3	$\frac{0.0}{25}$ 493.2	493.0
191	$\frac{+32}{50}$ 496.5	$\frac{+22}{30}$ 495.1	$\frac{+05}{25}$ 493.3	493.0 492.8
190	$\frac{+25}{50}$ 496.8	$\frac{+20}{32}$ 496.0	$\frac{+02}{26}$ 494.3	494.3 494.0
189	$\frac{+34}{50}$ 496.0	$\frac{+22}{32}$ 495.1	$\frac{+08}{28}$ 492.4	493.0 492.6
188	$\frac{+15}{50}$ 499.9	$\frac{+11}{32}$ 499.5 Fence	$\frac{+01}{26}$ 488.3	488.7 488.4
187	$\frac{+30}{50}$ 490.7	$\frac{+23}{34}$ 490.0	$\frac{+02}{29}$ 488.4	488.3 487.7
186	$\frac{+22}{50}$ 491.2	$\frac{+22}{36}$ 491.2	$\frac{+02}{30}$ 488.7	488.9 488.5
185	$\frac{+25}{50}$ 491.1	$\frac{+23}{35}$ 500.8	$\frac{+04}{31}$ 488.9	488.9 488.5



Fence

LEFAX FILING INDEX

$$11^{\circ} \quad \begin{array}{r} 488.4 \\ -14 \\ \hline 77 \end{array} \quad \begin{array}{r} 487.8 \\ -20 \\ \hline 50 \end{array}$$

$$10^{\circ} \quad \begin{array}{r} 489.7 \\ -15 \\ \hline 76 \end{array} \quad \begin{array}{r} 489.2 \\ -20 \\ \hline 50 \end{array}$$

$$10^{\circ} \quad \begin{array}{r} 490.1 \\ -29 \\ \hline 50 \end{array}$$

$$9^{\circ} \quad \begin{array}{r} 490.3 \\ -25 \\ \hline 50 \end{array}$$

$$8^{\circ} \quad \begin{array}{r} 491.5 \\ -25 \\ \hline 50 \end{array}$$

$$6^{\circ} \quad \begin{array}{r} 491.4 \\ -12 \\ \hline 110 \end{array} \quad \begin{array}{r} 485.7 \\ -33 \\ \hline 50 \end{array}$$

$$3^{\circ} \quad \begin{array}{r} 486.8 \\ -14 \\ \hline 50 \end{array}$$

$$2^{\circ} \quad \begin{array}{r} 486.5 \\ -12 \\ \hline 50 \end{array}$$

$$6^{\circ} \quad \begin{array}{r} 487.6 \\ -09 \\ \hline 50 \end{array}$$

$$7^{\circ} \quad \begin{array}{r} 486.6 \\ -19 \\ \hline 78 \end{array} \quad \begin{array}{r} 485.5 \\ -30 \\ \hline 50 \end{array}$$

10

Sta. Force Road Road

⊗

4870.0    483.7    4548

205  $\frac{+25}{50}$   $\frac{-13}{30}$   $\frac{-0.2}{24}$   $\frac{0.0}{50}$     485.0

4871.9    488.2    486.4

204  $\frac{+0.2}{50}$   $\frac{+12}{26}$   $\frac{-0.6}{19}$   $\frac{0.0}{2}$     489.0

4880    486.1

203  $\frac{+12}{50}$   $\frac{+14}{27.5}$   $\frac{0.0}{22}$   $\frac{0.0}{40}$     486.7

488.4    488.0

201  $\frac{+7.4}{50}$   $\frac{+20}{27}$   $\frac{0.0}{22}$   $\frac{0.0}{30}$     486.0

4886    488.5    4871.1

200  $\frac{+12}{50}$   $\frac{+12}{27}$   $\frac{-0.2}{20}$   $\frac{0.0}{7.0}$     487.3

4921.6    492.3

199  $\frac{+20}{50}$   $\frac{+12}{25}$   $\frac{0.0}{19}$   $\frac{0.0}{1.0}$     490.6

4911.8    490.3    488.3

198  $\frac{+30}{50}$   $\frac{+24}{27}$   $\frac{+0.2}{21}$   $\frac{0.0}{2}$     487.9

482.6    486.6    486.1

197  $\frac{+33}{50}$   $\frac{+20}{29}$   $\frac{+0.2}{22}$   $\frac{0.0}{4}$     484.6

4871.1    486.9    485.0

196  $\frac{+10}{50}$   $\frac{+16}{30}$   $\frac{-0.2}{22}$   $\frac{0.0}{42}$     485.3

488.5    488.2    486.8

195  $\frac{+16}{50}$   $\frac{+12}{31}$   $\frac{-0.1}{23}$   $\frac{0.0}{4.0}$     486.9

Fence

LEFAX FILING INDEX

3°

$$\begin{array}{r} 483.2 \\ 50 \overline{) 1} \end{array}$$

6°

$$\begin{array}{r} 485.0 \\ 5 \overline{) 20} \end{array}$$

$$\begin{array}{r} 484.8 \\ 50 \overline{) 22} \end{array}$$

4°

$$\begin{array}{r} 484.5 \\ 12 \overline{) 22} \end{array}$$

$$\begin{array}{r} 484.9 \\ 50 \overline{) 23} \end{array}$$

5°

$$\begin{array}{r} 484.6 \\ 10 \overline{) 21} \end{array}$$

$$\begin{array}{r} 484.7 \\ 50 \overline{) 23} \end{array}$$

6°

$$\begin{array}{r} 485.1 \\ 50 \overline{) 24} \end{array}$$

6°

$$\begin{array}{r} 485.0 \\ 50 \overline{) 25} \end{array}$$

6°

$$\begin{array}{r} 483.7 \\ 50 \overline{) 25} \end{array}$$

8°

$$\begin{array}{r} 483.7 \\ 50 \overline{) 25} \end{array}$$

8°

$$\begin{array}{r} 484.6 \\ 50 \overline{) 25} \end{array}$$

8°

$$\begin{array}{r} 484.6 \\ 50 \overline{) 25} \end{array}$$

2°

⊗

Fence Road Road Fence

214  $\frac{+5^A}{46}$   $\frac{+22^B}{28}$   $\frac{+1^C}{10}$  A888 A85A A890 A83.4

213  $\frac{+5^A}{50}$   $\frac{+5^B}{42}$   $\frac{+1^C}{27}$   $\frac{+1^D}{12}$  A87A A87A A83.4 A831 A81.5

212  $\frac{+7^A}{50}$   $\frac{+5^B}{33}$   $\frac{+3^C}{29}$   $\frac{+2^D}{13}$   $5^E$  A880 A85.9 A83.3 A82.5 A80.1

211  $\frac{+10^A}{50}$   $32$   $\frac{+2^B}{29}$   $\frac{+2^C}{13}$   $5^D$  A90.3 A82.3 A82.5 A80.3

210  $\frac{+6^A}{50}$   $\frac{+5^B}{30}$   $\frac{+2^C}{27}$   $\frac{+2^D}{10}$   $4^E$  A87.8 A86.1 A85.3 A85.2 A83.1

209  $\frac{6^A}{50}$   $\frac{+4^B}{32}$   $\frac{+1^C}{28}$   $\frac{+1^D}{10}$   $4^E$  A94.7 A92.9 A89.7 A89.8 A88.9

208  $\frac{+5^A}{50}$   $\frac{+3^B}{32}$   $\frac{+0^C}{27}$   $\frac{+1^D}{9}$   $3^E$  A93.3 A88.8 A88.9 A88.9 A84.4

207  $\frac{+1^A}{50}$   $\frac{+2^B}{33}$   $\frac{0^C}{27}$   $\frac{+0^D}{9}$  A86.5 A86.5 A86.5 A86.6

134  $\frac{+2^A}{50}$   $52$   $\frac{+0^B}{21}$   $\frac{0^C}{0}$  A85A A85.1

206  $\frac{+1^A}{50}$   $\frac{+1^B}{37}$   $\frac{+0^C}{25}$   $\frac{+0^D}{7}$  A86.0 A86.6 A86A A84.9 A84.8



Fence

5°  $\frac{-42}{15}$  479.2

5°  $\frac{-24}{50}$  499.1

$\frac{-13}{50}$  478.8

$\frac{-60}{50}$  479.4

$\frac{-29}{50}$  480.2

$\frac{-52}{50}$  483.4

$\frac{-12}{30}$  487.3

$\frac{-55}{50}$  472.9

$\frac{-12}{60}$  484.4

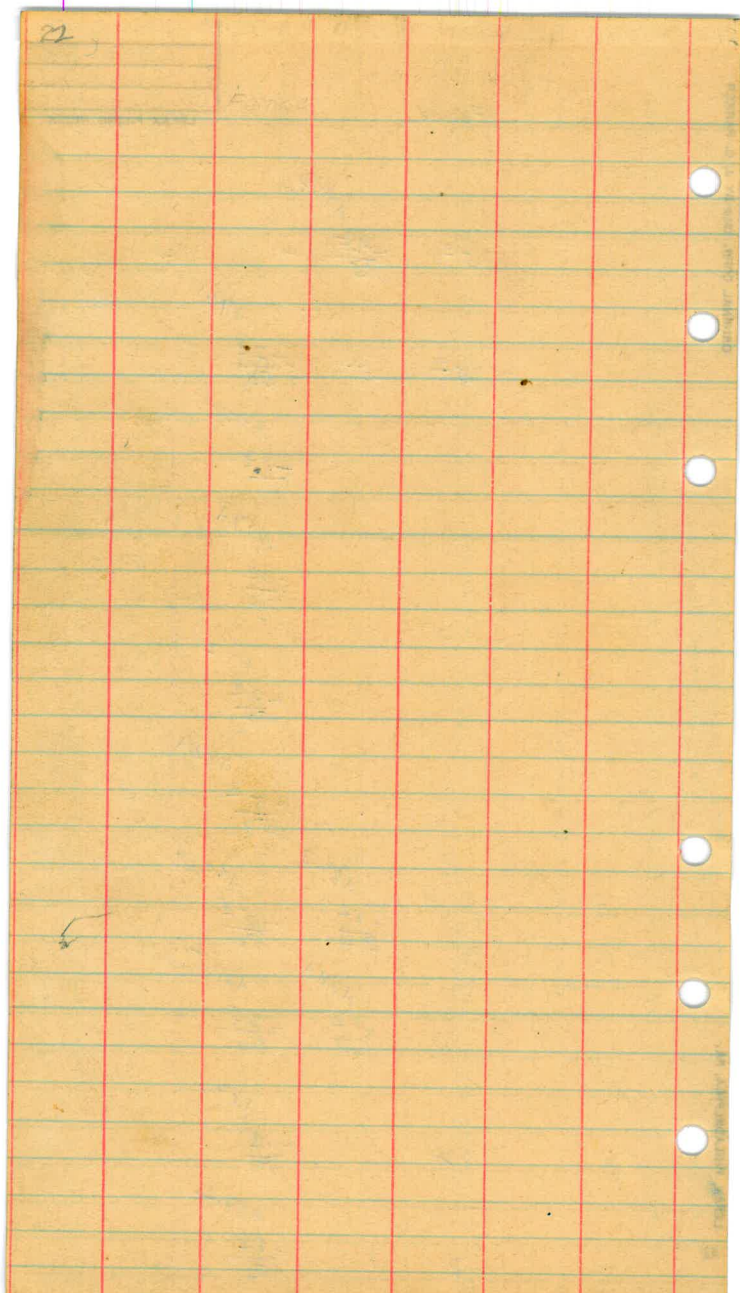
$\frac{-35}{50}$  482.5

12

$\frac{-18}{50}$  483.3

7

$\frac{-16}{50}$  483.2





Sta.	Fence	Road	±	
223	$\begin{array}{r} 491.2 \\ +9.9 \\ \hline 50 \end{array}$	$\begin{array}{r} 488.6 \\ +2.3 \\ \hline 39 \end{array}$	$\begin{array}{r} 481.2 \\ -0.1 \\ \hline 36 \end{array}$	481.3
282	$\begin{array}{r} 491.9 \\ +11.0 \\ \hline 50 \end{array}$	$\begin{array}{r} 488.3 \\ +2.4 \\ \hline 38 \end{array}$	$\begin{array}{r} 481.2 \\ +0.3 \\ \hline 33 \end{array}$	480.9
222	$\begin{array}{r} 494.6 \\ +13.5 \\ \hline 50 \end{array}$	$\begin{array}{r} 490.8 \\ +6.0 \\ \hline 40 \end{array}$	$\begin{array}{r} 0.0 \\ 36 \end{array}$	480.8
221	$\begin{array}{r} 489.7 \\ +2.2 \\ \hline 50 \end{array}$	$\begin{array}{r} 489.6 \\ -0.2 \\ \hline 45 \end{array}$		479.6
220	$\begin{array}{r} 486.3 \\ +2.2 \\ \hline 50 \end{array}$	$\begin{array}{r} 481.9 \\ +2.5 \\ \hline 32 \end{array}$	$\begin{array}{r} 0.0 \\ 30 \end{array}$	479.1
219	$\begin{array}{r} 489.1 \\ +2.4 \\ \hline 50 \end{array}$	$\begin{array}{r} 481.2 \\ +1.5 \\ \hline 23 \end{array}$	$\begin{array}{r} -0.1 \\ 18 \end{array}$	479.7
218+25	$\begin{array}{r} 484.5 \\ +3.6 \\ \hline 33 \end{array}$	$\begin{array}{r} 482.6 \\ +1.2 \\ \hline 16 \end{array}$	$\begin{array}{r} 481.1 \\ +0.2 \\ \hline 15 \end{array}$	480.9
217	$\begin{array}{r} 481.9 \\ +1.6 \\ \hline 34 \end{array}$	$\begin{array}{r} 480.8 \\ +0.5 \\ \hline 22 \end{array}$	$\begin{array}{r} 480.6 \\ +0.3 \\ \hline 9 \end{array}$	480.3
216	$\begin{array}{r} 484.0 \\ +2.2 \\ \hline 39 \end{array}$	$\begin{array}{r} 482.3 \\ +0.5 \\ \hline 27 \end{array}$	$\begin{array}{r} 482.4 \\ +0.5 \\ \hline 90 \end{array}$	481.6
215	$\begin{array}{r} 483.6 \\ +1.6 \\ \hline 50 \end{array}$	$\begin{array}{r} 482.5 \\ +0.5 \\ \hline 27 \end{array}$	$\begin{array}{r} 482.6 \\ +0.6 \\ \hline 12 \end{array}$	482.0



Sta. Road Fence

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Station	Angle	Distance	Calculation 1	Calculation 2
223	$\frac{0^\circ}{3}$		$\begin{array}{r} 476.5 \\ -4.5 \\ \hline 70 \end{array}$	$\begin{array}{r} 475.3 \\ -6.0 \\ \hline 15 \end{array}$
+82			$\begin{array}{r} 475.7 \\ -5.2 \\ \hline 7 \end{array}$	$\begin{array}{r} 475.3 \\ -5.3 \\ \hline 50 \end{array}$
222			$\begin{array}{r} 476.1 \\ -4.2 \\ \hline 12 \end{array}$	$\begin{array}{r} 476.0 \\ -4.8 \\ \hline 50 \end{array}$
221	$\frac{+0^\circ}{10}$		$\begin{array}{r} 475.7 \\ -4.1 \\ \hline 8 \end{array}$	$\begin{array}{r} 475.7 \\ -4.1 \\ \hline 50 \end{array}$
220	$\frac{+0^\circ}{10}$		$\begin{array}{r} 475.9 \\ -3.2 \\ \hline 70 \end{array}$	$\begin{array}{r} 477.1 \\ -3.0 \\ \hline 50 \end{array}$
219	$\frac{+11.3^\circ}{9^\circ}$	12	$\begin{array}{r} 477.6 \\ -2.1 \\ \hline 13 \end{array}$	$\begin{array}{r} 477.5 \\ -2.2 \\ \hline 50 \end{array}$
218+25	$\frac{480.2^\circ}{16^\circ}$	31	$\begin{array}{r} 478.2 \\ -2.2 \\ \hline 32 \end{array}$	$\begin{array}{r} 478.3 \\ -2.0 \\ \hline 50 \end{array}$
217	$5^\circ$		$\begin{array}{r} 478.7 \\ -1.6 \\ \hline 70 \end{array}$	$\begin{array}{r} 478.3 \\ -2.0 \\ \hline 50 \end{array}$
216	$5^\circ$		$\begin{array}{r} 478.8 \\ -3.0 \\ \hline 74 \end{array}$	$\begin{array}{r} 478.0 \\ -3.0 \\ \hline 50 \end{array}$
215	$6^\circ$		$\begin{array}{r} 478.8 \\ -3.0 \\ \hline 74 \end{array}$	$\begin{array}{r} 478.8 \\ -3.0 \\ \hline 50 \end{array}$

	Fence	Road	Road		♀
231	517.6 338 70	510.8 270 55	500.7 +163 52	501.1 +172 31	483.8
230	516.3 +263 70 Fence	509.3 +193 49	499.8 +98 45	500.8 +108 24	490.0
242	513.4 +221 75 Fence	509.2 9 61	498.3 +72 51	499.6 +83 30	491.3
229	511.1 +26 70 Fence	504.3 132 49	496.3 +53 44	506.1 +56 20	491.1
228	502.2 +216 72	491.6 +110 67	490.2 +96 52	490.2 +96 27	480.6
227	488.0 85 50 Fence	487.5 +82 48	484.0 +45 45	481.8 +23 12	479.5
281		482.3 +23 50	480.8 +08 33	480.4 +04 6	470.0
226		479.0 +11 50	479.0 00 33	479.0 +01 6	476.9
225		479.3 +28 50		00 29	476.5
267		485.9 +90 74 Fence	479.0 +30 44	480.6 +35 18	477.3 +05 8 476.8

Sta.

Fence

LEFAX FILING INDEX

		$\frac{121}{28}$	$\frac{118}{38}$
231			
		$\frac{190}{35}$	
230			
		$\frac{212}{47}$	$\frac{226}{65}$
242	20		
		$\frac{132}{40}$	$\frac{202}{58}$
229	16		$\frac{202}{23}$
		$\frac{50}{35}$	$\frac{52}{50}$
228			
		$\frac{10}{10}$	$\frac{42}{74}$
229			$\frac{45}{50}$
		$\frac{50}{16}$	$\frac{54}{50}$
281			
		$\frac{02}{6}$	$\frac{25}{50}$
226	20		
			$\frac{12}{50}$
225	?		
			$\frac{16}{50}$
267			







Fence

239

$$\begin{array}{r} 781.1 \\ -33 \\ \hline 30 \end{array}$$

238

$$\begin{array}{r} 477.5 \\ -62 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 476.4 \\ -76 \\ \hline 36 \\ \text{Fence} \end{array}$$

237

$$\begin{array}{r} 475.2 \\ -105 \\ \hline 47 \end{array}$$

$$\begin{array}{r} 474.7 \\ -110 \\ \hline 54 \end{array}$$

$$\begin{array}{r} 471.3 \\ -105 \\ \hline 75 \end{array}$$

236+50

$$\begin{array}{r} 473.3 \\ -105 \\ \hline 34 \end{array}$$

$$\begin{array}{r} 471.0 \\ -128 \\ \hline 50 \end{array}$$

236

$$\begin{array}{r} 472.5 \\ -148 \\ \hline 44 \end{array}$$

235

$$\begin{array}{r} 477.0 \\ -127 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 472.2 \\ -178 \\ \hline 68 \end{array}$$

234+55

$$\begin{array}{r} 472.1 \\ -188 \\ \hline 72 \end{array}$$

234

$$\begin{array}{r} 473.0 \\ -219 \\ \hline 91 \end{array}$$

233

$$\begin{array}{r} 494.4 \\ -21 \\ \hline 73 \end{array}$$

$$\begin{array}{r} 488.8 \\ -52 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 479.9 \\ -164 \\ \hline 78 \end{array}$$

$$\begin{array}{r} 473.3 \\ -202 \\ \hline 70 \end{array}$$

232

$$\begin{array}{r} 471.3 \\ -92 \\ \hline 31 \end{array}$$

$$\begin{array}{r} 470.5 \\ -10 \\ \hline 50 \end{array}$$

28

	$\Delta 70.1$		$\Delta 70.1$	$\Delta 66.6$	$\Delta 66.7$
248	$\frac{+4\frac{1}{2}}{50}$	45	$\frac{+4\frac{1}{2}}{43}$	$\frac{+0\frac{1}{2}}{33}$	$\frac{+0\frac{1}{2}}{11}$
					466.2

			$\Delta 66.6$		
+40		30	$\frac{-0\frac{1}{2}}{24}$	$\frac{0\frac{1}{2}}{22}$	

	$\Delta 65.3$				
247	$\frac{-0\frac{1}{2}}{50}$	30	$\frac{+0\frac{1}{2}}{24}$	$\frac{0\frac{1}{2}}{22}$	466.5

	$\Delta 65.7$		$\Delta 65.5$	$\Delta 65.5$	
246	$\frac{+0\frac{1}{2}}{50}$	29	$\frac{+0\frac{1}{2}}{24}$	$\frac{+0\frac{1}{2}}{22}$	465.3

	$\Delta 66.1$				
245	$\frac{-0\frac{1}{2}}{50}$	28	$\frac{0\frac{1}{2}}{24}$	$\frac{+0\frac{1}{2}}{22}$	466.2

	$\Delta 66.5$		$\Delta 67.8$	$\Delta 67.9$	
244	$\frac{-0\frac{1}{2}}{50}$		$\frac{+0\frac{1}{2}}{20}$	$\frac{+0\frac{1}{2}}{50}$	467.4

		$\Delta 74.3$	$\Delta 71.0$	$\Delta 71.2$	
243	$\frac{+3\frac{1}{2}}{50}$		$\frac{-0\frac{1}{2}}{21}$	$\frac{-0\frac{1}{2}}{6}$	471.2

		$\Delta 79.8$	$\Delta 75.8$	$\Delta 76.3$	
242	$\frac{2\frac{1}{2}}{50}$		$\frac{+0\frac{1}{2}}{24}$	$\frac{+1\frac{1}{2}}{8}$	475.0

		$\Delta 83.9$	$\Delta 80.2$	$\Delta 80.2$	
241	$\frac{+6\frac{1}{2}}{50}$		$\frac{+3\frac{1}{2}}{28}$	$\frac{+3\frac{1}{2}}{15}$	477.1

		$\Delta 89.7$	$\Delta 83.6$	$\Delta 84.3$	
240	$\frac{+2\frac{1}{2}}{50}$		$\frac{+1\frac{1}{2}}{22}$	$\frac{+1\frac{1}{2}}{10}$	482.5


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248

17

$$\begin{array}{r} 462.5 \\ -3.7 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 462.6 \\ -3.6 \\ \hline 50 \end{array}$$

249

5°

$$\begin{array}{r} 462.5 \\ -2.5 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 462.6 \\ -2.6 \\ \hline 50 \end{array}$$

247

4°

$$\begin{array}{r} 462.8 \\ -2.2 \\ \hline 82 \end{array}$$

$$\begin{array}{r} 463.0 \\ -2.5 \\ \hline 50 \end{array}$$

246

5°

$$\begin{array}{r} 464.2 \\ -1.1 \\ \hline 50 \end{array}$$

245

6°

$$\begin{array}{r} 465.0 \\ -1.2 \\ \hline 50 \end{array}$$

244

19°

$$\begin{array}{r} 466.9 \\ -0.5 \\ \hline 50 \end{array}$$

243

9°

$$\begin{array}{r} 467.6 \\ -3.6 \\ \hline 50 \end{array}$$

242

7°

$$\begin{array}{r} 470.5 \\ -4.5 \\ \hline 50 \end{array}$$

241

$$\begin{array}{r} 473.2 \\ -3.9 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 471.6 \\ -8.5 \\ \hline 50 \end{array}$$

240

Fence

$$\begin{array}{r} 476.7 \\ -3.8 \\ \hline 50 \end{array}$$



30

18

Sta.

257  $\frac{136}{50}$   $\frac{+110}{41}$   $\frac{+110}{27}$   $\frac{+39}{14}$   $\frac{+38}{8}$   $\frac{+176.5}{463.9}$   $\frac{+110}{46.9}$   $\frac{+39}{46.8}$   $\frac{+38}{46.7}$   $\frac{+176.5}{462.9}$

256  $\frac{+123}{50}$   $\frac{+76}{38}$   $\frac{+21}{27}$   $\frac{+21}{11}$   $\frac{+176.5}{464.1}$   $\frac{+76}{46.9}$   $\frac{+21}{46.7}$   $\frac{+21}{46.3}$

255  $\frac{+90}{50}$   $\frac{+50}{37}$   $\frac{+12}{30}$   $\frac{+16}{16}$   $\frac{+176.5}{467.9}$   $\frac{+50}{46.9}$   $\frac{+12}{46.2}$   $\frac{+16}{46.5}$   $\frac{+176.5}{461.9}$

254  $\frac{+64}{50}$   $\frac{39}{Fence}$   $\frac{+12}{33}$   $\frac{+12}{17}$   $\frac{+176.5}{467.9}$   $\frac{39}{46.9}$   $\frac{+12}{46.8}$   $\frac{+12}{46.6}$   $\frac{+176.5}{461.6}$

253  $\frac{+53}{50}$   $\frac{38}{Fence}$   $\frac{18}{32}$   $\frac{+12}{130}$   $\frac{+176.5}{466.5}$   $\frac{38}{46.9}$   $\frac{18}{46.0}$   $\frac{+12}{46.2}$   $\frac{+176.5}{461.2}$

252  $\frac{+50}{50}$   $\frac{36}{Fence}$   $\frac{+26}{30}$   $\frac{+25}{11}$   $\frac{+176.5}{466.4}$   $\frac{36}{46.9}$   $\frac{+26}{46.0}$   $\frac{+25}{46.4}$   $\frac{+176.5}{461.4}$

251  $\frac{10}{30}$   $\frac{32}{Fence}$   $\frac{+18}{28}$   $\frac{+19}{7}$   $\frac{+176.5}{463.3}$   $\frac{32}{46.9}$   $\frac{+18}{46.1}$   $\frac{+19}{46.2}$   $\frac{+176.5}{462.3}$

250  $\frac{-01}{50}$   $\frac{31}{Fence}$   $\frac{+02}{23}$   $\frac{+08}{5}$   $\frac{+176.5}{464.0}$   $\frac{31}{46.9}$   $\frac{+02}{46.3}$   $\frac{+08}{46.5}$   $\frac{+176.5}{461.6}$

72  $\frac{+03}{50}$   $\frac{30}{Fence}$   $\frac{-01}{22}$   $\frac{00}{40}$   $\frac{+176.5}{464.0}$   $\frac{30}{46.9}$   $\frac{-01}{46.6}$   $\frac{00}{46.7}$   $\frac{+176.5}{465.7}$

249  $\frac{+94}{50}$   $\frac{+64}{34}$   $\frac{-03}{28}$   $\frac{-03}{10}$   $\frac{+176.5}{495.7}$   $\frac{+64}{492.7}$   $\frac{-03}{46.3}$   $\frac{-03}{46.4}$   $\frac{+176.5}{466.6}$



379

Fence

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257

29

$$460.4$$

$$\frac{-25}{50}$$

256

11<sup>0</sup>

$$460.3$$

$$\frac{-20}{50}$$

255

$$460.4$$

$$\frac{-15}{50}$$

254

$$461.1$$

$$\frac{-0.5}{50}$$

253

$$\frac{0.3}{50}$$

252

$$\frac{0.2}{50}$$

251

$$461.6$$

$$\frac{-0.7}{20}$$

$$461.9$$

$$\frac{-0.9}{50}$$

250

$$0.0$$

$$\frac{0.0}{50}$$

$$464.5$$

$$\frac{-2.1}{50}$$

$$461.9$$

$$\frac{-2.2}{50}$$

172

5

$$462.3$$

$$\frac{-3.4}{74}$$

$$462.3$$

$$\frac{-3.4}{50}$$

249

16

$$462.5$$

$$\frac{-4.1}{27}$$

$$462.6$$

$$\frac{-4.0}{50}$$

Sta.					±
266	$\begin{array}{r} 491.4 \\ +32.5 \\ \hline 523.9 \end{array}$	$\begin{array}{r} 468.4 \\ 9.5 \\ \hline 477.9 \\ \text{Top Bank} \end{array}$	$\begin{array}{r} 459.2 \\ 9.0 \\ \hline 468.2 \\ \text{Bottom Bank} \end{array}$		458.9 ↑ edge Rd.
265	$\begin{array}{r} 481.1 \\ 20.0 \\ \hline 501.1 \end{array}$	$\begin{array}{r} 468.1 \\ +7.0 \\ \hline 475.1 \\ \text{Top Bank} \end{array}$	$\begin{array}{r} 461.2 \\ +0.4 \\ \hline 461.6 \\ \text{Bottom Bank} \end{array}$		461.1 Rd.
264	$\begin{array}{r} 489.1 \\ +38.4 \\ \hline 527.5 \end{array}$	$\begin{array}{r} 486.4 \\ +25.2 \\ \hline 511.6 \\ \text{Bottom Bank} \end{array}$	$\begin{array}{r} 479.1 \\ +18.4 \\ \hline 497.5 \\ \text{Top Bank} \end{array}$		460.5
263	$\begin{array}{r} 503.1 \\ +42.4 \\ \hline 545.5 \end{array}$	$\begin{array}{r} 497.0 \\ +36.3 \\ \hline 533.3 \\ \text{Wash} \end{array}$	$\begin{array}{r} 495.9 \\ +35.2 \\ \hline 531.1 \\ \text{Top Bank} \end{array}$		460.7
262	$\begin{array}{r} 487.9 \\ +26.8 \\ \hline 514.7 \end{array}$	$\begin{array}{r} 478.1 \\ +17.2 \\ \hline 495.3 \\ \text{Top Bank} \end{array}$	$\begin{array}{r} 459.9 \\ -0.2 \\ \hline 459.7 \\ \text{Bottom Bank} \end{array}$		461.1
261	$\begin{array}{r} 484.3 \\ +22.2 \\ \hline 506.5 \end{array}$	$\begin{array}{r} 474.3 \\ 17 \\ \hline 491.3 \\ \text{Top Bank} \end{array}$	$\begin{array}{r} 462.1 \\ +7.4 \\ \hline 469.5 \\ \text{Bottom Bank} \end{array}$		462.3
260	$\begin{array}{r} 475.2 \\ +11.0 \\ \hline 486.2 \end{array}$	$\begin{array}{r} 467.2 \\ +7.0 \\ \hline 474.2 \\ \text{Top Bank} \end{array}$	$\begin{array}{r} 463.7 \\ -0.5 \\ \hline 463.2 \\ \text{Bottom Bank} \end{array}$		464.2
259	$\begin{array}{r} 466.4 \\ 9.2 \\ \hline 475.6 \end{array}$	$\begin{array}{r} 466.9 \\ +1.5 \\ \hline 468.4 \\ \text{Fence} \end{array}$	$\begin{array}{r} 466.6 \\ +1.2 \\ \hline 467.8 \\ \text{Top Bank} \end{array}$	$\begin{array}{r} 463.3 \\ +0.2 \\ \hline 463.5 \\ \text{Bottom Bank} \end{array}$	465.4
258	$\begin{array}{r} 471.1 \\ +4.2 \\ \hline 475.3 \end{array}$	$\begin{array}{r} 468.0 \\ 36 \\ \hline 504.0 \\ \text{Fence} \end{array}$	$\begin{array}{r} 467.1 \\ +1.4 \\ \hline 468.5 \\ \text{Road} \end{array}$	$\begin{array}{r} 467.1 \\ +0.2 \\ \hline 467.3 \\ \text{Road} \end{array}$	466.9
258	$\begin{array}{r} 472.1 \\ +5.6 \\ \hline 477.7 \end{array}$	$\begin{array}{r} 468.0 \\ 41 \\ \hline 509.0 \\ \text{Fence} \end{array}$	$\begin{array}{r} 467.1 \\ +1.3 \\ \hline 468.4 \\ \text{Road} \end{array}$	$\begin{array}{r} 467.1 \\ +0.8 \\ \hline 467.9 \\ \text{Road} \end{array}$	466.5

Sta.

Fence

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266  $\frac{+03}{24}$  Rd.  $\frac{+05}{21}$  Rd.  $\frac{-88}{26}$  Rd.

265  $\frac{-08}{17}$  Rd.  $\frac{-16}{28}$  Rd.  $\frac{-134}{42}$  Rd.

264  $\frac{-01}{6}$  Rd.  $\frac{00}{23}$  Rd.  $\frac{-08}{35}$  Rd.  $\frac{-112}{54}$  Rd.

263  $\frac{+01}{80}$  Rd.  $\frac{+01}{25}$  Rd.  $\frac{-03}{38}$  Rd.  $\frac{-113}{54}$  Rd.

262  $\frac{+06}{22}$  Rd.  $\frac{-114}{42}$  Rd.

261  $\frac{00}{00}$  Rd.  $\frac{00}{21}$  Rd.  $\frac{-04}{32}$  Rd.  $\frac{-122}{49}$  Rd.

260  $\frac{00}{5}$  Rd.  $\frac{-45}{11}$  Rd.  $\frac{-50}{21}$  Rd.  $\frac{-130}{25}$  Rd.

259  $\frac{-22}{9}$  Rd.  $\frac{-46}{50}$  Rd.

253  $\frac{-02}{50}$  Rd.  $\frac{-22}{13}$  Rd.  $\frac{-48}{50}$  Rd.

258  $\frac{-52}{50}$  Rd.

76

A58.6 A59.1 A50.1

A60.3 A59.5 A49.7

A60.4 A60.0 A49.8

A60.8 A60.8 A60.8

A60.6 A49.7

A61.9 A50.1

A59.7 A69.2 A51.2

A62.7 A60.8

A61.7 A64.2 A62.1

A61.4



34

$$450 \quad \begin{array}{r} 458.5 \\ +37 \\ \hline 50 \end{array}$$

$$275 \quad \begin{array}{r} 457.5 \\ +35 \\ \hline 50 \end{array}$$

$$274 \quad \begin{array}{r} 462.8 \\ +92 \\ \hline 50 \end{array}$$

$$273 \quad \begin{array}{r} 478.0 \\ +240 \\ \hline 50 \end{array} \quad \begin{array}{r} 463.0 \\ +90 \\ \hline 140 \end{array} \quad \begin{array}{r} 0.0 \\ 2.0 \end{array}$$

$$272 \quad \begin{array}{r} 487.8 \\ +32.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 466.4 \\ +113 \\ \hline 10 \end{array} \quad \begin{array}{r} 455.2 \\ +0.1 \\ \hline 4 \end{array}$$

$$271 \quad \begin{array}{r} 487.7 \\ 302 \\ \hline 50 \end{array} \quad \begin{array}{r} 467.5 \\ +102 \\ \hline 10 \end{array} \quad \begin{array}{r} 457.1 \\ +0.2 \\ \hline 3.0 \end{array}$$

$$270 \quad \begin{array}{r} 498.7 \\ +408 \\ \hline 50 \end{array} \quad \begin{array}{r} 477.9 \\ +202 \\ \hline 19 \end{array} \quad \begin{array}{r} 468.7 \\ +0.8 \\ \hline 6 \end{array}$$

$$269 \quad \begin{array}{r} 493.4 \\ 382 \\ \hline 50 \end{array} \quad \begin{array}{r} 471.0 \\ +128 \\ \hline 11 \end{array} \quad \begin{array}{r} 452.8 \\ -0.2 \\ \hline 6 \end{array}$$

$$268 \quad \begin{array}{r} 483.1 \\ +246 \\ \hline 50 \end{array} \quad \begin{array}{r} 470.8 \\ 123 \\ \hline 24 \end{array} \quad \begin{array}{r} 458.7 \\ +0.2 \\ \hline 16 \end{array} \quad \begin{array}{r} 458.7 \\ +0.2 \\ \hline 11 \end{array}$$

$$267 \quad \begin{array}{r} 467.6 \\ +176 \\ \hline 50 \end{array} \quad \begin{array}{r} 462.4 \\ +48 \\ \hline 23 \end{array} \quad \begin{array}{r} 458.7 \\ 0.0 \\ \hline 20 \end{array} \quad \begin{array}{r} 458.7 \\ +0.2 \\ \hline 12 \end{array}$$

453.9

453.6

454.0

455.1

456.8

457.9

458.1

458.5

458.9

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$$\begin{array}{r}
 45A.3 \\
 \frac{+0.5}{60} \\
 \text{Rad.}
 \end{array}
 \quad
 \begin{array}{r}
 45A.5 \\
 \frac{-0.3}{20} \\
 \text{Rad.}
 \end{array}
 \quad
 \begin{array}{r}
 45A.1 \\
 \frac{-0.2}{24}
 \end{array}
 \quad
 \begin{array}{r}
 44A.2 \\
 \frac{-10.6}{24}
 \end{array}$$

$$\begin{array}{r}
 45A.3 \\
 \frac{+0.4}{17}
 \end{array}
 \quad
 \begin{array}{r}
 45A.1 \\
 \frac{+0.2}{22}
 \end{array}
 \quad
 \begin{array}{r}
 44A.1 \\
 \frac{-9.8}{66}
 \end{array}$$

$$\begin{array}{r}
 0.0 \\
 \frac{2.0}{20} \\
 \text{Rad.}
 \end{array}
 \quad
 \begin{array}{r}
 45B.9 \\
 \frac{+0.2}{15}
 \end{array}
 \quad
 \begin{array}{r}
 44A.7 \\
 \frac{+0.2}{19}
 \end{array}
 \quad
 \begin{array}{r}
 44A.5 \\
 \frac{-8.9}{41}
 \end{array}$$

$$\begin{array}{r}
 45A.1 \\
 \frac{+0.1}{40} \\
 \text{Rad.}
 \end{array}
 \quad
 \begin{array}{r}
 45A.4 \\
 \frac{+0.4}{23}
 \end{array}
 \quad
 \begin{array}{r}
 45A.4 \\
 \frac{+0.4}{28}
 \end{array}
 \quad
 \begin{array}{r}
 44A.5 \\
 \frac{-9.2}{43}
 \end{array}$$

$$\begin{array}{r}
 45B.7 \\
 \frac{+0.6}{19}
 \end{array}
 \quad
 \begin{array}{r}
 45B.8 \\
 \frac{+0.2}{23}
 \end{array}
 \quad
 \begin{array}{r}
 44A.5 \\
 \frac{+12.6}{44}
 \end{array}$$

$$\begin{array}{r}
 0.0 \\
 \frac{7.8}{78}
 \end{array}
 \quad
 \begin{array}{r}
 45B.9 \\
 \frac{+0.1}{22}
 \end{array}
 \quad
 \begin{array}{r}
 44A.5 \\
 \frac{-12.3}{44}
 \end{array}$$

$$\begin{array}{r}
 0.0 \\
 \frac{1.8}{18}
 \end{array}
 \quad
 \begin{array}{r}
 49B.0 \\
 \frac{0.0}{24}
 \end{array}
 \quad
 \begin{array}{r}
 44A.5 \\
 \frac{-12.9}{44}
 \end{array}$$

$$\begin{array}{r}
 0.0 \\
 \frac{1.5}{15}
 \end{array}
 \quad
 \begin{array}{r}
 45B.0 \\
 \frac{-0.1}{21}
 \end{array}
 \quad
 \begin{array}{r}
 44A.5 \\
 \frac{-11.3}{39}
 \end{array}$$

$$\begin{array}{r}
 45B.3 \\
 \frac{-0.2}{6}
 \end{array}
 \quad
 \begin{array}{r}
 45B.3 \\
 \frac{-0.2}{72}
 \end{array}
 \quad
 \begin{array}{r}
 44A.5 \\
 \frac{-11.0}{28}
 \end{array}$$

$$\begin{array}{r}
 45B.3 \\
 \frac{-0.1}{52} \\
 \text{Rad.}
 \end{array}
 \quad
 \begin{array}{r}
 45B.1 \\
 \frac{-0.2}{10}
 \end{array}
 \quad
 \begin{array}{r}
 44A.2 \\
 \frac{-10.2}{24}
 \end{array}$$

36						
279						456.5
280	$\frac{111}{50}$	467.1		459.2		456.5
281	$\frac{102}{50}$	467.4		459.3		456.7
282	$\frac{252}{50}$	481.0	466.7			455.7
283	$\frac{172.7}{50}$	472.7	465.0	453.6	453.6	
284	$\frac{182}{50}$	472.7	465.0	453.6	453.6	454.3
285	$\frac{102}{32}$	464.9				454.3
286	$\frac{102}{15}$	464.9				454.3
287	$\frac{102}{50}$	464.9				454.3
288	$\frac{72.4}{31}$	475.4	463.0			454.0
289	$\frac{72.4}{31}$	475.4	463.0			454.0
290	$\frac{132}{25}$	466.1	459.1			452.9
291	$\frac{62}{60}$	466.1	459.1			452.9
292	$\frac{112}{25}$	467.5				456.5
293	$\frac{163}{50}$	469.0	456.4	452.9		452.7
294	$\frac{32}{9}$	457.3				452.7
295	$\frac{28}{50}$					454.5
296	$\frac{28}{50}$					454.5

Sta.

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285	$\frac{+0.4}{70}$ Rd.	$\frac{0.2}{21}$ Rd.	$\frac{+0.2}{26}$	30 Fence	A56.7
284	$\frac{+0.4}{5}$ Rd.	$\frac{+0.4}{78}$ Rd.	$\frac{+0.2}{25}$	30 Fence	A57.1, A58.9
283	$\frac{-1.2}{2}$	$\frac{-1.0}{5}$ Rd.	$\frac{-0.3}{79}$ Rd.	$\frac{-0.8}{30}$ 30 Fence	A46.1, A54.5, A54.7, A55.4, A54.9
282			$\frac{-0.6}{40}$	$\frac{-0.6}{16}$	A53.1, A55.7
281	$\frac{+0.3}{11}$	$\frac{+0.5}{15}$	$\frac{-1.0}{30}$		A52.6, A52.8, A44.0
280	$\frac{+0.3}{3}$ Rd.	$\frac{+0.4}{15}$ Rd.	$\frac{+0.5}{20}$	20 Fence	A54.3, A54.4, A54.5, A45.2
279	$\frac{+0.1}{30}$	$\frac{+0.8}{14}$	$\frac{+1.2}{18}$	19 Fence	A53.7, A53.9, A41.9
278	$\frac{-3.2}{4}$	$\frac{-4.2}{8}$	$\frac{-3.8}{23}$	30 Fence	A52.6, A52.7, A52.9, A42.9
277	$\frac{+0.4}{30}$	$\frac{+0.3}{15}$	$\frac{+0.1}{19}$	25 Fence	A52.7, A52.8, A47.0
276	$\frac{-0.4}{10}$ Rd.	$\frac{-0.2}{17}$	17 Fence	$\frac{-6.1}{29}$	A53.9, A53.0, A46.4



38

Sta

R

	463.5	455.2	
295+06	$\frac{+12^0}{50}$	$\frac{+32}{32}$	451.5
	464.9	452.0	
294	$\frac{+15^8}{50}$	$\frac{+29}{5}$ $\frac{0^0}{1^0}$	449.1
	479.0	463.1	
293	$\frac{+21^1}{50}$	$\frac{+5^2}{6}$ $\frac{0^0}{0^0}$	457.9
	464.3	451.2	
292	$\frac{+16^4}{50}$	$\frac{+3^0}{2}$ $\frac{0^0}{0^0}$	448.2
	464.1		
291	$\frac{+15^5}{50}$	$\frac{0^0}{2^0}$	448.6
	469.3	455.0	
290	$\frac{+18}{50}$	$\frac{+4^4}{5}$ $\frac{0^0}{0^0}$	451.3
	470.1		
289	$\frac{+15^3}{50}$	$\frac{0^0}{0^0}$ $\frac{1}{0^0}$	452.8
	473.9	460.4	
288	$\frac{+20^8}{50}$	$\frac{+7^3}{8}$ $\frac{+0^5}{2}$ $\frac{0^0}{0^0}$	453.6
	477.7	462.1	453.1
287	$\frac{+23^4}{50}$	$\frac{+7^5}{7}$ $\frac{0^0}{1^0}$	454.6
		475.3	462.0
286-		$\frac{+9^9}{43.0}$ $\frac{+6^6}{7}$	455.4



Sta.

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295+06	$\frac{-13}{10}$	$\frac{450.2}{10}$	$\frac{450.2}{29}$	$\frac{450.0}{35}$	$\frac{451.5}{35}$	$\frac{447.4}{50}$
294	$\frac{+0.3}{3}$	449.4	$\frac{+0.4}{16}$	449.5	$\frac{+0.2}{19}$	447.3
293	$\frac{+0.2}{3}$	458.1	$\frac{+0.3}{16}$	458.2	$\frac{+0.5}{19}$	455.1
292	$\frac{-0.2}{20}$	448.0	$\frac{+0.4}{21}$	448.6	$\frac{+0.4}{21}$	446.4
291	$\frac{-1.0}{20}$	447.6	$\frac{+0.3}{20}$	448.9	$\frac{-1.8}{28}$	446.6
290	$\frac{+0.2}{20}$	451.5	$\frac{+0.5}{150}$	451.8	$\frac{+0.4}{18}$	449.0
289	$\frac{-4.2}{4}$	450.5	$\frac{-1.0}{80}$	450.8	$\frac{-3.4}{20}$	451.4
288	$\frac{+0.2}{42}$	453.3	$\frac{+0.1}{170}$	453.2	$\frac{+0.2}{19}$	453.3
287	$\frac{+0.3}{38}$	454.9	$\frac{+0.4}{18}$	458.0	$\frac{+0.5}{22}$	447.1
286.	$\frac{+0.4}{30}$	455.8	$\frac{+0.7}{18}$	46.1	$\frac{+0.6}{22}$	446.0
F	Rd.	Rd.	Rd.	Rd.	40	Fence

Sta.					
305	A75.4 $\frac{+32.2}{50}$				A43.2
304	A72.7 $\frac{+30.2}{50}$				A42.5
303		A55.6 $\frac{+12.2}{30}$	A46.8 $\frac{+3.2}{15}$		A43.6
302	A70.9 $\frac{+26.0}{50}$				A44.9
301	A54.6 $\frac{+8.8}{50}$	A50.1 $\frac{+4.3}{39}$	A47.6 $\frac{+1.8}{9}$	A46.0 $\frac{+0.2}{5}$	A45.8
300	A74.8 $\frac{+29.3}{50}$		A53.4 $\frac{+7.2}{7}$		A45.5
299	A71.7 $\frac{+28.5}{50}$		A56.7 $\frac{+10.5}{9}$		A46.2
298	A58.6 $\frac{+11.2}{50}$	A51.4 $\frac{+4.0}{36}$	A49.0 $\frac{+1.6}{9}$		A47.4
297	A71.5 $\frac{+24.0}{50}$		A56.2 $\frac{+7.9}{8}$		A47.5
296	A70.4 $\frac{+22.1}{50}$		A56.0 $\frac{+7.2}{11}$		A48.3

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37<sub>r</sub>

4428  
 $\frac{-04}{3}$      $\frac{00}{18}$      $\frac{+01}{21}$      $\frac{-30}{30}$      $\frac{-30}{50}$   
 4427    4430    4430    4420

305

$\frac{+02}{2}$      $\frac{+05}{16}$      $\frac{+05}{19}$      $\frac{-05}{24}$   
 4438    4442    4442    4418    4418

304

$\frac{+02}{2}$      $\frac{+06}{15}$      $\frac{+06}{19}$      $\frac{-18}{34}$      $\frac{-18}{50}$   
 4444    4445    4445    4431

303

$\frac{+03}{5}$      $\frac{-04}{20}$      $\frac{-04}{22}$      $\frac{-18}{25}$   
 4458    4460    4460    4434    4431

302

$\frac{+01}{4}$      $\frac{+02}{20}$      $\frac{+02}{20}$      $\frac{-24}{25}$      $\frac{-22}{40}$   
 4457    4457    4458    4423

301

$\frac{+02}{3}$      $\frac{+02}{17}$      $\frac{+02}{20}$      $\frac{-32}{30}$   
 4464    4464    4437    4436

300

$\frac{+02}{2}$      $\frac{+05}{16}$      $\frac{+02}{22}$      $\frac{-25}{28}$      $\frac{-26}{80}$   
 4476    4476    4477    4411

299

$\frac{00}{00}$      $\frac{+02}{14}$      $\frac{+02}{19}$      $\frac{-22}{27}$      $\frac{-33}{45}$   
 4478    4480    4480    4440

298

$\frac{+03}{2}$      $\frac{+05}{19}$      $\frac{+05}{19}$      $\frac{-35}{27}$   
 4476    4487    4488    4457

297

$\frac{+03}{2}$      $\frac{+04}{16}$      $\frac{+05}{19}$      $\frac{-26}{32}$   
 Rd.    Rd.

296



Sta.						
306	$\frac{+38^e}{50}$					442.6
307	$\frac{+37^e}{50}$					442.5
308			$\frac{+12^e}{30}$	$\frac{+2^e}{6}$	$\frac{-0^e}{4}$	441.7
309	$\frac{+35^e}{50}$		$\frac{+4^e}{34}$			441.6
310			$\frac{+14^e}{41}$	$\frac{-0^e}{16}$		440.7
311			$\frac{+16^e}{43}$	$\frac{+6^e}{4}$	$\frac{-0^e}{3}$	439.4
312			$\frac{+16^e}{35}$	$\frac{+9^e}{10}$	$\frac{0^e}{5}$	439.2
313	$\frac{+27^e}{59}$	$\frac{+10}{34}$	$\frac{+4^e}{32}$	$\frac{+4^e}{27}$	$\frac{+4^e}{15}$	435.3
335.2	$\frac{+4^e}{41}$	$\frac{+4^e}{37}$	$\frac{+5^e}{26}$	$\frac{+5^e}{22}$	$\frac{+0^e}{23}$	434.8
						440.0
						434.9
						440.0
						440.0
						439.4
						449.5
						444.3



370,

+35.2

313

312

311

310

309

308

307

306,

439.2    439.7    439.9    435.8  
 $\frac{+0.2}{3}$      $\frac{+0.2}{12}$      $\frac{+0.4}{18}$      $\frac{-3.2}{26}$

440.0    439.9    440.1    435.9    436.0  
 $\frac{+0.6}{6}$      $\frac{+0.5}{15}$      $\frac{+0.2}{18}$      $\frac{-3.5}{31}$      $\frac{-3.4}{50}$

440.8    440.3    440.3    438.9    437.6  
 $\frac{+0.1}{7}$      $\frac{-0.4}{22}$      $\frac{-0.4}{22}$      $\frac{-0.3}{27}$      $\frac{-3.1}{50}$

441.8    441.5    441.3    438.6    438.6  
 $\frac{+0.2}{3}$      $\frac{-0.1}{20}$      $\frac{-0.2}{24}$      $\frac{-3.0}{37}$      $\frac{-3.0}{50}$

441.4    441.9    442.0    438.5    438.4  
 $\frac{+0.3}{3}$      $\frac{+0.3}{16}$      $\frac{+0.3}{18}$      $\frac{-3.2}{39}$      $\frac{-3.2}{50}$

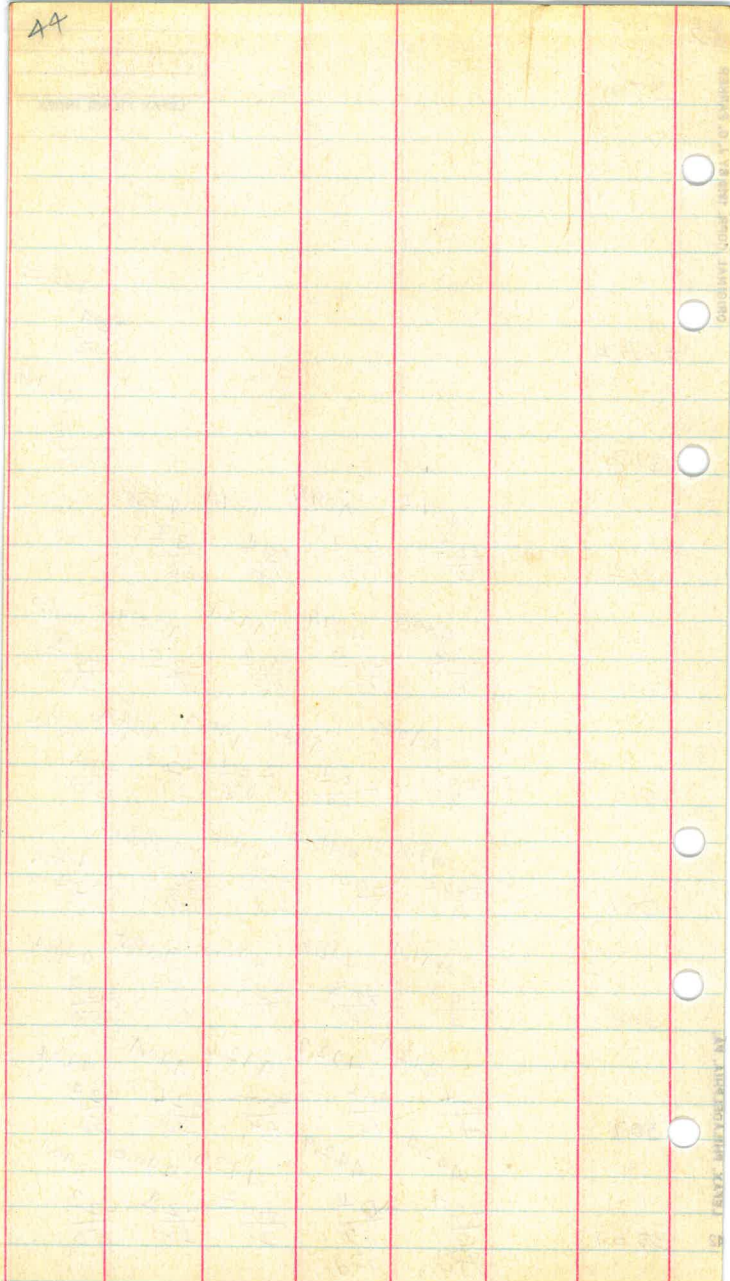
442.4    442.7    442.6    440.4    440.1  
 $\frac{-0.4}{4}$      $\frac{+0.2}{18}$      $\frac{+0.1}{22}$      $\frac{-2.1}{30}$      $\frac{-2.4}{50}$

442.4    442.9    443.0    440.0    440.1  
 $\frac{+0.4}{3}$      $\frac{+0.1}{17}$      $\frac{+0.2}{21}$      $\frac{-2.4}{28}$      $\frac{-2.2}{50}$   
 Ad,    Ad

435.2  
 $\frac{+0.4}{50}$

434.9  
 $\frac{-0.4}{50}$

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W. F. BAYZ, BUREAU, CHIT. NY.

Sta	Elev	Grade	cut	Area	Sum of areas	Length	EAG	say HP HP	Dg HP SR	SR
9+338	571.2	566.0	5.2	27.6	45.3	214	180.0			
11+48	571.8	568.2	3.6	17.7	24.7	98	44.8			
12+46	574.5	573.0	1.5	7.0	17.0	103	32.4			
13+49A	577.2	575.0	2.2	10.0	22.2	72	29.5			
14+21.7	575.8	573.2	2.6	12.2	35.3	28	18.3			
14+49.7	576.5	572.0	4.5	23.1	35.8	47	31.1			
14+97	570.2	567.5	2.7	12.7	28.1	48	24.9			
15+45	569.2	566.0	3.2	15.4						



Sta	Elev	Grade	Gut	Area	Sum of Areas	Length	EtG	CY. H.P.	S.R. →
15+45	569.2	566.0	3.2	15.4	26.4	103	50.3	✓	
16+48	565.4	563.0	2.4	11.0	53.5	201	199.0	✓	
18+49	566.3	559.0	7.3	42.5	72.9	32	43.2	✓	
18+81	563.8	558.2	5.6	30.4	62.0	67	76.9	✓	
19+48	564.8	559.0	5.8	31.6	104.0	56	107.8	✓	
20+04	571.8	561.0	10.8	72.4	124.2	48	110.4	✓	
20+52	571.5	563.0	8.5	51.8	80.8	43	64.3	✓	
20+99.9	569.4	564.0	5.4	29.0					



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Sta	Elev	Grade	cut	Area	sum of areas	Length	< E&G	cut H.P.	DG HP	SR
20+94.9	569.4	564.0	5.4	29.0	65.7	55	66.8	✓		
21+50	570.5	564.0	6.5	36.7	56.7	98	102.9	✓		
22+48	570.0	566.0	4.0	20.0	58.9	95	103.6	✓		
23+43	584.8	578.0	6.8	38.9	65.8	101	123.1	✓		
24+44	589.1	584.0	5.1	26.9	38.5	28	20.0			
24+71.6	587.5	585.0	2.5	11.6	64.3	120	142.9	✓		
25+92	596.6	588.0	8.6	52.7	107.2	54	107.2	✓		
26+46	596.0	587.2	8.8	54.5				✓		

E. Capriani  
 Pipe Line  
 Grades & Yardage  
 H.C.M. (2)  
 LEFAX FILING INDEX

Sta	Elev	Gra.	Cut	Area	Sum of Areas	Length	ETG	Earth	H.R. Dg.	S.R.
26+46	596.0	587.2	8.8	54.5	85.5	91	144.1			
27+37	590.0	584.3	5.7	31.0	51.0	34	32.1			
27+72	586.0	582.0	4.0	20.0	49.0	24	21.8			
27+95	585.7	580.3	5.4	29.0	65.0	105.0	126.3			
29+00	572.4	566.0	6.4	36.0 25.6	46.8	47				40.8 ✓
29+47	566.3	561.0	5.3	21.2	45.2	53.0				44.4 ✓
30+00	562.0	556.0	6.0	24.0 33.0	62.7	50.0	57.9			85.2 ✓
30+50	560.5	555.0	5.5	29.7						

2003.7

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Sta	Elev	Grade	cut	Area	Sum of Areas	Length	← FAG	City HP.E.	SR
30+50	560.5	555.0	5.5	29.7	49.7	100.0	92.0 ✓	HP.E. ✓	SR ✓
31+50	560.0	556.0	4.0	20.0	40.0	100.0	74.1 ✓	HP.E. ✓	SR ✓
32+50	564.0	560.0	4.0	20.0	40.0	250.0	185.0 ✓	HP.E. ✓	SR ✓
35+00	554.0	550.0	4.0	20.0	35.2	125.0	81.5 ✓	HP.E. ✓	SR ✓
* 36+25	551.2	547.4	3.8	15.2 18.8	34.0	125.0	490.5 ✓	HP.E. ✓	SR ✓
37+50	553.5	547.4	6.1	24.4	40.4	100.0	78.7 ✓	HP.E. ✓	SR ✓
38+50	552.0	548.0	4.0	16.0	51.2	100.0	74.7 ✓	HP.E. ✓	SR ✓
39+50	560.8	552.0	8.8	35.2	51.2	100.0	94.7 ✓	HP.E. ✓	SR ✓

El Capitan  
Pipe Line  
Grades & Yardage  
H.C.M. (3)  
LEFAX FILING INDEX



Sta.	Elev.	Grade	Cut	Area	Sum of Areas	Length	E+G	Earth	DG	HP	SR
39+50	560.8	552.0	8.8	35.2	52.8	50.0	558.0		40.9	48.9	
40+00	554.4	550.0	4.4	17.6	17.6	35.0			11.4	11.4	
40+35	549.2	549.2	0.0	0.0	0.0						
40+80	548.4	548.4	0.0	0.0	0.0						
41+00	550.5	548.0	2.5	10.0	10.0	20.0			3.7	3.7	
41+50	550.2	547.0	3.2	12.8	22.8	50.0			2.1	2.1	
42+50	551.6	546.0	5.6	22.4	35.2	100.0			65.2	65.2	
43+50	549.5	544.0	5.5	22.0	44.4	100.0			82.2	82.2	
					44.4						480.6



Sta	Elev	Grade	Cut	Area	Sum of Areas	Length	ETG	Eath	DG HP	SR
43+50	549.5	544.0	5.5	29.7	61.3	100.0	114.0	✓	57.1	✓
44+50	547.8	542.0	5.8	31.6	50.4	100.0	93.3	✓		
45+50	542.0	538.2	3.8	18.8	51.8	100.0	95.9	✓		
46+50	540.6	534.6	6.0	33.0	60.6	100.0	112.2	✓		
47+50	536.2	531.0	5.2	27.6	49.5	100.0	91.7	✓		
48+50	535.0	530.7	4.3	21.9	63.7	150.0	176.9	✓		
50+00	537.6	530.4	7.2	41.8	83.6	50.0	77.4	✓		
50+50	537.6	530.4	7.2	41.8						

E.I. Capitani  
 Pipeline  
 Grades & Yardage  
 ④  
 LEFAX FILING INDEX

374.01

Sta	Elev.	Grade	Cut	Area	Sum of Areas	Length	EtG	Earth	DG HP	SR
50+50	537.6	530.4	7.2	41.8	101.6	50.0	94.1	✓	59.1	✓
51+00	539.6	530.2	9.4	59.8	95.8	150.0	266.1	✓		
52+50	536.4	530.0	6.4	36.0	69.0	150.0	191.6	✓		
54+00	536.0	530.0	6.0	33.0	74.8	150.0	207.7	✓		
55+50	537.5	530.3	7.2	41.8	65.5	100.0	121.3	✓		
56+50	535.0	530.4	4.6	23.7	47.9	200.0	175.6	✓		
58+50	535.2	530.6	4.6	23.7	37.0	100.0	68.5	✓		
59+50	533.8	531.0	2.8	13.3				✓		

Sta	E1	Grd	Cut	Area	sum of Areas	Length	E & G	Earth	DG HP	SR
59+50	533.8	531.0	2.8	13.3	36.4	50.0	42.6	33.7	53	SR
60+00	539.5	535.0	4.5	23.1	60.5	50.0	56.0	✓	53	SR
+50	544.6	538.0	6.6	37.4	63.6	50.0	58.9	✓	53	SR
61	547.0	537.0	5.0	26.2	51.2	150.0	142.2	✓	53	SR
62+50	532.8	528.0	4.8	25.0	55.4	100.0	102.6	✓	53	SR
63+50	531.6	526.0	5.6	30.4	44.7	100.0	82.8	✓	53	SR
64+50	527.0	529.0	3.0	14.3	32.0	50.0	29.6	✓	53	SR
65	534.4	530.8	3.6	17.7	32.0	50.0	29.6	✓	53	SR



Sta	Elev	Grade	Cut	Area	Sum of Areas	Length	E & G	Eqth	DG HP	SR
65+	534.4	530.8	3.6	17.7	43.9	100.0	411.1	81.3	58.1	
66	534.0	534.0	5.0	26.2	36.2	150.0	100.6			
67	538.8	536.6	2.2	10.0	10.0	30.0	5.6			
67+80	537.0	537.0	0.0	0.0						
			Frettle -							
68	536.4	536.4	0.0	0.0						
69	547.4	540.0	7.4	43.3	43.3	90.0	72.2			
70+	547.8	540.2	7.6	44.9	88.2	50.0	81.7			
							512.2	321.7		



Sta	Elev	Grade	Cut	Area	Sum of Areas	Length	EBG	Earth	DG-HP	SR
70+	547.8	540.7	7.6	44.9	64.9	100.0	120.1			
71+	545.0	541.0	4.0	20.0	38.8	150.0	107.8			
72+	547.8	544.0	3.8	18.8	38.8	250.0	179.9			
75+	540.0	536.0	4.0	20.0	34.4	100.0	314.3			63.7
76+	534.6	530.0	4.6	18.4	55.3	100.0	102.8			63.7
77+	528.8	523.0	5.8	31.6	51.6	100.0	95.6			
78+	527.6	523.6	4.0	20.0			1419.1			63.7

Sta	Elev	Grade	Cut	Sum of Area	Sum of Areas	Length	EIG	Earth	DG	HP	SR
78+	527.6	523.6	4.0	20.0	43.7	100.0	1419.7 ✓ 80.9 ✓		64.7 ✓		63.7
79+	531.6	527.0	4.6	23.7	46.2	150.0	128.3 ✓				
80+50	533.4	528.0	4.4	22.5	51.5	250.0	238.0 ✓ 645.6				
82+00	525.4	520.0	5.4	29.0 21.6	40.0	160.0			111.1 ✓		118.1
84+60	534.6	530.0	4.6	18.4 20.5	48.1	100.0	55.0 ✓		89.2		118.1
85+60	537.0	531.0	6.0	27.6	90.0	40.0	60.7 ✓		66.7		
86+	544.0	532.0	12.0	62.4			652.5 ✓ 753.8				

CRENSHAW COUNTY ROAD DEPT. OF TRANSPORTATION

Sta	Elev	Grade	Cut	Area	Sum of Areas	Length	ELS	Earth DG	HP	SR
86+	574.0	537.0	12.0	62.4	79.8	60.0	622.52	87.9	75.0	
+60	537.0	533.7	3.8	16.6	47.6	140.0	145.1	123.9		
88+	579.6	573.0	6.6	31.0	60.8	200.0	277.0	225.0	597.1	181.8
90+	560.0	573.6	6.4	29.8	53.3	50.0	146.0	49.5		
90+50	560.4	555.2	5.2	23.5	23.5	55.0	53.1	23.9		
91+05	556.2	556.2	0.0	0.0	23.5	55.0	21.2			
92+03	558.7	558.7	0.0	0.0	31.5	47.0	23.3	27.5	750.0	
92+50	566.6	559.9	6.7	31.5			672.2			

7641.4



Sta	Elev	Grade	Cut	Area	Sum	Length	ESG	Earth	HP Dg	SR
92+50	566.6	559.9	6.7	31.5	31.5	100.0	61.1	58.3	73.3	✓
93+50	558.6	558.6	0.0	0.0	41.8	100.0	4	77.4	✓	✓
94+50	564.4	555.8	8.6	41.8	62.3	85.0		98.3	✓	✓
95+35	549.0	544.4	4.6	20.5	36.1	150.0		100.6	✓	✓
96+85	536.0	532.4	3.6	15.6	30.4	65.0		1028.2	6	36.5
97+50	536.0	532.0	4.0	16.0	40.8	50.0		114.1	✓	37.8
98+00	534.6	528.4	6.2	24.8						



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El Capitán  
Pipe Line  
Grades & Yardage  
H.C.M. - 8 -  
LEFAX FILING INDEX

Sta	Elev	Grade	Cut	Area	Sum	Length	ERG	Earth	DG	HP	SR
98+00	534.6	528.4	6.2	24.8	34.4	135.0	6.2		114.1	37.8	86.0
X 99+35	527.0	524.6	2.4	9.6 11.0	13.0	165.0	15.6		18.7	17.8	160.9
100+00	525.0	524.6	0.4	2.0	19.7	60.0	21.5		65.1	25.5	
100+60	528.0	524.4	3.6	17.7	40.2	115.0	85.5				
101+75	528.0	523.6	4.4	22.5	59.9	25.0	27.6				
X 102+00	530.4	523.8	6.6	37.4	52.8	175.0	171.1				
103+75	526.4	523.2	3.2	15.4	29.7	165.0	90.8				
105+40	525.8	522.8	3.0	14.3							

Sta	Elev.	Grade	Cut	Area	Sum	Length	EtG	Earth	D&HP	SR
105+40	525.8	522.8	3.0	14.3	65.3	120.0	145.1		134.1	
106+60	529.8	521.4	8.4	51.0	80.0	115.0	170.1			
107+75	521.4	516.0	5.4	29.0	57.3	275.0	292.5			
X 110+50	515.4	510.1	5.3	28.3 21.2	25.2	100.0	8'6101		46.7	46.7
111+50	521.0	520.0	1.0	4.0	12.0	150.0			33.4	33.4
113+00	568.0	566.0	2.0	8.0	46.4	25.0			21.5	21.5
113+25	575.6	566.0	9.6	38.4					166.7	

Sta	Elev.	Grade	Cut	Area	Sum	Length	E+G	Earth	DG HP	SR
113+25	575.6	566.0	9.6	38.4	47.2	75.0	750.0	1667.5	1667.5	65.5
X 114+00	542.2	540.0	2.2	8.8	22.7	65.0	17.4	17.4	17.4	1291
114+65	516.2	513.5	2.7	12.8	29.3	85.0	23.1	46.1	46.1	
115+50	510.4	507.0	3.4	16.6	39.1	450.0	325.8	325.8	325.8	600
120+00	508.4	504.0	4.4	22.5	46.2	400.0	342.2	342.2	342.2	
124+00	507.6	503.0	4.6	23.7	61.1	300.0	339.1	339.1	339.1	
127+00	505.6	499.0	6.6	37.4	77.7	300.0	431.7	431.7	431.7	
130+00	505.0	498.0	7.0	40.3	876.1	1113.8	1113.8	1113.8	1113.8	

11827

600



Sta	Elev.	Grade	Cut	Area	Sum	Length	E+G	Earth Dg-HP	SR
130+00	505.0	498.0	7.0	40.3	77.7	400.0	575.6	575.6	✓
134+00	502.6	496.0	6.6	37.4	74.8	183.7	259.0	259.0	✓
135+83.7	502.4954	495.4	6.6	37.4	50.8	200.0	188.1	188.1	✓
<del>137+00</del>	<del>502.0</del>	<del>496.7</del>	<del>5.3</del>	<del>28.3</del>	<del>45.0</del>	<del>100.0</del>	<del>123.5</del>	<del>83.2</del>	<del>✓</del>
139+00	501.6	497.2	4.4	22.5	66.6	100.0	123.5	83.2	✓
140+00	502.0	497.6	4.4	22.5	73.1	100.0	135.9	135.9	✓
141+00	505.5	499.0	7.5	44.1					
142+00	505.4	500.0	5.4	29.0					



Stg	Elev.	Grade	Cut	Area	Sum	Length	Estg	Earth	DG HP	SR
135+83.7	502.0	495.4	6.6	37.4	82.3	286.3		437.0		
138+70	502.0	494.4	7.6	44.9	44.9	20.0		16.6		
138+90	494.4	494.4	0.0	0.0		5.0				
138+95	494.4	494.4	0.0	0.0						
139+15	502.0	494.2	7.8	46.5	46.5	20.0		17.2		
144+00	500.0	492.6	7.4	43.3	89.8	485.0		807.5		
144+25	497.4	492.6	4.8	25.0	68.3	25.0		31.6		
141+00	497.8	492.0	5.8	31.6	56.6	125.0		131.1		

146+00 497.8 492.0 5.8 31.6

~~148+00~~ 496.0 491.8 4.2 21.3

148+30 499.0 491.6 7.4 43.3

150+00 498.0 491.5 6.5 36.7

168+00 490.4 485.0 5.4 29.0

168+56 495.6 485.0 10.6 70.5

=173+45

52.9 200.0

64.6 50.0

80.0 150.0

65.7 1800.0

99.5 56.0

196.0

59.9

222.2

2190.0

103.0

3862.0

2293.0

mmA3.0

4212.1

El Capitan  
Pipe Line  
Grades - Yardage  
H.C.M. - 10 -  
LEFAX FILING INDEX

Sta	Elev.	Grade	Cut	Area	Sum	Length	ETG	Earth	DG HP	SR
142+00	505.4	500.0	5.4	29.0	49.0	200.0	181.5	181.5		
144+00	505.0	501.0	4.0	20.0	43.1	200.0	159.6	159.6		
146+00	501.5	497.0	4.5	23.1	48.7	150.0	135.3	135.3		
147+50	501.3	496.4	4.9	25.6	60.1	150.0	166.9	166.9		
149+00	502.4	496.2	6.2	34.5	60.7	100.0	112.4	112.4		
150+00	501.0	496.0	5.0	26.2	72.7	115.0	154.8	154.8		
151+15	503.4	495.6	7.8	46.5	66.5	185.0	227.8	227.8		
153+00	499.0	495.0	4.0	20.0						

132.81, 14

185.33



Sta	Elev	Grade	Cut	Area	Sum	Length	E+G	Earth	DG HP	SR
153+00	499.0	495.0	4.0	20.0	80.7	300.0	448.3	448.3	1850.2	
156+00	504.0	494.5	9.5	60.7	89.7	150.0	249.2	249.2		
157+50	500.0	494.6	5.4	29.0	77.7	150.0	215.8	215.8		
159+00	502.5	494.4	8.1	48.7	84.7	200.0	313.7	313.7		
161+00	500.4	494.0	6.4	36.0	61.6	300.0	342.2	342.2		
164+00	496.5	491.6	4.9	25.6	92.4	125.0	213.9	213.9		
165+25	501.0	490.8	10.2	66.8						



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El Capitan  
Pipe Line  
Grades - Yardage  
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LEFAX FILING INDEX

Sta	Elev. Grade	Cut	Area	Sum. Length	Est. Gr	Eqth	DG HP SR
165+25 (Equation)	501.0	490.8	10.2	66.8	91.8	175.0	297.5
167+00	495.0	490.2	4.8	25.0	61.0	300.0	338.9
172+00	500.4	494.0	6.4	36.0	59.1	100.0	109.4
173+45	495.6	485.0	10.6	70.5	103.5	255.0	496.0
176+00	493.0	487.0	6.0	33.0	69.7	100.0	129.0
177+00	492.5	486.0	6.5	36.7	62.9	150.0	174.7
178+50	490.0	485.0	5.0	26.2			

Sta	Elev	Grade	Cut	Area	Sum	Length	EtG	Earth	DG. HP	SR
178+50	490.0	485.0	5.0	26.2	59.2	150.0	164.4	164.4		<del>964</del>
180+00	490.0	484.0	6.0	33.0	63.4	200.0	234.1	234.9		
182+00	486.6	481.0	5.6	30.4	67.1	300.0	372.3	372.8		
185+00	488.0	481.5	6.5	36.7	60.4	200.0	223.7	223.7		
187+00	486.6	482.0	4.6	23.7	49.9	300.0	277.2	277.2		
190+00	493.0	488.0	5.0	26.2	55.2	600.0	613.3	613.3		
196+00	484.4	479.0	5.4	29.0						

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Sta	Elev. Grade	Cut	Area	Sum	Length	E+G	Earth	DG HP	SR
196+00	484.4	479.0	5.4	29.0	56.6	100.0	104.8	✓	
197+00	484.0	478.8	5.2	27.6	104.0	200.0	385.2	✓	
199+00	489.8	478.6	11.2	76.4	110.9	200.0	410.7	✓	
201+00	484.8	478.6	6.2	34.5	79.4	200.0	294.1	✓	
203+00	486.2	478.6	7.6	44.9	75.3	200.0	278.9	✓	
205+00	484.1	478.5	5.6	30.4	99.1	200.0	367.0	✓	
207+00	488.4	478.0	10.4	68.7					

E-I Captain  
 Pipe Line  
 Grades - Yardage  
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 LEFAX FILING INDEX



Sta	Elev.	Grade	Cut	Area	Sum	Length	E+G	Earth	DG-HP	SR
207+00	488.4	478.0	10.4	68.7	141.1	75.0	196.0	196.0	✓	
207+75	488.0	477.2	10.8	72.4	102.8	125.0	238.0	238.0	✓	
209+00	481.6	476.0	5.6	30.4	55.4	100.0	102.6	102.6	✓	
210+00	479.8	475.0	4.8	25.0	69.9	300.0	388.3	388.3	✓	
213+00	482.0	474.4	7.6	44.9	73.9	400.0	547.4	547.4	✓	
217+00	479.4	474.0	5.4	29.0	66.4	300.0	368.9	368.9	✓	
220+00	478.6	472.0	6.6	37.4						

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Sta	Elev.	Grade	Cut	Area	Sum	Length	E+G	Earth	DG-HP	SR
220+00	478.6	472.0	6.6	37.4	70.4	550.0	717.0	717.0		
225+50	475.0	469.0	6.0	33.0	82.5	25.0	33.2	38.2		
225+75	478.6	470.4	8.2	49.5	75.7	75.0	105.1	105.1		
226+50	480.0	475.0	5.0	26.2	104.5	100.0	193.5	193.5		
227+50	490.4	479.0	11.4	78.3	156.6	50.0	145.0	145.0		
228+00	491.4	480.0	11.4	78.3	132.8	50.0	113.0	123.0		
228+50	489.0	480.2	8.8	54.5						

E I Capital  
 Pipe Line  
 Grades - Yardage  
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 LEFAX FILING INDEX

Sta	Elev.	Grade	Cut	Area	Sum	Length	EtG	Earth	DG-HP	SR
228+50	489.0	480.2	8.8	54.5	89.0	200.0	329.7	329.7	✓	
230+50	487.2	481.0	6.2	34.5	99.5	100.0	124.3	184.3	✓	
231+50	498.0	488.0	10.0	65.0	95.4	200.0	353.1	353.3	✓	
233+50	489.6	484.0	5.6	30.4	60.8	350.0	394.1	394.1	✓	
237+00	483.6	478.0	5.6	30.4	63.4	100.0	117.4	117.4	✓	
238+00	483.0	477.0	6.0	33.0	66.0	200.0	244.4	244.4	✓	
240+00	476.0	470.0	6.0	33.0						

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Sta	Elev.	Grade	Cut	Area	Sum	Length	ETG	Earth	DG-HP	S.T.R.
240+00	476.0	470.0	6.0	33.0	66.0	200.0	244.4	244.4	✓	
242+00	468.0	462.0	6.0	33.0	69.0	300.0	333.3	383.3	✓	
245+00	464.4	458.0	6.4	36.0	90.5	200.0	335.2	335.2	✓	
247+00	466.0	457.2	8.8	54.5	91.9	150.0	255.3	255.3	✓	
248+50	463.2	456.6	6.6	37.4	65.0	150.0	130.6	180.6	✓	
250+00	461.2	456.0	5.2	27.6	65.0	525.0	631.9	631.9	✓	
255+25	462.2	455.6	6.6	37.4						

E.I. Capitan  
 Pipe Line  
 Grades-Yardage  
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 LEFAX FILING INDEX



Sta	Elev.	Grade	Cut	Area	Sum	Length	EQ	Earth	DG+HP	SR
255+25	462.2	455.6	6.6	37.4	106.1	100.0	196.5	196.5		
256+25	466.0	455.6	10.4	68.7	124.9	75.0	173.2	173.2		
257+00	464.4	455.4	9.0	56.2	102.7	300.0	570.5	570.5		
260+00	460.9	453.1	7.8	46.5 31.2	60.8	300.0	560.7	560.7		337.8
265+00	460.4	453.0	7.4	29.6	53.6	100.0	92.6	92.6		992.6
266+00	458.4	452.4	6.0	24.0	48.8	400.0	566.4	566.4		361.5
270+00	457.2	451.0	6.2	24.8	51.2	250.0	237.0	237.0		237.0
272+50	455.0	448.4	6.6	26.4						1928.9

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ORIGINAL COPY, 1910 BY J. C. PARKER

ET Captain  
Pipe Line  
Grades - Yardage  
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LEFAX FILING INDEX

Sta	Elev	Grade	ECut	Area	Sum	Length	E+G	Earth	DG-H.P.	STR
272+50	455.0	448.4	6.6	37.4	71.9	150.0	162.2	199.0		
274+00	453.2	447.0	6.2	34.5	79.4	200.0	214.1	294.1		
276+00	454.0	446.4	7.6	44.9	82.3	135.0	123.1	206.5		
277+35	453.0	446.4	6.6	37.4 26.4	66.4	165.0	120.0	9'669	200	79.8
278+00	456.0	446.0	10.0	40.0	65.6	75.0			91.1	91.1
278+75	452.4	446.0	6.4	25.6	56.0	125.0			123.6	129.6
280+00	453.6	446.0	7.6	30.4	59.2	200.0			119.3	219.3
282+00	453.0	445.8	7.2	28.8						

Sta	Elev.	Grade	Cut	Area	Sum Length	E+G	Earth	DG-HP	S R
282+00	453.0	445.8	7.2	28.8	68.4	100.0		126.7	126.7
283+00	455.6	445.7	9.9	39.6	82.8	100.0		153.5	153.5
284+00	456.4	445.6	10.8	43.2	144.8	100.0	268.1	268.1	268.1
285+00	456.4	445.6	10.8	43.2	76.8	300.0		426.0	426.0
288+00	453.0	444.6	8.4	33.6	68.0	100.0		125.9	125.9
289+00	453.0	444.4	8.6	34.4	60.0	100.0		111.1	111.1
290+00	448.8	442.4	6.4	25.6	44.0	300.0		244.4	244.4
293+00	446.6	442.0	4.6	18.4					

LEFAX, PHILADELPHIA, PA.

ORIGINAL COPY. 1816 BY J. G. PARKER

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Sta	Elev.	Grade	Cut	Area	Sum Length	ETG	Eqth	DG-HP	SR
293+00	446.6	442.0	4.6	18.4	47.2	100.0		87.4	87.4
294+00	<sup>R</sup> 448.8	441.6	7.2	<del>28.8</del> 41.8	91.3	100.0	169.1	63.2	994.8
295+00	449.7	441.5	8.2	49.5	88.4	100.0	163.7	63.2	
296+00	447.8	441.0	6.8	38.9	74.9	200.0	277.4		
298+00	<sup>HP</sup> 446.8	440.4	6.4	<del>36.0</del> 25.6	45.6	200.0	201.1	168.9	3778.6
300+00	445.0	440.0	5.0	20.0	42.4	50.0		39.2	2081
300+50	<sup>R</sup> 445.2	439.6	5.6	<del>22.4</del> 30.4	63.4	150.0	176.1		
302+00	444.4	438.4	6.0	33.0					

El Capitan  
 Pipe Line  
 Grades - Yardage  
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 LEFAX FILING INDEX



Sta	Elev	Grade	Cut	Area	Sum	Length	EtG	Earth	DG-HP	SR
302+00	444.4	438.4	6.0	33.0	56.7	200.0		219.0		
304+00	441.2	436.6	4.6 <sup>EA</sup> 4.6 <sup>RV</sup>	23.7 18.4	45.6	100.0		386.1		84.4
305+00	442.8	436.0	6.8	27.2	52.8	300.0				293.3
308+00	441.2	434.8	6.4	35.6 36.0	76.3	100.0		141.3		372.7
309+00	441.4	434.4	7.0	40.3	69.3	225.0		288.8		
311+25	438.8	433.4	5.4	29.0	73.9	275.0		376.3		
314+00	440.0	432.4	7.6	44.9	83.8	75.0		116.4		
314+75	438.8	432.0	6.8	38.9						



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ORIGINAL COPR. 1910 BY J. G. PARKER

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Sta	Elev	Grade	Cut	Area	Sum	Length	EtG	Earth	DG-HP	SR
314+75	438.8	432.0	6.8	38.9	66.5	50.0		61.6		
315+25	437.2	432.0	5.2	27.6	63.6	225.0		265.0		
317+50	337.6	331.2	6.4	36.0	69.0	650.0		830.6		
324+00	436.0	430.0	6.0	33.0	62.0	100.0		114.8		
325+00	435.0	429.6	5.4	29.0	60.6	250.0		280.5		
327+50	434.8	429.0	5.8	31.6	59.2	100.0		109.6		
328+50	435.2	430.0	5.2	27.6	63.6	150.0		176.6		
330+00	437.6	431.2	6.4	36.0						

545  
2450

El. C. BITAN  
Pipe Line  
Grades - Yardage  
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LEFAX FILING INDEX

Sta	Elev	Grade	Cut	Area	Sum	Length	ETG	Earth	DG-HP	SIR
330+00	437.6	431.2	6.4	36.0	77.8	275.0		396.2		
332+75	439.6	432.4	7.2	41.8	98.0	100.0		181.5		
333+75	442.6	433.6	9.0	56.2	89.2	125.0		206.5		
335+00	441.0	435.0	6.0	33.0	59.2	300.0		328.8		
338+00	448.4	443.4	5.0	26.2	62.2	100.0		115.2		
339+00	453.4	447.0	6.4	36.0	62.2	350.0		403.1		
342+50	469.4	464.4	5.0	26.2	63.6	250.0		294.9		
345+00	482.4	475.8	6.6	37.4						

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Sta	Elev	Grade	Cut	Area	Sum Length	E+G	Earth	HP-DG	SR
345+00	482.4	475.8	6.6	37.4	83.9	75.0	116.5		
345+75	482.0	474.2	7.8	46.5	83.9	75.0	116.5		
346+50	478.2	471.6	6.6	37.4	73.4	350.0	475.7		
350+00	466.4	460.0	6.4	36.0	73.4	275.0	373.8		
352+75	462.2	455.6	6.6	37.4	63.6	125.0	147.2		
354+00	458.6	453.6	5.0	26.2	59.2	100.0	109.7		
355+00	458.0	452.0	6.0	33.0	62.0	350.0	401.8		
358+50	460.0	454.6	5.4	29.0					

ESCAPIAN  
 Pipe Line  
 Grades + Yardage  
 H.C.M. -18-  
 LEFAX FILING INDEX



Sta	Elev	Grade	Cut	Area	Sum	Length	E + G	Earth	DG-HP	S.R.
358+50	460.0	454.6	5.4	29.0	69.3	150.0		192.5		3859.4
360+00	462.8	455.8	7.0	40.3	88.3	85.0		139.0		
360+85	462.8	454.8	8.0	48.0	89.8	115.0		191.2		
362+00	460.0	452.8	7.2	41.8	80.7	575.0		859.3		
367+75	450.8	444.0	6.8	38.9	80.7	125.0		186.8		
369+00	450.0	442.8	7.2	41.8	83.6	50.0		77.4		
369+50	449.2	442.0	7.2	41.8	88.3	100.0		163.5		
370+50	448.6	440.8	7.8	46.5						



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ORIGINAL COPR. 1919 BY J. O. PARKER

El Capitan  
Pipeline  
Grades-Yardage  
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Sta	Elev	Grade	Cut	Area	Sum	Length	E+G	Earth	DG-HP	SR
370+50	448.6	440.8	7.8	46.5	126.7	100.0		234.6		
371+50	450.8	439.2	11.6	80.2	162.3	50.0		150.3		
372+00 E↑ EGR↓	450.4	438.6	11.8	82.1	158.5	50.0	146.8	0623.0 00		
372+50	449.2	438.0	11.2	76.4	110.9	100.0	205.3			
373+50	441.0	434.8	6.2	34.5	67.5	100.0	125.0			
374+50 E↑ E↓	437.8	431.8	6.0	33.0	84.0	200.0	311.0 471	311.1		
376+50	436.4	428.0	8.4	51.0	85.5	100.0	153	158.3		
377+50	432.2	426.0	6.2	34.5						

Sta	Elev.	Grade	Cut	Area	Sum Length	E+G	Earth	HP-DG	SR
377+50	432.2	422.6	6.2	34.5	8.0	100.0	150.0		
378+50	422.4	421.6	7.8	46.5	79.5	300.0	441.7		
381+50	415.0	409.0	6.0	33.0	71.9	150.0	199.7		
383+00	413.6	406.8	6.8	38.9	71.9	300.0	399.4		
386+00	409.0	403.0	6.0	33.0	66.0	100.0	122.2		
387+00	408.0	402.0	6.0	33.0	77.9	150.0	216.4		
388+50	408.4	400.8	7.6	44.9	69.9	150.0	194.2		
390+00	404.8	400.0	4.8	25.0					
<div style="position: absolute; top: 50%; left: 50%; transform: translate(-50%, -50%); opacity: 0.5; font-size: 2em;">           21            22            23            24            25            26            27            28            29            30            31            32            33            34            35            36            37            38            39            40            41            42            43            44            45            46            47            48            49            50            51            52            53            54            55            56            57            58            59            60            61            62            63            64            65            66            67            68            69            70            71            72            73            74            75            76            77            78            79            80            81            82            83            84            85            86            87            88            89            90            91            92            93            94            95            96            97            98            99            100         </div>									

390+00	404.8	400.0	4.8	25.0	55.4	250	286.2 ✓
392+00	403.6	398.0	5.6	30.4	66.4	250	307.0 ✓
395	418.4	412.0	6.4	36.0	66.4	300	360.0 ✓
398	426.6	421.0	5.6	30.4	63.4	350	411.0 ✓
401+50	432.0	426.0	6.0	33.0	90.4	250	477.0 ✓
409	418.6	412.0	6.6	37.4	77.1	250	460.0 ✓
411+50	416.0	409.0	7.0	40.0	126.2	150	351.0 ✓
413	419.2	407.0	12.2	86.0			

4400



Stk	Fl.	Grid.	Cut	L	E
A13	A19.2	4070	12.2	186.0	276.0 ✓
A14	A19.2	4056	13.6	179.0	277.0 ✓
A15	416.0	4046	11.4	104.5	290.0 ✓
A16+10	407.6	4076	5.0	68.6	117.7 ✓
417+10	408.0	4016	6.4	77.7	259.5 ✓
470	407.0	4000	7.0	300.0	666.4 ✓
472+10	404.4	398.4	6.0	73.2	276.0 ✓
472+10	406.0	398.2	7.8	79.5	14.7 ✓

XX No 41

427	405.0	395.2	9.8	63.5	110.0	455	916.0
42725	402.0	395.0	7.0	40.7	108.6	25	67.2
42750	404.2	395.0	9.2	58.0	96.3	15	21.4
42790	403.0	394.8	8.2	44.5	107.5	40	20.6
42810	400.4	394.4	6.0	33.0	87.5	20	20.5
42845	403.6	394.2	9.4	59.8	94.8	15	25.8
42890	400.4	393.6	6.8	38.9	98.9	116	21.5
=							1698.7

944

1698.7





472	380.6	375.0	5.3	30.4	10.3	21.5	201	120.0	120.0	✓
474	383.0	374.4	7.6	24.4	1.9	6.6	201	201	140.0	✓
475	380.	374.0	6.0	33.0	8.1	0.1	1.0	1.0	140.0	✓
476+70	381.0	373.0	8.0	48.0	1.4	1.8	2.5	2.5	140.0	✓
479	377.6	372.0	5.6	30.4	11.4	1.8	2.0	2.0	150.0	✓
480	380.0	371.6	8.4	51.0	10.8	0.1	2.0	2.0	150.0	✓
482	379.6	371.0	8.6	52.7	10.4	0.1	3.0	3.0	150.0	✓
485	377.4	370.2	7.2	41.8	9.4	0.6	3.0	3.0	150.0	✓

1500  
3400

El Capitán  
Pipe Line  
Grades-Yardage  
HCM -22-  
LEFAX FILING INDEX

							EG	
481	3774	370.2	7.2	41.8	94.5	400	✓ 700.0	
489	3776	369.0	8.6	52.7	100.9	350	✓ 659.0	
492AD	3760	368.0	8.0	48.0	75.6	325	✓ 45.0	
495AN	3768	371.6	5.2	27.6	71.6	275	✓ 140.8	
496AD	374	374	0.0	-	0.0	Piers		
49870	3752	375.2	0.0	-	11.0	30	✓ 28.2	
499750	3780	375.6	2.4	11.0	30.5	50	✓ 6.6	18/04.2
500	380.4	376.0	4.4	29.5	49.1	150	✓ 14.0	
501AD	384	378	6.0	37.6				

50150	374	378	60	27.6
502	3790	3770	20	28
504	3890	3764	3.6	17.6
50750	3800	3760	6.0	17.6
507	3830	3726	10.4	52.5
509	3730	3650	5.0	22.5
510	3726	3660	6.6	31.0

36.0	150	100.0	✓
4.0	100	44.4	✓
33.0	150	92.6	✓
70.0	150	104.5	✓
74.9	200	166.5	✓
53.5	100	96.6	✓

8-2686

9659  
~~100~~  
~~24.4~~





1-2  
37036

574	361.4	355.0	6.4	36.0	66.4	1400	1700	✓
578	371.4	353.8	5.6	30.4	99	200	1700	✓
580	362	353.8	8.2	44.5	101.8	200	400	✓
582	367	353.6	9.4	51.8	108.9	300	500	✓
585	360.4	353.6	6.8	35.9	115.8	200	800	✓
588	361.0	353.2	7.8	46.5	119.6	200	1000	✓
590	359	353.0	6.0	33.0	121.6	200	1100	✓
592	361.6	353	8.6	51.5	128	300	1200	✓





A8885

56740	370	36724	7.6	41.4	77.9	250	✓ 761.0
570	366	360	6.0	33.0	63.4	500	587.0
575	369.6	364	5.6	30.4	74.4	500	669.0
580	365.4	361.2	7.2	41.8	66.8	100	172.4
581	365.0	360.8	4.8	25.0	65.9	800	968.0
589	365.0	358.-	7.0	40.3	91.3	100	169.0
590	367.4	359	8.4	51.0	91.3	150	284.0
59150	368	361	7.0	40.3			

1910

25 25

Label	Value 1	Value 2	Value 3	Value 4	Value 5	Value 6	Value 7	Value 8	Value 9	Value 10	Value 11	Value 12
59110	368	196	7.0	40.2	66.5	1150	554.5	✓				
596	368	358	5.0	26.2	19.7	1100	219.0	✓				
598	362.0	306.4	6.1	33.0	10.4	1000	130.4	✓				
599	362.0	305.8	6.6	37.4	9.8	50	69.7	✓				
59110	362.	307.0	6.6	37.4	10.0	50	69.7	✓				
600	361	305	6.0	33.0	10.0	50	69.7	✓				
606	353.6	307	6.6	37.4	10.4	600	78.0	✓				
61110	351.0	307.4	8.6	52.7	90.1	550	918.0	✓				
605	346.6	339.0	5.6	20.0	80.1	350	539.0	✓				

3808

130.4  
69.7

3808

3808

615	3246	339.0	5.3	320.4
630	338.6	334.0	4.6	23.7
62450	336.4	329.0	7.4	43.3
62450	334.4	328.0	6.4	36.0
62450	328.0	328.0	10.1	65.0
650475	333.2	328.0	5.2	27.6
65	335.6	327.8	7.8	46.5
660	332.6	327	5.6	30.4

541	1500
67.0	850
79.0	1000
101.0	1000
94.6	125
74.1	425
76.9	500
200.0	

✓ 460.0  
 ✓ 1056.0  
 ✓ 1468.0  
 ✓ 187.0  
 ✓ 245.0  
 ✓ 582.0  
 ✓ 214

3740

6719  
 355.6

242 26



Sta	Elev	Grade	Cut	Area	Sum Length	ETG	Earth	HP-DG	S.R
6600	337.6	327.0	5.6	30.4	67.8	600.0	754.0		
666+00	331.0	324.4	6.6	37.4	50.7	500.0	469.9		
671+00	327.2	324.4	2.8	13.3	40.9	100.0	75.8		
672+00	327.2	322.0	5.2	27.6	59.2	350.0	384.0		
675+50	325.8	320.0	5.8	31.6	87.8	400.0	650.5		
679+50	325.0	316.0	9.0	56.2	86.6	105.0	168.6		
680+55	320.4	314.8	5.6	30.4	90.2	80.0	133.7		
681+35	325.0	315.6	9.4	59.8					

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681735	325.0	315.6	9.4	59.8	100.1	20.0	37.1
681755	323.0	316.0	7.0	40.3	76.3	245.0	346.0
684700	323.6	317.2	6.4	36.0	73.4	600.0	815.0
690700	324.6	318.0	6.6	37.4	76.3	300.0	424.0
693700	325.2	318.4	6.8	38.9	63.9	900.0	1066.0
702700	324.8	320.0	4.8	25.0	54.0	600.0	600.0
708700	320.0	314.6	5.4	29.0	63.5	300.0	353.0
711700	318.2	312.0	6.2	34.5			

EXG Earth

7874  
6

LEFAX FILING INDEX





						ETG	Earth
717+00	315.6	309.6	6.0	33.0	50.7	15.0	14.1
717+15	313.2	309.6	3.6	17.7	45.3	10.0	8.4
717+25	315.2	310.0	5.2	27.6	50.1	125.0	116.1
718+50	313.6	309.2	4.4	22.5	55.5	100.0	102.8
719+50	314.8	308.8	6.0	33.0	70.4	50.0	65.2
720+00	315.0	308.4	6.6	37.4	77.7	50.0	71.9
720+50	315.0	308.0	7.0	40.3	71.9	110.0	137.1
721+60	313.0	307.2	5.8	31.6	86.1	90.0	104.4
722+50	315.6	306.8	8.8	54.5	101.0	150.0	278.0
724+00	314.4	306.6	7.8	46.5			

51  
7877

6  
90.9  
10.5

51  
28



3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPY, 1919 BY J. G. PARKER

LEFAX FILING INDEX

29

78138

E+G Earth

735400	311.8	305.0	6.8	38.9	65.1	175.0	211.2
736775	308.4	303.4	5.0	26.2	53.8	100.0	99.6
737775	307.6	302.4	5.2	27.6	45.3	250.0	210.0
740725	306.0	302.4	3.6	17.7	50.7	125.0	117.4
744500	310.8	304.8	6.0	33.0	59.2	50.0	54.8
742700	311.0	306.0	5.0	26.2	49.9	500.0	461.5
747700	301.6	297.0	4.6	23.7	43.7	300.0	242.6
750700	304.0	300.0	4.0	20.0		3600.0	



750100	3040	300.0	4.0	20.0	37.7	150.0	102.0	Earth
751150	306.0	302.4	3.6	17.7	73.9	250.0	342.0	
754100	315.0	306.0	9.0	56.2	119.7	150.0	332.0	
755150	316.0	306.2	9.8	63.5	91.1	290.0	489.5	
758140	312.0	306.8	5.2	27.6	46.4	60.0	51.5	
759400	311.0	307.2	3.8	18.8	43.8	50.0	40.5	
759150	312.4	307.6	4.8	25.0	55.4	250.0	256.5	
762100	317.6	312.0	5.6	30.4				

LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1919 BY J. O. PARKER

LEFAX, PHILADELPHIA, PA.					ETG	Eqth	
762700	317.6	312.0	5.6	30.4	49.2	100.0	91.0
763700	317.0	312.2	3.8	18.8	69.8	150.0	193.9
764750	321.0	312.6	8.4	51.0	77.2	100.0	142.9
765750	318.0	313.0	5.0	26.2	80.7	150.0	224.0
767700	327.2	318.4	8.8	54.5	78.2	200.0	289.5
769700	330.6	326.0	4.6	23.7	49.9	50.0	46.2
769750	331.0	326.0	5.0	26.2	96.7	150.0	268.8
771700	337.0	326.4	10.6	70.5			

LEFAX FILING INDEX

30





73 LEFAX, PHILADELPHIA, PA.

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						EtG	Earth
784725	343.0	339.2	3.8	18.8	47.8	175.0	155.0
786700	346.8	341.4	5.4	29.0	65.0	300.0	361.0
789700	352.4	346.0	6.4	36.0	76.3	100.0	141.2
790700	351.0	344.0	7.0	40.3	67.9	50.0	62.8
790750	348.0	342.8	5.2	27.6	63.6	50.0	59.0
791700	348.4	342.0	6.4	36.0	53.7	100.0	99.4
792700	343.6 345.6	340.0	3.6 5.6	17.7 30.4	70.7	25.0	32.7
792725	346.4	339.4	7.0	40.3			

LEFAX FILING INDEX



									Eq	Eq
801700	3350	3300	5.0	26.2	52.4	25.0			24.2	
801725	3350	3300	5.0	26.2	66.5	175.0			215.5	
803700	3320	3250	7.0	40.3	70.7	100.0			130.9	
804700	3272	321.6	5.6	30.4	59.4	100.0	110.0			
805700	321.4	316.0	5.4	29.0	77.0	75.0	107.0			0.06101
805775	318.0	310.0	8.0	48.0	134.0	100.0	249.0			
806775	314.0	301.8	12.2	86.0	113.6	85.0	178.7			
807760	301.4	296.0	5.4	27.6	75.6	40.0	56.0			
808740	303.6	295.6	8.0	48.0						

Eq

Eq



									EtG Earth
808+00	303.6	295.6	8.0	48.0	86.9	170.0	273.4		
809+70	301.2	294.4	6.8	38.9	65.1	5.0	6.4		
809+75	299.2	294.2	5.0	26.2	63.6	25.0	29.5	1010.0	
810+00	300.6	294.0	6.6	37.4	3000.0				
811+00	299.6	294.0	5.6	30.4	67.8	100.0	125.7		
813+00	293.0	288.0	5.0	26.2	56.6	200.0	210.0		
814+00	294.8	290.0	4.8	25.0	51.2	100.0	94.7	1440.4	
814+75	296.0	291.4	4.6	23.7	48.7	75.0	67.6		
			3.1	7.1					
			124						

2471.9

EtG  
JE  
E  
EtG

Sta	Elev	Grade	Cut	Area	Sum	Length	EtG	Earth	DG-HP	SR
814+75	296.0	291.4	$\frac{1.5}{F}$ $\frac{3.1}{D.G.}$ 7.1	12.4	14.2	22.4	25.0	6.6	103.6	
815+00	295.6	291.6	1.5	2.5	7.1	10.0				
816+50	304.4	297.0	1.5	5.9	7.1	23.6	150.0	39.5	93.5	
817+00	298.0	298.0	0.0	0.0	0.0	7.1	50.0	6.6	21.9	
817+60	307.6	300.4	1.5	5.7	7.1	22.8	60.0	7.9	25.4	
819+00	304.0	300.6	1.5	1.9	7.1	7.6		36.8	78.6	
820+00	304.8	299.4	1.5	3.9	7.1	15.6	100.0	26.2	42.9	
822+00	298.0	297.0	1.0	0.0	4.5	0.0		42.9	57.9	

	F	DG	Area	E + G	DG-HP	S R
822+00	298.0	1.0	0.45 0.0			
823+10	300.0	1.5	2.571 10.0	23.6	20.4	
823+65	295.4	0.0	0.0 0.0	7.2	10.2	
Equation				<del>65.1</del>		
825+25	297.0	0.0	0.0 0.0			1149
826+25	310.0	1.5	6.571 26.0	13.2	48.2	
828+25	304.0	1.5	1.571 6.0	26.3	59.1	
829+00	302.4	1.5	2.971 11.6	19.7	24.4	
830+00	298.2	1.5	1.7 6.8	25.3	34.1	



Sta.	Elev	Grade	Cut	Area	Sum Length	ETG	Earth DG-HR	S.R.
830+00	298.2	295.0	1.5	1.771	6.8			
834+00	318.4	312.0	1.5	4.971	19.6			
				14.2	26.4	400.0	103.3	195.5
835+00	317.4	312.4	1.5	3.571	14.0			
				14.2	33.6	100.0	26.3	62.3
837+00	318.0	314.0	1.5	5.0	20.0			
				14.2	33.6	100.0	47.8	87.8
837+00	318.0	314.0	1.0	3.0	4.5	12.0		
				16.0	36.0	200.0	33.3	144.5
839+00	324.4	318.0	1.0	5.4	4.5	21.6		
				9.0	33.6	200.0	16.7	66.8
840+00	317.6	313.0	1.0	3.6	4.5	14.4		
				9.0	36.0	100.0	50.0	11.3
641	313.6	310.6	3.0	1.4				
+60	316.0	308.6	7.4	20.6				
					70.9	100		
					300.0			
					41.6	6.0		
					57.2			
					46.2			
					102.5			

10712

Sheir M



80840	2430	2474	56	710	710	218
80860	2466	2466	0.0	0	0	0
80910	2450	2450	0.0	0	20.4	11.2
80930	2420	244.4	7.6	30.4	46.4	60.0
850+	286.-	2810	4.0	16.0	210	1770
853+	2810	277.	4.0	16.0	58.0	44.5
85350	284	276	8.0	32.0	48.0	1110
85475	278.	274	4.	16.0	149.5	769.8



	FRG	Ku	DE+HP	SRU
848	270	265	1.6	oil
849	270	265	1.6	oil
850	270	265	1.6	oil
851	270	265	1.6	oil
852	270	265	1.6	oil
853	270	265	1.6	oil
854	270	265	1.6	oil
855	270	265	1.6	oil
856	270	265	1.6	oil
857	270	265	1.6	oil
858	270	265	1.6	oil
859	270	265	1.6	oil
860	270	265	1.6	oil
861	270	265	1.6	oil
862	270	265	1.6	oil
863	270	265	1.6	oil
864	270	265	1.6	oil
865	270	265	1.6	oil
866	270	265	1.6	oil
867	270	265	1.6	oil
868	270	265	1.6	oil
869	270	265	1.6	oil
870	270	265	1.6	oil
871	270	265	1.6	oil
872	270	265	1.6	oil
873	270	265	1.6	oil
874	270	265	1.6	oil
875	270	265	1.6	oil
876	270	265	1.6	oil
877	270	265	1.6	oil
878	270	265	1.6	oil
879	270	265	1.6	oil
880	270	265	1.6	oil
881	270	265	1.6	oil
882	270	265	1.6	oil
883	270	265	1.6	oil
884	270	265	1.6	oil
885	270	265	1.6	oil
886	270	265	1.6	oil
887	270	265	1.6	oil
888	270	265	1.6	oil
889	270	265	1.6	oil
890	270	265	1.6	oil
891	270	265	1.6	oil
892	270	265	1.6	oil
893	270	265	1.6	oil
894	270	265	1.6	oil
895	270	265	1.6	oil
896	270	265	1.6	oil
897	270	265	1.6	oil
898	270	265	1.6	oil
899	270	265	1.6	oil
900	270	265	1.6	oil

87765	271.6	265.6	6-	24.0	280	35	181
880	266	265	1-	4.0	37.6	100	695
891	270	261.6	8.4	33.6	37.6	80	49
880	282	282	0.0	0	0	40	0
880	282	282	0.0	0	10.4	80	151
885	282	282	2.6	10.4	10.4	65	171
885	282	282	0.0	0	0	60	0
885	282	282	0.0	0	0	60	0

5/2/11









876790	2657	260.	5.4	24.5	24.5	10	4.5
877	279.6	279.6	0	0	0	37	0
+27	28	28.	0	0	0	48	21.6
+85	261.6	276.	5.6	25.5	25.5	15	14.2
878	271.6	254.	5.6	25.5	25.5	25	21.2
+25	273.6	273.6	0	0	0	17	0
+62	252.6	252.6	0	0	0	28	0
+90	257.	257	0	0	0	890	24.2





73

88275	744	744	0	0	75.5	135	63.5
88260	2576	257	5.6	5.6	58.4	70	75.7
88430	760	253	7.0	329	55.5	70	72.0
885	259	274	5.	225	30.9	90	51.5
890	261	279	7	84	58.4	110	119.0
897	276	266	10	50.	67.6	50	62.9
890	270	266	4	17.6	19.0	25	8.9
875	266.	265.6	0.4	1.7			117.1
						17.5	

	L	F-G	Fa.	DG-HP	SB
88475	1775			717.1	
888	20	1.7	0.4	0.8	
88470	130	0	0	0	
890	70	329	7	476	
890	60	329	7	716.6	
89475	165	0	0	0	
890	5	205	4.6	1.9	

100% RECYCLED PAPER WITH 10% POST CONSUMER WASTE  
 100% RECYCLED PAPER WITH 10% POST CONSUMER WASTE



89470	267	260.6	6.4	29.8	34.0	45	77.7	6.7
+30	267	260.4	1.6	6.7	36.5	10	17.9	11.8.4
+60	266	260.4	5.6	25.5	32.4	30	14.60	
+65	265	261	4.0	17.6	43.1	55	44.0	
+75	264	261	1.2	4.7	71.8	10	4.0	
+90	267	261.6	5.4	24.5	50.0	20	18.5	
+95	266	261.6	4.6	20.5	45.0	60	50	
				10.0			849.0	

	L	E-G	Fa	DG-HP	S/R
8N460 766	2460	✓		118.4	
	30	✓		15.5	
490 762.6 760	10	✓		7.2	
895 767.6 760	55	✓		88.0	
45 769.6 79.6	15	✓		19.9	
470 769.5 79.5	10	✓		0	
480	30	✓		13.8	
896 767 209.2	140	✓		94.5	
897400 768					

CELLULAR TELEPHONE

DATE: 11/1/88

891140	28	28	0	0	0	15	0	0	0
+85	-	-	0	0	0	20	84	31	31
+75	260	28	✓	88	16.8	125	38.7	38.7	38.7
89	209	207	✓	88	38.7	100	70.8	70.8	70.8
900	262.5	276	6.5	24.8	3000	75	465.9	465.9	465.9
+75	259	258	1-	4	33.6	75	0.0	0.0	0.0
901+50	275	260	15.0	60	64	7.5	89.0	89.0	89.0
902	278	260	18-	7	127	50	177.1	177.1	177.1

1790

LEFAX FILING INDEX





91060x	27x	27x	0	0	0	138	✓
912	275.5	275.5	0	0	41.8	100	✓ 97.5
913	291.2	284	7.2	41.8	67.0	900	11200
922	331	326	5.	26.2	41.6	500	1385.0
927	305.0	302.2	3.2	15.4	15.4	87	176.8
989	299.6	299.6	0	0	0	150	0
994x7	297.2	297.2	0	0	27.4	63	43.6
930	303	296.4	6.6	27.4	30.0	30.0	183.8

15A  
31

~~183.8~~





927+50	248	295	3.0	14.7	67.0	250	788.5
920	302	296	8.-	48.0	74.0	50	688
+50	303	298	5.-	26.2	48.7	150	135.5
922	311.	306.6	4.4	22.5	47.5	100	87.8
923	302	302.6	4.8	25.0	46.0	200	171.0
925	289.6	285.4	4.2	21.2	54.0	100	100.6
926	286.	280	6.-	33	66.0	450	550.0
927+50	302	296	6.-	32			



95450	3226	322.	616	37.4	61.1	250	283.0
9574	3626	358	4.6	23.7	56.2	300	2660
960	3934	389	4.2	22.5	309.8	298.16.4	
961	400.	396;	4.0	20.0	415	100	78.5
962	389	385	3.0	14.8	343	200	171.0
965	384	378	3.2	16.6	309	200	114.4
967	375	367.2	6.6	37.4	54.0	200	200.0

2872

LEFAX FILING INDEX





977H10	306	352	4	70.2	40	250	185.0
980	306	302	4	70.2	212	200	100.1
982	335.6	324	1.6	7.2	44.6	150	174.0
983H10	306.6	328	6.6	37.4	70.4	150	106.0
985	314	309	6.0	33.0	50.7	100	03.7
986	267.6	264	3.6	17.7	32.0	100	59.2
987	257	244	3.0	14.2	14.2	30	7.9
990	239.4	239.4	0	0	14.2	30	7.9

215 65

	L	F-G	En	D	SR	SR
98720	779.4	779.4	0	0		
989	726	726	0	0	0	170
990	747	735.2	11.8	82.1	82.1	154.0
					<u>300.0</u>	203.4
99045	206	235.0	10.8	72.4	154.5	65
991	200	235.2	48	25.0	97.5	35
99375	200	221	.90	56.2	81.2	25
99410	222	229.6	3.4	16.6	77.8	35
						44.0
						42.1

2037



9m110	222	222,6	3,2	16,6	76,4	55	78,0
465	257	222,6	9,4	59,8	97,8	8,5	146,0
9m150	222	222	6,0	33,0	59,2	200	216,0
9m150	202	202	5,0	24,2	26,2	52	146,1
885	144	144	0	0	0	2/25	0
1000+10	148	148	0	0	34,5	90	57,5
1001+	216	216	6,2	34,5	57,5	450	022,0
1001+1001	228	228	4,0	20,0	57,5	450	022,0

					L	F.S	Fa	DG-HP	SRJ
100045									
100047	270.6	264	4.0	20.0	57.4	59.0			
100048	277	272	6.6	37.4	62.6	100			
100049	324	330	5.0	26.2	74.2	200			
100050	324	360	6.0	48.0	68.0	100			
100051	324	360	4.0	20.0	62.0	50			
100052	350.4	323	7.4	43.3	62.0	600			
100053	364	360	4.0	20.0	62.0	600			
100054	362	359.6	3.4	16.6	36.6	50			

1015750	3.0	16.6	56.9	50	57.7
1016+ 366.	7.0	40.7	56.9	25	76.4
+25 362.2	3.4	16.6	58.4	25	77.1
+50 366.0	7.2	51.8	61.8	50	57.2
1017 362	4.0	20.0	56.0	10	10.4
+10 362.4	6.4	26.0	52.6	65	62.2
+75 361.	3.0	16.6	49.0	25	71.8
1018 362	5.6	30.2			



	L	F-E	Fa	JG-HP	SR
1018+	4.6	30.4	4.8	75	63.5 ✓
+	3.2	15.4	5.8	45	44.0
1014+20	6.6	37.0	5.4	80	85.1 ✓
1020+	4.0	20.0	5.4	30	38.6 ✓
				40	48.6
1021	2.0	9.0	2.9	97.5	70.0
1020.5	4.4	22.5	3.5	17.5	72.5
1028	3.6	17.7	4.0	300	77.0

37686-

1078+	326	17.7	36.5	150	101.5
1079+50	320.4	2.8	38.8	150	108.0
1079+	326	4.0	56.0	125	130.0
1079+5	320.4	6.4	56.0	175	130.0
1079+50	324	4.0	70	85	215
1079+25	322.5	0	0	115	0
1079+50	311	0	mis	50	20.8
1079+	316.4	4.4	mis		





107201	5	26.7	63.6	100	118.0
107201	6.6	37.4	57.4	100	106.0
107201	4	20.0	38.8	200	144.0
1050	3.8	18.8	30.8	200	144.0
1052	4.0	20.1	38.8	300	155.0
1051	7.0	40.7	60.3	200	113.0
1051	5.1	24.7	66.5	300	170.0
1051	6.2	34.5	60.7	75	84.8

21824

	L	E-G	Fv	D.O. HP	S.R.
10875	34.5	115	13.5		
108790	0	150	0		
108790	17.7	160	54.5		
108901	37.7	200	139.5		
10895	54.5	300	776.0		
1088	55.0	200	166.7	✓	
1070	40.1	200		148.5	
1072					

23378

1072 ✓			4	17.6	↓ 0.1	.400	✓ 99.0
1076	312	309	5	22.5	↓ 8.0	1.50	132.5
1077+50	306.6	301	5.6	22.5	↓ 2.1	2.00 3.00 3.00	199.0
1080	266	262	4-	17.6	↓ 1.4	1.50	✓ 178.0
10801	225	219	6.	27.6	↓ 2.2	2.00	167.0
1081	181	180	4.	17.6	↓ 1.5	2.00	167.1
1081	166.4	157.2	7.2	24.0	↓ 1.6	1.00	95.5

1569.3



					L	E-G	Fa. De-HP	S-R
1085			7.2	34.0	51.6	100	95.5	
1086	146	144	4.0	17.6	52.7	200	195.0	
1088	129	126	7.4	35.1	52.7	200	195.0	
1090	141	117	4.0	17.6	55.2	400	334.0	
1094	106	100	6.0	27.6	57.4	300	219.0	
1097	101.4	95	6.4	24.8	100.0	100	185.0	
1098	107.6	94.4	13.2	70.2	129.1	200	512.0	
1100	103	90	13.0	68.9				

1100+			13.0	68.4		101.6	150		282.0
1101+50	91	84	7.	32.9		71.2	150		198.0
1102	88	80	8.	28.4		89.4	50		245.0
+50	87.4	79	8.4	57.0		88.4	25		82.6
+75	84.6	78	6.6	37.4		93.6	125		41.0
1105	87	78	9.0	56.2		82.4	400		276.0
1109	84	74	5.0	26.2		59.2	100		611.0
1110	92	87	6.0	33.0		30.00			109.5
							30.00		1060.1

7805





1115	160	4	17.6	38.1	✓600	141.0
1117	276.6	4.6	20.5	38.1	200	141.0
1119	274	4	17.6	35.2	400	261.0
1122	328	4	17.6	48.1	50	40.0
+50	327.6	5.6	20.5	45.0	50	41.7
1124	322	4.4	19.5	41.0	200	155.0
1126	323	5	22.5	35.4	100	65.5
1127	319	3	17.9			



1132+10	4	17.6	29.1	50	24.4
1133	4.4	19.5	19.5	50	18.1
+50	0	0	0	170	0
1134+70	0	0	8.4	30	4.7
1135	✓	6.4	6.0	200	106.0
1137	4.	17.6	8.10	300	179.0
1140	3.4	14.7	1810.00	110.0	1810.0

1810.0

1810.0  
110.0



	L	E-G	En	DG-HR	SR
1140		14.7	<del>258</del>	47.7	
1141		12.1	356	33.0	
450		24.5	104.5	20.0	
1142+50	20	186	85	47.2	
480	181	181	0	0	
1143+85	180.4	0	0	0	
1144+12	19.4	13.4	71.5	35.7	
1145	178.4	4.4	91.0	148.0	

892  
6

1145	4.4	140	19.5	75	27.1
75	0	0	66.3	95	116.1
114670	17.6	66.8	98.2	130	226.0
1148	6.8	31.9	81.9	75	189.9
75	10.-	50.-	72.5	1	121
76	5.-	22.5	54.4	79	20.5
1149+05	6.8	31.9	85.5	21	12
607	10.6	53.6			





1186	11.0	56.1	83.7	1.50	463.0
1187+50	6 -	21.6	52.1	7.50	772.0
1195	54	24.5	50.0	5.00	463.0
1200	56	25.5	50.0	5.00	327.0
					<u>327.0</u>



1210+10

0 0

+50

355

7.

329

329

40

26.7

121242

365.1

6.0

27.6

60.5

193

26.0

1011.4

1216

364

10.0

65.0

611.0

1795.0

1224

367

9.0

56.2

171.2

800

1235.0

5641.0

600

2000

111.2

4652  
9





1260			7.6	46.4						
1269	341	371	10-	65.0	109.9	900	1820.0			
1278	377	370	7-	40.7	105.3	900	1750.0			
1285	352	371.6	10.4	68.7	109.0	700	1471.0			
1290	378	368	10.0	65.0	188.7	500	1740.0			
						2000	6927.0			

6277-





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LEFAX, PHILADELPHIA, PA.

42

±


LEFAX FILING INDEX

T.P. 18° 7° 10° ← River Bottom  
 +71 11° 7° 10°  
 +35' 11° 7° 11°  
 42+00 10° 7° 9°

41+00 10 7 9 ← River Bottom

40+58 7° 7°

40+00 3° 6° 5°  
 38+95 16° 5° 4° Break

38+00 22° 7° 14° 63° Toe Slope

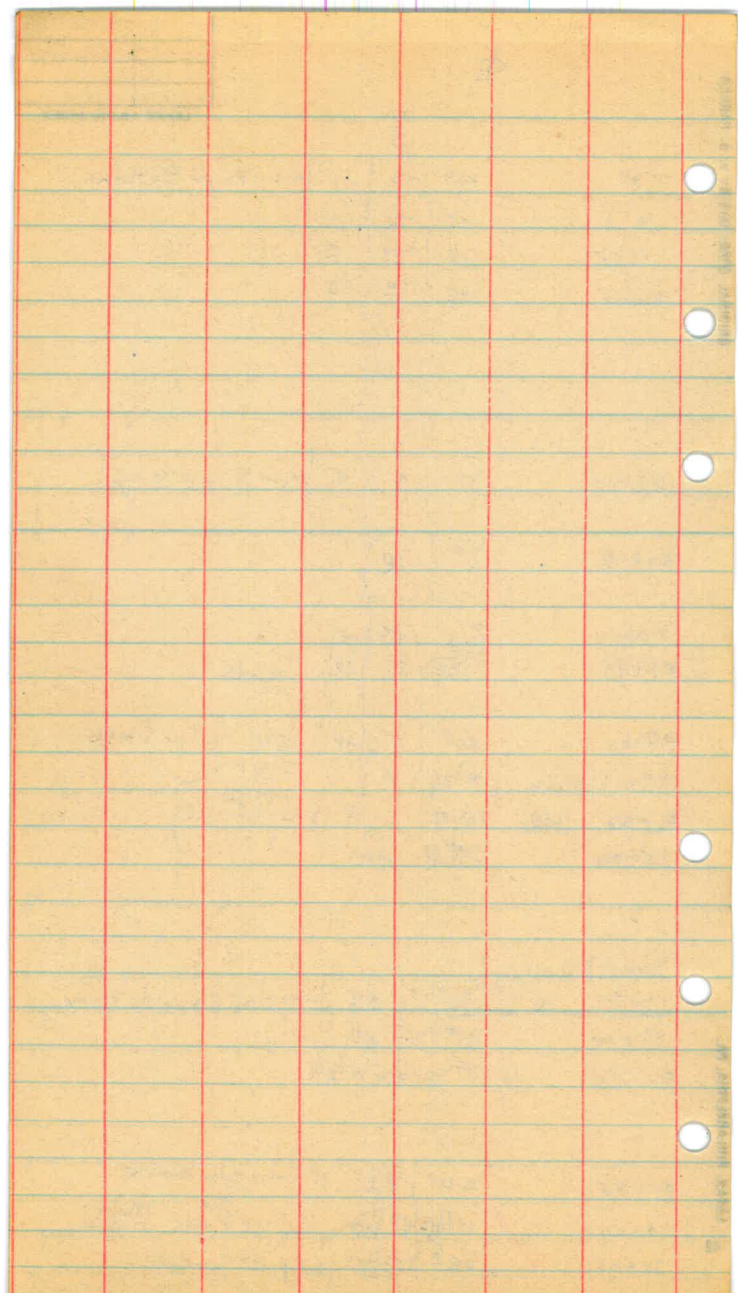
37+00 Break 9° 13° 7° Break  
 36+00 26° 11° 7° 1° 21° 16° 16°  
 35+00 25° 7° 44°

Forest Boundary  
34+00 38° 8° 21° ← Even Slope to river

33+00 41° 13° 8°  
 32+95 → 32+72 Wash

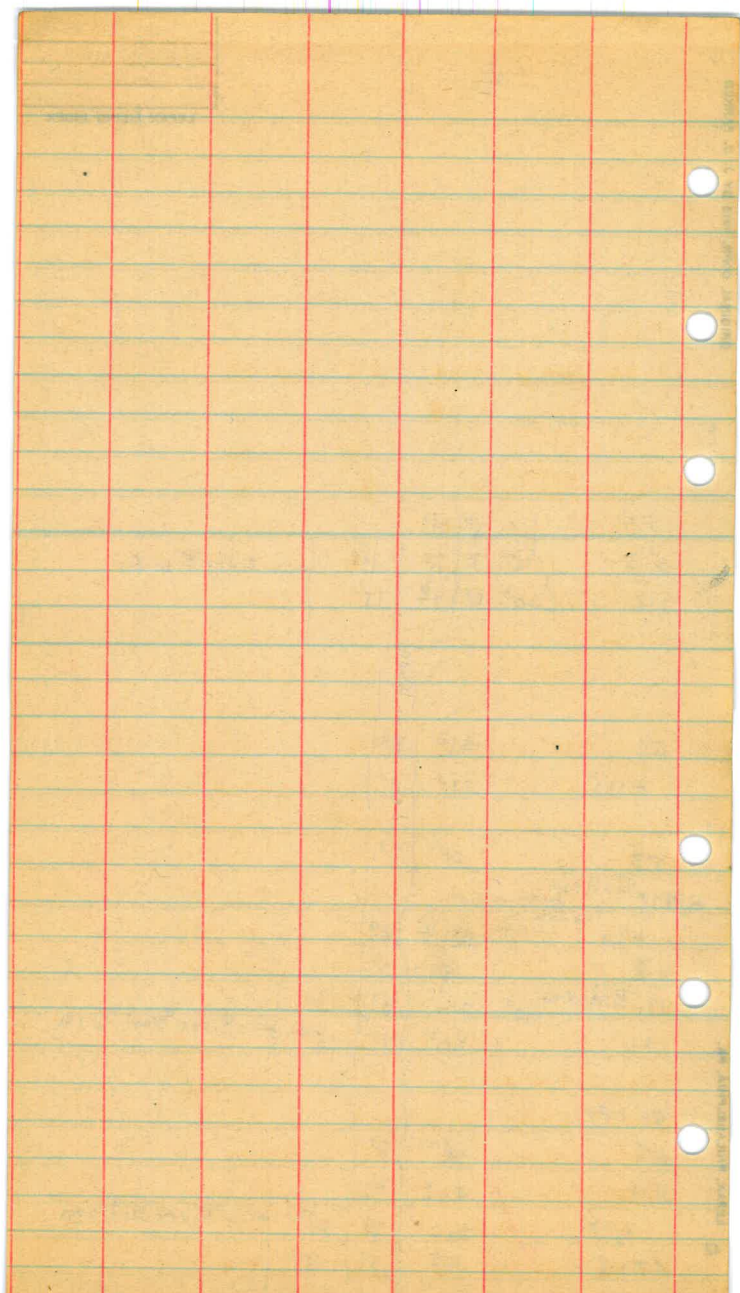
31+95 24° 7° 16° 9° ← Edge Bank

31+00 18° 12° 9° 15° 49° River Bottom  
 30+00 ✓ 28° 10° 73° 20° 12° ← 41°



54	6°	5°	9°		
53	15°	7°	7°	11°	← Edge Bank
52	30°	13°	8°	15°	
					Road
51		41°	8°		
+45		51°	8°		
50		39°	7°		
49+75	Gully				
+90	Top Bank				
		40°	9°	8°	
48		18°	7°		
47 Break	10°	27°	8°	19°	← River Bed Dry
46		30°	7°	15°	
45+89					
45		28°	8°		
44		40°	7°		
+55		20°	7°	25°	← River Bottom
43+00		16°	8°	15°	





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# El Capitan Pipeline Survey


LEFAX FILING INDEX

67+80  
~~66+32~~

67+00

66+00

65+50 Area

65

64

63

62

61

60

58+84

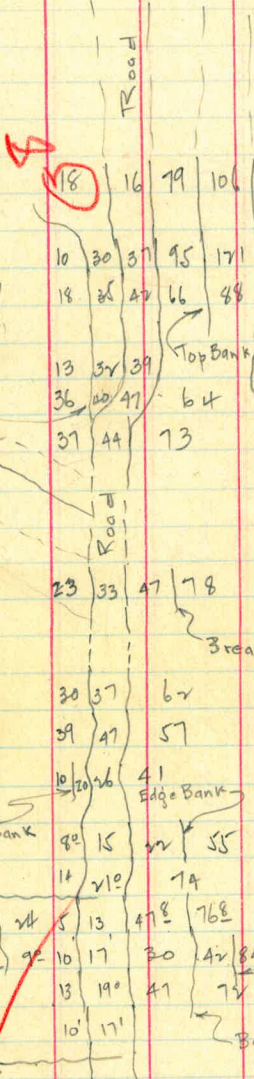
58+00

57+00 Gully

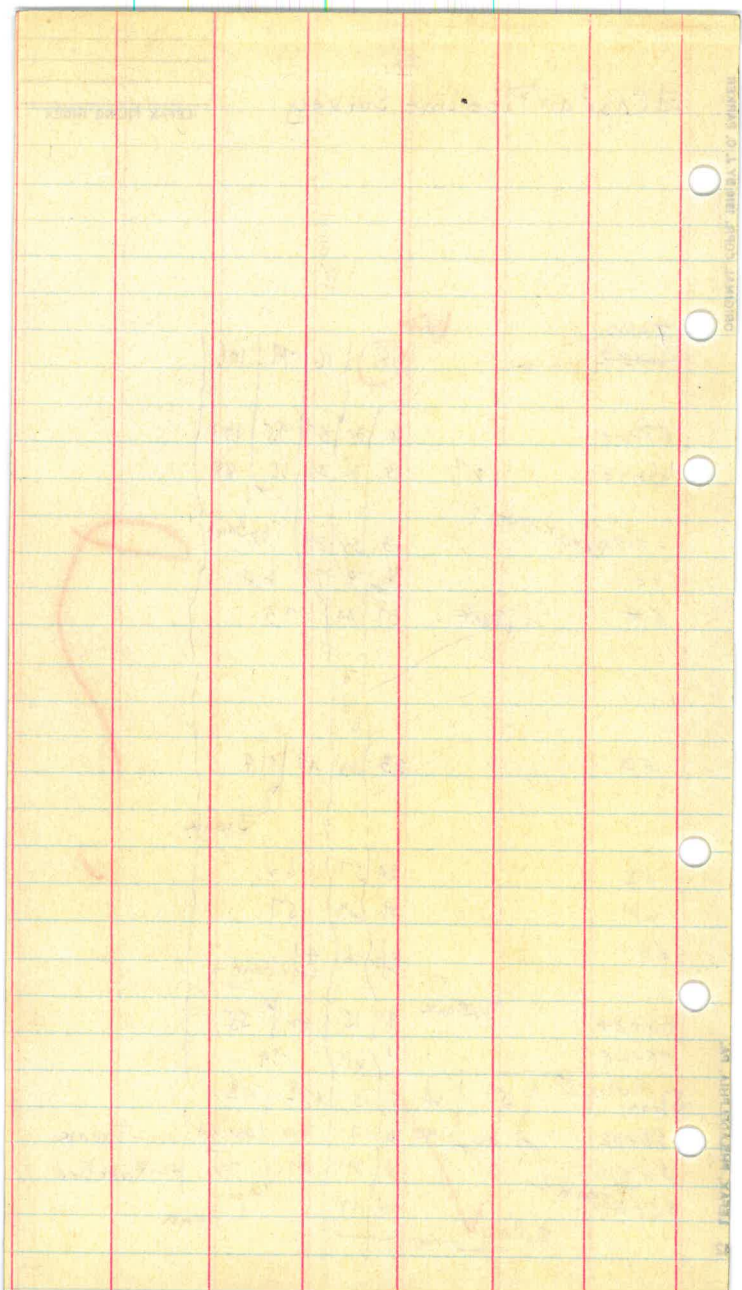
56+02

55+16 Break

55+00 Gully



LEFAX, PHILADELPHIA, PA. 42





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LEFAX, PHILADELPHIA, PA.

Sta to Sta	Length	Description	Loss of Head in Ft
1+41.7 2+34.3	87.6	24° Curve	
7+49.1	—	L 5° 27'	
8+51.8	—	L 1° 42'	
9+53.8 11+68.0	234.2	6° Curve	
11+72.2 13+25.3	153.1	6° Curve	
14+24.4 14+78.9	54.5	44° Curve	
19+27.5 21+03.1	175.6	6° Curve	
21+06.4 22+72.1	75.7	38° Curve	
24+52.9 25+01.6	48.7	24° Curve	
25+17.3 26+36.5	119.2	12° Curve	
27+77.5 28+17.6	40.1	34° Curve	
28+47.3 30+61.7	214.4	8° Curve	
30+85.8 32+22.7	136.9	6° Curve	
32+61.5 34+52.3	190.8	4° Curve	
35+60.4 37+05.8	145.4	12° Curve	
37+41.2 37+91.1	49.9	44° Curve	
38+22.1 38+85.1	63.0	24° Curve	
38+85.8 40+00.2	114.4	14° Curve	
40+96.5 41+55.0	58.5	10° Curve	
42+43.4 43+22.4	73.0	20° Curve	
43+47.8 44+75.5	127.67	10° Curve	
46+52.8 46+92.1	39.3	38° Curve	
47+49.0 48+28.3	79.3	32° Curve	
49+35.8 49+74.1	38.3	32° Curve	
51+42.9	—	L 2° 43'	
52+62.9 53+82.9	113.0	16° Curve	
55+63.4 57+34.7	165.3	12° Curve	
60+16.9 61+11.3	94.4	8° Curve	
61+15.6 61+55.1	39.5	44° Curve	
65+49.3 67+38.2	188.9	18° Curve	
69+80.9 70+20.0	39.1	76° Curve	
71+18.2 72+35.1	116.9	26° Curve	



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LEFAX, PHILADELPHIA, PA.  
12

El Cap Pipeline  
Loss of Head in  
Curves, Angles, Fittings

LEFAX FILING INDEX

Sta	to Sta	Length	Description	Loss of Head in Ft
72+833	-	-	44'2"	
75+875	76+271	396	20° curve	
77+443	79+445	200.2	18° curve	
79+475	81+36.8	189.3	10° curve	
83+575	83+973	398	28° curve	
85+933	-	-	43°06'	
91+627	93+487	186.0	10° curve	
94+486	96+469	198.3	4° curve	
97+912	99+225	137.3	18° curve	
102+908	-	-	42°07'	
105+591	106+496	90.5	10° curve	
106+567	110+390	382.3	10° curve	
113+215	-	-	44°38'	
114+241	115+964	172.3	28° curve	
116+129	116+ <sup>513</sup> <del>42</del>	39.0	24° curve	





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LEFAX, PHILADELPHIA, PA.

42


LEFAX FILING INDEX

Sta. L. Bear Dist Curve

N.83°08'W 4.2

11+68<sup>2</sup> E.C.

E = 7.2  
T = 112.1  
R = 954.93  
D = 60  
L = 2342

8+0+51<sup>2</sup> 14°03'R

9+33<sup>2</sup> B.C.

Mon. 1/18/24

5.82°49'W 82.0

8+51<sup>2</sup> 1°42'R

5.81°07'W 102.7

8+47<sup>2</sup> 5°27'L

5.86°34'W 514.8

2+34<sup>2</sup> E.C.

E = 41  
T = 44.3  
R = 238.73  
D = 34  
L = 87.6

8+91<sup>2</sup> 21°01'L

1+46<sup>2</sup> B.C.

N.72°25'W 146.7

0+00



Sta.	Elev.	Grade	Cut	End Area	Average Area	Horizontal Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds	Vol. Cu. Yds
999+100	232.8	226.33	6.5	36.4	<del>32.6</del> 34.1	17.8	1%	0.0	17.8	607.0	✓
999+128	232.0	226.21	5.8	31.6	28.8	25.0	1%	0.0	25.0	690.0	✓
999+128	230.6	226.04	4.6	23.7	22.4	25.0	6%	0.04	25.04	560.9	✓
999+128	229.1	224.93	4.2	21.2	19.1	25.0	6%	0.04	25.04	478.3	✓
999+128	226.9	223.13	3.5	17.0	17.0	25.0	15%	0.28	25.28	429.8	✓
1000+128	223.8	220.33	3.5	17.0	23.3	25.0	15%	0.28	25.28	589.0	✓
1000+128	222.1	216.58	5.5	29.6	31.3	25.0	15%	0.28	25.28	791.3	✓
1000+128	218.8	212.83	6.0	33.0						126,195.1	✓
										124,557.6	

4,613.0 9,303.5

(27)

Est #1

TRADE MARK

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns, with some lines starting with "1911" and "1912".

1911  
1912  
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THE UNIVERSITY OF CHICAGO PRESS

CHICAGO, ILLINOIS, U.S.A.

Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1000+62.8	218.8	212.83	6.0	33.0	32.6	25.0	15%	0.28	25.28	824.1	✓
1000+92.8	215.0	209.08	5.9	32.3	32.6	25.0	18%	0.40	25.4	828.0	✓
1001+17.8	210.8	204.76	6.0	33.0	25.6	25.0	18%	0.40	25.4	650.2	✓
1001+42.8	203.9	200.22	3.7	18.2	17.4	25.0	18%	0.40	25.4	442.0	✓
1001+62.8	199.1	195.67	3.4	16.5	17.4	20.2	18%	0.32	20.52	357.0	✓
1001+82.0	195.7	192.00	3.7	18.2	18.5	12.0	15%	0.13	12.13	224.6	✓
998+17	194.0	190.20	3.8	18.8	9.4	30.0	15%	0.09	30.16	287.6	✓
998+47	187.2	187.24	0.0	0.0			8%	0.07	119.804.6	428.765.7	✓

4,796.9 4,437.2

28

TRADE MARK

EST #1





LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
999+50	188.0	188.00	0.0	2.8	15.0	8%	0.05	15.05	42.1	✓
999+65	190.5	189.20	1.3	5.6	10.0	8%	0.03	10.03	116.3	✓
999+75	199.6	192.00	3.6	17.6	25.0	16%	0.32	25.32	633.0	✓
1000+00	199.9	194.00	5.9	32.3	25.0	16%	0.32	25.32	947.0	✓
1000+25	205.3	198.00	7.3	42.5	25.0	16%	0.32	25.32	1807.8	✓
1000+50	210.6	202.00	8.6	52.9	25.0	20%	0.50	25.50	1315.8	✓
1000+75	215.3	207.00	8.3	50.4	25.0	20%	0.50	25.50	1224.0	✓
1001+00	219.7	212.00	7.7	45.6	148.534.6	148.534.6				

(3)

FST #12

TRADE MARK

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6.966.9

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FRANCIS & TAYLOR, INC.

FRANCIS & TAYLOR, INC.



Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1001+00	219.7	212.00	7.7	45.6	25.0	20%	0.50	25.50	1173.0	✓
1001+25	224.8	217.00	7.8	46.4	25.0	20%	0.50	25.50	1086.3	✓
1001+50	228.8	222.00	6.8	38.8	25.0	20%	0.50	25.50	933.3	✓
1001+75	233.2	227.00	6.2	34.4	25.0	20%	0.50	25.50	823.6	✓
1002+00	237.6	232.00	5.6	30.2	25.0	20%	0.50	25.50	688.5	✓
1002+25	241.6	237.00	4.6	23.7	25.0	20%	0.50	25.50	612.0	✓
1002+50	246.7	242.00	4.7	24.3	25.0	20%	0.50	25.50	652.8	✓
1002+75	252.1	247.00	5.1	26.9	25.0	20%	0.50	25.50	572.37	✓

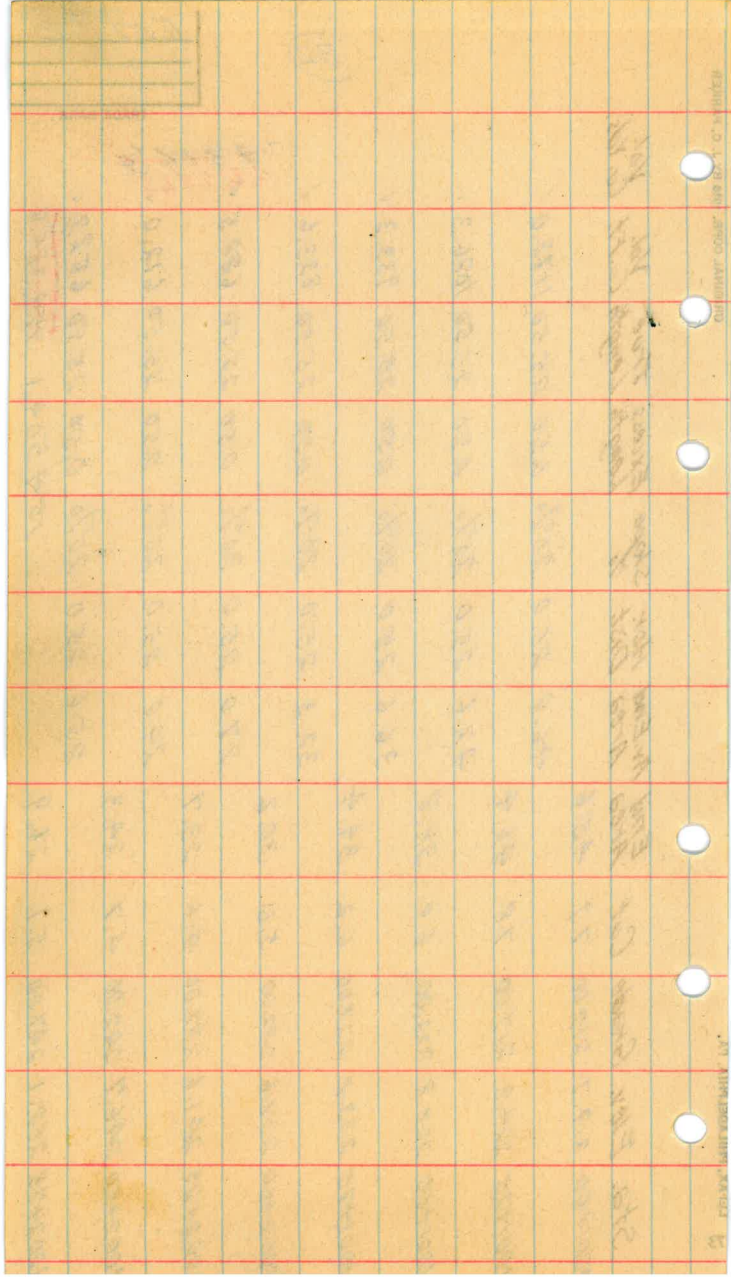
32

5718.0  
5722.37

Est #2

TRADE MARK

154,504.1  
154,384.8



Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1002+75	252.1	247.00	5.1	26.9	26.6	25.0	20%	0.50	25.50	678.3	✓
1003+00	257.0	252.00	5.0	26.2	33.7	25.0	20%	0.50	25.50	846.6	✓
1003+25	264.0	257.00	7.0	40.2	38.8	25.0	20%	0.50	25.50	989.4	✓
1003+50	268.6	262.00	6.6	37.3	34.4	25.0	12%	0.18	25.18	866.2	✓
1003+75	270.8	265.00	5.8	31.6	27.0	25.0	12%	0.18	25.18	679.9	✓
1004+00	272.4	268.00	4.4	22.4	20.0	25.0	5%	0.03	25.03	500.6	✓
1004+25	272.9	269.33	3.6	17.6	16.0	25.0	5%	0.03	25.03	400.5	✓
1004+50	273.7	270.67	3.0	14.3	15.9	25.0	15%	465.6	159.3437	159.3437	✓

33

Est #2

TRADE MARK

~~9.106.5~~  
51.906.5





Sta	Elev.	Grade Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1004+50	273.7	270.67	3.0	14.3	17.8	25.0	5%	0.03	25.03	495.5 ✓
1004+75	276.2	272.00	4.2	21.2	<del>27.4</del> 28.0	25.0	12%	0.18	25.18	689.9 ✓
1005+00	281.1	275.00	6.1	33.7		25.0	160,601.0	<del>160,601.0</del> 160,994.2		

See Pages 14, 15, 16 & 19 - Est #1  
for computations  
of yardage:

$$\left. \begin{array}{l} 966 + 25 - 968 + 15.6 \\ 969 + 50 - 970 + 75.5 \end{array} \right\} 9,359.0 \text{ Cu. Ft.}$$

Completed Aug. 23

$$\begin{array}{r} 9,359.0 \\ 169,853.2 \\ + 70,705.0 \\ \hline 169,960.0 \end{array}$$

34

Aug. 23

TRADE MARK

Est #2





Finished Grade  
July 10

(4)

TRADE MARK

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ex.	Vol. Cu. Fk.
949+00	287.9	283.33	4.6	23.7	23.7	25.0	9%	0.10	25.10	594.9	
948+75	290.1	285.50	4.6	24.9	24.9	25.0	9%	0.10	25.10	625.0	
948+50	292.7	287.67	5.0	26.2	26.9	25.0	9%	0.10	25.10	675.2	
948+25	295.0	289.83	5.2	27.6	27.9	25.0	9%	0.10	25.10	700.3	
948+00	297.3	292.0	5.3	28.2	28.9	25.0	9%	0.10	25.10	725.4	
947+75	299.7	294.17	5.5	29.6	30.9	25.0	9%	0.10	25.10	775.6	
947+50	302.2	296.33	5.9	32.3	31.9	25.0	9%	0.10	25.10	800.7	
947+25	304.3	298.50	5.8	31.6						1867.3	
										1969.8	

8886









LEFAX, PHILADELPHIA, PA.

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Sta. Elev. Grade Cut End Area Av. End Area Hor. Dist. Slope % Excess Length True Length Vol. Cu. Ft. Vol. Cu. Yds.

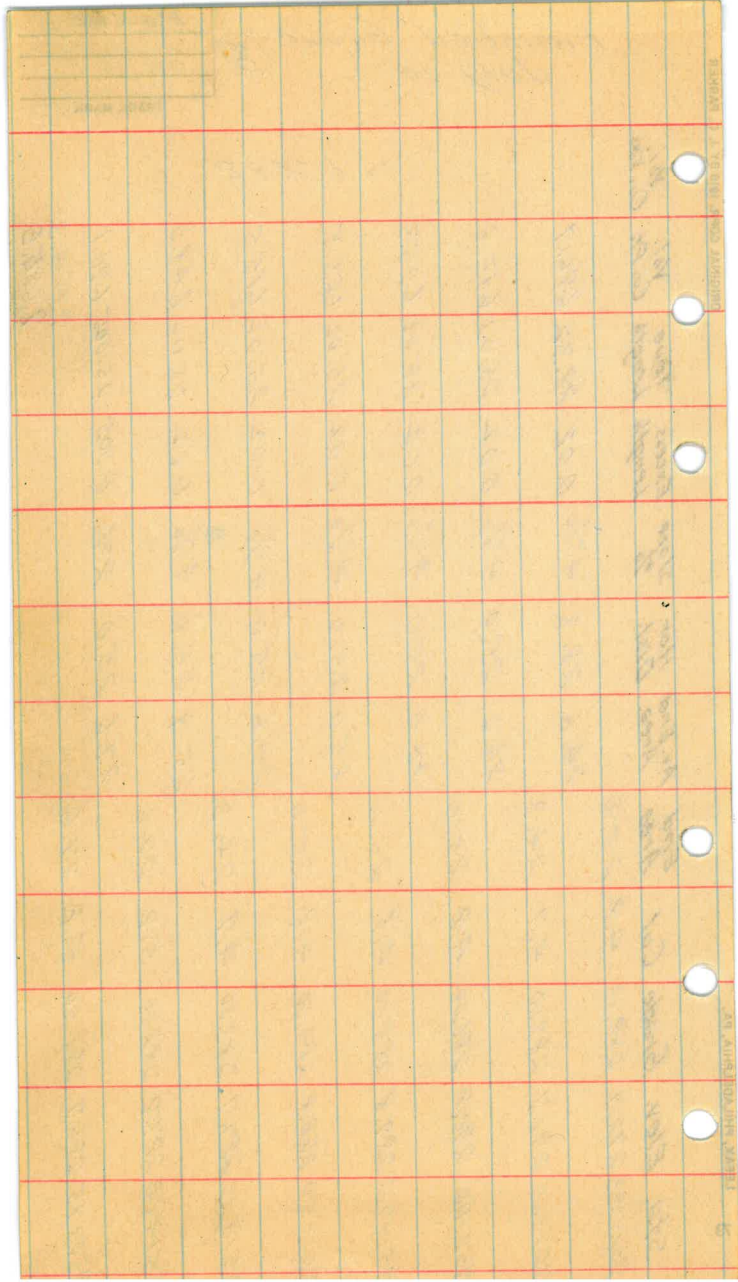
Finished Grade July 10 (2)

TRADE MARK

✓ ✓ 850

952133	292.9	288.13	4.8	25.0	24.6	28.3	4%	0.02	28.32	696.7	
952125	291.7	287.00	4.7	24.3	24.6	25.0	4%	0.02	25.02	615.5	
952100	290.8	286.00	4.8	25.0	25.0	25.0	4%	0.02	25.02	625.5	
951175	289.8	285.00	4.8	25.0	25.0	25.0	4%	0.02	25.02	625.5	
951150	288.8	284.00	4.8	25.0	24.6	25.0	4%	0.02	25.02	615.5	
951125	287.7	283.00	4.7	24.3	25.9	25.0	4%	0.02	25.02	648.0	
951100	287.2	282.00	5.2	27.6	27.6	25.0	2%	0.005	25.005	690.1	
950175	286.7	281.50	5.2	27.6						865.3	
										865.6	

865.3  
865.6





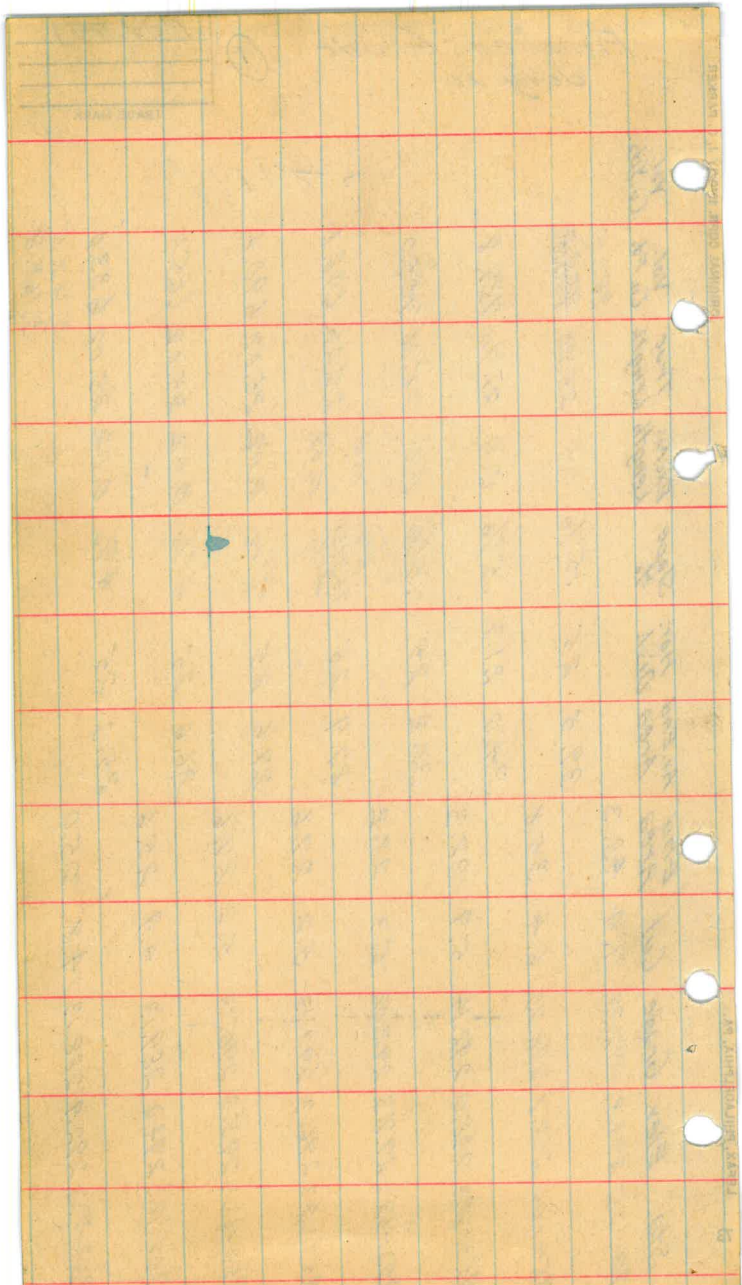
Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
954+25	292.8	292.37	7.4	43.3	39.5	25	.5%	0.0	25.00	987.5	
954+00	292.7	292.25	6.4	35.8	34.0	21.7	.5%	0.0	21.70	737.8	
953+93	292.0	292.14	5.9	32.3	30.2	25	.5%	0.0	25.00	755.0	
953+53.3	297.3	292.22	5.3	28.2	27.9	25	.5%	0.0	25.02	698.1	
953+28.3	296.3	291.13	5.2	27.6	27.6	25	4%	0.02	25.02	690.6	
953+03.3	295.3	290.13	5.2	27.6	26.6	25	4%	0.02	25.02	665.5	
952+78.3	294.0	289.13	4.9	25.6	25.3	25	4%	0.02	25.02	639.0	
952+53.3	292.9	288.13	4.8	25.0						5,167.5	
										5,168.8	

Finished Grade  
July 10

①

TRADE MARK

→ 7161



Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
985+50	334.3	330.00	4.3	21.8	22.4	25.0	6%	0.04	25.04	560.9	
985+25	335.9	331.4	4.5	23.0	21.5	25.0	6%	0.04	25.04	538.4	
985+00	336.8	332.8	4.0	20.0	20.3	25.0	6%	0.04	25.04	508.3	
984+75	338.3	334.20	4.1	20.6	18.0	25.0	6%	0.04	25.04	450.7	
984+50	338.8	335.60	3.2	15.4	16.2	25.0	6%	0.04	25.04	405.6	
984+25	340.5	337.00	3.5	17.0	15.6	25.0	6%	0.04	25.04	390.6	
984+00	341.4	338.4	3.0	14.3	14.5	25.0	6%	0.04	25.04	363.1	
983+75	342.9	339.8	3.1	14.8						22,894.9	846.0
										<del>25,894.4</del>	

Finished Grade  
July 17

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Co. Yds.
962+50	382.4	371.70	4.7	24.3	23.7	25.0	10%	0.12	25.12	595.3	
962+25	379.7	375.23	4.5	23.1	16.0	25.0	10%	0.12	25.12	401.9	
962+00	374.8	372.76	2.0	9.0	17.3	25.0	10%	0.12	25.12	434.6	
961+75	375.2	370.29	4.9	25.6	26.2	25.0	10%	0.12	25.12	658.1	
961+50	372.9	367.82	5.1	26.9							

80,876.6  
34.5  
2993.2

19

(Missing yardage  
not finished grade

Note: See August 23  
July 26

Accumulative  
July 26

TRADE MARK

9369.0  
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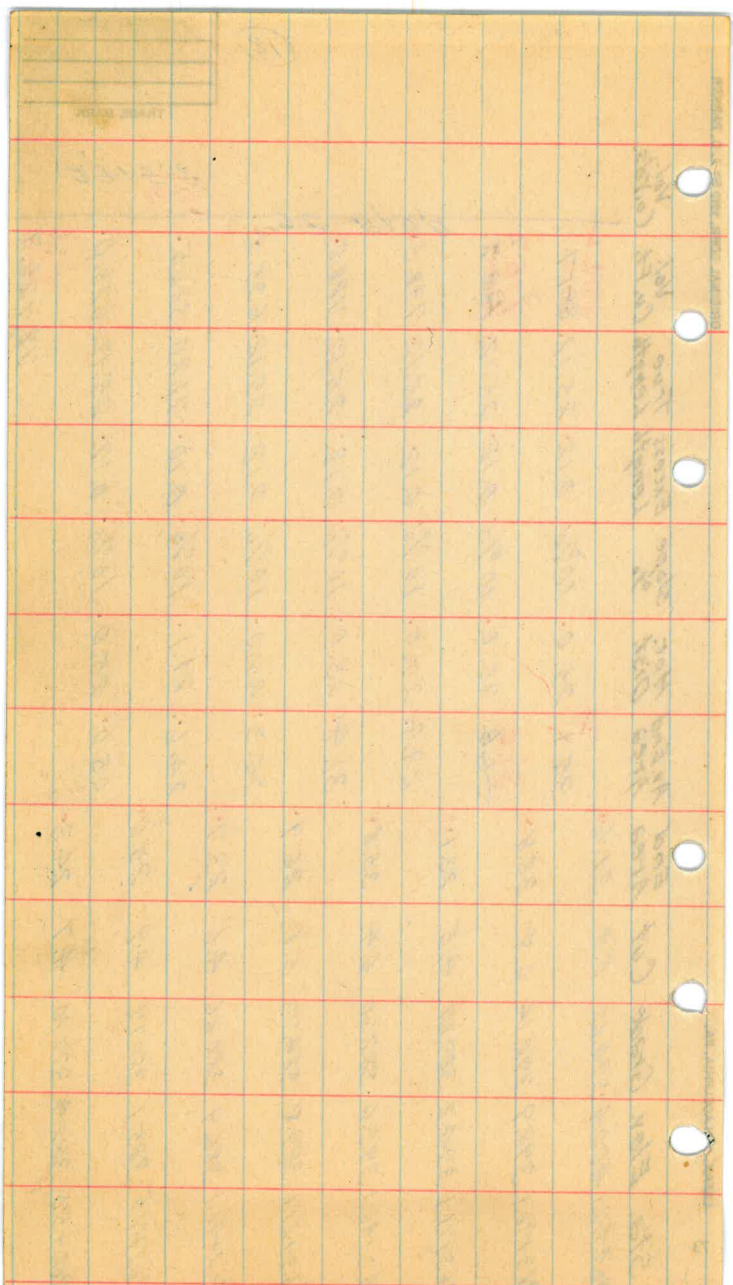
Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
964+21.1	400.4	394.62	5.8	31.6	35.1	25.0	10%	0.12	25.12	884.2	
963+96.1	398.9	392.14	6.8	38.8	<del>34.6</del> 31.9	25.0	10%	0.12	25.12	787	
963+71.1	394.2	389.67	4.5	23.1	29.4	25.0	10%	0.12	25.12	738.5	
963+46.1	393.6	387.20	6.4	35.8	31.4	25.0	10%	0.12	25.12	788.8	
963+21.1	389.8	384.73	5.1	26.9	25.3	25.0	10%	0.12	25.12	635.5	
962+96.1	386.9	382.26	4.6	23.7	24.6	21.1	10%	0.10	21.20	521.5	
962+75	385.1	380.17	4.9	25.6	25.0	25.0	10%	0.12	25.12	628.0	
962+50	382.4	377.70	4.7	24.3						446	
										78726.7	

July 26

(18)

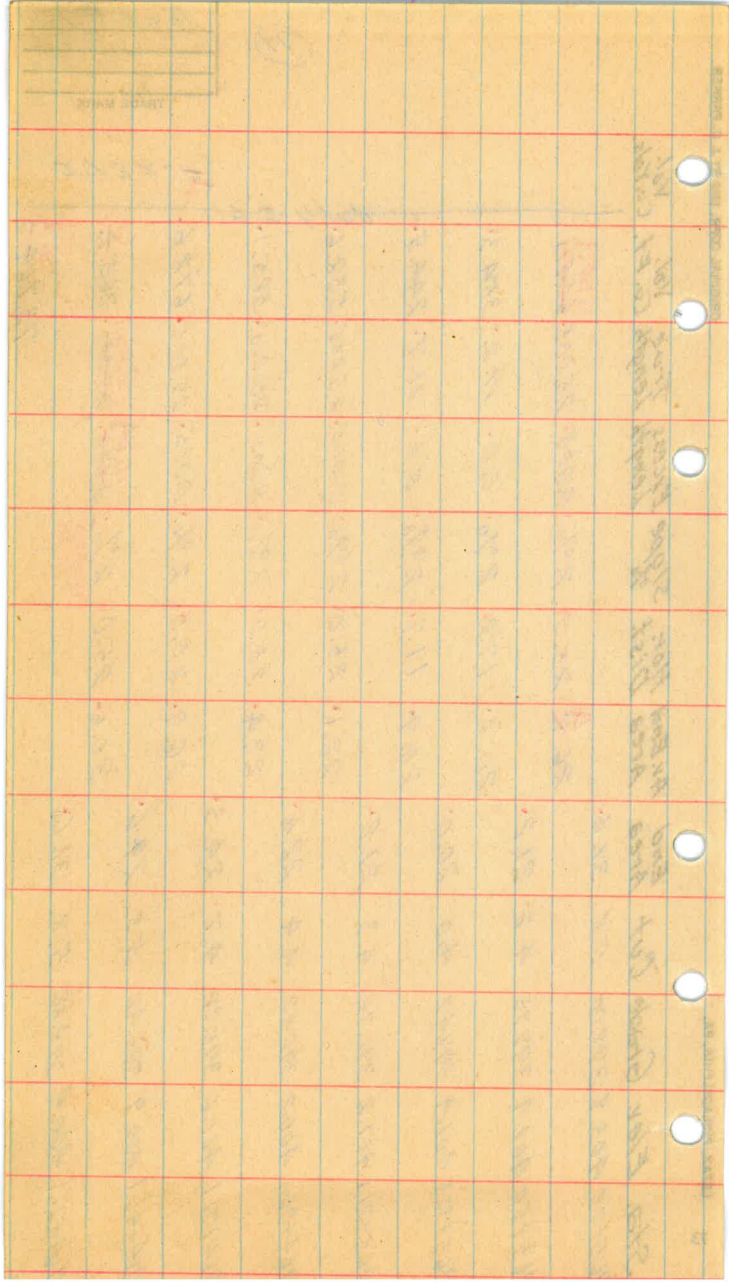
TRADE MARK

8.9  
5.9  
165









3

Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Cu. Yds.
9674241	411.7	406.54	4.9	25.6	25.9	29.1	1%	0.0	29.1	75.37	
967425	411.2	406.25	5.0	26.2	25.6	25.0	1%	0.0	25.0	690.0	
967400	410.8	406.00	4.8	25.0	25.0	25.0	6%	0.04	25.04	626.0	
966775	408.2	404.70	4.8	25.0	25.0	25.0	6%	0.04	25.04	626.0	
966750	407.6	402.50	4.8	25.0	27.6	25.0	6%	0.04	25.04	691.1	
966725	406.8	401.20	5.6	30.2	27.9	25.0	6%	0.04	25.04	698.6	
966700	404.5	399.60	4.9	25.6	28.6	25.0	6%	0.04	25.04	716.1	
965475	403.8	398.00	5.8	31.6							68,934.6

August 23

TRADE MARK

July 26

2590.2

16





Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
969400	403.8	397.50	6.3	35.1	35.8	25.0	9.5%	0.11	25.11	898.9	
968475	406.7	399.88	6.5	36.6	34.8	25.0	9.5%	0.11	25.11	873.8	
968450	408.3	402.25	6.0	33.0	32.3	25.0	9.5%	0.11	25.11	811.1	
968425	410.7	404.63	5.8	31.6	29.9	9.4	9.5%	0.09	9.44	282.3	
968400	410.8	405.52	5.3	28.2	25.0	11.5	9.5%	0.05	11.55	288.8	
968041	410.9	406.61	4.3	21.8	25.0	25.0	9.5%	0.02	25.02	625.5	
967491	412.1	406.79	5.3	28.2	26.9	25.0	1%	0.0	25.0	672.5	
967451	411.7	406.54	4.9	25.6						65,183.1	

July 26

August 23

15

TRADE MARK

24160

DATE	DESCRIPTION	AMOUNT	BALANCE
1/1/20	Opening Balance		100.00
1/5/20	Deposit	50.00	150.00
1/10/20	Withdrawal	20.00	130.00
1/15/20	Deposit	30.00	160.00
1/20/20	Withdrawal	10.00	150.00
1/25/20	Deposit	40.00	190.00
1/30/20	Withdrawal	15.00	175.00
2/5/20	Deposit	25.00	200.00
2/10/20	Withdrawal	30.00	170.00
2/15/20	Deposit	15.00	185.00
2/20/20	Withdrawal	20.00	165.00
2/25/20	Deposit	35.00	200.00
2/30/20	Withdrawal	10.00	190.00
3/5/20	Deposit	20.00	210.00
3/10/20	Withdrawal	25.00	185.00
3/15/20	Deposit	15.00	200.00
3/20/20	Withdrawal	30.00	170.00
3/25/20	Deposit	25.00	195.00
3/30/20	Withdrawal	15.00	180.00
4/5/20	Deposit	30.00	210.00
4/10/20	Withdrawal	20.00	190.00
4/15/20	Deposit	15.00	205.00
4/20/20	Withdrawal	25.00	180.00
4/25/20	Deposit	35.00	215.00
4/30/20	Withdrawal	10.00	205.00
5/5/20	Deposit	20.00	225.00
5/10/20	Withdrawal	30.00	195.00
5/15/20	Deposit	15.00	210.00
5/20/20	Withdrawal	25.00	185.00
5/25/20	Deposit	35.00	220.00
5/30/20	Withdrawal	10.00	210.00
6/5/20	Deposit	20.00	230.00
6/10/20	Withdrawal	30.00	200.00
6/15/20	Deposit	15.00	215.00
6/20/20	Withdrawal	25.00	190.00
6/25/20	Deposit	35.00	225.00
6/30/20	Withdrawal	10.00	215.00
7/5/20	Deposit	20.00	235.00
7/10/20	Withdrawal	30.00	205.00
7/15/20	Deposit	15.00	220.00
7/20/20	Withdrawal	25.00	195.00
7/25/20	Deposit	35.00	230.00
7/30/20	Withdrawal	10.00	220.00
8/5/20	Deposit	20.00	240.00
8/10/20	Withdrawal	30.00	210.00
8/15/20	Deposit	15.00	225.00
8/20/20	Withdrawal	25.00	200.00
8/25/20	Deposit	35.00	235.00
8/30/20	Withdrawal	10.00	225.00
9/5/20	Deposit	20.00	245.00
9/10/20	Withdrawal	30.00	215.00
9/15/20	Deposit	15.00	230.00
9/20/20	Withdrawal	25.00	205.00
9/25/20	Deposit	35.00	240.00
9/30/20	Withdrawal	10.00	230.00
10/5/20	Deposit	20.00	250.00
10/10/20	Withdrawal	30.00	220.00
10/15/20	Deposit	15.00	235.00
10/20/20	Withdrawal	25.00	210.00
10/25/20	Deposit	35.00	245.00
10/30/20	Withdrawal	10.00	235.00
11/5/20	Deposit	20.00	255.00
11/10/20	Withdrawal	30.00	225.00
11/15/20	Deposit	15.00	240.00
11/20/20	Withdrawal	25.00	215.00
11/25/20	Deposit	35.00	250.00
11/30/20	Withdrawal	10.00	240.00
12/5/20	Deposit	20.00	260.00
12/10/20	Withdrawal	30.00	230.00
12/15/20	Deposit	15.00	245.00
12/20/20	Withdrawal	25.00	220.00
12/25/20	Deposit	35.00	255.00
12/30/20	Withdrawal	10.00	245.00

2

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
970+75	381.6	376.00	5.6	32.2	33.4	25.0	16%	0.32	25.32	845.7	
970+50	386.5	380.00	6.5	36.6	34.8	25.0	16%	0.32	25.32	881.1	
970+25	390.0	384.00	6.0	33.0	32.6	25.0	16%	0.32	25.32	825.4	
970+00	393.9	388.00	5.9	32.3	34.8	25.0	9.5%	0.11	25.11	873.8	
969+75	397.0	392.37	6.6	37.3	40.2	25.0	9.5%	0.11	25.11	1009.4	
969+50	400.1	392.75	7.4	43.3	41.8	25.0	9.5%	0.11	25.11	1049.6	
969+25	402.1	395.12	7.0	40.2	37.6	25.0	9.5%	0.11	25.11	944.1	
969+00	403.8	397.50	6.3	35.1						60,730.2	

August

23

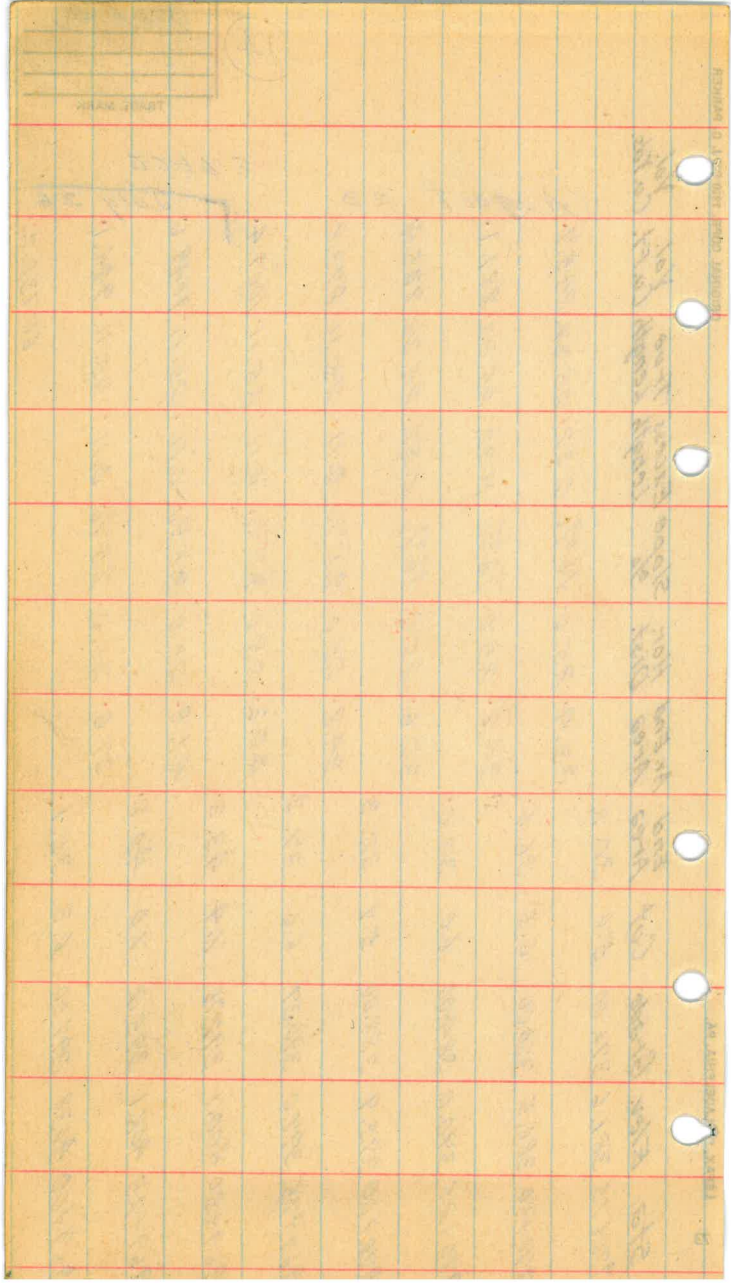
14

TRADE MARK

2249.3

July 26





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Finished Grade  
July 17

13

TRADE MARK

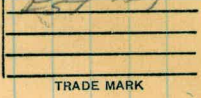
Sta.	Elev.	Grade	Cut	End Area	Ax. End Hor. Dist	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Cu. Yds.
971+75		367.50								
971+50	367.8	367.75	0.0		15.1	14%	0.0	25.0	377.5	
971+25	373.6	368.0	5.6	30.2	33.0	16%	0.32	25.32	835.6	
971+00	378.4	372.00	6.4	35.8	33.0	16%	0.32	25.32	835.6	
970+75	381.6	376.00	5.6	30.2					54,301.1	
									<del>54,303.6</del>	2011.2





Finished Grade  
July 17

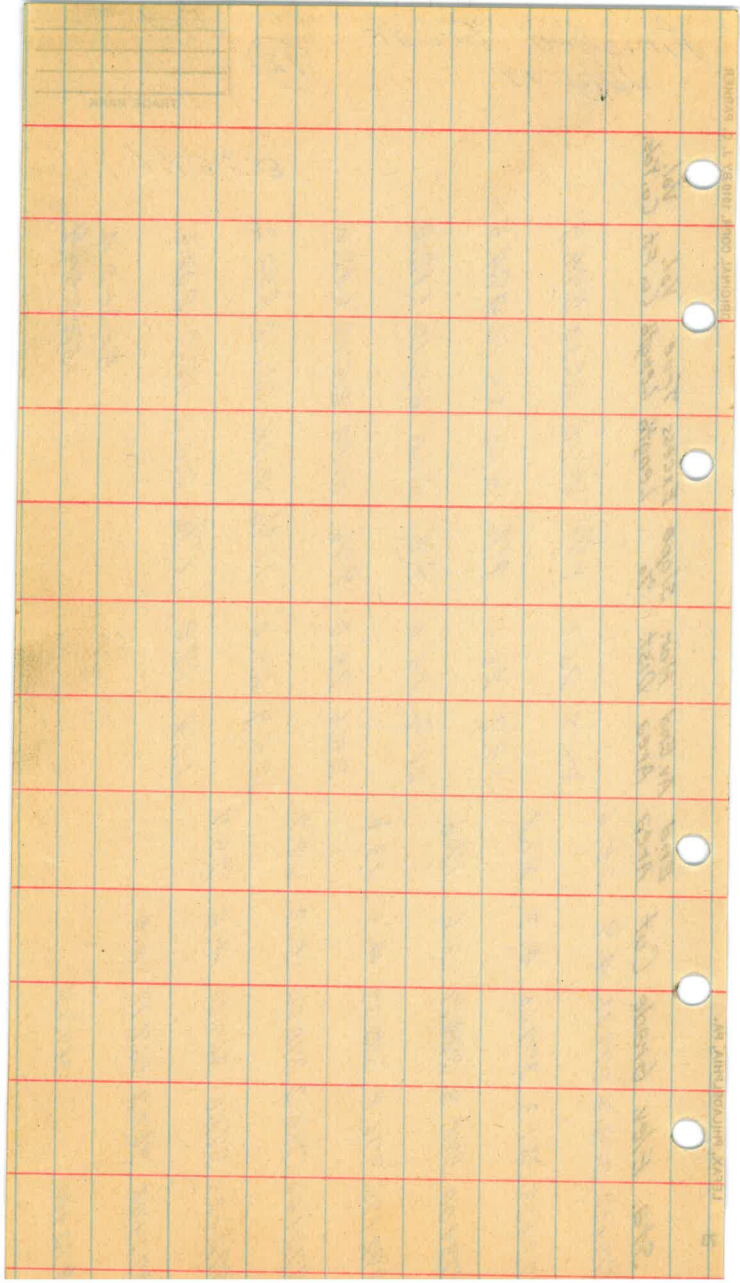
(12)



Sta.	Elev	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
972+50	384.2	372.33	4.9	25.6	23.7	25.0	9%	0.10	25.10	594.9	
973+25	381.3	377.00	4.3	21.8	19.7	25.0	9%	0.10	25.10	494.5	
973+00	378.3	374.67	3.6	17.6	20.4	25.0	9%	0.10	25.10	512.0	
972+75	376.8	372.33	4.5	23.1	25.6	25.0	9%	0.10	25.10	642.6	
972+50	375.3	370.00	5.3	28.2	25.9	25.0	12%	0.18	25.18	652.2	
972+25	371.6	365.00	4.6	23.7	11.8	17.0	1%	0.0	17.0	200.6	
972+00	367.2	367.17	0.0								
972+00		367.25									

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1935/

52,252.4  
-52,554.9



Finished Grade  
July 17

(11)


TRADE MARK

Sta.	Elev. Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Spae %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
973425	391.0	5.0	26.2	28.6	25.0	2%	0.005	25.005	715.1	1820.6
975100	391.3	5.7	30.9	33.4	25.0	2%	0.005	25.005	835.2	
974775	391.6	6.4	35.8	35.8	25.0	2%	0.005	25.005	895.2	
974450	391.2	6.4	35.8	34.0	25.0	2%	0.005	25.005	850.2	
974725	390.3	5.9	32.3	27.7	25.0	2%	0.005	25.005	692.6	
974700	388.5	4.5	23.1	23.4	25.0	9%	0.10	25.10	585.1	
973775	386.3	4.6	23.7	24.6	25.0	9%	0.10	25.10	617.5	
973450	384.2	4.9	25.6						49155.6	
									49158.1	





Finished Grade  
July 17

(10)

TRADE MARK

Sta.	Elev. Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Co. Yds.
97740	392.1	4.9	25.6	25.3	25.0	2%	0.005	25.005	632.6	
976+75	392.4	4.8	25.0	24.0	25.0	2%	0.005	25.005	600.1	
976+50	392.5	4.5	23.0	22.1	25.0	2%	0.005	25.005	552.6	
976+25	391.8	4.2	21.2	24.0	25.0	2%	0.005	25.005	600.1	
976+00	392.3	5.1	26.9	27.2	25.0	2%	0.005	25.005	680.1	
975+75	392.0	5.2	27.6	26.3	25.0	2%	0.005	25.005	657.6	
975+50	391.2	4.8	25.0	25.6	25.0	2%	0.005	25.005	640.1	
975+25	391.0	5.0	26.2						43,964.7	
									43,961.2	

168 8 091

DATE	DESCRIPTION	AMOUNT	CHECK NO.	BANK
10/25	10/25	100.00		
10/26	10/26	100.00		
10/27	10/27	100.00		
10/28	10/28	100.00		
10/29	10/29	100.00		
10/30	10/30	100.00		
10/31	10/31	100.00		
11/01	11/01	100.00		
11/02	11/02	100.00		
11/03	11/03	100.00		
11/04	11/04	100.00		
11/05	11/05	100.00		
11/06	11/06	100.00		
11/07	11/07	100.00		
11/08	11/08	100.00		
11/09	11/09	100.00		
11/10	11/10	100.00		
11/11	11/11	100.00		
11/12	11/12	100.00		
11/13	11/13	100.00		
11/14	11/14	100.00		
11/15	11/15	100.00		
11/16	11/16	100.00		
11/17	11/17	100.00		
11/18	11/18	100.00		
11/19	11/19	100.00		
11/20	11/20	100.00		
11/21	11/21	100.00		
11/22	11/22	100.00		
11/23	11/23	100.00		
11/24	11/24	100.00		
11/25	11/25	100.00		
11/26	11/26	100.00		
11/27	11/27	100.00		
11/28	11/28	100.00		
11/29	11/29	100.00		
11/30	11/30	100.00		
12/01	12/01	100.00		
12/02	12/02	100.00		
12/03	12/03	100.00		
12/04	12/04	100.00		
12/05	12/05	100.00		
12/06	12/06	100.00		
12/07	12/07	100.00		
12/08	12/08	100.00		
12/09	12/09	100.00		
12/10	12/10	100.00		
12/11	12/11	100.00		
12/12	12/12	100.00		
12/13	12/13	100.00		
12/14	12/14	100.00		
12/15	12/15	100.00		
12/16	12/16	100.00		
12/17	12/17	100.00		
12/18	12/18	100.00		
12/19	12/19	100.00		
12/20	12/20	100.00		
12/21	12/21	100.00		
12/22	12/22	100.00		
12/23	12/23	100.00		
12/24	12/24	100.00		
12/25	12/25	100.00		
12/26	12/26	100.00		
12/27	12/27	100.00		
12/28	12/28	100.00		
12/29	12/29	100.00		
12/30	12/30	100.00		
12/31	12/31	100.00		



Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Cu. Yds.
978434	388.9	384.44	4.5	23.0	22.1	25.0	2%	0.005	25.005	552.6	
978438.4	389.1	384.86	4.2	21.2	21.2	25.0	2%	0.005	25.005	530.1	
978438.4	389.5	385.27	4.2	21.2	20.9	25.0	2%	0.005	25.005	522.6	
977488.4	389.8	385.70	4.1	20.6	20.3	13.4	2%	0.003	13.403	272.1	
977475	389.9	385.92	4.0	20.0	24.1	25.0	2%	0.005	25.005	602.6	
977450	391.6	386.34	5.3	28.2	29.2	25.0	2%	0.005	25.005	730.1	
977425	392.4	386.75	5.6	30.2	27.9	25.0	2%	0.005	25.005	697.6	
977400	392.1	387.18	4.9	25.6						39601.5	
										39604.0	

Finished Grade  
July 17

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TRADE MARK

1466.7

DATE	DESCRIPTION	AMOUNT	BALANCE
1/1/20	Opening Balance		100.00
1/5/20	Deposit	50.00	150.00
1/10/20	Withdrawal	20.00	130.00
1/15/20	Deposit	30.00	160.00
1/20/20	Withdrawal	10.00	150.00
1/25/20	Deposit	40.00	190.00
1/30/20	Withdrawal	15.00	175.00
2/5/20	Deposit	25.00	200.00
2/10/20	Withdrawal	35.00	165.00
2/15/20	Deposit	15.00	180.00
2/20/20	Withdrawal	20.00	160.00
2/25/20	Deposit	30.00	190.00
2/30/20	Withdrawal	10.00	180.00
3/5/20	Deposit	45.00	225.00
3/10/20	Withdrawal	25.00	200.00
3/15/20	Deposit	15.00	215.00
3/20/20	Withdrawal	30.00	185.00
3/25/20	Deposit	20.00	205.00
3/30/20	Withdrawal	15.00	190.00
4/5/20	Deposit	35.00	225.00
4/10/20	Withdrawal	20.00	205.00
4/15/20	Deposit	10.00	215.00
4/20/20	Withdrawal	25.00	190.00
4/25/20	Deposit	30.00	220.00
4/30/20	Withdrawal	15.00	205.00
5/5/20	Deposit	40.00	245.00
5/10/20	Withdrawal	30.00	215.00
5/15/20	Deposit	20.00	235.00
5/20/20	Withdrawal	25.00	210.00
5/25/20	Deposit	15.00	225.00
5/30/20	Withdrawal	10.00	215.00
6/5/20	Deposit	30.00	245.00
6/10/20	Withdrawal	20.00	225.00
6/15/20	Deposit	10.00	235.00
6/20/20	Withdrawal	25.00	210.00
6/25/20	Deposit	35.00	245.00
6/30/20	Withdrawal	15.00	230.00
7/5/20	Deposit	25.00	255.00
7/10/20	Withdrawal	35.00	220.00
7/15/20	Deposit	15.00	235.00
7/20/20	Withdrawal	20.00	215.00
7/25/20	Deposit	30.00	245.00
7/30/20	Withdrawal	10.00	235.00
8/5/20	Deposit	45.00	280.00
8/10/20	Withdrawal	25.00	255.00
8/15/20	Deposit	15.00	270.00
8/20/20	Withdrawal	30.00	240.00
8/25/20	Deposit	20.00	260.00
8/30/20	Withdrawal	10.00	250.00
9/5/20	Deposit	35.00	285.00
9/10/20	Withdrawal	20.00	265.00
9/15/20	Deposit	10.00	275.00
9/20/20	Withdrawal	25.00	250.00
9/25/20	Deposit	30.00	280.00
9/30/20	Withdrawal	15.00	265.00
10/5/20	Deposit	40.00	305.00
10/10/20	Withdrawal	30.00	275.00
10/15/20	Deposit	20.00	295.00
10/20/20	Withdrawal	25.00	270.00
10/25/20	Deposit	15.00	285.00
10/30/20	Withdrawal	10.00	275.00
11/5/20	Deposit	30.00	305.00
11/10/20	Withdrawal	20.00	285.00
11/15/20	Deposit	10.00	295.00
11/20/20	Withdrawal	25.00	270.00
11/25/20	Deposit	35.00	305.00
11/30/20	Withdrawal	15.00	290.00
12/5/20	Deposit	25.00	315.00
12/10/20	Withdrawal	35.00	280.00
12/15/20	Deposit	15.00	295.00
12/20/20	Withdrawal	20.00	275.00
12/25/20	Deposit	30.00	305.00
12/30/20	Withdrawal	10.00	295.00

DATE DESCRIPTION AMOUNT BALANCE

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
980+13.5	377.6	373.97	4.1	20.6	24.7	22.1	11%	0.13	22.23	549.1	
980+13.4	381.3	375.93	5.4	28.9	28.2	25.0	11%	0.15	25.15	709.2	
979+88.4	383.9	378.71	5.2	27.6	27.9	25.0	11%	0.15	25.15	701.7	
979+63.4	386.8	381.50	5.3	28.2	30.2	25.0	11%	0.082	25.082	751.5	
979+38.4	389.1	383.19	5.9	32.3	31.6	25.0	2%	0.005	25.005	790.2	
979+13.4	389.3	383.61	5.7	30.9	27.6	25.0	2%	0.005	25.005	690.1	
978+88.4	388.7	384.03	4.7	24.3	23.6	25.0	2%	0.005	25.005	590.1	
978+63.4	388.9	384.44	4.5	23.0						35693.8	1322.0
										<del>35876.3</del>	

Finished Grade  
July 17

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TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
982+00	360.8	355.14	5.7	30.9	29.9	25.0	11%	0.15	25.15	732.0	
981+75	363.3	357.93	5.4	28.9	28.2	25.0	11%	0.15	25.15	734.4	
981+50	366.2	360.71	5.5	29.6	28.9	25.0	11%	0.15	25.15	726.87	
981+25	368.8	363.50	5.3	28.2	27.6	25.0	11%	0.15	25.15	694.1	
981+00	371.4	366.28	5.1	26.9	25.9	25.0	11%	0.15	25.15	657.4	114.1
980+75	373.9	369.07	4.8	25.0	20.7	25.0	11%	0.15	25.15	520.6	
980+50	375.3	371.85	3.4	16.5	18.5	14.5	11%	0.09	14.59	269.9	
980+35.5	377.6	373.97	4.1	20.6						39,905.9	30,908.4

Finished Grade  
July 17

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TRADE MARK





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Finished Grade  
July 17

(6)

TRADE MARK

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
983775	342.9	338.8	3.1	14.8	13.7	25.0	6%	0.04	25.04	343.0	
983750	343.9	341.20	2.7	12.6	14.0	25.0	6%	0.04	25.04	350.6	
983725	345.8	342.60	3.2	15.4	17.7	25.0	6%	0.04	25.04	443.2	
983700	348.0	344.00	4.0	20.0	21.2	25.0	11%	0.15	25.15	533.2	
982775	351.2	346.79	4.4	22.4	22.7	25.0	11%	0.15	25.15	570.9	9 5 86
982750	354.1	349.57	4.5	23.0	26.3	25.0	11%	0.15	25.15	661.4	
982725	357.9	352.36	5.5	29.6	30.2	25.0	11%	0.15	25.15	759.5	
982700	360.8	355.14	5.7	30.9						26,556.7	26,558.2



Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
983+75	342.9	338.8	3.1	14.8	13.7	25.0	6%	0.04	25.04	343.0	
983+50	343.9	341.20	2.7	12.6	14.0	25.0	6%	0.04	25.04	350.6	
983+25	345.8	342.60	3.2	15.4	17.7	25.0	6%	0.04	25.04	443.2	
983+00	348.0	344.00	4.0	20.0	21.2	25.0	11%	0.15	25.15	533.2	
982+75	351.2	346.79	4.4	22.4	22.7	25.0	11%	0.15	25.15	570.9	
982+50	354.1	349.57	4.5	23.0	26.3	25.0	11%	0.15	25.15	661.4	
982+25	357.9	352.36	5.5	29.6	30.2	25.0	11%	0.15	25.15	759.5	
982+00	360.8	355.14	5.7	30.9						26,556.7	26,509.2

Finished Grade  
July 17

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TRADE MARK

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86



DATE	DESCRIPTION	AMOUNT	BALANCE
1912	...	...	...
1913	...	...	...
1914	...	...	...
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1917	...	...	...
1918	...	...	...
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1920	...	...	...
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1922	...	...	...
1923	...	...	...
1924	...	...	...
1925	...	...	...
1926	...	...	...
1927	...	...	...
1928	...	...	...
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1930	...	...	...
1931	...	...	...
1932	...	...	...
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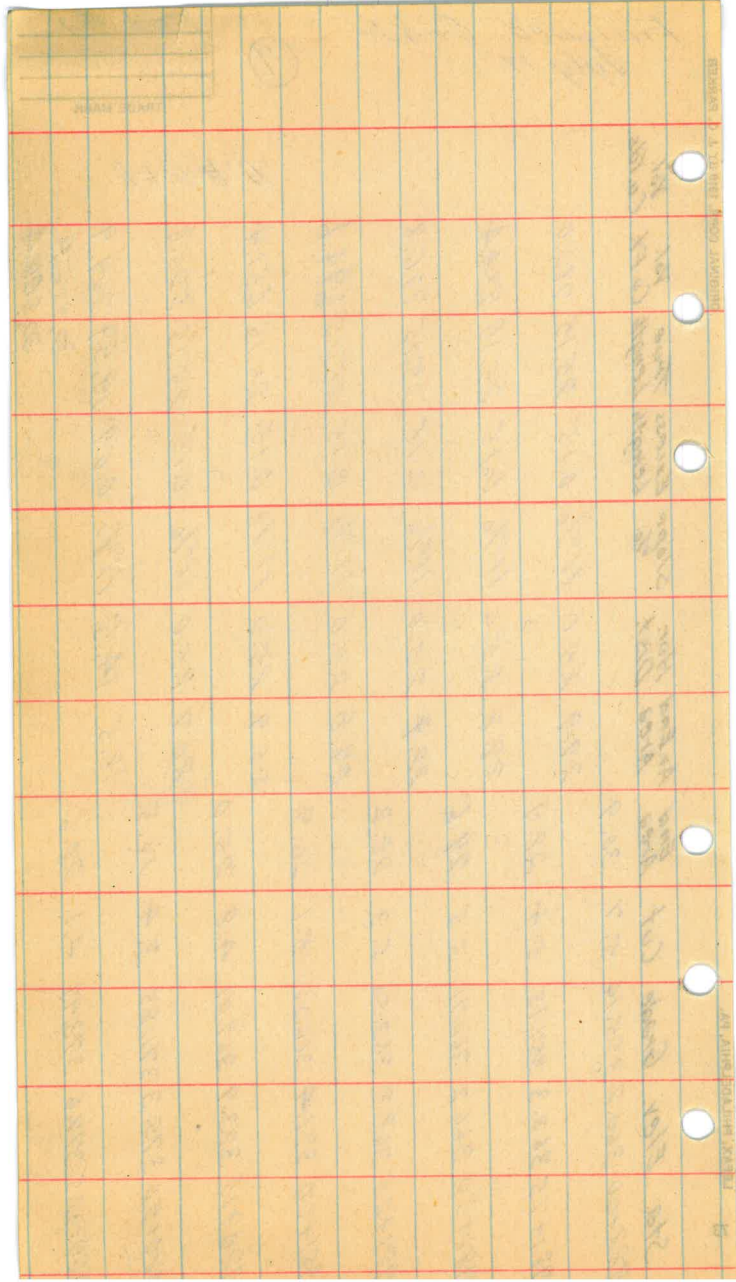
50. FLECK BIRTH 1817-87

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
982+00	360.8	355.14	5.7	30.9	29.9	25.0	11%	0.15	25.15	752.0	
981+75	363.3	357.93	5.4	28.9	29.2	25.0	11%	0.15	25.15	734.4	
981+50	366.2	360.71	5.5	29.6	28.9	25.0	11%	0.15	25.15	726.8	
981+25	368.8	363.50	5.3	28.2	27.6	25.0	11%	0.15	25.15	694.1	
981+00	371.4	366.28	5.1	26.9	25.9	25.0	11%	0.15	25.15	651.4	
980+75	373.9	369.07	4.8	25.0	20.7	25.0	11%	0.15	25.15	520.6	
980+50	375.3	371.85	3.4	16.5	18.5	14.5	11%	0.09	14.59	269.9	
980+35.5	374.6	373.47	4.1	20.6						30,905.9	
										30,988.4	

Finished Grade  
July 17

(7)

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
988+25	310.5	302.00	8.5	52.1.	50.8.	25.0.	32%	1.25.	26.25.	1333.5	✓
988+50	302.2	294.00	8.2	49.6.	47.6	25.0.	32%	1.25.	26.25.	1249.5	✓
988+75	293.7	286.00	7.7	45.6.	37.2.	25.0.	28%	0.96.	25.96.	965.7	✓
989+00	284.4	279.00	5.4	28.9	27.9.	25.0.	28%	0.96.	25.96.	724.3	✓
989+25	277.1	272.00	5.1	26.9.	26.9.	25.0.	28%	0.96.	25.96.	628.3	✓
989+50	270.1	265.00	5.1	26.9.	24.6.	25.0.	22%	0.60.	25.6.	629.8	✓
989+75	263.9	259.50	4.4	22.4.	23.7.	25.0.	22%	0.60.	25.6.	606.7	✓
990+00	258.8	254.00	4.8	25.0.						586.4	✓
										95220.4	✓
										3452.6	✓
										143.0	✓



Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
990+00	256.8	259.00	4.8	25.0	23.1	25.0	22%	0.60	25.6	591.4	✓
990+25	252.7	246.50	4.2	21.2	32.6	25.0	22%	0.60	25.6	834.6	✓
990+50	250.5	243.00	7.5	44.0	41.8	25.0	22%	0.60	25.6	1070.1	✓
990+75	244.4	237.50	6.9	39.5	33.6	25.0	22%	0.60	25.6	860.2	✓
991+00	237.2	232.00	5.2	27.6	13.8	30.0	24%	0.08	30.08	415.1	✓
991+20	234.0	230.04	0.0	0.0	0.0						
992+05	230.6	230.64	0.0	0.0	0.0						

TRADE MARK

22

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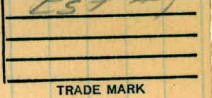
88,682.8  
~~94,997.8~~





Sta.	Elev.	Grade	Cut	End Area	Average Area	Horizontal Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
992+05	230.6	230.64	0.0	0.0	4.5	20.0	1%	0.0	20.0	90.0	✓
992+25	232.8	230.80	2.0	9.0	17.6	25.0	1%	0.0	25.0	490.0	✓
992+50	236.0	231.00	5.0	26.2	23.7	25.0	9%	0.10	25.10	594.9	
992+75	237.4	233.25	4.2	21.2	21.8	25.0	9%	0.10	25.10	547.2	
993+00	239.9	235.50	4.4	22.4	21.8	25.0	9%	0.10	25.10	547.2	
993+25	241.9	237.75	4.2	21.2	23.1	25.0	9%	0.10	25.10	579.8	
993+50	244.8	240.00	4.8	25.0	28.6	32.1	2%	0.006	32.106	918.2	
993+82	246.5	240.64	5.9	32.3						92,357.1	
										408,709.1	

3,730.0  
3,420.4







Sta.	Elev.	Grade	Cut Area	End Area	Hor. Dist.	Slope %	Excess Length	Proc. Length	Vol. Cu. Ft.	Vol. Co. Yds.
993+82.1	246.5	240.64	5.9	32.3	25.0	2%	0.005	25.005	807.7	✓
994+09.1	246.5	240.61	5.9	32.3	25.0	6%	0.04	25.04	826.3	✓
994+32.1	245.3	239.21	6.1	33.7	17.9	6%	0.03	17.93	636.5	✓
994+50	244.8	238.20	6.6	37.3	25.0	6%	0.04	25.04	731.2	✓
994+75	241.0	236.80	4.2	21.2	25.0	6%	0.04	25.04	445.7	✓
995+00	238.4	235.40	3.0	14.3	25.0	6%	0.04	25.04	415.7	✓
995+25	237.8	234.00	3.8	18.8	25.0	1%	0.0	25.0	413.2	✓
995+50	238.0	233.81	4.1	20.6	25.0	0.0	0.0	25.0	492.5	✓
									196,705.7	
									705,064.2	



Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
995750	238.0	233.87	4.1	20.6	26.1	25.0	1%	0.0	25.0	652.5	✓
995775	239.6	233.75	5.8	31.6	35.2	25.0	1%	0.0	25.0	880.0	✓
996100	240.5	233.67	6.8	38.8	40.3	25.0	1%	0.0	25.0	1007.5	✓
996125	240.7	233.50	7.2	41.8	39.8	25.0	1%	0.0	25.0	990.0	✓
996150	240.0	233.37	6.6	37.3	33.1	25.0	1%	0.0	25.0	827.5	✓
996175	238.6	233.25	5.4	28.9	40.0	25.0	1%	0.0	25.0	1000.0	✓
997100	241.5	233.12	8.4	51.2	52.9	25.0	1%	0.0	25.0	1322.5	✓
997125	241.8	233.00	8.8	54.6						103 386.7	✓

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GRAM SCALE

BRONKHORST HIGH Purity Air

BRONKHORST HIGH Purity Air

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
997+25	241.8	233.00	8.8	54.6	54.2	25.0	8%	0.08	25.08	1352.3	✓
997+50	238.7	231.00	8.7	53.7	46.6	25.0	8%	0.08	25.08	1168.7	✓
997+75	235.9	229.00	6.9	39.5	32.6	25.0	8%	0.08	25.08	817.6	✓
998+00	231.9	227.00	4.9	25.6	45.8	25.0	1%	0.0	25.0	1145.0	✓
998+25	236.9	226.83	10.1	65.9	66.4	25.0	1%	0.0	25.0	1660.0	✓
998+50	236.9	226.67	10.2	66.8	57.8	25.0	1%	0.0	25.0	1445.0	✓
998+75	234.6	226.50	8.1	48.8	42.7	25.0	1%	0.0	25.0	1067.5	✓
999+00	232.8	226.33	6.5	36.6						112,048.8	
										120,405.3	
										4,459.5	✓
										9150.0	✓

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Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.
985+50	333.6	330.00	3.6	17.6	25.0	1%	0.0	25.0	377.5
985+75	332.4	329.67	2.7	12.6	25.0	1%	0.0	25.0	265.0
986+00	331.2	329.33	1.9	9.5	25.0	1%	0.0	25.0	245.0
986+25	331.4	329.00	2.4	11.0	25.0	1%	0.0	25.0	335.0
986+50	332.0	328.67	3.3	15.9	25.0	1%	0.0	25.0	121,027.0

9952.5

29

FST 1

TRADE MARK



Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1007422.8	340.9	336.30	4.6	23.7	23.7	7.8	7%	0.02	7.82	183.0	
1008100											
1008107.0	342.5	338.05	4.5	23.1	21.8	25.0	7%	0.06	25.06	546.3	
1008133.8	343.9	339.80	4.1	20.6	24.1	25.0	7%	0.06	25.06	603.9	
1008157.8	346.8	341.55	5.2	27.6	27.9	25.0	7%	0.06	25.06	699.2	
1008182.8	348.6	342.30	5.3	28.2	28.9	7.7	7%	0.02	7.72	223.1	4621.1
1008190.5	349.3	343.84	5.5	29.6	29.9	25.0	7%	0.06	25.06	749.3	
1009115.5	351.2	345.59	5.6	30.2	29.9	25.0	7%	0.06	25.06	749.3	
1009140.5	352.8	347.34	5.5	29.6						124,781.1	

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557 41

TRADE MARK



Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns by the red lines. At the top left, there is a small grid or table structure. On the right side, there are four circular punch holes. At the bottom of the page, there is a small printed label that reads "2. GRADE UNIVERSITÄT W.".

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Con. Yds.
1008+40.5	352.8	347.34	5.5	29.6	28.2	25.0	7%	0.02	25.02	730.6	
1009+65.5	353.8	348.36	5.4	28.9	28.9	25.0	2%	0.005	25.005	722.6	
1010+90.5	354.3	348.94	5.4	28.9	28.2	25.0	2%	0.005	25.005	705.1	
1010+15.5	354.7	349.52	5.2	27.6	28.6	25.0	2%	0.005	25.005	715.1	
1010+40.5	355.6	350.11	5.5	29.6	29.6	25.0	2%	0.005	25.005	740.1	
1010+65.5	356.2	350.69	5.5	29.6	29.9	25.0	2%	0.005	25.005	747.6	
1010+90.5	356.9	351.27	5.6	30.2	30.9	12.2	2%	0.0	12.2	377.0	
1011+02.7	357.4	351.56	5.8	31.6						129,519.2	

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F57 41

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1011+20	357.9	357.56	5.8	31.6	32.3	22.3	2%	0.005	22.305	720.5	✓
1011+25	358.1	352.08	6.0	33.0	32.3	25.0	2%	0.005	25.005	807.7	✓
1011+50	358.5	352.66	5.8	31.6	28.6	25.0	2%	0.005	25.005	715.1	✓
1011+75	358.1	353.25	4.9	25.6	26.2	25.0	2%	0.005	25.005	655.1	✓
1012+00	358.9	353.83	5.1	26.9	28.6	25.0	2%	0.005	25.005	715.1	✓
1012+25	360.0	354.41	5.6	30.2	24.8	25.0	2%	0.005	25.005	620.1	✓
1012+50	358.9	355.00	3.9	19.4	20.6	25.0	1%	—	25.0	515.0	✓
1012+75	359.6	355.31	4.3	21.8						134,267.8	

6' 5" 166'



Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1012+75	359.6	355.31	4.3	21.8	25.0	1%	0.0	25.0	660.0	✓
1013+00	361.3	355.62	5.7	30.9	25.0	1%	0.0	25.0	722.5	✓
1013+25	361.0	355.92	5.1	26.9	25.0	1%	0.0	25.0	672.5	✓
1013+50	361.3	356.23	5.1	26.9	25.0	1%	0.0	25.0	650.0	✓
1013+75	361.3	356.54	4.8	25.0	25.0	1%	0.0	25.0	562.5	✓
1014+00	360.8	356.85	4.0	20.0	25.0	1%	0.0	25.0	575.1	✓
1014+25	361.4	357.16	4.2	21.2	25.0	1%	0.0	25.0	610.0	✓
1014+50	362.7	357.46	5.2	27.6	25.0	1%	0.0	25.0	138,660.4	✓

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F5741

TRADE MARK

9 58 1/2



Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns by the red margin lines. At the top left, there is a small rectangular box with a grid pattern. At the top center, there is a faint circular stamp. On the right side of the page, there are four circular punch holes. At the bottom of the page, there is a small rectangular stamp that reads "THE UNIVERSITY OF CHICAGO" and "THE DIVISION OF PHYSICAL SCIENCES".

Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1014+50	362.7	357.46	5.2	29.6	28.6	25.0	17%	0.0	25.0	715.0	✓
1014+75	363.3	357.77	5.5	29.6	26.4	25.0	17%	0.0	25.0	660.0	✓
1015+00	362.6	358.08	4.5	23.1	28.4	25.0	17%	0.0	25.0	710.0	✓
1015+25	364.5	358.39	6.1	33.7	26.2	25.0	17%	0.0	28.0	655.0	✓
1015+50	362.5	358.69	3.8	18.8	24.5	25.0	17%	0.0	25.0	612.5	✓
1015+75	364.6	358.00	5.6	30.2	27.2	25.0	10%	0.0	25.0	680.0	✓
1016+00	363.4	358.71	4.7	24.3	21.8	25.0	17%	0.0	25.0	545.0	✓
1016+25	362.3	358.42	3.9	19.4						143,237.9	✓

(34)

Est 71

TRADE MARK

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in blue ink and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns. At the top left, there is a small rectangular box containing some faint markings. On the right side of the page, there are four circular punch holes. The paper is placed on a white background.



7

LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1016+25	362.3	358.92	3.9	19.4	24.8	25.0	1%	0.0	25.0	620.0	✓
1016+50	363.7	358.13	5.6	30.2	24.8	25.0	1%	0.0	25.0	620.0	✓
1016+75	361.7	357.83	3.9	19.4	19.7	25.0	1%	0.0	25.0	492.5	✓
1017+00	361.5	357.54	4.0	20.0	32.0	25.0	1%	0.0	25.0	800.0	✓
1017+25	364.7	357.24	7.5	44.0	33.8	25.0	1%	0.0	25.0	845.0	✓
1017+50	361.6	356.95	4.6	23.7	21.8	25.0	1%	0.0	25.0	545.0	✓
1017+75	360.7	356.66	4.0	20.0	29.0	25.0	1%	0.0	25.0	725.0	✓
1018+00	363.1	356.36	6.7	38.0					147,	885.4	✓

(35)

TRADE MARK

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns. At the top left, there is a small grid or table structure. On the right side, there are four circular punch holes. The paper is mounted on a white background.

3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1018+00	363.1	356.36	6.7	38.0	31.8	25.0	1%	0.0	25.0	795.0	✓
1018+25	361.0	356.07	4.9	25.6	25.9	25.0	1%	0.0	25.0	647.5	✓
1018+50	360.8	355.76	5.0	26.2	25.2	25.0	1%	0.0	25.0	630.0	✓
1018+75	360.2	355.47	4.7	24.3	26.6	25.0	1%	0.0	25.0	665.0	✓
1019+00	360.6	355.18	5.4	28.9	31.6	25.0	1%	0.0	25.0	790.0	✓
1019+25	361.1	354.88	6.2	34.4	30.0	25.0	1%	0.0	25.0	750.0	✓
1019+50	359.5	354.59	4.9	25.6	27.9	25.0	1%	0.0	25.0	697.5	✓
1019+75	359.9	354.29	5.6	30.2						152,860.4	

(36)

Est #1

TRADE MARK



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Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Co. Yds.
1019+75	359.9	354.29	0.6	30.2	26.3	25.0	1%	0.0	25.0	657.5
1020+00	358.4	354.00	4.4	22.4	23.0	25.0	2%	0.005	25.005	575.1
1020+25	358.1	353.50	4.6	23.7	29.0	25.0	2%	0.005	25.005	725.1
1020+50	359.2	353.00	6.2	34.4	32.6	25.0	2%	0.005	25.005	815.2
1020+75	358.2	352.50	5.7	30.9	27.6	25.0	2%	0.005	25.005	690.1
1021+00	356.7	352.00	4.7	24.3	24.0	25.0	2%	0.005	25.005	600.1
1021+25	356.1	351.50	4.6	23.7	24.0	25.0	2%	0.005	25.005	600.1
1021+50	355.7	351.00	4.7	24.3					157,523.6	

(37)

N 78° 25'

TRADE MARK

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns. At the top left, there is a small rectangular box containing a grid pattern. On the right side of the page, there are four circular punch holes. At the bottom of the page, there is a small rectangular stamp or label with some faint text.



Sta.	Elev.	Grade Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Cu. Yds.
1021+50	355.7	351.00	4.7	24.3	28.6	25.0	—	25.0	715.0	✓
1021+75	356.9	350.90	6.0	33.0	29.6	25.0	—	25.0	740.0	✓
1022+00	355.8	350.80	5.0	26.2	26.6	25.0	—	25.0	665.0	✓
1022+25	355.8	350.70	5.1	26.9	27.6	25.0	—	25.0	690.0	✓
1022+50	355.9	350.60	5.3	28.2	24.7	25.0	—	25.0	617.5	✓
1022+75	354.9	350.50	4.2	21.2	31.1	25.0	—	25.0	777.5	✓
1023+00	357.5	350.40	7.1	41.0	34.0	25.0	—	25.0	850.0	✓
1023+25	355.4	350.30	5.1	26.9				162,578.6		

38

TRADE MARK



Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1023725	355.4	352.30	5.1	26.9	25.6	25.0	—	—	25.0	640.0	✓
1023750	354.9	352.20	4.7	24.3	24.3	25.0	—	—	25.0	607.5	✓
1023775	354.8	352.10	4.7	24.3	24.6	25.0	—	—	25.0	615.0	✓
1024700	354.8	352.00	4.8	25.0	25.3	25.0	—	—	25.0	632.5	✓
1024725	354.8	349.90	4.9	25.6	26.2	25.0	—	—	25.0	655.0	✓
1024750	354.9	349.80	5.1	26.9	35.8	25.0	—	—	25.0	895.0	✓
1024775	357.3	349.70	7.6	44.8	39.2	25.0	—	—	25.0	980.0	✓
1025700	355.7	349.60	6.1	33.7					167	603.6	✓

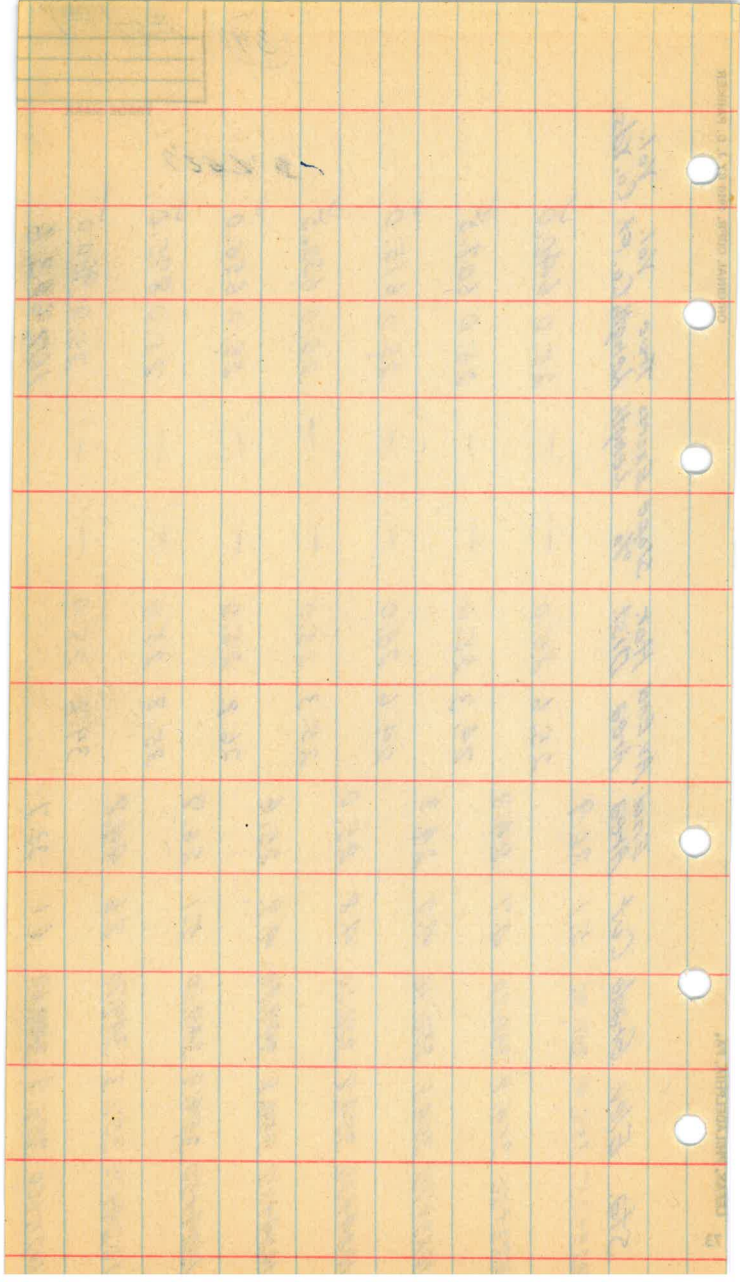
39

TRADE MARK

EST #1

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Sta.	Elev.	Grade	Cut	End Area	Avg. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1025+00	355.7	349.60	6.1	33.7	29.6	25.0	-	-	25.0	740.0	✓
1025+25	354.9	349.50	4.9	25.6	25.3	25.0	-	-	25.0	632.5	✓
1025+50	354.2	349.40	4.8	25.0	25.6	25.0	-	-	25.0	640.0	✓
1025+75	354.3	349.30	5.0	26.2	32.5	25.0	-	-	25.0	812.5	✓
1026+00	356.0	349.20	6.8	38.8	32.5	25.0	-	-	25.0	812.5	✓
1026+25	354.1	349.10	5.0	26.2	26.6	25.0	-	-	25.0	665.0	✓
1026+50	354.1	349.00	5.1	26.9	25.3	25.0	20%	0.005	25.105	632.6	✓
1026+75	353.2	348.56	4.6	23.7						172.538.7	

(40)

TRADE MARK

6,390.5





Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	T-ave Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1027175	353.2	348.58	4.6	23.7	25.3	25.0	2%	0.005	25.005	637.6	✓
1027100	353.2	348.13	5.1	26.9	27.6	25.0	2%	0.005	25.005	690.1	✓
1027125	353.0	347.69	5.3	28.2	34.6	25.0	2%	0.005	25.005	865.2	✓
1027150	354.3	347.25	7.1	41.0	36.6	25.0	2%	0.005	25.005	915.2	✓
1027175	352.7	346.81	5.9	32.3	36.2	25.0	2%	0.005	25.005	905.2	✓
1028100	353.4	346.38	7.0	40.2	39.8	25.0	2%	0.005	25.005	995.2	✓
1028125	352.8	345.94	6.9	39.5	35.6	25.0	2%	0.005	25.005	890.2	✓
1028150	351.3	345.50	5.8	31.6						178,432.4	

(41)

Est #1

TRADE MARK

9'809'9



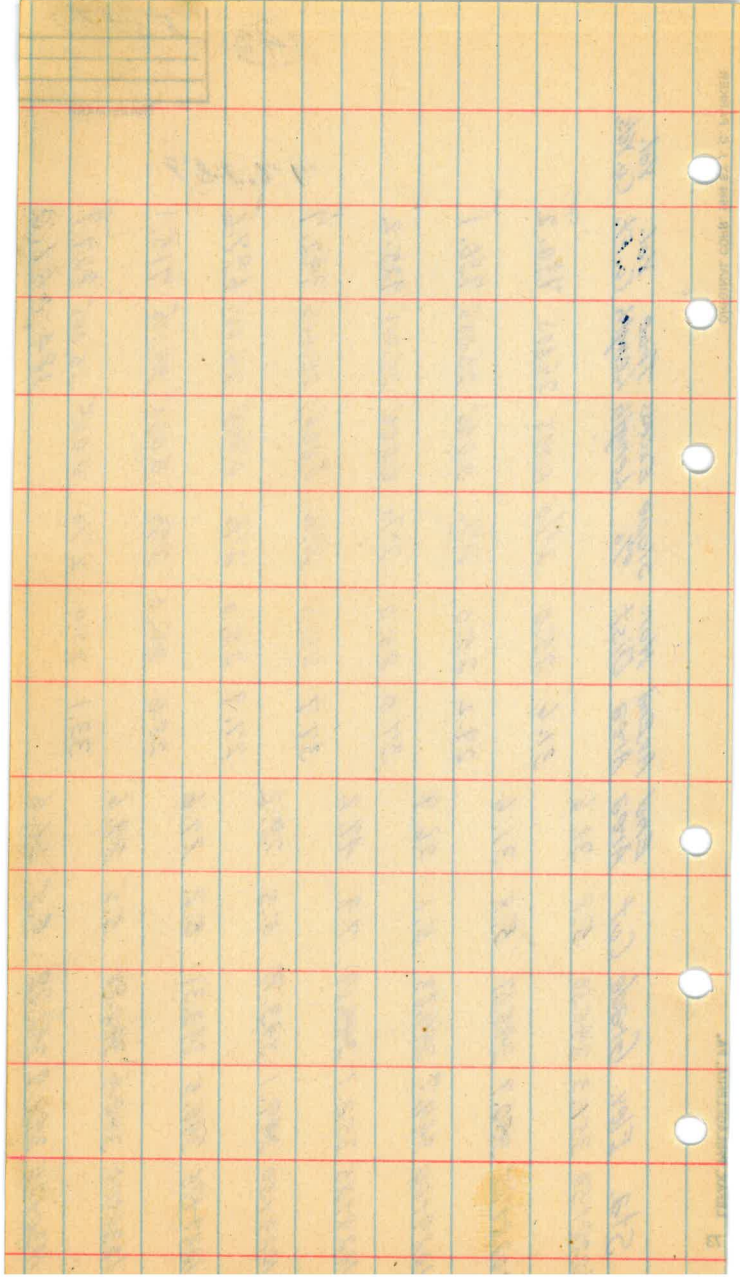
Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	Tree Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1028+50	351.3	345.50	5.8	31.6	31.6	25.0	2%	0.005	25.005	790.2	✓
1028+75	350.9	345.07	5.8	31.6	29.2	25.0	2%	0.005	25.005	730.1	✓
1029+00	349.7	344.63	5.1	26.9	37.0	25.0	2%	0.005	25.005	925.2	✓
1029+25	352.1	344.19	7.9	47.2	37.7	25.0	2%	0.005	25.005	942.7	✓
1029+50	349.1	343.75	5.3	28.2	27.9	25.0	2%	0.005	25.015	697.6	✓
1029+75	348.5	343.31	5.2	27.6	28.6	25.0	2%	0.005	25.105	715.1	✓
1030+00	348.4	342.88	5.5	29.6	33.1	25.0	2%	0.005	25.005	827.7	✓
1030+25	348.9	342.88	6.5	36.6					184,061.0		

(42)

EST 41  
TRADE MARK

176189





Sta	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	Tree Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1030+25	348.9	342.94	6.5	36.6	33.4	6.2	2%	0.0	6.2	207.1	✓
1030+31.2	347.9	342.33	5.6	30.2	32.6	25.0	2% 1030+50 4%	0.005	25.005	815.2	✓
1030+56.2	348.1	341.75	6.3	35.1	33.7	25.0	4%	0.02	25.02	843.2	✓
1030+61.2	346.7	340.75	5.9	32.3	32.0	25.0	4%	0.02	25.02	800.6	✓
1031+06.2	345.6	339.75	5.8	31.6	27.6	25.0	4%	0.02	25.02	690.6	✓
1031+31.2	343.4	338.75	4.6	23.7	25.6	18.7	4%	0.02	18.72	479.2	✓
1031+50	343.2	338.00	5.2	27.6	27.6	25.0	4%	0.02	25.02	690.6	✓
1031+75	342.2	337.00	5.2	27.6	27.6	25.0	4%	0.02	25.02	188,587.5	✓

43

Page 41  
TRADE MARK

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and the age of the document. The notes are organized into several columns, with some lines starting with numbers like '18', '19', '20', '21', '22', '23', '24', '25', '26', '27', '28', '29', '30', '31', '32', '33', '34', '35', '36', '37', '38', '39', '40', '41', '42', '43', '44', '45', '46', '47', '48', '49', '50'. There are also some larger numbers like '1000' and '10000' visible. The paper has four circular punch holes along the right edge. At the bottom right, there is a small printed text: "The University of Chicago Press" and "Chicago, Ill., U.S.A.".

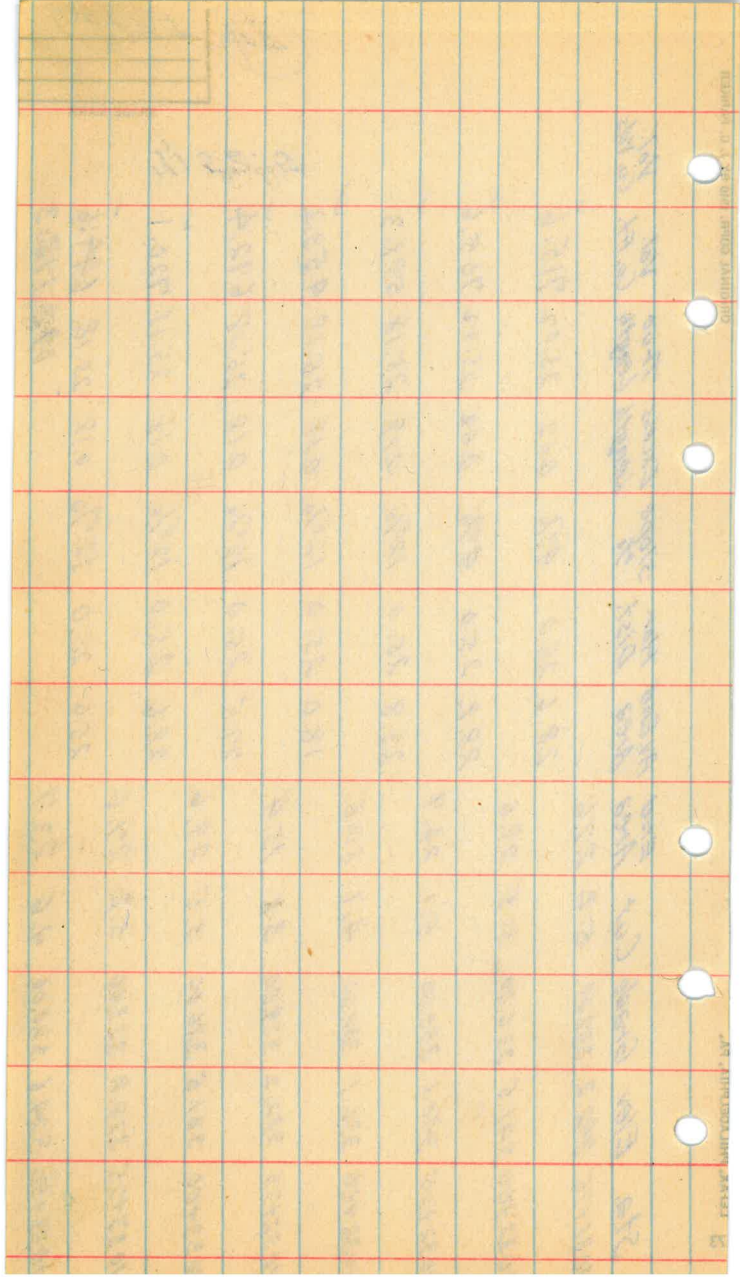


Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	Tree Length	Vol. Co. Ft.	Vol. Cu. Yds.
1031+75	342.2	332.00	5.2	27.6	28.6	25.0	4%	0.02	25.02	715.6	✓
1032+00	341.5	336.00	5.5	29.6	28.2	25.0	4%	0.02	25.02	705.6	✓
1032+25	340.1	335.00	5.1	26.9	23.8	25.0	12%	0.18	25.18	599.3	✓
1032+50	336.1	332.00	4.1	20.6	18.0	25.0	12%	0.18	25.18	453.2	✓
1032+75	332.2	328.00	3.2	15.4	27.5	25.0	12%	0.18	25.18	692.4	✓
1033+00	331.5	326.00	5.5	29.6	28.6	25.0	12%	0.18	25.18	720.1	✓
1033+25	328.2	323.00	5.2	27.6	25.6	25.0	12%	0.19	25.18	644.6	✓
1033+50	324.6	320.00	4.6	23.7					193.18.3		✓

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Est #1

TRADE MARK



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LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope	Excess Length	True Length	Vol. Cu.Yds
1033150	324.6	320.00	4.6	23.7	25.6	25.0	16%	0.32	25.32 648.2 ✓
1033775	321.2	316.00	5.2	27.6	30.3	25.0	16%	0.32	25.32 767.2 ✓
1034100	318.0	312.00	6.0	33.0	28.0	25.0	16%	0.32	25.32 709.0 ✓
1034425	312.5	308.00	4.5	23.1	11.6	7.0	27%	0.0	7.0 81.2 ✓
1034732	307.9	307.99	0.0						
1035100	306.8	306.80	0.0						
1035425	310.3	306.40	3.9	19.4	9.7	25.0	27%	0.005	25.005 242.5 ✓
1035750	314.5	306.00	4.5	23.1	21.2	25.0	27%	0.005	25.005 530.1 ✓

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TRADE MARK

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196,096.5





LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 P. I. C. PARKER

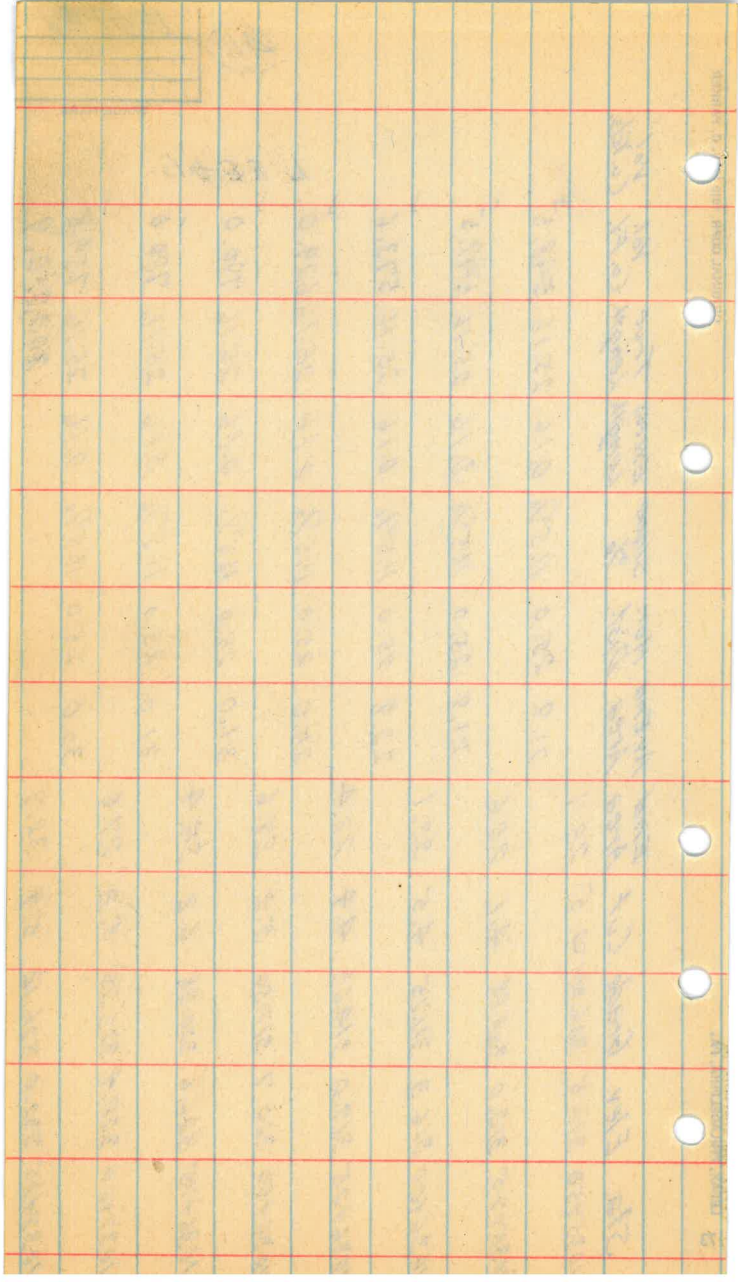
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Sta.	Elev.	Grade	Cut	End Area	Ave End Area	Hor. Dist.	Sigae %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1035750	310.5	306.00	4.5	23.1	21.8	25.0	11.5%	0.16	25.16	548.5	
1035775	313.0	308.88	4.1	20.6	21.8	25.0	11.5%	0.16	25.16	548.5	
1036100	316.3	311.75	4.5	23.1	22.8	25.0	11.5%	0.16	25.16	573.6	
1036125	319.0	314.63	4.4	22.4	25.0	25.0	11.5%	0.16	26.16	629.0	
1036150	322.7	317.50	5.2	27.6	31.0	25.0	11.5%	0.16	25.16	780.0	143.7
1036175	326.6	320.38	6.2	34.4	31.0	25.0	11.5%	0.16	25.16	780.0	
1037100	328.7	323.25	5.2	27.6	30.0	25.0	11.5%	0.16	25.16	754.8	
1037125	332.0	326.12	5.9	32.3					200.710.9		

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EST 71

TRADE MARK

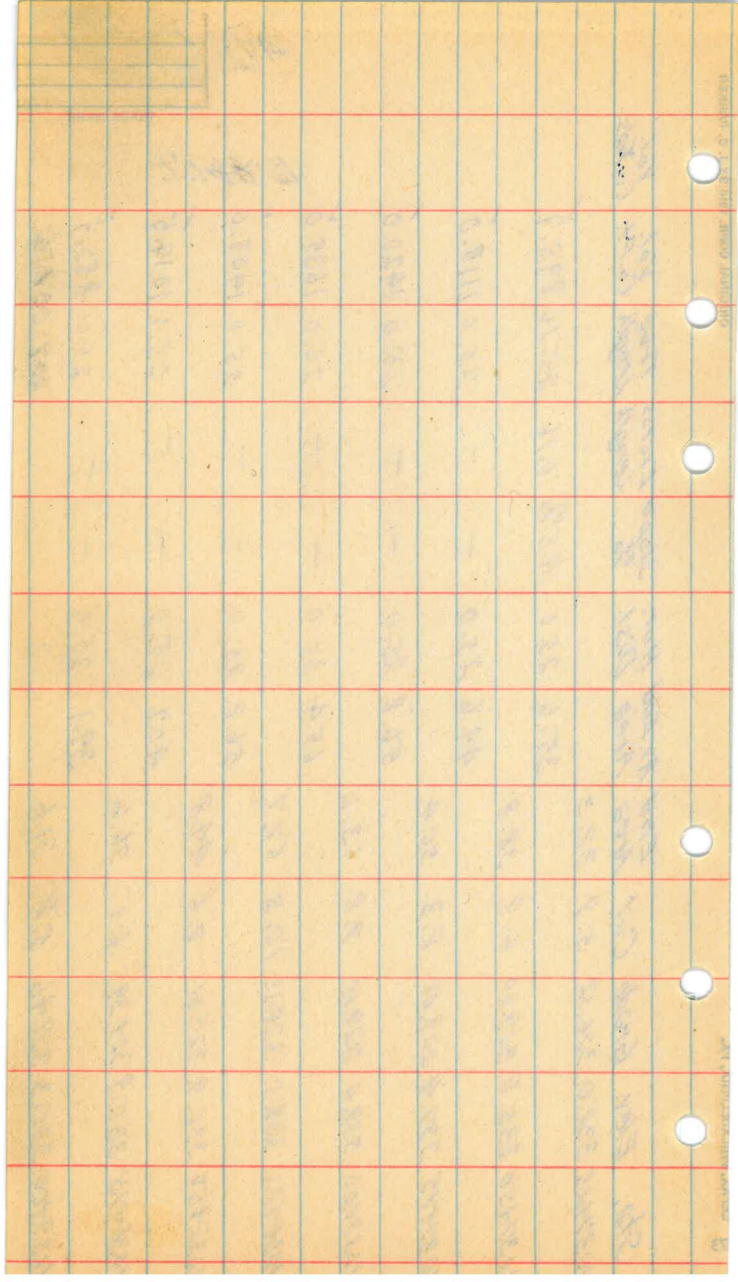


Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1037425	332.0	326.12	5.9	32.3	25.0	11.5%	0.16	25.16	895.7	✓
1037450	335.8	329.00	6.8	38.8	25.0	—	—	25.0	1115.0	✓
1037475	337.4	329.08	8.3	50.4	25.0	—	—	25.0	1420.0	✓
1037400	339.0	329.15	9.8	63.2	25.0	—	—	25.0	1635.0	✓
1037425	339.5	329.23	10.3	67.7	25.0	—	—	25.0	1405.0	✓
1037450	336.9	329.31	7.6	44.8	25.0	—	—	25.0	1017.5	✓
1037475	335.9	329.39	6.5	36.6	25.0	—	—	25.0	852.5	✓
1037400	335.3	329.46	5.8	31.6	25.0	—	—	209.05	851.6	✓

(47)

Est #1

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1039+00	335.3	329.46	5.8	31.6	25.5	25.0	-	-	25.0	637.5	-
1039+25	333.4	329.54	3.9	19.4	14.7	25.0	-	-	25.0	367.5	-
1039+50	331.8	329.62	2.2	10.0	5.0	11.0	-	-	11.0	55.0	-
1039+61	329.6	329.65	0.0				-	-			
1040+58	330.0	329.95	0.0		15.1	17.0	-	-	17.0	256.7	6.998 1/4
1040+75	335.6	330.00	5.6	30.2	35.2	25.0	15%	0.28	25.28	889.9	-
1041+00	340.8	333.75	7.0	40.2	44.1	25.0	15%	0.28	25.28	1114.8	-
1041+25	345.5	337.50	8.0	48.0						212,378.0	-



Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
104125	346.5	331.50	8.0	48.0	44.1	25.0	15%	0.28	25.28	114.8	
104150	348.2	341.25	7.0	40.2	32.9	25.0	15%	0.28	25.28	83.17	
104175	349.9	345.00	4.9	25.6	25.9	25.0	4%	0.02	25.02	648.0	
104200	351.0	346.00	5.0	26.2	26.9	25.0	4%	0.02	25.02	673.0	
104225	352.2	347.00	5.2	27.6	28.6	25.0	4%	0.02	25.02	715.6	
104250	353.5	348.00	5.5	29.6	27.9	25.0	4%	0.02	25.02	698.1	
104275	354.0	349.00	5.0	26.2	24.6	25.0	4%	0.02	25.02	615.5	
104300	354.5	350.00	4.5	23.1						217.66	9.7

(49)

8-1908

TRADE MARK

557 71





Sta.	Elev. Grade	Cut	End Area	Avg. End Area	Hor. Dist.	Slope %	Excav. Length	Trac. Length	Vol. Co. Vols.	Vol. Co. Vols.
1043700	354.5	352.00	4.5	23.1	26.6	25.0	—	25.0	665.0	✓
1043725	355.5	349.88	5.6	30.2	33.0	25.0	—	20.0	825.0	✓
1043750	356.2	349.75	6.4	35.8	34.4	25.0	—	25.0	860.0	✓
1043775	355.76	349.62	6.0	33.0	32.3	25.0	—	25.0	807.5	✓
1044700	355.3	349.50	5.8	31.6	32.6	25.0	—	25.0	815.0	✓
1044725	355.5	349.38	6.1	33.7	31.3	25.0	—	25.0	782.5	✓
1044750	354.6	349.25	5.4	28.9	26.3	25.0	—	25.0	657.5	✓
1044775	354.5	349.12	5.4	28.9	28.9	25.0	—	25.0	722.5	✓
								223	1472	

50

TRADE MARK

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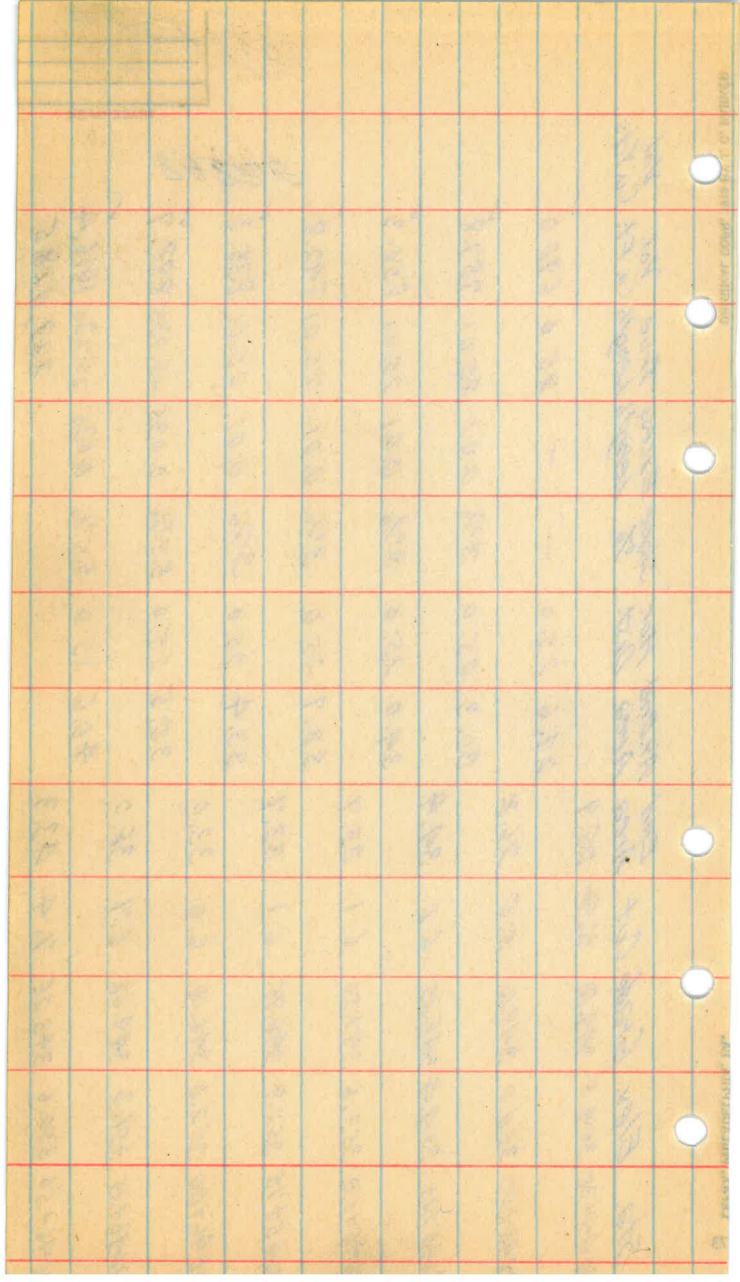
DATE	DESCRIPTION	AMOUNT	CHECK NO.	BANK	INITIALS
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Sta.	Elev.	Grade Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu Yds.	Vol. Cu Yds.
1044775	354.5	342.12	5.4	28.9	21.6	25.0	-	25.0	690.0	✓
1045100	354.0	349.16	5.0	26.2	30.3	25.0	3%	0.01	25.01	757.8
1045725	354.4	348.25	6.2	34.4	34.0	25.0	3%	0.01	25.01	850.3
1045750	353.6	347.50	6.1	33.7	33.7	25.0	3%	0.01	25.01	842.8
1045775	352.9	346.75	6.1	33.7	33.4	25.0	3%	0.01	25.01	835.3
1046100	352.0	346.00	6.0	33.0	35.5	25.0	5.5%	0.035	25.035	888.7
1046425	351.3	344.62	6.7	38.0	40.6	25.0	5.5%	0.035	25.035	1016.4
1046750	350.6	343.25	7.4	43.3					229,028.5	✓

(51)

Est #1

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excav. Length	Trap Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1046+50	350.6	343.25	7.4	43.3	44.0	25.0	5.5%	0.035	25.035	1101.5	✓
1046+75	349.5	341.88	7.6	44.8	43.6	25.0	5.5%	0.035	25.035	1091.5	✓
1047+00	347.8	340.50	7.3	42.5	39.2	25.0	5.5%	0.035	25.035	981.4	✓
1047+25	345.5	339.12	6.4	35.8	32.4	25.0	5.5%	0.035	25.035	811.1	✓
1047+50	343.2	337.75	5.4	28.9	26.3	25.0	5.5%	0.035	25.035	658.4	✓
1047+75	341.0	336.38	4.6	23.7	22.2 27.8	25.0	5.5%	0.035	25.035	555.8	✓
1048+00	339.3	335.00	4.3	21.8	21.2	25.0	4.7%	0.02	25.02	530.4	✓
1048+25	338.1	334.10	4.1	20.6					234	758.6	✓

(52)

TRADE MARK

84698

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in blue ink and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns, with some lines starting with numbers like '100', '200', '300', '400', '500', '600', '700', '800', '900', and '1000'. There are also some faint markings and a small rectangular stamp or box in the upper left corner. The paper has four circular punch holes along the right edge.

THE UNIVERSITY OF CHICAGO LIBRARY

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3 LEFAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Average Area	Horizontal Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Co. Yds.
1048+25	338.1	334.00	4.1	20.6	19.4	25.0	4%	0.02	25.02	485.4	✓
1048+50	336.7	333.00	3.7	18.2	18.5	25.0	4%	0.02	25.02	462.9	✓
1048+75	335.8	332.00	3.8	18.8	18.5	25.0	4%	0.02	25.02	462.9	✓
1049+00	334.7	331.00	3.7	18.2	18.2	25.0	4%	0.02	25.02	455.4	✓
1049+25	333.7	330.00	3.7	18.2	19.4	25.0	4%	0.02	25.02	485.4	✓
1049+50	333.1	329.00	4.1	20.6	20.9	25.0	4%	0.02	25.02	522.9	✓
1049+75	332.2	328.00	4.2	21.2	23.1	25.0	4%	0.02	25.02	578.0	✓
1050+00	331.8	327.00	4.8	25.0					238,	211.5	✓

33

TRADE MARK

9 82288

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in blue ink and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns, with some lines starting with "1911" and "1912".

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THE UNIVERSITY OF MICHIGAN

2 1911-1912



3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Ave End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1050+00	331.8	327.00	4.8	25.0	23.4	25.0	2%	0.005	25.005	585.1	✓
1050+25	330.8	326.50	4.3	21.8	24.4	25.0	2%	0.005	25.005	610.1	✓
1050+50	331.1	326.00	5.1	26.9	23.8	25.0	2%	0.005	25.005	595.1	✓
1050+75	329.6	325.50	4.1	20.6	20.9	25.0	2%	0.005	25.005	522.6	✓
1051+00	329.2	325.00	4.2	21.2	22.2	25.0	2%	0.005	25.005	555.1	✓
1051+25	329.0	324.50	4.5	23.1	22.4	25.0	2%	0.005	25.005	560.1	✓
1051+50	328.3	324.00	4.3	21.8	21.5	25.0	2%	0.005	25.005	539.6	✓
1051+75	327.7	323.50	4.2	21.2					242.177.2		

54

EST #1

TRADE MARK

96968

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in blue ink and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns. At the top left, there is a small rectangular box containing a grid. On the right side, there are four circular punch holes. The paper is mounted on a white background with a vertical strip of white tape at the top.

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1051475	327.7	323.50	4.2	21.2	19.4	25.0	2%	0.105	25.005	485.1	✓
1052100	326.6	323.00	3.6	17.6	20.4	25.0	2%	0.005	25.005	510.1	✓
1052725	327.0	322.50	4.5	23.1	21.6	25.0	2%	0.005	25.005	540.1	✓
1052750	326.0	322.00	4.0	20.0	21.2	25.0	-	-	25.0	530.0	✓
1052775	326.3	321.90	4.4	22.4	21.8	25.0	-	-	25.0	545.0	✓
1053100	326.0	321.80	4.2	21.2	21.8	25.0	-	-	25.0	545.0	✓
1053725	326.1	321.70	4.4	22.4	26.6	25.0	-	-	25.0	665.0	✓
1053750	327.3	321.60	5.7	30.9					245.9995		✓

(55)

EST 47

TRADE MARK

0'1116

DATE	DESCRIPTION	AMOUNT	BALANCE
1/1/20	OPENING BALANCE		100.00
1/5/20	SALES	50.00	150.00
1/10/20	PAYROLL	20.00	130.00
1/15/20	RENT	30.00	100.00
1/20/20	SALES	75.00	175.00
1/25/20	UTILITIES	15.00	160.00
1/30/20	SALES	60.00	220.00
2/5/20	PAYROLL	25.00	195.00
2/10/20	RENT	35.00	160.00
2/15/20	SALES	80.00	240.00
2/20/20	UTILITIES	20.00	220.00
2/25/20	SALES	90.00	310.00
2/28/20	PAYROLL	30.00	280.00
3/5/20	RENT	40.00	240.00
3/10/20	SALES	100.00	340.00
3/15/20	UTILITIES	25.00	315.00
3/20/20	SALES	110.00	425.00
3/25/20	PAYROLL	35.00	390.00
3/30/20	RENT	45.00	345.00
4/5/20	SALES	120.00	465.00
4/10/20	UTILITIES	30.00	435.00
4/15/20	SALES	130.00	565.00
4/20/20	PAYROLL	40.00	525.00
4/25/20	RENT	50.00	475.00
4/30/20	SALES	140.00	615.00
5/5/20	UTILITIES	35.00	580.00
5/10/20	SALES	150.00	730.00
5/15/20	PAYROLL	45.00	685.00
5/20/20	RENT	55.00	630.00
5/25/20	SALES	160.00	790.00
5/30/20	UTILITIES	40.00	750.00
6/5/20	SALES	170.00	920.00
6/10/20	PAYROLL	45.00	875.00
6/15/20	RENT	60.00	815.00
6/20/20	SALES	180.00	995.00
6/25/20	UTILITIES	45.00	950.00
6/30/20	SALES	190.00	1140.00
7/5/20	PAYROLL	50.00	1090.00
7/10/20	RENT	65.00	1025.00
7/15/20	SALES	200.00	1225.00
7/20/20	UTILITIES	50.00	1175.00
7/25/20	SALES	210.00	1385.00
7/30/20	PAYROLL	55.00	1330.00
8/5/20	RENT	70.00	1260.00
8/10/20	SALES	220.00	1480.00
8/15/20	UTILITIES	55.00	1425.00
8/20/20	SALES	230.00	1655.00
8/25/20	PAYROLL	60.00	1595.00
8/30/20	RENT	75.00	1520.00
9/5/20	SALES	240.00	1760.00
9/10/20	UTILITIES	60.00	1700.00
9/15/20	SALES	250.00	1950.00
9/20/20	PAYROLL	65.00	1885.00
9/25/20	RENT	80.00	1805.00
9/30/20	SALES	260.00	2065.00
10/5/20	UTILITIES	65.00	2000.00
10/10/20	SALES	270.00	2270.00
10/15/20	PAYROLL	70.00	2200.00
10/20/20	RENT	85.00	2115.00
10/25/20	SALES	280.00	2395.00
10/30/20	UTILITIES	70.00	2325.00
11/5/20	SALES	290.00	2615.00
11/10/20	PAYROLL	75.00	2540.00
11/15/20	RENT	90.00	2450.00
11/20/20	SALES	300.00	2750.00
11/25/20	UTILITIES	75.00	2675.00
11/30/20	SALES	310.00	2985.00
12/5/20	PAYROLL	80.00	2905.00
12/10/20	RENT	95.00	2810.00
12/15/20	SALES	320.00	3130.00
12/20/20	UTILITIES	80.00	3050.00
12/25/20	SALES	330.00	3380.00
12/30/20	PAYROLL	85.00	3300.00
1/5/21	RENT	90.00	3210.00
1/10/21	SALES	340.00	3550.00
1/15/21	UTILITIES	85.00	3465.00
1/20/21	SALES	350.00	3815.00
1/25/21	PAYROLL	90.00	3725.00
1/30/21	RENT	95.00	3630.00
2/5/21	SALES	360.00	3990.00
2/10/21	UTILITIES	90.00	3900.00
2/15/21	SALES	370.00	4270.00
2/20/21	PAYROLL	95.00	4175.00
2/25/21	RENT	100.00	4075.00
2/28/21	SALES	380.00	4455.00
3/5/21	UTILITIES	95.00	4360.00
3/10/21	SALES	390.00	4750.00
3/15/21	PAYROLL	100.00	4650.00
3/20/21	RENT	105.00	4545.00
3/25/21	SALES	400.00	4945.00
3/30/21	UTILITIES	100.00	4845.00
4/5/21	SALES	410.00	5255.00
4/10/21	PAYROLL	105.00	5150.00
4/15/21	RENT	110.00	5040.00
4/20/21	SALES	420.00	5460.00
4/25/21	UTILITIES	105.00	5355.00
4/30/21	SALES	430.00	5785.00
5/5/21	PAYROLL	110.00	5675.00
5/10/21	RENT	115.00	5560.00
5/15/21	SALES	440.00	6000.00
5/20/21	UTILITIES	110.00	5890.00
5/25/21	SALES	450.00	6340.00
5/30/21	PAYROLL	115.00	6225.00
6/5/21	RENT	120.00	6105.00
6/10/21	SALES	460.00	6565.00
6/15/21	UTILITIES	115.00	6450.00
6/20/21	SALES	470.00	6920.00
6/25/21	PAYROLL	120.00	6800.00
6/30/21	RENT	125.00	6675.00
7/5/21	SALES	480.00	7155.00
7/10/21	UTILITIES	120.00	7035.00
7/15/21	SALES	490.00	7525.00
7/20/21	PAYROLL	125.00	7400.00
7/25/21	RENT	130.00	7270.00
7/30/21	SALES	500.00	7770.00
8/5/21	UTILITIES	125.00	7645.00
8/10/21	SALES	510.00	8155.00
8/15/21	PAYROLL	130.00	8025.00
8/20/21	RENT	135.00	7890.00
8/25/21	SALES	520.00	8410.00
8/30/21	UTILITIES	130.00	8280.00
9/5/21	SALES	530.00	8810.00
9/10/21	PAYROLL	135.00	8675.00
9/15/21	RENT	140.00	8535.00
9/20/21	SALES	540.00	9075.00
9/25/21	UTILITIES	135.00	8940.00
9/30/21	SALES	550.00	9490.00
10/5/21	PAYROLL	140.00	9350.00
10/10/21	RENT	145.00	9205.00
10/15/21	SALES	560.00	9765.00
10/20/21	UTILITIES	140.00	9625.00
10/25/21	SALES	570.00	10195.00
10/30/21	PAYROLL	145.00	10050.00
11/5/21	RENT	150.00	9900.00
11/10/21	SALES	580.00	10480.00
11/15/21	UTILITIES	145.00	10335.00
11/20/21	SALES	590.00	10925.00
11/25/21	PAYROLL	150.00	10775.00
11/30/21	RENT	155.00	10620.00
12/5/21	SALES	600.00	11220.00
12/10/21	UTILITIES	150.00	11070.00
12/15/21	SALES	610.00	11680.00
12/20/21	PAYROLL	155.00	11525.00
12/25/21	RENT	160.00	11365.00
12/30/21	SALES	620.00	12085.00
1/5/22	UTILITIES	155.00	11930.00
1/10/22	SALES	630.00	12560.00
1/15/22	PAYROLL	160.00	12400.00
1/20/22	RENT	165.00	12235.00
1/25/22	SALES	640.00	12875.00
1/30/22	UTILITIES	160.00	12715.00
2/5/22	SALES	650.00	13365.00
2/10/22	PAYROLL	165.00	13200.00
2/15/22	RENT	170.00	13030.00
2/20/22	SALES	660.00	13690.00
2/25/22	UTILITIES	165.00	13525.00
2/28/22	SALES	670.00	14195.00
3/5/22	PAYROLL	170.00	14025.00
3/10/22	RENT	175.00	13850.00
3/15/22	SALES	680.00	14530.00
3/20/22	UTILITIES	170.00	14360.00
3/25/22	SALES	690.00	15050.00
3/30/22	PAYROLL	175.00	14875.00
4/5/22	RENT	180.00	14695.00
4/10/22	SALES	700.00	15495.00
4/15/22	UTILITIES	175.00	15320.00
4/20/22	SALES	710.00	16030.00
4/25/22	PAYROLL	180.00	15850.00
4/30/22	RENT	185.00	15665.00
5/5/22	SALES	720.00	16485.00
5/10/22	UTILITIES	180.00	16305.00
5/15/22	SALES	730.00	17035.00
5/20/22	PAYROLL	185.00	16850.00
5/25/22	RENT	190.00	16660.00
5/30/22	SALES	740.00	17400.00
6/5/22	UTILITIES	185.00	17215.00
6/10/22	SALES	750.00	17965.00
6/15/22	PAYROLL	190.00	17775.00
6/20/22	RENT	195.00	17580.00
6/25/22	SALES	760.00	18340.00
6/30/22	UTILITIES	190.00	18150.00
7/5/22	SALES	770.00	18920.00
7/10/22	PAYROLL	195.00	18725.00
7/15/22	RENT	200.00	18525.00
7/20/22	SALES	780.00	19305.00
7/25/22	UTILITIES	195.00	19110.00
7/30/22	SALES	790.00	19900.00
8/5/22	PAYROLL	200.00	19700.00
8/10/22	RENT	205.00	19495.00
8/15/22	SALES	800.00	20295.00
8/20/22	UTILITIES	200.00	20095.00
8/25/22	SALES	810.00	20905.00
8/30/22	PAYROLL	205.00	20700.00
9/5/22	RENT	210.00	20490.00
9/10/22	SALES	820.00	21290.00
9/15/22	UTILITIES	205.00	21085.00
9/20/22	SALES	830.00	21915.00
9/25/22	PAYROLL	210.00	21705.00
9/30/22	RENT	215.00	21490.00
10/5/22	SALES	840.00	22330.00
10/10/22	UTILITIES	210.00	22120.00
10/15/22	SALES	850.00	22970.00
10/20/22	PAYROLL	215.00	22755.00
10/25/22	RENT	220.00	22535.00
10/30/22	SALES	860.00	23495.00
11/5/22	UTILITIES	215.00	23280.00
11/10/22	SALES	870.00	24150.00
11/15/22	PAYROLL	220.00	23930.00
11/20/22	RENT	225.00	23705.00
11/25/22	SALES	880.00	24585.00
11/30/22	UTILITIES	220.00	24365.00
12/5/22	SALES	890.00	25255.00
12/10/22	PAYROLL	225.00	25030.00
12/15/22	RENT	230.00	24800.00
12/20/22	SALES	900.00	25700.00
12/25/22	UTILITIES	225.00	25475.00
12/30/22	SALES	910.00	26385.00
1/5/23	PAYROLL	230.00	26155.00
1/10/23	RENT	235.00	25920.00
1/15/23	SALES	920.00	26840.00
1/20/23	UTILITIES	230.00	26610.00
1/25/23	SALES	930.00	27540.00
1/30/23	PAYROLL	235.00	27305.00
2/5/23	RENT	240.00	27065.00
2/10/23	SALES	940.00	28005.00
2/15/23	UTILITIES	235.00	27770.00
2/20/23	SALES	950.00	28720.00
2/25/23	PAYROLL	240.00	28480.00
2/28/23	RENT	245.00	28235.00
3/5/23	SALES	960.00	29195.00
3/10/23	UTILITIES	240.00	28955.00
3/15/23	SALES	970.00	29



LEFAY, PENNSYLVANIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Avg. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Co. Yds.
1053+50	327.3	321.60	5.7	30.9	28.2	25.0	—	—	25.0	705.0	✓
1053+75	326.4	321.50	4.9	25.6	<del>22.2</del> 21.2	25.0	—	—	25.0	680.0 555.0	✓
1054+00	326.8	321.40	5.4	28.9	30.6	25.0	—	—	25.0	765.0	✓
1054+25	327.2	321.30	5.9	32.3	33.7	25.0	—	—	25.0	842.5	✓
1054+50	327.5	321.20	6.3	35.1	38.4	25.0	—	—	25.0	960.0	✓
1054+75	328.3	321.10	7.2	41.8	41.0	25.0	—	—	25.0	1025.0	✓
1055+00	328.0	321.00	7.0	40.2	40.2	25.0	10%	—	25.0	1005.0	✓
1055+25	327.8	320.75	7.0	40.2	40.2	25.0	10%	—	25.0	980.0	✓

(56)

EST 7

TRADE MARK

9' x 800' 6"



3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Ax. End Hor. Area	Sp. %	Excess Length	Tree Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1055+25	327.8	320.75	7.0	40.2	44.9	1%	—	25.0	1122.5	✓
1055+50	328.7	320.50	8.2	49.6	46.3	1%	—	25.0	1132.5	✓
1055+75	327.3	320.25	7.1	41.0	40.2	1%	—	25.0	1005.0	✓
1056+00	326.9	320.00	6.9	39.5	38.0	1%	—	25.0	950.0	✓
1056+25	326.3	319.75	6.5	36.6	35.5	1%	—	25.0	887.5	✓
1056+50	325.7	319.50	6.2	34.4	30.0	1%	—	25.0	750.0	✓
1056+75	324.1	319.25	4.9	25.6	25.9	1%	—	25.0	647.5	✓
1057+00	324.0	319.00	5.0	26.2					258,475.0	

59

TRADE MARK

9543.1





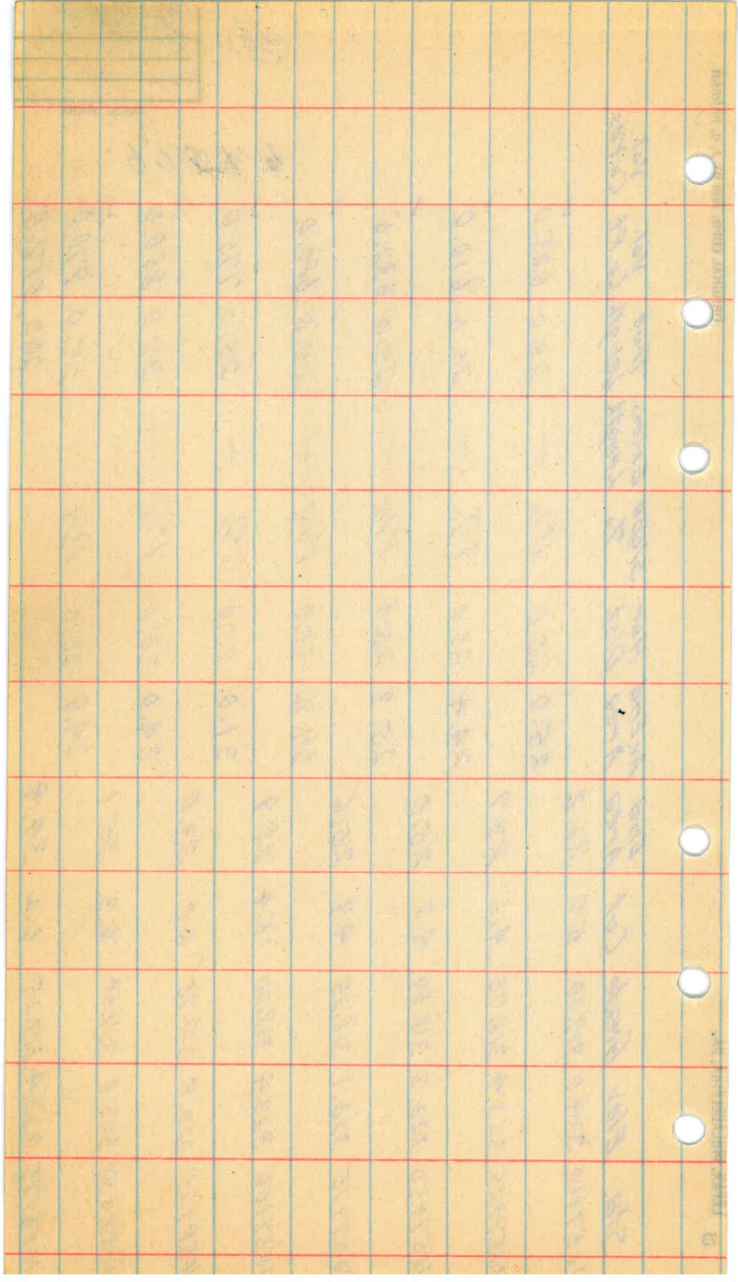
Sta.	Elev. Grade	Cut	End Area	Av. End Hor. Area	Hor. Dist.	5000 %	Exc. Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1057+00	324.0	5.0	26.2	25.0	25.0	1%	—	25.0	625.0	✓
1057+25	323.4	4.6	23.7	24.4	25.0	1%	—	25.0	610.0	✓
1057+50	323.3	4.8	25.0	25.3	25.0	1%	—	25.0	632.5	✓
1057+75	323.1	4.9	25.6	27.2	25.0	1%	—	25.0	680.0	✓
1058+00	323.4	5.4	28.9	31.0	25.0	1%	—	25.0	775.0	✓
1058+25	323.8	6.0	33.0	34.0	25.0	1%	—	25.0	850.0	✓
1058+50	323.8	6.3	35.1	34.8	25.0	1%	—	25.0	870.0	✓
1058+75	323.4	6.2	34.4					263	577.5	✓

(58)

Feet

TRADE MARK

6' 59 4/8



Sta.	Elev.	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1058+75	323.4	317.25	6.2	34.4	32.0	25.0	1%	-	25.0	800.0	
1059+00	322.5	317.00	5.5	29.6	29.2	25.0	4%	0.02	25.02	730.6	
1059+25	321.4	316.00	5.4	28.9	28.6	25.0	4%	0.02	25.02	715.6	
1059+50	320.3	315.00	5.3	28.2	24.7	25.0	4%	0.02	25.02	618.0	
1059+75	318.2	314.00	4.2	21.2	15.6	25.0	4%	0.02	25.02	390.3	1488.6
1060+00	315.2	313.00	2.2	10.0	5.0	20.0	2%	0.0	20.0	100.0	
1060+20	312.6	312.60	0.0								
1060+95	311.1	311.10	0.0								266,872.0

59

EST 21

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1060+95	311.1	311.10	0.0		0.4	5.0	2%	0.0	5.0	2.0	
1061+00	311.2	311.00	0.2	0.8	2.8	25.0	2%	0.005	25.005	70.0	
1061+25	311.6	310.50	1.1	4.7	6.4	25.0	2%	0.005	25.005	160.0	
1061+50	311.8	310.00	1.8	8.0	12.8	25.0	2%	0.005	25.005	320.0	
1061+75	313.1	309.50	3.6	17.6	16.2	25.0	2%	0.005	25.005	405.1	
1062+00	312.1	309.00	3.1	14.8	15.6	25.0	2%	0.005	25.005	390.1	
1062+25	311.9	308.50	3.4	16.5	18.2	25.0	2%	0.005	25.005	455.1	
1062+50	312.0	308.00	4.0	20.0						268,674.3	

(60)

6.2566

TRADE MARK

Handwritten ledger table with columns for various numerical entries and a date column on the right. The table is oriented vertically on the page.

Date	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1/1	100	200	300	400	500	600	700	800	900	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	2000	2100	2200	2300	2400	2500	2600	2700	2800	2900	3000	3100	3200	3300	3400	3500	3600	3700	3800	3900	4000	4100	4200	4300	4400	4500	4600	4700	4800	4900	5000	5100	5200	5300	5400	5500	5600	5700	5800	5900	6000	6100	6200	6300	6400	6500	6600	6700	6800	6900	7000	7100	7200	7300	7400	7500	7600	7700	7800	7900	8000	8100	8200	8300	8400	8500	8600	8700	8800	8900	9000	9100	9200	9300	9400	9500	9600	9700	9800	9900	10000

Sta.	Elev.	Grade	Cut	End Area	Ave. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Co. Yds.
1062150	312.0	308.00	4.0	20.0	22.2	25.0	1%	-	25.0	535.0	✓
1062175	312.4	307.70	4.7	24.3	27.0	25.0	1%	-	25.0	675.0	✓
1063100	312.9	307.40	5.5	29.6	32.4	25.0	1%	-	25.0	810.0	✓
1063125	313.4	307.10	6.3	35.1	33.0	25.0	1%	-	25.0	925.0	✓
1063150	312.5	306.80	5.7	30.9	28.0	25.0	1%	-	25.0	700.0	✓
1063175	311.3	306.50	4.8	25.0	25.3	25.0	1%	-	25.0	632.5	✓
1064100	311.1	306.20	4.9	25.6							
			Aug. 10				First Estimate		272,871.8		

TRADE MARK

(61)





Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1064100	311.1	306.20	4.9	25.6	22.5	25.0	1%	0.0	25.0	562.5	✓
1064125	308.8	305.90	3.9	19.4	19.4	25.0	1%	0.0	25.0	485.0	✓
1064150	309.5	305.60	3.9	19.4	20.0	25.0	1%	0.0	25.0	500.0	✓
1064175	309.4	305.30	4.1	20.6	21.5	25.0	1%	0.0	25.0	537.5	✓
1065100	309.4	305.00	4.4	22.4	20.0	25.0	4%	0.02	25.02	500.4	✓
1065125	309.7	306.08	3.6	17.6	15.1	25.0	4%	0.02	25.02	377.8	✓
1065150	309.9	307.17	2.7	12.6	12.4	25.0	4%	0.02	25.02	310.2	✓
1065175	310.8	308.25	2.6	12.1	12.4	25.0	4%	0.02	25.02	310.2	✓
										3,273.4	

TRADE MARK

Est "2"

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns. On the right side of the page, there are four circular punch holes. At the bottom of the page, there is a small rectangular stamp or label that is partially obscured and difficult to read. The paper shows signs of age, including some staining and discoloration.

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	T. Fuel Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1065+75	310.8	308.25	2.6	12.1	13.2	25.0	4%	0.02	25.02	330.3	✓
1066+00	312.3	309.33	3.0	14.3	14.0	25.0	4%	0.02	25.02	350.3	✓
1066+25	313.3	310.42	2.9	13.7	15.6	25.0	4%	0.02	25.02	390.3	✓
1066+50	315.1	311.50	3.6	17.6	17.0	25.0	4%	0.02	25.02	425.3	✓
1066+75	316.0	312.58	3.4	16.5	18.2	25.0	4%	0.02	25.02	455.4	✓
1067+00	317.7	313.66	4.0	20.0	22.2	25.0	4%	0.02	25.02	555.4	✓
1067+25	319.4	314.75	4.7	24.3	25.0	25.0	4%	0.02	25.02	625.5	✓
1067+50	320.7	315.83	4.9	25.6						6405.9	

②

TRADE MARK

Est # 2

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns, with some lines starting with "1910" and "1911".

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CONFIDENTIAL COPY FOR U.S. GOVERNMENT

CONFIDENTIAL COPY FOR U.S. GOVERNMENT



Sta	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1067750	320.7	315.83	4.9	25.6	25.6	25.0	4%	0.02	25.02	640.5	
1067775	321.8	316.91	4.9	25.6	22.5	25.0	4%	0.02	25.02	563.0	
1068100	321.9	318.00	3.9	19.4	22.2	25.0	1%	0.0	25.0	555.0	
1068125	323.1	318.29	4.8	25.0	25.0	25.0	1%	0.0	25.0	625.0	
1068150	323.4	318.57	4.8	25.0	27.0	25.0	1%	0.0	25.0	675.0	
1068175	324.3	318.86	5.4	28.9	29.6	25.0	1%	0.0	25.0	740.0	
1069100	324.7	319.14	5.6	30.2	28.9	25.0	1%	0.0	25.0	722.5	
1069125	324.6	319.42	5.2	27.6	28.9	25.0	1%	0.0	25.0	722.5	10,926.9

TRADE MARK

Est # 2

③

904.70



LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1069+25	324.6	319.42	5.2	27.6	31.7	25.0	1%	0.0	25.0	792.5	✓
1069+50	326.1	319.71	6.4	35.8	30.7	25.0	1%	0.0	25.0	767.5	✓
1069+75	324.9	320.00	4.9	25.6	25.9	15.9	—	—	15.9	411.8	✓
1069+90.9	324.9	319.93	5.0	26.2	26.2	25.0	—	—	25.0	655.0	✓
1070+15.9	324.8	319.82	5.0	26.2	27.9	25.0	—	—	25.0	697.5	✓
1070+40.9	325.2	319.71	5.5	29.6	32.4	25.0	—	—	25.0	810.0	✓
1070+65.9	325.9	319.60	6.3	35.1	32.4	25.0	—	—	25.0	810.0	✓
1070+90.9	325.0	319.99	5.5	29.6	32.4	25.0	—	—	25.0	810.0	✓
										15,871.2	

Est. #2

TRADE MARK





LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	Tree Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1070+90.9	325.0	319.49	5.5	29.6	29.2	10.0	-	-	10.0	292.0	✓
1071+00.9	324.8	319.44	5.4	28.9	27.2	24.1	-	-	24.1	655.3	✓
1071+25	324.2	319.33	4.9	25.6	26.2	25.0	-	-	25.0	655.0	✓
1071+50	324.3	319.22	5.1	26.9	28.6	25.0	-	-	25.0	715.0	✓
1071+75	324.7	319.11	5.6	30.2	28.9	25.0	-	-	25.0	722.5	✓
1072+00	324.2	319.00	5.2	27.6							
										18,911.2	

5

Est # 2

TRADE MARK

16,000 ✓

700.0 ✓



Sta.	Elev.	Grade	Cut	End Area	Avg. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1072+00	324.2	319.00	5.2	27.6	26.6	25.0	3%	0.01	25.01	665.3	✓
1072+25	323.2	318.25	4.9	25.6	25.9	25.0	3%	0.01	25.01	647.8	✓
1072+50	322.5	317.50	5.0	26.2	31.8	25.0	3%	0.01	25.01	795.3	✓
1072+75	323.4	316.75	6.6	37.3	32.4	25.0	3%	0.01	25.01	810.3	✓
1073+00	321.2	316.00	5.2	27.6	29.2	25.0	3%	0.01	25.01	730.3	✓
1073+25	321.0	315.25	5.7	30.9	29.2	25.0	3%	0.01	25.01	730.3	✓
1073+50	319.7	314.50	5.2	27.6	26.3	25.0	3%	0.01	25.01	657.8	✓
1073+75	318.6	313.75	4.8	25.0						23,948.3	





3 LEXAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1073+75	318.6	318.75	9.8	25.0	25.6	25.0	3%	0.01	25.01	690.3	✓
1074+00	318.0	313.00	5.0	26.2	26.9	25.0	2%	0.005	25.005	672.6	✓
1074+25	317.8	312.57	5.2	27.6	28.6	25.0	2%	0.005	25.005	715.1	✓
1074+50	317.6	312.14	5.5	29.6	28.6	25.0	2%	0.005	25.005	715.1	✓
1074+75	316.9	311.72	5.2	27.6	27.2	25.0	2%	0.005	25.005	680.1	✓
1075+00	316.4	311.29	5.1	26.9	27.6	25.0	2%	0.005	25.005	690.1	✓
1075+25	316.2	310.86	5.3	28.2	26.2	25.0	2%	0.015	25.015	655.1	✓
1075+50	315.1	310.43	4.7	24.3	26.2	25.0	2%	0.015	25.015	655.1	✓

TRADE MARK

Est 42

④

1923 1924 1925 1926 1927 1928 1929 1930 1931 1932 1933 1934 1935 1936 1937 1938 1939 1940 1941 1942 1943 1944 1945 1946 1947 1948 1949 1950 1951 1952 1953 1954 1955 1956 1957 1958 1959 1960 1961 1962 1963 1964 1965 1966 1967 1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1989 1990 1991 1992 1993 1994 1995 1996 1997 1998 1999 2000 2001 2002 2003 2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 2015 2016 2017 2018 2019 2020 2021 2022 2023 2024 2025 2026 2027 2028 2029 2030 2031 2032 2033 2034 2035 2036 2037 2038 2039 2040 2041 2042 2043 2044 2045 2046 2047 2048 2049 2050 2051 2052 2053 2054 2055 2056 2057 2058 2059 2060 2061 2062 2063 2064 2065 2066 2067 2068 2069 2070 2071 2072 2073 2074 2075 2076 2077 2078 2079 2080 2081 2082 2083 2084 2085 2086 2087 2088 2089 2090 2091 2092 2093 2094 2095 2096 2097 2098 2099 2100

ONE HUNDRED AND SEVENTY-NINE

21 THREE HUNDRED AND SEVENTY-NINE

LEFAX, PHILADELPHIA, PA.

ORIGINAL CORR. 1910 BY J. C. PARKER

Sta	Elev.	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1075+50	315.1	310.93	4.7	29.3	24.6	25.0	2%	0.015	25.015	615.1	✓
1075+75	314.8	310.00	4.8	25.0	28.3	25.0	4%	0.02	25.02	708.1	✓
1076+00	314.8	309.00	5.8	31.6	29.9	25.0	4%	0.02	25.02	748.1	✓
1076+25	313.3	308.00	5.3	28.2	29.2	9.5	4%	0.008	9.508	277.6	✓
1076+50	313.2	307.62	5.6	30.2	30.2	25.0	4%	0.02	25.02	755.6	✓
1076+75	312.2	306.62	5.6	30.2	30.2	25.0	4%	0.02	25.02	755.6	✓
1076+84.5	311.2	305.62	5.6	30.2	30.9	25.0	4%	0.02	25.02	773.1	✓
1077+08.5	310.4	304.62	5.8	31.6	30.9	25.0	4%	0.02	25.02	33,349.9	✓

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TRADE MARK  
EST # 2

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THE UNITED STATES OF AMERICA

2025



LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Co. Yds.
1077+95	308.4	304.62	5.8	31.6	29.2	25.0	4%	0.02	25.02	730.6	✓
1077+95	308.3	303.24	5.1	26.9	27.9	25.0	4% 1077+50 8%	0.04	25.04	698.6	✓
1077+95	306.6	301.24	5.4	28.9	27.9	5.0	8%	0.02	5.02	140.1	✓
1077+65	305.9	300.84	5.1	26.9	26.0	10.5	8%	0.03	10.53	273.8	✓
1077+95	304.8	300.00	4.8	25.0	27.3	25.0	13%	0.21	25.21	688.2	✓
1078+00	302.3	296.75	5.5	29.6	33.8	25.0	13%	0.21	25.21	852.1	✓
1078+25	300.2	293.50	6.7	38.0	36.9	25.0	13%	0.21	25.21	930.2	✓
1078+50	296.6	290.25	6.4	35.8					37663.5		

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Est 72  
TRADE MARK

1394.94



3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1078+50	286.6	290.25	6.4	35.8	36.6	25.0	13%	0.21	25.21	922.7	✓
1078+75	293.6	287.00	6.6	37.3	35.5	25.0	18%	0.40	25.40	901.7	✓
1079+00	288.5	282.40	6.1	33.7	34.4	25.0	18%	0.40	25.40	873.8	✓
1079+25	284.1	277.80	6.3	35.1	33.0	25.0	18%	0.40	25.40	838.2	✓
1079+50	278.9	273.20	5.7	30.9	26.6	25.0	18%	0.40	25.40	675.6	✓
1079+75	273.0	268.60	4.4	22.4	22.1	25.0	18%	0.40	25.40	561.3	✓
1080+00	268.3	264.00	4.3	21.8	25.0	25.0	21%	0.54	25.54	638.5	✓
1080+25	264.0	258.67	5.3	28.2					43,075.3		

(10)

Est # 2

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Avg. End Area	Hor. Dist.	Slope %	Excess Length	Tree Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1080+25	264.0	258.67	5.3	28.2	31.0	25.0	21%	0.54	25.54	791.7	✓
1080+50	259.4	253.33	6.1	33.7	34.8	25.0	21%	0.54	25.54	888.8	✓
1080+75	254.4	248.00	6.4	35.8	34.0	25.0	21%	0.54	25.54	868.4	✓
1081+00	248.6	242.67	5.9	32.3	30.6	25.0	21%	0.54	25.54	781.5	✓
1081+25	242.7	237.33	5.4	28.9	28.9	25.0	21%	0.54	25.54	738.1	✓
1081+50	237.4	232.00	5.4	28.9	31.3	25.0	21%	0.54	25.54	799.4	✓
1081+75	232.8	226.67	6.1	33.7	30.3	25.0	21%	0.54	25.54	773.9	✓
1082+00	226.4	221.33	5.1	26.9					48, 717.1		

TRADE MARK

Est # 2

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3 LEFAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1082+00	226.4	221.33	5.1	26.9	25.0	21%	0.54	25.54	653.8	✓
1082+25	220.7	216.00	4.7	24.3	25.0	21%	0.54	25.54	643.6	✓
1082+50	215.7	210.67	5.0	26.2	25.0	21%	0.54	25.54	574.6	✓
1082+75	209.1	205.33	3.8	18.8	25.0	21%	0.54	25.54	510.8	✓
1083+00	204.2	200.00	4.2	21.2	25.0	20%	0.50	25.50	604.4	✓
1083+25	200.0	195.00	5.0	26.2	25.0	20%	0.50	25.50	637.5	✓
1083+50	194.6	190.00	4.6	23.7	25.0	20%	1.50	25.50	645.2	✓
1083+75	190.1	185.00	5.1	26.9	25.0	20%	52	25.50	987.0	✓

(12)

Est # 2

TRADE MARK





3 LEFAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1083+75	192.1	185.00	5.1	26.9	26.6	25.0	20%	0.50	25.50	698.3	✓
1084+00	185.0	180.00	5.0	26.2	31.8	25.0	22%	0.60	25.60	814.1	✓
1084+25	181.2	179.57	6.6	52.3	43.8	25.0	22%	0.60	25.60	1121.3	✓
1084+50	172.9	169.19	8.3	50.4	57.7	25.0	22%	0.60	25.60	1477.1	✓
1084+75	173.7	163.71	10.0	65.0	63.2	25.0	22%	0.60	25.60	1617.9	✓
1085+00	167.9	158.28	9.6	61.4	49.4	25.0	22%	0.60	25.60	1264.6	✓
1085+25	159.4	152.85	6.6	37.3	34.4	25.0	22%	0.60	25.60	880.6	✓
1085+50	153.2	147.93	5.8	31.6					60,840.9		

(13)

Est 2

TRADE MARK

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LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1085750	153.2	147.93	5.8	31.6	34.8	25.0	22%	0.60	25.60	890.9	✓
1085775	148.7	142.08	6.7	38.0	35.8	25.0	10%	0.12	25.12	899.3	✓
1086100	145.5	139.93	6.1	33.7	34.0	25.0	10%	0.12	25.12	854.1	✓
1086125	143.1	136.86	6.2	34.4	35.5	25.0	10%	0.12	25.12	891.8	✓
1086150	140.8	134.28	6.5	36.6	43.5	25.0	10%	0.12	25.12	1092.7	✓
1086175	140.0	131.71	8.3	50.4	42.0	25.0	10%	0.12	25.12	1055.0	✓
1087400	135.2	129.14	6.1	33.7	34.0	25.0	10%	0.12	25.12	854.1	✓
1087425	132.8	126.57	6.2	34.4					67,398.8		

(A)

Est # 2

TRADE MARK





3 LEFAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1087+25	129.8	126.57	6.2	34.4	31.6	25.0	10%	0.12	25.12	793.8	✓
1087+50	129.4	124.00	5.4	28.9	31.6	25.0	3%	0.01	25.01	790.3	✓
1087+75	128.6	123.36	6.2	34.4	37.3	25.0	3%	0.01	25.01	932.9	✓
1088+00	129.7	122.72	7.0	40.2	36.2	25.0	3%	0.01	25.01	905.4	✓
1088+25	128.0	122.07	5.9	32.3	28.0	25.0	3%	0.01	25.01	700.3	✓
1088+50	126.0	121.43	4.6	23.7	27.0	25.0	3%	0.01	25.01	675.3	✓
1088+75	126.4	120.79	5.6	30.2	30.2	25.0	3%	0.01	25.01	755.3	✓
1089+00	125.8	120.15	5.6	30.2					72,932.1		

(15)

EST # 2

TRADE MARK



LEFAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1089+00	125.8	120.15	5.6	30.2	22.2	25.0	3%	0.01	25.01	730.3	✓
1089+25	124.8	118.51	5.3	28.2	25.6	25.0	3%	0.01	25.01	640.3	✓
1089+50	123.4	118.86	4.5	23.1	22.8	25.0	3%	0.01	25.01	570.2	✓
1089+75	122.6	118.22	4.4	22.4	20.6	25.0	3%	0.01	25.01	515.2	✓
1090+00	121.4	117.58	3.8	18.8	18.8	25.0	3%	0.01	25.01	470.2	✓
1090+25	120.7	116.94	3.8	18.8	20.6	25.0	3%	0.01	25.01	515.2	✓
1090+50	120.7	116.29	4.4	22.4	25.6	25.0	3%	0.01	25.01	640.3	✓
1090+75	121.0	115.65	5.4	28.9	25.6	25.0	3%	0.01	25.01	77,013.8	✓

16

EST. 1912

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1090+75	121.0	115.65	5.4	28.9	28.2	25.0	3%	0.01	25.01	705.3	✓
1091+00	122.2	115.00	5.2	27.6	28.6	25.0	5%	0.03	25.03	715.9	✓
1091+25	119.3	113.83	5.5	29.6	27.9	25.0	5%	0.03	25.03	698.3	✓
1091+50	117.7	112.67	5.0	26.2	25.2	25.0	5%	0.03	25.03	630.8	✓
1091+75	116.2	111.50	4.7	24.3	23.7	25.0	5%	0.03	25.03	593.2	✓
1092+00	114.8	110.33	4.5	23.1	22.4	25.0	5%	0.03	25.03	560.7	✓
1092+25	113.5	109.17	4.3	21.8	22.1	25.0	5%	0.03	25.03	553.2	✓
1092+50	112.9	108.00	4.4	22.4					81,471.2		

(17)

Est #2

TRADE MARK

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns, with some lines starting with a date, possibly "1888".

Small printed text at the bottom of the page, likely a manufacturer's mark or brand name, which is partially obscured by the paper's texture and the binding holes.

73 LEFAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1092750	112.4	108.00	4.4	22.4	24.3	25.0	5%	0.03	25.03	608.2	✓
1092775	111.8	106.83	5.0	26.2	25.0	25.0	5%	0.03	25.03	625.8	✓
1092800	110.3	105.67	4.6	23.7	24.6	25.0	5%	0.03	25.03	615.7	✓
1092825	109.4	104.50	4.9	25.6	26.2	25.0	5%	0.03	25.03	655.8	✓
1092850	108.4	103.33	5.1	26.9	26.9	25.0	5%	0.03	25.03	673.3	✓
1092875	107.3	102.17	5.1	26.9	27.9	25.0	5%	0.03	25.03	698.3	✓
1092900	106.4	101.00	5.4	28.9	27.9	25.0	2%	0.005	25.015	697.6	✓
1092925	105.6	100.50	5.1	26.9	27.9	25.0	2%	0.005	25.015	86,045.9	✓

(18)

EST #2

TRADE MARK

DATE	DESCRIPTION	AMOUNT	BALANCE	DATE	DESCRIPTION	AMOUNT	BALANCE
1/1/20	OPENING BALANCE		100.00				
1/5/20	SALES	50.00	150.00				
1/10/20	PAYROLL	25.00	125.00				
1/15/20	RENT	30.00	95.00				
1/20/20	UTILITIES	15.00	80.00				
1/25/20	SALES	40.00	120.00				
1/30/20	PAYROLL	25.00	95.00				
2/5/20	RENT	30.00	65.00				
2/10/20	UTILITIES	15.00	50.00				
2/15/20	SALES	35.00	85.00				
2/20/20	PAYROLL	25.00	60.00				
2/25/20	RENT	30.00	30.00				
2/28/20	UTILITIES	15.00	15.00				
3/1/20	CLOSING BALANCE		15.00				

24 FRANKS MANUFACTURING CO. ONE HUNDRED AND FIFTY EIGHT



LEFAX, PHILADELPHIA, PA.

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Sta	Elev	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1094+25	105.6	100.50	5.1	26.9	26.0	25.0	2%	0.005	25.005	650.1	650.1
1094+50	104.8	100.00	4.8	25.0	25.3	25.0	2%	0.005	25.005	632.6	632.6
1094+75	104.4	99.50	4.9	25.6	26.2	25.0	2%	0.005	25.005	655.1	655.1
1095+00	104.1	99.00	5.1	26.9	25.6	25.0	2%	0.005	25.005	690.1	690.1
1095+25	103.2	98.50	4.7	24.3	27.6	25.0	2%	0.005	25.005	690.1	690.1
1095+50	103.7	98.00	5.7	30.9	28.6	25.0	3%	0.01	25.01	715.3	715.3
1095+75	102.2	97.25	5.0	26.2	30.3	25.0	3%	0.01	25.01	757.8	757.8
1096+00	102.7	96.50	6.2	34.4					90	787.00	787.00

(19)

Est #2

TRADE MARK

862.98



3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1096400	102.7	96.50	6.2	34.4	31.3	25.0	3%	0.01	25.01	782.8	✓
1096425	101.0	95.75	5.3	28.2	29.9	25.0	3%	0.01	25.01	747.8	✓
1096450	102.8	95.00	5.8	31.6	32.3	25.0	2%	0.005	25.005	807.6	✓
1096475	101.5	95.50	6.0	33.0	28.4	25.0	2%	0.005	25.005	710.4	✓
1097400	100.6	96.00	4.6	23.7	18.7	25.0	7%	0.06	25.06	468.6	✓
1097425	100.6	97.75	2.9	13.7	15.4	25.0	7%	0.06	25.06	385.9	✓
1097450	103.0	99.50	3.5	17.0	20.4	25.0	7%	0.06	25.06	511.2	✓
1097475	105.8	101.25	4.6	23.7					95,	201.3	✓

(20)

EST # 2

TRADE MARK

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns, with some entries appearing to be dates or short phrases. At the bottom of the page, there are four circular punch holes. The paper is mounted on a white background.



3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPIR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1097775	105.8	101.25	4.6	23.7	25.0	7%	0.06	25.06	593.9	✓
1098400	107.6	103.00	4.6	23.7	25.0	17%	0.0	25.0	665.0	✓
1098425	108.2	102.75	5.5	29.6	25.0	19%	0.0	25.0	722.5	✓
1098450	107.8	102.50	5.3	28.2	25.0	17%	0.0	25.0	680.0	✓
1098475	107.2	102.25	5.0	26.2	25.0	17%	0.0	25.0	647.5	✓
1099400	106.9	102.00	4.9	25.6	25.0	3%	0.01	25.01	640.3	✓
1099425	106.2	101.25	4.9	25.6	25.0	3%	0.01	25.01	655.3	✓
1099450	105.6	100.50	5.1	26.9	25.0	3%	0.01	25.01	99,805.8	✓

(21)

Est. #2

TRADE MARK

DATE	DESCRIPTION	AMOUNT	BALANCE
1/1/20	OPENING BALANCE	100.00	100.00
1/5/20	PAYROLL	50.00	50.00
1/10/20	RENT	25.00	25.00
1/15/20	UTILITIES	15.00	10.00
1/20/20	SALES	30.00	40.00
1/25/20	PAYROLL	50.00	10.00
1/30/20	RENT	25.00	15.00
2/5/20	UTILITIES	15.00	0.00
2/10/20	SALES	30.00	30.00
2/15/20	PAYROLL	50.00	20.00
2/20/20	RENT	25.00	0.00
2/25/20	UTILITIES	15.00	15.00
2/30/20	SALES	30.00	45.00
3/5/20	PAYROLL	50.00	0.00
3/10/20	RENT	25.00	25.00
3/15/20	UTILITIES	15.00	10.00
3/20/20	SALES	30.00	40.00
3/25/20	PAYROLL	50.00	0.00
3/30/20	RENT	25.00	25.00
4/5/20	UTILITIES	15.00	10.00
4/10/20	SALES	30.00	40.00
4/15/20	PAYROLL	50.00	0.00
4/20/20	RENT	25.00	25.00
4/25/20	UTILITIES	15.00	10.00
4/30/20	SALES	30.00	40.00
5/5/20	PAYROLL	50.00	0.00
5/10/20	RENT	25.00	25.00
5/15/20	UTILITIES	15.00	10.00
5/20/20	SALES	30.00	40.00
5/25/20	PAYROLL	50.00	0.00
5/30/20	RENT	25.00	25.00
6/5/20	UTILITIES	15.00	10.00
6/10/20	SALES	30.00	40.00
6/15/20	PAYROLL	50.00	0.00
6/20/20	RENT	25.00	25.00
6/25/20	UTILITIES	15.00	10.00
6/30/20	SALES	30.00	40.00
7/5/20	PAYROLL	50.00	0.00
7/10/20	RENT	25.00	25.00
7/15/20	UTILITIES	15.00	10.00
7/20/20	SALES	30.00	40.00
7/25/20	PAYROLL	50.00	0.00
7/30/20	RENT	25.00	25.00
8/5/20	UTILITIES	15.00	10.00
8/10/20	SALES	30.00	40.00
8/15/20	PAYROLL	50.00	0.00
8/20/20	RENT	25.00	25.00
8/25/20	UTILITIES	15.00	10.00
8/30/20	SALES	30.00	40.00
9/5/20	PAYROLL	50.00	0.00
9/10/20	RENT	25.00	25.00
9/15/20	UTILITIES	15.00	10.00
9/20/20	SALES	30.00	40.00
9/25/20	PAYROLL	50.00	0.00
9/30/20	RENT	25.00	25.00
10/5/20	UTILITIES	15.00	10.00
10/10/20	SALES	30.00	40.00
10/15/20	PAYROLL	50.00	0.00
10/20/20	RENT	25.00	25.00
10/25/20	UTILITIES	15.00	10.00
10/30/20	SALES	30.00	40.00
11/5/20	PAYROLL	50.00	0.00
11/10/20	RENT	25.00	25.00
11/15/20	UTILITIES	15.00	10.00
11/20/20	SALES	30.00	40.00
11/25/20	PAYROLL	50.00	0.00
11/30/20	RENT	25.00	25.00
12/5/20	UTILITIES	15.00	10.00
12/10/20	SALES	30.00	40.00
12/15/20	PAYROLL	50.00	0.00
12/20/20	RENT	25.00	25.00
12/25/20	UTILITIES	15.00	10.00
12/30/20	SALES	30.00	40.00

2 FELIX ARISTIDEZ, INC. OF PRINT JOBS 100% C. NIPREL

Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu.Yds.
1099+750	105.6	100.50	5.1	26.9	22.6	3%	.009	22.609	601.4
1099+726	104.8	99.82	5.0	26.2	25.0	3%	0.01	25.01	649.8
1099+976	104.0	99.07	4.9	25.6	25.0	3% 11%	0.14	25.14	764.3
1100+226	102.8	96.51	6.3	35.1	25.0	11%	0.15	25.15	920.5
1100+476	100.5	93.76	6.7	38.0	25.0	11%	0.15	25.15	875.2
1100+726	102.8	96.51	6.3	35.1	25.0				
1100+476	100.5	93.76	6.7	38.0	25.0				
1100+726	96.8	91.01	5.8	31.6					

(22)

TRADE MARK  
~~103.674.7~~  
 103,675.0

Est #2

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns, with some lines starting with '1000', '10000', and '100000'. There are four circular punch holes along the right edge of the paper. A faint rectangular stamp is visible in the top left corner, and a small circular mark is present near the top center. The paper is placed on a white background with a light blue vertical line on the left and a light green vertical line on the right.

ONE THOUSAND AND SIXTY TWO  
ONE THOUSAND AND SIXTY TWO



Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1100+976	92.8	91.01	5.9	31.6	25.0	11%	0.15	25.15	784.7	✓
1100+976	94.0	88.26	5.7	30.9	25.0	11%	0.12	25.02	715.6	✓
1101+226	92.2	87.25	5.0	26.2	25.0	3%	0.01	25.01	655.3	✓
1101+476	91.4	86.41	5.0	26.2	25.0	3%	0.01	25.01	585.2	✓
1101+726	89.7	85.58	4.1	20.6	25.0	3%	0.01	25.01	602.7	✓
1101+976	92.0	84.75	5.2	27.6	25.0	3%	0.01	25.01	680.3	✓
1102+226	89.0	83.92	5.1	26.9	25.0	3%	0.01	25.01	697.8	✓
1102+976	88.5	83.08	5.4	28.9	25.0	3%	0.01	25.01	108,336.6	✓

(23)

TRADE MARK

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and bleed-through from the reverse side. The notes are organized into several columns, with some lines starting with a small square symbol. There are five circular punch holes along the right edge of the paper. A faint stamp or logo is visible in the top left corner.

3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1102+416	88.5	83.08	54	28.9	27.9	25.0	3%	0.01	25.01	697.8	✓
1102+726	87.3	82.25	5.1	26.9	29.6	25.0	3%	0.01	25.01	740.3	✓
1102+976	87.3	81.42	5.9	32.3	33.7	25.0	3%	0.01	25.01	842.8	✓
1103+226	86.9	80.58	6.3	35.1	38.0	25.0	3%	0.01	25.01	950.4	✓
1103+476	86.8	79.75	7.1	41.0	40.2	25.0	3%	0.01	25.01	1005.4	✓
1103+726	85.8	78.92	6.9	39.5	30.4	17.4	3%	0.007	17.407	529.2	✓
1103+90	82.5	78.33	4.2	21.2	34.6	10.0	3%	0.04	10.004	346.1	✓
1104+00	86.0	78.00	8.0	48.0						113,498.6	✓

(24)

Est 72

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope $\frac{1}{2}$	Excess Length	True Length	Vol. Co. Ft.	Vol. Cu. Yds.
1104100	86.0	78.00	8.0	48.0	25.0	—	—	25.0	1282.5 $\checkmark$	4
1104125	86.8	78.05	8.8	54.6	25.0	—	—	25.0	1242.5 $\checkmark$	36
1104150	85.7	78.10	7.6	49.8	25.0	—	—	25.0	1150.0 $\checkmark$	282
1104175	86.0	78.15	7.9	47.2	25.0	—	—	25.0	1200.0 $\checkmark$	36
1105100	86.3	78.20	8.1	48.8	25.0	—	—	25.0	1200.0 $\checkmark$	4
1105125										
1105150										
1105175										
									118,323.6	

(25)

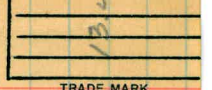
Est # 2

TRADE MARK



Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1143+64	180.72	180.72	0.0		17.2	11.0					^
1143+75	186.7	180.50	6.2	39.4	59.7	15.0					7.4
1143+90	192.3	180.20	12.1	85.0	79.6	10.0					^
1144+00	191.0	180.00	11.0	79.2	61.9	25.0					13.4
1144+25	184.9	176.67	8.2	49.6	47.2	25.0					^
1144+50	180.9	173.33	7.6	44.8	46.8	25.0					
1144+75	178.1	170.00	8.1	48.8	50.8	25.0					
1145+00	115.3	166.67	8.6	52.9							

TRADE MARK







3 LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	By End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.
1145100	175.3	166.67	8.6	52.9	55.0	25.0				1
1145125	172.4	162.33	9.1	57.1	45.8	25.0				
1145150	166.2	160.00	6.2	34.4	31.0	25.0				10.0
1145175	164.2	159.00	5.2	27.6	31.4	25.0				
1146100	164.3	158.00	6.3	35.1	42.8	25.0				1
1146125	165.3	157.00	8.3	50.4	55.9	25.0				
1146150	165.6	156.00	9.6	61.4	60.1	25.0				
1146175	160.8	151.50	9.3	58.8						

TRADE MARK

16.0

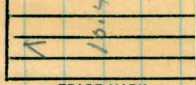


SJ LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Average Area	Horizontal Dist.	Slope %	Excess Length	TFUP Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1146775	160.8	157.50	8.3	58.8	57.1	29.5					
1147100.5	155.1	146.19	8.9	55.4	46.4	25.0					1
1147428.5	148.3	141.69	6.6	37.3	39.6	25.0					
1147754.5	144.5	137.28	7.2	41.8	38.8	25.0					11.0
1147779.5	139.7	133.28	6.4	35.8	33.0	25.0					
1148104.5	135.2	129.64	5.6	30.2	35.2	25.0					
1148429.5	134.6	127.64	7.0	40.2	46.6	25.0					
1148754.5	134.4	125.82	8.6	52.9							

TRADE MARK







Sta.	Elev.	Grade	Cut	End Area	Avg. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1148	134.5	134.4	8.6	52.9	56.8	8.7					
1148	163.2	135.0	125.47	9.5	60.6						



R LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 BY J. C. PARKER

Sta	Elev.	Grade	Cut	End Area	Av End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
12121 <sup>1/2</sup>	363.0	357.35	5.6	30.2	29.6	30.2	6%	.05	30.7	908.7	5.4
	364.5	359.10									
12121 <sup>3/4</sup>	358.7	353.00	5.4	28.9	32.4	56.6	—	—	56.6	1833.8	6.4
1213+00	359.8	353.24	6.4	35.8	40.7	100.0	—	—	100.0	4070.0	7.0
1214+00	361.4	353.67	7.7	45.6	50.9	100.0	—	—	100.0	5090.0	8.8
1215+00	363.1	354.09	9.0	56.2	58.0	100.0	—	—	100.0	5800.0	8.6
1216+00	363.9	354.52	9.4	59.7	57.6	100.0	—	—	100.0	5760.0	
1217+00	363.8	354.94	8.9	55.4	55.8	100.0	—	—	100.0	5580.0	
1218+00	364.4	355.37	9.0	56.2							
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TRADE MARK

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DATE	DESCRIPTION	AMOUNT	BALANCE
10/1	1000	1000	1000
10/2	500	500	500
10/3	200	300	300
10/4	100	200	200
10/5	100	100	100
10/6	100	0	0
10/7	100	100	100
10/8	100	0	0
10/9	100	100	100
10/10	100	0	0
10/11	100	100	100
10/12	100	0	0
10/13	100	100	100
10/14	100	0	0
10/15	100	100	100
10/16	100	0	0
10/17	100	100	100
10/18	100	0	0
10/19	100	100	100
10/20	100	0	0
10/21	100	100	100
10/22	100	0	0
10/23	100	100	100
10/24	100	0	0
10/25	100	100	100
10/26	100	0	0
10/27	100	100	100
10/28	100	0	0
10/29	100	100	100
10/30	100	0	0
10/31	100	100	100

ST. FRANCIS UNIVERSITY





DATE	DESCRIPTION	AMOUNT	BALANCE
10/1	1000	1000	1000
10/2	500	500	500
10/3	200	300	300
10/4	100	200	200
10/5	100	100	100
10/6	100	0	0
10/7	100	100	100
10/8	100	0	0
10/9	100	100	100
10/10	100	0	0
10/11	100	100	100
10/12	100	0	0
10/13	100	100	100
10/14	100	0	0
10/15	100	100	100
10/16	100	0	0
10/17	100	100	100
10/18	100	0	0
10/19	100	100	100
10/20	100	0	0
10/21	100	100	100
10/22	100	0	0
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10/24	100	0	0
10/25	100	100	100
10/26	100	0	0
10/27	100	100	100
10/28	100	0	0
10/29	100	100	100
10/30	100	0	0
10/31	100	100	100

AMOUNT PAID

DATE

LEFAX, PHILADELPHIA, PA.

ORIGINAL COPR. 1910 P.V. J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1225+00	367.5	358 <sup>2</sup>	9 <sup>2</sup>	58 <sup>2</sup>	56 <sup>2</sup>	100	-	-	100 <sup>2</sup>	5620 <sup>2</sup>	6.4
1226+00	366.9	358 <sup>2</sup>	8 <sup>2</sup>	53 <sup>2</sup>	57 <sup>2</sup>	100	-	-	100 <sup>2</sup>	5720 <sup>2</sup>	7.4
1227+00	367.8	358 <sup>2</sup>	9 <sup>2</sup>	60 <sup>2</sup>	59 <sup>2</sup>	100	-	-	100 <sup>2</sup>	5930 <sup>2</sup>	7.0
1228+00	367.6	358 <sup>2</sup>	9 <sup>2</sup>	58 <sup>2</sup>	58 <sup>2</sup>	100	-	-	100 <sup>2</sup>	5840 <sup>2</sup>	8.4
1229+00	367.8	358 <sup>2</sup>	9 <sup>2</sup>	58 <sup>2</sup>	64 <sup>2</sup>	100	-	-	100 <sup>2</sup>	6420 <sup>2</sup>	7.8
1230+00	369.0	358 <sup>2</sup>	10 <sup>2</sup>	69 <sup>2</sup>	67 <sup>2</sup>	100	-	-	100 <sup>2</sup>	6730 <sup>2</sup>	
1231+00	368.6	358 <sup>2</sup>	10 <sup>2</sup>	65 <sup>2</sup>	64 <sup>2</sup>	100	-	-	100 <sup>2</sup>	6460 <sup>2</sup>	
1232+00	368.8	358 <sup>2</sup>	9 <sup>2</sup>	64 <sup>2</sup>						304988 <sup>2</sup>	

TRADE MARK

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1295 86





Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1232+00	368.8	358.2	9 <sup>2</sup>	64 <sup>1</sup>	61 <sup>0</sup>	100	-	-	100 <sup>0</sup>	6100 <sup>0</sup>	7.4
1233+00	368.4	359.2	9 <sup>2</sup>	58 <sup>0</sup>	58 <sup>0</sup>	200	-	-	200 <sup>0</sup>	11600 <sup>0</sup>	
1235+00	368.9	359.2	9 <sup>2</sup>	58 <sup>0</sup>							
										522-688 <sup>2</sup>	
										321-352.3	
										11909	34

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EST. 42

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Sta.	Elev.	Grade	Cut	End Area	Ave. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1207+190	329.7	329.73	0.0 ✓	0.0	5.2 ✓	10.0	3%	0.004	10.004	52.0 ✓	5.0
1208+100	332.3	330.00	2.3 ✓	12.5	15.6 ✓	33.9	7%	0.08	33.98	530.1 ✓	5.2 ✓
1208+33.9	336.5	332.44	4.1 ✓	20.6	16.6 ✓	25.0	7%	0.06	25.06	416.0 ✓	6.4
1208+58.9	336.9	334.24	2.7 ✓	12.6	6.3 ✓	25.0	7%	0.06	25.06	157.9 ✓	6.0
1208+83.9	335.9	335.9	0.0 ✓	0.0							

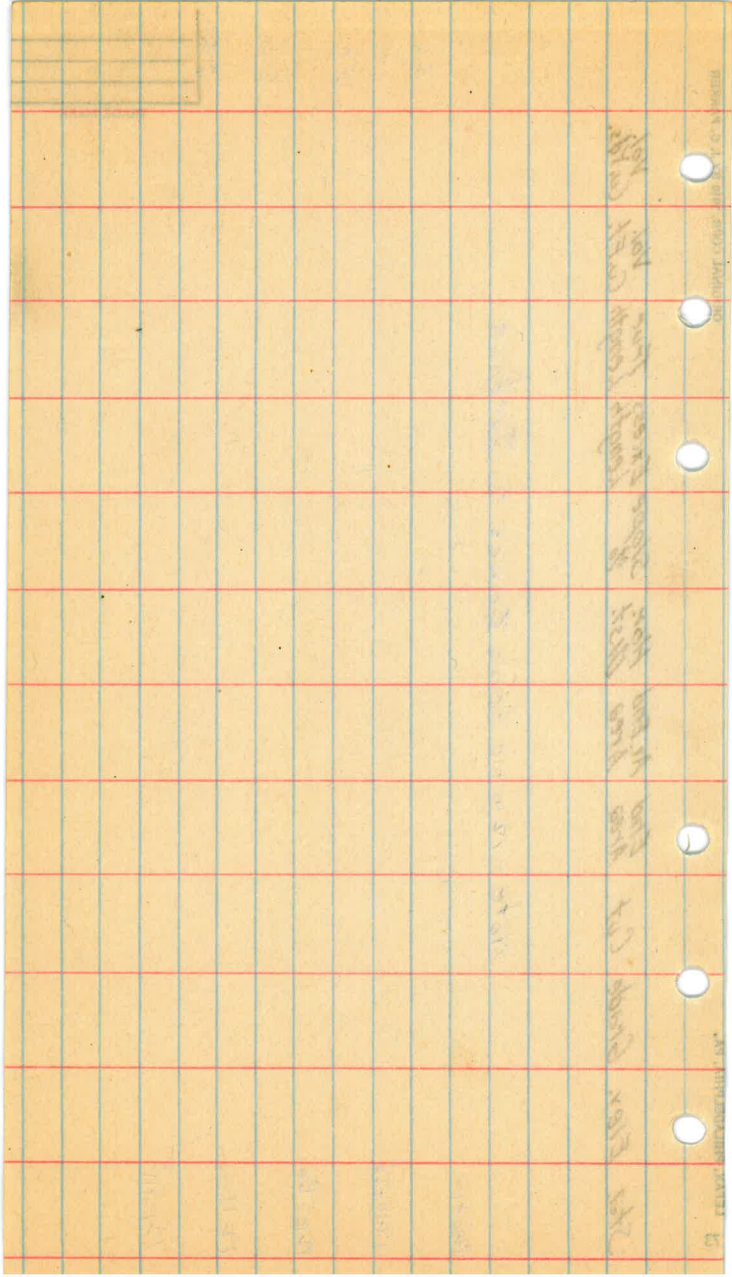
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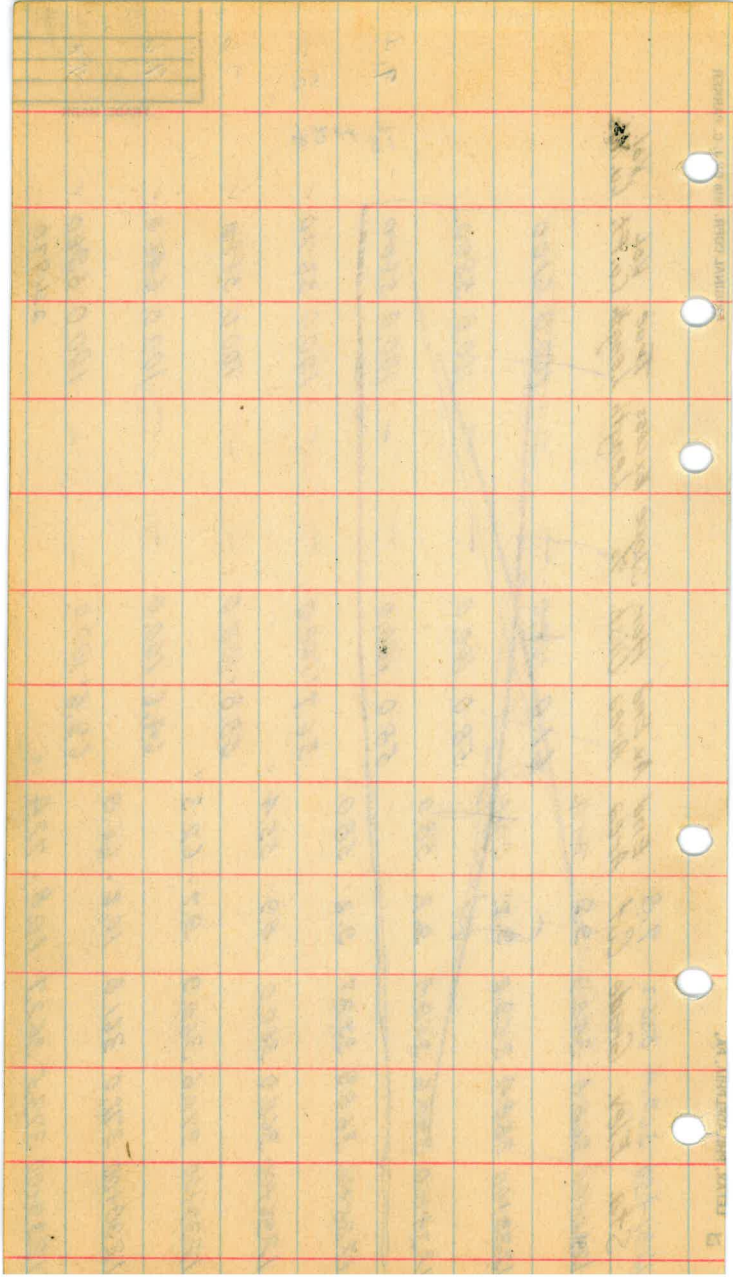


Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Kol. Co. Ft.	Kol. Cu. Yds.
1231750	368.4	555.2	9.8							
1232700	368.8	358.9	9.9	61.0	100.0	-	-	100.0	6100	
1233700	368.4	359.2	9.2	58.0	100.0	-	-	100.0	5800	
1234700	368.6	359.4	9.2	58.0	100.0	-	-	100.0	5800	
1235700	368.9	359.7	9.2	58.0	100.0	-	-	100.0	5870	8.0
1236700	368.9	360.0	8.9	55.4	100.0	-	-	100.0	5580	7.6
1237700	370.6	360.9	9.7	62.3	100.0	-	-	100.0	6460	7.6
1238700	372.0	361.8	10.2	66.8	100.0	-	-	100.0	6960	7.8
1239700	373.5	362.7	10.8	72.4	100.0	-	-	100.0	24970	

TRADE MARK

9.4  
8.0  
7.6

7.6
7.8





Sta	Elev.	Grade	Cut	End Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1239+00	373.5	362.7	10.8	72.4	100.0	-	-	100.0	7100	8.0
1240+00	374.2	363.7	10.5	69.6	100.0	-	-	100.0	7000	8.0
1241+00	375.2	364.6	10.6	70.5	100.0	-	-	100.0	7240	7.2
1242+00	376.5	365.5	11.0	74.2	100.0	-	-	100.0	7280	7.2
1243+00	377.8	367.1	10.7	71.4	100.0	-	-	100.02	6730	6.2
1244+00	379.2	369.4	9.8	63.2	100.0	2%	0.02	100.02	5930	9.0
1245+00	380.6	371.7	8.9	55.4	100.0	2%	0.02	100.02	5210	7.2
1246+00	382.1	374.0	8.1	49.8	100.0	2%	0.02	100.02	71460	

TRADE MARK



Sta.	Elev.	Grade	Cut	End Area	Av End Area	Hor Dist	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1246+00	382.1	374.0	8.1	48.8	52.5	100.0	—	—	100.0	5250	8.0
1247+00	383.3	374.3	9.0	56.2	64.1	100.0	—	—	100.0	6410	8.0
1248+00	384.3	374.7	9.6	72.0	74.2	100.0	—	—	100.0	7420	9.0
1249+00	385.2	375.0	10.2	76.5	77.4	100.0	—	—	100.0	7740	13.0
1250+00	385.7	375.3	10.4	78.2	78.2	100.0	—	—	100.0	7820	12.4
1251+00	386.1	375.7	10.4	78.2	79.6	100.0	—	—	1000	7960	10.4
1252+00	386.8	376.0	10.8	81.0	80.2	100.0	—	—	100.0	8020	10.2
1253+00	386.9	376.3	10.6	79.5	80.2	100.0	—	—	122080		

TRADE MARK

10.4
10.2

4521  
7





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Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1253+00	386.9	376.3	10.6	79.5	76.6	100.0	—	—	100.0	7660	9.6
1254+00	387.3	376.7	10.6	79.7	73.4	100.0	—	—	100.0	7340	10.6
1255+00	387.5	377.0	10.5	73.0	72.0	100.0	—	—	100.0	7200	10.4
1256+00	387.1	376.9	10.2	70.9	69.8	100.0	—	—	100.0	6980	9.8
1257+00	386.6	376.7	9.9	68.8	69.2	100.0	—	—	100.0	6920	10.0
1258+00	386.6	376.6	10.0	69.5	67.0	100.0	—	—	100.0	6700	9.4
1259+00	385.8	376.5	9.3	64.6	68.1	100.0	—	—	100.0	6810	9.4
1260+00	386.7	376.4	10.3	71.6						171690	

TRADE MARK

84
94



Sta.	Elev.	Grade	Cut	End Area	Ar. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1260+00	386.7	376.4	10.3	71.6	74.0	100.0	-	-	100.0	7400	9.4
1261+00	387.2	376.2	11.0	76.4	79.8	100.0					12.8
1262+00	387.5	376.1	11.4	83.2	79.9	100.0					12.2
1263+00	386.5	376.0	10.5	76.6	76.6	100.0					9.4
1264+00	385.7	375.2	10.5	76.6	76.2	100.0					8.4
1265+00	384.7	374.3	10.4	75.9	74.1	100.0					11.0
1266+00	383.4	373.5	9.9	72.3	72.3	100.0					12.0
1267+00	382.5	372.6	9.9	72.3							





Sta.	Elev. Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Vol. Co. Ft.	Vol. Co. Yds.
1267+00	382.5	2.9	72.3	71.9	100.0				11.0
1268+00	381.6	2.8	71.5	70.8	100.0				9.8
1269+00	380.6	2.6	70.1	67.6	100.0				12.6
1270+00	379.8	2.9	65.0	62.0	100.0				11.0
1271+00	378.9	2.1	59.1	58.4	100.0				11.8
1272+00	378.6	2.7	57.7	58.0	100.0				7.6
1273+00	378.5	2.5	58.4	57.3	100.0				9.0
1274+00	378.1	2.4	56.2						

TRADE MARK



Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1274+00	378.1	370.4	7.7	56.2	54.4	100.0				9.2	
1275+00	377.5	370.3	7.2	52.6	56.5	100.0				11.2	
1276+00	377.1	370.2	6.9	50.4	50.0	100.0				11.6	
1277+00	376.9	370.1	6.8	49.6	51.1	100.0				10.4	
1278+00	377.2	370.0	7.2	52.6	55.8	100.0				9.4	
1279+00	378.3	371.2	8.1	59.1	63.2	100.0					9.8
1280+00	379.6	371.4	9.2	67.2	68.6	100.0					12.2
1281+00	380.3	370.7	9.6	70.1							

DATE	DESCRIPTION	AMOUNT	INITIALS	REMARKS
10/1	1000	1000	1000	1000
10/2	1000	1000	1000	1000
10/3	1000	1000	1000	1000
10/4	1000	1000	1000	1000
10/5	1000	1000	1000	1000
10/6	1000	1000	1000	1000
10/7	1000	1000	1000	1000
10/8	1000	1000	1000	1000
10/9	1000	1000	1000	1000
10/10	1000	1000	1000	1000
10/11	1000	1000	1000	1000
10/12	1000	1000	1000	1000
10/13	1000	1000	1000	1000
10/14	1000	1000	1000	1000
10/15	1000	1000	1000	1000
10/16	1000	1000	1000	1000
10/17	1000	1000	1000	1000
10/18	1000	1000	1000	1000
10/19	1000	1000	1000	1000
10/20	1000	1000	1000	1000
10/21	1000	1000	1000	1000
10/22	1000	1000	1000	1000
10/23	1000	1000	1000	1000
10/24	1000	1000	1000	1000
10/25	1000	1000	1000	1000
10/26	1000	1000	1000	1000
10/27	1000	1000	1000	1000
10/28	1000	1000	1000	1000
10/29	1000	1000	1000	1000
10/30	1000	1000	1000	1000
10/31	1000	1000	1000	1000

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Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Ft.
1185+05 <sup>s</sup>	240.2	229.6	10.6			10.0					
1185+15 <sup>s</sup>	239.9	229.7	10.2			30.0					
1185+45 <sup>s</sup>	239.4	229.8	9.6			13.4					9.0
1185+58 <sup>s</sup>	240.2	229.9	10.3			16.1					
1185+75	240.3	229.9	10.4			25.0					
1186+00	240.7	230.0	10.7			25.0					
1186+25	241.5	231.7	9.8			25.0					
1186+50	242.6	233.3	9.3								

TRADE MARK



Sta.	Elev.	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1186+50	242.6	233.3	9.3 <sub>v</sub>			25.8					10.0
1186+75 <sup>8</sup>	244.1	235.1	9.0 <sub>v</sub>			17.3					
1186+93 <sup>1</sup>	245.0	236.2	8.8 <sub>v</sub>			17.1					
1187+10.2	245.8	237.3	8.5 <sub>v</sub>			14.8					
1187+25	246.0	238.3	7.7 <sub>v</sub>			25.0					
1187+50	247.3	240.0	7.3 <sub>v</sub>			25.0					
1187+75	248.1	241.1	7.0 <sub>v</sub>			17.2					
1187+92.2	248.6	241.9	6.7 <sub>v</sub>								

8.0

TRADE MARK





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Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1187+92.2	248.6	241.9	6.7 ✓			38.7					1
1188+302	250.2	243.7	6.5 ✓			38.6					
1188+695	252.0	245.4	6.6 ✓			5.5					7.4
1188+75	252.1	245.6	6.5 ✓			2.5					
1189+00	252.6	246.8	5.8 ✓			2.5					1
1189+25	254.0	247.9	6.1 ✓			2.5					
1189+50	255.2	249.1	6.1 ✓			21.8					
1189+71	256.3	250.2	6.1 ✓								

TRADE MARK

76

DATE	DESCRIPTION	AMOUNT	INITIALS	REMARKS
1950-01-01	1000000000	100		
1950-01-02	1000000000	100		
1950-01-03	1000000000	100		
1950-01-04	1000000000	100		
1950-01-05	1000000000	100		
1950-01-06	1000000000	100		
1950-01-07	1000000000	100		
1950-01-08	1000000000	100		
1950-01-09	1000000000	100		
1950-01-10	1000000000	100		
1950-01-11	1000000000	100		
1950-01-12	1000000000	100		
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1950-01-22	1000000000	100		
1950-01-23	1000000000	100		
1950-01-24	1000000000	100		
1950-01-25	1000000000	100		
1950-01-26	1000000000	100		
1950-01-27	1000000000	100		
1950-01-28	1000000000	100		
1950-01-29	1000000000	100		
1950-01-30	1000000000	100		
1950-01-31	1000000000	100		

21 CHECK SUBTOTALS 100

Sta. Elev. Grade. Cut End Ax End Hor Slippe Excess True Vol. Vol.  
 1189+71.3 256.3 250.2 6.1 ✓ Area Area Dist. % Length Length Co. Ft. Cu. Yds.

1190+00 257.3 251.3 6.0 ✓

1190+25 258.4 252.5 5.9 ✓

1190+50 259.7 253.6 6.1 ✓

1190+75 261.0 254.7 6.3 ✓

1191+00 255.9 262.1 6.2

1191+25

28.2

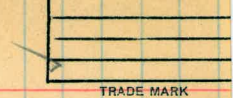
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TRADE MARK





Sta	Elev	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1191400	262.1	255.9	6.2	✓		25.0					
1191425	263.5	257.0	6.5	✓		25.0					
1191450	264.2	258.1	6.1	✓							



Sta.	Elev.	Grade	Cut	Area	End	Av. End	Hor.	Slope	Excess	True	Vol.	Vol.
					Area	Area	Dist.	%	Length	Length	Cu. Ft.	Cu. Yds.
1191												
1192												
1193												
1194+00												
1194+75												

1191

1192

1193

1194+00

1194+75

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3 LEXAFAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1194+75	277.5	272.9	4.6 ✓			15.8 ✓					
1194+90	279.8	273.6	6.2 ✓			28.5					^
1195+19	280.2	274.9	5.3 ✓			30.7					
1195+50	282.5	276.4	6.1 ✓			25.0					6.4
1195+75	283.4	277.6	5.8 ✓			25.0					
1196+00	284.7	278.8	5.9 ✓			25.0					
1196+25	286.3	280.0	6.3 ✓			25.0					
1196+50	287.7	281.2	6.5 ✓			25.0					

TRADE MARK

DATE	DESCRIPTION	AMOUNT	INITIALS	REMARKS
10/10/19	1000	1000		
10/11/19	1000	1000		
10/12/19	1000	1000		
10/13/19	1000	1000		
10/14/19	1000	1000		
10/15/19	1000	1000		
10/16/19	1000	1000		
10/17/19	1000	1000		
10/18/19	1000	1000		
10/19/19	1000	1000		
10/20/19	1000	1000		
10/21/19	1000	1000		
10/22/19	1000	1000		
10/23/19	1000	1000		
10/24/19	1000	1000		
10/25/19	1000	1000		
10/26/19	1000	1000		
10/27/19	1000	1000		
10/28/19	1000	1000		
10/29/19	1000	1000		
10/30/19	1000	1000		
10/31/19	1000	1000		

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Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1196+50	287.7	281.2	6.5 ✓			25.0				6.4	
1196+75	288.7	282.4	6.3 ✓			25.0					
1197+00	289.8	283.6	6.2 ✓			25.0					
1197+25	291.0	284.8	6.2 ✓			25.0					
1197+50	292.5	286.0	6.5 ✓			25.0				6.0	
1197+75	294.0	287.4	6.6 ✓			25.0					
1198+00	295.1	288.8	6.3 ✓			25.0					
1198+25	296.4	290.2	6.2 ✓			25.0					

TRADE MARK





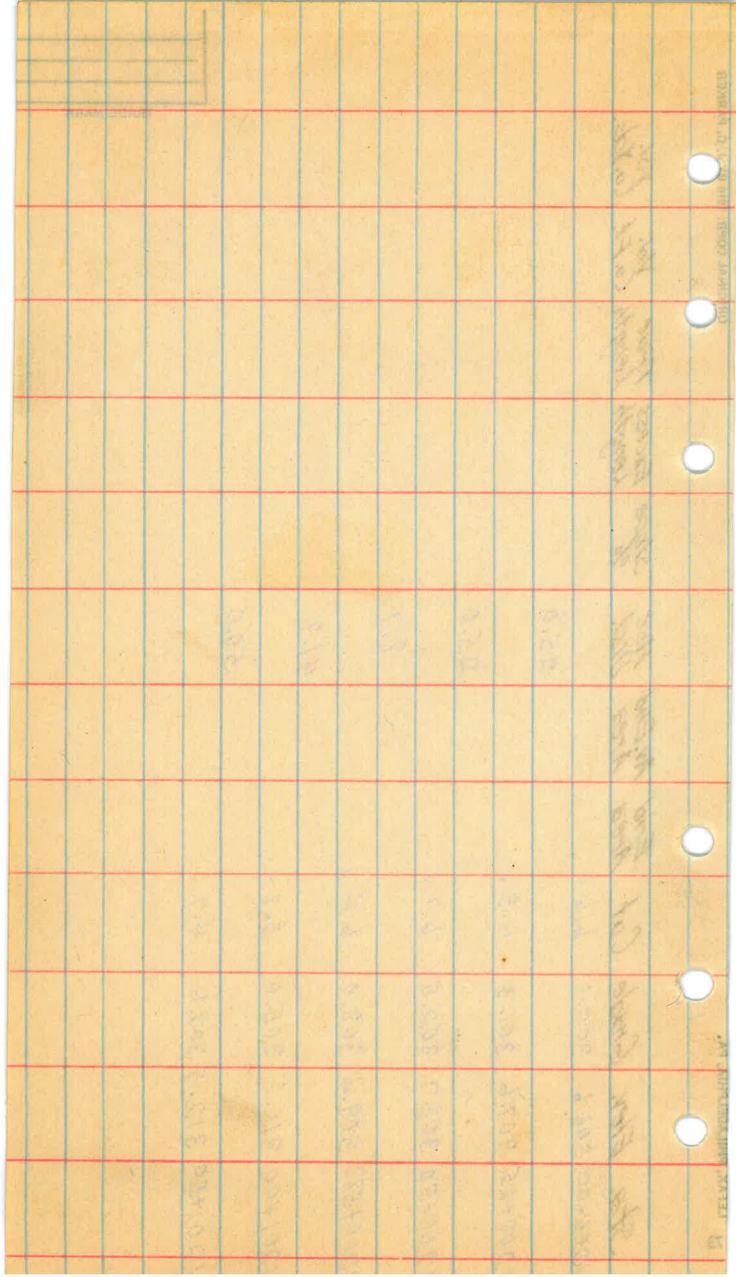
Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	Troc Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1198+25	296.4	290.2	6.2 ✓			25.0					6.4
1198+50	297.8	291.6	6.2 ✓			25.0					
1198+75	298.9	293.0	5.9 ✓			25.0					
1199+00	300.3	294.4	5.9 ✓			25.0					
1199+25	302.0	295.8	6.2 ✓			25.0					
1199+50	303.3	297.2	6.1 ✓			25.0					
1199+75	305.0	298.6	6.4 ✓			25.0					
1200+00	306.6	300.0	6.6 ✓			25.0					

DATE	DESCRIPTION	AMOUNT	BALANCE
1/1/19	OPENING BALANCE	100.00	100.00
1/15/19	SALES	50.00	150.00
1/20/19	PAYROLL	25.00	125.00
1/25/19	RENT	75.00	50.00
1/30/19	SALES	30.00	80.00
2/5/19	PAYROLL	25.00	55.00
2/10/19	RENT	75.00	(20.00)
2/15/19	SALES	40.00	(40.00)
2/20/19	PAYROLL	25.00	(65.00)
2/25/19	RENT	75.00	(140.00)
2/28/19	SALES	30.00	(110.00)
3/5/19	PAYROLL	25.00	(135.00)
3/10/19	RENT	75.00	(210.00)
3/15/19	SALES	40.00	(170.00)
3/20/19	PAYROLL	25.00	(195.00)
3/25/19	RENT	75.00	(270.00)
3/28/19	SALES	30.00	(240.00)
3/31/19	PAYROLL	25.00	(265.00)
4/5/19	RENT	75.00	(340.00)
4/10/19	SALES	40.00	(300.00)
4/15/19	PAYROLL	25.00	(325.00)
4/20/19	RENT	75.00	(400.00)
4/25/19	SALES	30.00	(370.00)
4/30/19	PAYROLL	25.00	(395.00)
5/5/19	RENT	75.00	(470.00)
5/10/19	SALES	40.00	(430.00)
5/15/19	PAYROLL	25.00	(455.00)
5/20/19	RENT	75.00	(530.00)
5/25/19	SALES	30.00	(500.00)
5/31/19	PAYROLL	25.00	(525.00)
6/5/19	RENT	75.00	(600.00)
6/10/19	SALES	40.00	(560.00)
6/15/19	PAYROLL	25.00	(585.00)
6/20/19	RENT	75.00	(660.00)
6/25/19	SALES	30.00	(630.00)
6/30/19	PAYROLL	25.00	(655.00)
7/5/19	RENT	75.00	(730.00)
7/10/19	SALES	40.00	(690.00)
7/15/19	PAYROLL	25.00	(715.00)
7/20/19	RENT	75.00	(790.00)
7/25/19	SALES	30.00	(760.00)
7/31/19	PAYROLL	25.00	(785.00)
8/5/19	RENT	75.00	(860.00)
8/10/19	SALES	40.00	(820.00)
8/15/19	PAYROLL	25.00	(845.00)
8/20/19	RENT	75.00	(920.00)
8/25/19	SALES	30.00	(890.00)
8/31/19	PAYROLL	25.00	(915.00)
9/5/19	RENT	75.00	(990.00)
9/10/19	SALES	40.00	(950.00)
9/15/19	PAYROLL	25.00	(975.00)
9/20/19	RENT	75.00	(1050.00)
9/25/19	SALES	30.00	(1020.00)
9/30/19	PAYROLL	25.00	(1045.00)
10/5/19	RENT	75.00	(1120.00)
10/10/19	SALES	40.00	(1080.00)
10/15/19	PAYROLL	25.00	(1105.00)
10/20/19	RENT	75.00	(1180.00)
10/25/19	SALES	30.00	(1150.00)
10/31/19	PAYROLL	25.00	(1175.00)
11/5/19	RENT	75.00	(1250.00)
11/10/19	SALES	40.00	(1210.00)
11/15/19	PAYROLL	25.00	(1235.00)
11/20/19	RENT	75.00	(1310.00)
11/25/19	SALES	30.00	(1280.00)
11/30/19	PAYROLL	25.00	(1305.00)
12/5/19	RENT	75.00	(1380.00)
12/10/19	SALES	40.00	(1340.00)
12/15/19	PAYROLL	25.00	(1365.00)
12/20/19	RENT	75.00	(1440.00)
12/25/19	SALES	30.00	(1410.00)
12/31/19	PAYROLL	25.00	(1435.00)

RENTAL INSTRUCTIONS 54\*

RENTAL INSTRUCTIONS 54\*

Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1200+00	306.6	300.0	6.6 ✓			25.0				
1200+25	307.6	301.3	6.3 ✓			25.0				
1200+50	308.7	302.5	6.2 ✓			8.7				
1200+582	309.4	303.0	6.4 ✓			41.3				
1201+00	310.8	305.0	5.8 ✓			50.0				
1201+50	312.5	307.6	4.9 ✓							





Sta.	Elev.	Grade	Cut	End Area	Avg. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1200											
1201											
1204											
1203											

1200

1201

1204

1203

6.0

6.0

5.8

TRADE MARK



Sta. Elev. Grade Cut End Area Area Hor. Dist. Slope Excess True Vol. Vol. Cu Yds. Length Cu Ft.

1203

1204

1204+50

1205

1206+00

1206+50

1206+87

7.0

9.2

7.0

7.2

8.6

7.2

0.0

7.2

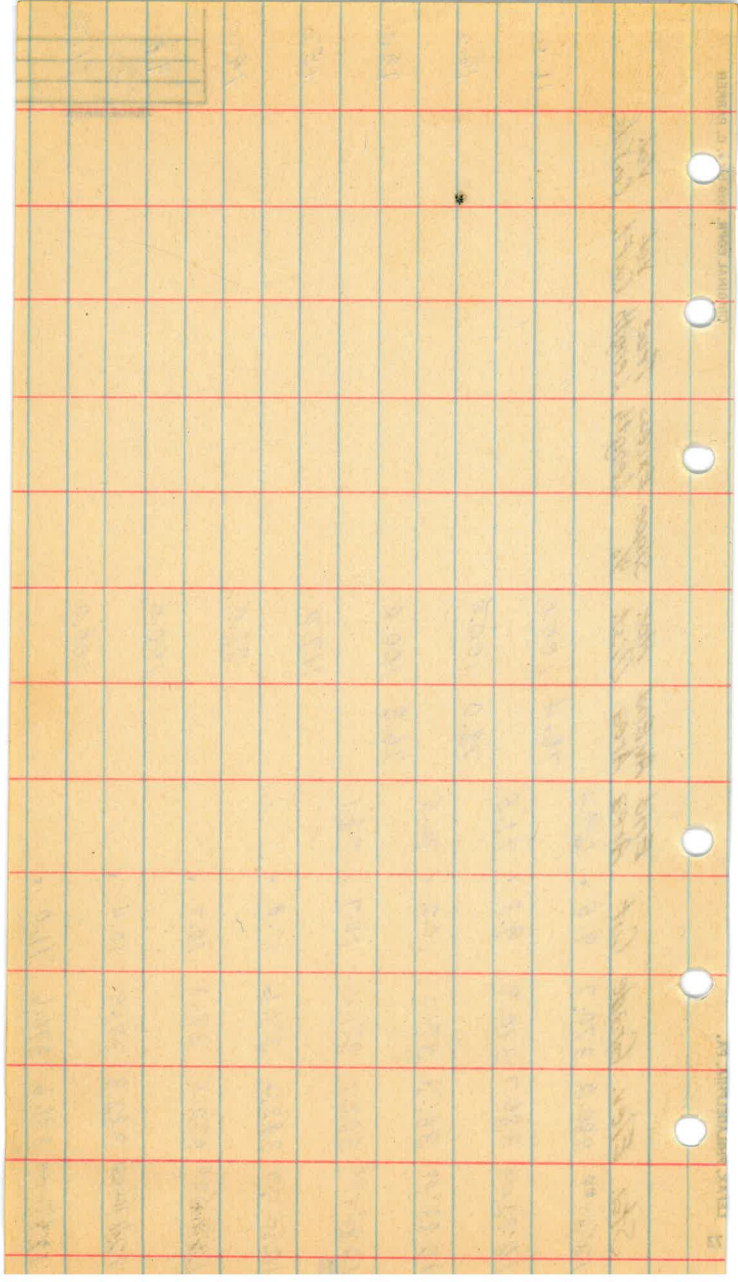
TRADE MARK

Note. 1201+30  
Allowance is to be made for Lowering Grade  
to get under drain at Sta. 1203+30.  
Force acct. allowed from 1201+30 to 1205+30

1201+30  
1202+30  
1203+30  
1204+30  
1205+30  
1206+30  
1207+30  
1208+30  
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1299+30  
1300+30



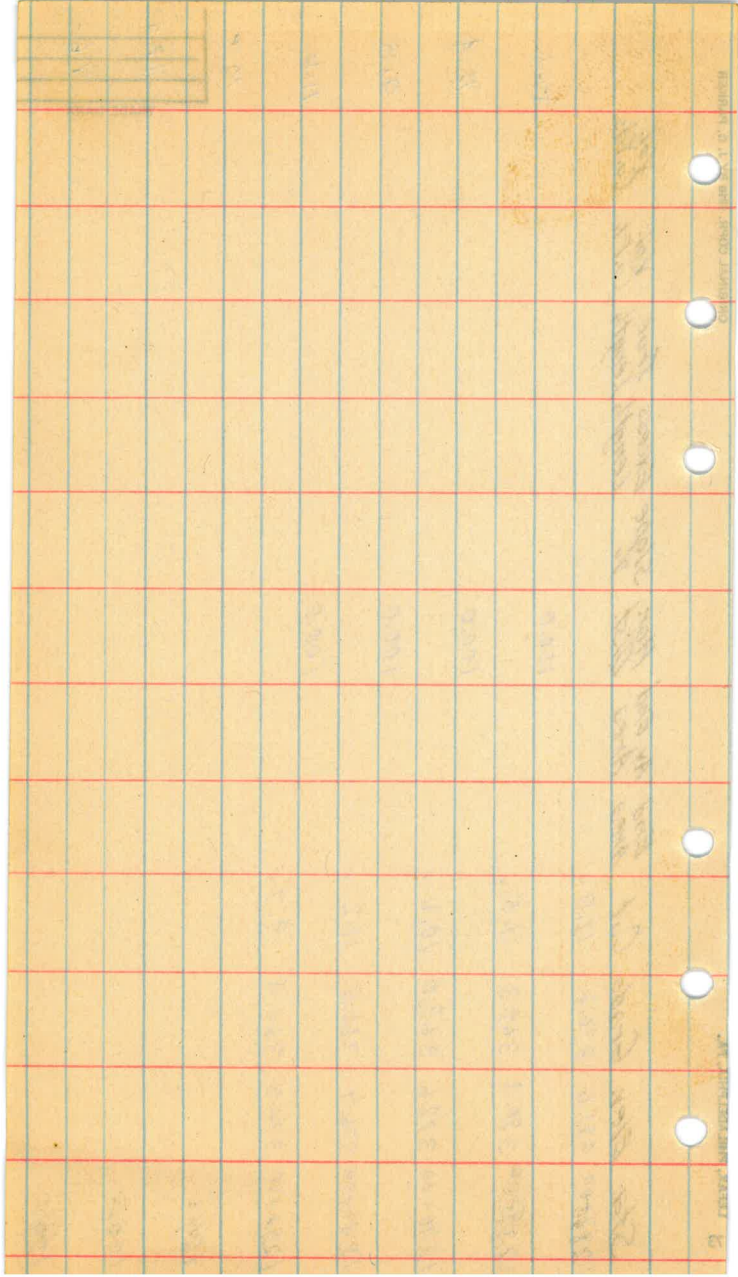
Sta.	Elev.	Grade	Cut	End Area	Ave End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1281+00	380.2	370.7	9.5 ✓	69.4	70.4	100.0					11.0
1282+00	380.7	370.9	9.8 ✓	71.5	73.0	100.0					16.0
1283+00	381.3	371.1	10.2 ✓	74.5	76.3	100.0					13.0
1284+00	382.1	371.4	10.7 ✓	78.1		117.0					15.0
1285+17	382.6	371.6	11.0 ✓			83.0					14.0
1286+00	382.5	371.8	10.7 ✓								
1287+00	382.3	371.9	10.4 ✓			100.0					
1288+00	381.6	370.6	11.0 ✓			100.0					



Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu.Yds.
1288+00	381.6	370.6	11.0 ✓			100.0				12.6
1289+00	380.8	369.3	11.5 ✓			100.0				11.4
1290+00	378.6	368.0	10.6 ✓			100.0				9.8
1291+00	376.7	366.5	10.2 ✓			100.0				11.6
1292+00	374.3	364.6	9.7 ✓							10.2
1293										
1294										
1295										

TRADE MARK

11.0  
9.6





Sta. Elev. Grade Cut Area Av. End Hor. Slope Excess True Vol. Val.  
 Length Length C. Ft. Cu Yds. C. Yds.

1295

12.6

1296

14.8

1297

13.4

1298

10.8

1299

13.8

1300

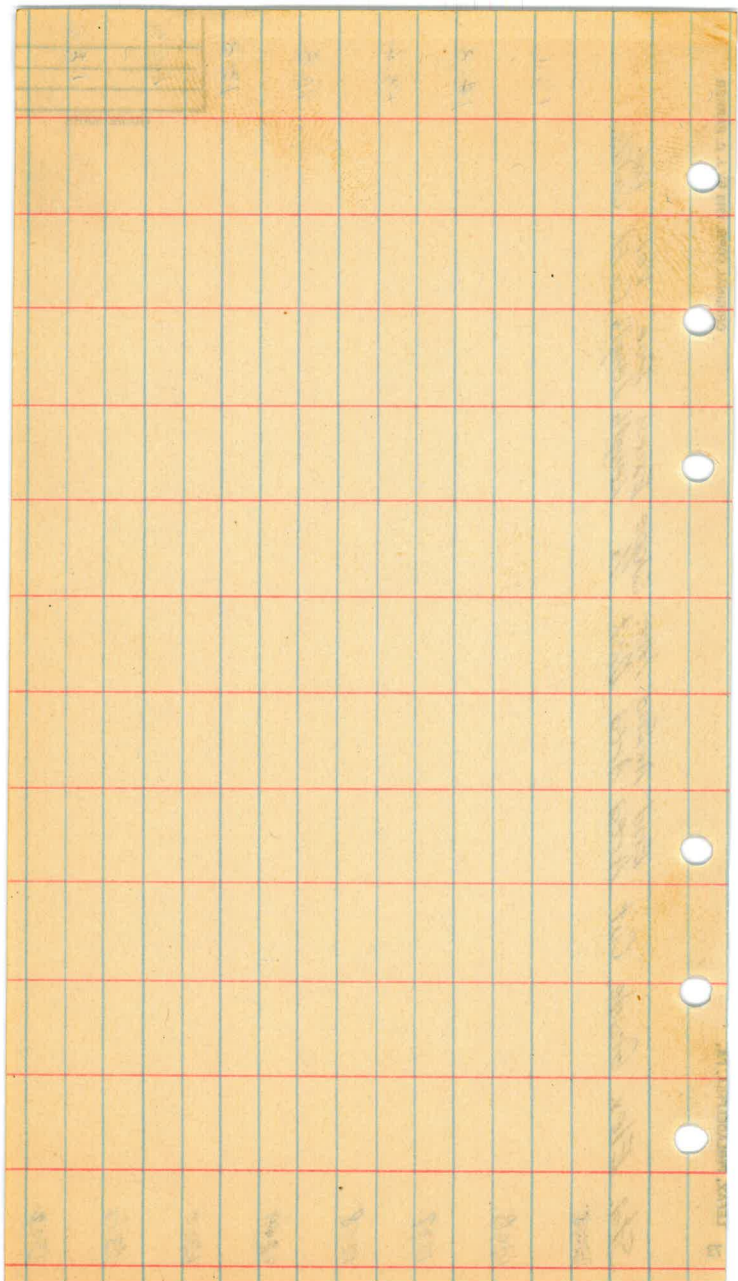
10.6

1301

12.9

1302

TRADE MARK



Sta. Elev. Grade Cut Area End Area Hor. Dist. Slope Excess True Vol. Vol. Length Lengths Cu. Ft. Cu. Yds.

1302

11.5

1303

12.0

1304

11.0

1305

9.4

1306

15.0

1307

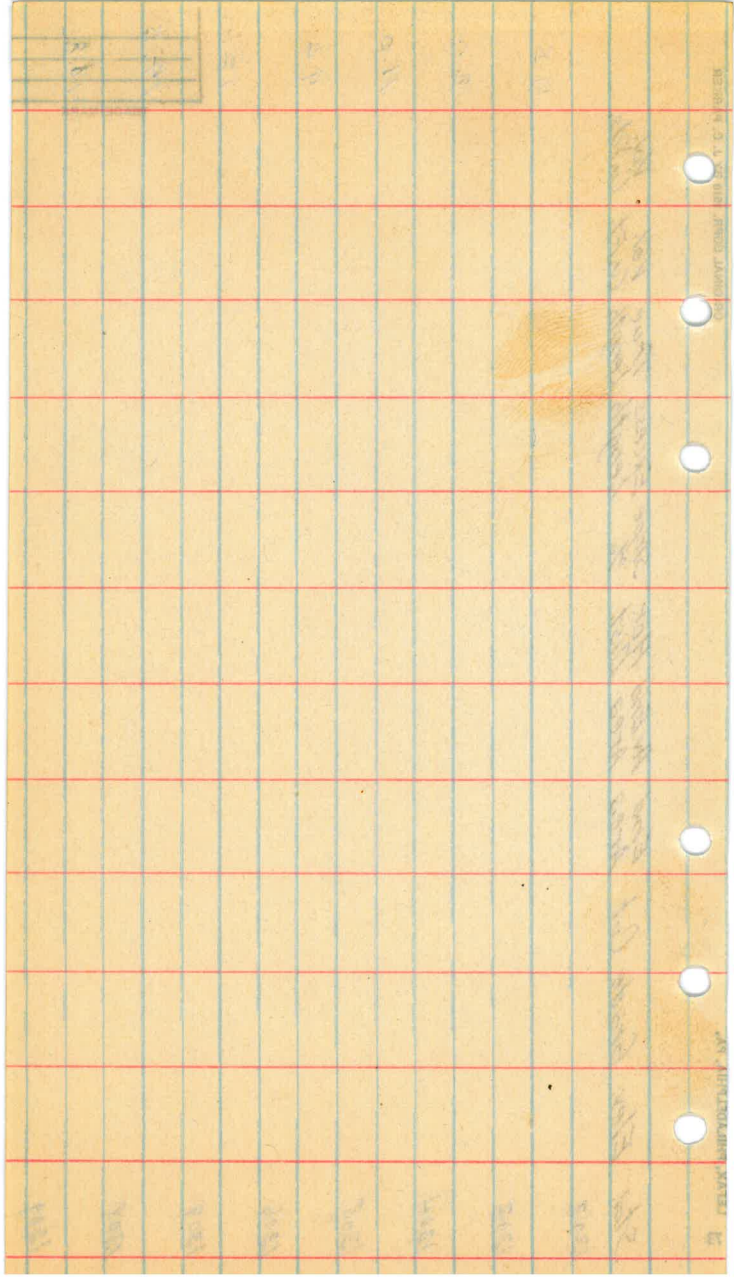
14.5

1308

10.8

1309

TRADE MARK

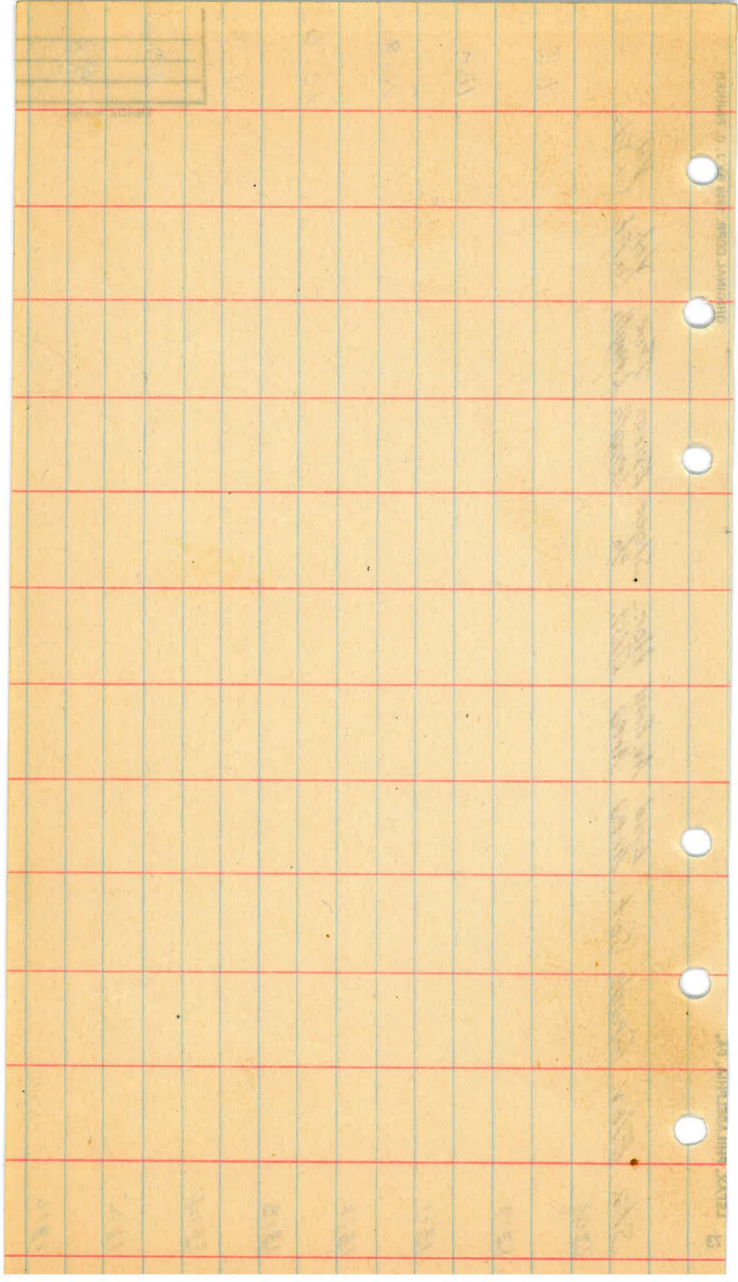




Sta.	Elev.	Grade	Cut	End Area	Av End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1309										11.5	
1310										11.0	
1311										10.8	
1312										10.5	
1313										11.3	
1314											10.0
1315											9.8
1316											

TRADE MARK

10.0
9.8

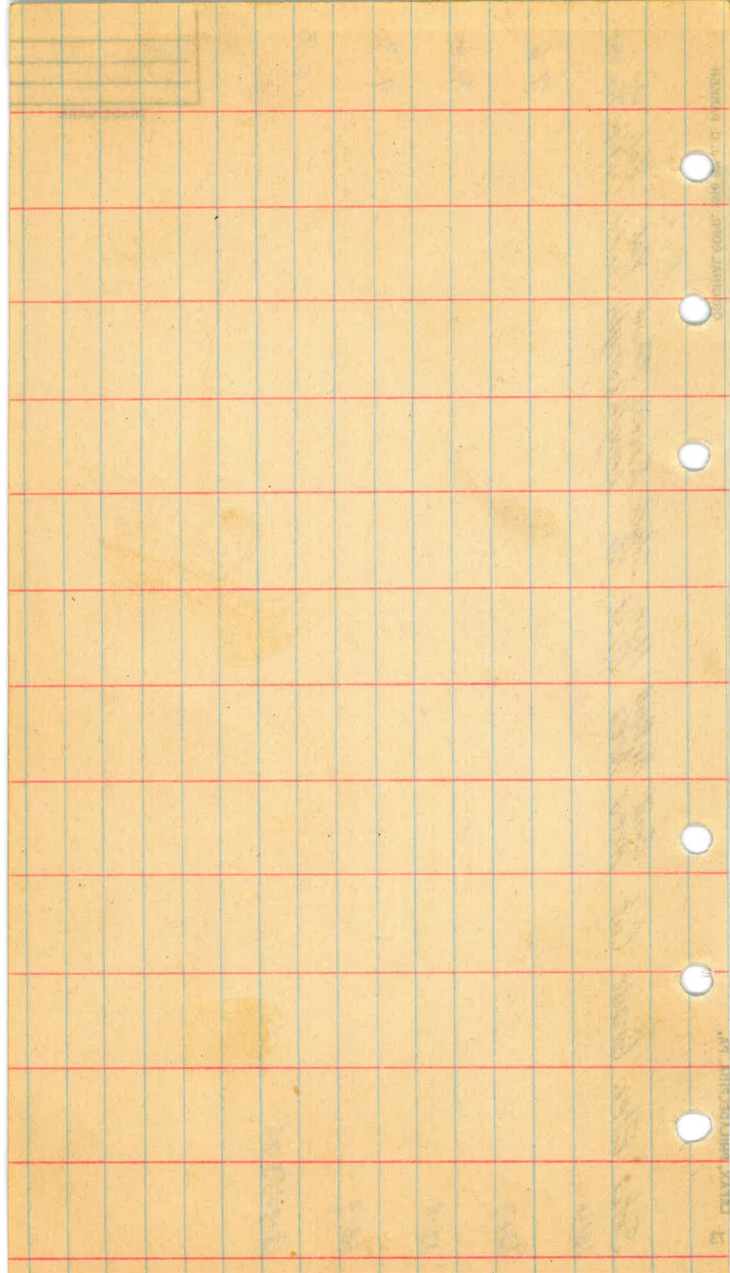


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Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess True Length	Vol. Cu. Yds.	Av. Top width
1316										7.6
1317										8.4
1318										9.3
1319										10.3
1319+85.26										

TRADE MARK





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Sta	Elev	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1156											
1157											
1158											
1159											
1160											
1161											
1162											
1163											

8.6  
9.6  
12.0  
9.0  
7.0

7.0
8.0

TRADE MARK

1. 1000  
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 100. 1000

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Sta Elev Grade Cut End Area Av End Area Hor. Dist. Slope % Excess Length True Length Vol. Vol. Cu. Yds. Cu. Yds.

1163

1164

1165

1166

1167

1168

1169

1170

7.4

8.0

7.0

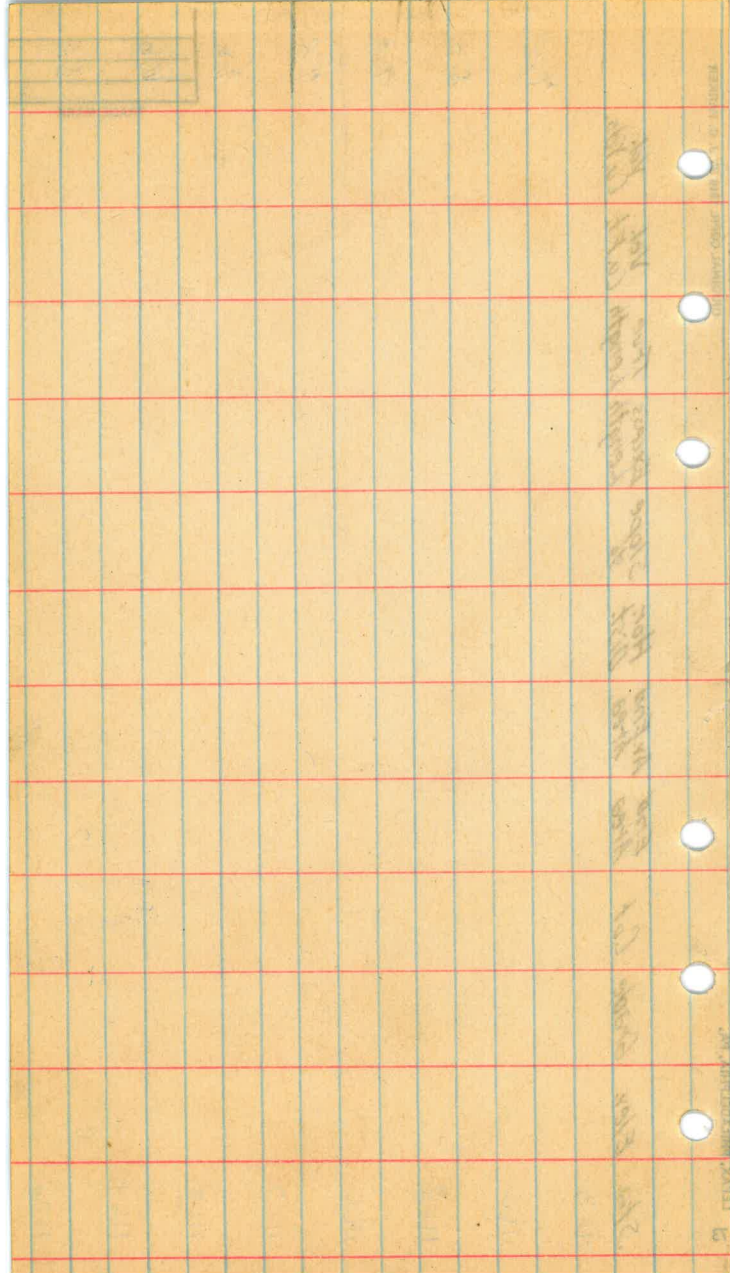
7.8

7.0

6.6

6.0

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Average Area	Horizontal Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1170										7.8	
1171										8.2	
1172										7.6	
1173										9.0	
1174										9.0	
1175											8.2
1176											7.4
1177											

TRADE MARK

8.2
7.4

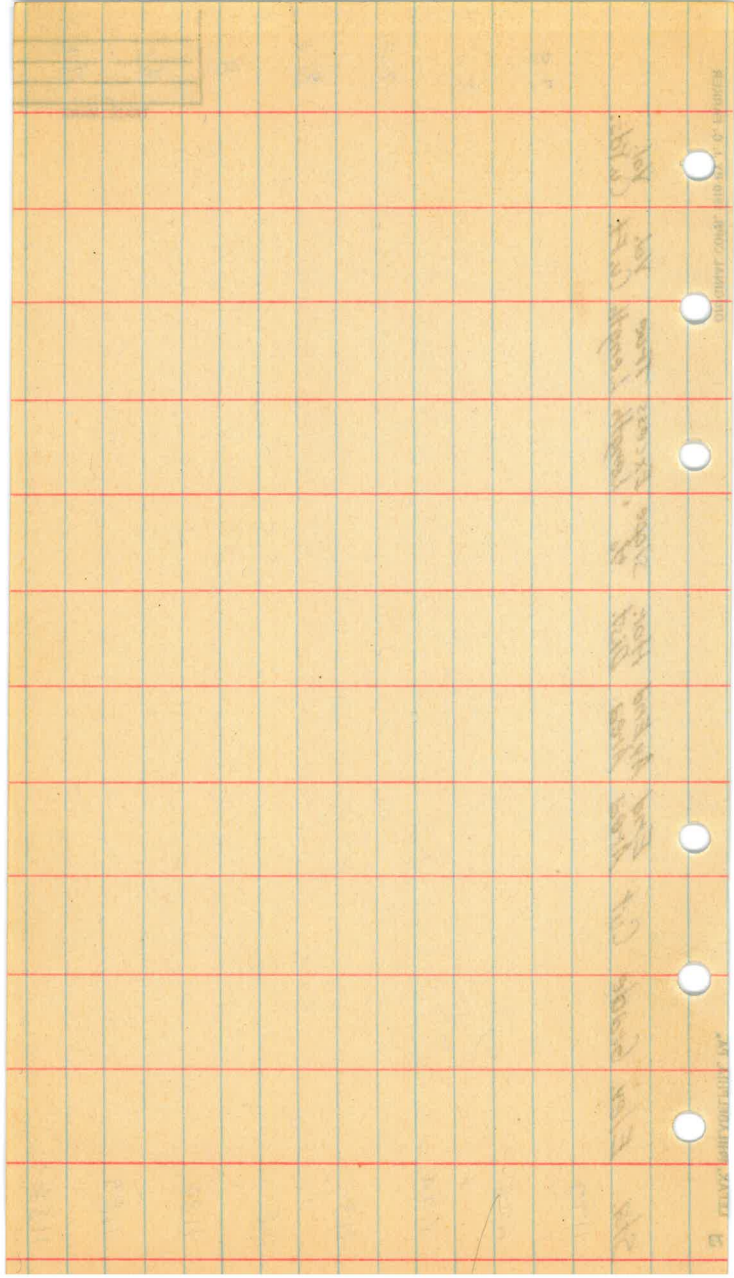


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Sta	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1177										7.8
1178										8.0
1179										7.4
1180										8.0
1181										8.0
1182										8.0
1183										9.0
1184										9.2

TRADE MARK



NOT  
DATE  
TIME  
PLACE

THE UNIVERSITY OF CHICAGO PRESS

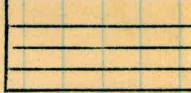


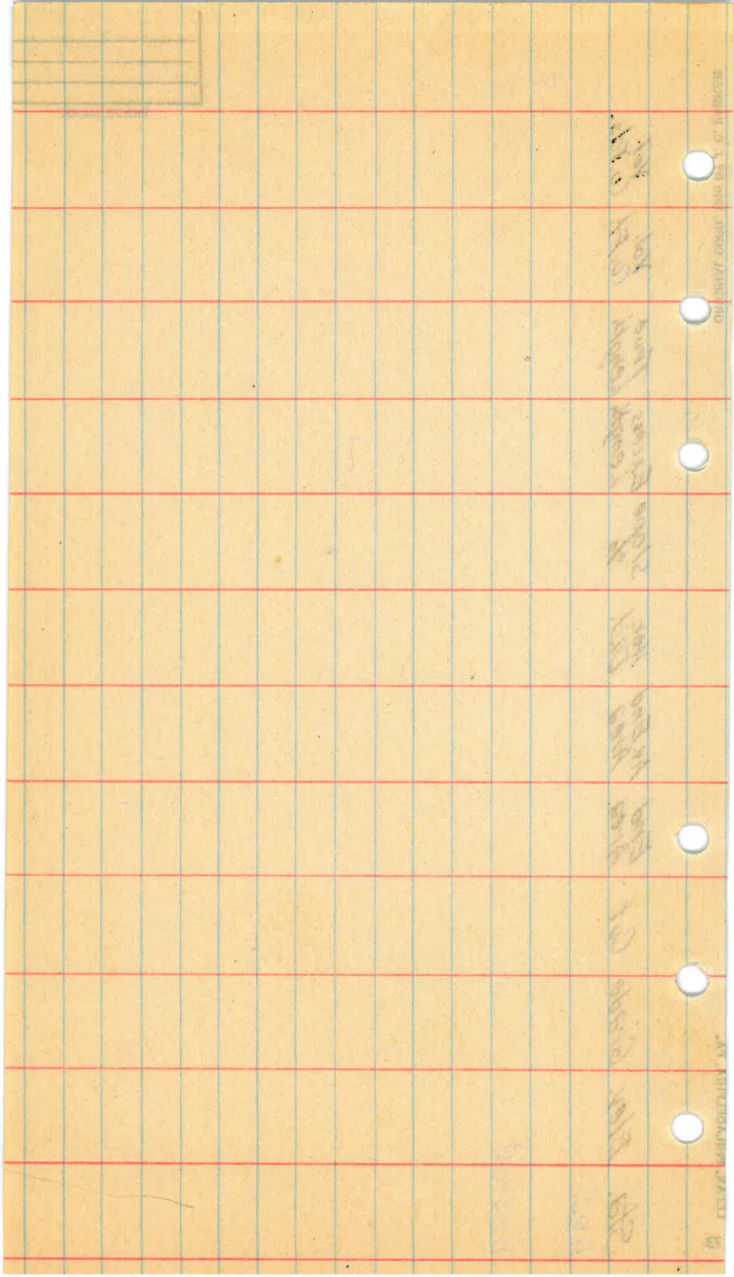
Sta.	Elev.	Grade	Cut.	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1184											9.0
1185											

1184

1185

9.0





THE SHIRT COMPANY 100 N. Y. ST. N. J. 07030

THE SHIRT COMPANY 100 N. Y. ST. N. J. 07030

Sta	Elev.	Grade	Cut	End Area	Av End Area	Hor Dist	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1115										8.8	8.8
1116										7.6	7.6
1117										7.6	7.6
1118										8.8	8.8
1119										9.0	9.0
1120										7.8	7.8
1121										8.0	8.0
1122											

TRADE MARK





Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Cu. Ft.	Vol. Cu. Yds.
1108									6.0
1109									6.2
1110									6.0
1111									
1112 #30									
1113									
1114									
1115									

End Area

Hor. Dist.

Slope %

Excess Length

True Cu. Ft.

Vol. Cu. Yds.

Note - Allow 1:2 Slopes for Ditch bet. Sta. 1101 to Sta. 1111+00.

From Sta. 1101+00 - East - Allow regular slopes.

0.0

0.0

8.6

8.0

10.2

TRADE MARK



Sta	Elev.	Grade	Cut	Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1105										
1106										
1107										
1108										

1105  
1106  
1107  
1108





Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hbr. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1143464	180.72	180.72	0.0	—	17.2	11.0	2%	0.005	11.005	189.3	
1143475	186.7	182.50	6.2	34.4	59.9	15.0	2%	0.005	15.005	895.8	
1143490	192.3	180.20	12.1	85.0	79.6	10.0	2%	0.005	10.005	196.2	
1144100	191.0	180.00	11.0	74.2	61.9	25.0	13%	0.21	25.21	1560.5	
1144125	184.9	176.67	8.2	49.6	47.2	25.0	13%	0.21	25.21	1189.9	
1144150	180.9	173.33	7.6	44.8	46.8	25.0	13%	0.21	25.21	1179.8	
1144175	178.1	170.00	8.1	48.8	33.2	25.0	13%	0.21	25.21	837.0	
1145100	175.3	166.67	3.6	17.6					17660.5	17660.5	77660.7

901499

Handwritten notes on a piece of aged, yellowed paper with blue horizontal lines and red vertical margin lines. The text is written in cursive and is mostly illegible due to fading and the age of the document. The notes are organized into several columns, with some numbers and words visible. At the top left, there is a small rectangular box containing some faint markings. On the right side of the page, there are four circular punch holes. At the bottom of the page, there is a small, faint stamp or mark.

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Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
1145+00	175.3	166.67	3.6	17.6	37.4	25.0	13%	0.21	25.21	942.9	943.2
1145+25	172.4	163.33	9.1	57.1	45.8	25.0	13%	0.21	25.21	1155.6	
1145+50	166.2	160.00	6.2	34.4	31.0	25.0	4%	0.02	25.02	775.6	
1145+75	164.2	159.00	5.2	27.6	31.4	25.0	4%	0.02	25.02	785.6	
1146+00	164.3	158.00	6.3	35.1	43.8	25.0	4%	0.02	25.02	1070.9	
1146+25	165.3	157.00	8.3	50.4	55.9	25.0	4%	0.02	25.02	1398.6	
1146+50	165.6	156.00	9.6	61.4	60.1	25.0	18%	0.40	25.40	1526.5	
1146+75	160.8	151.50	9.3	58.8				1842.64		1844.26	6827.62

DATE	DESCRIPTION	AMOUNT	CHECK NO.	BANK	BALANCE
1/1/20	OPENING BALANCE	100.00			100.00
1/5/20	DEPOSIT	50.00	101	ABC BANK	150.00
1/10/20	PAYROLL	25.00	102	ABC BANK	125.00
1/15/20	DEPOSIT	75.00	103	ABC BANK	200.00
1/20/20	RENT	100.00	104	ABC BANK	100.00
1/25/20	DEPOSIT	100.00	105	ABC BANK	200.00
1/30/20	UTILITY	50.00	106	ABC BANK	150.00
2/5/20	DEPOSIT	150.00	107	ABC BANK	300.00
2/10/20	PAYROLL	75.00	108	ABC BANK	225.00
2/15/20	DEPOSIT	100.00	109	ABC BANK	325.00
2/20/20	RENT	100.00	110	ABC BANK	225.00
2/25/20	DEPOSIT	100.00	111	ABC BANK	325.00
2/28/20	UTILITY	50.00	112	ABC BANK	275.00
3/5/20	DEPOSIT	150.00	113	ABC BANK	425.00
3/10/20	PAYROLL	75.00	114	ABC BANK	350.00
3/15/20	DEPOSIT	100.00	115	ABC BANK	450.00
3/20/20	RENT	100.00	116	ABC BANK	350.00
3/25/20	DEPOSIT	100.00	117	ABC BANK	450.00
3/28/20	UTILITY	50.00	118	ABC BANK	400.00
3/31/20	CLOSING BALANCE				400.00



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TRADE MARK

Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
114675	160.8	151.50	9.3	58.8	57.1	29.5	18%	0.48 0.40	29.98 29.90	1711.9	✓
114704 <sup>5</sup>	155.1	146.19	8.9	55.4	46.4	25.0	18%	0.40	25.40	1178.6	✓
114729 <sup>5</sup>	148.3	141.69	6.6	37.3	39.6	25.0	18%	0.40	25.40	1005.8	
114754 <sup>5</sup>	144.5	137.28	7.2	41.8	38.8	25.0	16%	0.32	25.32	982.4	7068.8
114779 <sup>5</sup>	139.7	133.28	6.4	35.8	33.0	25.0	16%	0.32	25.32	835.6	
114804 <sup>5</sup>	135.2	129.64	5.6	30.2	35.2	25.0	8%	0.08 <del>190861.3</del> 190852.0	25.08	882.8	
114829 <sup>5</sup>	132.6	127.64	7.0	40.2				190861.3 190861.3	190,857.1		

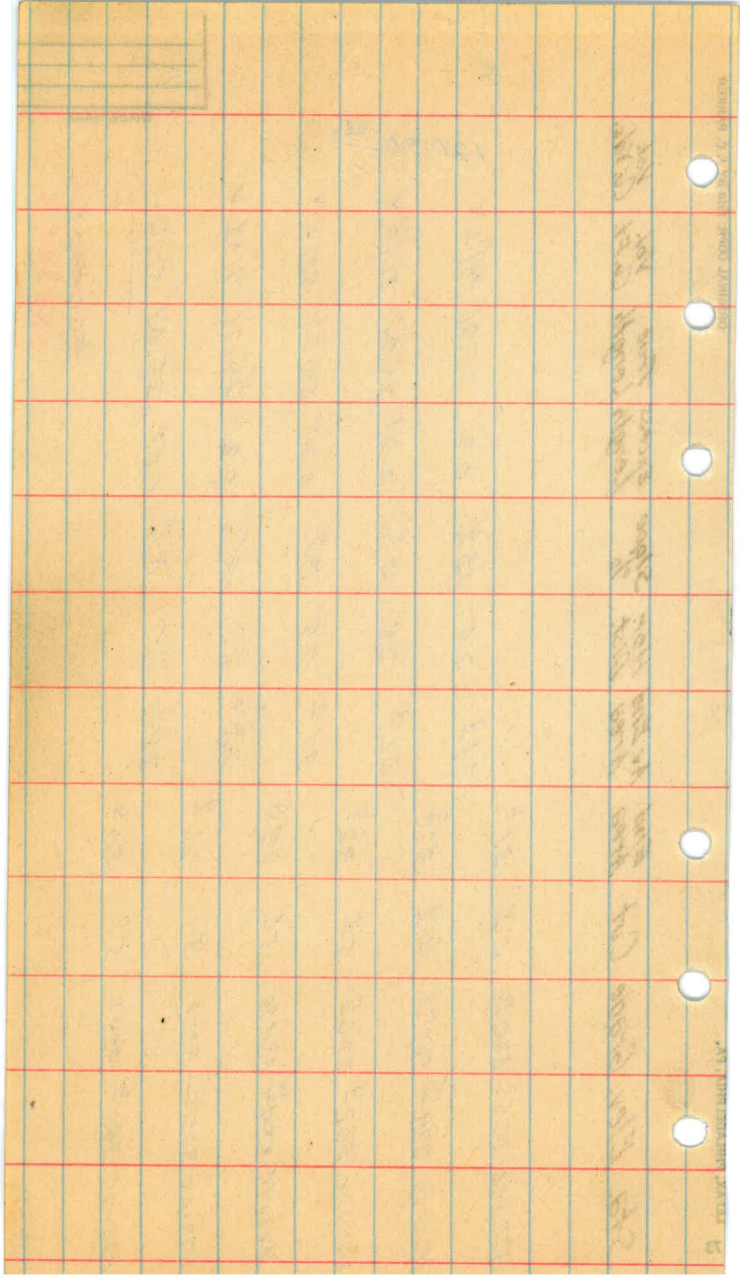


Sta. Elev. Grade Cut End Area Hor. Dist. Slope % Excess True Length Vol. Cu. Yds. Vol. Cu. Yds.

122+00	325 <sup>8</sup>	320 <sup>0</sup>	5 <sup>8</sup>	31 <sup>6</sup>	25	13%	0.2	25.2	791 <sup>6</sup> ✓	12050 <sup>6</sup>	7.2
122+25	329 <sup>15</sup>	323 <sup>25</sup>	5 <sup>9</sup>	32 <sup>2</sup>	25	13%	0.2	25.2	814 <sup>2</sup> ✓		
122+50	332 <sup>4</sup>	326 <sup>5</sup>	5 <sup>9</sup>	32 <sup>2</sup>	25	13%	0.2	25.2	781 <sup>5</sup> ✓		
122+75	334 <sup>85</sup>	329 <sup>15</sup>	5 <sup>5</sup>	29 <sup>6</sup>	25	13%	0.2	25.2	710 <sup>2</sup> ✓		
123+00	335 <sup>25</sup>	333 <sup>0</sup>	5 <sup>1</sup>	26 <sup>9</sup>	25	8%	0.08	25.08	717 <sup>2</sup> ✓		
123+25	340 <sup>6</sup>	335 <sup>0</sup>	5 <sup>6</sup>	30 <sup>2</sup>							

~~326508~~  
325367.9

TRADE MARK



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Sta.	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
123+25	340 <sup>6</sup>	335 <sup>0</sup>	5 <sup>6</sup>	30 <sup>2</sup>	25	8%	0.08	25.08	759 <sup>4</sup>	✓
123+50	342 <sup>6</sup>	337 <sup>2</sup>	5 <sup>6</sup>	30 <sup>2</sup>	25	8%	0.08	25.08	810 <sup>4</sup>	✓
123+75	343 <sup>03</sup>	336 <sup>03</sup>	6 <sup>3</sup>	34 <sup>4</sup>	25	0.7%	0.06	25.06	872 <sup>4</sup>	✓
124+00	342 <sup>90</sup>	336 <sup>67</sup>	6 <sup>3</sup>	35 <sup>1</sup>	25	0.7%	0.06	25.06	889 <sup>4</sup>	✓
124+25	342 <sup>90</sup>	336 <sup>50</sup>	6 <sup>4</sup>	35 <sup>8</sup>	25	0.7%	0.06	25.06	892 <sup>4</sup>	✓
124+50	342 <sup>43</sup>	336 <sup>33</sup>	6 <sup>1</sup>	33 <sup>1</sup>	25	0.7%	0.06	25.06	801 <sup>2</sup>	✓
124+75	341 <sup>16</sup>	336 <sup>16</sup>	5 <sup>6</sup>	30 <sup>2</sup>	25	0.7%	0.06	25.06	801 <sup>2</sup>	✓

12235<sup>87</sup>

~~331504.5~~  
330.368.6

TRADE MARK

7.8

^

9.4

DATE	DESCRIPTION	AMOUNT	BALANCE
1/1	Balance		100.00
1/2	...	...	...
1/3	...	...	...
1/4	...	...	...
1/5	...	...	...
1/6	...	...	...
1/7	...	...	...
1/8	...	...	...
1/9	...	...	...
1/10	...	...	...
1/11	...	...	...
1/12	...	...	...
1/13	...	...	...
1/14	...	...	...
1/15	...	...	...
1/16	...	...	...
1/17	...	...	...
1/18	...	...	...
1/19	...	...	...
1/20	...	...	...
1/21	...	...	...
1/22	...	...	...
1/23	...	...	...
1/24	...	...	...
1/25	...	...	...
1/26	...	...	...
1/27	...	...	...
1/28	...	...	...
1/29	...	...	...
1/30	...	...	...
1/31	...	...	...
TOTAL			...

THE UNIVERSITY OF THE STATE OF NEW YORK  
 OFFICE OF THE COMPTROLLER OF THE STATE

Sta	Elev.	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1124+75	341 <sup>7</sup> / <sub>16</sub>	336 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	30 <sup>2</sup>	25	0.7%	0.06	25.06	699 <sup>2</sup> / <sub>16</sub>	✓
1125+00	340 <sup>2</sup> / <sub>16</sub>	336 <sup>0</sup> / <sub>16</sub>	4 <sup>2</sup> / <sub>16</sub>	25 <sup>1</sup> / <sub>2</sub>	25	8%	0.08	25.08	770 <sup>0</sup> / <sub>16</sub>	✓
1125+25	340 <sup>4</sup> / <sub>16</sub>	334 <sup>0</sup> / <sub>16</sub>	6 <sup>4</sup> / <sub>16</sub>	35 <sup>2</sup> / <sub>16</sub>	25	8%	0.08	25.08	917 <sup>2</sup> / <sub>16</sub>	✓
1125+50	338 <sup>6</sup> / <sub>16</sub>	332 <sup>0</sup> / <sub>16</sub>	6 <sup>6</sup> / <sub>16</sub>	37 <sup>2</sup> / <sub>16</sub>	25	8%	0.08	25.08	872 <sup>2</sup> / <sub>16</sub>	✓
1125+75	335 <sup>8</sup> / <sub>16</sub>	330 <sup>0</sup> / <sub>16</sub>	5 <sup>8</sup> / <sub>16</sub>	32 <sup>2</sup> / <sub>16</sub>	25	8%	0.08	25.08	757 <sup>4</sup> / <sub>16</sub>	✓
1126+00	333 <sup>10</sup> / <sub>16</sub>	328 <sup>0</sup> / <sub>16</sub>	5 <sup>10</sup> / <sub>16</sub>	28 <sup>2</sup> / <sub>16</sub>	25	14%	0.24	25.24	797 <sup>6</sup> / <sub>16</sub>	✓
1126+25	330 <sup>12</sup> / <sub>16</sub>	324 <sup>0</sup> / <sub>16</sub>	6 <sup>12</sup> / <sub>16</sub>	25 <sup>1</sup> / <sub>2</sub>						

1241420  
8.14

3363194  
335183.5

TRADE MARK

DATE	DESCRIPTION	AMOUNT	CHECK NO.	BANK	INITIALS
1/15/20	...	...	...	...	...
1/20/20	...	...	...	...	...
1/25/20	...	...	...	...	...
2/1/20	...	...	...	...	...
2/5/20	...	...	...	...	...
2/10/20	...	...	...	...	...
2/15/20	...	...	...	...	...
2/20/20	...	...	...	...	...
2/25/20	...	...	...	...	...
3/1/20	...	...	...	...	...
3/5/20	...	...	...	...	...
3/10/20	...	...	...	...	...
3/15/20	...	...	...	...	...
3/20/20	...	...	...	...	...
3/25/20	...	...	...	...	...
4/1/20	...	...	...	...	...
4/5/20	...	...	...	...	...
4/10/20	...	...	...	...	...
4/15/20	...	...	...	...	...
4/20/20	...	...	...	...	...
4/25/20	...	...	...	...	...
5/1/20	...	...	...	...	...
5/5/20	...	...	...	...	...
5/10/20	...	...	...	...	...
5/15/20	...	...	...	...	...
5/20/20	...	...	...	...	...
5/25/20	...	...	...	...	...
6/1/20	...	...	...	...	...
6/5/20	...	...	...	...	...
6/10/20	...	...	...	...	...
6/15/20	...	...	...	...	...
6/20/20	...	...	...	...	...
6/25/20	...	...	...	...	...
7/1/20	...	...	...	...	...
7/5/20	...	...	...	...	...
7/10/20	...	...	...	...	...
7/15/20	...	...	...	...	...
7/20/20	...	...	...	...	...
7/25/20	...	...	...	...	...
7/31/20	...	...	...	...	...

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 DATE 01-15-20 BY 60322 UCBAW/STP



Sta.	Elev.	Grade	Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
126+25	330.8	324.5	6.3	35.1	34.0	25	14%	0.24	25.24	<del>858.2</del> 857.2	8.6
126+50	329.0	321.0	6.0	33.0	32.6	25	14%	0.24	25.24	822.8	8.6
126+75	323.4	317.5	5.9	32.3	28.0	25	14%	0.24	25.24	706.2	8.6
127+00	318.6	314.0	4.6	23.1	20.4	25	7%	0.06	25.06	511.2	8.2
127+25	315.8	312.30	3.5	17.0	9.1	25	7%	0.06	25.06	<del>225.5</del> 228.2	8.2
127+50	310.9	310.4	0.5	1.2	0.6	2	7%	0.00	2.00	1.2	8.2
127+52			0	0						<del>587.45</del> 588.09.1	
											12529.96

TRADE MARK

DATE	DESCRIPTION	AMOUNT	BALANCE
1900	...	...	...
1901	...	...	...
1902	...	...	...
1903	...	...	...
1904	...	...	...
1905	...	...	...
1906	...	...	...
1907	...	...	...
1908	...	...	...
1909	...	...	...
1910	...	...	...
1911	...	...	...
1912	...	...	...
1913	...	...	...
1914	...	...	...
1915	...	...	...
1916	...	...	...
1917	...	...	...
1918	...	...	...
1919	...	...	...
1920	...	...	...
1921	...	...	...
1922	...	...	...
1923	...	...	...
1924	...	...	...
1925	...	...	...
1926	...	...	...
1927	...	...	...
1928	...	...	...
1929	...	...	...
1930	...	...	...
1931	...	...	...
1932	...	...	...
1933	...	...	...
1934	...	...	...
1935	...	...	...
1936	...	...	...
1937	...	...	...
1938	...	...	...
1939	...	...	...
1940	...	...	...
1941	...	...	...
1942	...	...	...
1943	...	...	...
1944	...	...	...
1945	...	...	...
1946	...	...	...
1947	...	...	...
1948	...	...	...
1949	...	...	...
1950	...	...	...
1951	...	...	...
1952	...	...	...
1953	...	...	...
1954	...	...	...
1955	...	...	...
1956	...	...	...
1957	...	...	...
1958	...	...	...
1959	...	...	...
1960	...	...	...
1961	...	...	...
1962	...	...	...
1963	...	...	...
1964	...	...	...
1965	...	...	...
1966	...	...	...
1967	...	...	...
1968	...	...	...
1969	...	...	...
1970	...	...	...
1971	...	...	...
1972	...	...	...
1973	...	...	...
1974	...	...	...
1975	...	...	...
1976	...	...	...
1977	...	...	...
1978	...	...	...
1979	...	...	...
1980	...	...	...
1981	...	...	...
1982	...	...	...
1983	...	...	...
1984	...	...	...
1985	...	...	...
1986	...	...	...
1987	...	...	...
1988	...	...	...
1989	...	...	...
1990	...	...	...
1991	...	...	...
1992	...	...	...
1993	...	...	...
1994	...	...	...
1995	...	...	...
1996	...	...	...
1997	...	...	...
1998	...	...	...
1999	...	...	...
2000	...	...	...

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ANN ARBOR, MICHIGAN



DATE	DESCRIPTION	AMOUNT	BALANCE
1912	...	...	...
1913	...	...	...
1914	...	...	...
1915	...	...	...
1916	...	...	...
1917	...	...	...
1918	...	...	...
1919	...	...	...
1920	...	...	...
1921	...	...	...
1922	...	...	...
1923	...	...	...
1924	...	...	...
1925	...	...	...
1926	...	...	...
1927	...	...	...
1928	...	...	...
1929	...	...	...
1930	...	...	...
1931	...	...	...
1932	...	...	...
1933	...	...	...
1934	...	...	...
1935	...	...	...
1936	...	...	...
1937	...	...	...
1938	...	...	...
1939	...	...	...
1940	...	...	...
1941	...	...	...
1942	...	...	...
1943	...	...	...
1944	...	...	...
1945	...	...	...
1946	...	...	...
1947	...	...	...
1948	...	...	...
1949	...	...	...
1950	...	...	...
1951	...	...	...
1952	...	...	...
1953	...	...	...
1954	...	...	...
1955	...	...	...
1956	...	...	...
1957	...	...	...
1958	...	...	...
1959	...	...	...
1960	...	...	...
1961	...	...	...
1962	...	...	...
1963	...	...	...
1964	...	...	...
1965	...	...	...
1966	...	...	...
1967	...	...	...
1968	...	...	...
1969	...	...	...
1970	...	...	...
1971	...	...	...
1972	...	...	...
1973	...	...	...
1974	...	...	...
1975	...	...	...
1976	...	...	...
1977	...	...	...
1978	...	...	...
1979	...	...	...
1980	...	...	...
1981	...	...	...
1982	...	...	...
1983	...	...	...
1984	...	...	...
1985	...	...	...
1986	...	...	...
1987	...	...	...
1988	...	...	...
1989	...	...	...
1990	...	...	...
1991	...	...	...
1992	...	...	...
1993	...	...	...
1994	...	...	...
1995	...	...	...
1996	...	...	...
1997	...	...	...
1998	...	...	...
1999	...	...	...
2000	...	...	...
2001	...	...	...
2002	...	...	...
2003	...	...	...
2004	...	...	...
2005	...	...	...
2006	...	...	...
2007	...	...	...
2008	...	...	...
2009	...	...	...
2010	...	...	...
2011	...	...	...
2012	...	...	...
2013	...	...	...
2014	...	...	...
2015	...	...	...
2016	...	...	...
2017	...	...	...
2018	...	...	...
2019	...	...	...
2020	...	...	...
2021	...	...	...
2022	...	...	...
2023	...	...	...
2024	...	...	...
2025	...	...	...
2026	...	...	...
2027	...	...	...
2028	...	...	...
2029	...	...	...
2030	...	...	...
2031	...	...	...
2032	...	...	...
2033	...	...	...
2034	...	...	...
2035	...	...	...
2036	...	...	...
2037	...	...	...
2038	...	...	...
2039	...	...	...
2040	...	...	...
2041	...	...	...
2042	...	...	...
2043	...	...	...
2044	...	...	...
2045	...	...	...
2046	...	...	...
2047	...	...	...
2048	...	...	...
2049	...	...	...
2050	...	...	...

PERMANENT PAPER

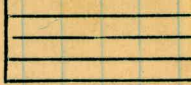
PERMANENT PAPER



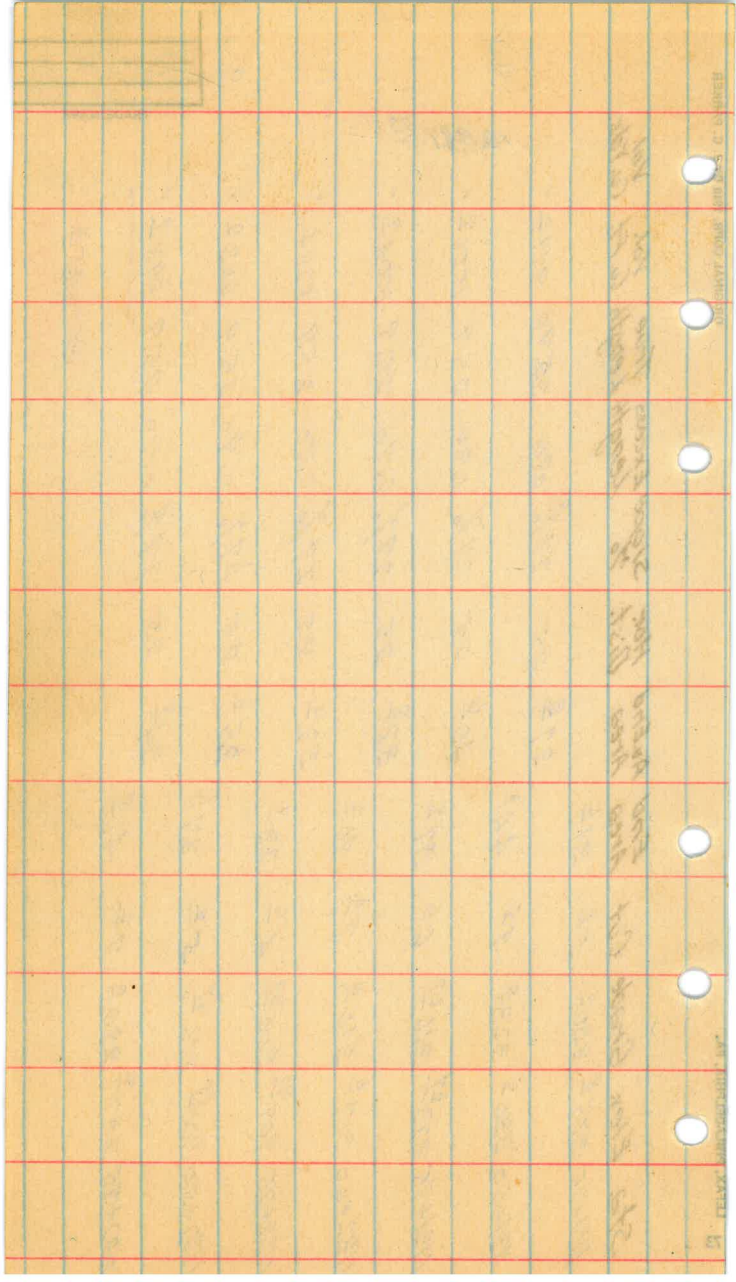
Sta.	Elev.	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1129+75	329 <sup>2</sup>	323 <sup>0</sup>	4 <sup>3</sup>	21 <sup>2</sup>	25 <sup>4</sup>	25	8%	0.08	25.08	637 <sup>0</sup>	✓
1130+00	332 <sup>4</sup>	327 <sup>0</sup>	5 <sup>4</sup>	28 <sup>2</sup>	29 <sup>6</sup>	25	8%	0.08	25.08	742 <sup>4</sup>	✓
1130+25	334 <sup>6</sup>	329 <sup>0</sup>	5 <sup>6</sup>	30 <sup>2</sup>	30 <sup>2</sup>	25	8%	0.08	25.08	775 <sup>0</sup>	✓
1130+50	336 <sup>8</sup>	331 <sup>0</sup>	5 <sup>8</sup>	31 <sup>6</sup>	30 <sup>2</sup>	25	8%	0.08	25.08	775 <sup>0</sup>	✓
1130+75	338 <sup>6</sup>	333 <sup>0</sup>	5 <sup>6</sup>	30 <sup>2</sup>	34 <sup>5</sup>	25	6%	0.04	25.04	863 <sup>2</sup>	✓
1131+00	338 <sup>2</sup>	331 <sup>5</sup>	6 <sup>3</sup>	28 <sup>8</sup>	35 <sup>2</sup>	25	6%	0.04	25.04	881 <sup>4</sup>	✓
1131+25	335 <sup>8</sup>	330 <sup>0</sup>	5 <sup>8</sup>	31 <sup>6</sup>							
										346219 <sup>2</sup>	
										345089.4	
											8.2
											12780 <sup>87</sup>



Sta.	Elev	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1131+25	335 <sup>8</sup>	330 <sup>0</sup>	5 <sup>8</sup>	31 <sup>6</sup>	37 <sup>0</sup>	25	27%	0.90	25.90	919 <sup>0</sup>	✓
1131+50	330 <sup>5</sup>	323 <sup>0</sup>	7 <sup>5</sup>	44 <sup>0</sup>	40 <sup>6</sup>	25	27%	0.90	25.9	1051 <sup>5</sup>	✓
1131+75	323 <sup>27</sup>	316 <sup>67</sup>	6 <sup>6</sup>	37 <sup>2</sup>	38 <sup>8</sup>	25	27%	0.90	25.9	1004 <sup>9</sup>	✓
1132+00	317 <sup>0</sup>	310 <sup>0</sup>	7 <sup>0</sup>	40 <sup>2</sup>	32 <sup>0</sup>	25	27%	0.90	25.9	828 <sup>8</sup>	✓
1132+25	307 <sup>93</sup>	303 <sup>33</sup>	4 <sup>6</sup>	23 <sup>1</sup>	25 <sup>6</sup>	25	27%	0.90	25.9	663 <sup>0</sup>	✓
1132+50	301 <sup>81</sup>	296 <sup>67</sup>	5 <sup>2</sup>	27 <sup>6</sup>	34 <sup>2</sup>	25	27%	0.90	25.9	898 <sup>1</sup>	✓
1132+75	297 <sup>2</sup>	290 <sup>0</sup>	7 <sup>2</sup>	41 <sup>8</sup>							
										<del>3576.95<sup>2</sup></del>	
										350509.3	

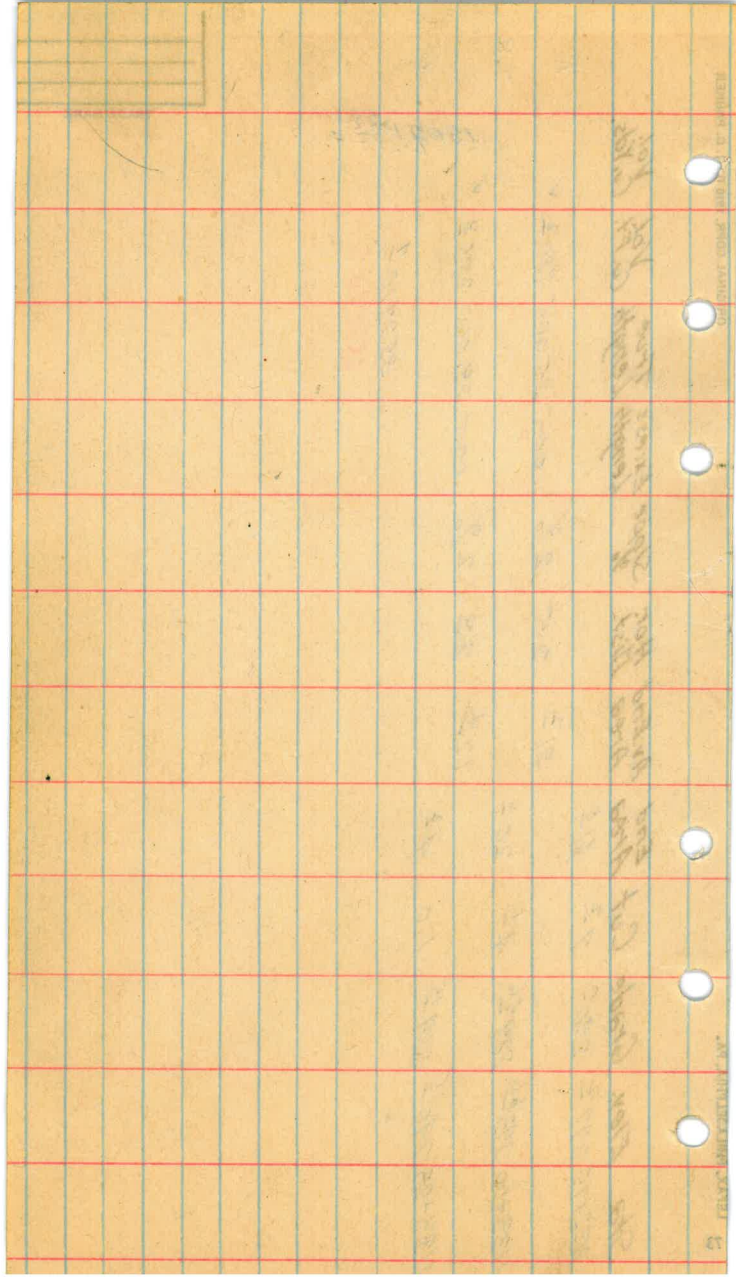
12981<sup>83</sup>

✓





Sta	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	% Slope	Excess Length	True Length	Vol. Cu. Yds.	Vol. Cu. Yds.
132+75	291 <sup>2</sup>	290 <sup>0</sup>	7 <sup>2</sup>	41 <sup>2</sup>	31 <sup>2</sup>	25	2%	.005	25.005	180 <sup>2</sup>	✓
133+00	293 <sup>6</sup>	289 <sup>5</sup>	4 <sup>1</sup>	20 <sup>2</sup>	12 <sup>2</sup>	23	2%	.005	28.005	285 <sup>2</sup>	✓
133+23	290 <sup>5</sup>	289 <sup>5</sup>	1.0	4 <sup>2</sup>							7.8
										13021	29
										352410	✓
										351574.8	



2 FRANKLIN COUNTY, N.Y.

OFFICE OF THE COUNTY CLERK

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1134765	286.6	286.62	0.0		0.4	10.0	2%	0.0	10.0	4.0	✓
1134775	286.6	286.44	0.2	0.8	5.4	25.0	2%	0.005	25.0	135.0	✓
1135700	288.2	286.00	2.2	10.0	17.2	25.0	5%	0.03	25.03	430.5	✓
1135725	289.4	284.67	4.7	24.3	22.4	25.0	5%	0.03	25.03	560.7	✓
1135750	287.4	283.33	4.1	20.6	21.2	25.0	5%	0.03	25.03	530.6	✓
1135775	286.3	282.00	4.3	21.8	32.9	25.0	20%	0.50	25.50	839.0	✓
1136700	284.5	277.00	7.5	44.0	49.8	25.0	20%	0.50	25.50	1142.4	✓
1136725	279.7	272.00	7.7	45.6				121,965.5	21,929.2		✓

TRADE MARK

36

DATE	DESCRIPTION	AMOUNT	BALANCE	DATE	DESCRIPTION	AMOUNT	BALANCE
1/1	BY BALANCE	100.00	100.00				
1/5	PAID	20.00	80.00				
1/10	RECEIVED	15.00	95.00				
1/15	PAID	10.00	85.00				
1/20	RECEIVED	30.00	115.00				
1/25	PAID	5.00	110.00				
1/30	RECEIVED	25.00	135.00				
2/5	PAID	18.00	117.00				
2/10	RECEIVED	12.00	129.00				
2/15	PAID	7.00	122.00				
2/20	RECEIVED	22.00	144.00				
2/25	PAID	14.00	130.00				
2/28	RECEIVED	18.00	148.00				
3/5	PAID	9.00	139.00				
3/10	RECEIVED	28.00	167.00				
3/15	PAID	11.00	156.00				
3/20	RECEIVED	20.00	176.00				
3/25	PAID	13.00	163.00				
3/30	RECEIVED	24.00	187.00				
4/5	PAID	16.00	171.00				
4/10	RECEIVED	26.00	197.00				
4/15	PAID	10.00	187.00				
4/20	RECEIVED	19.00	206.00				
4/25	PAID	12.00	194.00				
4/30	RECEIVED	21.00	215.00				
5/5	PAID	14.00	201.00				
5/10	RECEIVED	23.00	224.00				
5/15	PAID	17.00	207.00				
5/20	RECEIVED	27.00	234.00				
5/25	PAID	15.00	219.00				
5/30	RECEIVED	25.00	244.00				
6/5	PAID	18.00	226.00				
6/10	RECEIVED	29.00	255.00				
6/15	PAID	11.00	244.00				
6/20	RECEIVED	20.00	264.00				
6/25	PAID	13.00	251.00				
6/30	RECEIVED	22.00	273.00				
7/5	PAID	16.00	257.00				
7/10	RECEIVED	28.00	285.00				
7/15	PAID	10.00	275.00				
7/20	RECEIVED	19.00	294.00				
7/25	PAID	12.00	282.00				
7/30	RECEIVED	21.00	303.00				
8/5	PAID	14.00	289.00				
8/10	RECEIVED	26.00	315.00				
8/15	PAID	11.00	304.00				
8/20	RECEIVED	20.00	324.00				
8/25	PAID	13.00	311.00				
8/30	RECEIVED	23.00	334.00				
9/5	PAID	17.00	317.00				
9/10	RECEIVED	29.00	346.00				
9/15	PAID	10.00	336.00				
9/20	RECEIVED	19.00	355.00				
9/25	PAID	12.00	343.00				
9/30	RECEIVED	22.00	365.00				
10/5	PAID	16.00	349.00				
10/10	RECEIVED	28.00	377.00				
10/15	PAID	11.00	366.00				
10/20	RECEIVED	20.00	386.00				
10/25	PAID	13.00	373.00				
10/30	RECEIVED	23.00	396.00				
11/5	PAID	17.00	379.00				
11/10	RECEIVED	29.00	408.00				
11/15	PAID	10.00	398.00				
11/20	RECEIVED	19.00	417.00				
11/25	PAID	12.00	405.00				
11/30	RECEIVED	22.00	427.00				
12/5	PAID	16.00	411.00				
12/10	RECEIVED	28.00	439.00				
12/15	PAID	11.00	428.00				
12/20	RECEIVED	20.00	448.00				
12/25	PAID	13.00	435.00				
12/30	RECEIVED	23.00	458.00				

THE UNIVERSITY OF CHICAGO

THE UNIVERSITY OF CHICAGO



Sta	Elev.	Grade	Cut	End Area	Avg End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1136+25	279.7	272.00	7.7	45.6	44.8	25.0	20%	0.50	25.50	147.4	✓
1136+50	274.5	267.00	7.5	44.0	41.0	19.6	20%	0.39	19.99	819.6	✓
1136+86	269.8	263.08	6.7	38.0	32.1	25.0	20%	0.50	25.50	818.6	✓
1136+96	263.1	258.08	5.0	26.2	25.0	25.0	20% 22%	0.58	25.58	639.5	✓
1137+26	257.2	252.61	4.6	23.7	21.8	25.0	22%	0.60	25.60	558.1	✓
1137+46	251.0	247.01	4.0	20.0	23.1	25.0	22%	0.60	25.60	591.4	✓
1137+89	246.4	241.41	5.0	26.2	30.6	25.0	22%	0.60	25.60	783.4	✓
1137+99	242.1	235.81	6.3	35.1			12.7, 318.5			127, 282.2	✓

TRADE MARK

F 91 # 2

27  
~~114.16~~  
~~115.50~~  
 8.2

Handwritten notes on a yellowed, lined page with red vertical margin lines and four punch holes on the right side. The text is written in blue ink and is mostly illegible due to fading and bleed-through from the reverse side. A small rectangular stamp is visible in the top left corner. The page is oriented vertically on the page.

2 TELUX INTYDORHT BY

ONE THIRTY FOUR TWO SIX FOUR

Sta.	Elev.	Grade	Cut	End Area	Av. End Area	Hbr. Dist.	Slippe %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1137+94.6	242.1	235.81	6.3	35.1	32.4	25.0	22%	0.60	25.60	829.4	✓
1138+19.6	235.7	230.21	5.5	29.6	31.6	25.0	22% 8%	0.19	25.19	796.0	✓
1138+44.6	233.6	227.99	6.1	33.7	29.4	25.0	8%	0.08	25.08	737.4	✓
1138+69.6	230.4	225.57	4.8	25.0	26.3	25.0	8%	0.08	25.08	659.6	✓
1138+94.6	228.8	223.65	5.2	27.6	26.9	9.2	8%	0.03	9.23	248.3	✓
1139+03.8	227.9	222.92	5.0	26.2	28.9	21.2	8%	0.07	21.27	614.7	✓
1139+25	227.1	221.29	5.8	31.6	30.9	25.0	8%	0.08	25.08	715.0	✓
1139+50	225.0	219.36	5.6	30.2			13%	978.9		137,942.6	

8.6

(28)

~~4886.16~~  
11888.1

Est 72

TRADE MARK

1  
2

TELETYPE UNIT "A"  
COMMUNICATIONS SECTION  
U.S. AIR FORCE  
WALLINGFORD AIR FORCE BASE  
WALLINGFORD, VERMONT

TO: SAC, BOSTON  
FROM: SAC, WASHINGTON  
SUBJECT: [Illegible]

[Faint, mostly illegible teletype text follows]



3 LEFAX, PHILADELPHIA, PA.

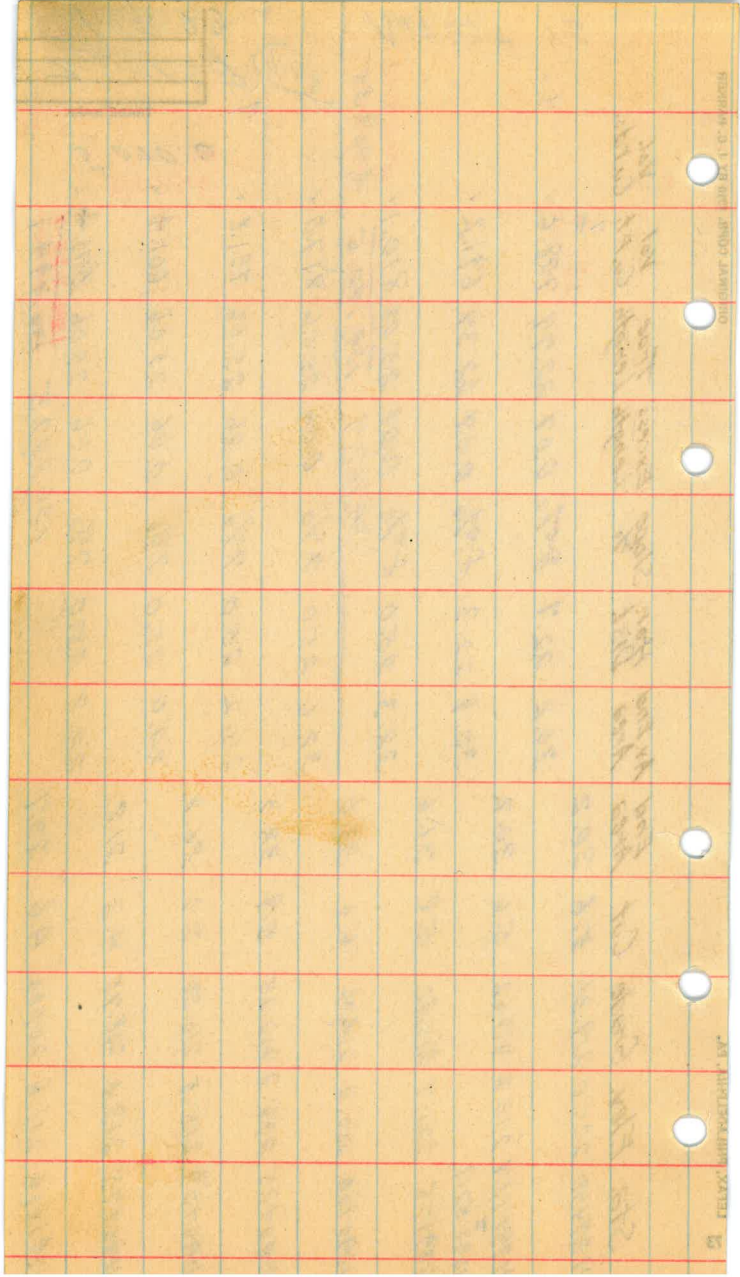
ORIGINAL COPR. 1910 BY J. C. PARKER

Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1139+50	225.0	219.36	5.6	30.2	30.2	22.7	8%	0.07	22.77	687.6	9.0
1139+75	223.2	217.62	5.6	30.2	30.9	22.3	8%	0.07	22.37	691.2	✓
1139+52.7											
1139+75	221.7	215.92	5.8	31.6	32.3	25.0	8%	0.08	25.08	810.1	✓ 4969.18
1190+00	220.0	214.00	6.0	33.0	32.6	25.0	7%	0.06	25.06	817.0	✓
1190+25	228.2	212.25	5.9	32.3	29.2	25.0	7%	0.06	25.06	731.8	✓
1190+50	215.5	210.50	5.0	26.2	24.0	25.0	7%	0.06	25.06	601.4	✓
1190+75	213.0	208.75	4.3	21.8	22.8	25.0	7%	0.06	25.06	571.4	✓
1191+00	211.6	207.00	4.6	23.7			136.8895			156.094.1	

August 16

(29)

Aug. 23  
7/15  
TRADE MARK  
5070.0  
5070.0



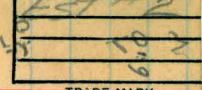
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3

Sta.	Elev. Grade	Cut	End Area	Av. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Cords.
1141+00	211.6	207.00	4.6	23.7	25.0	7%	0.06	25.06	676.6	✓
1141+25	210.8	205.25	5.6	30.2	25.0	7%	0.06	25.06	659.1	✓
1141+50	207.9	203.50	4.4	22.4	25.0	7%	0.06	25.06	546.3	✓
1141+75	206.0	201.75	4.2	21.2	25.0	7%	0.06	25.06	611.5	✓
1142+00	205.2	200.00	5.2	27.6	25.0	34%	1.41	26.41	1327.3	✓
1142+25	203.3	191.50	11.8	82.0	25.0	34%	1.41	26.41	1327.3	✓
1142+50	192.0	183.00	9.0	56.2	14.0	2%	-	14.0	393.4	✓
1142+64		0.0				143	048.6	142	924.5	✓

(30)



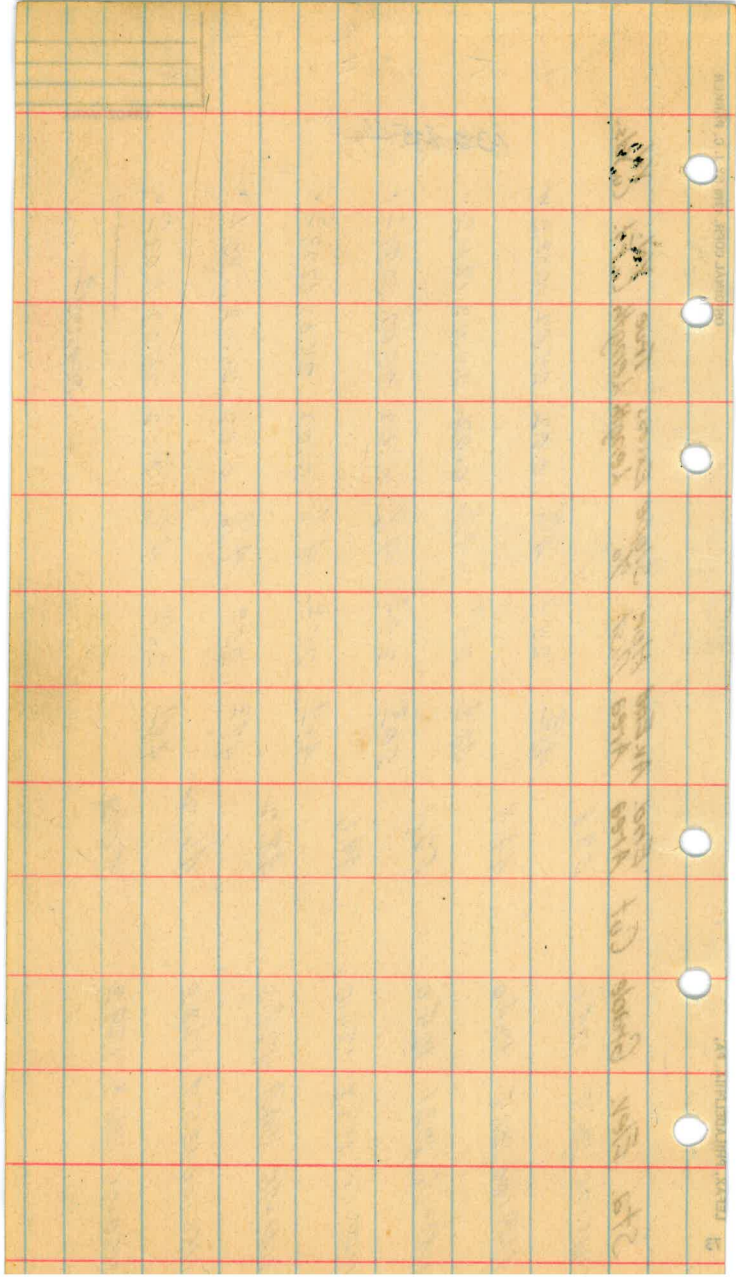
TRADE MARK







Sta.	Elev.	Grade	Cut	End. Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
148+75	131.5	125.0		37.8	41.3	25°	4%	0.02	25.02	1039.3	10.4
149+00	131.5	124.0		44.8	48.4	25°	4%	0.02	25.02	1211.0	1
149+25	133.1	125.0		52.1	50.8	25°	4%	0.02	25.02	1271.0	13285.11
149+50	133.8	126.0		49.6	48.9	25°	4%	0.02	25.02	1223.5	11.0
149+75	134.9	127.0		48.2	47.3	25°	4%	0.02	25.02	1180.9	
150+00	135.7	128.0		46.2	48.1	25°	4%	0.02	25.02	1203.5	
150+25	136.3	129.0		50.2							
										3598.35	
										358698.0	



10/20  
10/21  
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10/23  
10/24  
10/25  
10/26  
10/27  
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10/29  
10/30  
10/31

2. FLYNN UNIVERSITY, NY

3 LEFAX, PHILADELPHIA, PA.

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Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slippe %	Excess Length	Top Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1150+35	136.3	129.0		50.0	50.1	25.0	4%	0.02	25.02	1253.5	✓
1150+50	137.2	130.0		50.2	47.4	25.0	4%	0.02	25.02	1185.9	✓
1150+75	137.7	131.0		44.1	44.2	25.0	4%	0.02	25.02	1105.1	✓
1151+00	138.5	132.0		43.6	39.6	25.0	3%	0.01	25.01	988.2	✓
1151+25	139.1	132.8		35.5	36.2	25.0	3%	0.01	25.01	905.2	✓
1151+50	139.7	133.5		36.8	36.1	25.0	3%	0.01	25.01	915.2	✓
1151+75	140.4	134.2		31.4							
										13,520.54	8.6
										990.4	✓
										988.2	✓
										8.6	✓
										3733.36	✓
										365.054.5	✓

TRADE MARK

№	Имя	Фамилия	Отчество	Дата рождения	Место рождения	Место работы	Стаж	Звание	Специальность	Среднее образование	Среднее специальное образование	Высшее образование	Стаж в профессии	Стаж в должности	Стаж в организации	Стаж в отрасли	Стаж в стране	Стаж в мире	Стаж в семье	Стаж в браке	Стаж в детстве	Стаж в юности	Стаж в зрелости	Стаж в старости	Стаж в жизни																																																																																																																																																																																												
1	Иван	Иванов	Иванович	1950	Москва	Инженер	10	Инженер	Инженер	Среднее	Среднее специальное	Высшее	15	5	10	15	20	25	30	35	40	45	50	55	60	65	70	75	80	85	90	95	100	105	110	115	120	125	130	135	140	145	150	155	160	165	170	175	180	185	190	195	200	205	210	215	220	225	230	235	240	245	250	255	260	265	270	275	280	285	290	295	300	305	310	315	320	325	330	335	340	345	350	355	360	365	370	375	380	385	390	395	400	405	410	415	420	425	430	435	440	445	450	455	460	465	470	475	480	485	490	495	500	505	510	515	520	525	530	535	540	545	550	555	560	565	570	575	580	585	590	595	600	605	610	615	620	625	630	635	640	645	650	655	660	665	670	675	680	685	690	695	700	705	710	715	720	725	730	735	740	745	750	755	760	765	770	775	780	785	790	795	800	805	810	815	820	825	830	835	840	845	850	855	860	865	870	875	880	885	890	895	900	905	910	915	920	925	930	935	940	945	950	955	960	965	970	975	980	985	990	995	1000

ТОВАРИЩАМ НАШЕГО ПУТИ



LEFAX, PHILADELPHIA, PA.

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Sta. Elev.	Grade Cut	End Area	Average Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cut Ft.	Vol. Cu Yds.
1151+75	140.4	134.2	36.4	25.0	3%	0.01	25.01	935.4	✓
1152+00	141.2	135.0	38.5	25.0	3%	0.01	25.01	1022.1	✓
1152+25	142.0	135.8	43.2	25.0	3%	0.01	25.01	975.4	✓
1152+50	142.8	136.5	34.5	25.0	3%	0.01	25.01	860.2	✓
1152+75	143.0	137.2	34.2	25.0	3%	0.01	25.01	920.4	✓
1153+00	143.9	138.0	39.2	25.0	3%	0.01	25.01	1075.4	✓
1153+25	146.4	138.8	46.8						

13734  
12  
6.8

592583.4  
370844.3

TRADE MARK

DATE	DESCRIPTION	AMOUNT	CHECK NO.	BANK
12/1/50	...	...	...	...
12/2/50	...	...	...	...
12/3/50	...	...	...	...
12/4/50	...	...	...	...
12/5/50	...	...	...	...
12/6/50	...	...	...	...
12/7/50	...	...	...	...
12/8/50	...	...	...	...
12/9/50	...	...	...	...
12/10/50	...	...	...	...
12/11/50	...	...	...	...
12/12/50	...	...	...	...
12/13/50	...	...	...	...
12/14/50	...	...	...	...
12/15/50	...	...	...	...
12/16/50	...	...	...	...
12/17/50	...	...	...	...
12/18/50	...	...	...	...
12/19/50	...	...	...	...
12/20/50	...	...	...	...
12/21/50	...	...	...	...
12/22/50	...	...	...	...
12/23/50	...	...	...	...
12/24/50	...	...	...	...
12/25/50	...	...	...	...
12/26/50	...	...	...	...
12/27/50	...	...	...	...
12/28/50	...	...	...	...
12/29/50	...	...	...	...
12/30/50	...	...	...	...
12/31/50	...	...	...	...

RECORDS COMPANY

RECORDS COMPANY

Sta	Elev	Grade	Cut	End Area	Avg End Area	Hpr. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1153+25	146.4	138.8		46.8	52.2	25.0	3%	0.01	25.01	1305.5	✓
1153+50	149.9	139.5		57.2	56.4	25.0	3%	0.01	25.01	1410.6	✓
1153+75	148.8	140.2		55.0	54.0	25.0	3%	0.01	25.01	1350.6	✓
1154+00	147.8	141.0		53.1	51.2	22.2	3%	0.01	22.21	1197.2	✓
1154+22.2	149.0	141.2		49.2	43.8	27.8	3%	0.01	27.21	1191.8	✓
1154+50	149.1	142.5		38.2	36.2	25.0	3%	0.01	25.01	907.9	✓
1154+75	149.0	143.2		34.2						715.1	✓
										14,005.47	7.0
										4915.6	1
										378	8.0

4915.6  
378 147.8

DATE	DESCRIPTION	AMOUNT	BALANCE
10/10	10/10	100.00	100.00
10/11	10/11	100.00	200.00
10/12	10/12	100.00	300.00
10/13	10/13	100.00	400.00
10/14	10/14	100.00	500.00
10/15	10/15	100.00	600.00
10/16	10/16	100.00	700.00
10/17	10/17	100.00	800.00
10/18	10/18	100.00	900.00
10/19	10/19	100.00	1000.00
10/20	10/20	100.00	1100.00
10/21	10/21	100.00	1200.00
10/22	10/22	100.00	1300.00
10/23	10/23	100.00	1400.00
10/24	10/24	100.00	1500.00
10/25	10/25	100.00	1600.00
10/26	10/26	100.00	1700.00
10/27	10/27	100.00	1800.00
10/28	10/28	100.00	1900.00
10/29	10/29	100.00	2000.00
10/30	10/30	100.00	2100.00
10/31	10/31	100.00	2200.00

OFFICE OF THE COMPTROLLER

STATE OF NEW YORK



Sta	Elev	Grade	Cut	End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
1154+75	1490	1432		34 <sup>2</sup>	25.0	3%	0.01	25.01	832 <sup>2</sup>	✓
1155+00	1495	1440		32 <sup>2</sup>	25.0	3%	0.01	25.01	805 <sup>2</sup>	✓
1155+25	1500	1442		32 <sup>2</sup>	25.0	3%	0.01	25.01	810 <sup>2</sup>	✓
1155+50	1507	1452		32 <sup>2</sup>	25.0	3%	0.01	25.01	790 <sup>2</sup>	✓
1155+75	1512	1462		30 <sup>2</sup>	25.0	3%	0.01	25.01	745 <sup>2</sup>	✓
1156+00	1523	1470		29 <sup>2</sup>	25.0	3%	0.01	25.01	690 <sup>2</sup>	✓
1156+25	1526	1472		26 <sup>2</sup>	25.0	3%	0.01	25.01	690 <sup>2</sup>	✓
<del>382 822.1</del> 382 822.1										



Sta.	Elev.	Grade	Cut	End Area	Ax End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Cu. Ft.	Vol. Cu. Yds.
15625	152.6	147.8		26.2							
15645.0	153.8	148.5		27.1	27.0	25.0	3%	0.01	25.01	675.3	

26.2

147.8

27.1

148.5

27.0

25.0

3%

0.01

25.01

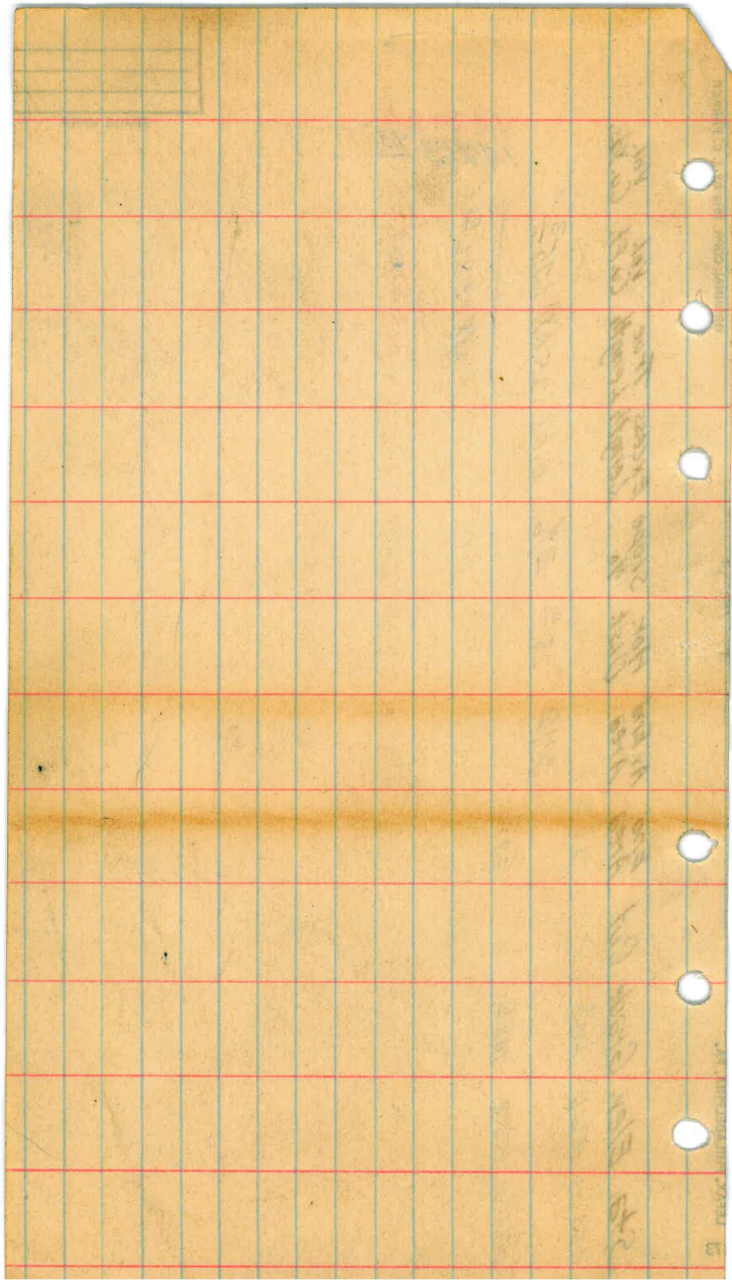
675.3

~~4823.26~~

383 497.4

14203.6  
~~17863.93~~

TRADE MARK



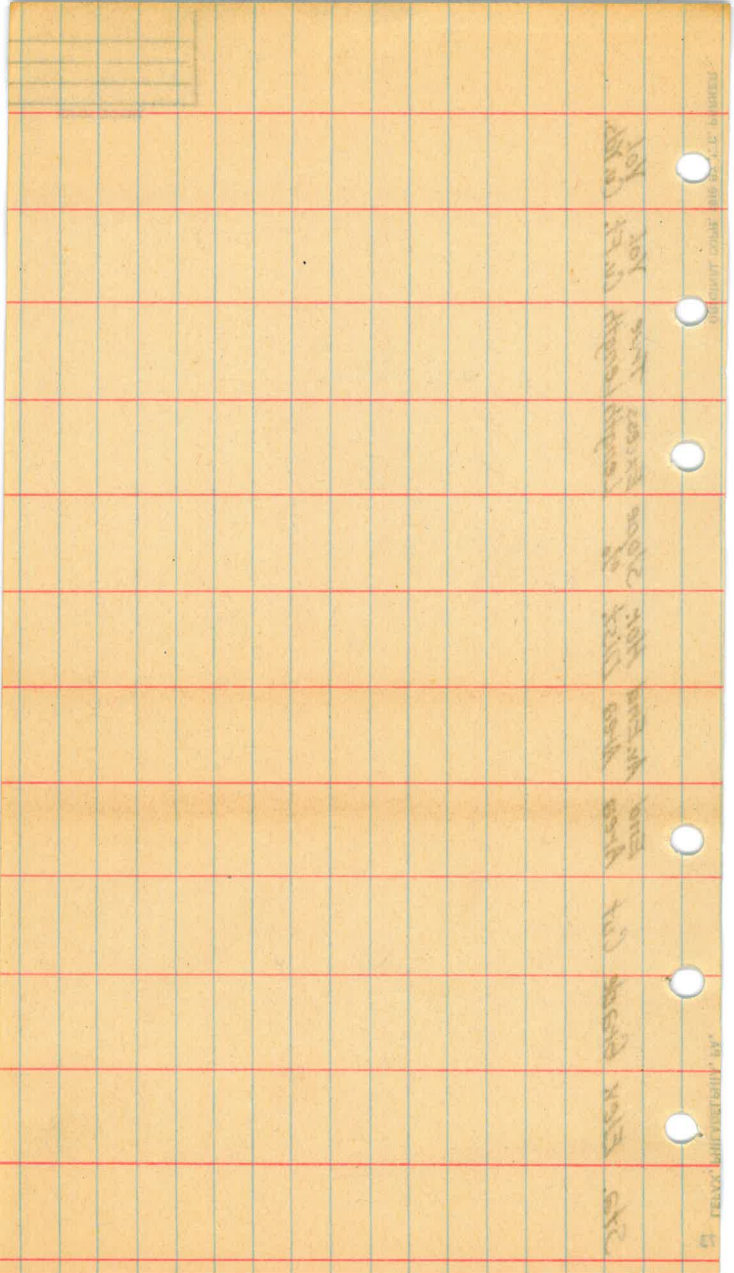


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<i>Sta.</i>	<i>Elev</i>	<i>Grade</i>	<i>Cut</i>	<i>End Area</i>	<i>Av. End Area</i>	<i>Hd. Dist.</i>	<i>Slope %</i>	<i>Excess Length</i>	<i>True Length</i>	<i>Vol. Cu. Yds.</i>	<i>Vol. Cu. Yds.</i>
-------------	-------------	--------------	------------	-----------------	---------------------	------------------	----------------	----------------------	--------------------	----------------------	----------------------

TRADE MARK



1900  
1901  
1902  
1903  
1904  
1905  
1906  
1907  
1908  
1909  
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1911  
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TELEX MICROFILM BY  
MICROFILM CARD 816 500 0000







Sta Elev. Grade Cut Area End Area Av. End Hor. Dist. slope % Excess Length True Length Cu. Ft. Cu. Yds.















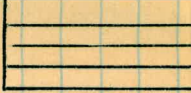




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Sta. Elev. Grade Cut Area Av. End Hor. Slope Excess True Vol. Vol.  
Area Area Area Dist. % Length Cu. Ft. Cu. Yds.



TRADE MARK



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Sta. Elev. Grade Cut Area End Area Hbr. Slope % Excess True Vol. Vol. Length Cu.Ft. Cu.Yds.

TRADE MARK





Lefax Notes of Relocation West of 810  
and Other Data on Lefax Sheets.



$\Delta = 25^\circ 20'$   
 $\frac{1}{2}\Delta = 12^\circ 40'$   
 $R = 572.96$   
 $190 + 00$   
 $128.8$   


---

 $188 + 71.2$   
 $253.3$   


---

 $19124.5$

$51296$   
 $.22475$   
 $286480$   
 $401.072$   
 $229184$   
 $114592$   
 $114592$   


---

 $3745$   
 $2520$   


---

 $6305$   


---

 $128.7727600$

$57296$   
 $.02494$   


---

 $229184$   
 $515664$   
 $229184$   
 $114592$   


---

 $142896224$   


---

 $10) 25.283$

$20.3$   
 $19.6$   


---

 $0.7$

$\Delta = 19^\circ 23'$   
 $\frac{1}{2}\Delta = 9^\circ 41.50'$   
 $D = 50$   
 $R = 114.59$   
 $T = 19.6$   
 $L = 38.8$

$38.76$   
 $50) 19.3833$   
 $150$   
 $438$   
 $400$   


---

 $383$   
 $350$   


---

 $333$   


---

 $168 + 33.8$   
 $19.6$   


---

 $168 + 14.2$   
 $38.8$   


---

 $16853.0$

$\Delta = 22^\circ 12' R$  Tan. 19619

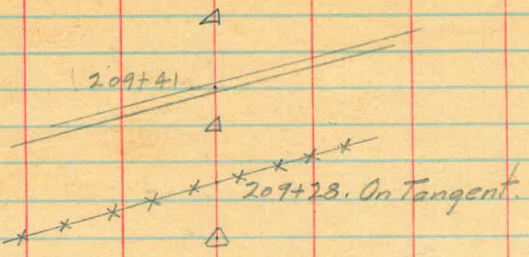
$\frac{1}{2}\Delta = 11^\circ 06'$  Ex. Sec. 01906

$D = 8^\circ$	19619
$R = 716.2$	<u>716.2</u>
$T = 140.5$	39238
$E = 13.7$	117714
$L = 277.5$	19619
	<u>137333</u>
	140511278

209+30	716.2
<u>140.5</u>	<u>.01906</u>
207+89.5	42972
<u>277.5</u>	644580
210+670	<u>7162</u>
	13650772
	<u>277.5</u>

	8) 22.2
	<u>16</u>
114.59	62
<u>17078</u>	<u>56</u>
91672	60
80213	<u>56</u>
802130	40
<u>114590</u>	
195696802	





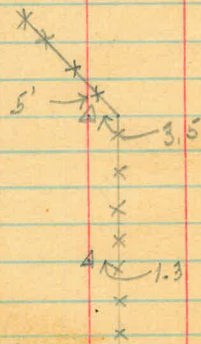
209+28

204+59

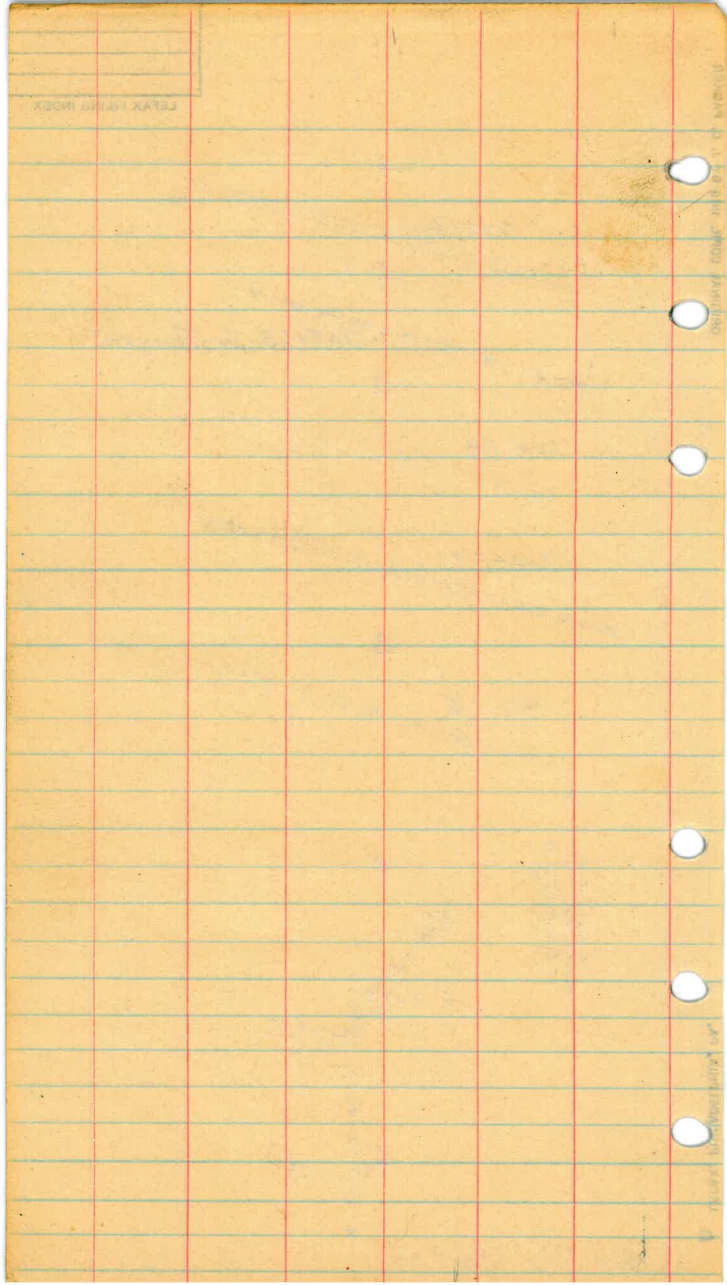
25°20R

197+76

Grain +  
Alfalfa



Old Sta. 186+00



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Reference Points

L

±

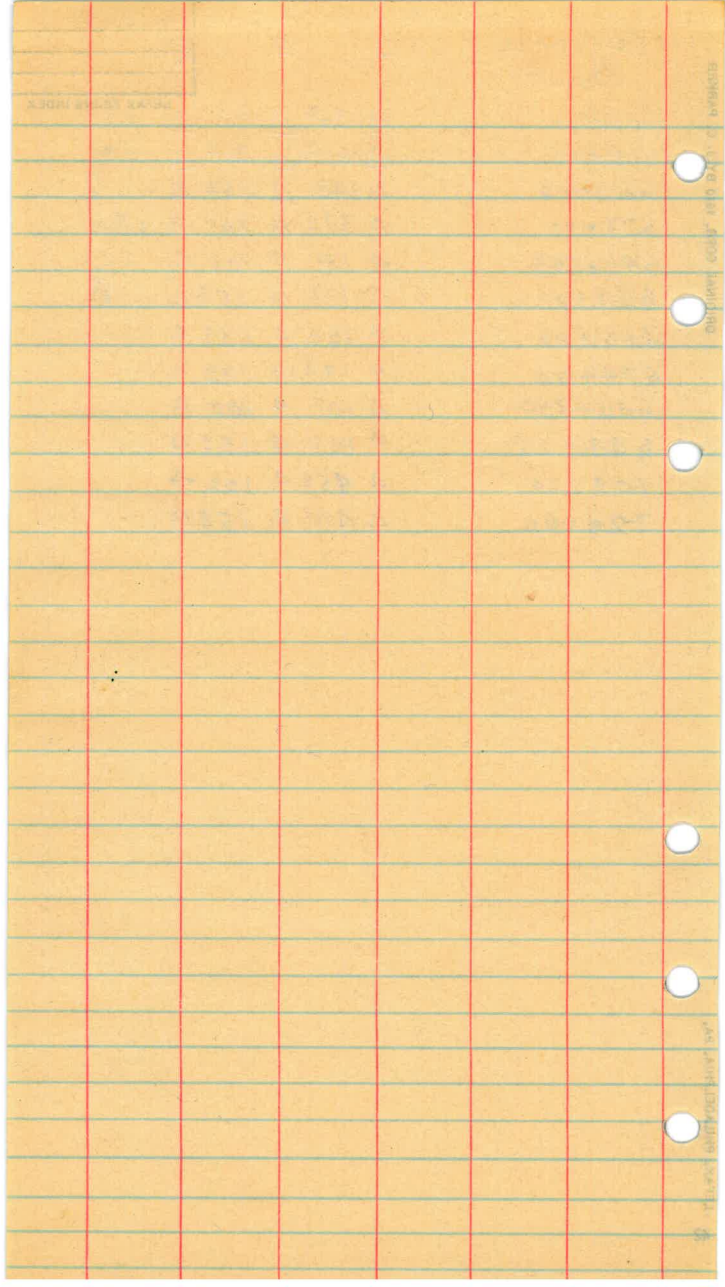
P
1.1

LEFAX FILING INDEX

601+00	Δ 30°	Δ 8°	Δ 5.5
614+00	Δ 41°	Δ 26°	Δ 5.8
623+00	Δ 14°	Δ 26°	Δ
633+00	Δ 37°	Δ 26°	Δ 6.5
645+562	Δ 13°	Δ 10°	Δ
654+00	Δ 13°	Δ 15°	Δ
664+00	Δ 15°	Δ 13°	Δ
674+00	Δ 13°	Δ 13°	Δ
680+95°	Δ 10°	Δ 10°	Δ
684+00	Δ 12°	Δ 15°	Δ
704+00	Δ 45°	Δ 10°	Δ
724+00	Δ 40°	Δ 15°	Δ

Rel. Line

LEFAX, PHILADELPHIA, PA.





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42

LEFAX FILING INDEX

N.89°32'W  
824+95<sup>87</sup> E.C.

P.I.  
824+35° 26'46" R.

E=  
R=286.48  
T=68.16  
D=20  
L=133.83

823+61<sup>84</sup> B.C.

S.63°42'N. 670.15

816+91<sup>81</sup> E.C.

A  
816+20 19°20' L

E=  
T=74.98  
R=286.48  
D=20  
L=146.67

815+45<sup>82</sup> B.C.

N.86°58'W 374.15

811+70<sup>87</sup> E.C.

P.I.  
811+11<sup>85</sup> 51°12' L

E=  
T=68.63  
R=143.24  
D=40  
L=128.00

810+42<sup>87</sup> B.C.

N.35°46'W 718.77

803+24<sup>81</sup> E.C.

P.I.  
802+17<sup>81</sup>

T=118.6



531°26'W5.

840+61<sup>67</sup> E.C.

<sup>A</sup>839+96° 24°R

E=  
T=67.66  
R=318.31  
D=18°  
L=133.33

839+28<sup>34</sup> B.C.

57°26'W

838+96<sup>33</sup> E.C.

E=  
T=68.89  
R=170.99  
D=30°  
L=132.22

<sup>A</sup>838+33° 39°40'L

837+64<sup>14</sup> B.C.

547°06'W

833+96<sup>62</sup> E.C.

E=  
T=67.72  
R=220.37  
D=26°  
L=131.41

<sup>A</sup>833+33° 34°10'L

832+65<sup>29</sup> B.C.

581°16'W

830+10<sup>85</sup> E.C.

E=  
T=71.93  
R=477.47  
D=22°  
L=142.78

<sup>A</sup>829+40° 17°08'R

828+68<sup>07</sup> B.C.

564°08'W

826+19<sup>75</sup> E.C.

<sup>F.T</sup>825+61° 26°20'L

825+00<sup>08</sup> B.C.

N89°32'W

824+93<sup>67</sup> E.C.

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42


LEFAX FILING INDEX

5.43°56'N  
853+93<sup>37</sup> E.C.

$\Delta$   
853+52° 16'40" R

E =  
T = 41.96  
R = 286.48  
D = 20°  
L = 83.33

853+10<sup>09</sup> B.C.

5.27°16'W

851+97<sup>92</sup> E.C.

$\Delta$   
851+44° 13'0" R

E =  
T = 54.41  
R = 477.47  
D = 12°  
L = 108.33

850+89<sup>59</sup> B.C.

5.14°16'W

850+20<sup>12</sup> E.C.

$\Delta$   
849+36° 19'50" R

E =  
T = 91.55  
R = 409.26  
D = 14°  
L = 141.67

848+58<sup>45</sup> B.C.

5.5°34'E

845+55<sup>99</sup> E.C.

$\Delta$   
845+00 11'4" L

E =  
T = 56.34  
R = 572.96  
D = 10°  
L = 112.33

844+43<sup>66</sup> B.C.

5.5°40'W

842+47<sup>82</sup> E.C.

$\Delta$   
841+84° 25'46" L

E =  
T = 65.52  
R = 286.48  
D = 20°  
L = 128.33

841+18<sup>00</sup> B.C.

5.31°26'W

840+6<sup>67</sup> E.C.

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42


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870+4021°30'L

869+98.16 BC.  
561°42'W

868+35.64 EC.

△  
867+4710°40'L

866+57.86 BC  
572°22'W

866+48.92 EC.

△  
865+95 13°00'R.

865+40.59 B.C.  
559°22'W

△  
864+00 0°26'R  
558°56'W

859+77.54 E.C.

△  
859+09 11°0'R

858+40.04 BC  
547°56'W  
EC.

△  
856+50° 4°0'R

BC.  
853+93<sup>37</sup> E.C. 5.43°56'W

E=  
T=89.14  
R=954.93  
D=6°00'  
L=177.78

E=  
T=54.41  
R=477.47  
D=12°0'  
L=108.33

E=  
T=68.96  
R=716.20  
D=8°00'  
L=137.6

E=  
T=  
R=  
D=  
L=



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LEFAX FILING INDEX

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$S7^{\circ}42'E$   
878+57.3 EC.

$\Delta$   
877+97  $24^{\circ}30'L$

877+34.8 BC  
 $S16^{\circ}48'W$

875+70.58 EC.

$\Delta$   
875+00  $17^{\circ}09'L$

874+28.36 BC.  
 $S33^{\circ}52'W$

873+19.08 EC.

$\Delta$   
872+40  $6^{\circ}20'L$

871+66.75 BC  
 $S40^{\circ}12'W$

870+80.85

$\Delta$   
870+40  $21^{\circ}30'L$

869+98.16 BC.

E=  
T=62.20  
R=286.48  
D=20°  
L=122.50

E=  
T=71.64  
R=477.47  
D=12°  
L=142.22

E=  
T=79.25  
R=1432.4  
D=4°  
L=158.33

E=  
T=41.84  
R=220.37  
D=26°  
L=82.69

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LEFAX FILING INDEX

Sta

674+00

684+00.3 D°57'R

Δ 680+95 1°22'L

588.46W

89.52  
122  
91.19  
89.60  
1.14  
88.46

Δ 674+00 0°25'R

589.52'W

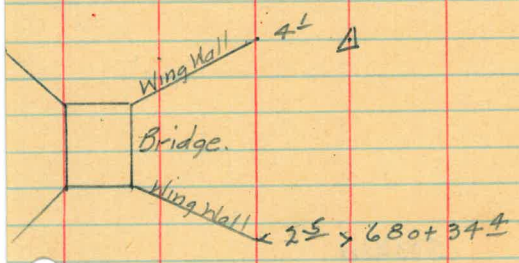
589.43W



684+00  
680+95  
3 05 3

= 684+00

681+29 < 4<sup>±</sup> ⊗ Tel. Pole.



679+86 < 4<sup>±</sup> ⊗ Tel. Pole.

= 674+00 P.O.T.

N.86°0'W

732+13<sup>Z</sup> E.C.

731+26<sup>S</sup> P.I. 10°12'R

729+98<sup>Z</sup> B.C.

5.83°48'N

728+00 P.I. 1°15'L

5.85°03'N


724+00 P.I. 1°15'R

5.83°48'N

717+98<sup>Z</sup> B.C.

83	48
1	15
<hr/>	
85	03
83°48'	
10°12'	
<hr/>	
92°00'	

△

3°  Old Hub 731+73

18" Corr. Iron Culvert  9.0 . 730+07.

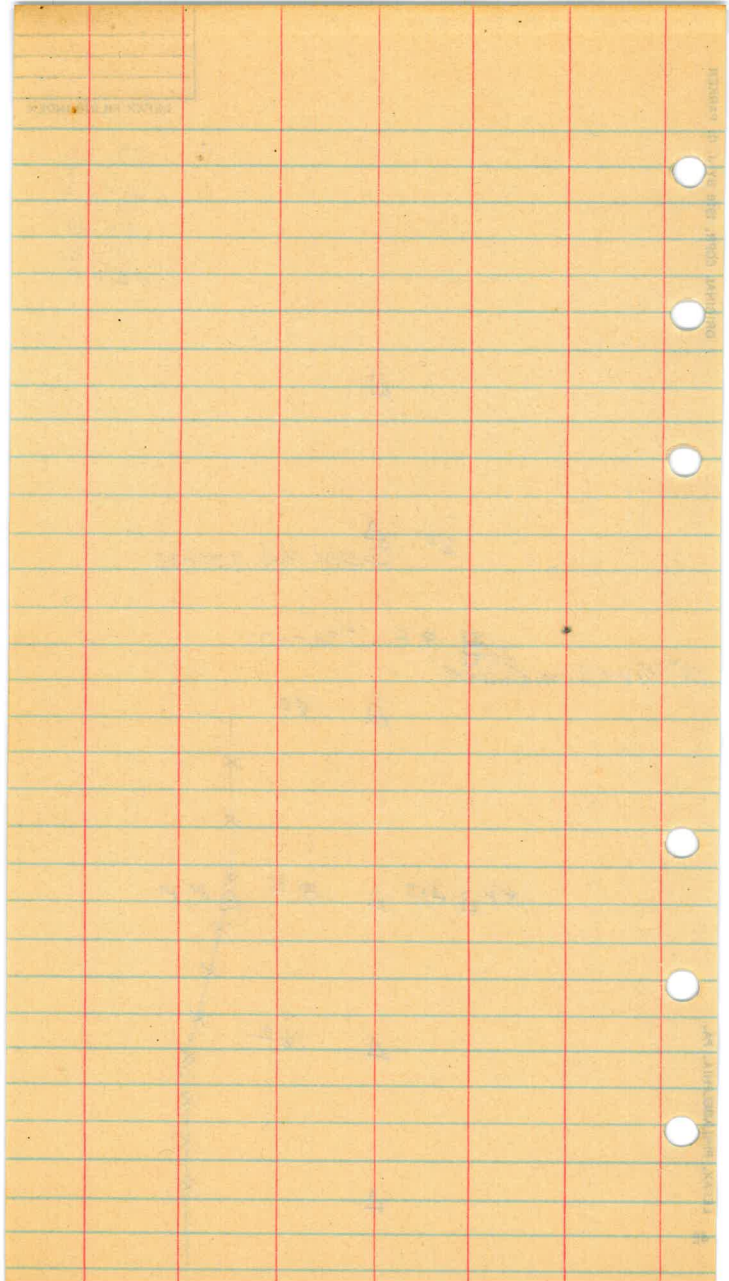
△ 8°

RR  41°  8.2  R.P.

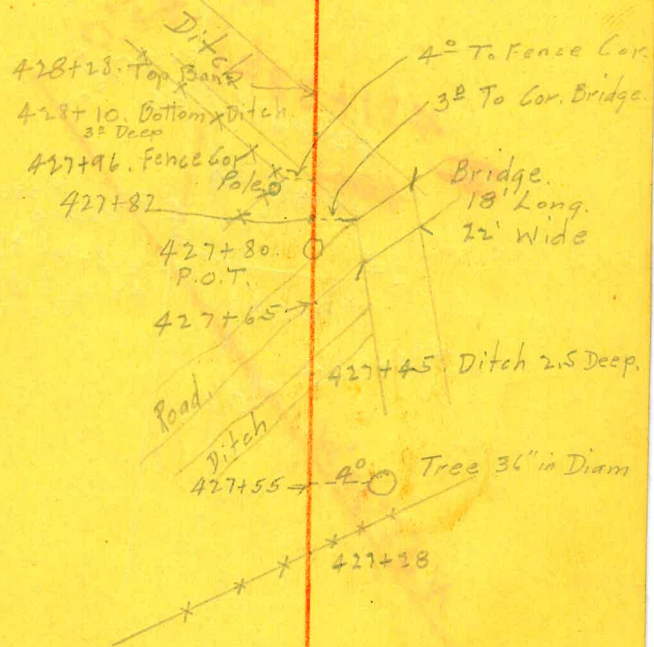
△ 16°

△



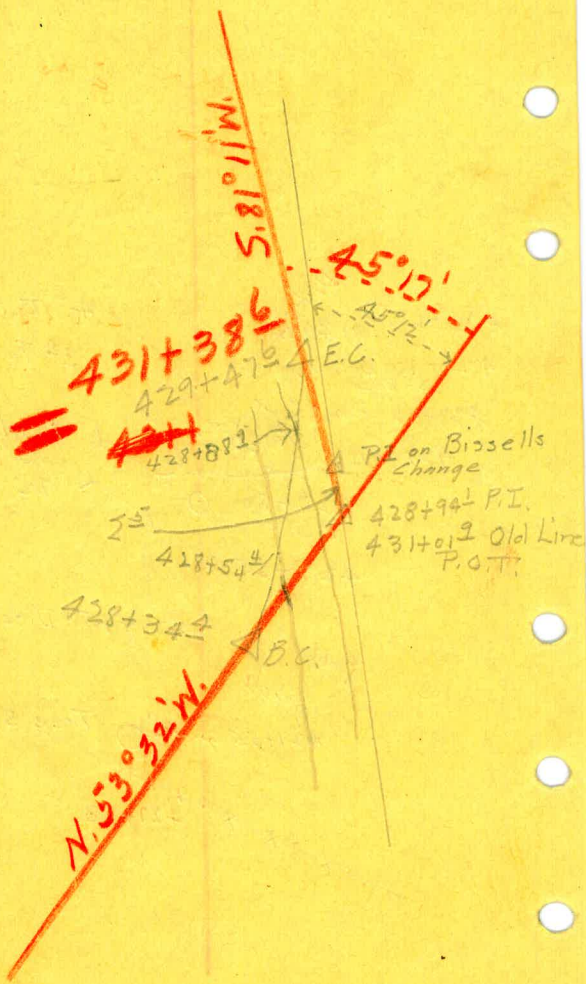






432+00  
98.1  
431+01.9

432+00



E.C. 589+78  
E.C. 589+79.2

589+27.4  
P.I.  
589+24.1

New Location

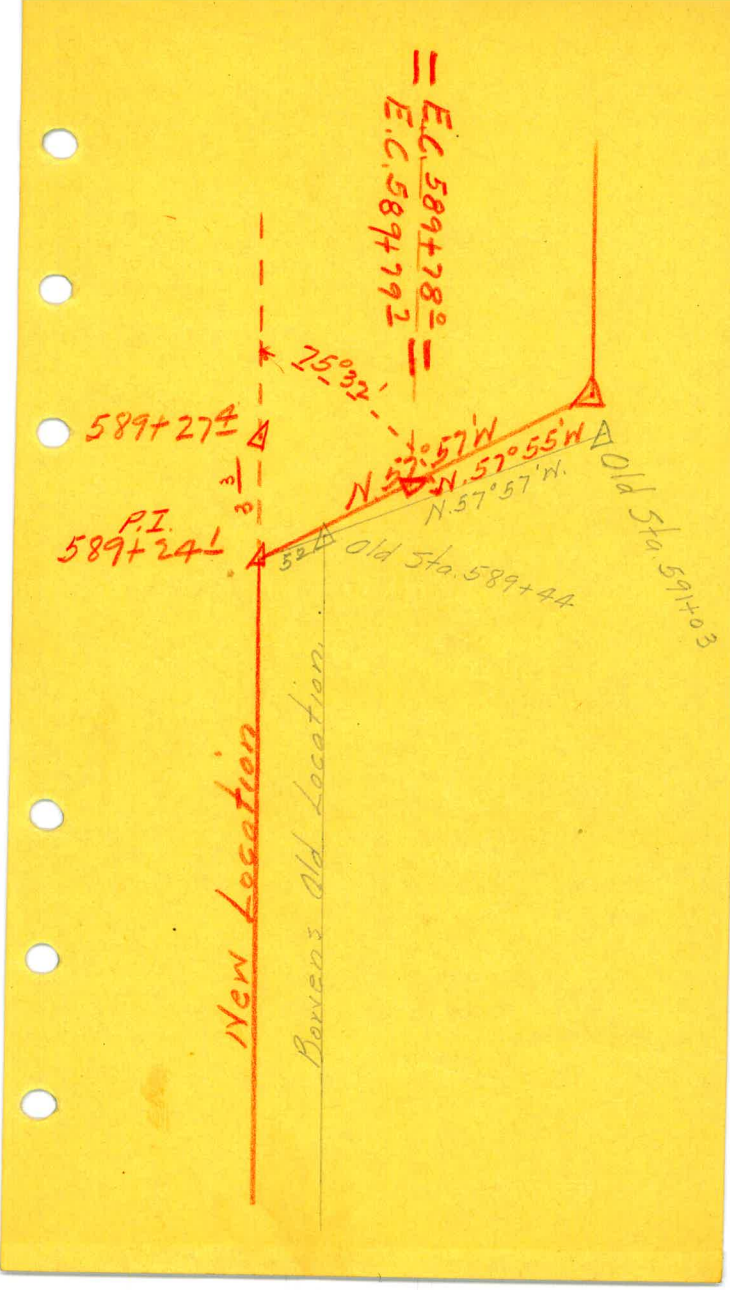
Boyers Old Location

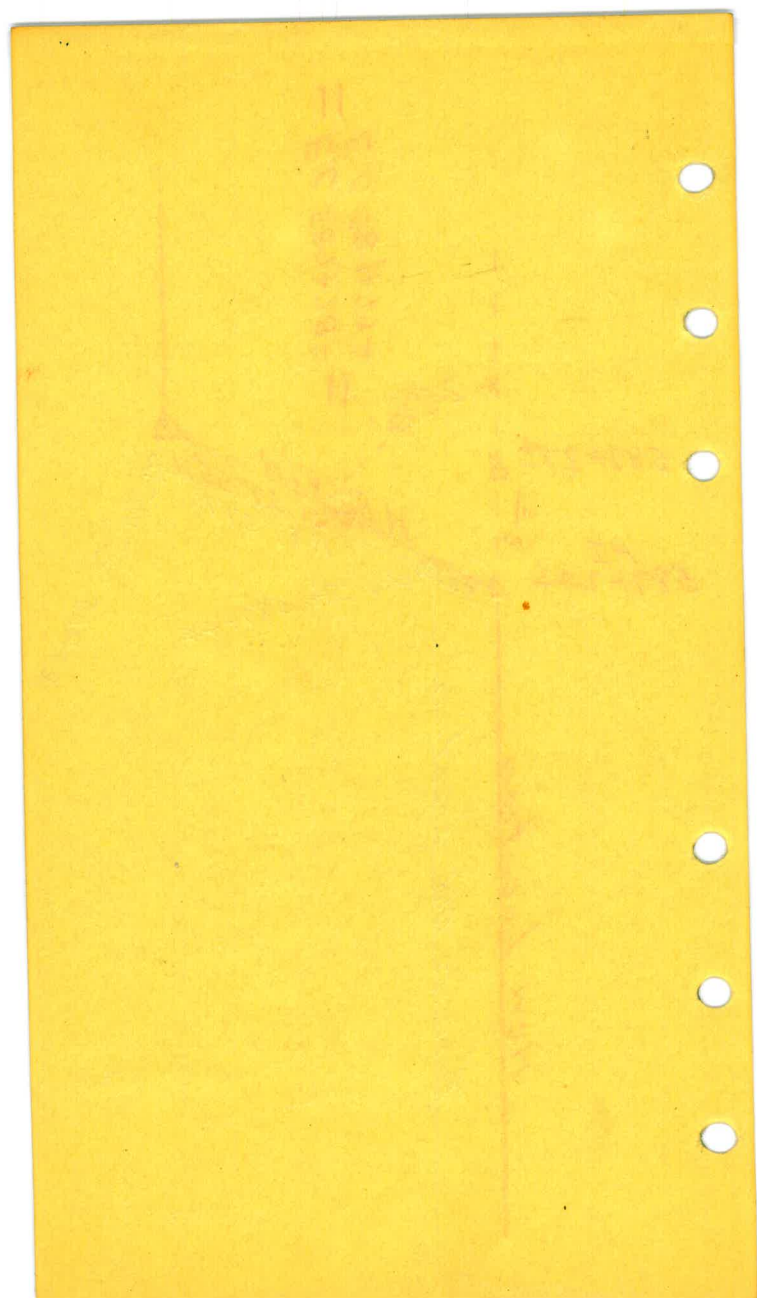
25°32'

N. 57°57' W.  
N. 57°55' W.  
N. 57°57' W.

Old Sta. 589+44

Old Sta. 591+03







	Bear Dist	Co	Sin	N	S	E	W
Sta. B							
A	N48°09'E	2107.5	667	745			
312+65	N74°08'E	197	273	962	1402.84	1569.91	
313+32	N89°08'W	72.0	015	1.000	53.78	189.51	72.0
335+10	S48°14'W				1.08		
B.	S78°37'W	68.0	197	980	1448.42		1622.40
A.	N48°09'E	2103.0	667	745	1966		51.33
					1402.70	1566.73	
					1457.56	1468.08	1756.14
							1745.73

1

Sta.	Bear	Dist	Cos	Sin	N.	E.	S.	W.
D		<u>N 26° 27' E</u>	<u>1945</u>	<u>445</u>				
C		N 23° 15' E	617	394	567.02	243.10		
B		N 78° 37' E	68.0		13.40	66.64		
335710		S 35° 31' W			966.94		462.03	
345+82		S 26° 01' W			1357.50		661.38	
360+92		S 89° 45' W	58	1.000				
D					580.44	0.123	580	
					2324.67	309.74	1181.41	
					580.44		307.70	
					1744.25	871.67	871.67	
C		N 26° 27' E	1953.4					

(2)

Sta.	Bear	Dist	Cos	Sin	N	S	E	W.
A15+42	$180^{\circ}33'E$ $180^{\circ}40'E$	2221 <u>2213</u>	<u>162</u>	<u>787</u>				
E	$N. 81^{\circ}08'E$	3175	154	988	488.95		3136.90	
D	$N. 87^{\circ}25'E$	58	.006	1000			58.0	
360+92	$S. 80^{\circ}40'W$				123			
372+00	$S. 82^{\circ}21'W$					179.50		1093.60
378+00	$S. 80^{\circ}59'W$					79.80		594.60
402+00						376.80		2371.20
A15+42						217.40		1324.55

(13)



Sta	Bear	Dist	Cos	Sin	N	S	E	W.
402+00								
	580°40'N					217.40		1324.55
415+42	180°30'E	2221.	.164	986	364.22		2189.05	
E								
					489.18	853.50	3174.90	5383.95
					489.18			3194.70
					364.32			2189.05

(3)

WESTBURY LITHO CO. NEW YORK, N.Y.



415742

N8090E 2213

E

N8088E 3175

988

D

N2222E 1945

445

C

N2303E 617

394

B

<sup>04809</sup>  
N4770E 2103

745

A

N7408E 86.0

962

313784

54814W 2126.

746

335+10

Cos

Sin

N

S

E

W.

313690

865.52

243.10

1566.74

1556.22

82.73

1415.92

1586.00

4

	N.	S	E	W
335+10				
345+82		✓ 966.94		✓ 462.03
360+92		✓ 1357.50		✓ 661.38
372+00		✓ 179.50		✓ 1093.60
378+00		✓ 79.80		✓ 594.60
402+00		✓ 376.80		✓ 2371.20
415+42	✓ 4233.45	✓ 217.40	✓ 588.47	✓ 1322.55
E	4227.93	4593.86	8093.26	8093.26
	370.93	4022.93	70.52	5894.99
		370.93	88.94.97	2198.57
	370.93		2198.57	

FRANK LINTAS MARK

CHERRYHOF ROAD, AND 801 S. T. AVENUE

FRANK LINTAS MARK

Sta. Bear Dist Cos. Sin N. E. W

415747

~~N 80° 44' E~~ 2123 (161) 187

E

N 81° 2' E 3176.0 153 988

3137.89

D

N 26° 2' E 1951.0 896 444

866.24

C

N 24° 2' E 615.0 914 407

2501.30

B

N 48° 2' E 2109.0 665 747

1575.42

A

N 74° 00' E 197.0 273 962

189.51

312763

Map Location  
2123 (161)  
LEFAX FILING INDEX



Sta.	Bear	Dist	Cos.	Sin	N.	S.	E.	W
312+63 <sup>2</sup>								72.00
313+35 <sup>2</sup>	N 89° 08' W	72.10	0.15	1.00	1.08			
335+10	548° 14' W					1498.42		1622.40
345+82						966.94		462.03
360+92						1357.50		661.38
372+00						179.50		1093.60
378+00						79.80		574.60



73

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37840

402 to

415+42

18078E 2213.0

E

W

F

S.

N.

2371.20

376.80

1324.53

217.40

2181.40

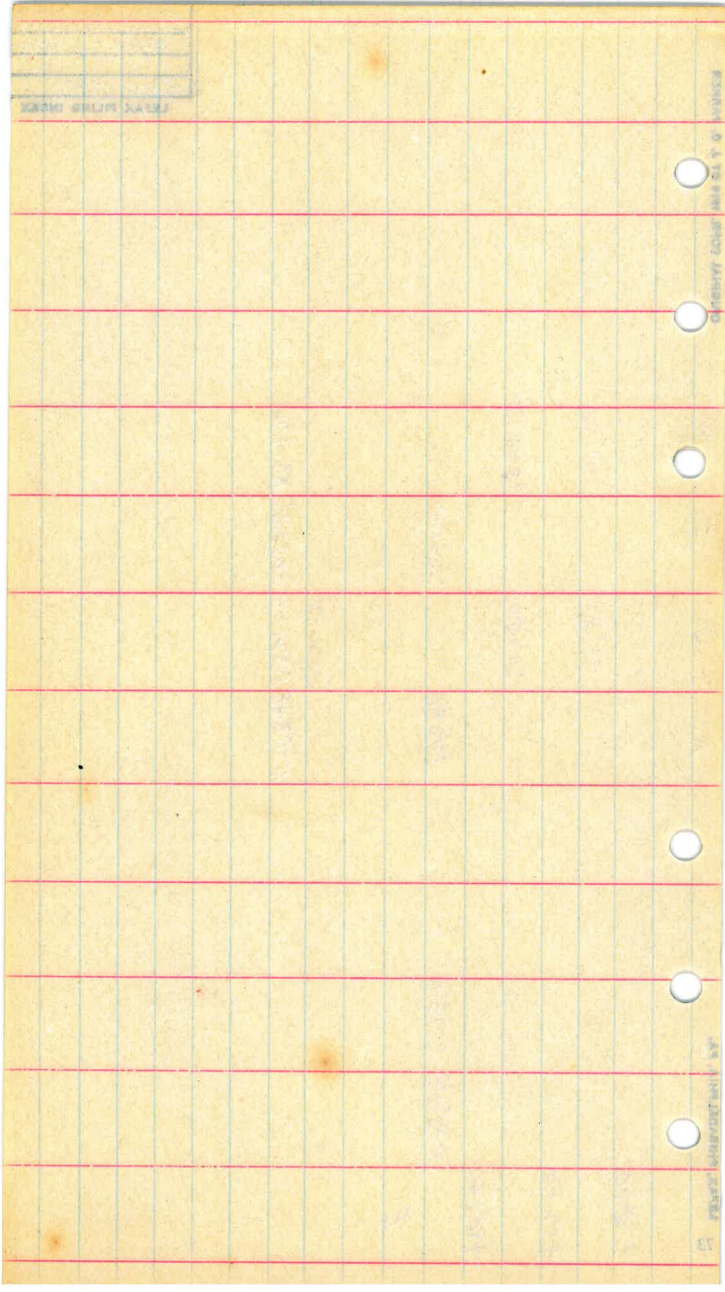
372.88

4026.36

425348 5132.64 6020.36 8201.76

11600.600 Lines
1242/10000
842 (13)

LEFAX FILING INDEX



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LEFAX FILING INDEX

LEFAX, PHILADELPHIA, PA.

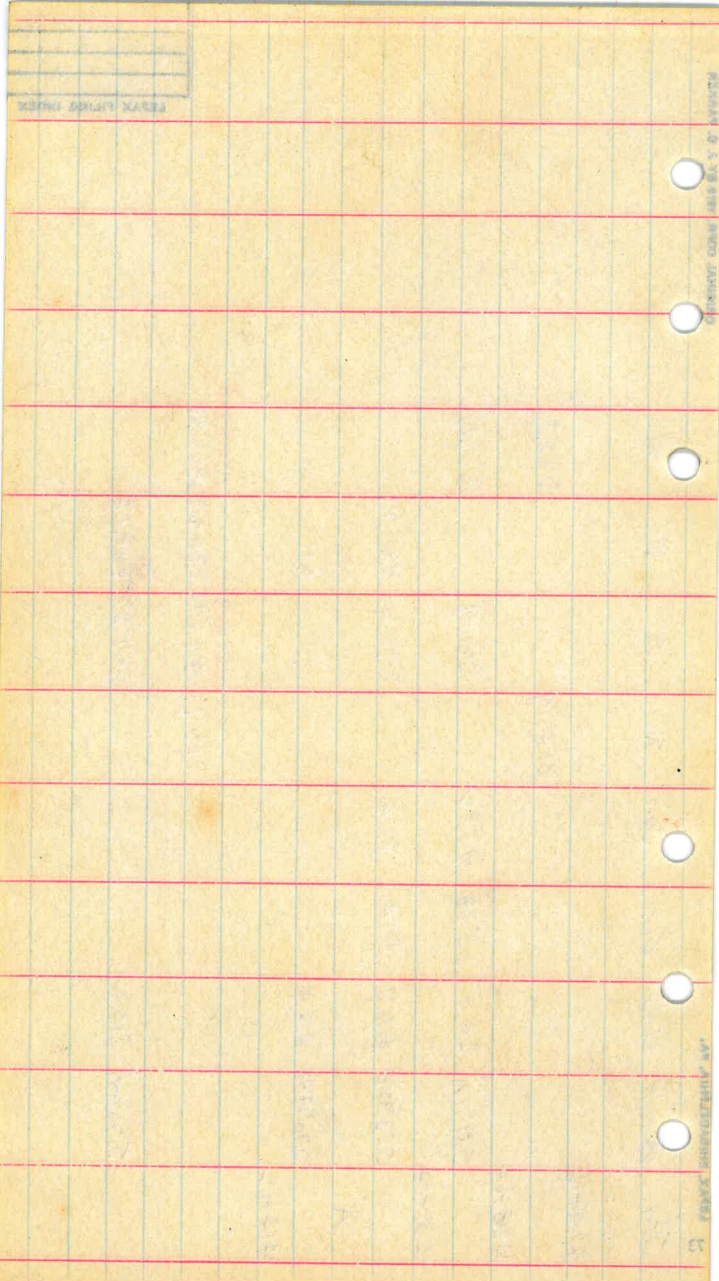
73



Sta.	Bear. Dist.	Cos.	Sin.	N.	S.	E	W
414+62	580' 8" J. Barton 80	168 .162	986 987		13.44 12.96		7888 78.96
415+42				175.51			30.26 ✓
417+20				101.36			96.60 ✓
418+60				34.41			86.40 ✓
419+53				27.35			280.59 ✓
422+35				70.95			166.52 ✓
424+16							



Sta.	Bear	Dist	Com	Dir	N.	S	E	W
424+16					304.19			328.83 ✓
428+64						36.79 ✓		237.17 ✓
431+04	581°11'W	240	1538	9882 ✓		396.20 ✓	536.27 ✓	
"A"	553°32'E	667	594	804 ✓		267.83	765.88	
414+62	570°05'E	811	330	744 ✓				
	570°48'E	814.4						
					713.77	446.43 ✓		1305.25 ✓
						445.95	536.17	1905.33 ✓
	570°48'	814.4				267.82	769.06	



KONTO DEBITO KASBA

KONTO KREDITO KASBA

KONTO KREDITO KASBA

Sta.	Bear	Dist	Cos.	Sid	N	S	E	W
51425	N.3977E	323	774	633				
D	N.4236E	428	736	677	315.01		189.76	
C	N.5610E	363	557	831	202.19		301.65	
B.	N.7033E	309	333	943	102.90		291.39	
A	N.7926E	622	185	983	115.07		611.43	
494700								
495758						37.45		153.42
502495						179.95		715.38







Sta.	Bear.	Dist.	Cos	Sin	N.	S.	E.	W.
"A"								
4294324	N.53°32'W	495.4	.594	.804	294.27			398.30
B	S.9°E	694.36	.988	.156		686.03	108.32	
C	N.81°06'E	980.3	.155	.988	151.95		968.54	
D	N.85°6'W	2.6	.988	.155	(2.57)			(.90)
"A"	N.70°45'W	718.4	.330	.944	(23707)			(678.17)
					446.22	686.03	1076.86	398.30
						446.22	398.30	
						239.81	678.56	

Property Tie. S.E. Cor.  
Block 25. Lot 5 side

Sta.	Bear.	Dist	Cos	Sin	N	S	E	W
442+0								
455+37	58°01'N	1337	110	985		277.29	134.74	
467+00	58°58'N	1163	157	988		182.59	1149.04	
442+0	N 80°34'E	2498.3	164	986		409.88	2465.98	





Sta.	Bear	Dist	Cos	Sin	N	S	E	W
C.								
D.	5.90°E	61.84	988	156		61.09	9.65	
43/104	N53.32°W	171.65	594	804	10196			138.01

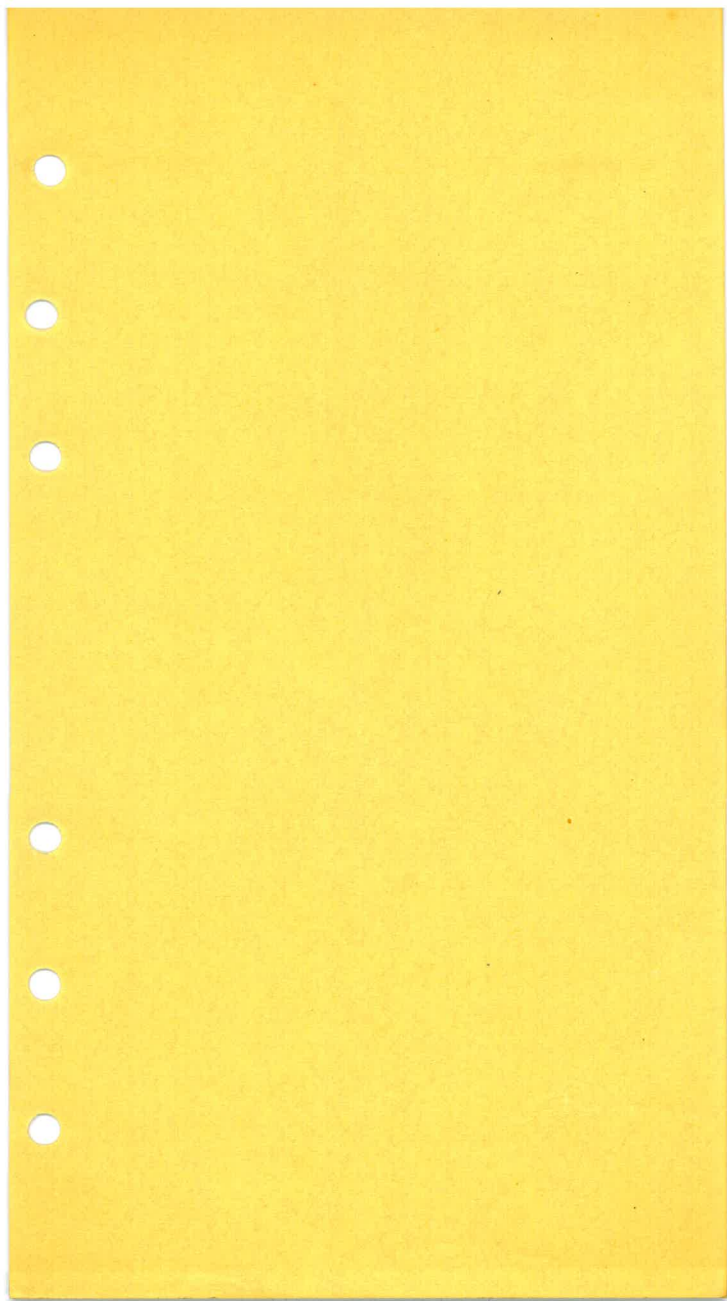
Property Line T.E. N.W.  
Cor. E.K. 5. Lakeside

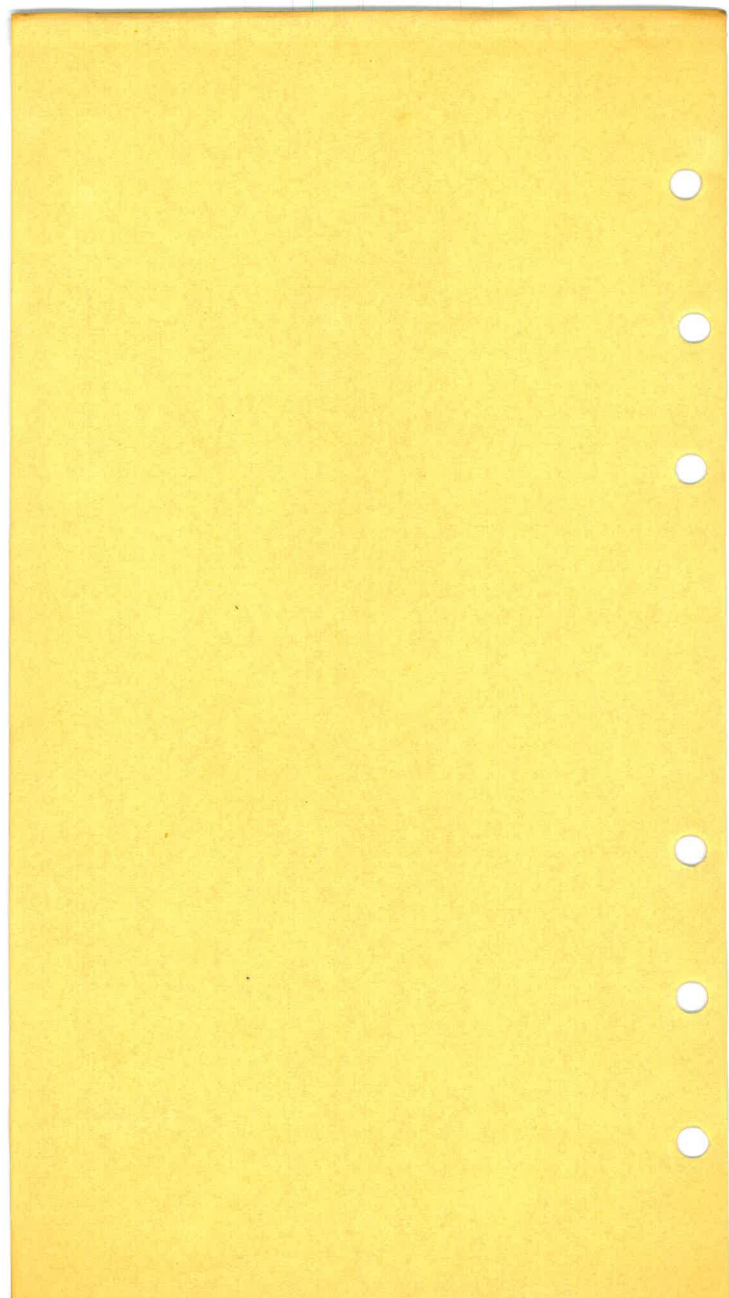
TRIPLE LINE INDEX

PROPERTY CORNER NUMBER 50

PROPERTY CORNER NUMBER 50









A B

C D E

424352

	N	S	E	W
	234.06	2539	182.16	1009.04
279205		34.78	184.80	
50705E		64.96	153.81	
N8733E			116.88	
57709E	5.03	57.99	254.67	
516433E				
239.09	183.12	892.32	1009.04	



	60+15	65+50	66+83	67+80	69+00	71+06	A	B
Code	N 5428x	N 7340x	N 7820x	57954x	57925x	N 6220E	58750E	
Col	581	281	202	175	285	464	035	
Dir	814	960	979	985	958	886	999	
N	✓ 310.86	✓ 37.37	✓ 19.59			367.80	82.59	
S				21.00		58.71	12.60	
E	4.35.49 ✓	122.68 ✓	94.26 ✓	118.08 ✓		197.35 ✓	157.71 ✓	✓ 17.35
W						973.56 ✓	359.64 ✓	
								✓ 17.35

488.09

	N	S	E	N
B.	32.59	1260	571.25	2
C.	500.70	313.30	413.72	931.07
60+15	130.71	57.38	42.49	
	450.39	393.01	931.07	973.56
	393.01			931.07
	57.38			42.49

ЧЕРНЫЙ ПИЛИТ КАРД

С ПЕРВОГО ГОДА ИСПОЛНЕНИЯ

С ПЕРВОГО ГОДА ИСПОЛНЕНИЯ

	B	D	Co	Sub	N	S	E	W
31406								
A				82.59	157.71			
B					12.60	357.64		
C					300.70	413.72		
60+15	53635E	715	803	596				
E'	N3631W	71.4	804	595	57.41	57.41	42.61	42.48
B'	N5255W	511.4	589	808	301.21			413.21
A'	N8955W	360.0	036	999	12.96			357.64



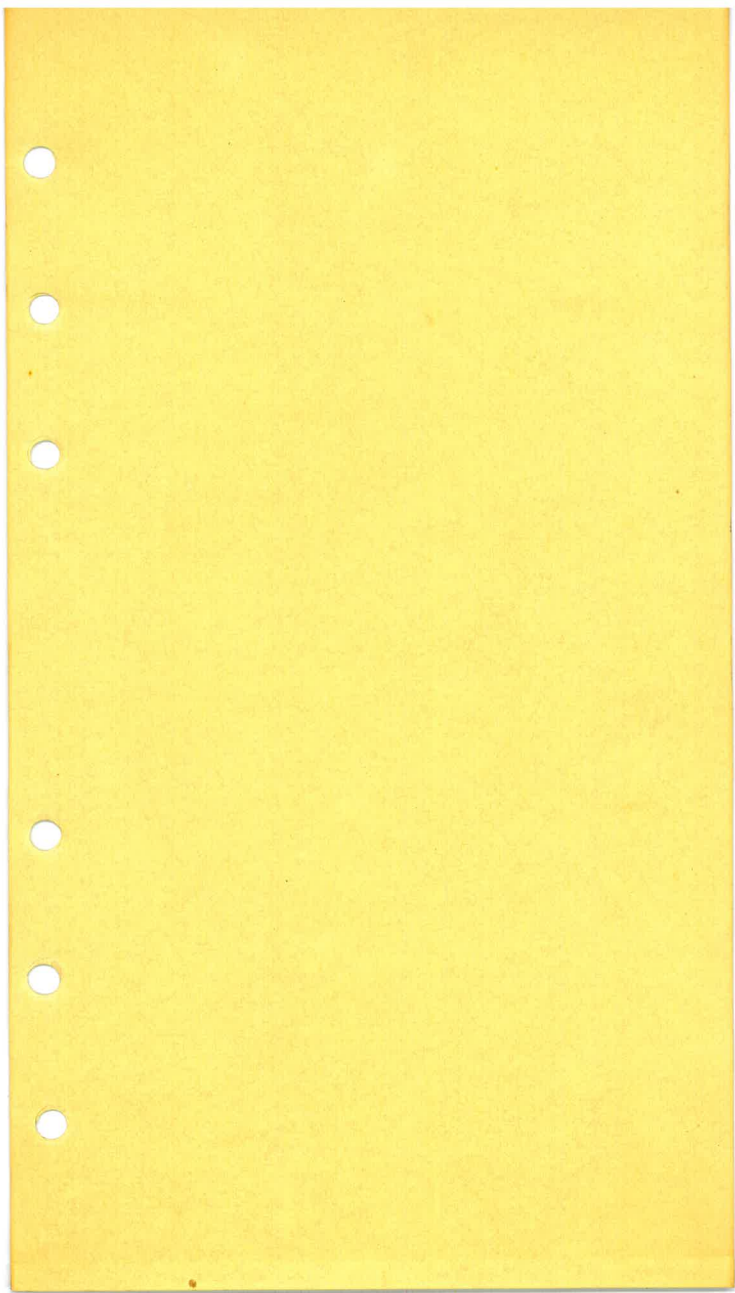
	N.	S.	E.	W.
A'				
71406	5.62%W	178.0	465	885
		82.77	157.53	
	454.17	453.48	973.68	972.86
	3.48		<u>2.86</u>	
	<u>.69</u>		<u>.82</u>	

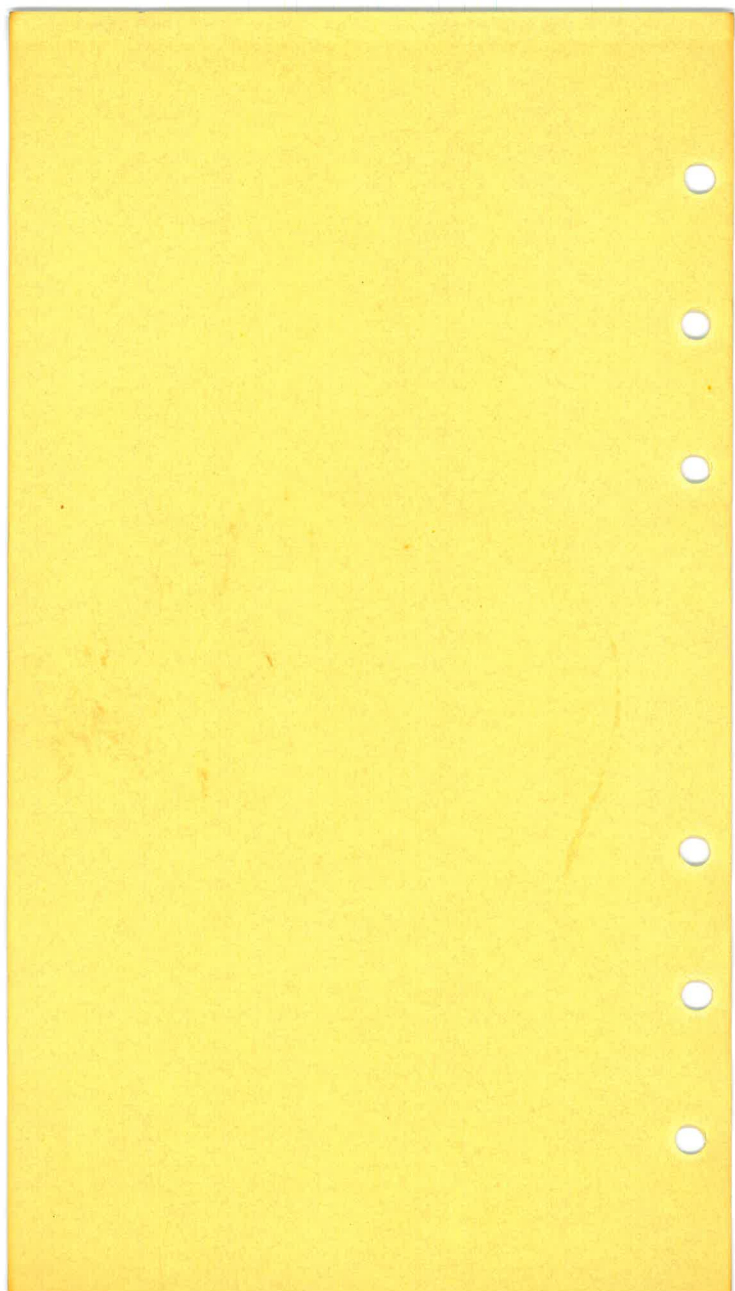
FLY'S LITTLE WORK

CRISWELL TOLSON 5112 BA Y 97 11/10/58

CRISWELL TOLSON 5112 BA Y 97 11/10/58







Jh. Bear Dist Cos Sim N. S. E. W.

33+57

S. 78° 25' E 203

31+54 ±

S. 81° 38' W 31.4

31+23 ±

N. 69° 26' W 132.1

A

32+55

N. 81° 03' W 103.2

33+57 ±





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42

73	22
19.	20
8	2
2	42
87	18


LEFAX FILING INDEX

78	21
21	47
100	08
79	52
167	79
69	00

N. 87° 18' W

71+06  $\frac{1}{2}$  R. 19° 20'

Old Sta. 71+06

205.9

S. 73° 22' W

P.I. 69+00  $\frac{1}{2}$  L. 6° 30'

Old Sta. 69+00

120.4

S. 79° 52' W

P.I. 67+79.8 L. 21° 45'

Old Sta. 67+80

96.5

N. 78° 21' W

P.I. 66+83  $\frac{3}{4}$  L. 4° 1'

Old Sta. 66+83

133.1

N. 73° 40' W

65+50.3 P.I. L. 19° 12'

Old Sta. 65+50

535.3

N. 54° 08' W

P.O.T.

316.2

60+15  $\frac{1}{4}$  L. 10° 20'

N. 44° 08' W

56+02

210+67° E.C.

209+30° 22' 12" R

$$E = 13.7$$

$$T = 140.5$$

$$R = 716.2$$

$$D = 8^{\circ}$$

$$L = 277.5$$

207+89° B.C.

197+78° P.O.T.

5.6385W

191+24° E.C.

190+00°  
190+00° 25' 20" R

$$E = 14.3$$

$$T = 128.8$$

$$R = 572.96$$

$$D = 10^{\circ}$$

$$L = 253.3$$

188+71° B.C.

5.3745W

185+83°

$$\begin{array}{r} 18 \\ 33 \overline{) 610.6} \\ \underline{33} \\ 280 \\ \underline{264} \end{array}$$

1263  
 P.B. ~~1673~~

E.C. 34+52.3  $\Delta$  E.C.  $\equiv$   
 P.O.T.

P.I. 33+57'  $\Delta$

33+80  $\circ$

8'

L. 11°37'

2.96

E = 3.0

D = 10°

R = 572.96

T = 58.3

31+72  $\circ$

P.I. 31+54'  $\Delta$

31+20  $\Delta$

R. 12°12'

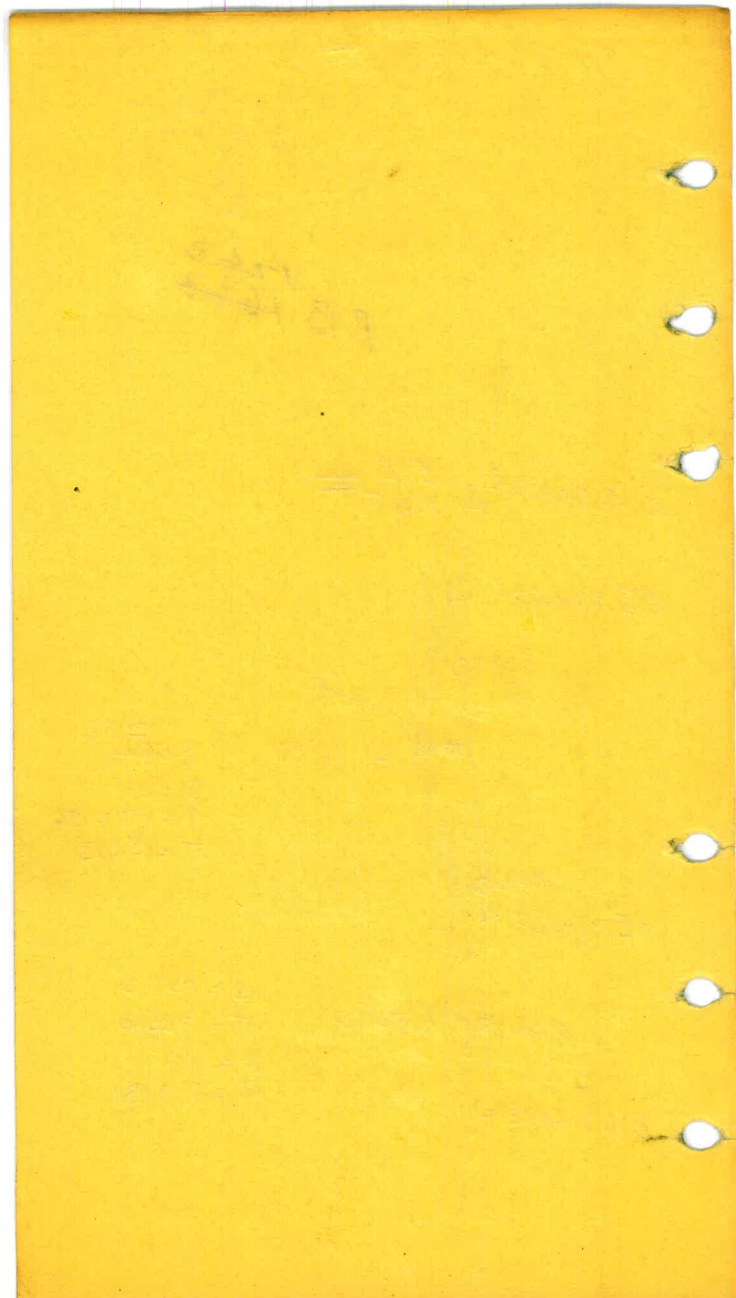
$\Delta = 12°12'$

T = 34.0

D = 18°

R = 318.31

B.C. 30+85.8  $\Delta$





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Sta	B	Dist	Cos	Sin	N	S	E	W	ZEW
0-52.87									
1+77.1									
3+51.3									
6+00.3									
7+99.8					26.81			840.27	
A	N8°20'E	102	.151	.989	15.40		100.88		
B	N86°45'E	559.1	.059	.998	33.47		557.79		
C	S72°25'E	191.	.302	.953		57.68	182.02		
0-52.87	S1°28'W	18'	1.000	.026	75.68	18.00		.47	
					75.68	75.69		840.69	

E/Cap Pipe Line	
Phase/Location	
T.A.M.	①
LEFAX FILING INDEX	

Sta	B	Dist	Cos	Sin	N	S	E	W
11981	N75°29'W				43.90			169.30
13773					4.08			34.36
14076					1.70			40.36
1448	N82°02'E	49.0	.138	.990	6.76		48.51	
A	S73°41'E	203.5	.17731	.96078				
11981						56.46	195.51	
					56.94	56.24	244.02	244.02



PROOF & TRIM MARK

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U.S. GOVERNMENT PRINTING OFFICE

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Sta	B	Dist	Cos	Sin	N	S	E	W
164983						29.48		128.31
18499.9						26.87		121.41
194593						49.92		221.23
21481.2					69.70		208.60	
A	N71°31'E	219.9	31703	94842				
16498.3	N82°03'E	265.0	.138	.990	36.57	106.27	162.35	470.95
					✓	65.80	470.95	
						40.57		

El Cap Pipe Line  
 Paper Location  
 T.A.M. - (E)  
 LEFAX FILING INDEX



Sta	Bear	Dist	cos Sin	N	S	E	W
25+25	S88°31'W	20.0'	.025	.999	0.50	19.98	252.45
25+45	S88°15'W	100.0	.108	.994	10.80	99.40	
28+00	N81°13'E	158.0	.153	.988	24.17	156.10	
29+00	S77°07'E	221.2	.223	.975	49.32	215.73	
A							
25+25				60.63	60.63	371.83	371.83
				11.70			15.810
				49.33			215.73

21 TRUCK MANUFACTURER'S 5.500 19.9%

TRUCK MANUFACTURER'S 5.500 19.9%



73

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ORIGINAL COPY. 1910 BY J. O. PARKER

	Bear	Dist	Gas	Sin	N	S	E	W
Sta								
29+00	588°49'W	100.0	.108	.994		10.80		99.40
30+00					102.60			463.60
34+75					74.81			227.05
37+14					18.23			74.02
38+00					41.99			85.22
38+95	570°27'E	90.0	.335	.942				
A	585°34'E	88	.077	.997		30.15	84.78	
B						6.78	87.74	
					23.763	47.73	172.52	959.29

51 Copy 11/10/1910  
 Paper Location  
 T.A.M. - (3)  
 LEFAX FILING INDEX

Sta	Bear	Dist	Gas	Sin	N	S	E	W
B	563°36'E	134	,445	.896	237.63	47.73	172.52	959.29
C	581°03'E	277	,156	.988		59.63	120.06	
D	578°28'E	203	,285	.958		43.21	273.68	
E	581°38'E	200.7	,145	.989		57.86	194.47	
29700						29.20	198.56	
					237.63	237.63	959.29	959.29
					208.48		760.73	
					29.20		198.56	

9.002

3 LEFAX, PHILADELPHIA, PA.

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	Bear	Diet	Gas	Sim	N	S	E	W
Sta 42471					22.51 22.84			80.89 80.98
43+55					52.18 51.71			228.15
45+89					41.24 40.63			298.29
48+90					27.90 27.27			152.52
50+45					74.98 74.75			517.38 215.28
52+75								
A	58203'E	184	.138	.990		25.39	182.16	
B	57920'E	188	.185	.983		34.78	184.80	
			218.8	218.8	216.72	60.17	366.96	975.22 977.20 ✓

21 Cap 11 P 2 L 10 S  
 22 per Location  
 TAM  
 LEFAX FILING INDEX



Sta	Bear	Dist	Gas	Sin	N	S	E	W
B	56705E	167	.589	.921	21.55 216.72	60.17	366.96	977.20 975.22
C	N87033E	117	.043	.999		64.96	153.81	
D	S77°09'E	261.2	.222	.975	5.03		116.88	
E	S77°30'E	259.1	.216	.976		58.10 56.01	254.76 252.78	
A2471	564023E	94	.432	.902		40.61	84.79	
			223.84 165.74 58.10	✓	221.75 165.74 56.01	221.75 220.87	975.22 976.20	975.22 972.44 252.78
					223.84	165.74	722.44	977.20
					223.84	165.74	722.44	977.20



A. 38495

PROPERTY COUNTY, MISSISSIPPI



73

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Sta	Bear	Dist	Co's	Sin	N	S	E	W
60+15		535.0			310.84			435.49
65+50					37.37			127.68
66+83					19.59			94.96
67+80						21.00		<del>118.08</del> <del>118.75</del>
69+00								
71+06	N62°30'E	178.0	464	88.6	182.59	58.71	157.71	197.35
A	S87°59'E	360.0	935	999				
B					450.39	92.31	359.64	973.76
							517.35	945.60

F1 Cap Type Linc  
 Relocations  
 T.A. Mill (E)  
 LEFAX FILING INDEX

Site	Bear	Dist	Cos	Sin	N	S	E	W
B	S62°54'E	511.4	.538	.809	450.39	92.31	517.35	973.56 <del>973.66</del>
C	S36°35'E	71.5	.803	.596	300.70 300.67	413.60 413.79		
6015					57.41	42.61		
					450.39	450.39	973.66	973.66
					149.72		559.96	559.96
					200.67		413.70	413.70
								973.56
								559.96
								413.60

511.4  
516.5

73

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Sta  
74+78  
77+78  
A  
74+78

Bear  
Dist  
Cas  
Sin  
N89°30'E 240.5  
S82°35'E 60.0

5.70  
2.10  
992  
992

M  
S

E  
W

300.00  
240.42  
7.80  
7.80  
5.70  
2.10  
59.58  
300.00  
59.58  
240.42

LEFAX FILING INDEX  
7.A. Milk (6)



S fa	Bear Dist	Gas	Sin	N	S	E	W
79+80				71.81			294.21
82+83				80.41			<del>165.42</del> <del>165.41</del>
84+67				44.53			52.75
85+68							
A	S62°15'E	216.0	.885		100.66	191.16	
79+80	S73°24'E	336.2	.957		96.09	322.21	
				196.75	196.75	513.37	513.37
				100.66			191.16
				96.09			322.21





Sta Beet Dist Cas Sin N S E W

857368

92700

92738

A

857368

NA6 1514 38.0 .685

SIN 15'E 309.0 .400 .916

S02 15E 390.9 .45787 .88802

276.56

.728 26.03

.916

.88802

602.85

27.66

123.60 283.04

178.99 347.47

302.59 123.60 283.04 630.51

123.60 302.59 630.51 283.04

178.99 347.47

71 Cap Noe Use  
Page 10/10/10  
7/10/10 (9)  
LEFAX FILING INDEX

*M. J. P. M. J. P.*  
*Water Metering*

Sta.	Bear.	Dist.	Cos.	Sin.	N	S	E	W
94400					162.45			234.27
96785					39.73			53.94
99752					67.89			169.82
99735						25.21	134.67	
		579245	1370	.184	.983			
H								
		554415	313.3	.5781	.8197			
B								
		546456	93.0	.685	.728			
94700						63.71	627.70	
					27007	8892	201.37	458.03
					8892	170.07	458.03	202.37
					181.15			255.66

Sta. Beach Dist. Cas. Sin. N. S. E. W.

102+30

✓ 192+11 ✓ 120.0 ✓ .184 ✓ .983

✓ 22.08

✓ 117.96

103+50

104+69

✓ 29.27

✓ 115.31

105+16

✓ 58131E 313.6 ✓ .14752 ✓ .98906

✓ 5.08

✓ 76.85

102+30

46.27 310.12

✓ 310.12

✓ 51.35

✓ 5.08

✓ 51.35

✓ 46.27

✓ 5.08

✓ 310.12

Flap Pipeline  
Paper Location  
A. Cleach (B)  
LEFAX FILING INDEX



Sta	Bear	Dist	Cos	Sin	N	S	E	W
152+00	5309M	100.0	.601	.799		60.10		79.90
153+00	53913M	300	.775	.632		232.50		189.60
156+00	14089F	397.8	.73551	.67752	292.60	292.60	269.50	269.50





Sta. Bear Dist. Cas. Sin N S E W

141100

224.05 147.13

145732

143.34

78.54

150785

321.29

450.14

141500 1129°31'E 787.8 .87420 .48557

688.68

382.55

688.68 147.13 529.68

147.13

382.55

LEFAX FILING INDEX  
C/ Lab Philadelphia  
Paper Location  
HC 1000 (9)

Sta.	Bear.	Dist.	Cos.	Sin.	N.	S.	E.	W.
186+00								
189+00	S36°19'W	300.0	.806	.592		24.18		177.69
206+34						1287.59		1006.54
186+00	N37°45'E	1934.2	.79069	.61222	1529.37	1529.37	1184.14	1184.14



Sta.	Beer	Dist	Gas	Sin	N	S	E	W	N	S	E	W
126731									116.47	572.16	111.24	561.37
129700						191.80		188.57		453.69		450.13
132700						219.00		204.90				
134700						137.80		144.80				
134733						23.56		23.10				
A												
B												
126731												

Continued

LEFAX FILING INDEX  
 2. Check (16)  
 Oper Locales  
 4. 106/106/line



Sta.	Bear. Dist	Cos.	Sin	N.	S.	E.	W.
229442				12.62			82.0
230425					38.43		206.43
232435					23.44		76.48
233415	5.4879W	8.0	.665	.747	5.32		6.0
233423	N78°26'E 351.7	2005	.97969				
A	5.5996E 31.0	.511	.860	70.41	15.84	26.67	
229442					83.03	26.67	37.81
				12.62	70.41		347.14

Sta	Bear	Dist	Cos	Sim	N	S	E	W
222182								
225167								
A								
222182								

165-44E	32.7	.443	.897	28.73	14.48	29.31	79.98
54992E	66.68	.69901	.76078	43.21	43.21	50.65	79.96
							79.98

LEFAX FILING INDEX  
 4 (Leak) (1)  
 Paper location  
 1/605 line line

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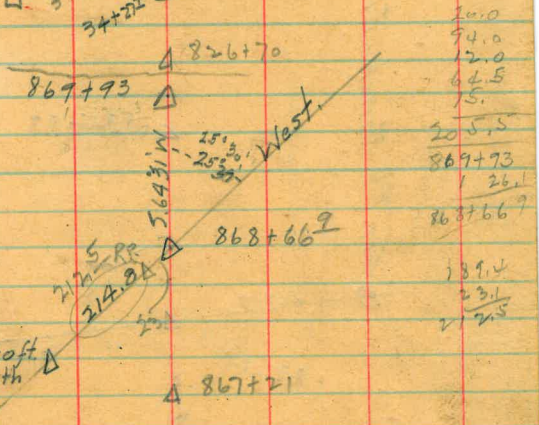
42

1640  
 155  
 1.603  
 96.0  
 45  
 148.8  
 20.0  
 20.6  
 139.4

90 98.8  
 62 173  
 28 116.1  
 751


LEFAX FILING INDEX

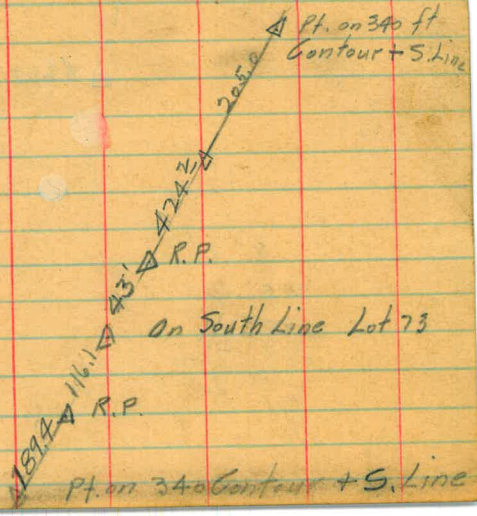
Cor # 8, Rancho El Cajon  
 N. 8° 02' W



99.2  
 100.0  
 100.0  
 60.0  
 60.0  
 5.0  
 427.2  
 20.0  
 94.0  
 12.0  
 64.5  
 15.  
 205.5  
 867+93  
 1 26.1  
 868+66.2  
 139.4  
 23.1  
 212.5

Pt. on 34.0 ft  
 Contour + South  
 Line Lot 473

"G"  
 62.0  
 "F"



on South Line Lot 73

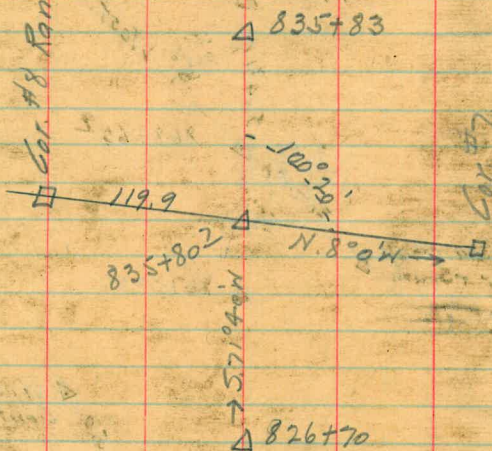
Pt. on 340 Contour + S. Line



$$\begin{array}{r} 32+273 \\ 33+076 \\ \hline 1+19.9 \end{array}$$

$$\begin{array}{r} 835783 \\ 23 \\ \hline 835807 \end{array}$$

Car. #8 Rancho El Cajon



$$\begin{array}{r} 80 \\ 100.20 \\ +80 \\ \hline 108.20 \\ \hline 71.40 \end{array}$$



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BX 85

Sta	+ <u>337.602</u> -	Elev
+63	3.6	334.0
802+00	3.1	334.5
802+258 <small>Back</small>	2.7	334.9
= 802+2053		
B.M. # 89.	5.523	332.079 ✓

Rec. Elev. 332.103

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Sta - 344.907 - Elev

+10 4.4 338.5

795+00 6.1 338.8

796+00 5.0 339.9

+15 4.7 340.2

+32 6.6 338.3

797+00 9.3 335.6

798+00 11.6 333.3

T.P. 333.082  
4.520 337.602 11.820 337.058

+22 5.5 332.1

799+00 6.5 331.1

800+00 9.6 328.0

+25 10.1 327.5

801 3.2 334.4

+20 2.3 335.3



Sta.	Elev.	Grade	Cut	End Area	Ax. End Area	Hor. Dist.	Slope %	Excess Length	True Length	Vol. Co. Ft.	Vol. Co. Yds.
986+50	332.0	328.67	3.3	15.9.	18.2.	25.0.	1%	0.0.	25.0.	4550	✓
986+75	332.4	328.33	4.1	20.6.	23.4.	25.0.	1%	0.0.	25.0.	5850	✓
987+00	333.0	328.00	5.0	26.2.	36.3.	25.0.	14%	0.24.	25.24.	916.2	✓
987+25	332.3	324.50	7.8	46.7.	46.8.	25.0.	14%	0.24.	25.24.	1181.2	✓
987+50	328.9	321.00	7.9	47.2.	54.3.	25.0.	22%	0.60.	25.6.	1390.1	✓
987+75	325.1	315.50	9.6	61.4.	53.5.	25.0.	22%	0.60.	25.6.	1369.6	✓
988+00	317.7	310.00	7.7	45.6.	48.8.	25.0.	32%	1.25.	26.25.	1281.0	✓
988+25	310.5	302.00	8.5	52.1.						78653.6	✓

TRADE MARK

2918.1  
3222.7

20

78653.6  
8402.6

