

6

WEST

—————

SECTION

BOOK

NO. 226

W226



MICROFILMED

JAN , 1

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
IRVING PARK STATION  
CHICAGO, ILL.

92 FIFTH ST.  
PORTLAND, ORE.

79 NEW MONTGOMERY ST.  
SAN FRANCISCO, CAL.

AGENTS FOR  
"BERGER" TRANSITS and LEVELS  
"GURLEY" SURVEYING and HYDRAULIC INSTRUMENTS  
"CHICAGO" STEEL TAPES, etc.

H<sup>n</sup> line. Topography  
Sta.

9-8-27

P.O.G.  
Elliott  
Brooks  
Bailey

60+49

1940  
10.8

360

1930  
10.5

1925  
20.7  
2.77

1920  
29.8

1915  
43.1

Trig. above line = Elev.  
at station & dist. out

59+95

1930  
5.3

26

1925  
4.3

1920  
16.0

1915  
27.7  
35.3

1910  
35.9  
12.9

1905  
46.1

✓

59+25

1925  
8.0

20

1915  
16.8

1910  
26.7  
26.7

1905  
39.1

1900  
53.8  
2.2

1895  
60.2

1890  
73.9  
13.1

1880  
101.9

✓

58+63-46

1935  
5.0

32

1930  
5.8

1925  
14.5  
2.17

1920  
25.3  
1.2

1915  
36.8

1910  
47.7  
1.2

1905  
55.9

1900  
61.9

✓

58+00

1930  
5.5

26

1925  
3.2

1920  
11.6

1915  
22.0  
1.1

1910  
31.9

1905  
39.2

✓

57+50

1930  
3.0

28

1925  
6.2

1920  
13.7

1915  
33.0

1910  
41.8

✓

57+00

1935  
7.3

32

1930  
1.5

1925  
8.8

1920  
24.8

1915  
32.9

1910  
46.7

✓

50  
Rock

10  
50

H<sup>g</sup> line Topography  
Sta.

9-8-77  
P.O.G.  
Elliot  
Brooks  
Bailey

65+75

1930	18.9	1915	1910	1905	1900
3.8		14.5	34.3 41.7	55.3	76.0

64+82

1935	20.8	1925	1920	1915	1910
11.5	27.8	10.5	25.7 18.0 37.0	43.4	62.4

63+81.90

1940	37.4	1935	1930	1925	1920	1915
7.2		8.5	20.5	32.5 17.0 49.0	42.2	59.5

24.2  
23.3  
18.9

62+51.23

1935	32.8	1930	1925	1920	1915	1910
5.3		7.5	17.0	27.5 17.0 29.4	44.9	56.9

27.7  
24.7  
27.8

61+93.2

1930	29.0	1925	1920	1915	1910
2.0		7.7	15.0 13.0 23.0	28.6	37.5

61+69

1925	21.5	1920	1915	1910	1905
9.5		3.0	17.0 13.9	29.7 25.0	43.0

61+00 ✓

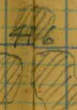
1935	33.4	1930	1925	1920	1910
1.6		4.7	17.8	26.9	

"H" Sta. Topography

9-8-27  
P.G.G.  
Elliott  
Brooks  
Bailey

72+80

1945  
14.2



1940 2.7  
1935 17.5  
1930 31.0  
1925 45  
1920 62.0  
1915 75.5  
1910 ✓

Single Boulders - diameter

72+00

1930  
36.2

1925  
6.8

73.8

1920  
24.8

1915  
40.6

1910  
52.0

1915 ✓  
9.5

70+50

1920  
17.5

1915  
9.0

70.8

1910  
1.7

1905  
11.2

1900 ✓  
21.8

69+25

1925  
7.2

71.7

1920  
2.5

1915  
10.8

1910 ✓  
21.8

68+81.33

1930  
9.7

1925  
1.7

74.4

1920  
7.0

1915  
21.7

1910 ✓  
28.8

67+86

1935  
6.1

72.3

1930  
5.5

1925  
15.6

1920  
22.0

1915  
36.5

1910 ✓  
49.0

66+85

1925  
8.0

72.0

1920  
5.2

1915  
20.0

1910 ✓  
42.0

Soil

7.5  
1.7  
3.3

31.7  
57  
87.9  
5.1  
22.3  
24.9  
2  
26.9  
4.0  
22.0

81+00

1930  
20.7

1925  
10.5

1920  
2.3

1915  
11.5

1910 ✓  
12.8

80+50

1930  
20

1925  
10

20.4

1920  
1.0

1915  
7.0

1910 ✓  
17.2

79+00

1935  
9.0

30.1

1925  
5.5

1920  
11.3

78+43

1935  
12.1

1930  
8.2

26.0

1920  
7.4

1915 ✓  
12.6

24.3  
12.7  
37.0

78+00  
77+00

soil

29.2  
8.9  
38.1

76+48.18

Rock

1935  
9.1

32.0

1930  
12.2

1925  
21.4

1920  
35.0

1915 ✓  
53.0

76+00

74+68.8

Soil

1935  
12.0

32.0

1930  
7.0

1925  
22.6

1920  
38.5

1915  
48.0

1910 ✓  
62.5

74+25

1935  
15.0

31.4

1930  
4.6

1925  
30.3

1920  
43.7

1915  
63.8

1910  
85.5

1/4" line Topography

9-2-27

87+91

Rock ↑

65.6

1905 1910 1915 50 45 40 35 30 25 20 15 10  
 P.O. 30.3 42.0 51.5 63.7 71.0 82.1 93.2 104.3 115.4 126.5  
 P.O. Gr Elliott Brooks Bailey

86+28.5

21.7

1920 1925 1930 1915  
 11.6 23.8 36.8 47.0

85+07

1925 1920 1915 1910 27.5  
 46.7 41.0 30.0 8.7

11.1  
 29.3  
 40.7  
 51.7  
 34.1

84+59

1930 1925 1920 19.6  
 25.5 14.5 0.8

GR. 26  
 25.6  
 43.7  
 11.0 12.2  
 56.0

84+00

1925 1920 1915 10.0 ✓  
 33.7 22.2 10.0

83+50

1925 1920 1915 12.4 ✓  
 33.5 28.5 13.5

20.3  
 72.4  
 23.7

12.3  
 72.8  
 24.6

82+50

Soil ↓

1930 1925 27.9 1920 1915 1910 ✓  
 12.2 2.8 7.6 16.0 35.2

81+60

1930 1925 21.5 1920 1915 1910 ✓  
 18.5 7.5 2.6 8.8 25.5

H line Topography  
Sta.

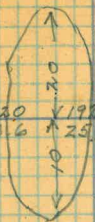
9-9-27

P.O.G.  
Elliott  
Brooks  
Bailey

94+00

Many loose boulders

1925 1930 2008 1925 1920 1920 1920 1915 1911 1905  
15.7 2.0 20.8 3.5 12.5 23.6 25.6 32.0 36.6 43.5



92+64.8

1925 1920 1915 1907 1910 1905 1900 1895 1890  
13.8 7.5 1.5 13.7 12.0 15.0 22.0 22.1 33.8

196  
29  
13  
11  
25

92+00

Rock

1930 1925 1920 1913 1915 1910 1905  
20.3 13.7 3.9 17.3 3.2 8.0 14.5

91+25

1930 1925 1920 1915 1910 1905 1900 99.6  
46.9 38.7 28.9 21.5 14.1 6.6 1.0

91+00

99+50

springs  
(slippery clay)

1925 1920 1915 1910 1905 1900 99.0 1895 1890  
77.9 63.5 50.0 36.6 23.8 8.0 6.1 18.0

89+50

1925 1920 1915 1910 1905 1900 98.7 1895 1890  
104.8 97.1 88.5 76.0 51.0 36.7 16.5 25.3

88+50

71.3 1940 1935 1930 1925 1920 1915 1910  
5.8 20.7 43.2 50.2 62.9



1. line Topography  
Sta.

9-12-27

ROG  
Eliott  
Brecht  
Bailey

Conts 9-16-27

Rainy

98+80

1930  
15.0

75.1

1920  
46

1915  
50

1910  
100

1900  
133

1925  
160

1915  
242

1910  
30.1

1905  
310

Rock  
outcrop



98+23

1940  
14.8

1935  
2.3

31.6

1930  
7.3

1925  
16.6

1920  
21.0

1915  
203

1910  
38.2

1905  
410

97+64.3

1935  
39

31.5

1930  
1.2

1925  
11.6

1920  
15.3

1915  
29.6

1910  
37.6

97+20

1940  
6.0

36.7

1935  
5.0

1930  
12.2

1925  
15.0

1920  
28.7

1915  
35.3

1910  
41.5

1905  
52.5

1900  
57.5

96+51

1935  
15.8

1930  
12.7

1925  
6.0

31.5

1920  
2.1

1915  
9.8

1910  
22.2

1905  
30.0

1900  
32.5

96+00

1930  
10.4

1925  
1.5

23.9

1920  
7.0

1915  
16.3

1910  
21.4

1905  
28.4

1900  
31.5

95+00 V

1930  
11.2

1925  
2.8

23.5

1920  
5.6

1915  
16.0

1910  
23.5

1905  
39.1

1900  
43.1

Rocks many loose boulders

Line Topography

Sta.

9-16-77  
P.O.S.  
Elliot  
Brant's  
Bailey

103+75

1925 1930 1925 1920 1920 1915 1910 1905 1900  
47.5 172 15.5 25.8 11.0 17.0 4.0 54.2 73.7

103+00

1930 1925 1920 1920 Road 1915 1910 1905 1900  
20.7 8.6 1.5 23.3 31.5 9.0 54.0

102+20

1925 1930 1925 1920 1915 Road 1910 1905 1900  
18.0 3.0 3.6 8.3 12.8 38.2 43.8 50.8

101+50

1920 1925 1920 1915 1910 Road 1905 1900  
15.8 7.7 3.0 8.2 34.7 41.5

101+00

1925 1920 1915 1910 1905 Road 1900  
26.5 15.3 11.0 7.5 33.0 4.0

100+00

1925 1920 1915 1910 1905 0.3 Road 1900 1895  
32.0 24.2 21.0 9.0 3.7 21.0 25.0

99+50

1925 1920 1915 1915 1910 0.3 1905 1900 Road 1895  
33.8 25.8 22.4 13.7 6.0 11.0 3.7 23.5

Earth Boulders

Rocks

Profile Topography

9-11-27  
R.D.S.  
E. H. ...  
Burdick  
Bailey

111+00

1935 1930 25.0 1920 1915 1910 1905  
179 70.5 5.0 15.0 24.2 34.0

110+27

1940 1935 30.8 1930 1925 1920 1915 1910 1905  
34.7 18.0 2.0 12.5 24.7 35.5 49.5 62.5

107+50

1935 Road 1930 1925 1920 1915 1910  
503 281 201 102 41 13.2 6.9

107+00

1935 Road 31.4 1930 1925 1920 1915 1910  
24.5 1.0 8.7 19.0 27.0 35.5

106+50

1935 Road 31.1 1930 1925 1920 1915 1910  
14.8 7.3 19.0 30.8 42.7 53.7

105+00

1935 Road 1930 1925 1920 1915 1910 1905 1900  
41.8 18.3 3.2 18.3 2.0 14.3 23.3 32.0

104+25

1935 1930 1925 21.2 1920 1915  
54.8 38.5 37.0 6.0 101.0

Earth Boulders

H Line Topog.  
Sta.

9-16-27  
R.G.  
Ellis  
Bailey

122+43.

1925 1920 1915 1910 1905 1900  
34.0 25.0 12.0 10.0 20.3 30.2

120+11 20 1915 1910 1905 1900 1895 1890 1885 1880 1875  
9.4 8.8 74.8 62.0 50.6 39.0 29.3 18.3 7.0 76.6

118+50

1930 1925 1920 1915 1910 1905  
26.0 17.7 5.4 4.0 16.0 28.5

87.6

117+50

1930 1925 1920 1915 1910 1905 1900  
21.2 8.7 5.4 20.8 36.5 45.8 62.5

115+00

1930 1925 1920 1915 1910 1905 1900  
19.0 5.2 23.4 10.7 27.8 42.0 55.4 65.3

113+70

1930 1925 1920 1915 1910 1905 1900  
73.5 68.0 60.5 49.0 35.3 2.0 15.0

112+77

1930 1925 1920 1915 1910 1905 1900  
47.1 26.7 8.7 20.5 12.0 31.5 47.0 60.0 75.5

East to Boulder

Hine Top up  
SL

132+00 1915 1910 1905 1900 1895 1890 1885 1880 72.7

734 627 537 446 374 233 120 27

130+90 1915 1910 1905 1900 1895 1890 1885 81.7

72.5 62.2 47.5 37.3 28.5 18.7 7.5

129+68 1920 1915 1910 1905 1900 1895 92.5

61.0 50.7 40.5 31.0 18.6 6.5

127+75 33.0

1930 1925 1920 1915 1910 1905 1900  
6.0 160 270 370 480 58.8 69.0

126+53.2 1920 1915 1910 1905 1900 92.5

42.3 34.3 22.6 11.0 1.3

125+00 1920 1915 1910 1905 1900 62.0

39.4 13.0 12.0

1925 1900  
3.0 12.5

123+86 1920 1915 1910 1905 1900 92.5

39.2 31.0 25.5 11.8 3.2

4-17-27  
206  
Elliot  
Boyley

Earth Bankers

H Line Topog.  
Sta.

9-17-27  
P.O.G.  
Ellis  
Bailey

132 141+50 1920 59.0 1915 58.0 1910 38.0 1905 21.2 1900 13.0 1895 5.0

134 140+33 1920 27.0 1915 17.7 1910 2.8 1905 5.0 1900 17.0 1895 25.7

137+75

17 138+85 1925 26.2 1920 17.0 1915 8.0 1910 9.8 1905 11.8 1900 21.6

12 137+25 1915 44.5 1910 35.7 1905 27.4 1900 20.0 1895 11.0 1890 1.6

12 136+50 1920 36.0 1915 29.6 1910 22.4 1905 13.5 1900 5.0

12 135+50 1920 22.1 1915 16.1 1910 8.8 1905 2.0

12 134+50 1920 51.0 1915 42.5 1910 32.2 1905 23.7 1900 15.0 1895 5.0

Earth Boulders

25

137  
5.2  
22.0  
12.7  
10.2

137  
5.2  
22.0  
12.7  
10.2

H Line Topog.  
Sta

9-17-27

P. O. B.  
Elliot  
Bailey

146+00

Bottom of draw 1944.5  
43.0

145+50

Bottom of draw 1925 1930 1935 1940 43  
32.1 25.6 20.6 10.7

144+64.6

143+75

1920 1915 1910 1905 42.5 1900 1900 1905 1910 1915  
29.0 20.5 11.4 3.2 3.0 13.5 20.0 32.0

142+75

1925 1920 1915 6 1910 1905 1900  
21.5 13.0 6.0 2.4 12.2 21.7

141+77.7

1920 1915 1910 1905 2  
18.0 11.0 6.2 2.7

158.3  
22.7  
11.0  
6.5  
4.5

Rocky

✓

2 ✓

H' Line Lower Location

±

Party -

Leach

Goodbody

Nov. 8, 1927.

129+63	1605	1610	1615	1620	1625	1630		
	240	200	141	90	52	13		

1635	1640
30	60

129+00	1610	1615	1620	1625	1626.9		
	153	111	65	18			

1630	1635	1640
19	51	86

128+10	1610	1615	1620	1625	1630	1635	1637.3
	143	115	86	60	38	15	

1640
18

127+50	1610	1615	1620	1625	1630	1635.0
	139	116	89	60	37	

1640
123

126+50		1610	1615	1616.7			
		76	26				

1620	1625	1630	1635	1640
33	32	90	115	136

125+28	1610	1615	1620	1625		
	116	83	50	8		

1630	1635	1640
28	57	87

Nov. 8, 1927

124+25



H' Line

Lower Location

138+50	1610	1615	1620	1625	1630	1635	1638.3
	203	188	166	138	63	29	
					25	34	

1640
13

Same Slope

137+50	1610	1615	1620	1625	1630.4
	253	216	171	82	

± Rd. 18L

1635	1640
46	91

137+00	1610	1615	1620	1625	1630.4
	194	132	81	41	

± Rd. +56

1635	1640
46	91

135+50	1615	1619.8
	79	

1625	1630	1635	1640
79	124	229	245

Earth

134+64	1610	1615	1620	1625	1629	1630	1635
	148	108	87	62	38	33	9

± Rd. ± Rd.

1640
18

134+55 ± Rd.

134+10 ± Rd.

132+00	1610	1615	1620	1625	1630	1635	1640
	62	3					

1620	1625	1630	1635	1640
48	79	108	125	144

131+00	1610	1615	1620	1625	1630	1631.5
	126	81	52	28	9	

1635	1640
13	36

H' Line Lower Location

145+66	1615 60	1620 46	1625 23	1630 6	1635 50	1640 96	1645 128
--------	------------	------------	------------	-----------	------------	------------	-------------

145+12  $\pm$  wash.

1628.6

74

1636.0

Earth

144+22	1615 96	1620 72	1625 48	1630 14
--------	------------	------------	------------	------------

1635 16	1640 56	1645 78
------------	------------	------------

143+50  $\pm$  wash.

1612.1

142+91	1610	1615 39	1620 28	1625 10
--------	------	------------	------------	------------

1630 15	1635 42	1640 70	1645 96
------------	------------	------------	------------

142+31  $\pm$  wash.

1613.0

141+88	1615	1620	1625	1630	1635
on Bank	156	142	124	99	47

1640 43	1645 73
------------	------------

140+73	1615	1620	1625	1630	1635	1640	1645
	146	113	86	61	41	25	7

139+50	1610	1615	1620	1625	1630	1635	1635.2
	247	197	151	90	53	20	

1640 21
------------

H Line Lower Location

±

150+00 1615 1620 1625 1630 1635 1636.2 1640 1645  
 180 163 113 54 10

49 118

149+26 1615 1620 1625 1630  
 193 154 101 32  
 39

1635 1640 1645  
 6 42 72

148+89<sup>26</sup> P.I. 1615 1620 1625 1630 1635 1640 1645  
 134 102 37 18 34 74 99

148+50 Earth 1615 1620 1625 1630 1635.5 1640 1645  
 120 108 80 36 30 71

147+50 1615 1620 1625 1630 1635 1638.0 1640 1645  
 188 155 121 75 24 23 45  
 34 44 121

146+50 1615 1620 1625 1630 1635 1638.5 1640 1645  
 144 125 99 64 23 19 60

146+10 ± small wash 1631.4

H Line Lower Location

Party Leach

Nov. 9, 1927.

Good body.

157+00	1615 187	1620 130	1625 50	1629.5	1630 5	1635 76	1640 (55) 131	1645 (63) 194
--------	-------------	-------------	------------	--------	-----------	------------	------------------	------------------

154+50	1615 302	1620 199	1625 114	1630 44	1634.2	1635 12	1640 70	1645 131
--------	-------------	-------------	-------------	------------	--------	------------	------------	-------------

153+50	1615 57	1620 44	1625 24	1630 5	1630.7	1635 33	1640 79	1645 127
--------	------------	------------	------------	-----------	--------	------------	------------	-------------

153+25 Edge of Bank →

152+95 & wash

← Drainage 1616.2

Edge of Bank.

152+69	1614 59	1615 57	1620 38	1625.5	1630 43	1635 95	1640 190	1645 250
--------	------------	------------	------------	--------	------------	------------	-------------	-------------

152+00	1615 90	1620 54	1625 36	1627.6	1630 33	1635 124	1640 207	1645 277
--------	------------	------------	------------	--------	------------	-------------	-------------	-------------

Nov. 9, 1927

151+50	1615 71	1620 50	1625 15	1625.7	1630 37	1635 107	1640 182	1645 267
--------	------------	------------	------------	--------	------------	-------------	-------------	-------------

H' Line Lower Location

1636.9  
86  
3.5

1615 342	1620 285	1625 238	1630 181	1635 142	1640 88	1636.9 3.1	1635 34	1630 70	1635 80	1640 90
-------------	-------------	-------------	-------------	-------------	------------	---------------	------------	------------	------------	------------

166+50 Edge of Bank.

165+90 Earth. ≠ wash

165+60 Edge of Bank.

164+75	1615 315	1620 253	1625 163	1630 69 90	1633.7	1635 13	1640 100	1645 196 310 211
--------	-------------	-------------	-------------	------------------	--------	------------	-------------	---------------------------

164+20 Edge of Bank

163+95 Field ≠ small wash

163+75 Edge of Bank.

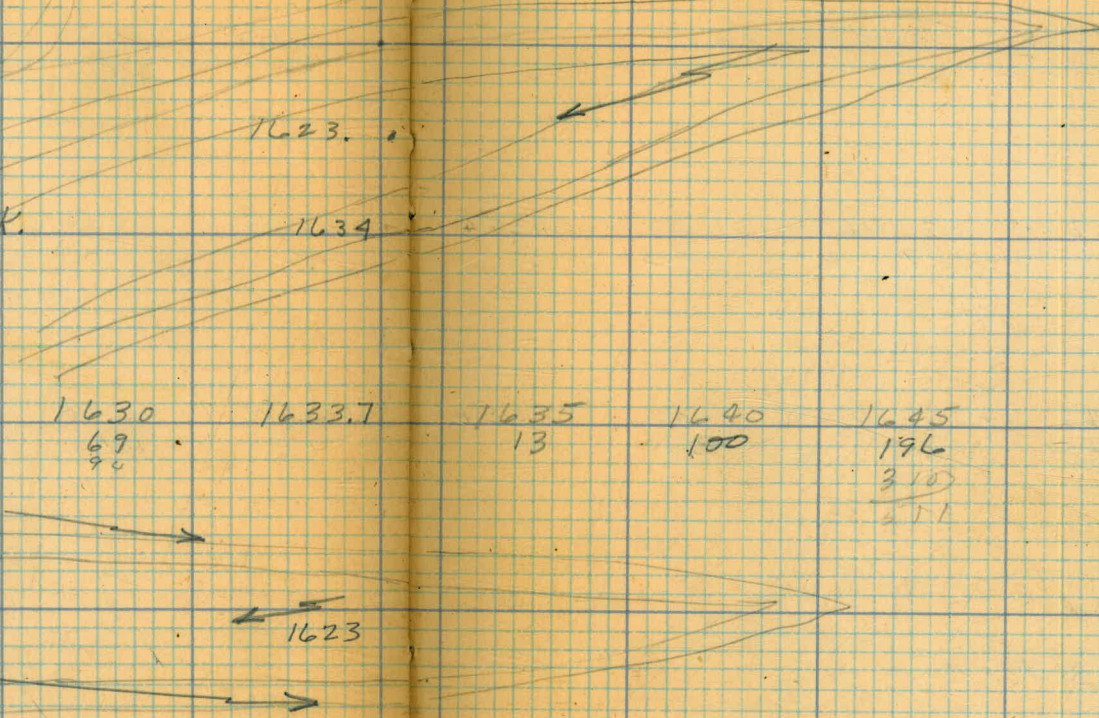
163+00	1615 189	1620 146	1625 126	1630 50	1633.6	1635 18	1640 86 68	1645 154
--------	-------------	-------------	-------------	------------	--------	------------	------------------	-------------

159+00	1615 176	1620 138	1625 96	1630 17	1631.6	1635 47	1640 124	1645 188
--------	-------------	-------------	------------	------------	--------	------------	-------------	-------------

158+50

158+00	1615 160	1620 151	1625 119	1630 71	1635 25	1637.3	1640 (D) 116	1645 187
--------	-------------	-------------	-------------	------------	------------	--------	-----------------	-------------

Earth (Plowed Field)



14' Line

±

178	1620 12 4	1625 78	1630 33	1633.7 59 92
-----	--------------	------------	------------	--------------------

1635 70	1640 44	1645 78	1650 107
------------	------------	------------	-------------

175+00	1620 15 8	1625 97	1630 61	1635 23	1638.4
--------	--------------	------------	------------	------------	--------

1640 92	1645 43	1650 73
------------	------------	------------

172+00	1622 230	1625 182	1630 100	1635 36 60	1638.1
--------	-------------	-------------	-------------	------------------	--------

1640 18	1645 80	1650 130
------------	------------	-------------

Earth

170+90 ± Road

→ To Bee Hives

170+50 Edge of Bank.

170+30 ± wash.

1630.0

170+00 Edge of Bank.

1636.6

169+00	1620 265	1625 224	1630 165 90	1635 89	1640 24	1641.0
--------	-------------	-------------	-------------------	------------	------------	--------

1645 61	1650 148
------------	-------------

H' Line

186+25

1617.5

1620

1625

1630

1635

9.5  
3.0

9

56

103

150

185+50

1620

1625

1626.3

1630

1635

1640

1645

1650

106

28

29

83

145

184

217

183+50

1620

1625

1628.3

1630

1635

1640

1645

1650

174

51

14

82

134

173

208

35

Earth.

182+75

1620

1625

1630

1632.4

1635

1640

1645

1650

233

128

37

26

88

131

171

180+50

1620

1625

1630

1635

1636.0

1640

1645

1650

225

184

122

69

14

42

96

151

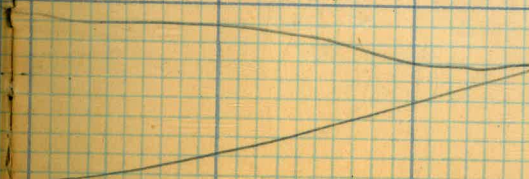
58

+32 Edge of Bank,

+16 ± wash.

1622.0

179+00 Edge of Bank.



H Line

191+60	1625 69	1630 52	1635 23	1639.6 55 1645.1	1640 20	1645 26	1650 50	1655 69
--------	------------	------------	------------	------------------------	------------	------------	------------	------------

191+15		1625 71	1630 51	1635 29	1640 30	1645 28 54	1650 62	1655 82
--------	--	------------	------------	------------	------------	------------------	------------	------------

190+50		1625 50	1630 27	1634.8 55	1635 10	1640 29 69	1645 64	1650 98	1655 125
--------	--	------------	------------	--------------	------------	------------------	------------	------------	-------------

190+25 Edge of Bank

189+85 Earth & wash.

16170

189+60 Edge of Bank.

189+50				1623.7 55 1629.2	1625 70	1630 34	1635 71	1640 101	1645 127	1650 167	1655 181
--------	--	--	--	------------------------	------------	------------	------------	-------------	-------------	-------------	-------------

188+00 <sup>07</sup>	1620 51	1625 26	1630 60	1631.3	1635 15	1640 49	1645 70	1650 95
----------------------	------------	------------	------------	--------	------------	------------	------------	------------

Note - Follow Contours around Parallel to Curve

187+50	1620 37	1625 21	1630 3	1631.8	1635 15	1640 33	1645 55	1650 75
--------	------------	------------	-----------	--------	------------	------------	------------	------------



H Line

Note: Follow Contours Parallel To Curve.

Cloudy and Raining  
Nov. 10, 1927

Party  
Leach  
Bate  
Goodbody

199756		1625 40	1630 17	1635 20	1640 24	1645 44	1650 64	1655 85			
199400			1625 31	1627.9	1630 4	1635 30	1640 48	1645 77	1650 86	1655 102	
198450		1625 43	1630 29	1635 13	1638.6	1640 5	1645 22	1650 37	1655 55		
197414	1625 33	1630 22	1635 11	1642.8	1640 5	1645 21	1650 38	1655 66			
196400				1622.0	1625 8	1630 22	1635 40	1640 58	1645 71	1650 84	1655 98
194450				1620.3	1625 19	1630 36	1635 55	1640 73	1645 87	1650 102	1655 115
193400				1624.8	1625 12	1630 17	1635 25	1640 47	1645 65	1650 76	1655 90

Earth

14' Line

Party Leach  
Bate  
Goodbody

Nov. 11, 1927.

Decorated Granite

208+00 1625 1630 1635 1640 1644.9 1650 1655  
69 49 33 19 19 43.5

207+00 1625 1630 1635 1640 1645 1650 1655 1655.5  
100 87 68 50 35 172 22

206+50 1625 1630 1635 1640 1645 1650 1655 1655.5  
125 107 88 71 53 32 3

Nov. 11, 1927

205+50 1625 1630 1635 1640 1645 1648.9 1650 1655  
94 74 47 30 12 8 27

204+50 1625 1630 1635 1640 1640.8 1645 1650 1655  
58 41 20 2 14 31 50

203+00 1625 1630 1632.9 1635 1640 1645 1650 1655  
29 8 28 22 36 49 63

201+00 1625 1630 1635 1637.3 1640 1645 1650 1655  
48 31 12 5 25 43 56

H' Line

218+50	1625 97	1630 52	1635 23	1640 2	1640.7	1645 23	1650 22 55	1655 38 V		
217+25	1625 161	1630 97	1635 47 114 61	1638.2	1640 18	1645 69	1650 113	1655 167		
215+00		1625 32	1627.7	1630 33	1635 78	1640 113	1645 147	1650 175	1655 215	
213+75		1625 172	1626.0	1630 56	1635 142 92	1640 224	1645 293	1650 344	1655 390	
211+50			1623.5	1625 72	1630 28	1635 47	1640 67	1645 82	1650 98	1655 113
210+00		1625 39	1630 16	1633.8	1635 5	1640 26	1645 40	1650 58 14 76	1655 76	
208+80 <sup>99</sup> EC.	1625 55	1630 30	1635 14	1638.2	1640 5	1645 22.5	1650 27	1655 51.5		

Decomposed Granite

226+00

±  
1643.3

Left edge Rd.

18° ←  
Rt. edge Rd.

225+00 1625 1630 1635 1640 1641.6 1641.6  
58 39 25 14

1641 1645 1650 1655  
11 ← 14 ← 20 31

224+00

→

Edge of Rd.  
13° Left

Edge of Rd.  
7° Rt. ↓  
Edge of Bank.

223+38.82

1625 1630 1635 1640 1640.0  
49 36 21 8 ←

1640 1645 1650 1655  
10 ← 15° 23 39

223+00 ± Road.

Left edge Road

Edge of Rd

222+67

Edge of Road

1639

1637.8

21 ←

Left edge Rd

Rt edge Road

222+63

Bank.

1641.3

Edge of Road and Bank

222+25

1625 1630 1635 1640 1642.5  
39 15

1645 1650 1655  
5 22 47

221+25.89

1625 1630 1634.7  
43 19

1635 1640 1645 1650 1655  
10 16 32 44 55

220+00

1625 1630 1635 1637.3  
56 30 11

1640 1645 1650 1655  
8 28 40 55

231+50      1630 1635 1640 1645 1650 1650.5  
 43      42      30      15      2

1655      1660  
 7      38

230+75      1630 1635 1640 1645      1647.4  
 Nov. 14, 1927      72      45      22      9

1650      1655      1660  
 10      28      60

Left edge of  
 96 Road

230+50      1630 1635 1640 1640 1642.8  
 72      46      23      13

1645      1650      1655      1660  
 8      24      44      80

229+00

1640.2      1645 1650 1652.6 1652.6 1655 1660 1665 1670  
 13      25      28      48      62      51      68      81

1645  
 7

Left edge of Rd.      Rt. edge Rd.

227+25      1630 1635 1640 1642.8  
 58      49      19      12.2  
 3.0

1647.5 1647 1650 1655 1660  
 8      26      30      37      48

Left edge Rd.      Rt edge Rd.

226+92.87 B.C.

8

26

Edge of Bank

226+00 1625 1630 1635 1640 1643.3  
 65      49      28      9

1645 1650 1655  
 17.6      28      43

52  
19  
31

235+55	1630 <sup>52</sup> 59	1635 <sup>19</sup> 43	1640 19	1643.5	1645 28	1650 46	1655 64	1660 88
--------	--------------------------	--------------------------	------------	--------	------------	------------	------------	------------

235+50  
2<sup>nd</sup> Bank of wash → 1642.5

235+31  
w/ wash → 1634.5

234+63	1630 50	1635 37	1640 26	1645 62	1645.9 5.5	1650 19	1655 65	1660 79
--------	------------	------------	------------	------------	---------------	------------	------------	------------

1<sup>st</sup> Bank of wash →

233+90	1630 59	1635 67	1640 47	1645 28 61	1650 5	1655 18	1660 47
--------	------------	------------	------------	------------------	-----------	------------	------------

232+84	1630 31	1635 18	1640 8	1642.2	1645 4	1650 18	1655 26	1660 50
--------	------------	------------	-----------	--------	-----------	------------	------------	------------

232+00	1630 47	1635 37	1640 27	1645 18	1648.3	1650 10	1655 28	1660 45
--------	------------	------------	------------	------------	--------	------------	------------	------------

±

42.8  
42  
26.0

26

240+50

1635 1639.3  
16

1640 1645 1650 1655 1660 1665  
12 16 25 42 51 66  
17

240+22

± wash

1632

240+00

1635 1640 1640.7  
8 12

1645 1650 1655 1660 1665  
46 47 54 76 95

239+00

1635 1640 1645 1650 1655 1656.8  
64 54 39 29 15

1660 1665  
27 53

Earth and Rock

238+12

1635 1640 1645 1650 1655  
99 84 49 25

1660 1665  
23 36

237+15

1630 1635 1640 1641  
92 67 12

1645 1650 1655 1660  
36 58 75 92

236+16

1630 1635 1640 1645 1649.0  
70 58 42 20

1650 1655 1660  
5 22 42

Solid Rock

244+91 1635 1640 1645 1650 1655 1660 1661.9 1665  
76 68 54 43 24 9 33

244+7900 ↳ Top of large Rock  
9' high

Earth and Rock

244+00 1635 1640 1645 1650 1655 1660 1662.9 1665  
102 83 62 52 24 6 38

243+25 1635 1640 1645 1650 1655 1658.0 1660 1665  
83 65 38 18 5 38 74

242+747 1635 1640 1645 1646.7 1650 1655 1660 1665  
66 41 4 23 39 58 85

241+63 1635 1640 1645 1650 1655 1657.6 1660 1665  
68 52 30 18 9 15 44

241+00 1635 1640 1645 1648.9 1650 1655 1660 1665  
64 46 28 3 22 38 ~ 49



249+75 1635 1640 1645 1650 1655 1655.4 1660 1665  
158 140 108 58 19

1660 1665  
144 188

248+63 1635 1640 1645 1650 1655 1660 1662.0 1665  
155 130 105 84 67 33 31

Rock

248+00 1635 1640 1645 1650 1655 1660 1660.8 1665  
143 132 112 91 29 11 30

road

247+25 1635 1640 1645 1650 1655 1658.7 1660 1665  
125 114 60 48 32 15 37

Earth

247+00 ± small wash.

246+60 1635 1640 1645 1650 1655 1660 1665  
84 65 53 43 33 16 13

245+61 <sup>31</sup>/<sub>x</sub> 1635 1640 1642.5 1645 1650 1655 1660 1665  
20 6 15 39 57 80 91

260+50 1635 1640 1645 1650 1655 1658.5  
59 48 37 31 17

1660 1665  
6 26.5  
26  
27

259+50 1635 1640 1645.1  
30 13

1650 1655 1660 1665  
21 41 58 77

258+50

257+50 1635 1640 1645 1648.4  
51 36 20

1650 1655 1660 1665  
5 25 43 67

256+75

1635 1637.6  
72

1640 1645 1650 1655 1660 1665  
8 33 57 76 93 125  
69

254+10

1570

High water mark.

253+25

1557

Center of Santa Maria Creek.

253+15

1570

High water mark.

Earth and Rock.

Leach A. C.  
Bate J. F. L.  
Goodbody, J. R.

265+42

1635 1639.4  
36

1640 1645 1650 1655 1660 1665  
13 39 64 80 102 125

265+00 1630 1640 1645 1650 1655 1656.5  
107 88 68 39 1010

1660 1665  
24 56

264+00 1635 1640 1645 1648.5  
49 29 12

1650 1655 1660 1665  
6 30 57 83

263+85

1645

⊕ small Wash

263+34 1635 1640 1645 1650 1654  
66 50 34 17

1655 1660 1665  
5 27 47

262+0 1635 1640 1645 1650 1654.5  
57 43 19 2

1655 1660 1665  
9 25 41

Nov. 15, 1927

261+45 1635 1640 1645 1648.0  
43 31 18

1650 1655 1660 1665  
2 20 39 56

Earth and Large Rocks

274+18		1640 63	1645 27	1649.3	1650 2	1655 52	1660 91	1665 122	1670 151	
272+50			1640 15	1642.4	1645 14	1650 41	1655 64	1660 90	1665 118	1670 154
271+25		1640 31	1645 59	1649.6	1650 5 40	1655 72	1660 105	1665 153	1670 187	
269+50	1635 79	1640 62	1645 46	1650 18 1652.5	1655 216	1660 49	1665 72			
					1650					
268+26	1635 386	1640 340	1645 289	1650 29	1653.5	1655 28	1660 63	1665 87		
267 265+0	1635 201	1640 135	1645 52	1649.1	1650 11	1655 52	1660 90	1665 130		
266+10	1635 76	1640 59	1645 41	1650	1655 33	1660 75	1665 120			

Easthead Scatterd Rock

Rocks  
250

18  
1652.5

281+10	1640	1645	1650	1652.0	1655	1660	16
	120	74	34		71	150	99

279+50	1640	1645	1650	1653.0	1655	1660	21	37
	36	27	15		15	67		

278+88	1640	1645	1650	1652.7	1655	1660	
	20	17	9		16	58	

278+50

Large Rock

on line

on line

16 x 22 14" in height

182.5 Cy Yds

277+50	1640	1645	1650	1655	1658.3	1660	1665	1670
	108	93	82	36		63	110	207

Earth and Rocks

276+05		1640	1643.2	1645	1650	1655	1660	1665	1670
		23		12	49	74	107	130	175

275+0	1640	1645	1646.5	1650	1655	1660	1665	1670
	49	12		19	52	79	102	145

287+50 1640 1645 1650 1655 1655.8  
 182 115 51 7

1660 1665 1670  
 65 108 154

286+72.9 Second Edge Pavement 1653.5

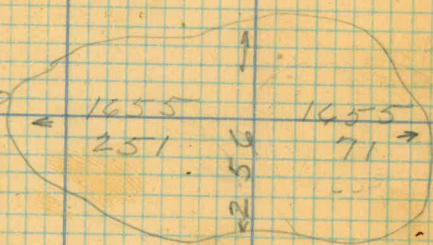
286+50.7 First Edge Concrete Pavement 1653.9

Ramona Julian Highway

1640 1645  
 378 358

284+99.4 1650 1655 1655 1652.6  
 321 251 71

1655 1660 1665 1670  
 70 151 201 241



284+00 1645 1646.6  
 5

1650 1655 1660 1665 1670  
 20 54 90 137 178  
 1670

282+50 1640 1645 1647.9  
 86 33

1650 1655 1660 1665  
 19 71 149 221

281+76 1640 1645 1646.2  
 29 4

1650 1655 1660  
 25 76 150

59  
36  
~~105~~

291+00	1640 122	1645 51	1649.9	1650 12	1655 38	1660 86	1665 130	1670 174
--------	-------------	------------	--------	------------	------------	------------	-------------	-------------

296+00	1640 126	1645 89	1650 63	1655 37	1660 59	1665 50	1670 103
--------	-------------	------------	------------	------------	------------	------------	-------------

289+33	1640 105	1645 32	1648.4	1650 13	1655 53	1660 95	1665 142	1670 185
--------	-------------	------------	--------	------------	------------	------------	-------------	-------------

288+75	1640 97	1645 67	1650 52	1655 36	1660.1	1665 40	1670 85
--------	------------	------------	------------	------------	--------	------------	------------

288+25			1656.5
--------	--	--	--------

287+84	Wash	1648.2
--------	------	--------

287+75	1st Bank Wash	1651.2
--------	---------------	--------

293+0 1640 1645 1650 1655 1655.2  
56 33 1

1660 1665 1670 1675  
34 64 110 138

292+85 2nd Bank Wash 1651.2

292+70  $\phi$  Wash 1638.5

292+30 1st Bank Wash 1642.5

292+00 1640 1645 1650 1653.8  
129 108 68

1655 1660 1665 1670  
21 75 129 177

291+85 same as

291+50

291+50 1640 1645 1650 1654.5  
154 100 48

1655 1660 1665 1670  
5 77 115 159



Start of farm Property.

Nov 16 1927

Party - Leach  
Bate  
Goodbody

302+60<sub>n</sub> 1652

302+19 \$ wash 30' Left well 1629

301+78 Edge of Bank. 1650

301+43 1645 1650 1655.4 1660 1665 1670 1675  
52 26 34 62 87 173

300+30 1645 1650 1655 1657.7 1660 1665 1670 1675  
75 41 13 112 35 58 83

297+30 Edge of Bank. 1657.

297+05 \$ small wash. 1650

296+79 Earth Edge of Bank. 1658.

296+50 1645 1650 1655 1660 1661.8 1665 1670 1675  
134 98 53 16 31 66 101

Nov 16, 1927

295+30 1645 1650 1655 1660 1662.8 1665 1670 1675  
181 130 92 44 34 76 105

294+0 1645 1650 1652.8 1655 1660 1665 1670 1675  
63 30 48 62 81 107 130

H' line

306+50	1645	1650	1655	1660	1663.3	1665	1670	1675
	76	48	38	22		14	46	79

End of Euc. Trees

305+73	1645	1650	1655	1660	1663.5	1665	1670	1675
	81	58	39	22		11	39	68

305+50	Bank of wash.				1660.2
--------	---------------	--	--	--	--------

305+25	wash.				1652.0
--------	-------	--	--	--	--------

305+00	1645	1650	1655	1660	1660.4	1665	1670	1675
	97	63	43	22	12	21	45	72

Bank of wash

House.  
25°

Note. wash varies about 12° off Rt. Angle.

304+00	wash.				1645	1649.7	1650	1655	1660	1665	1670	1675
					52		20	40	64	90	116	152

Eucalyptus Trees.

303+79	1645	1650	1653.7	1655	1660	1665	1670	1675
	53	35		8	36	62	88	135

303+00	1645	1650	1653.8	1655	1660	86 ft. to canyon wall	
	59	28		13	41		

309+50	1645	1650	1655	1660	1663.	1665	1670	1675
	78	60	41	15	1	8	35	59
				PK				
				3				

+29 Bank. 1661.

309+00  $\neq$  small wash.

308+82	Bank.	1645.	1650	1655	1657.5	1660	1665 <sup>v</sup>	1670	1675
		41	31	16	12.5	9	31	53	77
				25	50				

308+67 Bank. 1655

+48  $\neq$  wash. 1650

+34 Bank. 1655

308+00	1645	1650	1655	1657.3	1660	1665	1670	1675
	55	39	76	12.5	15	37	61	86
			PK		16			

307+39 1655.5

307+16  $\neq$  of wash. 1650.

307+00 Edge of Bank. 1657.2

Decomposed Granite

316+17

1641.1

1645  
14

1650  
29

1655  
48

1660  
73

1665  
93

1670  
110

1675  
120

300' end approx.

Solid Rock

315+50

1645

1650

1655

1660

1664.2

1665

1670

1675

Feet Bank Wash

78

51

35

24

3#

6

32

53

314+90

314+75

1645

1650

1655

1660

1665

1670

1675

87

68

37

14

3

12

12

36

Parallel Curve with Contours

30'

8 ft. High

314+50

313+50

1645

1650

1655

1660

1665

1670

1675

83

69

48

31

12

11

33

312+00

1645

1650

1655

1660

1665

1670

1675

Earth

127

104

81

59

35

11

32

311+00

Bank.

1665

310+56

± wash.

1650

310+20

1645

1650

1655

1660

1664.1

1665

1670

1675

Edge of Bank.

89

72

47

25

4

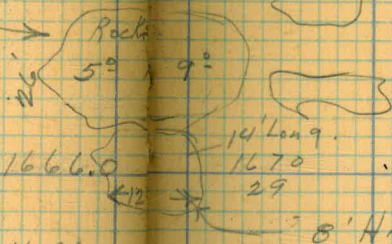
28

57

H. Line Lower Location

+25

18 High



326+00

1645	1650	1655	1660	1665	1666.50	1670	1675
52	37	14	11	20	29	50	

318+70

small wash.

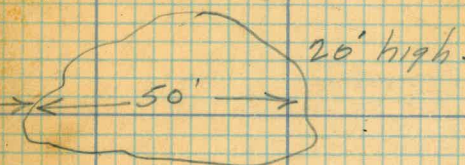
1644.0

318+50

1645	1647.7	1650	1655	1660	1665	1670	1675
10		8	43	61	73	84	96

217+83

1632.5



+45

Approx. →

1645	1650	1655	1660	1665	1670
69	73	118	126	138	151

+30

Earth and Rock.

1646

1645	1650	1655	1660	1665	1670	1675
120	69	93	118	126	138	151

317+00

1645	1648.7
27	

1650	1655	1660	1665	1670	1675
8	39	57	73	88	104

316+50

Same as

Sta. 317+00

#23 small wash.

1669

328+00	1650	1655	1660	1665	1670	1671.4	1675	1680
	51	43	33	18	3	5.4	12	25
						70		

327+00	1650	1655	1660	1665	1668.5	1670	1675	1680
	59	41	25	12		5	20	33

325+80						1656		
--------	--	--	--	--	--	------	--	--

325+65	1650	1655	1659.0	1660	1665	1670	1675	1680
	36	14		3	26	50	67	86

325+16	1650.0	1655	1660	1665	1670	1675	1680
		29	35	84	105	121	134

324+67 shift	1650	1655	1657.4	1660	1665	1670	1675	1680
	23	112		11	28	51	67	85

322+75	1645	1650	1655	1660	1660.6	1665	1670	1675
	64	35	16	12		16	32	57

321+83 <sup>83</sup>	1645	1650	1655	1660	1664.7	1665	1670	1675
	89	65	43	23		12	20	39

16528  
55  
2

Leach  
Bate  
Good body

337+0 1650 1652.5 1655 1660 1665 1670 1675 1680  
22 25 40 49 60 77 125

336+0.5  $\neq$  wash. 1618.0

Nov. 17, 1921

335+00 1650 1655 1660 1663.2 1665 1670 1675 1680  
39 32 15 11 36 57 79

Earth and Rock

333+00 1650 1655 1660 1665 1666.9 1670 1675 1680  
58 39 21 5 9 24 31

Follow Contours Parallel to Cupre

331+38~~82~~ 1650 1655 1660 1663.7 1665 1670 1675 1680  
43 27 11 6 21 35 47

329+50 1650 1655 1660 1665 1670 1675 1680 1691.6  
118 102 86 71 57 41 29 80  
6 23 11.5 9.5 7.7

328+96  $\neq$  small wash 1687

Solid Rock  
118  
← 20' ↑  
Hairs.

341+25 1650 1655 1660 1665 1668.9  
137 80 34 15

40' Solid Rock  
Nose.  
1670 1675 1680  
7 33 46

340+88<sup>20</sup> First Bank Wash 1684.3

340+60 1650/1655/1660/1665/1670/1675/1680/1687.0  
183 142 102 74 58 41 24

339+50 1650 1655 1660 1665 1670 1675 1676.4  
150 108 65 44 25 5

338+74<sup>20</sup> 1650 1655 1660 1663.6 1665 1670 1675 1680  
76 46 18 9 36 110 118

338+0  $\frac{1}{2}$  Wash 1636.5

Top Ridge

337+36<sup>20</sup> 1650 1655 1660 1661.4 1665 1670 1675 1680  
60 41 17 21 50 83 141

Earth and Scattered Rock



349+99

♀ small Wash

1650

145

349+0	1655	1660	1665	1670	1675	1680	1686.4
	130	114	93	70	40	23	

348+19	1650	1655	1660	1665	1670	1675	1680	1690.0
	149	144	124	112	93	83	55	

347+50	1650	1655	1660	1665	1668.5	1670	1675	1680	♀ wash
	97	79	64	30					

347+00	1650	1655	1660	1665	1670	1675	1680	1691.2
		62	49	42	28	15		

345+50	1650	1655	1660	1665	1670	1675	1677.6	1680
	54	45	37	31	21	11	120	7

344+0	1650	1655	1660	1665	1670	1672.9	1675	1680
	111	81	50	34	13		5	31

1650

124

342+32	1655	1660	1665	1670	1675	1680	1687.0
	113	96	83	55	34	19	

Earth and Rock

Solid Rock

Sta 346+37.3 to 347+00

1680

1675

1680

Solid Rock

178

355+50 1655 1660 1665 1670.4

76 52 23

355+0 1655 1660 1665 1670 1672.5

71 50 67 48 30 10

1655  
104

353+50 1660 1665 1670 1675 1680 1685 1688.4

89 67 63 44 28 12

18' High  
45 x 28

353+38

Solid Rock 35' Left &

1655  
101

Solid Rock  
125'

352+68 1660 1665 1670 1675 1680 1685 1704.5

96 92 76 71 59 43

352+0

Solid Rock

351+60 1655 1660 1665 1670 1675 1680.0

63 50 37 31 21

1685  
9

1655  
120

350+0 1660 1665 1670 1675 1680 1685 1694.5

106 90 72 57 44 31

20

1670 1675 1680 1685

3 24 41 62

1675 1680 1685

10 32 55

Scattered Rock  
Decomposed Granite

Earth and Rock

44  
18  
92

360+20 1st Bank Wash 1658.7

359+0	1655	1660	1665	1666.6	1670	1675	1680	1685
	91	54	16		24	61	92	114
						65		
						73		
						38		

358+68  $\frac{1}{2}$  Wash 1666.2

358+34  $\frac{1}{2}$  Hogs Back 1664.9

358+00  $\frac{1}{2}$  Wash 1660.4

357+76 1st Bank Wash 1670.8

357+28	1655	1660	1665	1670	1675	1676.0	1680	1685
	138	106	73	38	6		24	48

36770 1655 1660 1665 1665.9  
41 23 4

1670 1675 1680 1685  
20 68 112 151

365495 1655 1660 1665 1670 1674.0  
117 91 61 25

1675 1680 1685  
5 39 70

36540 2nd Bank 1662.2  
-7

364771 1/2 Wash 1658.7

364750 1st Bank 1661.5

363750 1655 1660 1664.2  
37 13

1665 1670 1675 1680 1685  
7 40 69 101 134

361750 1655 1659.8  
50

1660 1665 1670 1675 1680 1685  
5 39 71 93 112 140

361420 2nd Bank Wash 1658.6

360481 1/2 Wash 1643.9

Party  
Leach  
Bate  
Good body

Nov. 18, 1927

373+50	1660 73	1665 44	1670 25	1675 5	1676.0	1680 21	1685 48	1690 77
--------	------------	------------	------------	-----------	--------	------------	------------	------------

372+71	Bank of wash.				1671.1			
--------	---------------	--	--	--	--------	--	--	--

372+50	E wash.				1663.2			
--------	---------	--	--	--	--------	--	--	--

372+24	Bank of small wash.				1665.7			
--------	---------------------	--	--	--	--------	--	--	--

371+83	1660 23	1665 9	1667.8 22.3	1670 8	1675 26	1680 44	1685 64	1690 79
--------	------------	-----------	----------------	-----------	------------	------------	------------	------------

Earth and Rocks.

370+50	1660 24	1665 2	1665.4 2	1670 23	1675 32	1680 52	1685 65	1690 84
--------	------------	-----------	-------------	------------	------------	------------	------------	------------

↑  
70' Rock  
↓  
130'  
Solid

22' High

369+25	1660 66	1665 39	1670 14	1672.5	1675 12	1680 31	1685 60	1690 89
--------	------------	------------	------------	--------	------------	------------	------------	------------

Nov. 18, 1927

368+50	1660 77	1665 41	1670 9	1671.2	1675 24	1680 63	1685 85	1690 98
--------	------------	------------	-----------	--------	------------	------------	------------	------------

367+50		1655 26	1660.0	1665 80	1670 99	1675 111	1680 136	1685
--------	--	------------	--------	------------	------------	-------------	-------------	------

381+75  $\neq$  wash. 1630.6

380+83 Bank. 1660 1665 1665.9 1670 1675 1680 1685 1690  
61 13 49 78 114 134 161  
63 63

379+00 1659.1 1660 1665 1670 1675 1680 1685 190  
5 34 71 108 141 172 194

378+80 Bank. 1658

378+35  $\neq$  wash. 1643.1

378+00 Bank of wash. 1659.5

377+87  $\neq$  wash. 1660 1665 1670 1675 1680 1685 1690  
30 23 57 88 125 151 190  
120

377+56 Bank. 1660

376+70  $\neq$  wash. 1630.0

376+15 1654.9 1660 1660 1660 1665 1670 1675 1680 1685 1690  
55 107 169 176 183 198 221 240 261  
12 12 20

375+65

Approx  $\rightarrow$   $\frac{1660}{209}$  1665 1670 1675 1680 1690  
216 225 238 251 281

374+75 1660 1665 1670 1671.5 1675 1680 1685 1690  
61 46 9 50 102 134 155

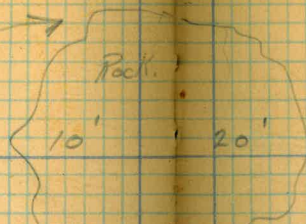
386+85<sup>93</sup> PI

Contacts same as

386+50

386+50	1660 28	1665 17	1670 24	1671.0	1675 10	1680 19 24	1685 30	1690 43
--------	------------	------------	------------	--------	------------	------------------	------------	------------

386+30



386+00

El. Top of Rocks. 1990.

385+40

El. Top of Rocks. 1690

385+29

1660 41	1665 29	1670 15	1673.3	1675 8	1680 17	1685 31	1690 44
------------	------------	------------	--------	-----------	------------	------------	------------

384+50

1660 47	1665 42	1670 30	1675 19	1680 9	1682.6	1685 20	1690 102
------------	------------	------------	------------	-----------	--------	------------	-------------

383+81

Solid Rocks.

1660 58	1665 33	1670 19 24 32	1673.3	1675 6	1680 24	1685 42	1690 57
------------	------------	------------------------	--------	-----------	------------	------------	------------

383+00

1660 16	1665 6	1669.9	1675 12	1680 24	1685 1 31	1690 38
------------	-----------	--------	------------	------------	-----------------	------------

Solid Rock.

Solid Rock

30'

Solid Rock.

382+25

1648.1	1660 43	1665 54	1670 68	1675 78	1680 89	1685 98	1690 113
--------	------------	------------	------------	------------	------------	------------	-------------

395+65

1665 1670 1675 1676.3  
22 12 2

1680 1685 1690 1695  
11 22 31 46

1671.8

Earth and Rocks.

394+00

1665 1670 1675 1679.8  
29 19 10

1680 1685 1690 1695  
10 9 22 32

392+25

1665 1670 1675 1679.1  
27 15 8

1680 1685 1690 1695  
10 12 21 29

391+32

1665 1670 1675 1680 1685 1690 1695 1696.3  
47 37 29 22 15 7 2

390+55 El. Rock. 10' Left.

1710

390+18

1665 1670 1675 1680 1685 1690 1693.5  
57 47 39 27 21 13

1695  
5

Rocky.

389+85

Large Rock.

70' High.

1665  
7.6

388+85

1670 1675 1680 1685 1690 1695 1700.0  
69 63 47 37 26 12



401+30	1665 40	1670 30	1675 21	1680 9	1683.3	1685 4	1690 16	1695 21 <sup>0</sup>
--------	------------	------------	------------	-----------	--------	-----------	------------	-------------------------

401+00

400+75	1665 59	1670 51	1675 43	1680 30	1685 23	1690 11	1691.9	1695 6 <sup>0</sup>
--------	------------	------------	------------	------------	------------	------------	--------	------------------------

400+40

400+27	1665 43	1670 28	1675 15 2 <sup>0</sup>	1680 2	1680.6	1685 9	1690 20	1695 34
--------	------------	------------	------------------------------	-----------	--------	-----------	------------	------------

399+75

Solid Rock ← 36 →

399+50	1665 34	1670 24	1675 14	1680 5	1682.9	1685 5	1690 12	1695 22
--------	------------	------------	------------	-----------	--------	-----------	------------	------------

397+75	1665 38	1670 24	1675 14	1690.5	1680 1	1685 14	1690 30	1695 42
--------	------------	------------	------------	--------	-----------	------------	------------	------------

396+75		1665 3	1668.7	1670 14	1675 25	1680 35	1685 47	1690 63	1695 71
--------	--	-----------	--------	------------	------------	------------	------------	------------	------------

Solid Rock

14' High

34

Earth and Rock

4265  
79

410+0  
Nov. 19, 1927 1670 1675 1680 1685 1690 1692.8

1665  
103

409+00 1670 1675 1680 1685 1690 1691.6

407+75 1665 1670 1672.5 1675 1680 1685 1690 1695

406+50 1665 1670 1675 1676.4 1680 1685 1690 1695

405+50 1665 1670 1675 1680 1680.7 1685 1690 1695

404+50 1665 1668.9 1670 1675 1680 1685 1690 1695

403+00 1665 1670 1675 1680 1682.7 1885 1890 1895

Leach  
Bate  
Goodbody

Earth on scattered rocks

1695  
1

1695  
9

1675 1680 1685 1690 1695  
6° 19 31 42 55

1680 1685 1690 1695  
12 20 29 44

1685 1690 1695  
8 18 29

1670 1675 1680 1685 1690 1695  
2 14 23 32 45 56

1885 1890 1895  
3 13 25

Earth and Rocks

1665  
62

418+83<sup>20</sup> 1670 1675 1680 1685 1690 1695 1702.4  
53 44 39 32 22 14  
<sub>14</sub> <sub>17</sub>

417+21 1665 1670 1675 1680 1685 1886.1 1690 1695  
37 32 24 15 2 7 15  
<sub>17</sub>  
<sub>17</sub>

417+00  
← 70 Solid Rock → 1683.6  
136

416+16<sup>20</sup> 1665 1670 1675 1680 1685 1686.0 1690 1695  
92 86 58 37 16 7 19  
<sub>34</sub>

414+83 1665 1670 1675 1680 1683.3 1685 1690 1695  
39 27 13 3 6 28 46

414+00 1665 1670 1677.4 1675 1680 1685 1690 1695  
16 5 6 15 33 55 87  
EARTH

412+75  
Crack Bed 1606.0

423+50	1670	1675	1680	1680.4
	39	27	2	

Ground Pot hole

422+75

16' High  
Solid Rock

← 40 →

↓ 25 ↓

422+0	1665	1670	1675	1679.7
	65	43	18	

421+0	1665	1670	1675	1680	1685
	299	275	258	242	223

420+27 <sup>12</sup>	1665	1670	1675	1680	1685	1689.1
	104	69	44	25	11	

1665  
65

419+25	1670	1675	1680	1685	1690	1694.6
	57	46	31	18	6	

419+0

↑ 422  
Solid Rock

Scattered Rocks (Laying on line)

1685	1690	1695	1700
11	20	36	53

1680	1685	1690	1695
1	17	39	56

Saddle

1690	1695	1700	1700	1698.1
207	195	160	35	

Earth and Rock

1690	1695
3	22

1695
5

Party

Leach  
Bate  
Goodbody

432+25	1670 95	1675 61	1680 17	1682.4	1685 21	1690 60	1695 98	1700 130	
Nov. 21, 1927									
431+0	1670 67	1675 20		1677.1	1680 16	1685 42	1690 67	1695 94	1700 124
430+0	1670 85	1675 47	1680 19	1682.6	1685 13	1690 50	1695 92	1700 139	
429+0	1670 66	1675 16		1676.9	1680 38	1685 87	1690 148	1695 178	1700 212
428+50	Wash			1659.0					
427+50	1670 54	1675 23		1677.2	1680 24	1685 70	1690 103	1695 139	1700 185
424+50	1670 43	1675 30	1680 19	1684.6	1685 2	1690 35	1695 49	1700 67	

437+00			1669.1		1670	1675	1680	1685	1690	1695	1700
					71	84	104	117	149	155	164

436+33	1680	1675	1680.2	1685	1690	1695	1700
	36	73		18	80	93	104

435+85			1659.		1670	1675	1680	1685	1690	1695	1700
					71	100	126	138	157	175	185

435+50		1670	1674.2	1675	1680	1685	1690	1695	1700
		50		28	44	61	97	87	100

↩

434+70 <sup>39</sup>	1670	1675	1680	1685	1686.4	1690	1695	1700
	64	41	24	8		19	41	85

434+28		1670		1675	1675.2	1680	1685	1690	1695	1700
		33		6		24	51	80	104	117

433+50	1670	1675	1680	1685	1685.8	1690	1695	1700
	84	62	30	5		29	63	97

441732	1670	1675	1680	1685	1690	1695	1695.5	1700
	115	90	52	27	14	2		11

440785	1670	1675	1680	1685	1690.0	1695	1700
	196	102	59	24		11	21

440700	1670	1675	1680	1685	1690	1695	1700.2	1700
	194	170	144	108	65	32		11

439706  $\pm$  small wash. 1686

Earth

77	1670	1675	1680	1685	1690	1693.6	1695	1700
	95	84	51	40	24		10	36

750  $\pm$  wash. 1685.9

438700	1670	1675	1680	1685	1690	1693.0	1695	1700
	121	100	78	52	21		10	31

450+13  $\neq$  wash. 1681

449+90 Bank of Wash. 1695.

449+50	1675	1680	1685	1690	1691.8	1695	1700	170.5
	78	61	34	10		20	60	98

446+50	1675	1680	1685	1688.2	1690	1695	1700	170.5
	55	36	15		8	37	75	95

445+70	1675	1680	1685	1690	1694	1695	1700	170.5
	92	64	32	29		5	22	72

444+75					1674.5	1675	1680	1685	1690	1695	1700	170.5
						3	21	58	85	140	152	163

444+0	1675	1680	1685	1690	1691.7	1695	1700	170.5
	101	65	31	7		24	51	79

443+50 Rocks in cluster and

443+00	1675	1680	1685	1690	1691.5	1695	1700	170.5
	111	79	30	14		36	62	83

442+50	1670	1675	1680	1683.0	1685	1690	1695	1700
	97	45	12		9	38	53	69

Earth and Rocks.



454+88	1675	1680	1683.3	1680	1685	1690	1695	1700	1705
	25			9	38	91	100	113	132

454+35	1675	1680	1683.1	1685	1690	1695	1700	1705
	33	13		8	25	40	60	98

453+50 Same as at Sta. 453+14.

453+14			1671.2	1675	1680	1685	1690	1695	1700	1705
				21	37	49	56	71	114	137

452+80 Practically the same  
as at Sta. 453+14.

452+37	1675	1680	1684.3	1685	1690	1695	1700	1705
	34	15		3	19	40	64	97

451+10 B			1686.7						
----------	--	--	--------	--	--	--	--	--	--

450+95 $\frac{1}{2}$ wash, small.			1675.5						
-----------------------------------	--	--	--------	--	--	--	--	--	--

450+80			1684						
--------	--	--	------	--	--	--	--	--	--

450+35 Bank of wash			1687.8						
---------------------	--	--	--------	--	--	--	--	--	--

461700	1675	1680	1685	1690	1694.0	1695	1700	1705
	50	45	30	18		4	17	35

459741			1675	1680	1682.6	1685	1690	1695	1700
			59	26		22	45	55	72

458786 <sup>90</sup>	1675	1680	1685	1690	1695	1698.9	1700	1705
	89	69	54	34	19		20	37

457783	1675	1680	1685	1690	1694.3	1695	1700	1705
	61	48	32	16		1	19	40

457728	± small wash				1688.3			
--------	--------------	--	--	--	--------	--	--	--

456750	1675	1680	1685	1690	1691.4	1695	1700	1705
	63	47	24	5		21	66	87

455750	1675	1680	1685	1690	1691.8	1695	1700	1705
	52	37	25	8		10	30	70

FATHS AND FEET.

Leach  
Bate  
Goodbody.

467+29 1675 1680 1685 1690 1697.7  
99 57 30 11

1695 1700 1705  
9 29 46

466+30 1675 1680 1685 1690 1695  
114 69 36 18

1700 1705  
26 45

Cultivated land

465+35 1675 1680 1685 1690 1692.2  
118 103 63 18

1695 1700 1705  
17 51 81

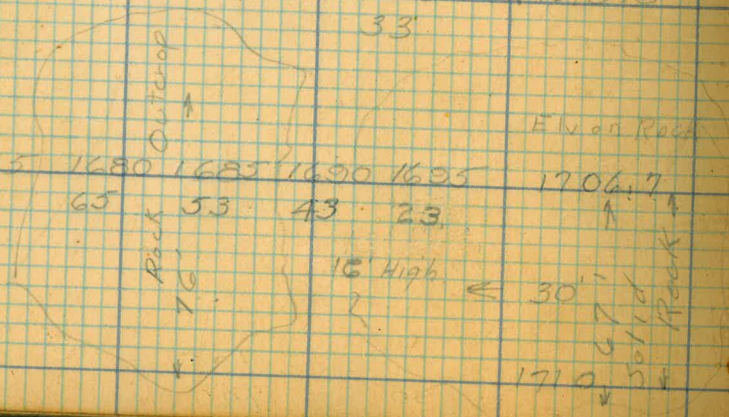
464+0 1675 1680 1685 1690.1  
Nov. 22, 1927 172 97 45

1695 1700 1705  
25 44 61

← 30 →  
Solid Rock  
shale

463+37 1675 1678.8  
33

1680 1685 1690 1695 1700 1705  
20 44 59 81 96 109



462+25 1675 1680 1685 1690 1695 1706.7  
73 65 53 43 23

1700 1705  
5 48

461+25 1710  
Solid Rock

FOLIATED ROCK

476+00	1680	1685	1690	1695	1698.7			
	96	50	29	13				

1700	1705	1710
8	25	45

472+50	1675	1680	1685	1690.1			
	220	149	68				

1695	1700	1705
65	121	146

472+10			1690		
	Small Wash in center of Large Wash.				

477+0			1675	1677.2			
			10				

1680	1685	1690	1695	1700	1705
14	65	91	181	Out	

471+0	1675	1680	1685	1687.9			
	89	52	33				

1690	1695	1700	1705
34	108	202	251

470+50	1675	1680	1680	1682.5			
	237	82	22				
	Field		82'	82'			
	300'						

1685	1690	1695	1700	1705
54	137	170	213	255

470+00 <sup>3</sup>	1675	1680	1685	1690	1690.5		
	216	140	70	6			

1695	1700	1705
36	71	112

1690 1695 1700 1705 1710  
 202 241 306 357 378

341  
39

486+0 1680 1685 1690 1695 1695.8  
 137 99 82  
 53  
 13.8

1695 1690 1685 1680 1685  
 15 52 142 159 184

485+0 Same as 483+50 1680.5

483+50 1680.3

1685 1690 1695 1700 1705 1710  
 53 82 150 210 274 297

482+0 1680 1685 1690 1694.0  
 82 53 25  
 57  
 8.8

1695 1700 1705 1710  
 6 31 59 90

480+0 1680 1685 1690 1691.8  
 84 47 15  
 64  
 8.0

1695 1700 1705 1710  
 26 58 70 85

478+32 1680 1685 1690 1691.7  
 95 54 10

1695 1700 1705 1710  
 27 54 67 80

477+0 1680 1685 1690 1690.8  
 113 57 10

1695 1700 1705 1710  
 30 47 52 65

Party Leach  
Bate  
Goodbody

218+57 1855 1860 1865 1870 1875 1878  
63 45 32 18 8

219+50 1855 1860 1865 1870 1875 1880 1880.9  
71 54 36 31 19 2

219+57.32 =  
495+59.32

1855 1860 1864.0  
E.W. D... 537 44 14

$$219+57.32 \times 0.2\% = 43.31$$

1930

Nov. 23, 1927

43.9

1892.1

Power Drop

453+0 1680 1685 1700 1705 1700 1705 1708.1  
135 125 123 101

1880 1885 1890 1895 1900 1905  
3 16 46 61 82 116

1885  
13

1880 1885 1890 1895 1900 1905  
117 157 170 191 288 290

1865 1870 1875  
14 48 63

1710  
40

Mesa Grande Rd. →

To Aldrich's Hidden Home →

210+09.  
210+32. Intersection  
210+44. Edge of Road.

213+62  
Bank. ↗  
1855 1860 1862.1  
16 3° 1859.4

1865 1870 1875 1880 1885  
7° 22 41 67 84

214+34  
44' from  
B.C. on Semi Tan.  
1855 1860 1865 1865.6  
25 14 1°

1870 1875 1880 1885  
17 0 35 58 81

215+22.  
(32' For. from  
PT. on Semi Tan.)  
No curve  
1855 1860 1865 1867.1  
54 21 9

1870 1875 1880 1885  
12 39 52 80

216+05  
1855 1860 1863.5  
39 14

1865 1870 1875 1880 1885  
5 25 57 69 92

216+67  
1847.8

1855 1860 1865 1870 1875 1880 1885  
31 56 67 106 119-158 171 201

217+73  
1855 1860 1865 1868.4  
49 21 13

1870 1875 1880 1885  
6 27 57 82

204+25	1855	1860	1865	1870	1874.6	1875	1880	1885	Edge of Rd.
	63	49	37	25		1 <sup>e</sup>	28 <sup>e</sup>	68	80

204+53<sup>19</sup>

Bank of large wash ↗

1868.7

206+27

Bank of large wash ↗

1861.2

Earth & Rock

206+50

1855  
33

1860  
6

1861.9

1865  
9

1870  
35

1875  
79

1880  
110

1885  
131

207+12

1842.6

1845  
5

1850  
13

1855  
27

1860  
44

1865  
56

1870

1875

1880

1885

208+00

1855  
32

1860  
27

1865  
17

1868.8

1870  
8

1875  
38

1880  
64

1885  
86

209+25

↳ abandoned Rd.



1855  
65

197+50

1850  
42

1865  
26

1870  
16

1875  
2

1875.7

1880  
12

1885  
22

198+50

1855  
33

1860  
19

1865  
6

1868.2

1870  
7

1875  
31

1880  
56

1885  
73

198+80

± Wash

1848

1871.2

199+15

1855  
23

1860  
17

1865  
9

1870  
12

1870.7

1875  
10

1880  
29

1885  
49

Hops back

199+50

± Wash

1855.A

200+00

64 F.C.

1855  
80

1860  
67

1865  
59

1870  
32

1875  
6

1876.9

1880  
12

1885  
45

Earth + Rock

201+50

1855  
64

1860  
54

1865  
39

1870  
24

1875  
8

1877.2

1880  
12

1885  
29

202+50

1855  
40

1860  
28

1865  
15

1870  
3

1871.0

1875  
10

1880  
24

1885  
33

203+50

1855  
65

1860  
54

1865  
39

1870  
26

1875  
11

1878.7

1880  
8

1885  
22

Edge of Rd  
47

192+71

1854.5

Earth and Rock

1855 1860 1865 1870 1875 1880 1885  
1 16 31 44 54 64 74

193+78

1855 1860 1865 1870 1872.5  
53 47 27 6

1875 1880 1885  
12 29 40

194+0

1855 1860 1865 1870 1874.7  
51 37 30 20

1875 1880 1885  
1 16 33

194+83

1865.1

1855

82



195+37

1860 1865 1870 1875 1880 1881.3  
71 61 43 23 5

Decomposed Granite

1885  
19

196+25

1855 1860 1865 1866.8  
24 15 3

1870 1875 1880 1885  
6 19 32 45

196+85

Small wash

1859.2

Nov. 25, 1927

Leach  
Gate  
Good body

18940	1855	1860	1863.1	1865	1870	1875	1880	1885
	49	25		13	36	46	54	62

189450	1855	1860	1865	1870	1874.8	1875	1880	1885
	61	44	25	11		1	15	32

189490	Same as 189450			1874.8				
--------	----------------	--	--	--------	--	--	--	--

190418	Small Draw			1864.2				
--------	------------	--	--	--------	--	--	--	--

Hogs Back

190450	1855	1860	1865	1869.0	1870	1875	1880	1885
	39	27	16		3	13	25	37

190467	Small Draw			1863.7				
--------	------------	--	--	--------	--	--	--	--

191450	1855	1860	1865	1870	1875	1879.8	1880	1885
	62	55	47	40	24		1	20

1855

30



19240	1860	1865	1870	1875	1876.3	1880	1885
	64	30	17	4		11	29

Earth & Scattered Rock

184+0

Solid  
1860 1861.0  
5  
2.5  
Solid

Rock  
1865 1870 1875 1880 1885 1890 Road  
6 16 24 37 50 61 63  
Rock

184+50

Solid Rock RT  $\frac{1}{2}$

185+00

1860

1865

1870

1875.0

21

17

10

1880

1885

1890

10

19

27

186+0

2nd Bank Wash

See Level notes

186+22<sup>x</sup>

1860

1862.5

1865

1870

1875

1880

1885

1890

Road

8

4

15

30

49

58

71

75

186+40

1st Bank Wash

186+75

1860

1865

1870

1873.0

1875

1880

1885

1890

31

21

6

8

22

35

55

187+91

1860

1865

1870

1875

1877.7

1880

1885

1890

26

17

13

6

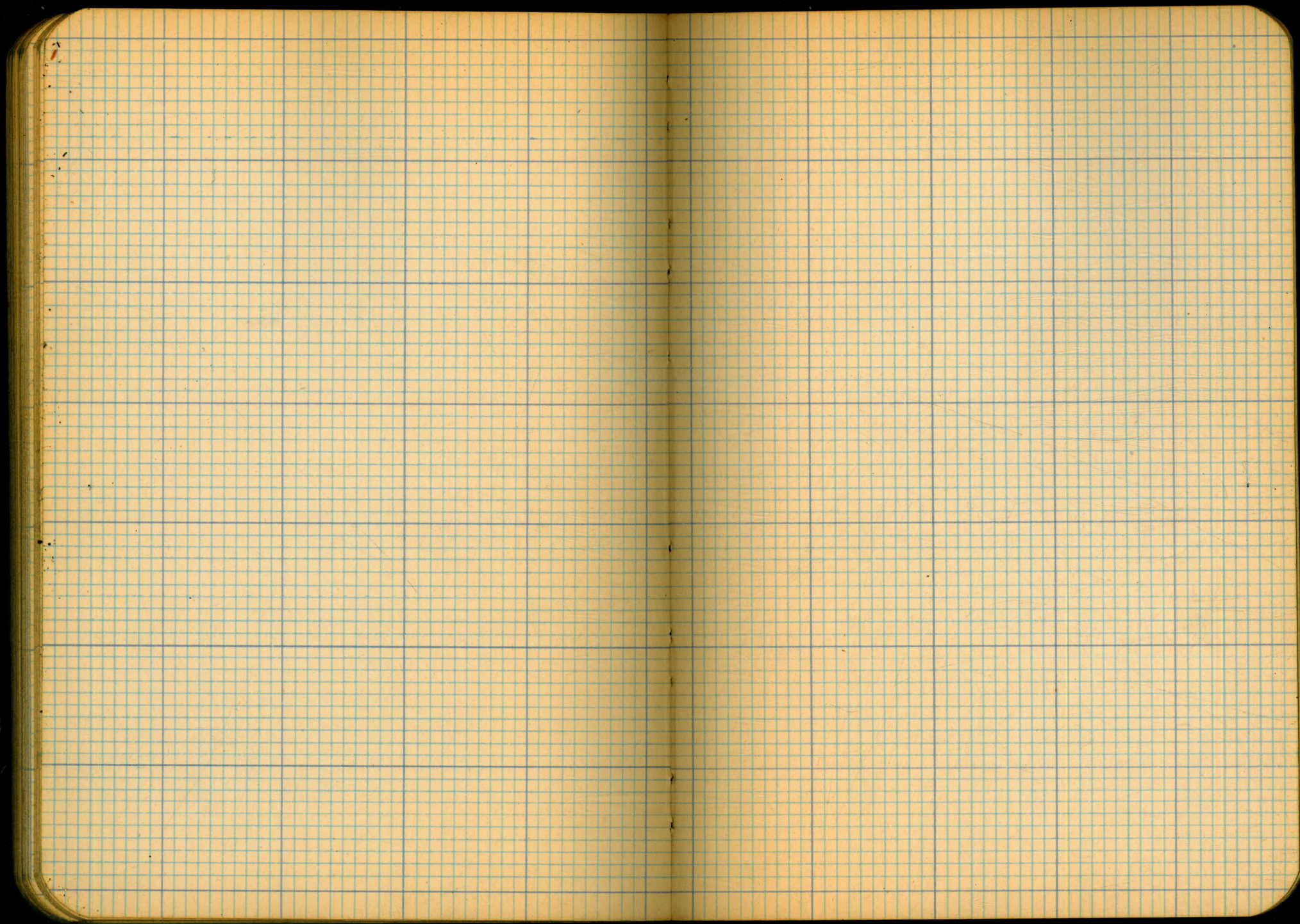
17

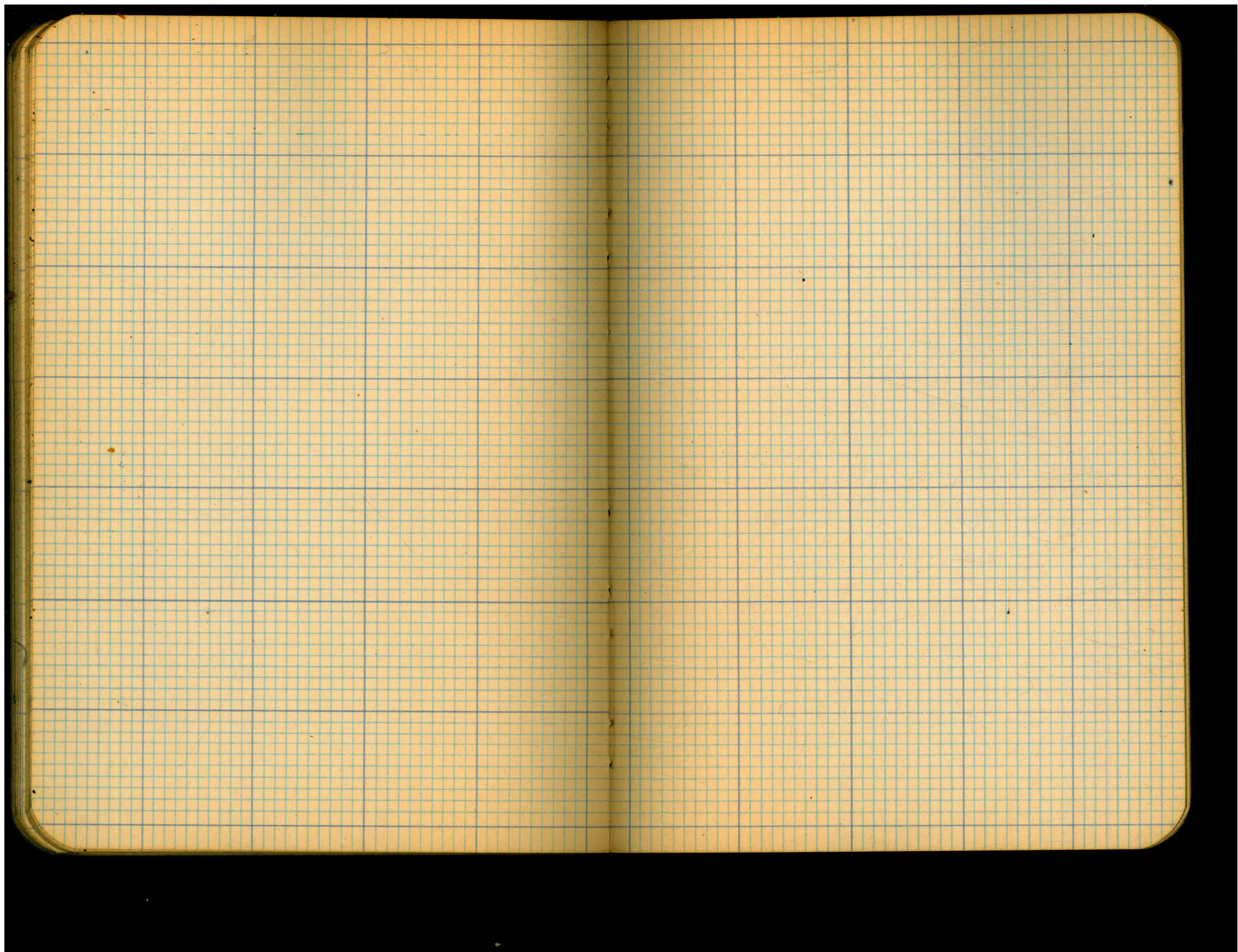
29

41

Earth + Rock

46' Solid Rock → 15' High  
135' Rock





DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in

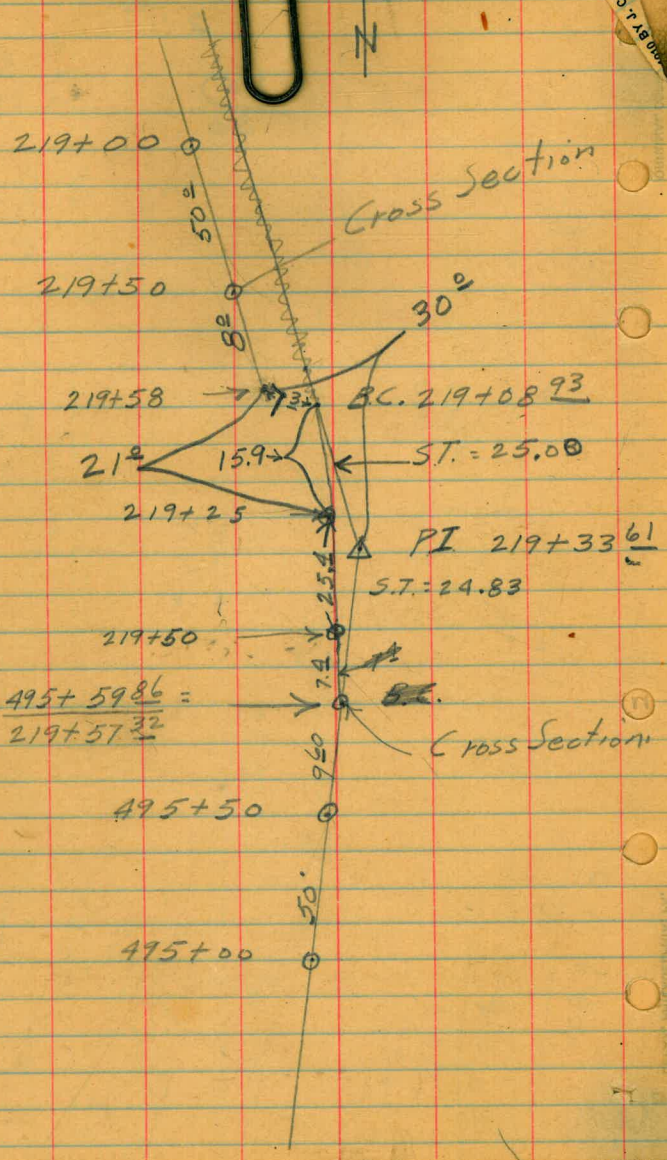
---

IMPROVED TABLES  
AND  
INFORMATION

---

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given  $I$  may be found by dividing tangent (or external), opposite  $I$  by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



$$\frac{495 + 5986}{219 + 5732} =$$

1972 50 18 20 95 10 120  
 3 5 4 9 3  
 5 3 7  
 211,573  
 420

485

144  
2 8 8  
16 11 14  
5 27  
732 0 9

97.6 93.7  
124  
169.4  
25

44  
16  
48130  
0.5

218  
2  
144  
19  
1306  
27 144  
5 27.46  
7.8 218  
2

558  
55

10 58 250  
1907

59 3  
4163  
8 8 415+00  
1852.5  
1688.6  
1883.6  
16,868  
18819  
176.5

16577 436  
1937  
1873

1862.2  
78.9  
1994.6  
10 6  
18,648  
18,678  
170  
172  
3 0 4 8  
5 3  
5 0 7,501  
20  
8825

219  
177  
4240  
0061

7.16 81  
4 3  
015861

24.00



10° 01' 50"

17687

17663

25

25  
30


TRADE MARK

ORIGINAL COPY

LEFAX, PHILADELPHIA, PA.

42

1652.0  
1988 10  
35.4 3.5

730  
445  
4200  
8.4  
146+00  
26 00

2.8.5  
7 3  
10.1 3  
1649.3  
19 00

1645.2  
5.3  
1639.4  
27  
5.2  
287  
2  
5.24  
66  
28  
3.8

John  
7.5  
3.7  
11.2

7.5  
3.7  
11.2  
7.8  
7.8  
11.6

5.6  
3.8  
7.4  
211.57  
42.91  
495  
59.86  
1699.1  
99.12  
197.2  
763.150  
93

193C.  
43.9  
7892.419  
5.5  
43.9 12

193C.  
43.9  
7892.419  
5.5  
43.9 12

144  
2  
28.8  
19.14  
5.5  
733

97.692.7  
169.5  
10 56  
256  
1907.

558  
55  
59.3  
472  
55  
1850.5  
1688.6

18.14  
9.3  
52.7  
1883.6  
16.868

1862.12  
78.9  
46.  
1894.6  
10.6

1862.12  
78.9  
46.  
1894.6  
10.6

53.8  
6.5  
7.64  
172  
1671.7

170  
18.64  
10.6  
170  
18.64  
10.6

219  
177  
42400  
8A.00  
1906.

1891.7  
45  
19850  
015861

218

144  
19

1306

27 144

27.46

218

436

1937

1893

219

52

0.2 1.8

1.20

0.076

661

219

1891.7

45

19850

015861