Survey of the

El Monte Ranch Road

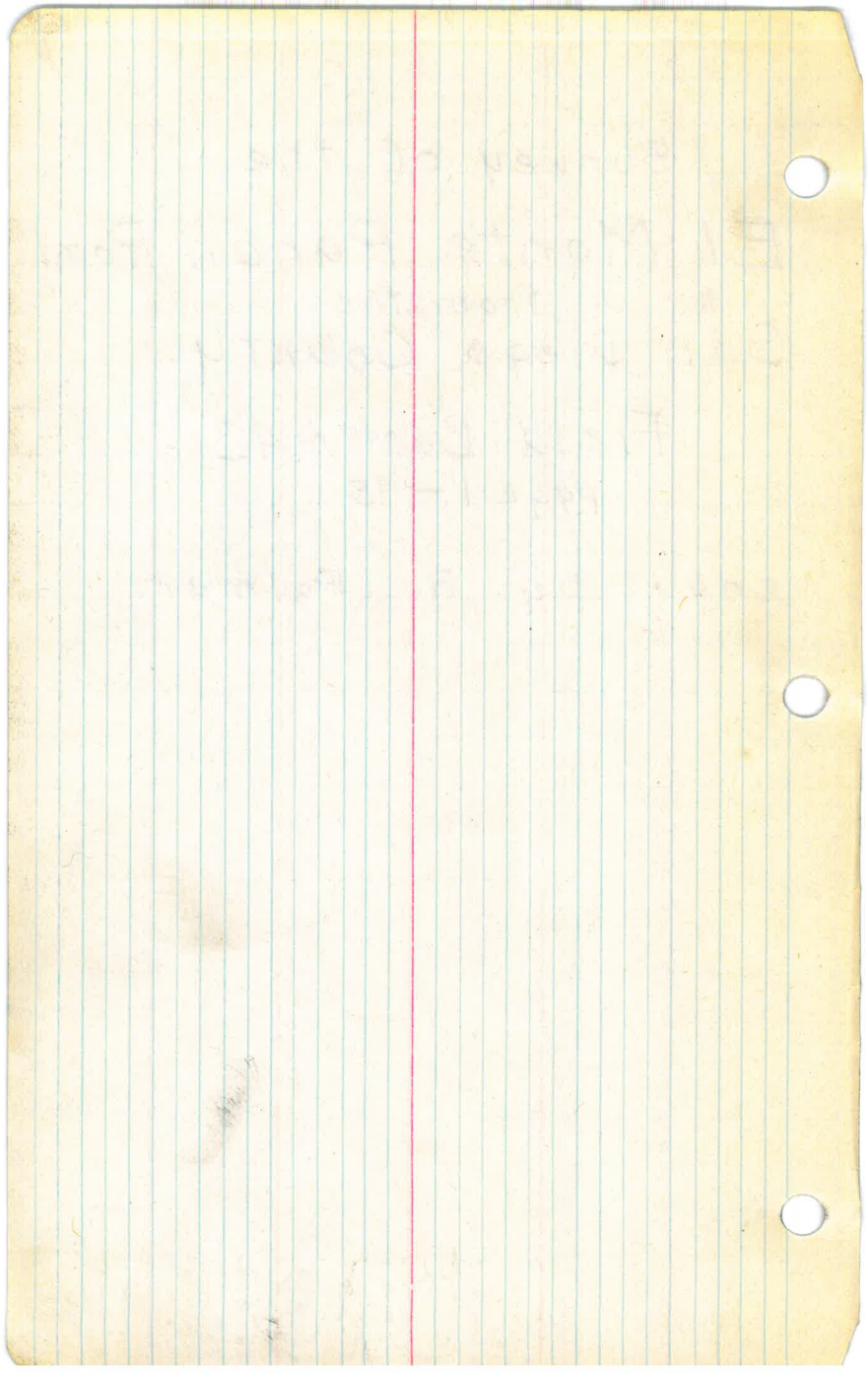
from the

San Diego County

Field Book #43

page 1 – 13

copy by R.C. Palmer



9/17/13

Survey of El Monte Ranch Road

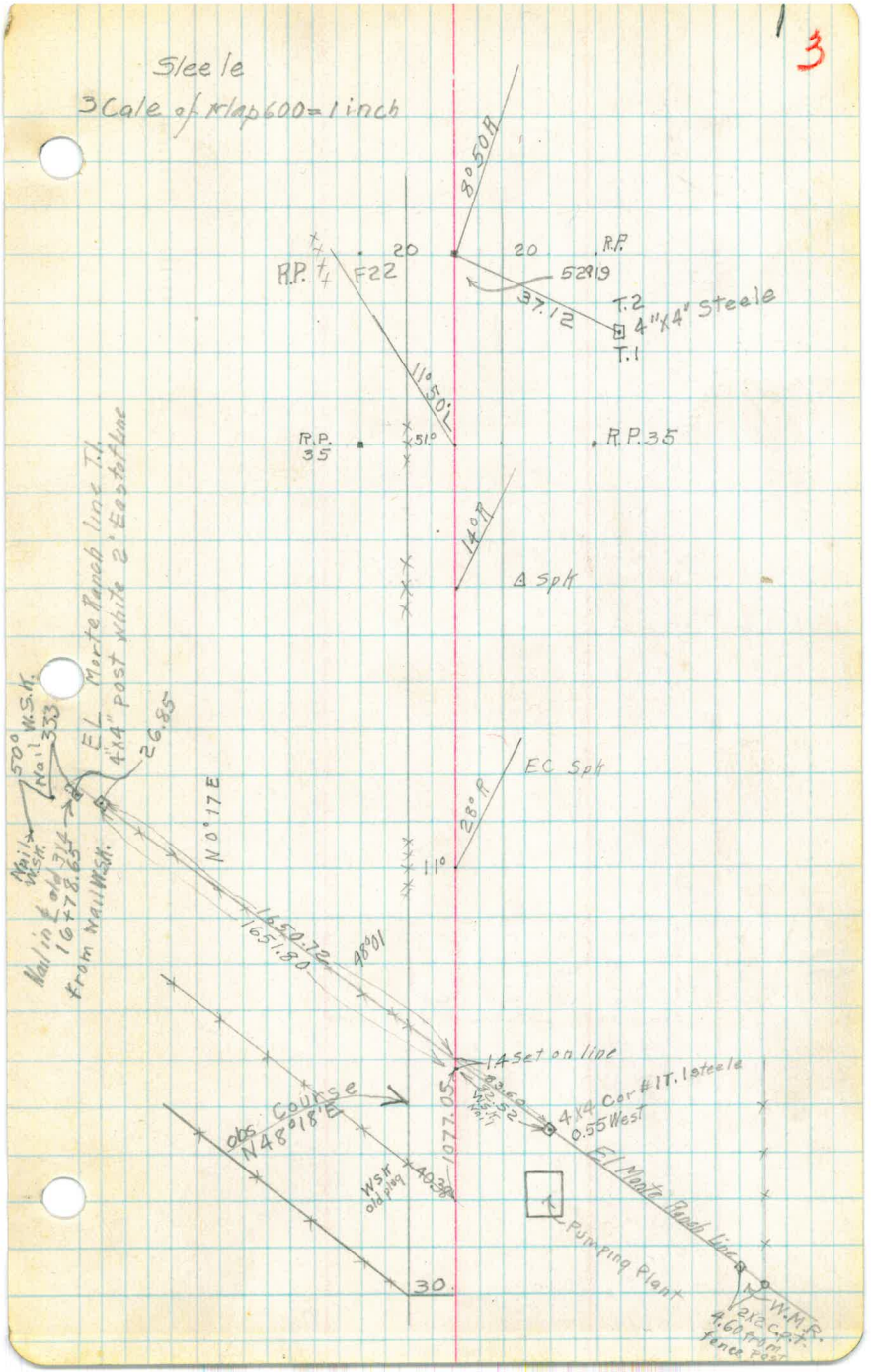
Watson
Williams
Bates

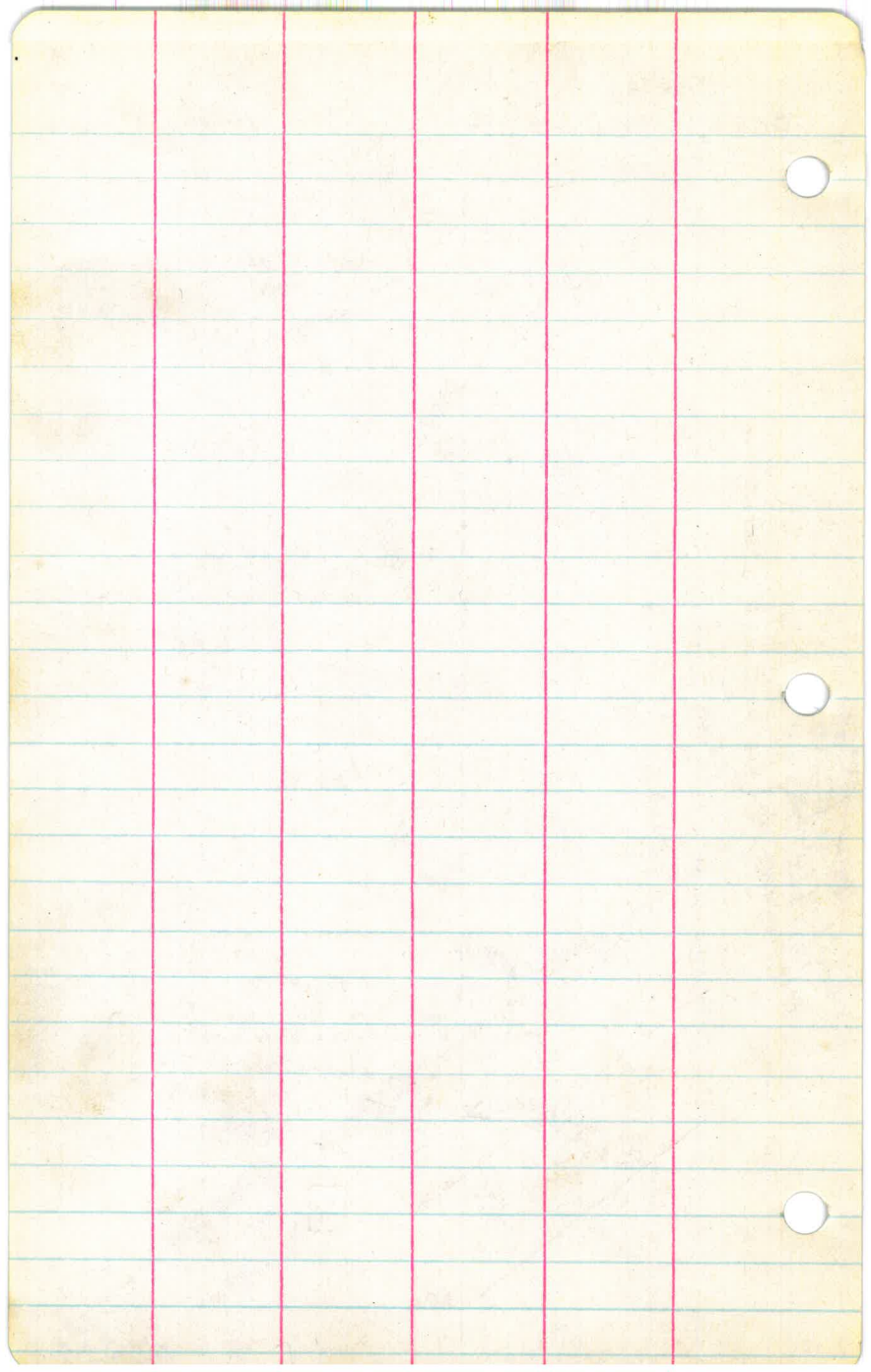
		Curve			
9+67.2	Δ		8°50R	N87°18E	308.6
6+17.0	Δ		11°50'L	N78°28E	350.2
3+07.1	Δ		14°R	S89°42E	309.9
1+59.9	E.C.				
1+12.10	P.I.	R=200 T=49.9 L=97.7 E=6.1	28°R	N76°18'E	197.1
0+62.2	B.C.				
0+00				N48°18E	112.10

All reference points from 6+17.00 to 47+95.2 inclusive are 0.10 less than noted

Steele

Scale of Map 600 = 1 inch





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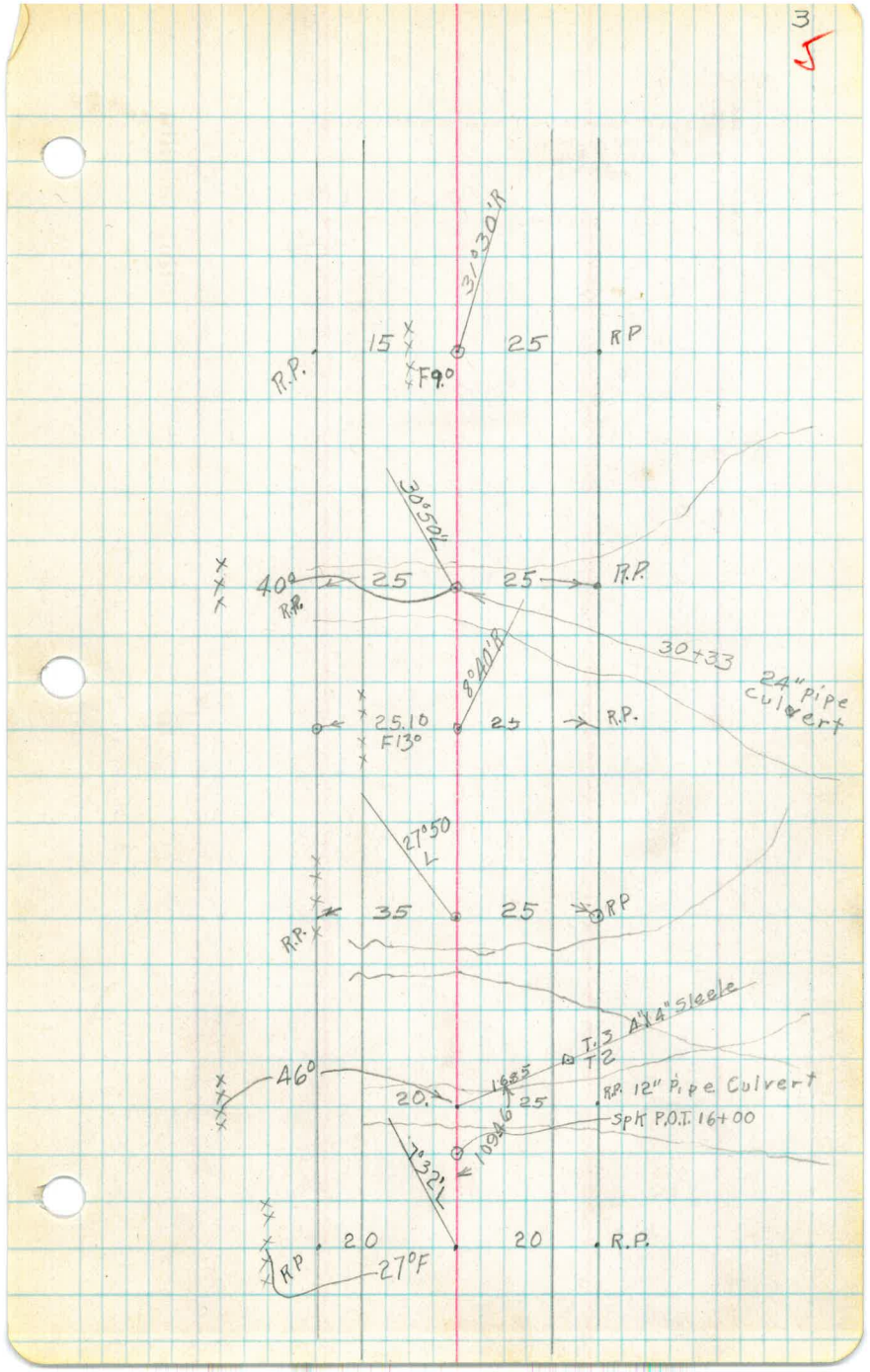
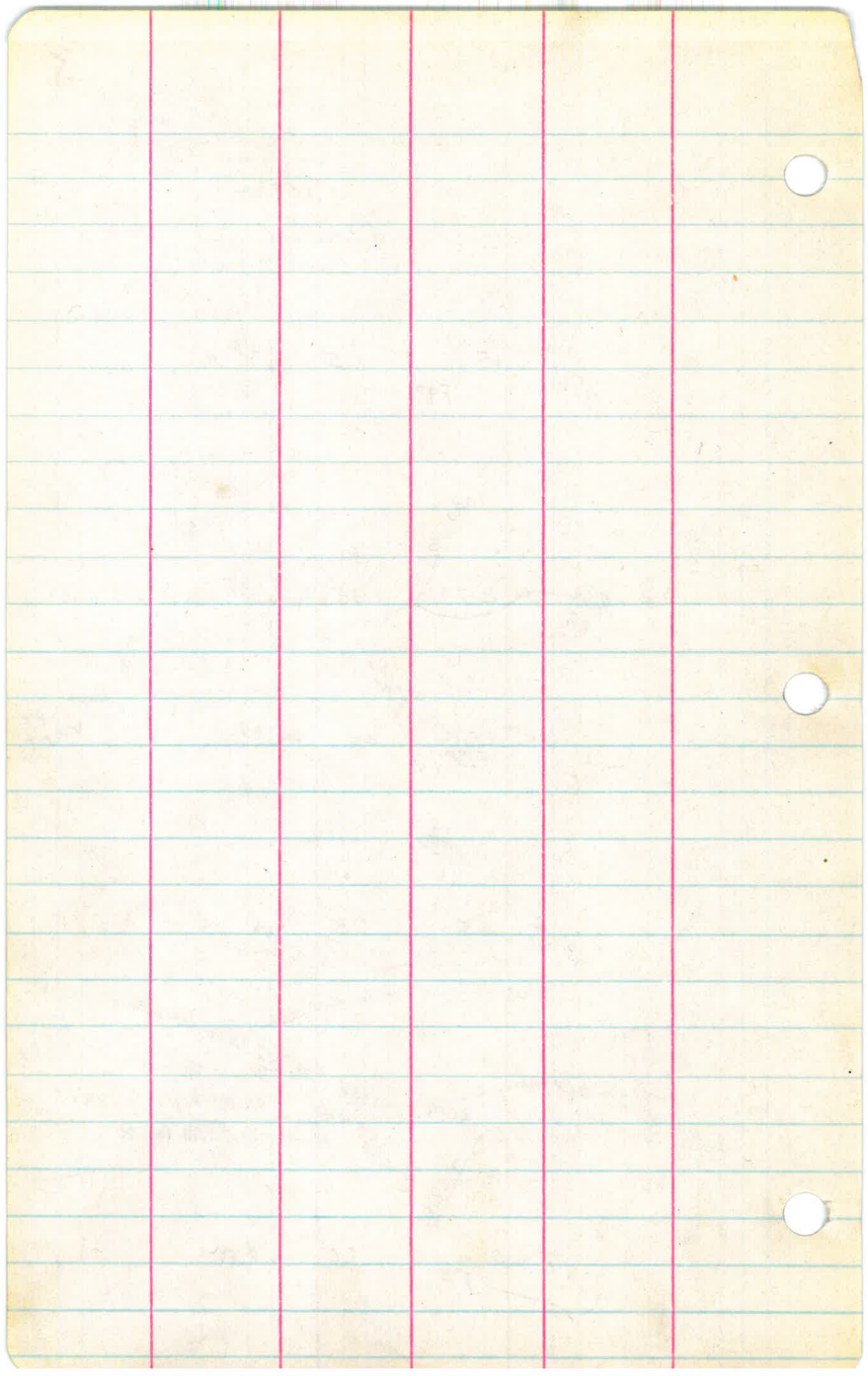
Survey of El Monte Ranch Road

Sta		Curve	Δ	Course	
33+95.05	EC				
		R = 200 T = 56.4 L = 109.95 E = 7.8	31°30R	N52°E	332.8
33+05.5	P.I				
32+49.10	B.C.				
31+96sp+	P.O.T.				
30+85.45	E.C.				
30+33	P.I.	R = 200 T = 55.13 L = 107.60 E = 7.46	30°50L	N20°30E	275.2
29+77.85	BC				
26+66.6	A		8°40R	N51°20E	366.4
21+16.5	EC				
20+21.3	P.I.	R = 400 T = 99.10 L = 194.3 E = 12.10	27°50'L	N42°40E	649.2
19+22.2	B.C.				
17+47.9	A		9°16'L	N70°30E	273.4
15+98	P.O.T.				
12+75.8	A		7°32L	N79°46E	472.1


31°30'R
R.P.
15
F9°
25
RP
30°50'L
40°
R.P.
25
25
R.P.
8°40'R
30+33
24" Pipe Culvert
25.10
F13°
25
R.P.
27°50
L
R.P.
35
25
RP
T.S
T.S
A 4" Steele
46°
20.
25
R.P. 12" Pipe Culvert
Spk P.O.T. 16+00
7°32'L
RP
20
20
R.P.
27°F



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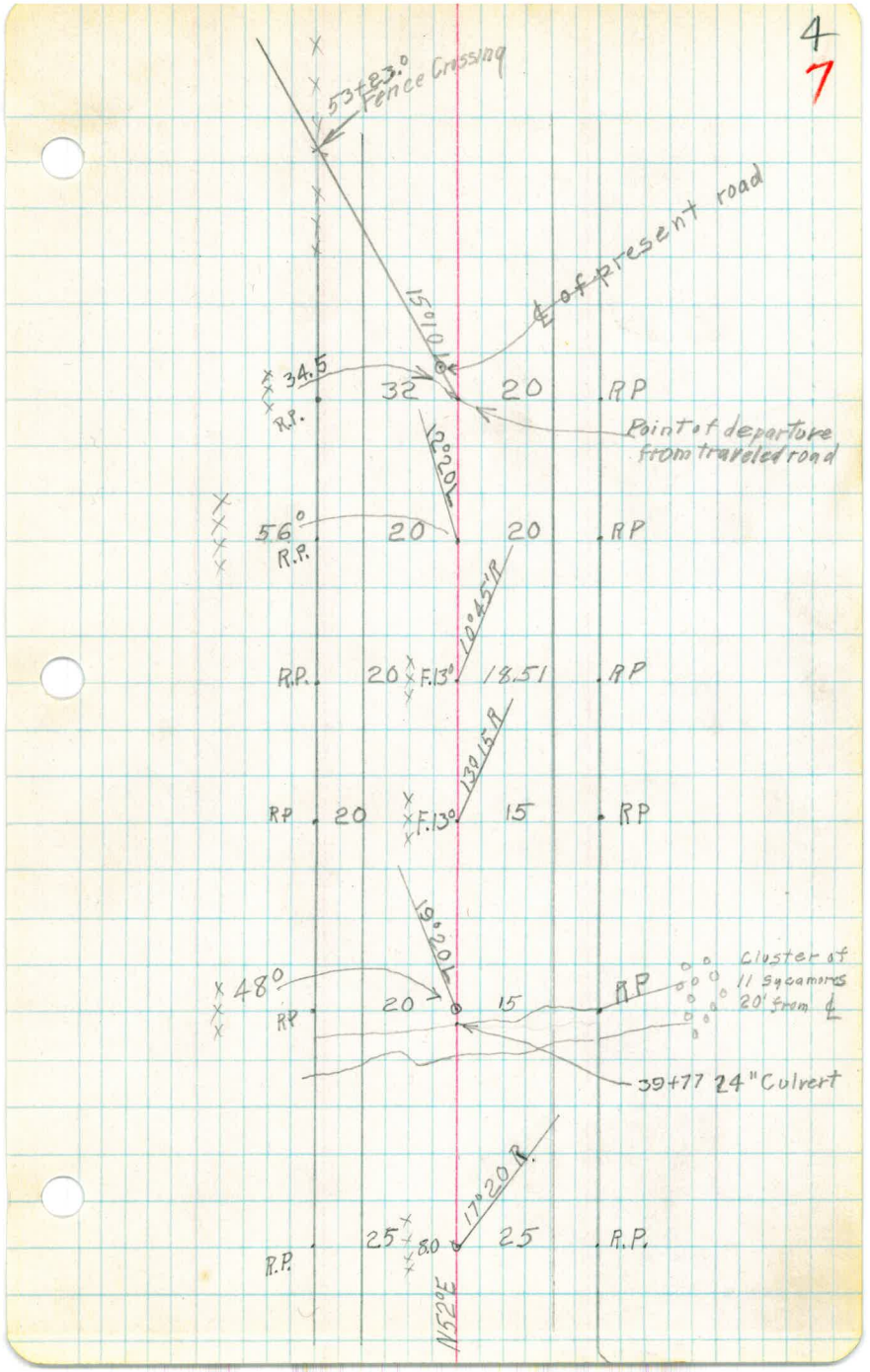
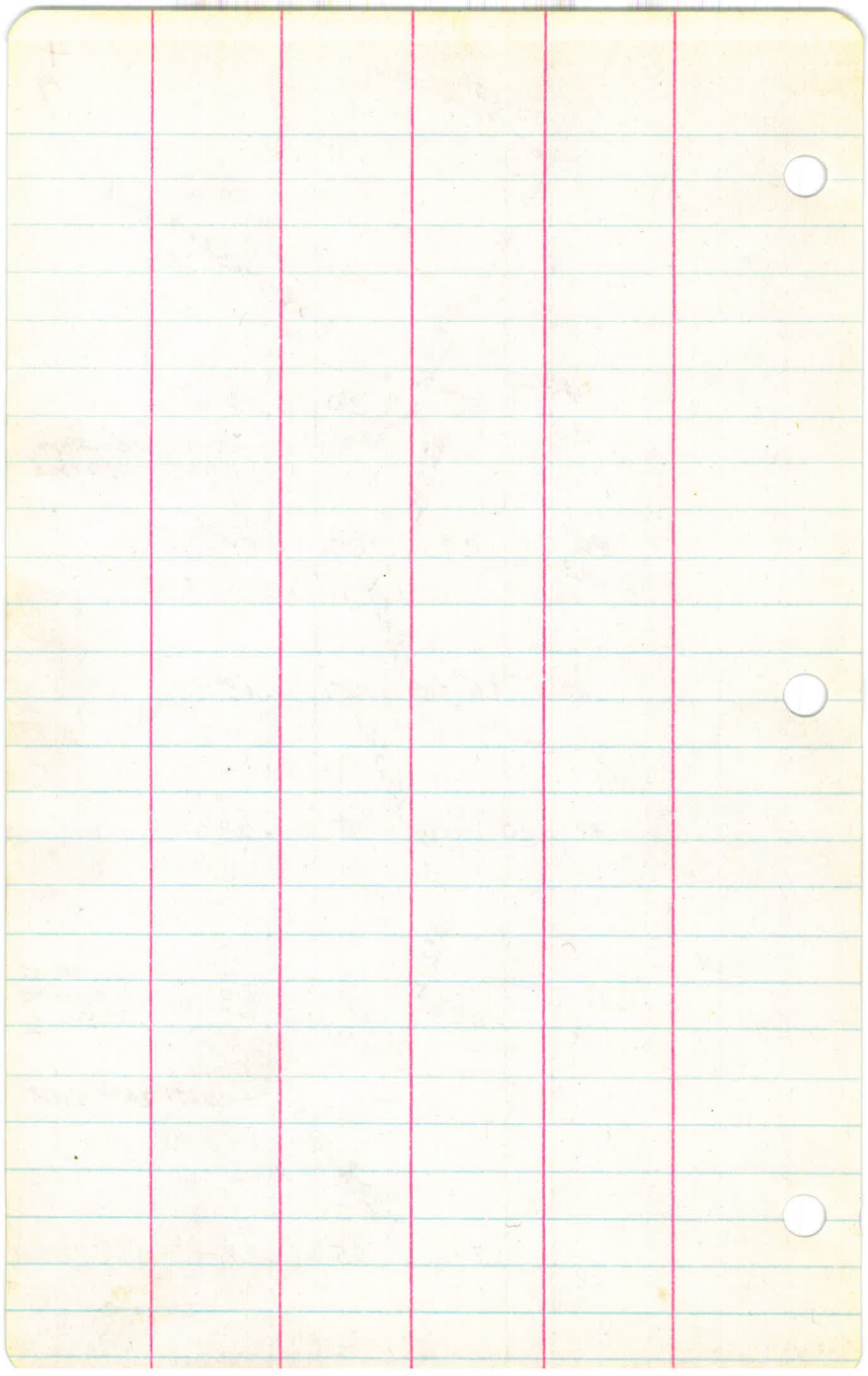
Survey of El Monte Ranch Road

Sta		Curve	Δ	Coarse	
52+81.15	E.C				
52+15.4	P.I.	R=500 T=66.57 L=132.35 E=4.41	15°10L	N46°30E	1028.42
51+48.8	B.C.				
47+95.2	Δ		12°20L	N61°40E	420.2
45+22.2	Δ		10°45'R	N74°E	273.°
42+53.7	Δ		13°15R	N63°15E	observed N63°15E course
40+10.84	EC				
39+44	P.I.	R=400 T=68.13 L=134.97 E=5.68	19°20L	N50°E	311.0
38+75.87	B.C.				
36+95.45	EC				
36+35.45	P.I.	R=400 T=68.97 L=121.00 E=4.62	17°20R	N69°20E	309.52
35+74.45	BC				


53+83.0
Fence Crossing
℄ of present road
15°10' R
34.5
32
20
RP
R.P.
Point of departure from traveled road
12°20' L
56°
20
20
RP
R.P.
40°45' R
R.P.
20
F.13°
18.51
RP
39°15' R
RP
20
F.13°
15
RP
19°20' L
48°
RP
20
15
RP
Cluster of 11 Sycamores 20' from ℄
39+77 24" Culvert
17°20' R.
25
80
25
R.P.
R.P.
N 52° E



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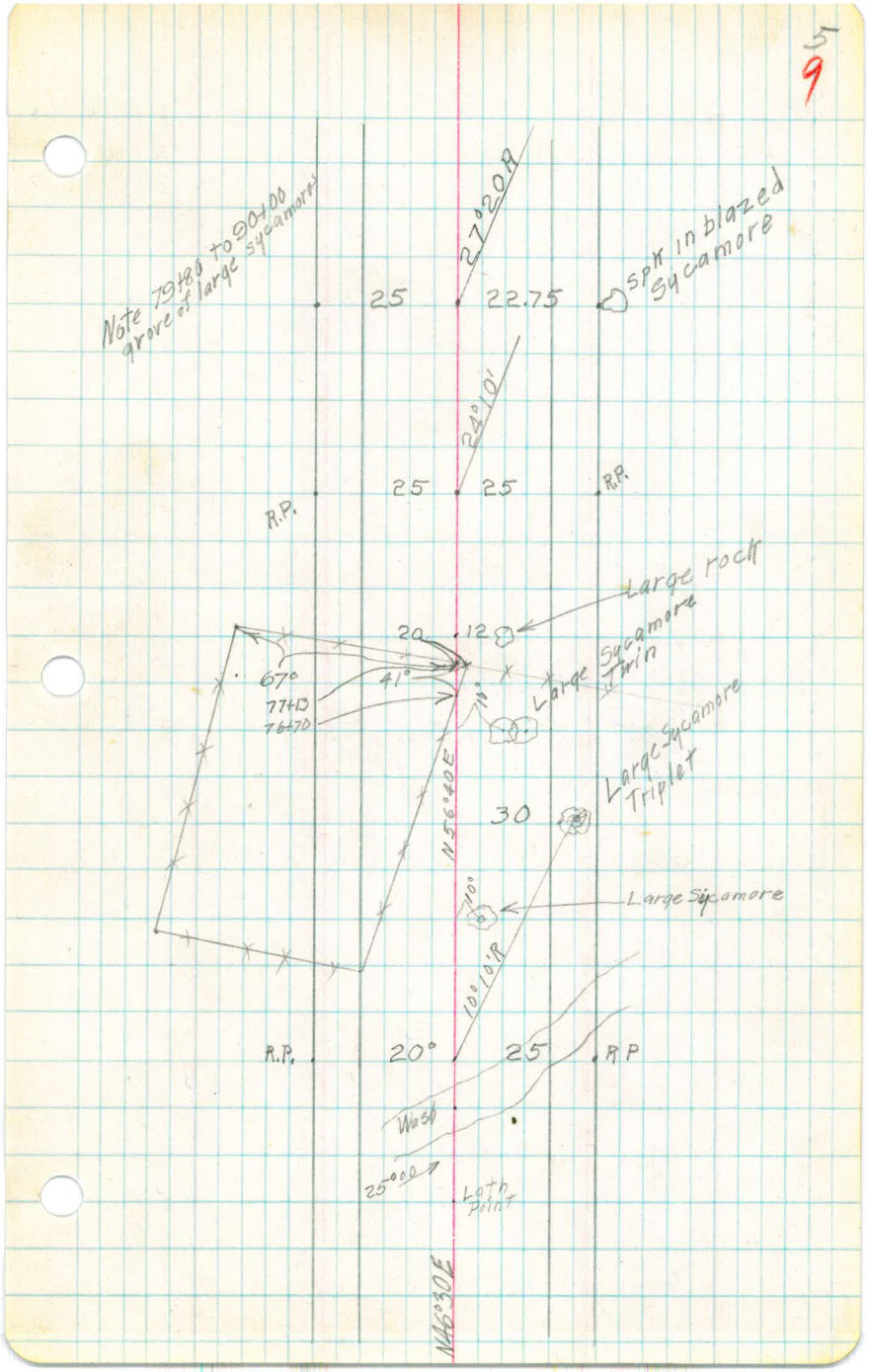
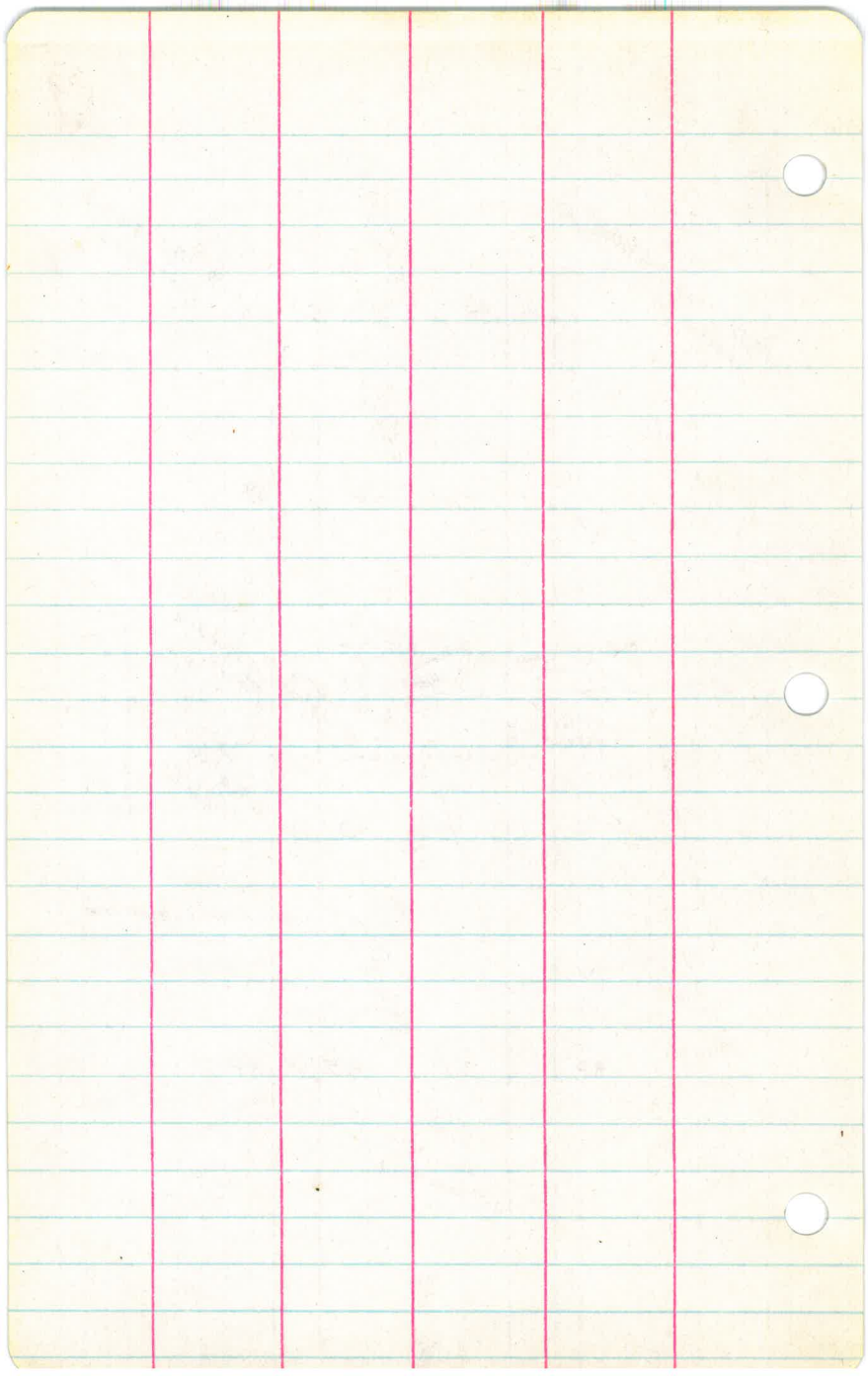
Survey of El Monte Ranch Road

Sta		Curve	A	Course	
85+49.17	E.C.				
84+79	P.I.	R = 300 T = 72.95 L = 143.12 E = 8.74	27°20 R	S71°50E	625.5
84+06.5	B.C.				
80+63.08	E.C.				
79+80	P.I.	R = 400 T = 85.63 L = 168.71 E = 9.06	24°10R	N80°50E	501.55
78+94.37	B.C.				
77+75					
76+00	POT				
71+21					
65+64					
63+67					
62+43	A		10°10'R	N56°40E	1737.°
61+75	24" Culvert				
60+00	P.O.T.				


Note 79+80 to 90+00 grove of large sycamores
25
22.75
Spk in blazed Sycamore
27°20R
24°10'
25
25
R.P.
R.P.
Large rock
20
12
Large Sycamore Twin
67°
41°
77+13
76+70
11°
Large Sycamore Triplet
30
N 15°40E
10°
Large Sycamore
10°10'R
R.P.
20°
25
R.P
Wash
25°00
Lgth Point
N 63°30E



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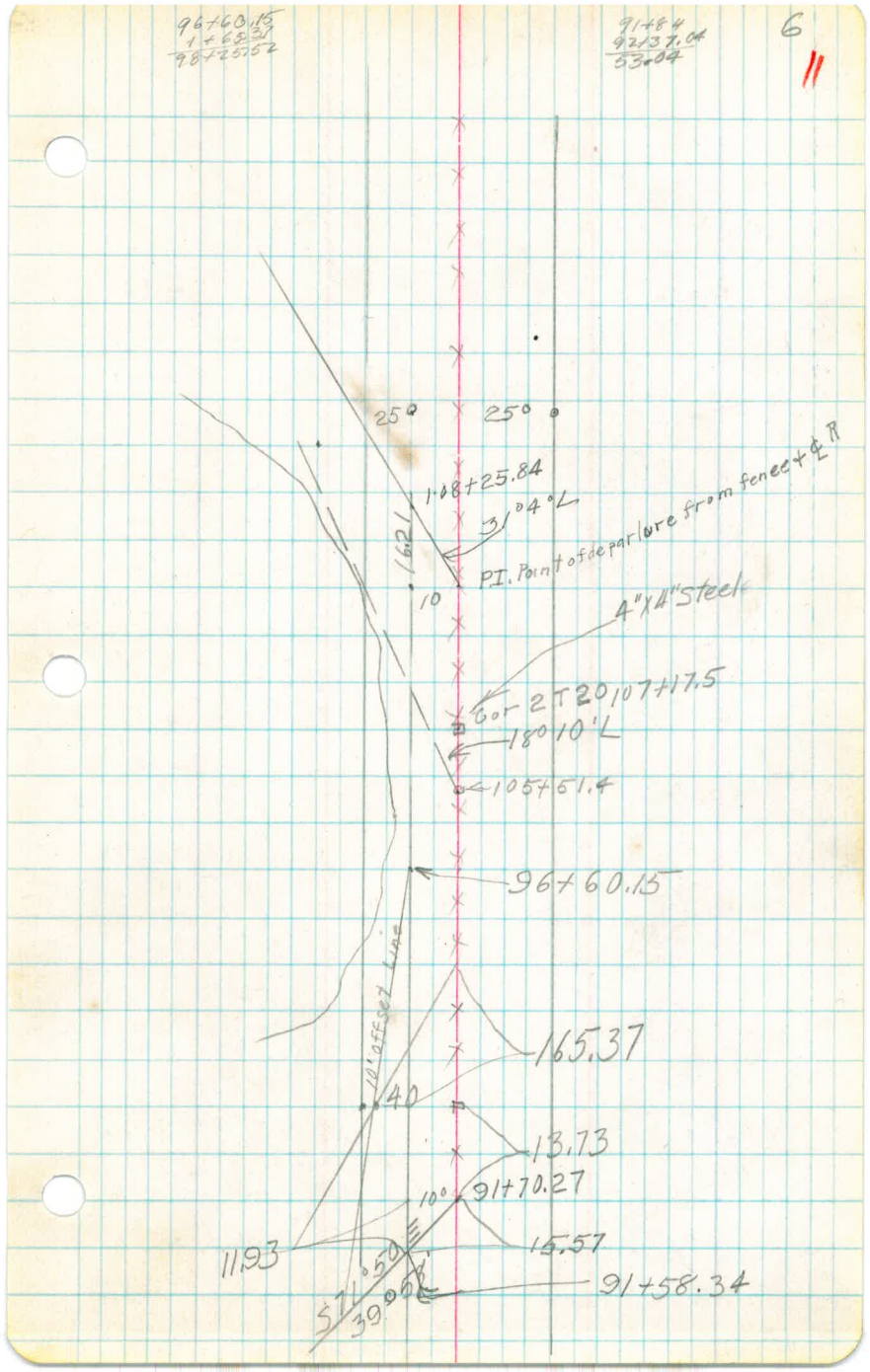
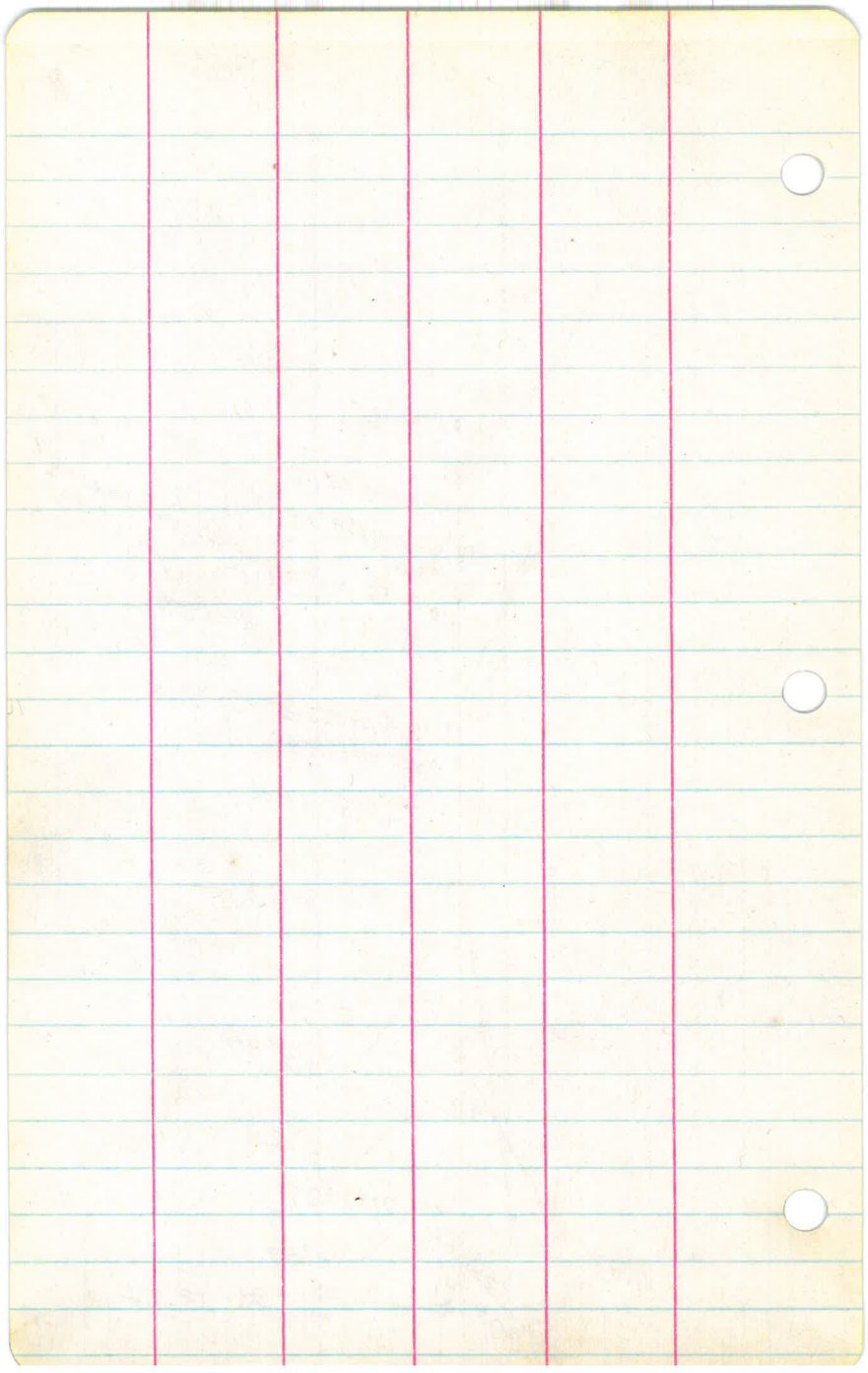
Survey of El Monte Ranch Road

115+20	#1 P.O.T.			
110+12.77	EC #2	=110+44.48 #1		
109+49.9	=PI #2	R=400 T=63.96 L=126.83 E=5.08	18°10L	N36°32E
109+96.51	Line #1			
108+85.94	BC			
			13°30L	N54°42E
105+93	Δ 10' offset Line	=105+94.18 ℄	13°30L	
105+51.4	Δ ℄ Road			
98+25.52	Δ ℄ Road			
96+60.15	Δ 10' offset Left		3°28L	N68°12E
91+63.17	EC			
91+01.72	PI	R=200 T=65.95 L=127.46 E=10.60	36°30L	71°48E
90+35.77				

See page #12


96+60.15
1+65.37
98+25.52
91+84
92+37.04
53.04
6
11
25°
25°
1+88+25.84
3°04' L
162'
P.I. Point of departure from fence ℄ R
10
4"X4" Steel
60' 2T20 107+17.5
180 10' L
105+61.4
96+60.15
165.37
40
13.73
10°
91+70.27
15.57
91+58.34
1193
51°50'
39°00'
10' Offset Line



9/25/13 Survey of El Monte Ranch Road

147+17.85 #1 = A
146+86.14 #2 — 2°00R N63°12'E 982.15

140+36.15 #1 = A
140+04.44 #2 — 16°10R N61°12'E 681.70

139+00 #1 P.O.T.

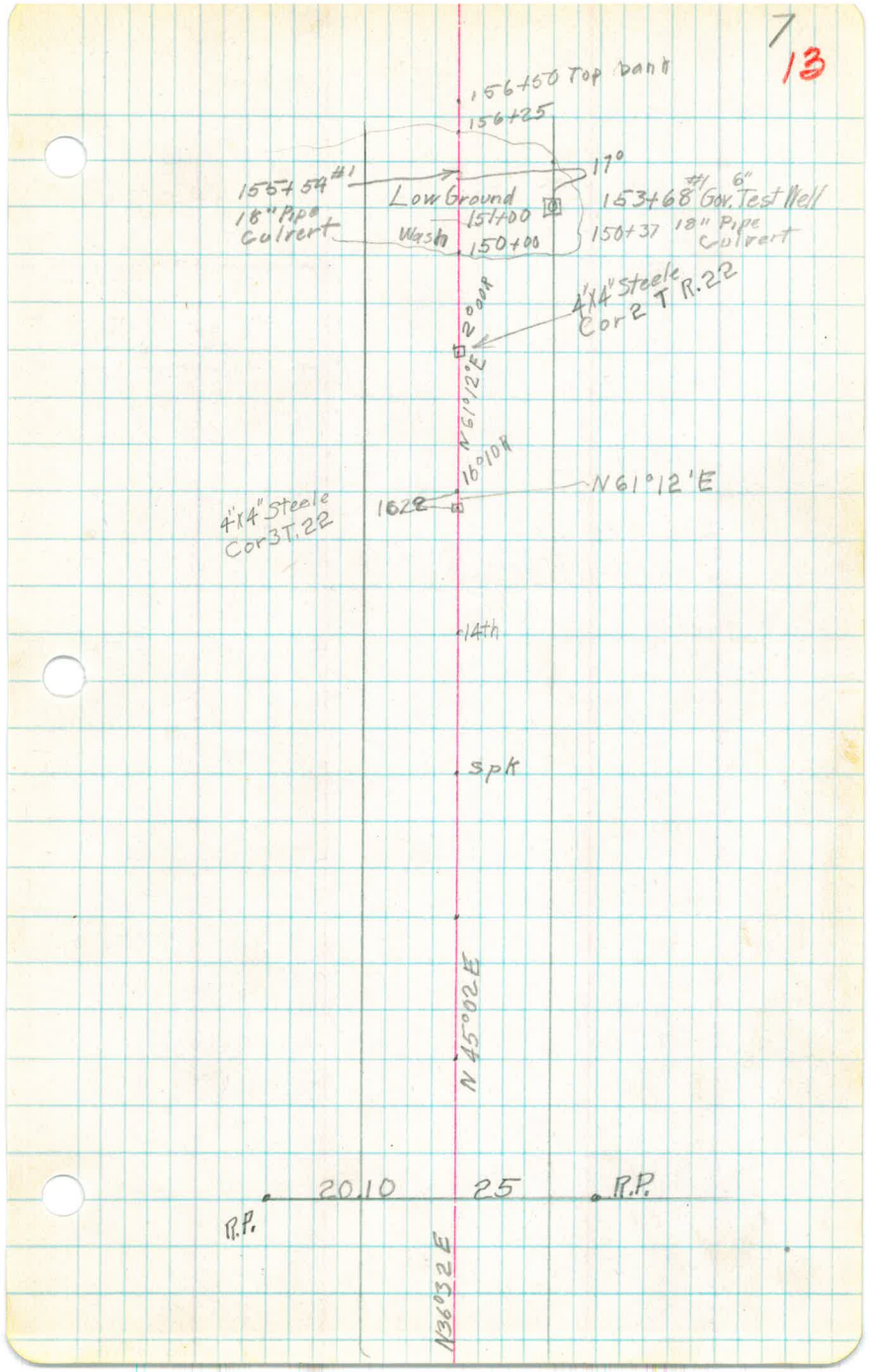
134+00 P.O.T.

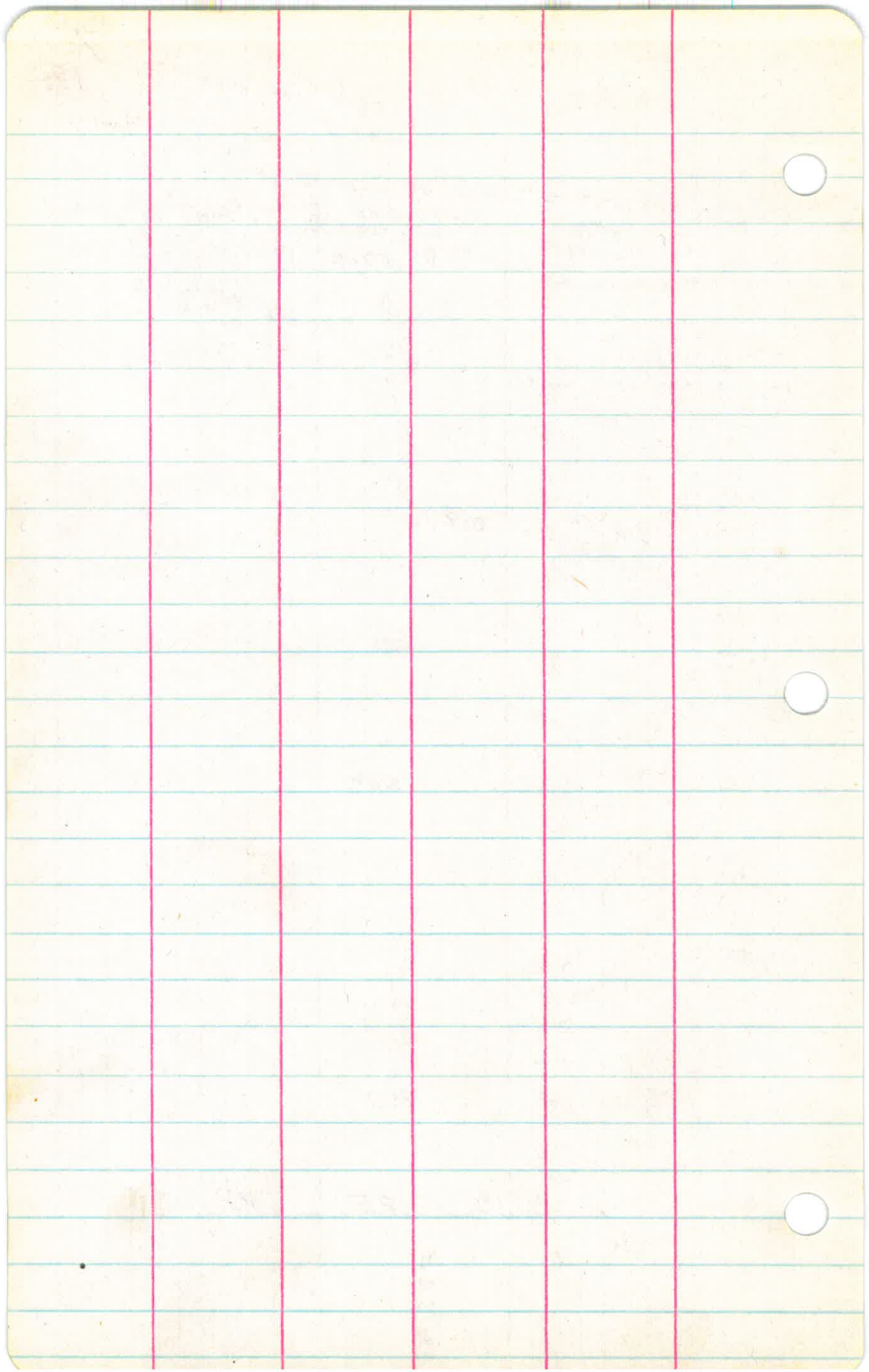
138+00 #1 P.O.T.

125+00 #1 P.O.T.

119+78.41 #1 = A
119+46.29 #2 — 8°30R N45°02'E 2058.15

7
13


156+50 Top bank
156+25
17°
155+54 #1
18" Pipe Culvert
Low Ground
Wash
151+00
150+00
153+68 #1 6" Gov. Test Well
150+37 18" Pipe Culvert
4"x4" Steele Cor 2 T R.22
200ft
N 61° 12' E
160ft
N 61° 12' E
4"x4" Steele Cor 3T. 22
1628
14th
spk
N 45° 02 E
20 10 25
R.P.
R.P.
N 36° 32 E



Survey of El Monte Ranch Rd

178+60 #2 P.O.T.

174+54.36 #2 EC

174+20 #1
173+88.29 #2 P.I. R=200 T=71.81 L=137.88 E=12.5 39°30R N83°42E 987.45

173+16.48 B.C.

170+71.29 #2 P.O.T.

168 #1 P.O.T.

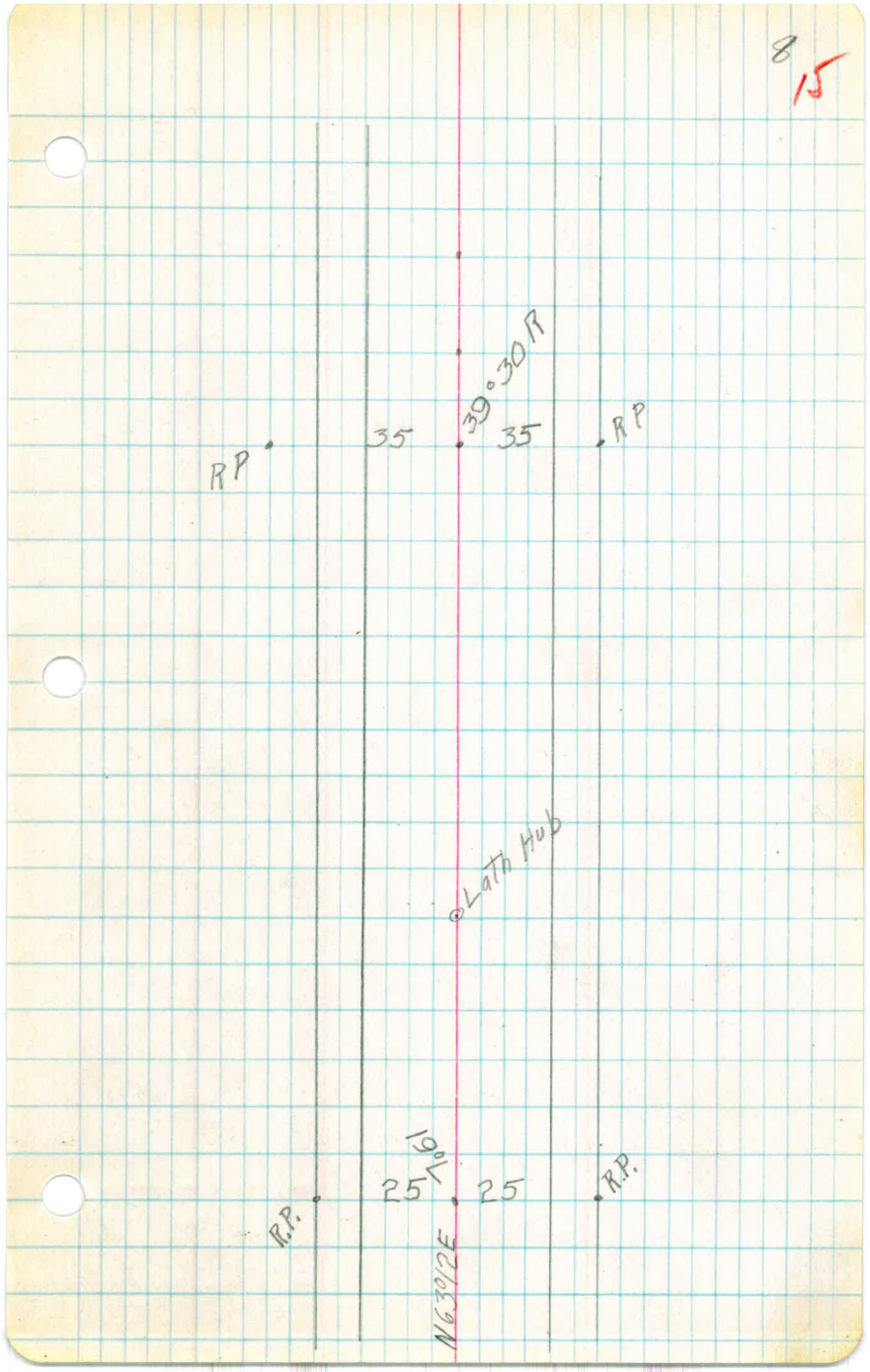
164 #1 P.O.T.

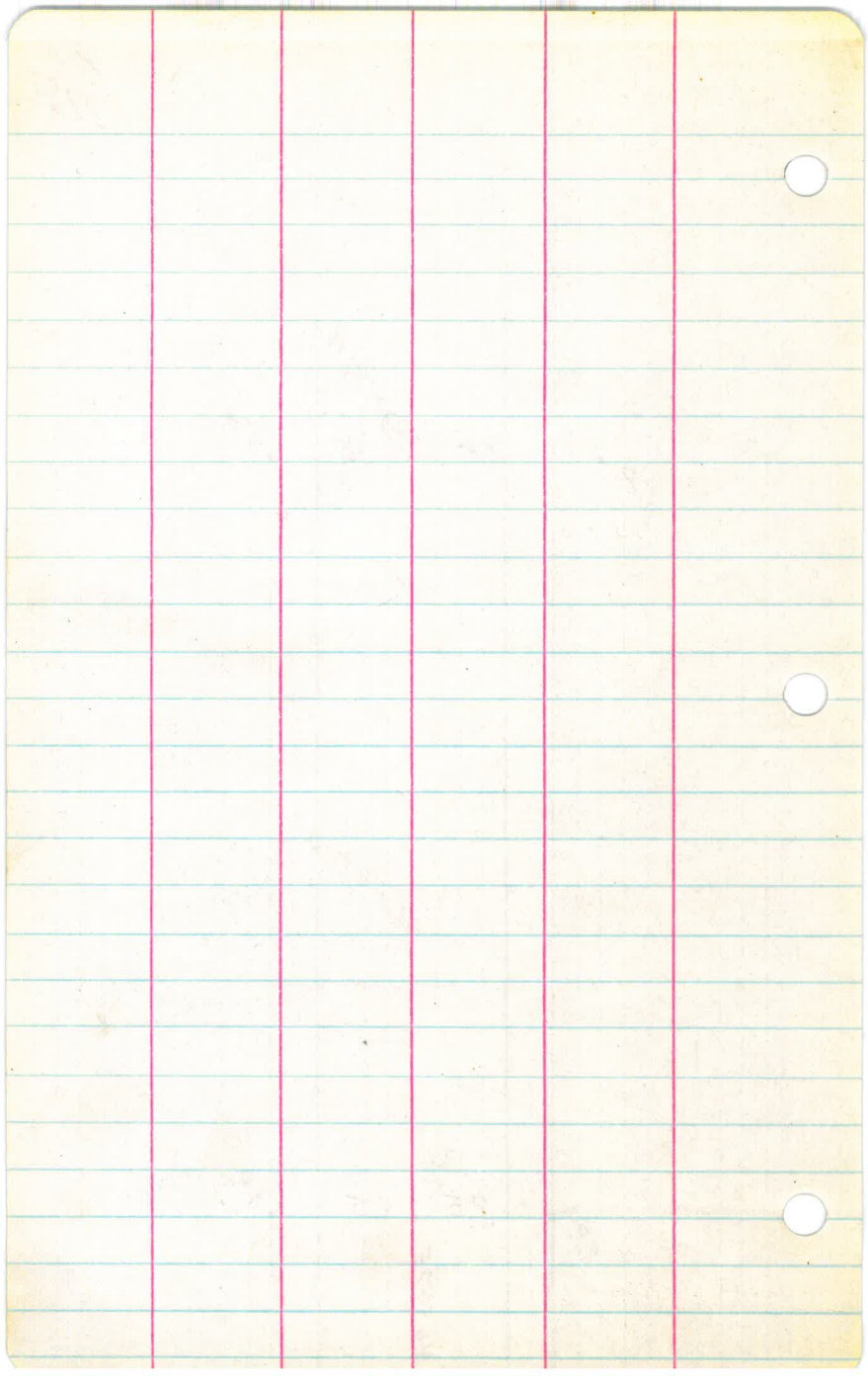
157+34.00 #2 E.C.

157+00 #1 = P.I. R=400 T=66.94 L=132.65 E=5.56 19°00L N44°12E 1721.23
156+68.29 #2

156+33.06 #1 B.C.

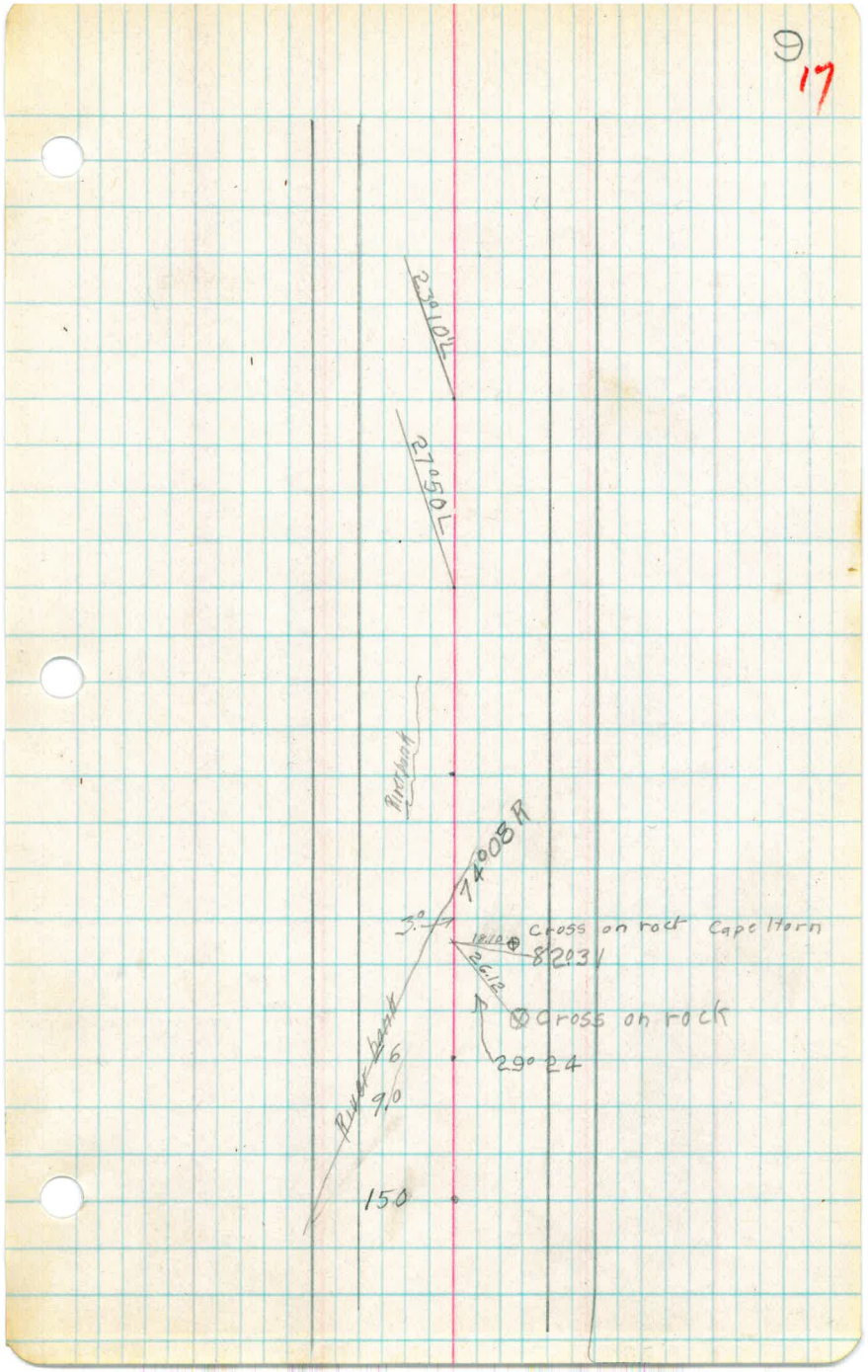
156+01.35 #2

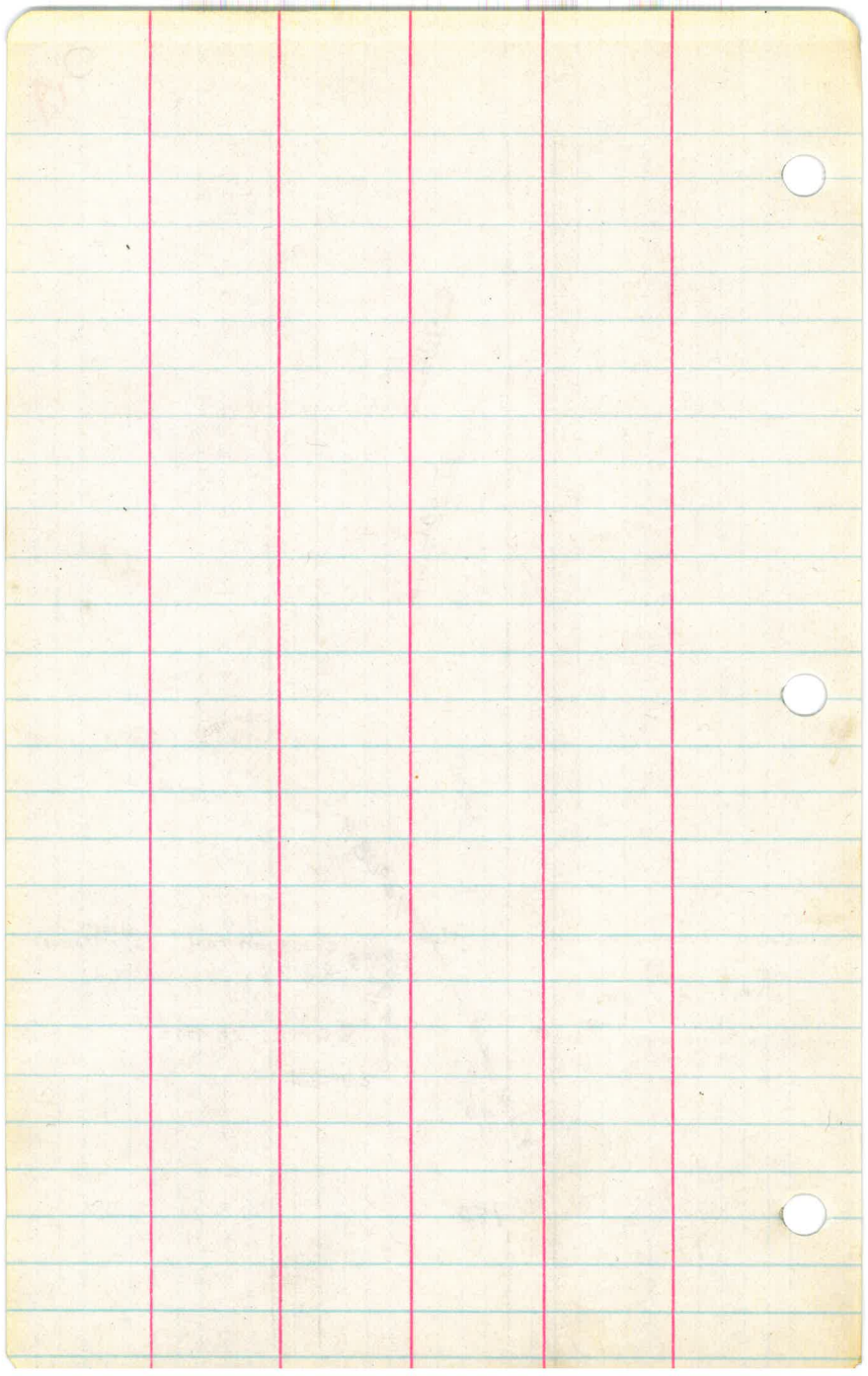

39°30'R
RP
35
35
RP
@Lath Hub
19°
25
25
R.P.
R.P.
N63°12'E



Survey of El Monte Ranch Road

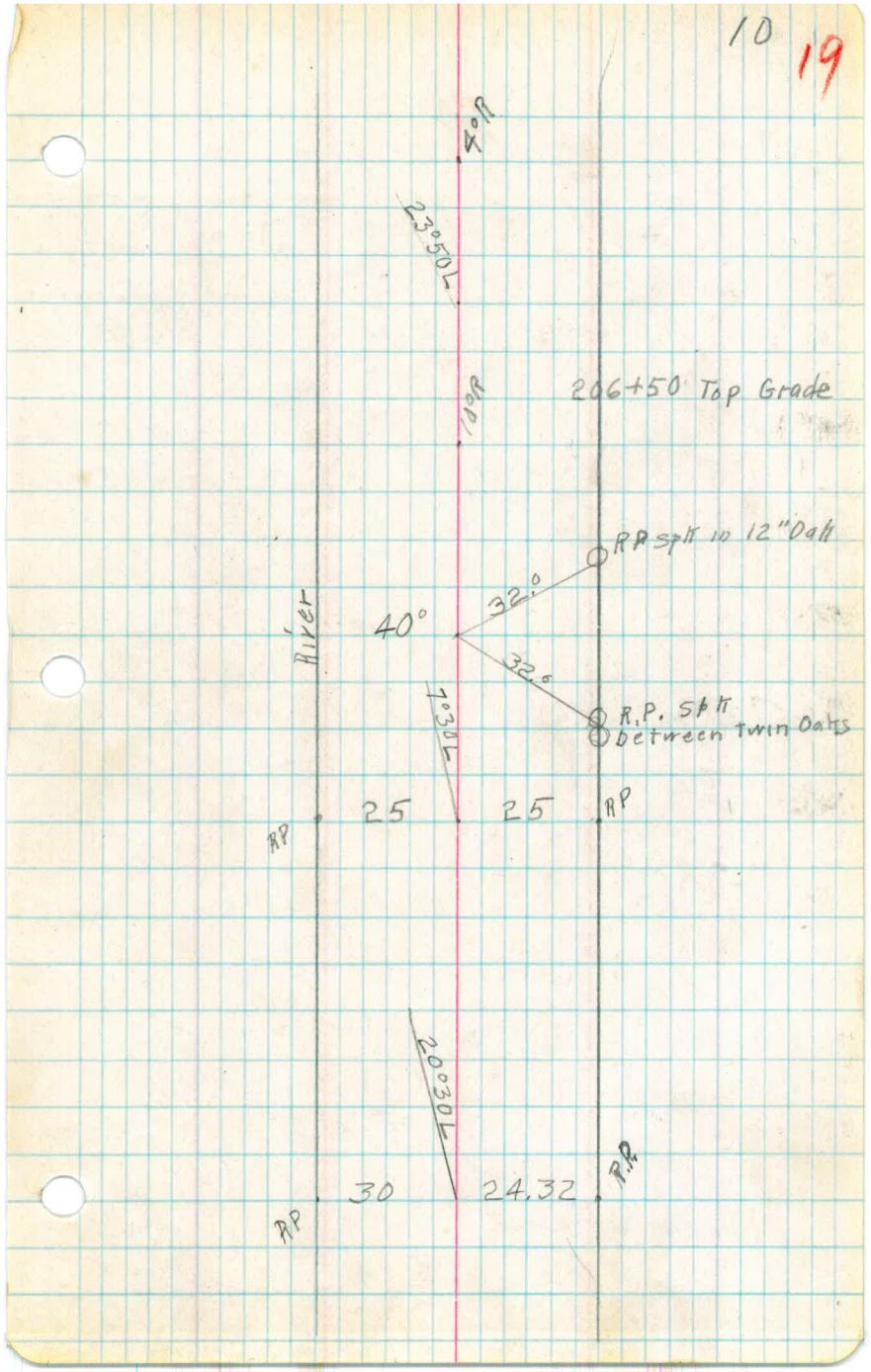
192+73.87 #2	EC				
192+34.0	P.I.	R=200 T=41.00 L=80.87 E=	23°10'L	S61°10E	113.37
191+39.8	EC				
190+68.4	P.I.	R=300 T=74.33 L=145.23	27°50L	S38°00E	168.53
189.94.07	B.C.				
187+31.17	E.C.				
186+93.48	P.I.	R=700 T=52.88 L=90.57 E=1.73	74°08'R	S10°10'E	390.11
186+40.60	BC				
186+00					
183+70	A		12°00R	S84°18E	323.48

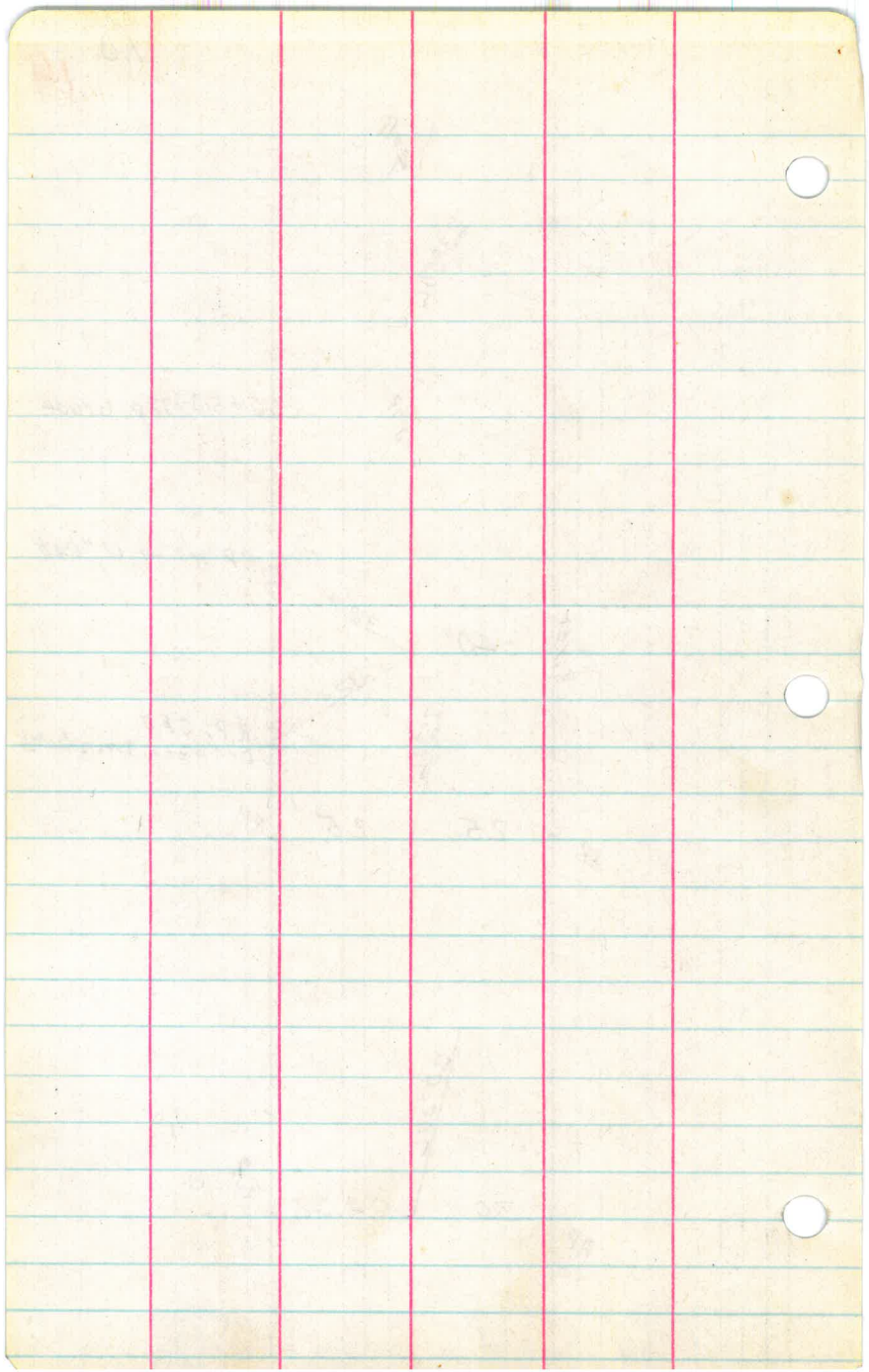

239°10'L
270°50'L
Riverbank
74°00'R
3°
Cross on rock Cape Horn
8'203'
Cross on rock
290°24
River bank
9.0
150



Survey of El Monte Ranch Road

210+77.76	#2 A	Eq 0.18.2 ft	4°00R	S62°50E	591.31
208+28.91	E.C.				
207+67.43	#2 P.I.	R=300 T=63.31 L=124.79 E=7.79	23°50L	S66°50E	312.16
207+04.12	B.C.				
206+28.88	#2 Watsons hand Level line A=21568		10°00R	S43°00E	138.55
202+96.16	#2 E.C.				
202+28.88	#2 P.I.	R=300 T=69.72 L=137.00 E=8.0	26°10R	S53°00E	402.44
201+59.16	#2 BC				
199+75.43	#2 A		7°30L	S79°10E	253.45
198+14.28	#2 =20750 Watsons hand level line				
198+07.18	#2 A		10°00R	S71°40E	168.25
194+01.33	#2 E.C.				
193+46.24	#2 P.I.	R=300 T=52.25 L=107.34 E=	20°30L	S81°40E	458.10

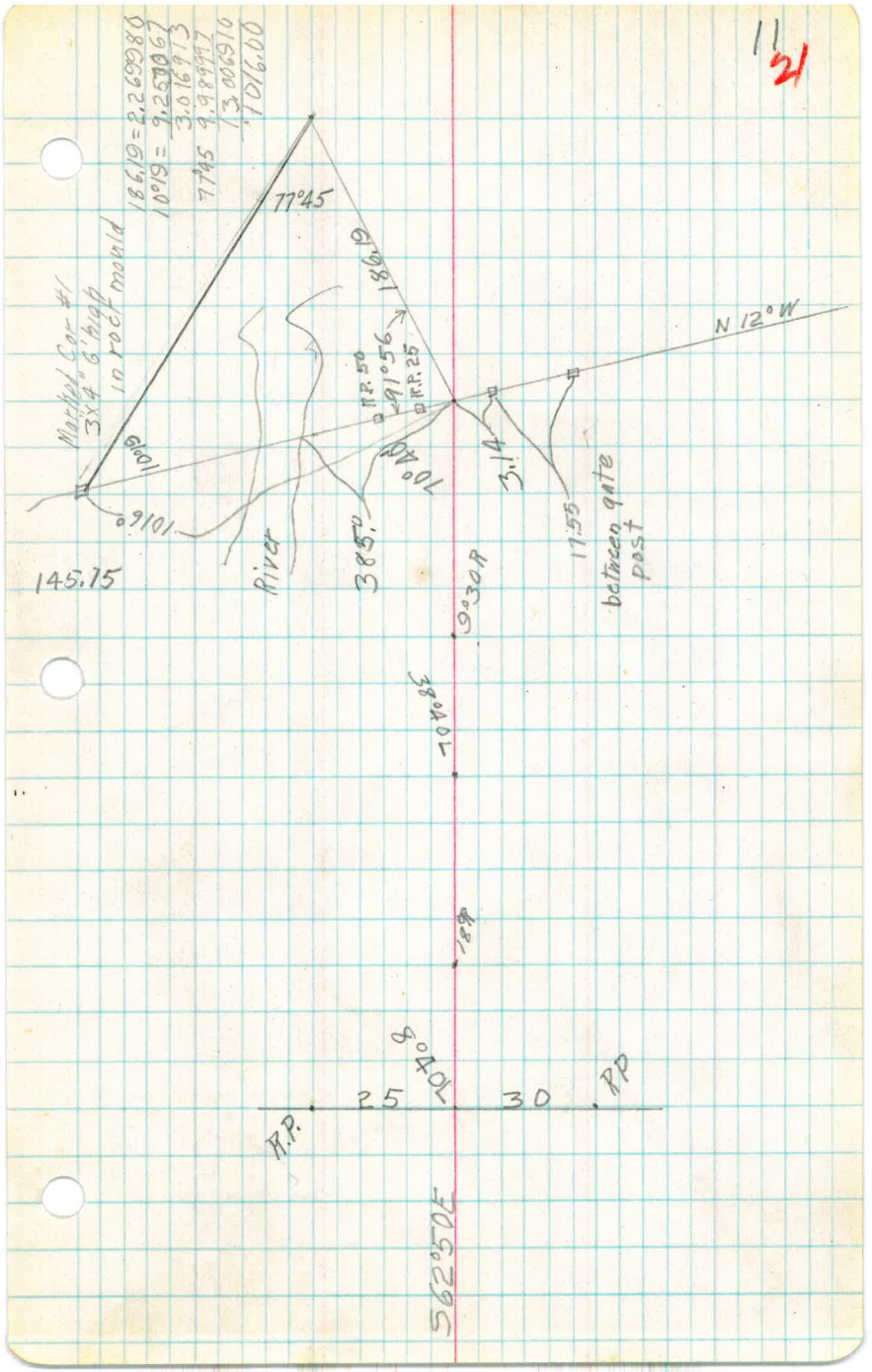

40°
23°50L
206+50 Top Grade
RP
RP split in 12" Oak
32°
River
40°
32°
7°30L
R.P. Split
between twin Oaks
RP
25
25
RP
20°30L
RP
30
24.32
RP

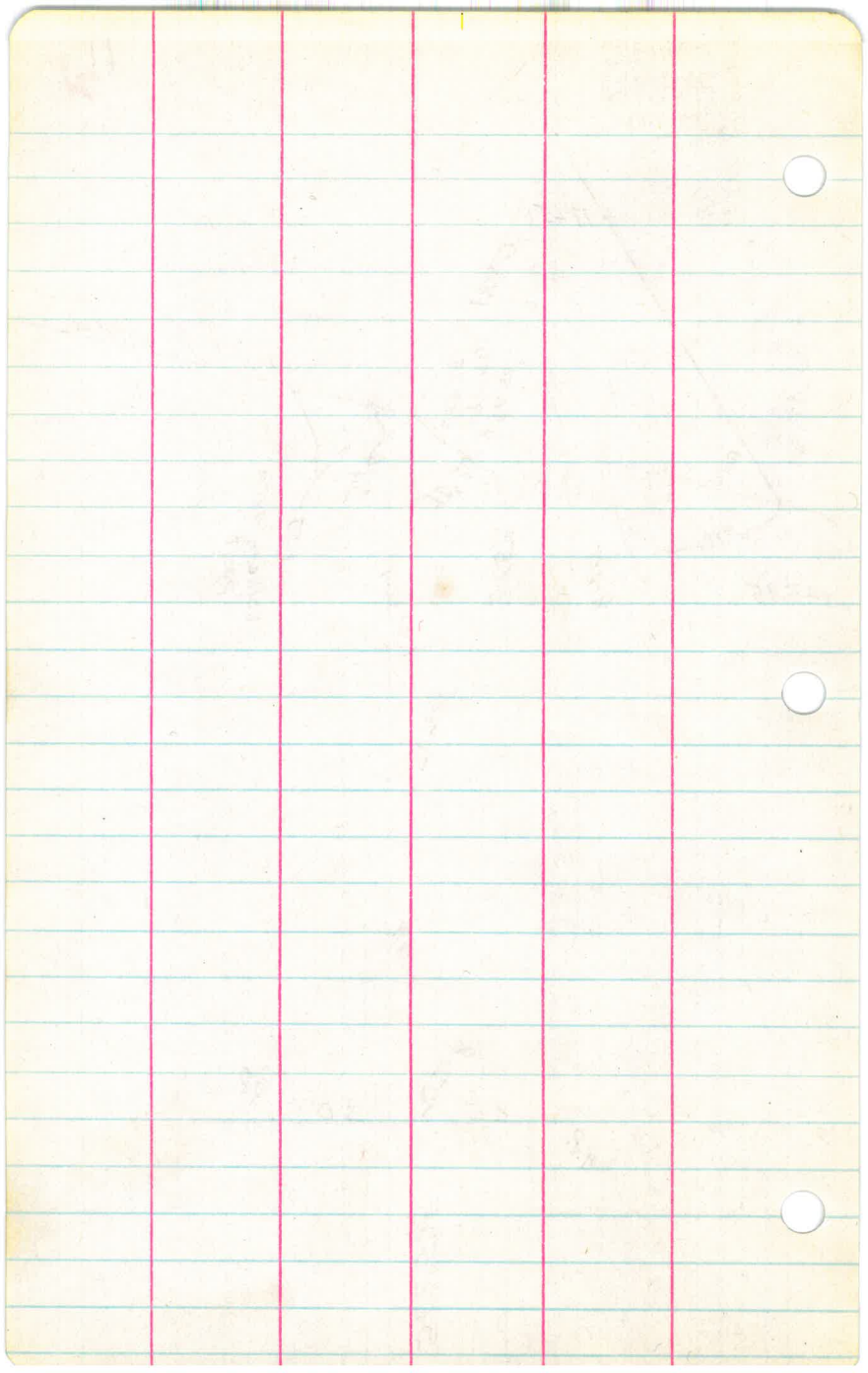


Survey of El Monte Ranch Road

226+22.11 Int & Road & E Line El Monte Ranch

224+76.34	A		9°30R	S82°40E	Solar S82°37'E
222+90.71	E.C.				
222+25.91	P.I.	R=200 T=70.17 L=134.97 E=11.95	38°40'L	N87°50E	255.82
221+55.74	B.C.				
220+87.87	EC				
220+25.56	P.I.	R=400 T=63.35 L=125.66 E=5°	18°R	S53°30E	201.39
219+62.21 #2	B.C.				
216+69.07 #2	A		8°40'L	S71°30E	356.49
214+27.10	P.O.T.			S62°50'E	


186.19 = 2.269988
10°19 = 9.257067
3.016913
77°45 9.989997
1.3002910
106.00
77°45
186.0
N 12° W
Marked Cor #1
3x4" 6' high
in rock mound
Gate
9101
145.75
River
385.0
100.40
P.P. 50
P.P. 25
91°56
3.14
11.55
between gate post
9°30 P
284.0
189
8°40
P.P.
25
30
P.P.
562.50E



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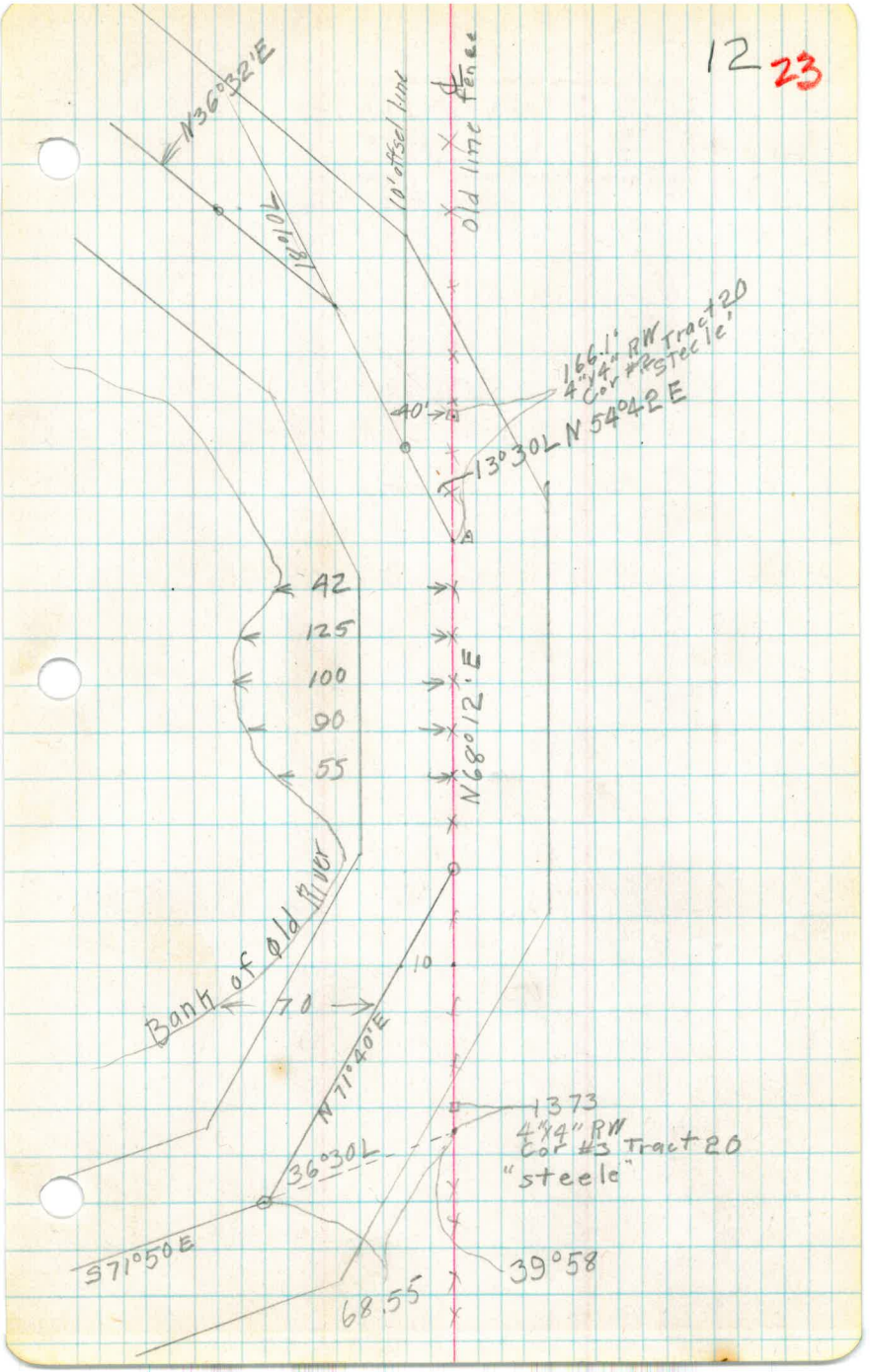
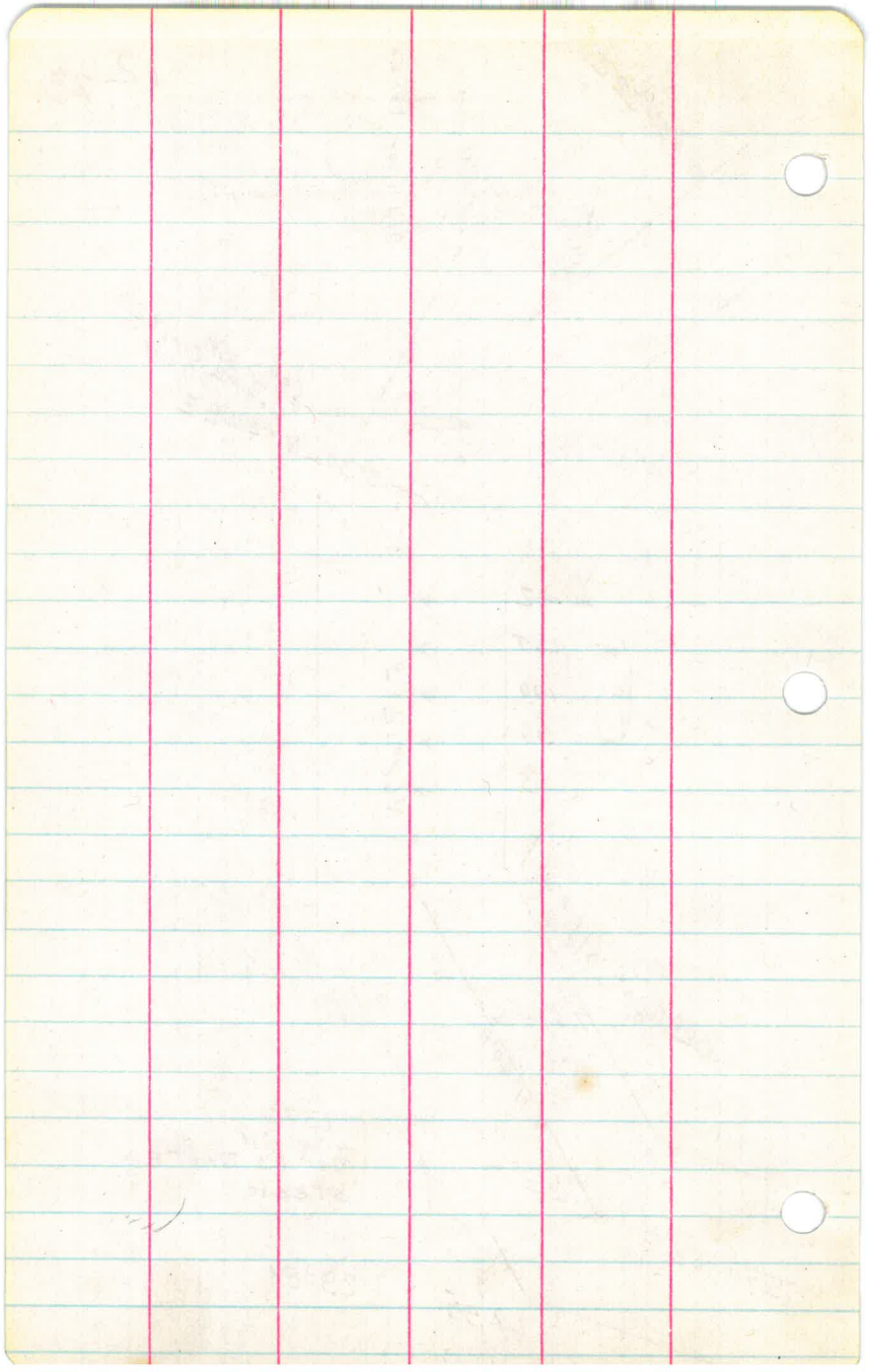
Change in Alignment for old Survey see page 6

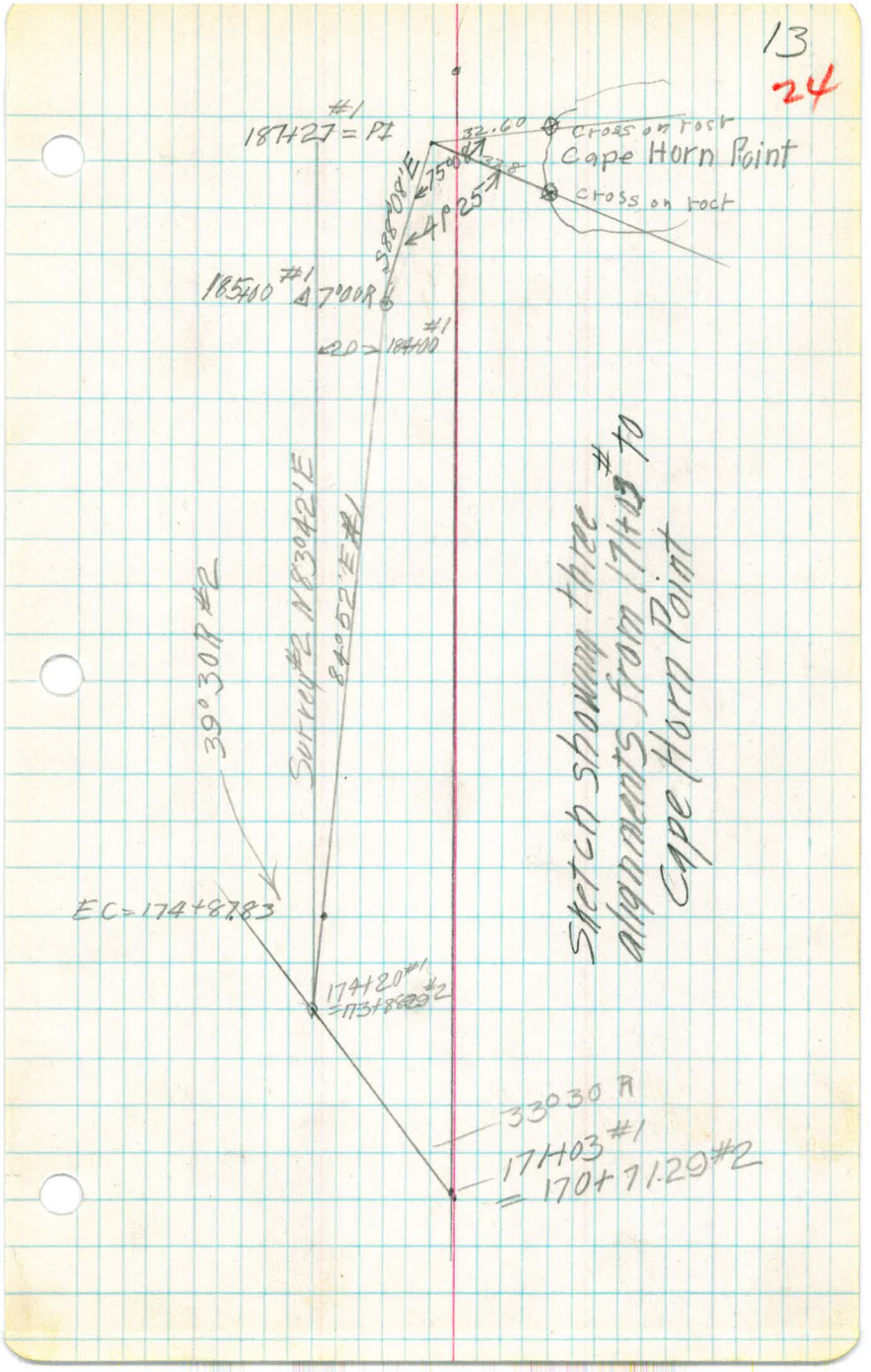
110+12.77 #2 E.C. = 101+44.88 Line #1

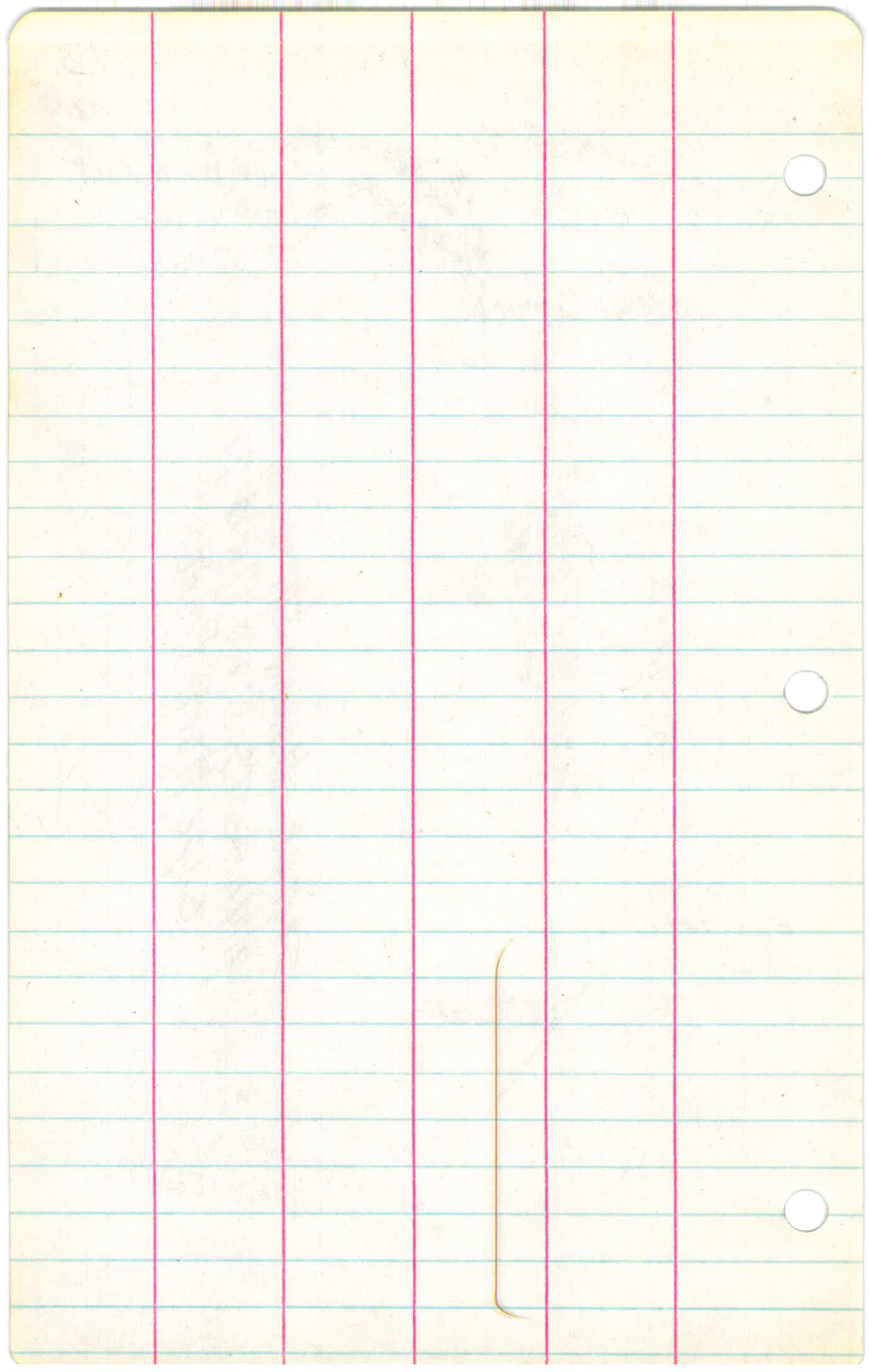
Equation

109+49.9	#2 P.I. = 109+90.51 #1	R=400 T=63.96 L=126.33 E=5.08	18°10L	N36°32'E	997.47
108+85.94	B.C.				
105+94.18	PI of 10' offset line				
105+51.4	Δ		13°30L	N54°42E	398.5
104+00					
103+00					
102+00					
101+00					
100+00					
98+25.32	Δ		3°28'L	N68°12E	725.88
97+00					
96+60.15	P.T. 10' offset line				
96+00					
91+63.17	E.C.				
91+01.72	P.I.	R=200 T=65.95 L=127.4 E=10.60	36°30L	N71°40E	728.3
90+35.77	B.C.				


N36°32'E
10' offset line
Old line fence
18.10'
166.1'
4"x4" RW
Cor #2 Tract 20
"Steele"
40'
N54°42E
13°30L
42
125
100
90
55
N68°12'E
Bank of old River
70
10
N71°40'E
1373
4"x4" RW
Cor #3 Tract 20
"steele"
36°30L
S71°50E
39°58
68.55'




#1
187+27 = PI
32.60
Cross on rock
Cape Horn Point
cross on rock
S88°08'E
150.00
41°25'
185+10 #1
Δ 7°00R
#1
20 → 184+00
Survey #2 N83°42'E
84.52' E #1
39°30R #2
EC=174+87.83
174+20 #1
=173+86.89 #2
Sketch showing three alignments from 174+03 #1 to Cape Horn Point
33°30 R
174+03 #1
= 170+71.20 #2



76+00 El Monte Ranch Topography

74+80

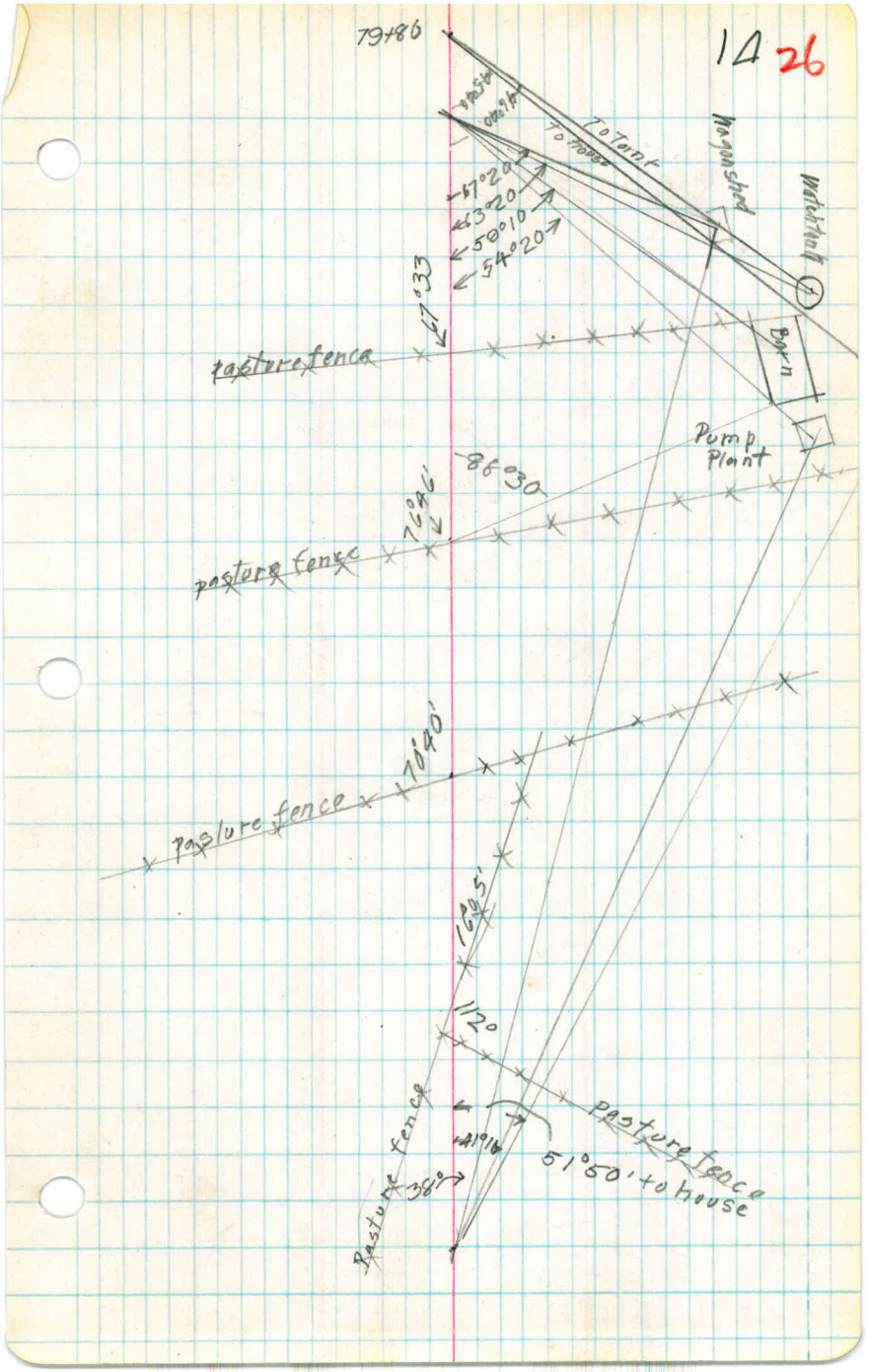
70+39

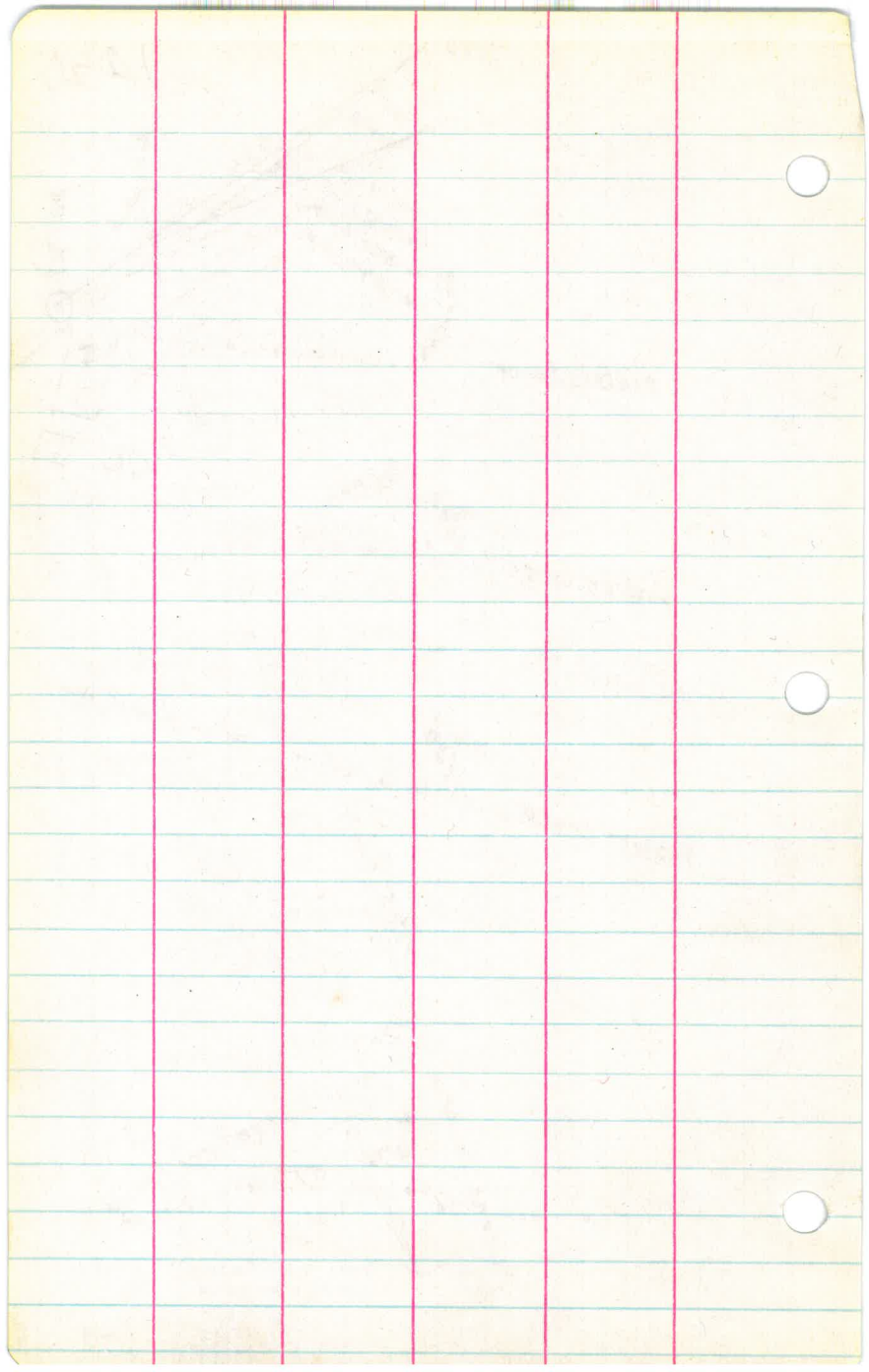
66+29

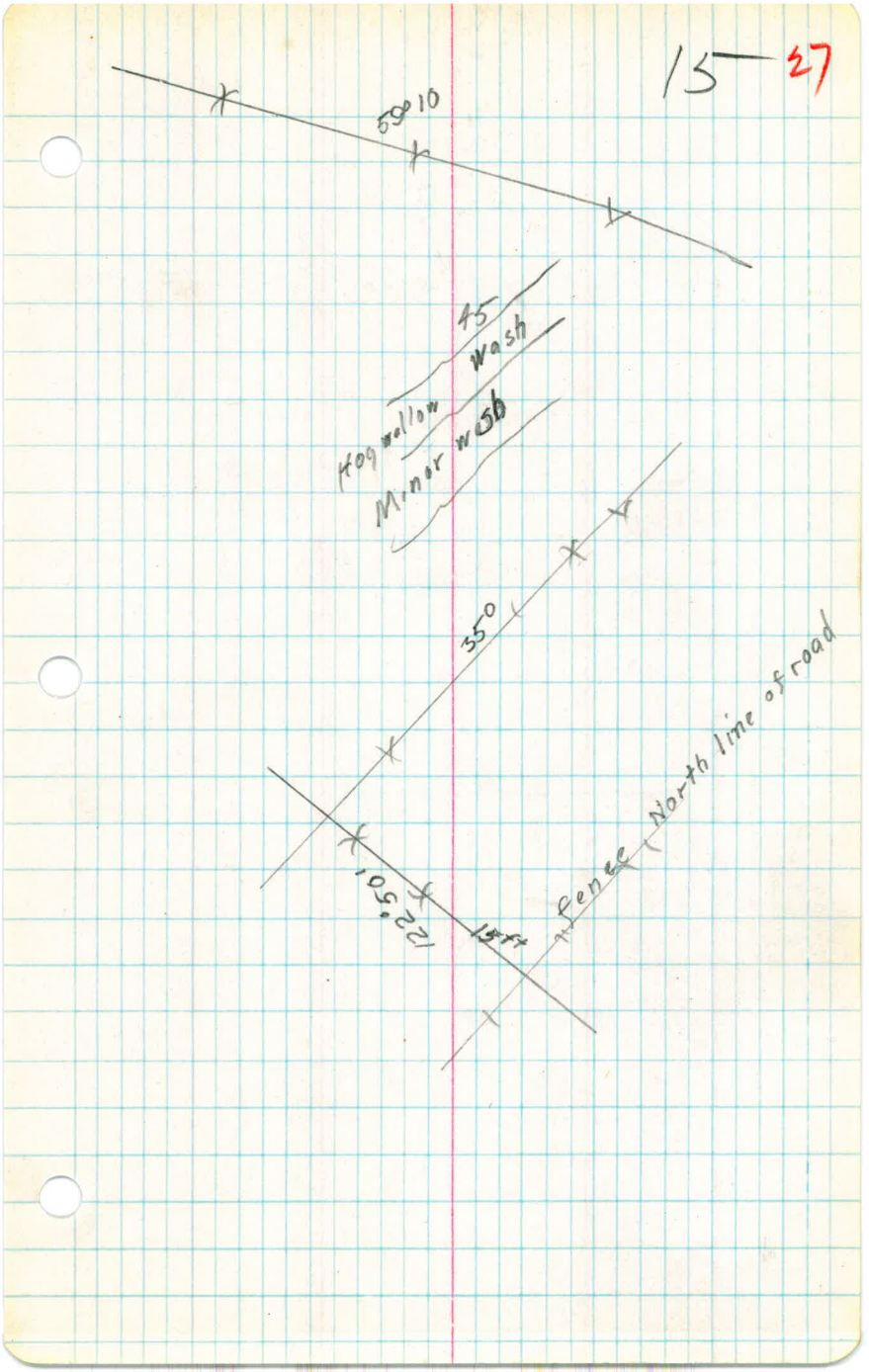
63+25

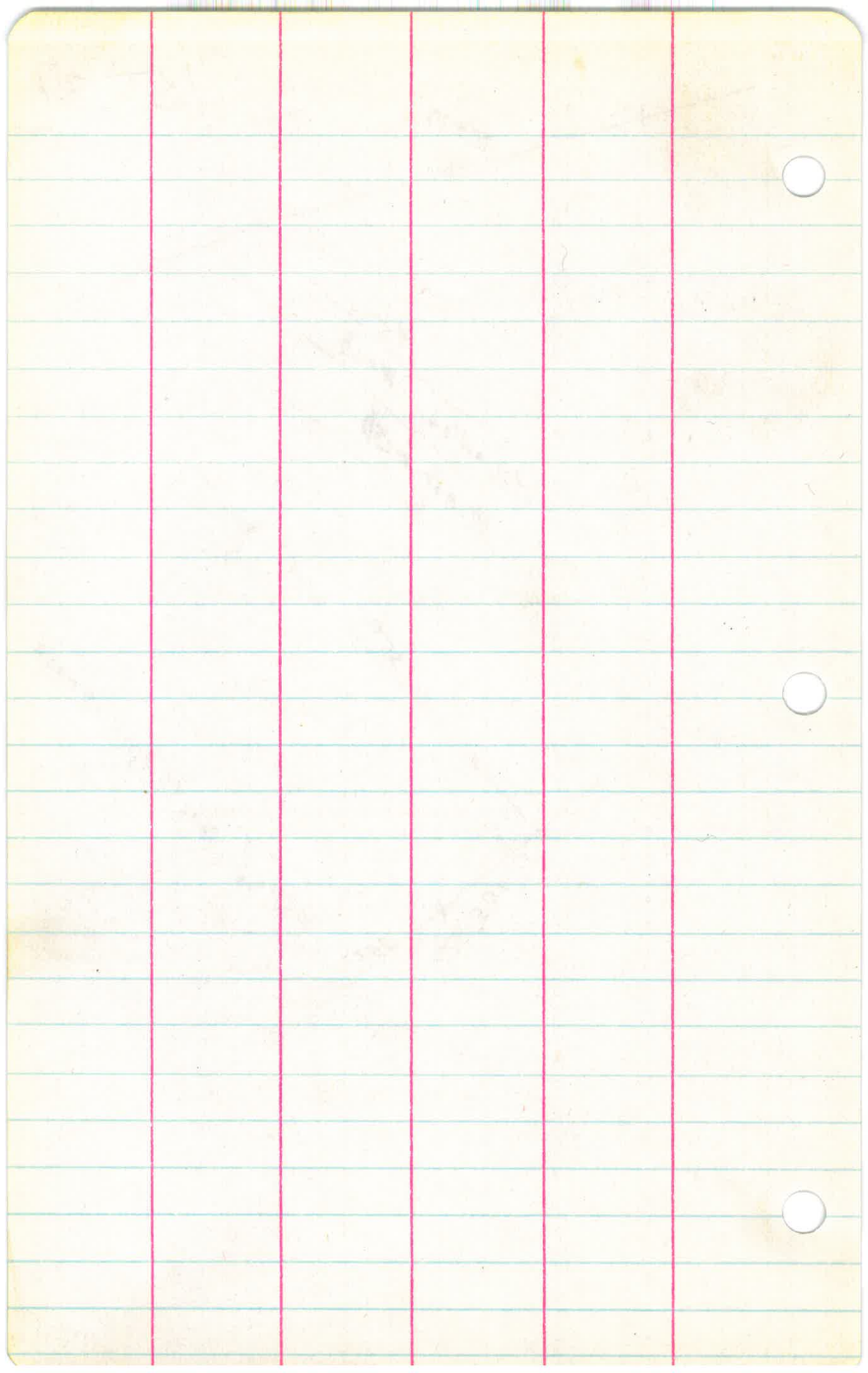
62+63

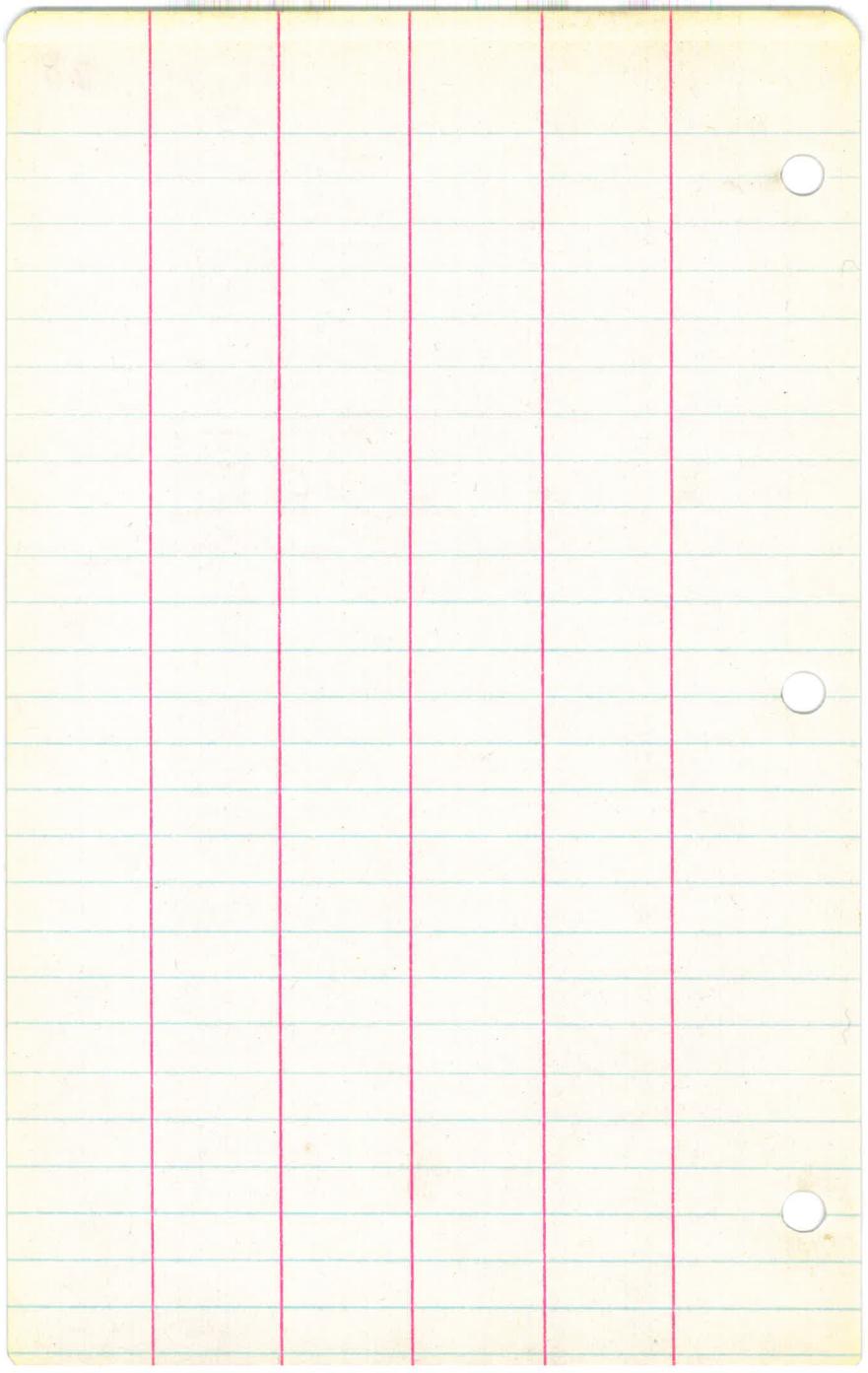
62+43 △


79+86
To Tank
To House
Magnolia Rd
Windmill
Barn
Pump Plant
47°33'
67°20'
63°20'
50°10'
54°20'
pasture fence
86°30'
76°46'
pasture fence
70°40'
pasture fence
16°45'
112°
pasture fence
141°16'
38°
Pasture fence
51°50' to house




500 10
45
Wash
Hog wallow
Minor wash
350
122°50'
15ft
fence North line of road





INDEX

Yellow

Levels from Richards intersection with Williams Axis El Capitan Dam Sta 63+37.14 to Sta. 2+86.78. Richards San Diego River Road Survey

White

Elevations taken from the cross section of the right of way on Richards El Capitan County Road Survey at 15' to the left of the center line

Ties

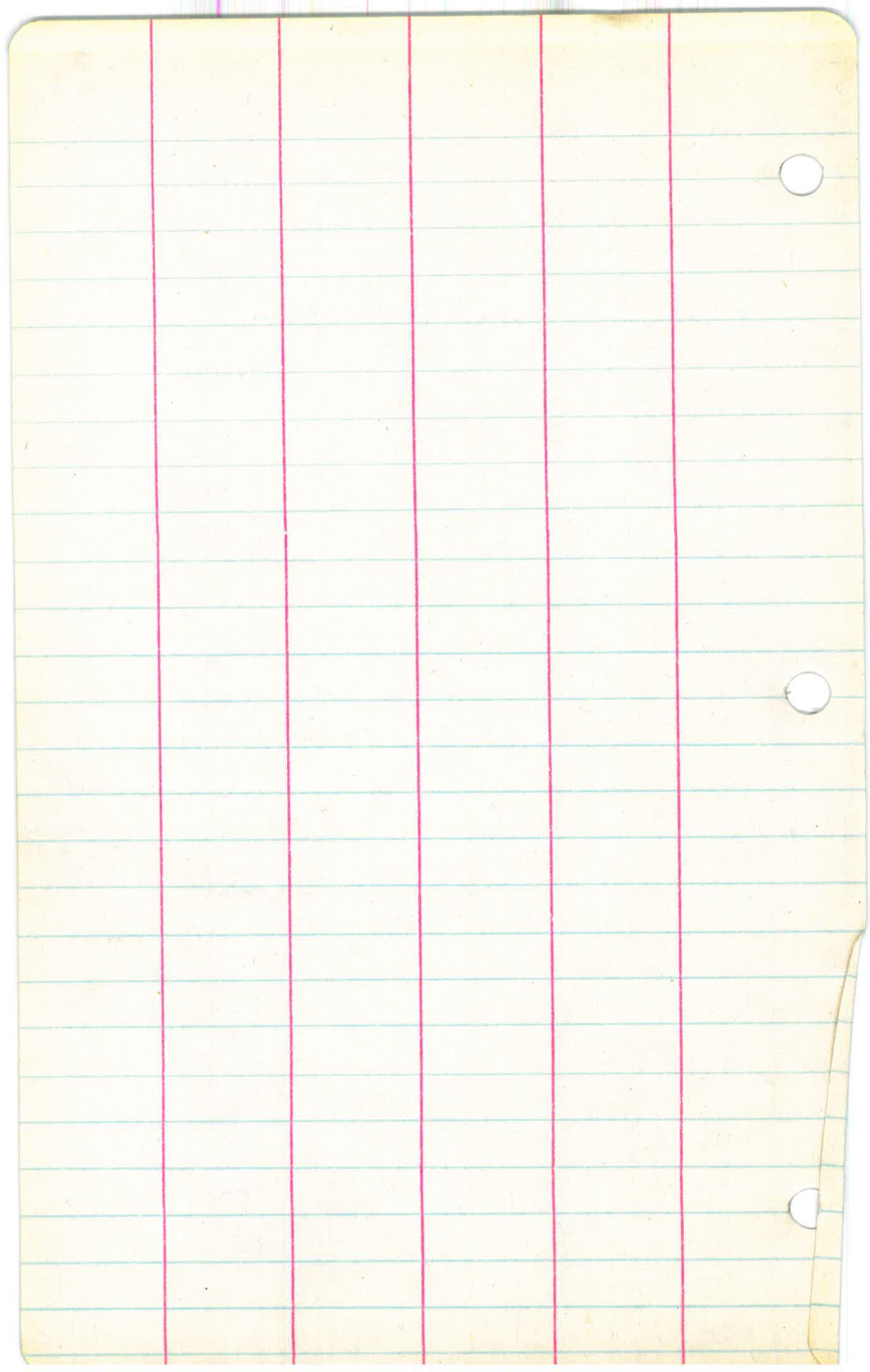
Preliminary Survey for Pipe line from El Capitan Damsight #3 to Sta. 2+86.78 EC on Richards Road Survey up the San Diego River

Yellow

Copy of Richards Notes of re-location of the El Capitan Road

Levels from E.C. 2+86.78 Richards Road Survey = Sta

51+68.31 Pipe line Survey
White
Cross Section of Right-
of-way on Richards El
Capitan County Road
Sta 10+00 to Sta 138+05.57
(El Monte Ranch East Line)



Levels from Richards Intersection with Williams Axis El Capitan Dam Sta. 63+37.14 to Sta. 2+86.78 Richards San Diego River Road Survey.

Sept. 16. 1927.
Converse
Rauner
McBain.
Pages 1-7.

Levels on Above Line from Sta. 62+76 to Sta. 139+05.57.
Pages 8-17.

B.M #2.				570.56
	4.22	574.78		
T.P.			3.39	571.39
	3.02	574.41		
T.P.			0.835	573.575
	4.81	578.385		
T.P.			9.52	568.865
	6.805	575.670		
B.M. #1.			4.21	571.46
			4.4	571.3
			2.1	573.6
63+37.14		Out	5.5	570.2
63+00			4.3	571.4
T.P.			1.36	574.31
	11.82	586.13		
62+00			8.2	577.9
61+50			6.5	579.6
61+00			5.8	580.3
60+00			7.5	578.6
T.P.			9.59	576.54
	2.53	579.07		
59			2.5	576.6
58			3.3	575.8
57			4.5	574.6

Sept. 16. 1929.
Converse
Rauner
Mc Bain.

(2) 37

Nail in Sycamore Tree 20' Rt. Sta.
11+50. El Capitan Pipe Line Survey.

575.67
571.46
4.21

Reset B.M. #1. Nail in Oak Tree 3' L. Sta. 17+09.
0+00 Halers Survey. On Hub.
0-52.87 Halers Survey. On Hub.
Richards Station on Axis El Capitan Dam.

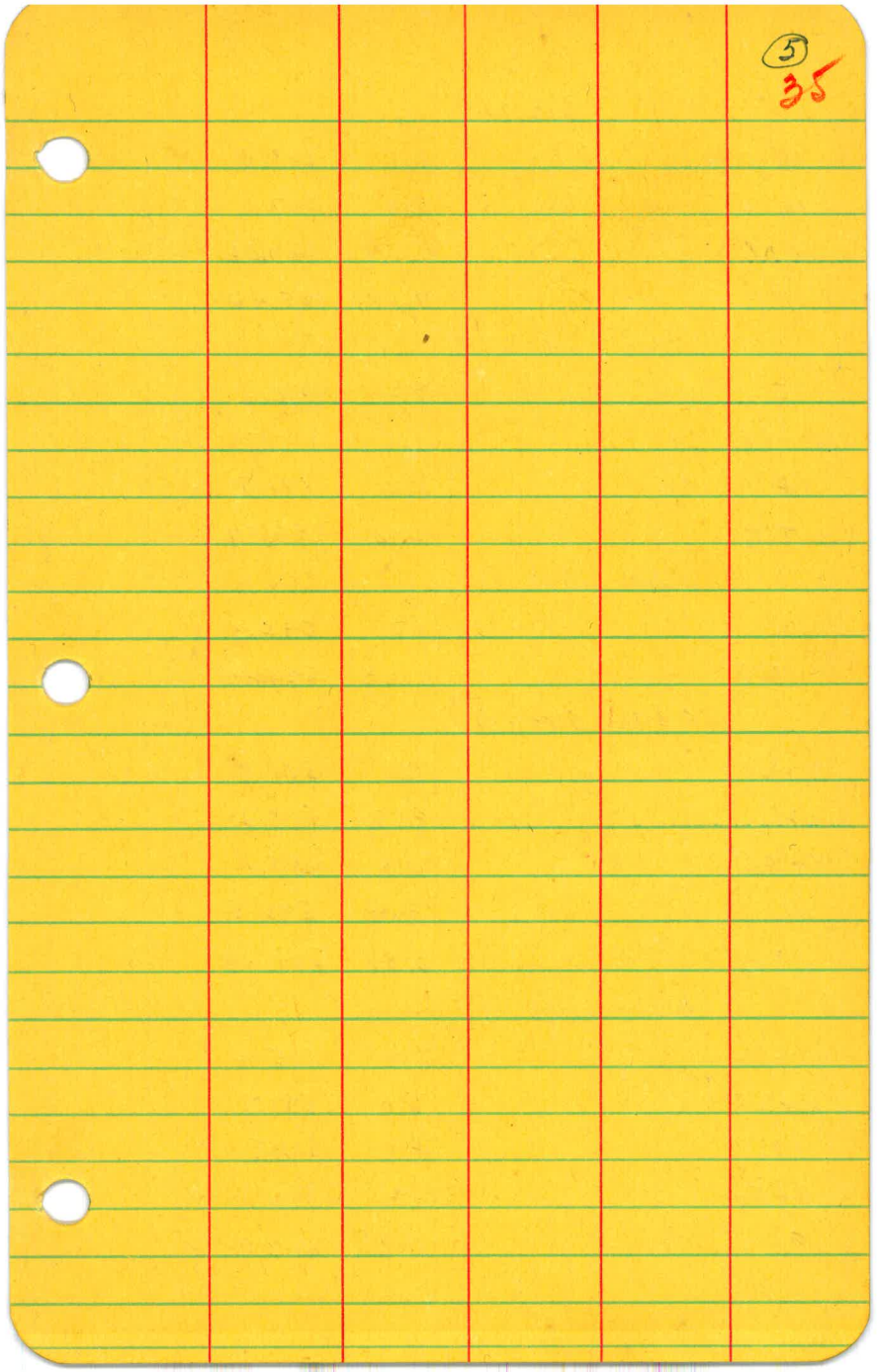
		579.07		
56			2.4	576.7
T.P.			0.73	578.34
	6.10	584.44		
55			4.6	579.8
54			3.8	580.6
53			7.5	576.9
52			7.7	576.7
T.P.			7.16	577.28
	4.74	582.02		
51			4.7	577.3
B.M.			4.05	577.97
50			4.5	577.5
49+40			6.2	575.8
49			5.8	576.2
T.P.			5.36	576.66
	12.08	588.74		
48+50			10.8	577.9
48			7.1	581.6
47+55			1.6	587.1
T.P.			0.61	588.13
	7.45	595.58		
47			5.1	590.5
46			4.8	590.8
45			5.9	589.7

Nail in Oak Tree 10' R. Sta. 50+25.

		595.58		
44			6.1	589.5
T.P.			5.65	589.93
	5.27	595.20		
43			6.7	588.5
42			4.1	591.1
41			0.3	594.9
T.P.			0.41	594.79
	9.87	604.66		
40			7.5	597.2
39+60			4.8	599.9
39+25			6.3	598.4
39			6.1	598.6
38			5.0	599.7
37			6.3	598.4
T.P.			6.11	598.55
	6.40	604.95		
36			5.5	599.5
35			7.9	597.1
34			6.3	598.7
B.M.			6.90	598.05
33			4.8	600.2
32			3.2	601.8
T.P.			3.15	601.80
	0.40	607.20		

Nail in Oak Tree 15'R. Sta. 34+25. (Public Camp Grounds)

		602.20		
31+50			3.2	599.0
31			6.2	596.0
30+65			7.0	595.2
30			6.6	595.6
29			4.8	597.4
T.P.			4.85	597.35
	8.84	606.19		
28			8.0	598.2
27			5.5	600.7
26			2.4	603.8
25			1.2	605.0
T.P.			1.23	604.96
	9.83	614.79		
24			7.1	607.7
23			4.0	610.8
22			2.7	612.1
21+40			2.0	612.8
21			2.5	612.3
T.P.			2.39	612.40
	3.29	615.69		
20			5.0	610.7
19			6.1	609.6
18			6.3	609.4
T.P.			5.89	609.80
	3.14	612.94		


5
35

		612.94			
17			4.1	608.8	
16			5.8	607.1	
B.M.			5.58	607.36	
T.P.			7.48	605.46	
	2.80	608.26			
15			3.2	605.1	
14+55			3.1	605.2	
14			6.6	601.7	
T.P.			12.74	595.52	
	0.49	596.01			
13			1.7	594.3	
T.P.			11.53	584.48	
	8.44	592.92			
12+25			11.0	581.9	
12			13.5	579.4	
11+85			11.8	581.1	
11			2.4	590.5	
T.P.			0.89	592.03	
	11.14	603.17			
10+60			7.8	595.4	
10+35			6.0	597.2	
10			4.9	598.3	
9+50			4.4	598.8	
9			0.3	602.9	
B.M.			2.00	601.17	

Nail in Oak Tree 10' R. Sta. 15+65.

Bottom Chocolate Creek.

Nail in Oak Tree 10' L. Sta. 9+25

B.M				601.17
	4.93	606.10		
8			3.0	603.1
7			1.4	604.7
T.P.			0.80	605.30
	12.64	617.94		
6+40			11.6	606.3
6			8.0	609.9
5			2.4	615.5
4			0.1	617.8
T.P.			0.30	617.64
	4.47	622.11		
3			5.0	617.1
2+86.78 = 51+68.31			5.3	616.8
B.M.			9.95	612.16
2+27.81 P.I. #2 Out			6.8	615.3

(7)
37

= 2+86.78 E.C. Richards Survey =
= 51+68.31 P.O.T. Pipe Line Survey =

Nail top Oak Stump 45' R. Sta. 2+75

B.M.#1.				571.46
	4.15	575.61		
62+76			3.6	572.0
63			15.0	560.6
+27			5.8	569.8
+25			10.9	564.7
+97			12.5	563.1
64			16.7	558.9
+57			9.6	566.0
+87			7.5	568.1
65			7.3	568.3
+40			6.9	568.7
B.M.#1				571.46
	4.61	576.07		
65+75			4.7	571.9
+83			3.4	572.7
66			2.5	573.6
+19.26			0.9	575.2
T.P.			0.20	575.87
	1.15	577.02		
+55			1.2	575.8
67			3.4	573.6
68			7.0	570.0

Sept. 27. 1927.

Nail in Oak Tree 3' L. Sta. 1+09. El Capitan Pipe Line Survey.

Top River Bank.
Bottom of Bank
Top of Bank

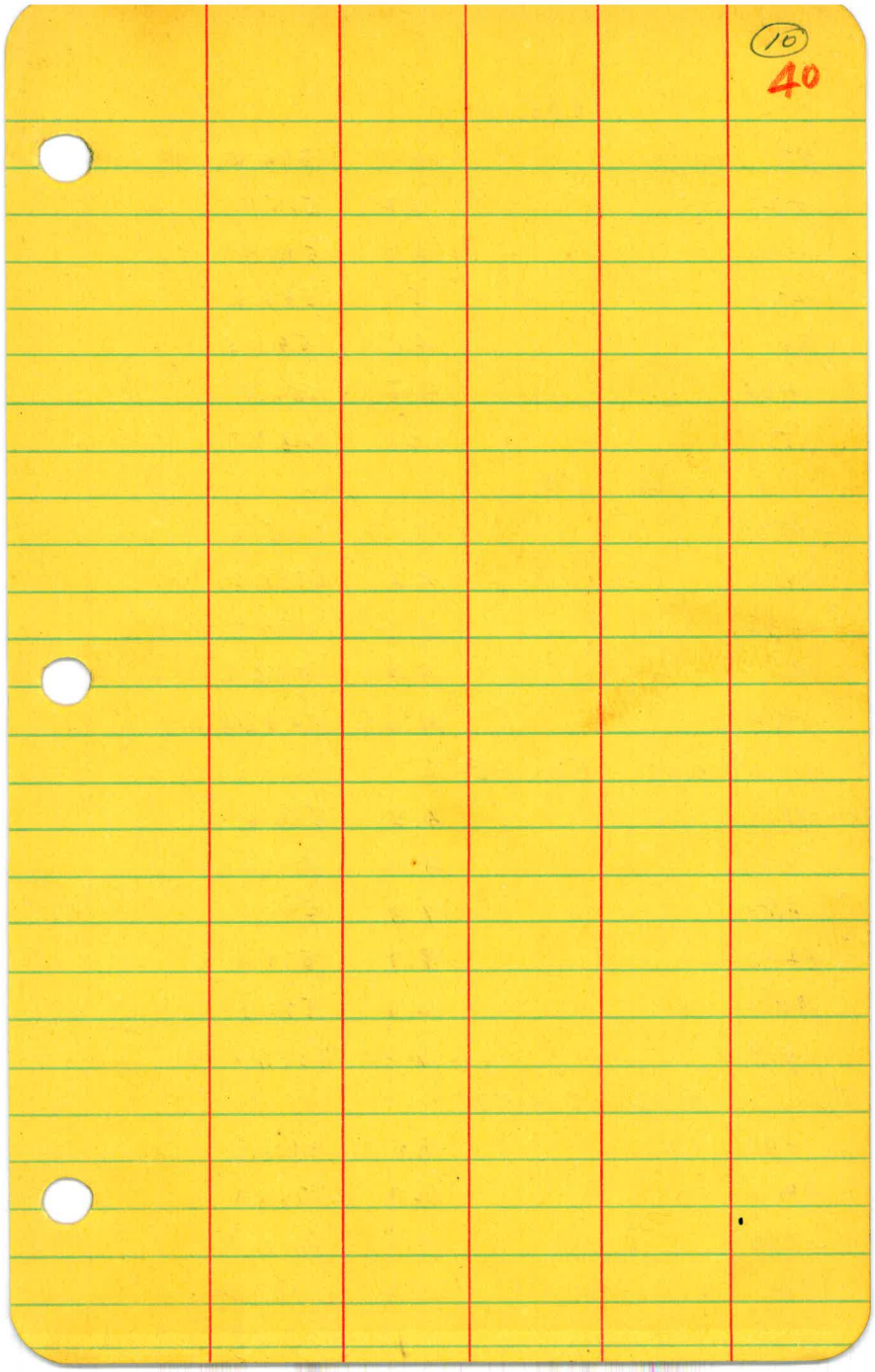
From Sta. 62+76 to Sta. 64+87 the road was washed away by flood of Feb. 1927.

		577.02		
69			7.1	569.9
70			4.3	572.7
+66			6.6	570.4
+97			8.0	569.0
T.P.			8.08	568.94
	4.85	573.79		
71+28			4.7	569.1
+93			3.7	570.1
72			3.8	570.0
73			5.1	568.7
+79			6.0	567.8
B.M.#2.			3.22	570.57
74			6.2	567.6
+41			6.8	567.0
75+04			5.6	568.2
+46			5.5	568.3
76			3.8	570.0
T.P.			4.21	569.58
	1.33	570.91		
+02			2.3	568.6
+11			4.0	566.9
+22			0.7	570.2
+75			1.7	569.2
77			2.8	568.1

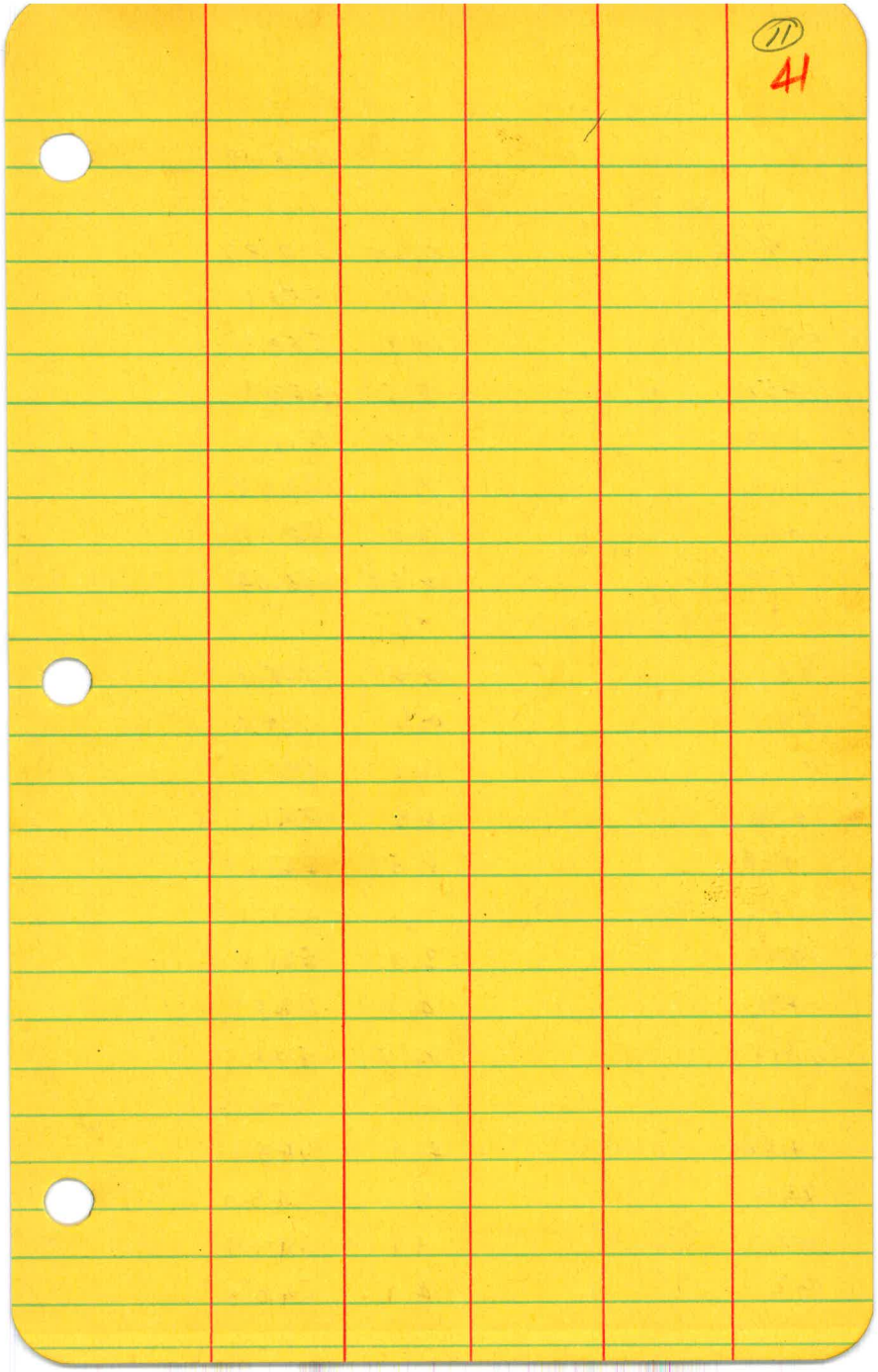
9
39

Nail in Sycamore 7' Rt. 73+94. El. 570.564

		570.91		
77+66			4.5	566.4
+83			5.2	565.7
78			5.4	565.5
79			5.3	565.6
80			7.7	563.2
81			7.3	563.6
82			7.0	563.9
T.P.			7.02	563.89
	7.45	571.34		
+34			8.0	563.3
+60			12.3	559.0
83			5.8	565.5
+27			4.3	567.0
84+07	6		3.2	568.1
T.P.			3.29	568.05
	6.27	574.32		
+87			6.4	567.9
85			6.2	568.1
+17			6.2	568.1
+87			4.7	569.6
86			4.3	570.0
+41			2.8	571.5
T.P.			0.64	573.68
	11.44	585.12		


(10)
40

		585.17		
87			10.6	574.5
+21			9.2	575.9
+50			6.2	578.9
+78			5.1	580.0
88			4.6	580.5
+35			2.5	582.6
T.P.			1.25	583.87
	9.14	593.01		
+72			7.1	585.9
89			4.4	588.6
+35			2.7	590.3
90			8.4	584.6
T.P.			12.43	580.58
	0.27	580.85		
91			4.3	576.6
+13			4.9	576.0
+57			7.8	573.1
+89			9.9	571.0
92			10.6	570.3
T.P.			12.87	567.98
	0.84	568.82		
+61			3.2	565.6
93			5.7	563.1
+52			7.9	560.9
94			9.4	559.4
T.P.			9.93	558.89


11
41

				558.89	
	10.28	569.17			
B.M #4			0.30	568.87	
+55			10.6	558.6	
95			10.9	558.3	
+58			9.5	559.7	
+78			8.2	561.0	
96			8.3	560.9	
+67			12.1	557.1	
T.P.			12.33	556.84	
	0.47	557.26			
97			2.2	555.1	
98			4.7	552.6	
99			5.8	551.5	
+76			6.6	550.7	
T.P.			6.58	550.68	
	2.32	553.00			
100			3.0	550.0	
+76			4.3	548.7	
101			4.5	548.5	
+16			4.7	548.3	
+54			4.9	548.1	
+91			5.0	548.0	
102			5.1	547.9	
103			4.2	548.8	

(12)
47

Oak Tree 30' L. 95+50 El. 568.844

Top Hub. P.I. # 47.

Sept. 28. 1927

		553.00		
+77			5.9	547.1
T.P.			5.74	547.26
	0.16	547.42		
104			2.2	545.2
+39			4.5	542.9
105			5.5	541.9
106			8.5	538.9
+25			9.0	538.4
+55			8.7	538.7
T.P.			9.06	538.36
	3.95	542.31		
106+85.11 = 106+81.11			3.8	538.5
107			3.7	538.6
+74			4.8	537.5
108			4.8	537.5
+44			4.7	537.6
109			5.0	537.3
110			5.9	536.4
+20			6.3	536.0
T.P.			5.44	536.87
	3.95	540.82		
+45			4.8	536.0
111			4.2	536.6
+33			4.6	536.2
+67			5.6	535.2

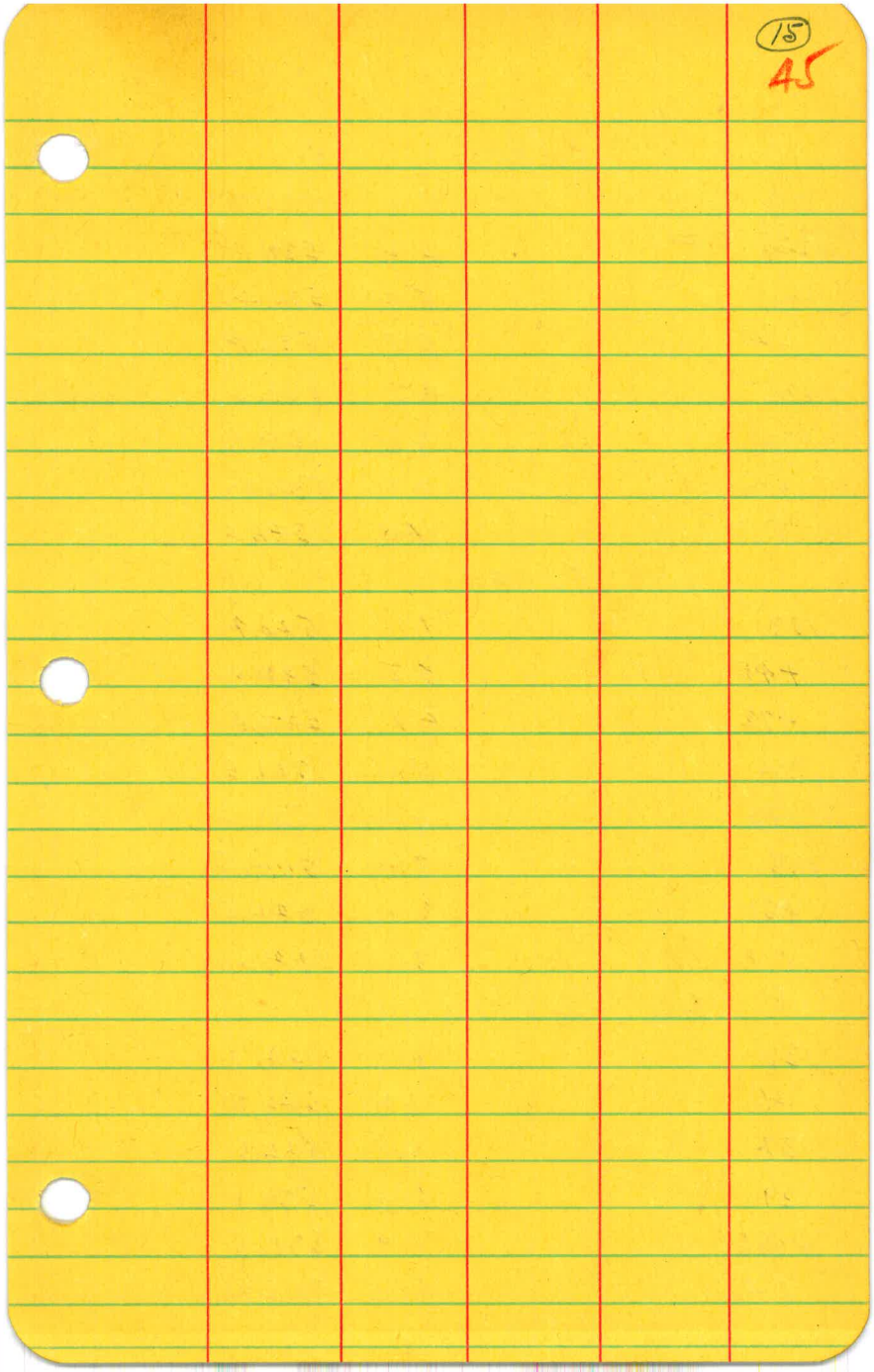
= Sta. 106+85.11 E.C.
= Sta. 106+81.11 E.C =

		540.82		
112			6.4	534.4
+74			8.1	532.7
T.P.			7.64	533.18
	9.83	543.01		
113+04			9.8	533.2
+32			9.5	533.5
+68			6.4	536.6
+83			6.0	537.0
114			6.0	537.0
+63			4.8	538.2
+84			5.2	537.8
115			5.6	537.4
+65			6.0	537.0
116			6.4	536.6
T.P.			6.91	536.10
	4.69	540.79		
+41			4.7	536.1
B.M #6			1.13	539.66
117			4.8	536.0
118			5.3	535.5
+50			5.1	535.7
119			2.7	538.6
+83			6.0	534.8
T.P.			6.00	534.79

(14)
44

Nail in Oak Tree 18R Sta. 116+60 El 539.618

				534.79	
	2.34	537.13			
120			2.4	534.7	
+19			2.3	534.8	
+54			3.2	533.9	
121			3.7	533.4	
122			5.0	532.1	
+18			5.2	531.9	
123			7.0	530.1	
+83			7.7	529.4	
124			8.4	528.7	
+39			9.7	527.4	
+94			9.6	527.5	
T.P.			9.68	527.45	
	7.75	535.70			
125+48			5.4	529.8	
126			4.2	531.0	
+35			4.6	530.6	
+83			4.7	530.5	
127			4.1	531.1	
128			4.3	530.9	
+41			3.8	531.4	
+89			3.9	531.3	
T.P.			4.09	531.11	
	5.21	536.32			


15
45

		536.32		
129			5.0	531.3
129+34.32 = 129+36.01			5.2	531.1
130			5.7	530.4
+41			5.5	530.8
131			4.7	531.6
132			2.2	534.1
+40			1.5	534.8
T.P.			1.48	53484
	12.61	547.45		
133			7.1	540.4
+45			5.5	542.0
+79			4.9	542.6
134			5.0	542.5
+72			4.1	543.4
135			3.0	544.5
+36			3.0	544.5
T.P.			3.05	544.40
	3.01	547.41		
136			2.7	544.7
+60			1.2	546.2
137			2.8	544.6
139			8.4	539.0
+05.57			8.9	538.5
T.P.			13.10	534.31

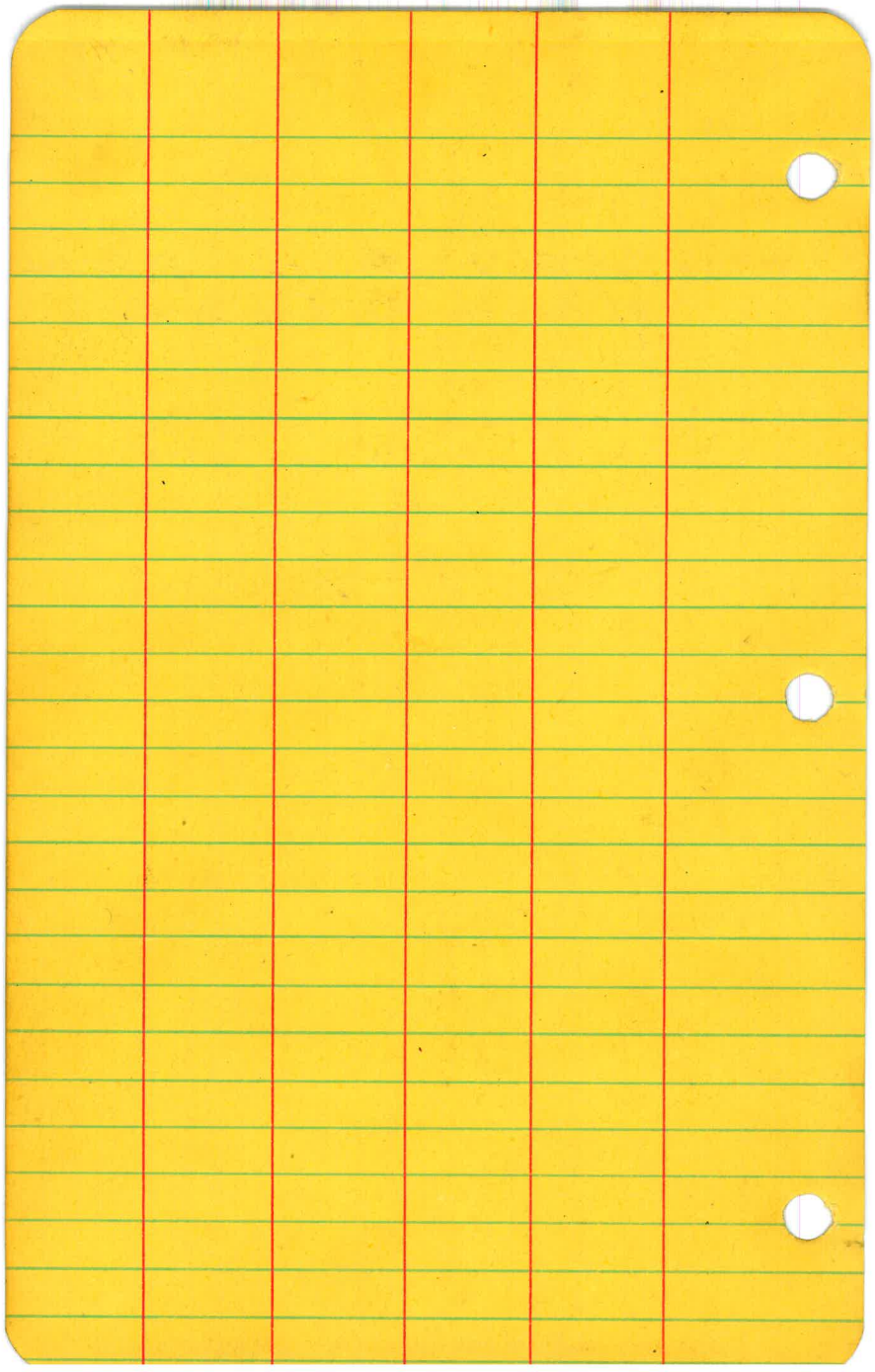
= Sta. 129+34.32 E.C =
= Sta. 129+36.01 E.C. =

End of Richards Road, Survey on
E. Line El Monte Ranch.

T.P.				534.31	
	0.39	534.70			
B.M.#9			4.75	529.95	

(17)
47

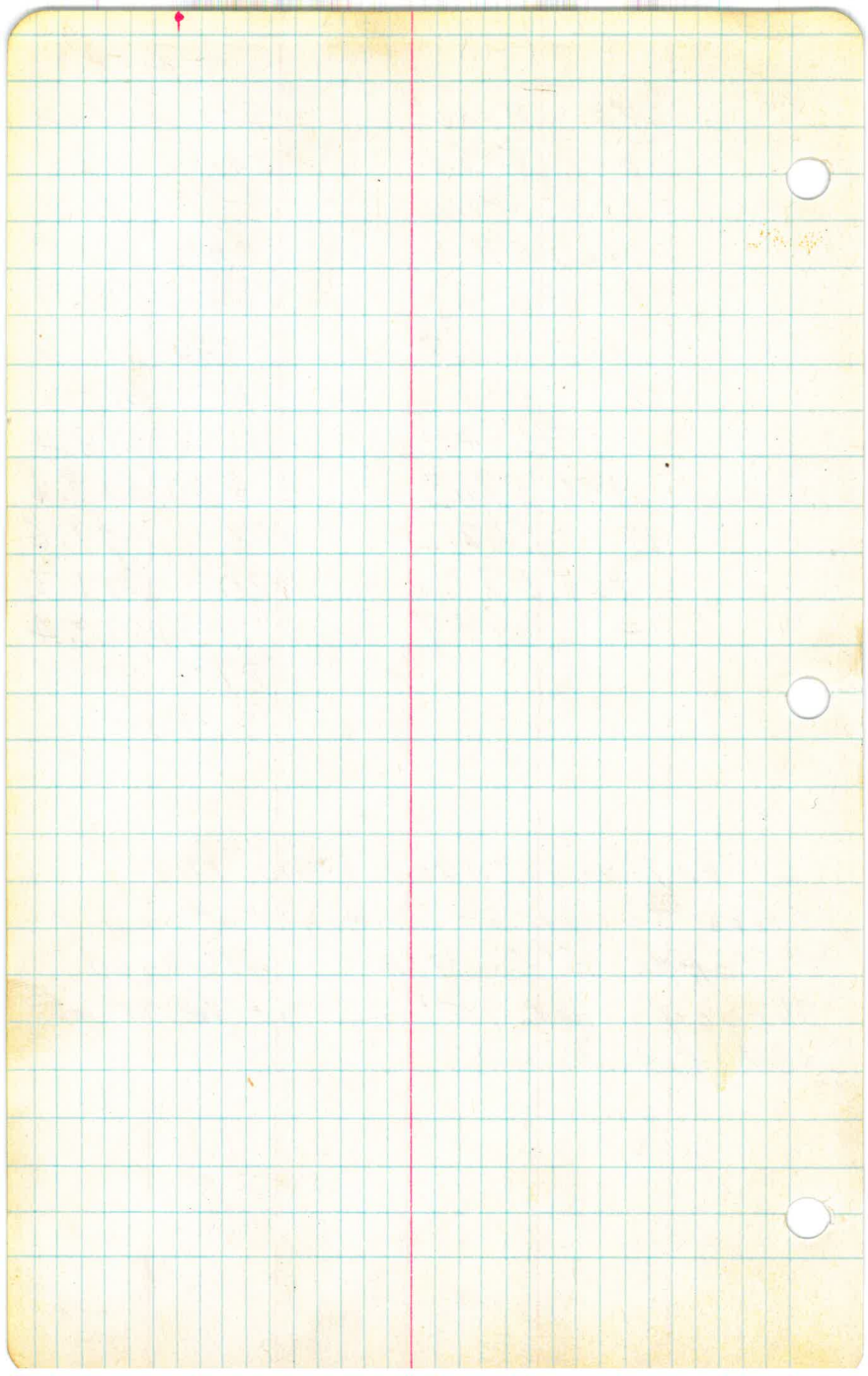
Nail in Oak Tree 11'L. Sta. 77+50 El. 529.90
El Capitan Pipe Line Survey.



Sta.	Elev.
10	599.8
+35	597.2
+60	596.6
11	590.3
+85	581.8
12	580.6
+25	584.4
+50	591.3
13	602.2
+25	597.2
14	609.7

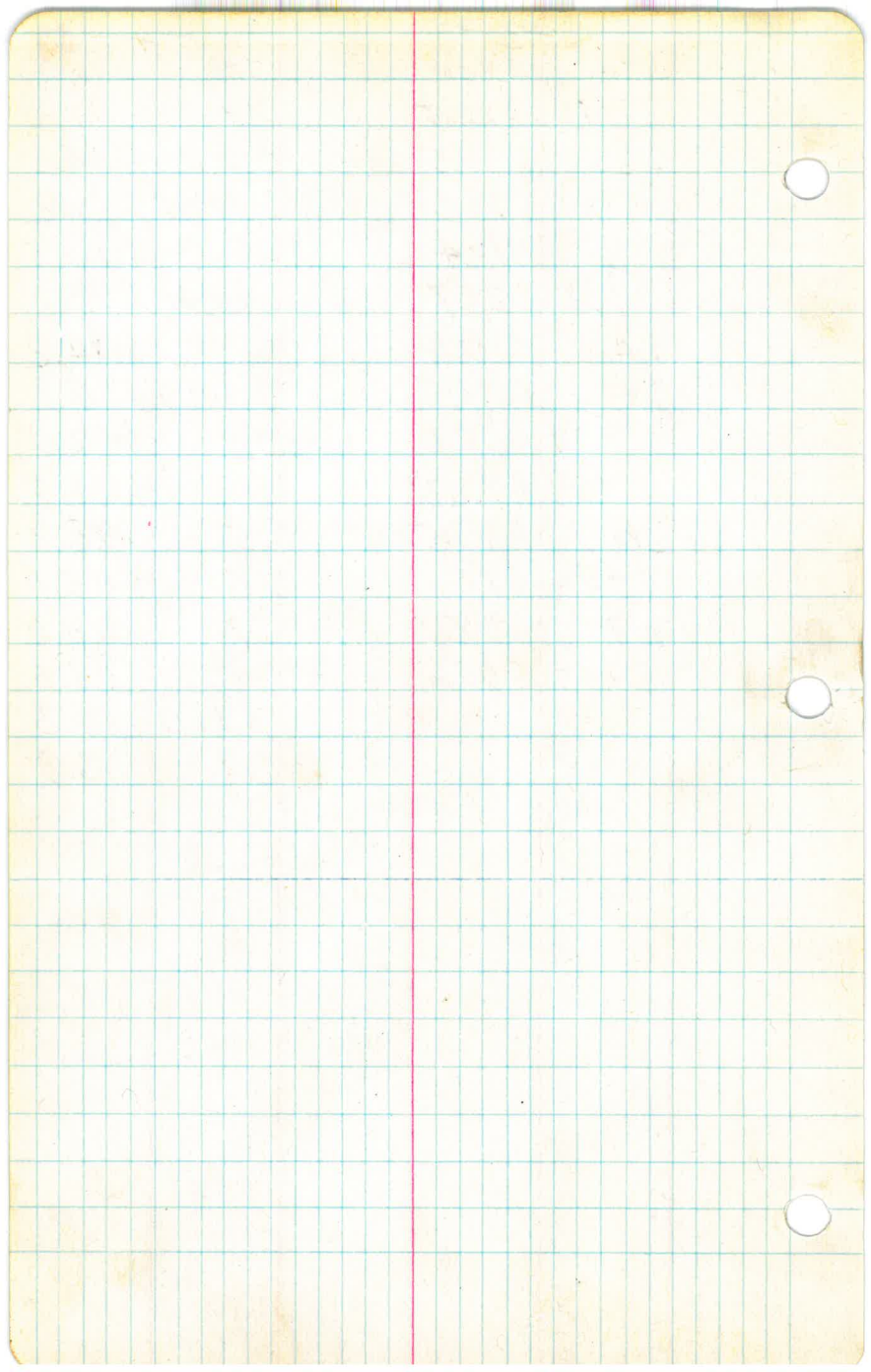
Sta	Elev.
14+55	612.1
15	611.0
+48	612.8
16	613.9
+40	613.9
17	613.8
18	618.4
+30	619.1
19	619.6
20	621.7
+30	623.4
21	625.9

Elevations taken from the Cross Section of the right of way on Richards El Capitan County Road Survey at 15' to the left of the Center line.



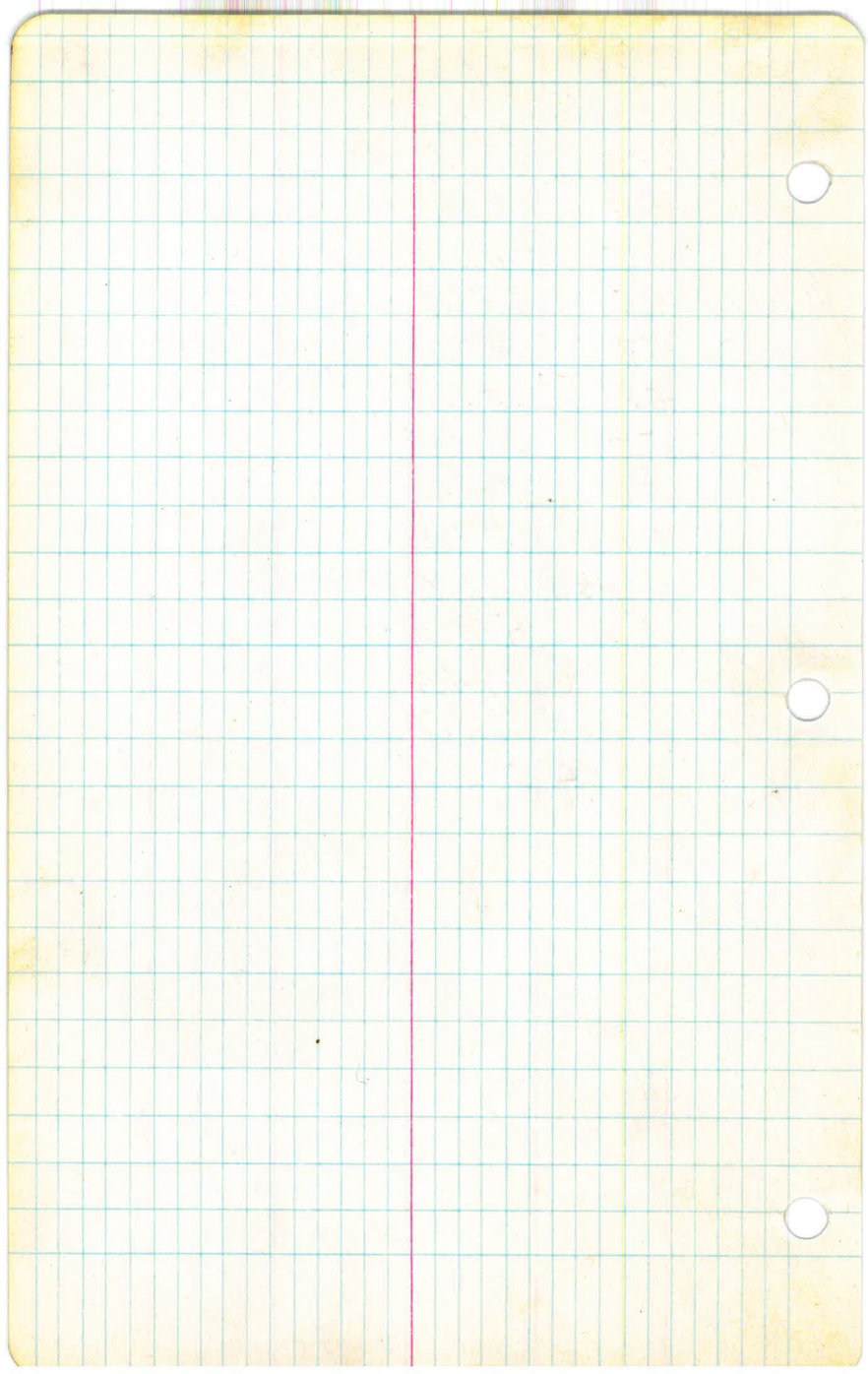
Sta.	Elev.
21+16	622.5
22	623.5
+60	615.3
23	616.4
+38	621.7
24	615.8
25	619.6
+29	609.6
+63	605.3
26	605.5
+64	611.1
27	608.7
+55	605.6

Sta.	Elev.
28	607.3
29	604.6
+35	603.2
30	600.5
+64	598.2
31	604.2
32+09	606.9
33	602.0
34	601.5
35	598.8
36	605.6
37	603.0
38	608.6
+60	610.3
39	603.3



50

Sta	Elev
52+50	580.5
53	580.8
54	580.9
55	580.9
56	579.9
57	580.2
58	581.1
59	581.7
60	584.2
61	587.1
+50	583.8
62	579.8
+76	574.4
63	572.7
+22	572.0

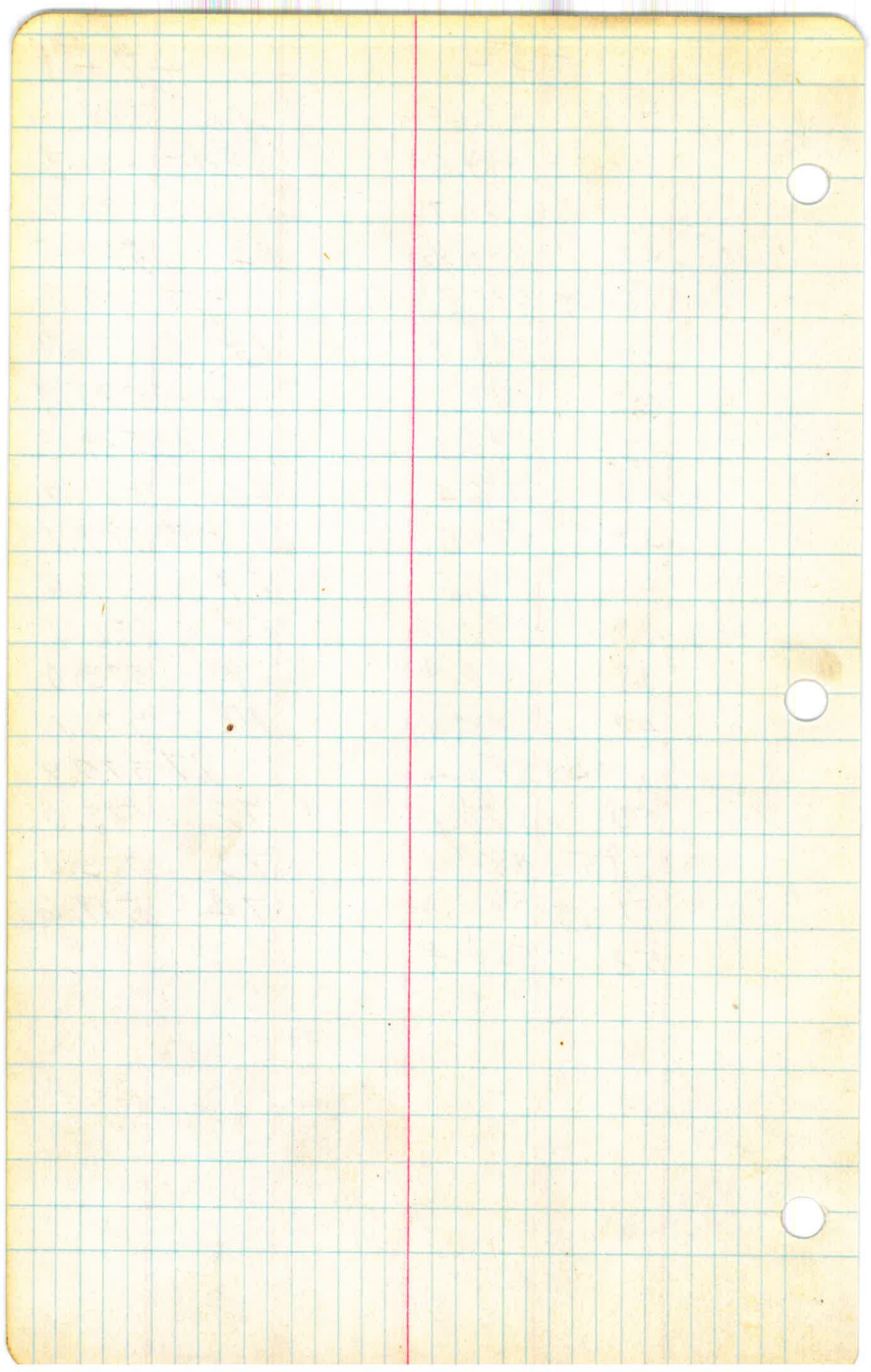


-5-

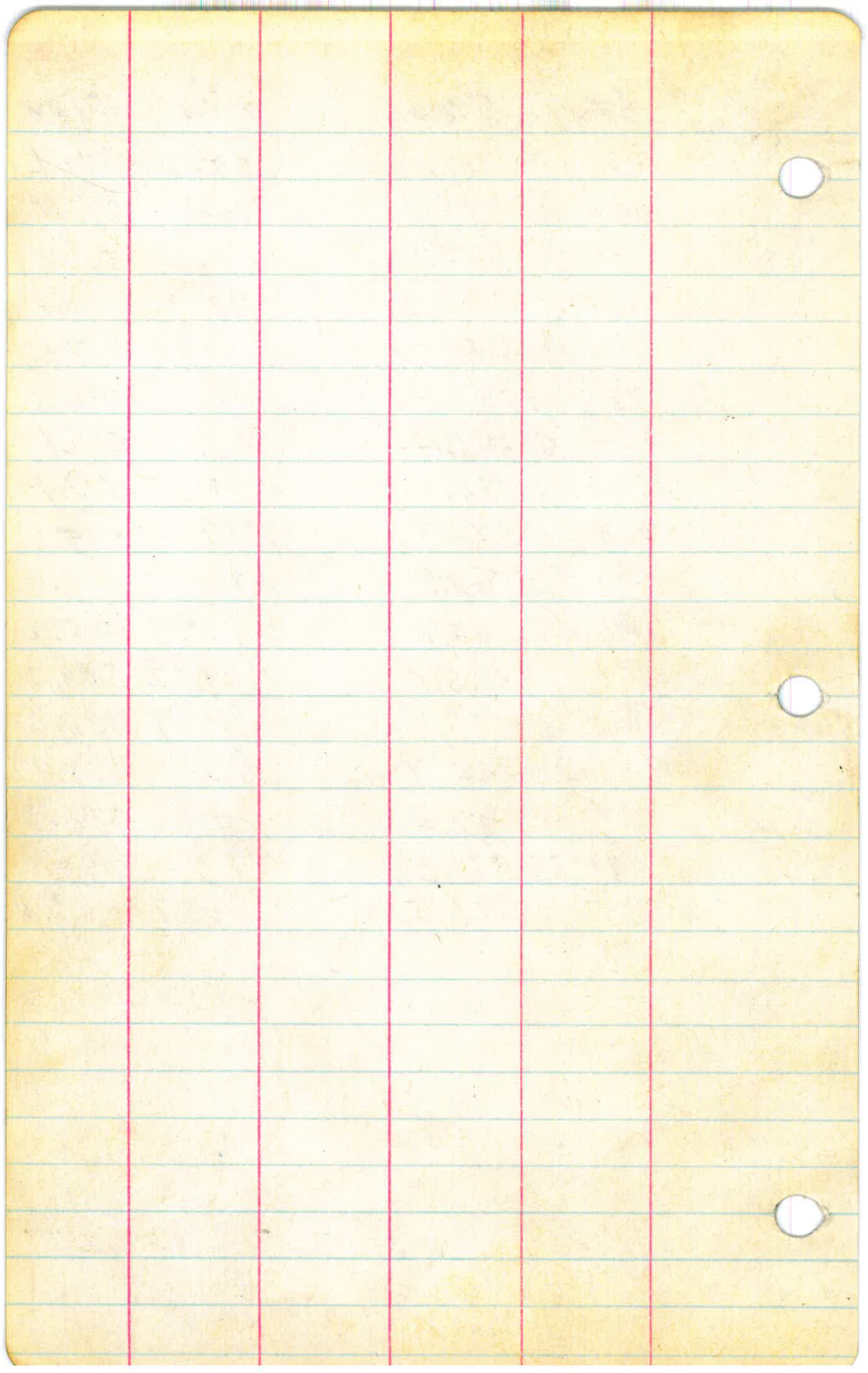
Sta.	Elev.
39+25	599.6
+60	603.7
40	602.3
+55	601.8
41	601.9
42	597.8
43	596.3
44	596.4
45	597.0
46	599.6
47	601.0
48	586.4
49	585.0
+40	583.4
50	579.0
+50	5840
51	580.2
52	580.4

-7-51

Sta.	Elev.
63+25	572.3
+82	570.2
64	569.5
+57	570.2
65	570.9
+40	575.9
+83	579.3
66	577.7
+55	579.1
67	577.6
68	572.8
69	573.0
70	576.1
97	575.8
72	573.0
73	573.0
74	571.6

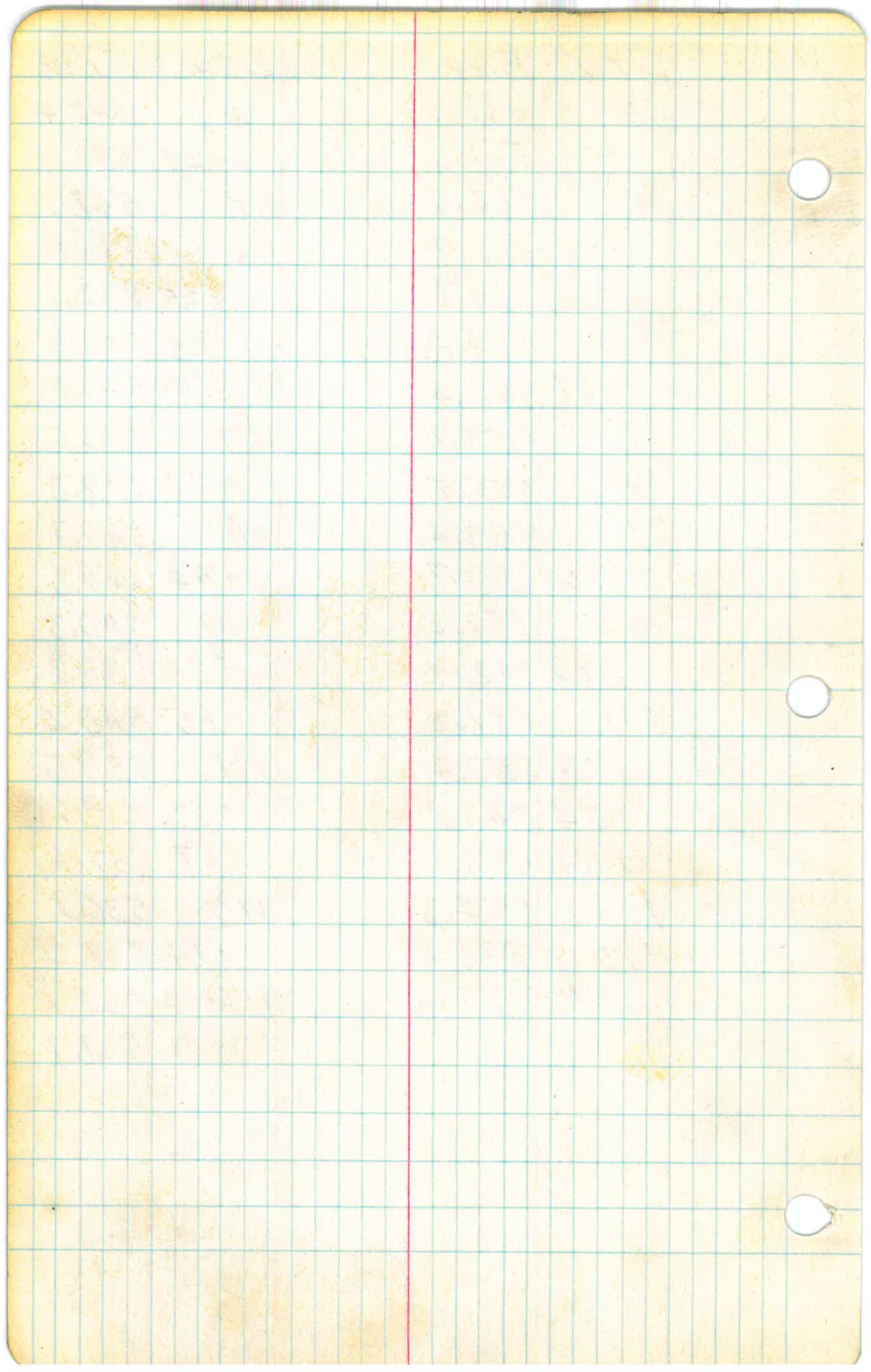


Sta.	Elev.	Sta.	Elev
74+41	572.2	85+82	571.1
75+04	571.9	86-	575.1
+46	572.6	+41	580.3
76+11	571.0	87	584.8
+22	571.2	+78	587.3
77	576.4	88	588.8
+66	573.8	89	595.6
+83	576.1	+35	597.9
78	574.9	90	595.6
79	568.8	91	584.2
80	564.4	+13	585.2
81	568.9	+52	584.2
82	565.8	+89	580.6
+80	564.9	92	579.9
83	567.4	+61	572.3
84+07.6	571.3	93	569.9
85	573.5	+52	563.4



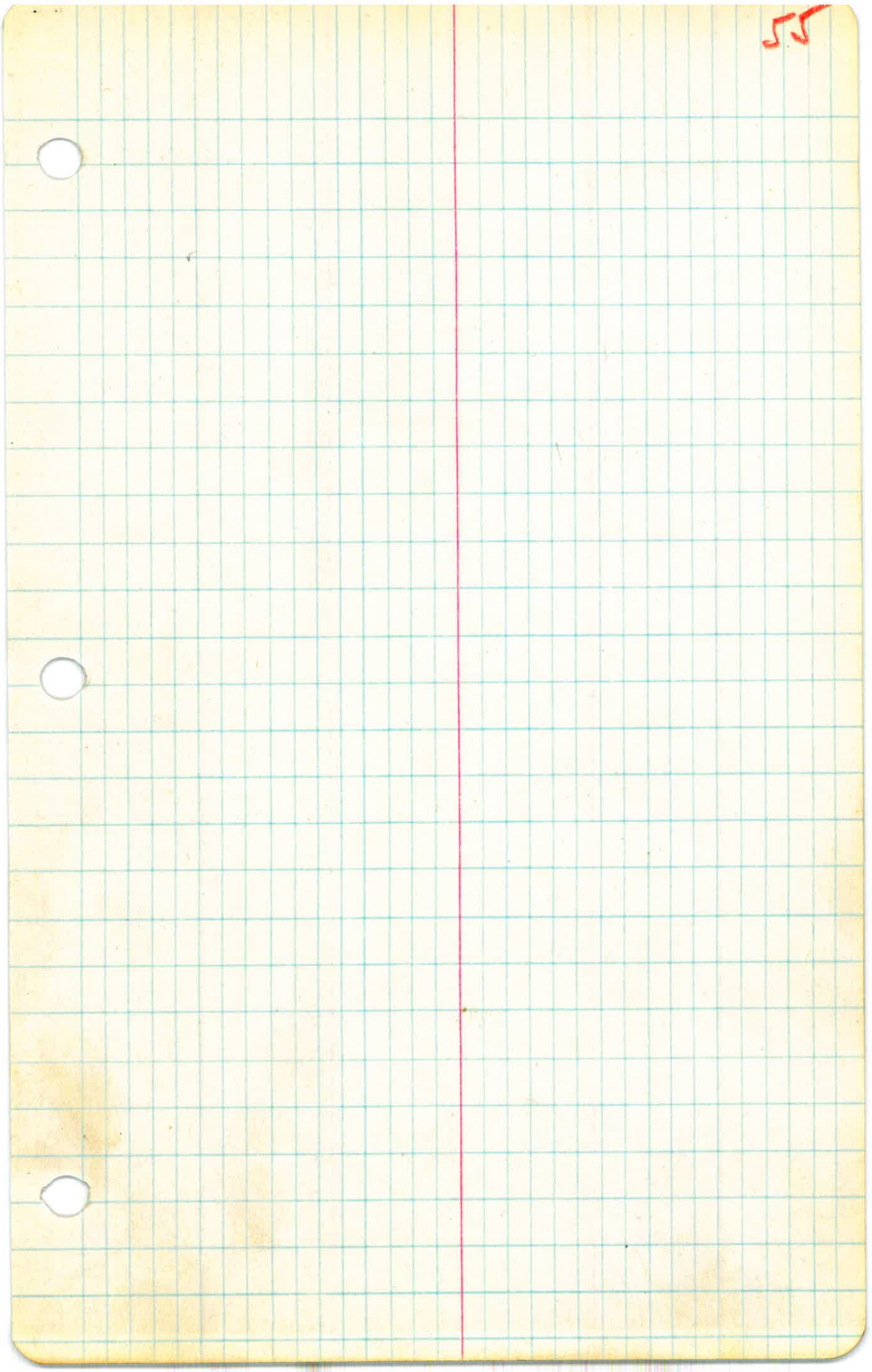
53

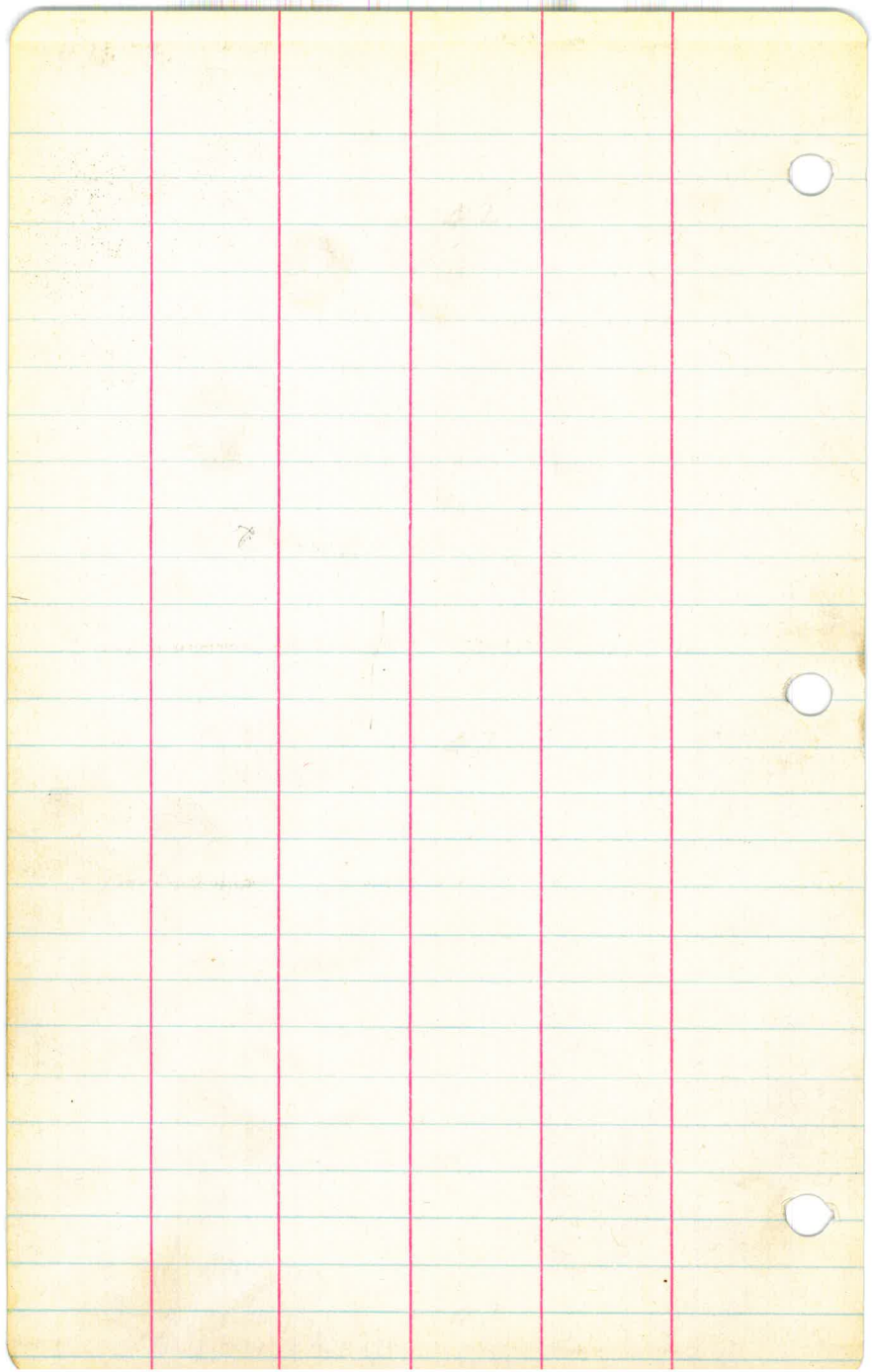
Sta.	Elev.	Sta.	Elev.
94	562.6	104	548.4
+55	561.2	+39	547.4
95	562.6	105	547.5
+58	563.9	106	545.6
+78	564.6	+25	542.1
96	564.4	+55	538.9
+67	560.4	106+85.4 = 106+81.1	540.8
97	559.2	107	543.5
98	555.5	+74	542.3
99	553.4	108	540.7
+76	552.7	+44	540.3
100	552.2	109	540.3
+76	552.9	110 +20	540.8 539.3
101	551.2	+45	540.4
+16	550.9	111	539.6
+54	549.8	+33	539.6
+91	554.6	+67	537.6
102	554.3	112	536.1
103	558.6	+74	537.0
+72	557.0	113+04	538.4
		+32	537.7



Over

Sta.	Elev.	Sta.	Elev.	Sta.	Elev.
				125+48	535.2
		113+83	539.1	126	535.6
		114	538.5	+35	533.1
		+63	539.8	+83	532.0
		+84	539.5	127	532.8
		115	539.3	128	531.9
		+65	537.5	+41	534.5
		116	537.0	+89	537.0
		+41	536.2	129	537.5
		117	536.0	+34 32 +36 21	538.5
		118	536.7	130	537.4
		+50	538.8	+41	528.2
		119	539.4	131	539.2
		+83	535.4	132	534.8
		120	534.2	13 +40	535.6
		+19	535.3	133	547.3
		+54	534.9	+45	548.2
		121	534.8	+79	547.2
		122	535.8	134	546.8
		+18	535.7	+73	547.0
		123	533.7	135	548.6
		+83	540.6	+36	549.4
		124	540.9	136	549.7
				+60	547.5
		+39	540.3	137	545.5
		+94	538.1	138	540.0
				0+57	539.4

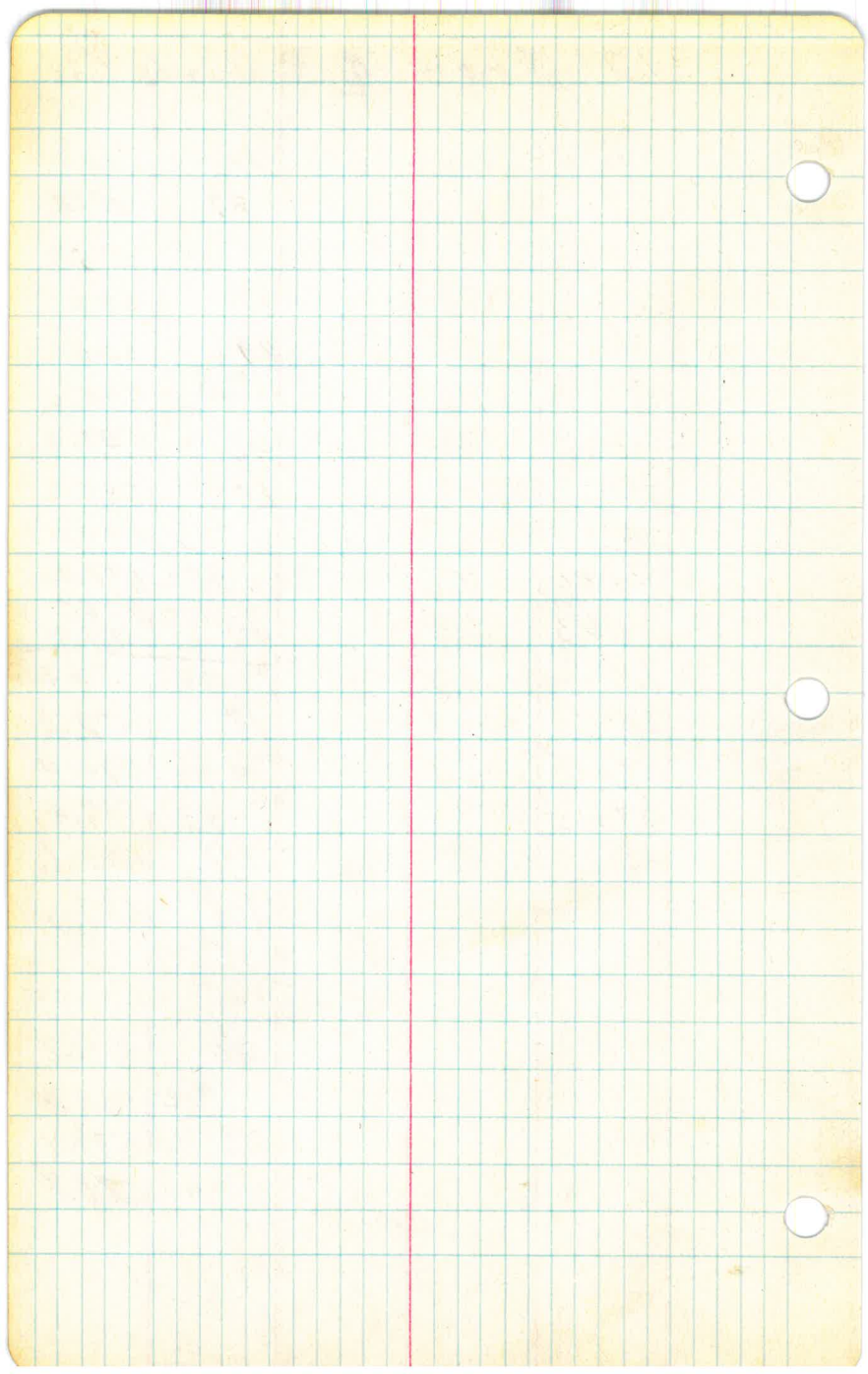




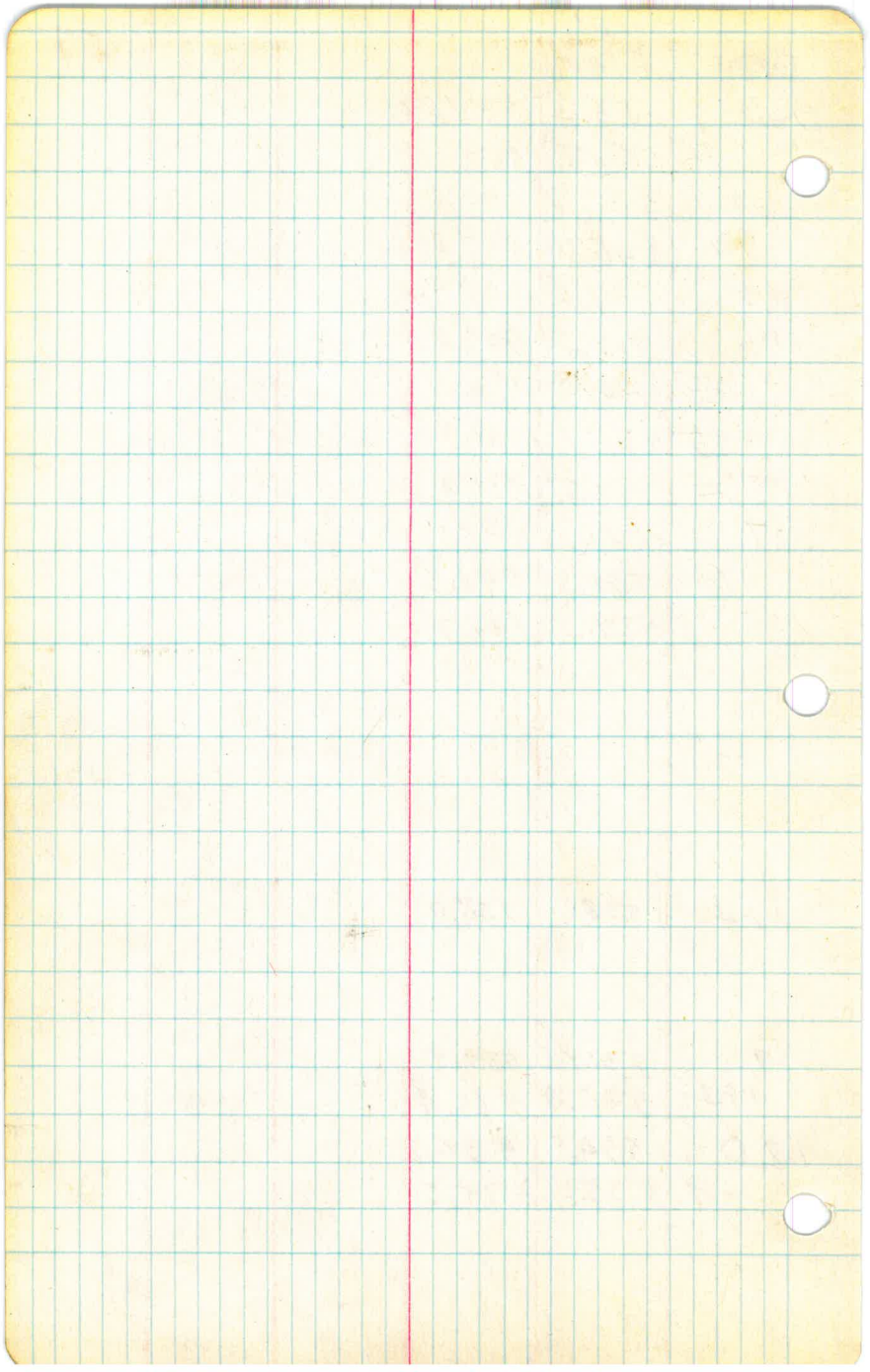
10' from ℄ Richards Road

Sta	Elev
21	621.2
21+16	617.7
22	618.8
+60	611.1
23	610.9
+38	619.6
24	611.7
25	612.4
+29	607.6
+63	604.4
26	606.3
26+64	608.1
27+	606.1
27+53	599.6
28	600

Sta	Elev
87	582.8
+78	585.0
88	586.6
89	590.6
+55	595.6
90	593.4
91	580.2
+13	579.4
+52	581.2
92 +89	776.3
	575.9
76+22	570.2
77	572.4
+66	571.4
+83	569.4
78	570.6
79	567.3
85	571.8
+82	569.8
86	571.7
+41	578.8



Sta.	Elev	
103	553.2	558.6 ℄
+72	550.2	557.0 ℄
104	545.6	548.4 ℄
+39	546.7	547.4 ℄
105	542.9	547.5 ℄
106	539.4	545.6 ℄
+25	538.5	542.1 ℄
+55	538.8	538.9 ℄
106+85 = 11	539.3	540.8 ℄
107	540.0	543.5 ℄
+74	540.3	542.3 ℄
108	539.3	540.7 ℄
114	5385	538.0
19	538.9	539.4
+83	535.0	535.4
120	534.5	534.2
+19	535.1	535.3
12		



80

Tie from P.I. #63. Sta. 138+05.57 Richards Road Survey to El Capitan "A" Line Survey. Also Tie from El Capitan "A" Line Survey to East Line El Monte Rancho.

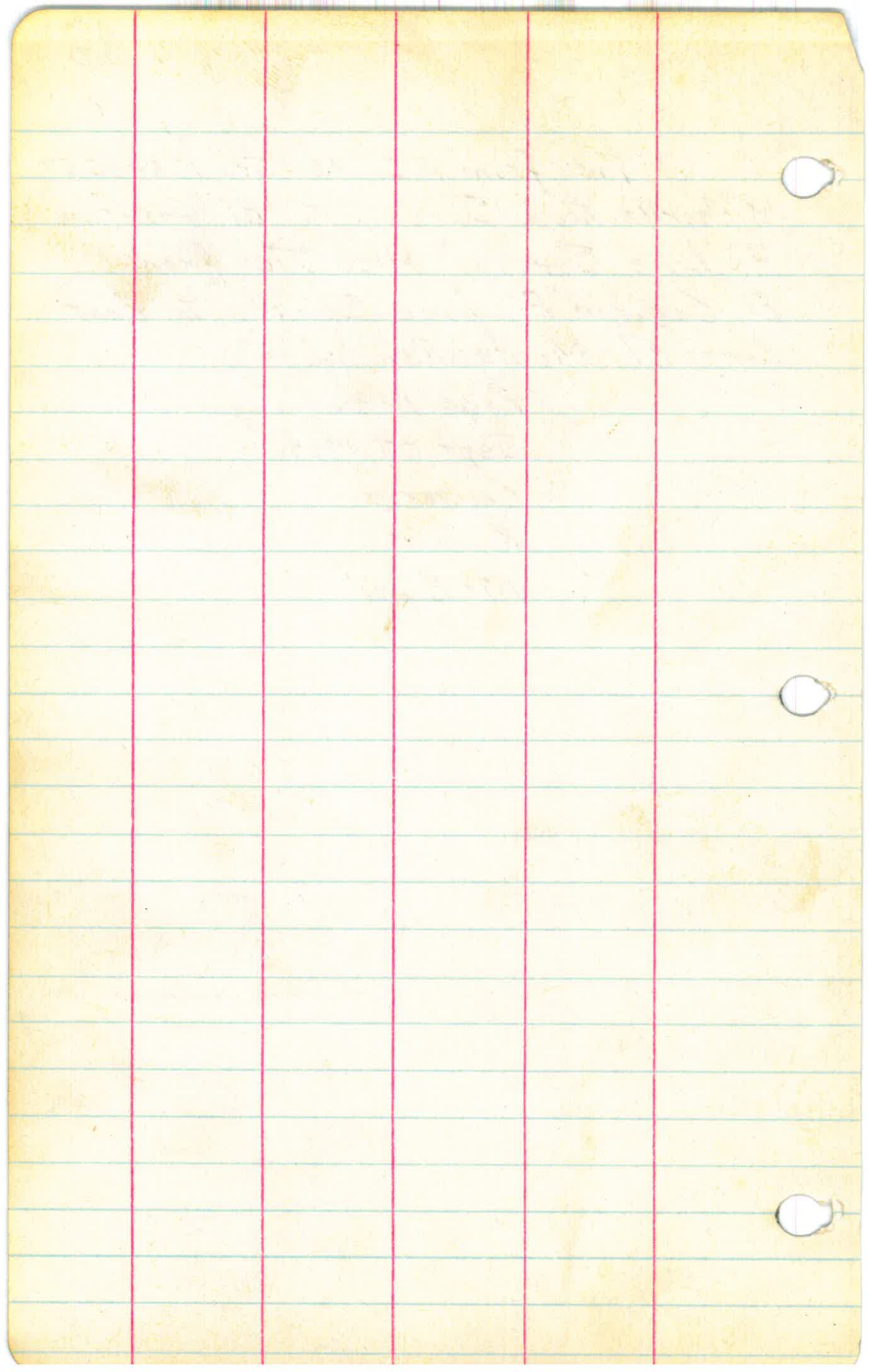
Page 1-3.

Sept. 27. 1927.

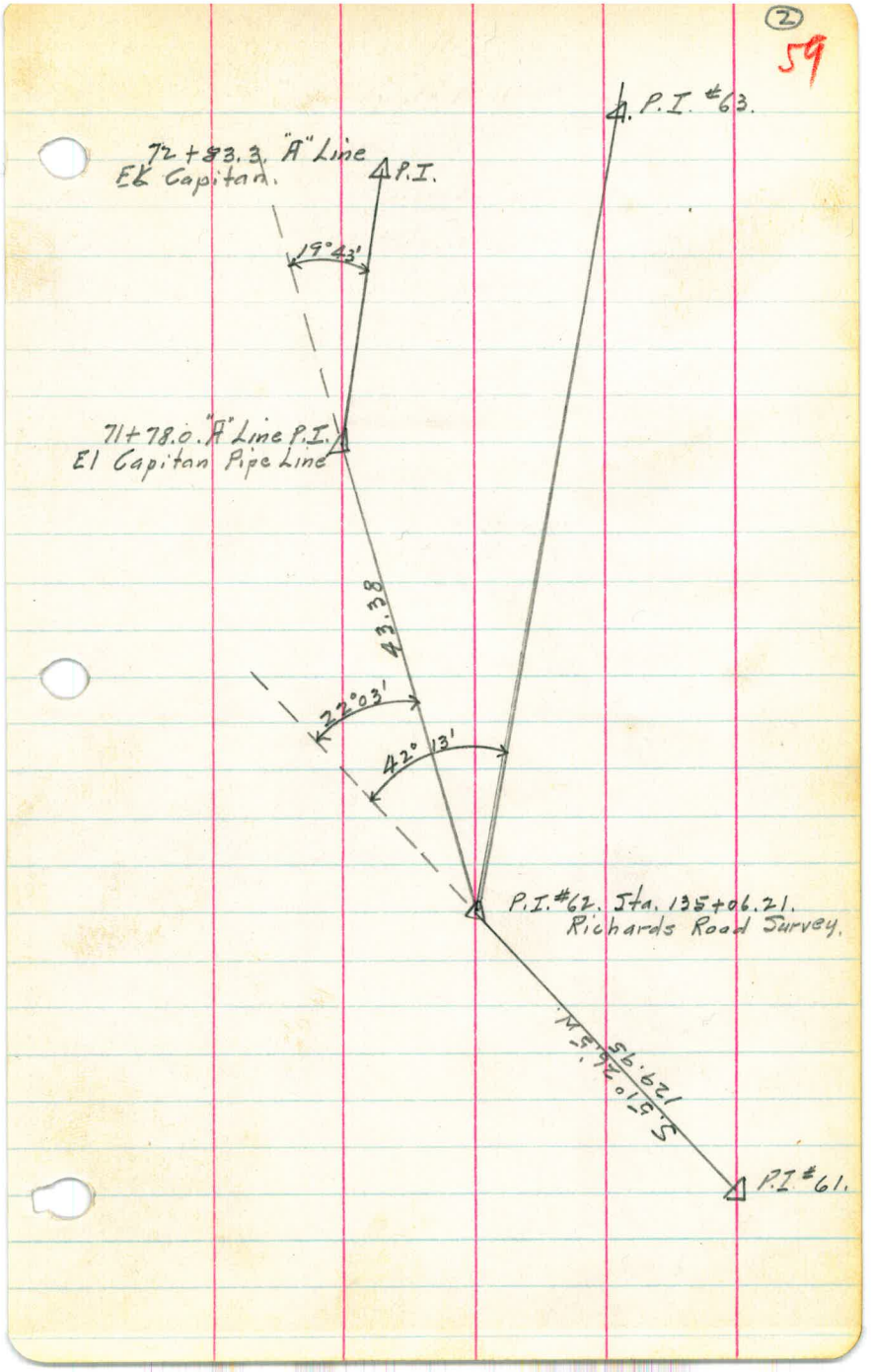
Converse

Rauner

Mc Bain.

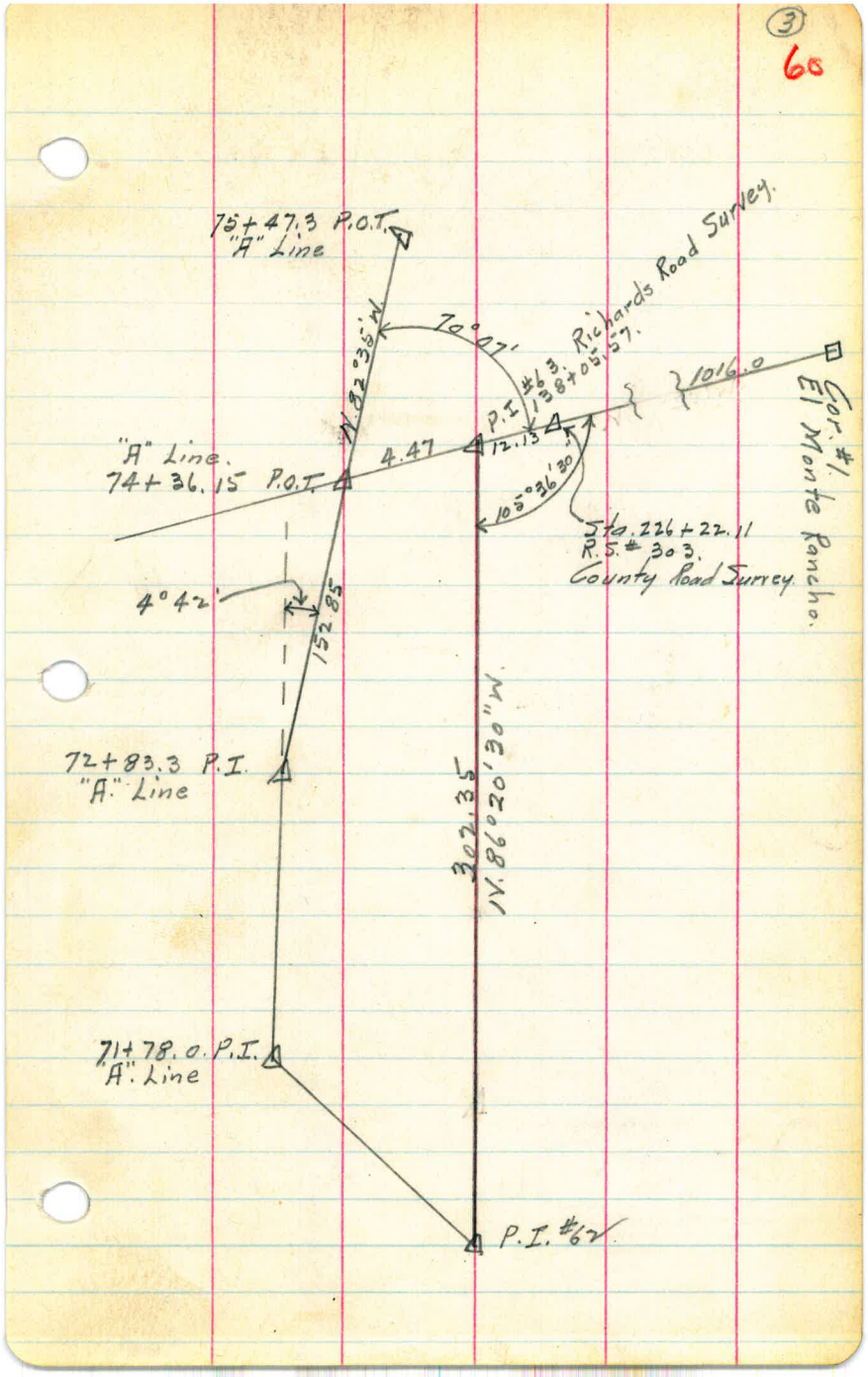


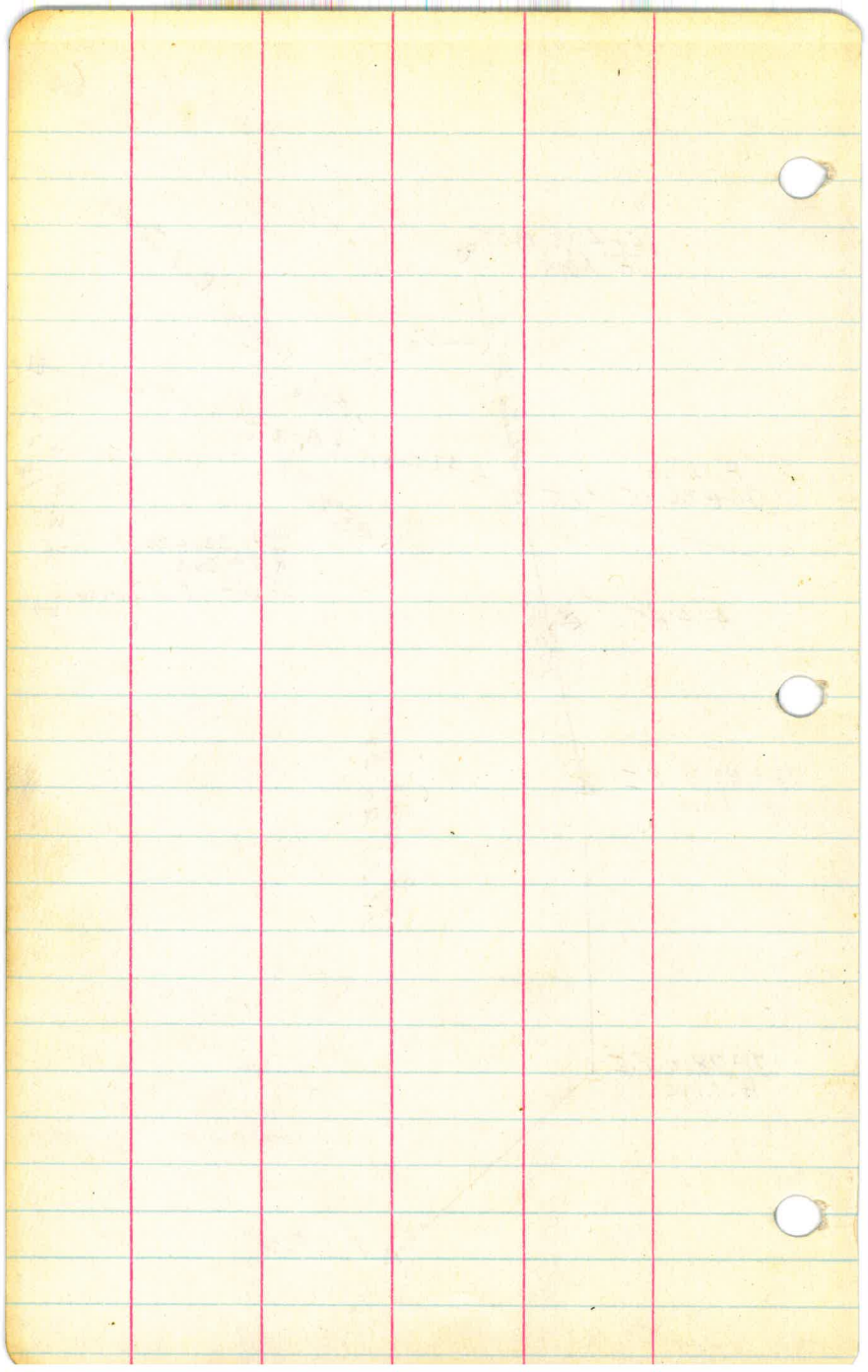
59


72+83.3. "A" Line
E& Capitan.
P.I.
19°43'
71+78.0. "A" Line P.I.
El Capitan Pipe Line
43.38
22°03'
42° 13'
P.I. #63.
P.I. #62. Sta. 135+06.21.
Richards Road Survey.
S 51° 45' W
129.95
P.I. #61.

72 + 833
1 52 85
74 36 15

82° 35' W
70 07
12 28


75+47.3 P.O.T.
"A" Line
N.82°35'W.
10°07'
Richards Road Survey.
P.I. #63
138+05.57
1016.0
Cor. #1
El Monte Rancho.
"A" Line.
74+36.15 P.O.T.
4.47
12.13
10°36'30"
Sta. 226+22.11
R.S. #303.
County Road Survey.
4°42'
R
152.85
72+83.3 P.I.
"A" Line
302.35
N.86°20'30"W.
71+78.0 P.I.
"A" Line
P.I. #62



Ties between Traverse of
160 foot Contour on El Capitan
Reservoir Survey, and Temporary
Axis of El Capitan Dam #3, in
Indian Reservation.

Sept. 12. 1927.

Conreirse

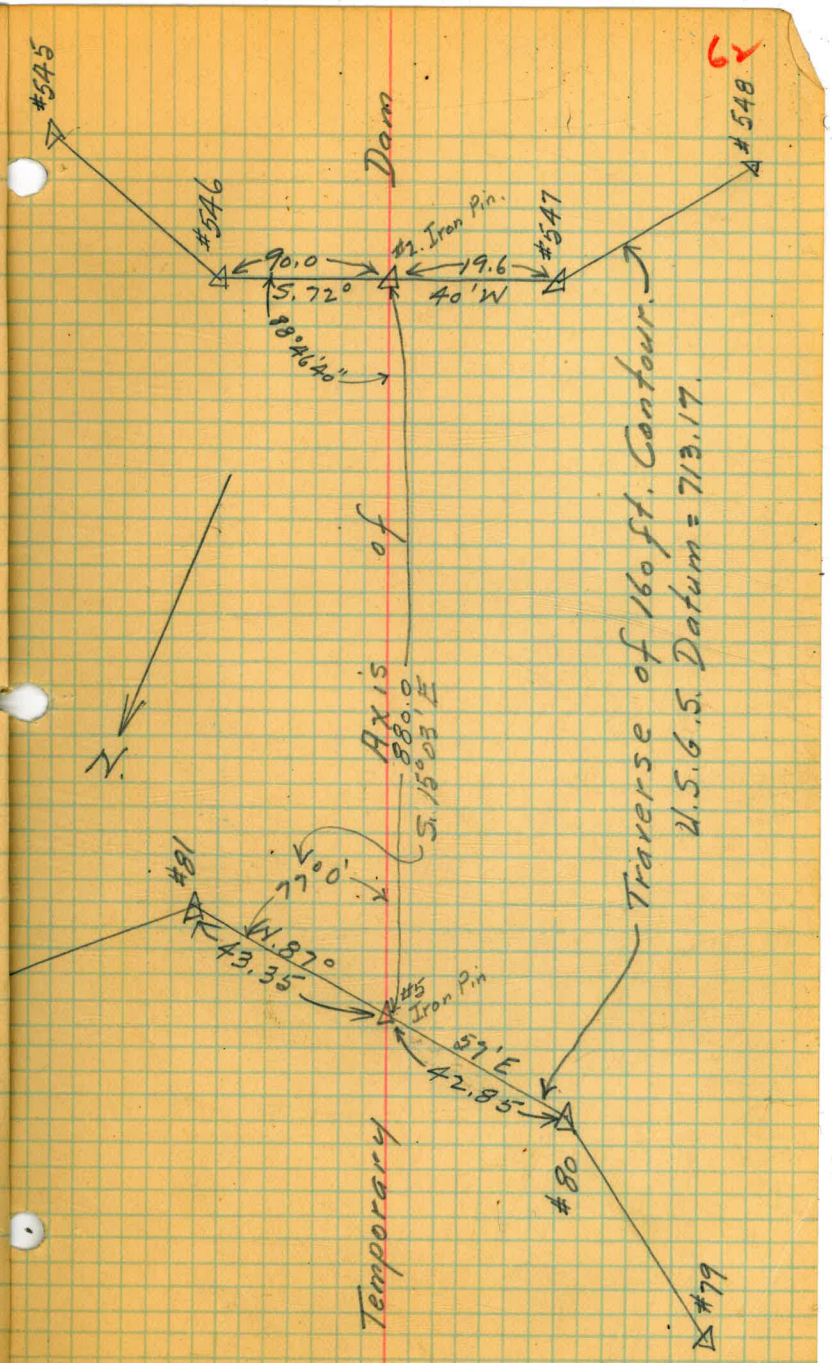
Rauner

Mc Bain.

Sept. 12. 1927.

88°47'
3 (266°20'
88°46'40"

77°0'
3 (231°0'
77°0'



Location of Points on Temporary
Axis of El Capitan Dam #3, also
Elevations on Same.

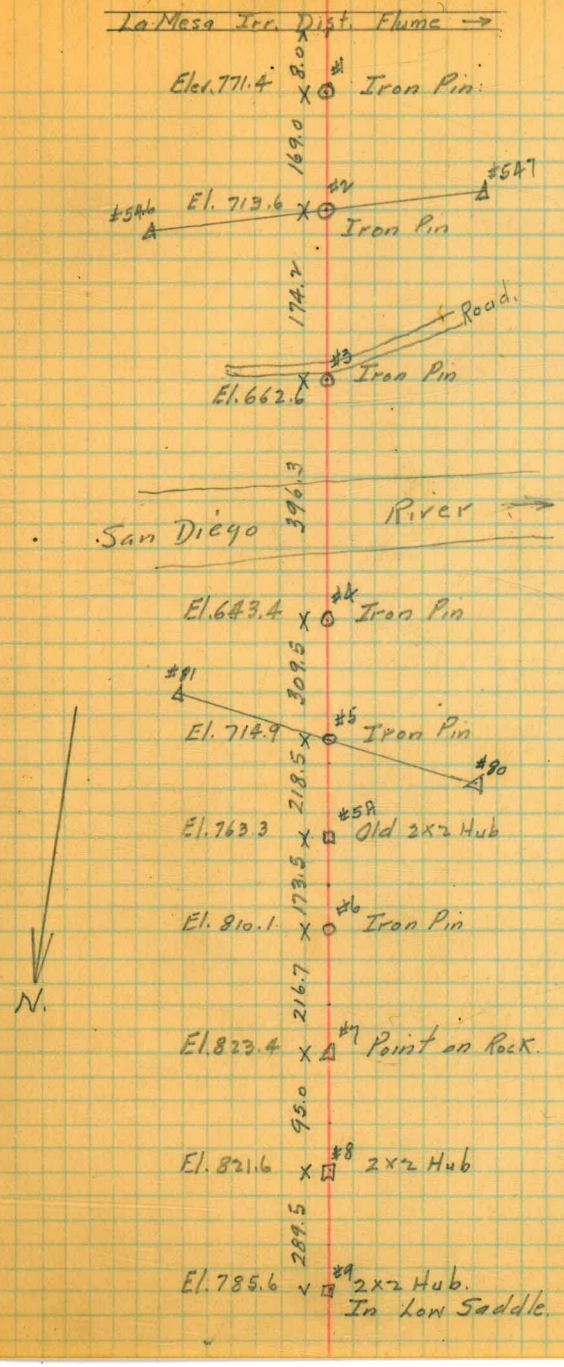
Sept. 13. 1937.

Converse

Rawner

Mc Bain.

Note- These distances are by Stadia.
Elevations are by Vertical Angles
calling #80 and #81 on Contour Survey
Elev. 713.17.



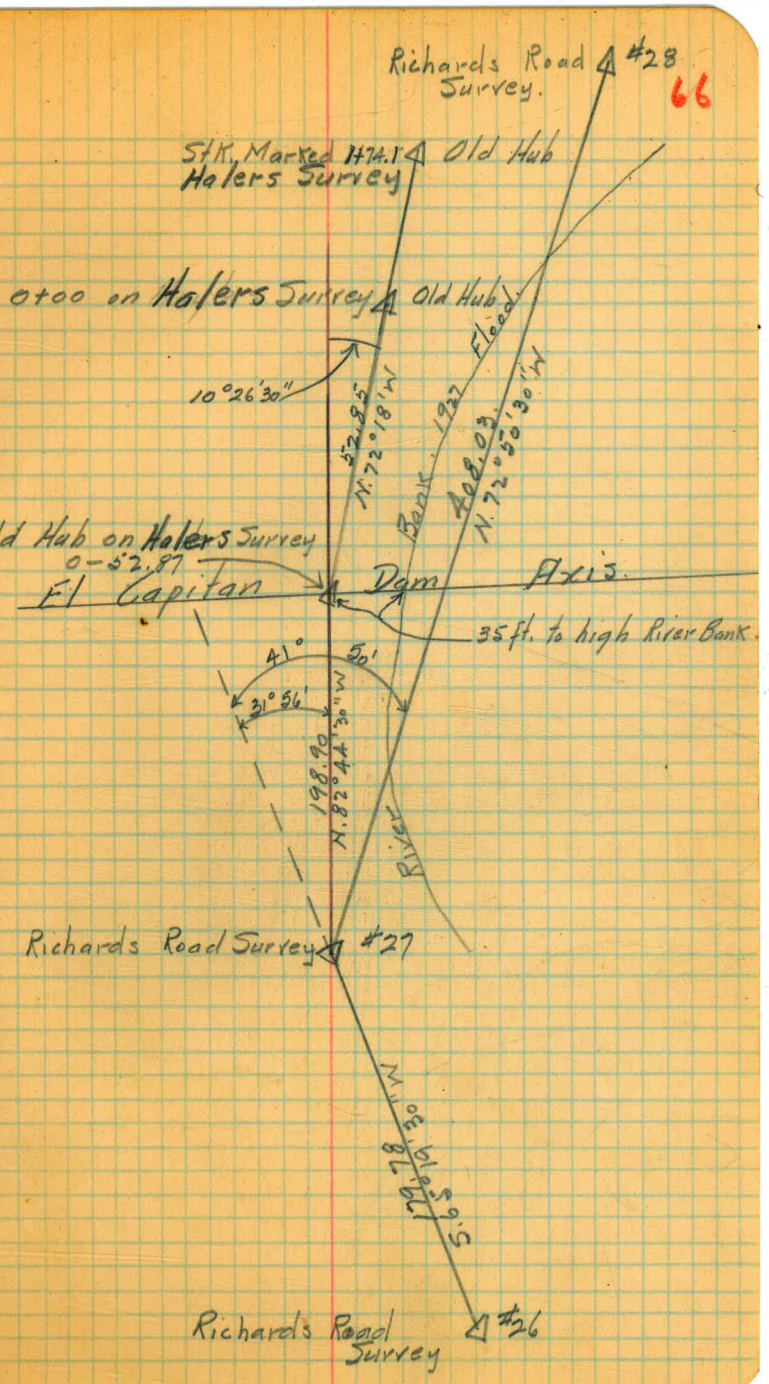
Tie between Richards Road Survey and Halers Survey for El Capitan Pipe Line, at El Capitan Dam.

Sept. 14. 1927.

Converse

Rauner

McBain.


Richards Road Survey. #28
S.K. Marked 174.1 Holers Survey
Old Hub
0+00 on Holers Survey
Old Hub
10°26'30"
52.85'
N. 72°18' W
Bank of 1927 Flood
408.03'
N. 72°30'30" W
Old Hub on Holers Survey
0-52.87
El Capitan
Dam
Axis.
35 ft. to high River Bank.
41°
50'
31°56'
N. 82°44'30" W
198.90
River
Richards Road Survey #27
N. 16°30' E
278.78'
S.S.
Richards Road Survey #26

(1)
67

Preliminary Survey for
Pipe Line from El Capitan
Dam Site #3. to Stg. 2786.78 E.C.
on Richards Road Survey
up the San Diego River.
Sept. 1927.
Converse
Rauner
McBain
Pages 1-16.

Sta. Hor. Δ Dist. Bearing Mag.

Stadia Dist. Pin #3 to 0+00 = 59.0.

Vert. Δ = -29°49'

Stadia Dist. 0+00 to Pin #4 = 347.0

Vert. Δ = +1°04'

1+71.39 P.O.T.

272.33'

S55°15.0'W S.40°50'W

Δ 0+27.67 L.48°35.5'

27.67'

N76°09.5'W S.89°30'W

131°24'
525°38'
131°24'

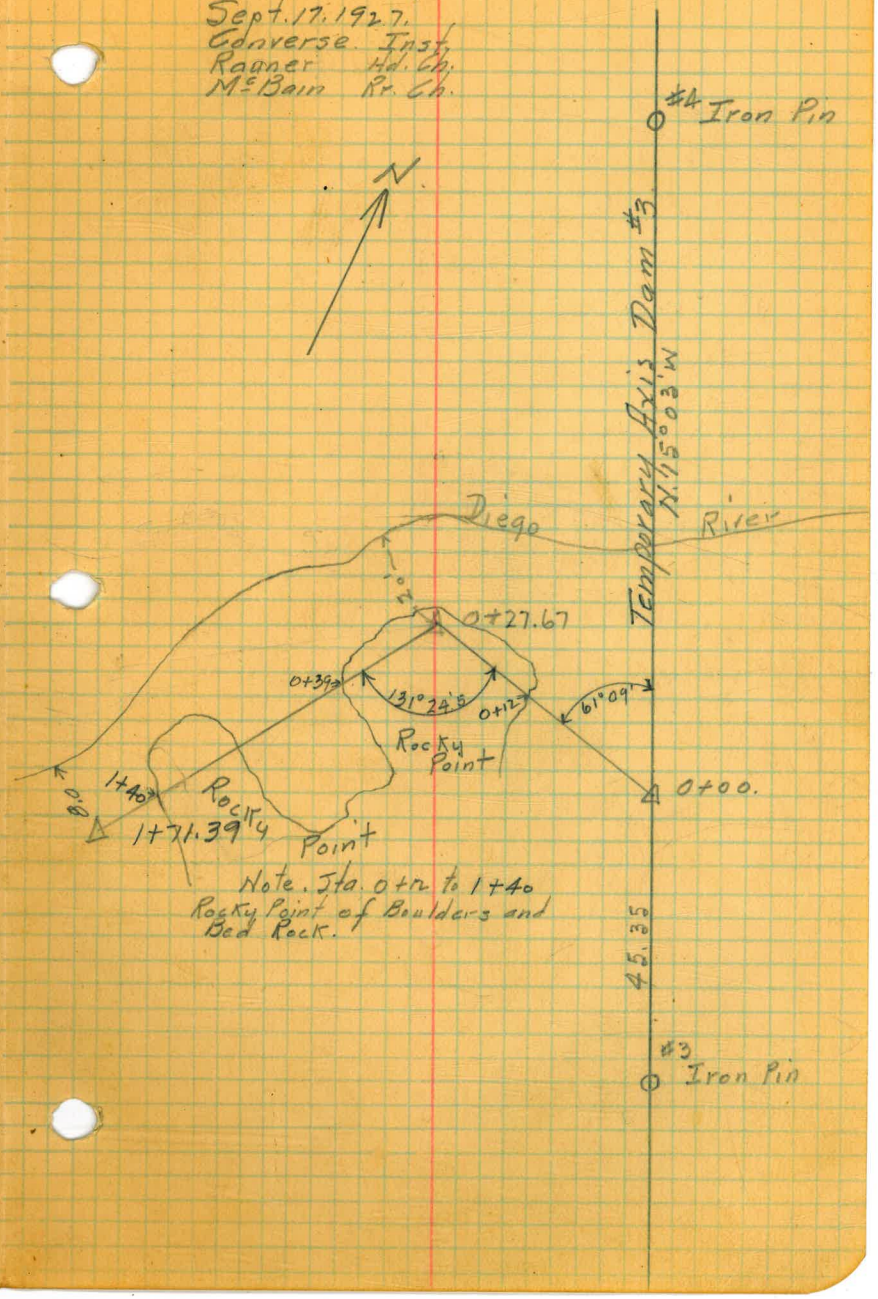
Δ 0+00 L.61°09'

N15°00.5'W N.29°0'W 61°09'

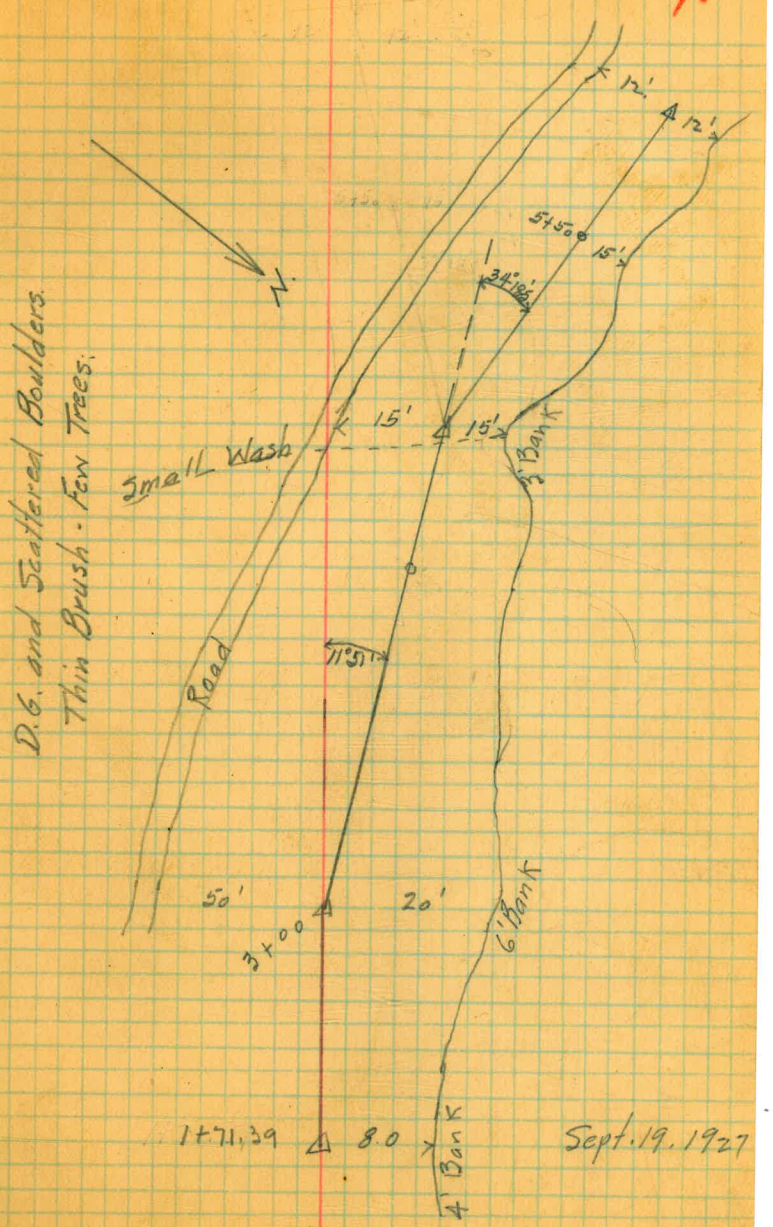
244°36'
61°09'

Note - These Bearings carried backwards from Tangent on Richards Road Surrey

Sept. 17. 1927.
Converse Inst.
Ragner Hd. Ch.
McBain Rr. Ch.



Sta.	Hor. Δ	Dist.	Bearing. Mag.
6+63	Δ		
		188.0'	N78°35.5'W S.87°20'W
4+75	Δ 34°18.5 R		
		175.0'	S67°06.0'W S.52°40'W
3+00.	Δ 11°51' R.		
		272.33'	
1+71.39	P.O.T.		S55°15.0'W

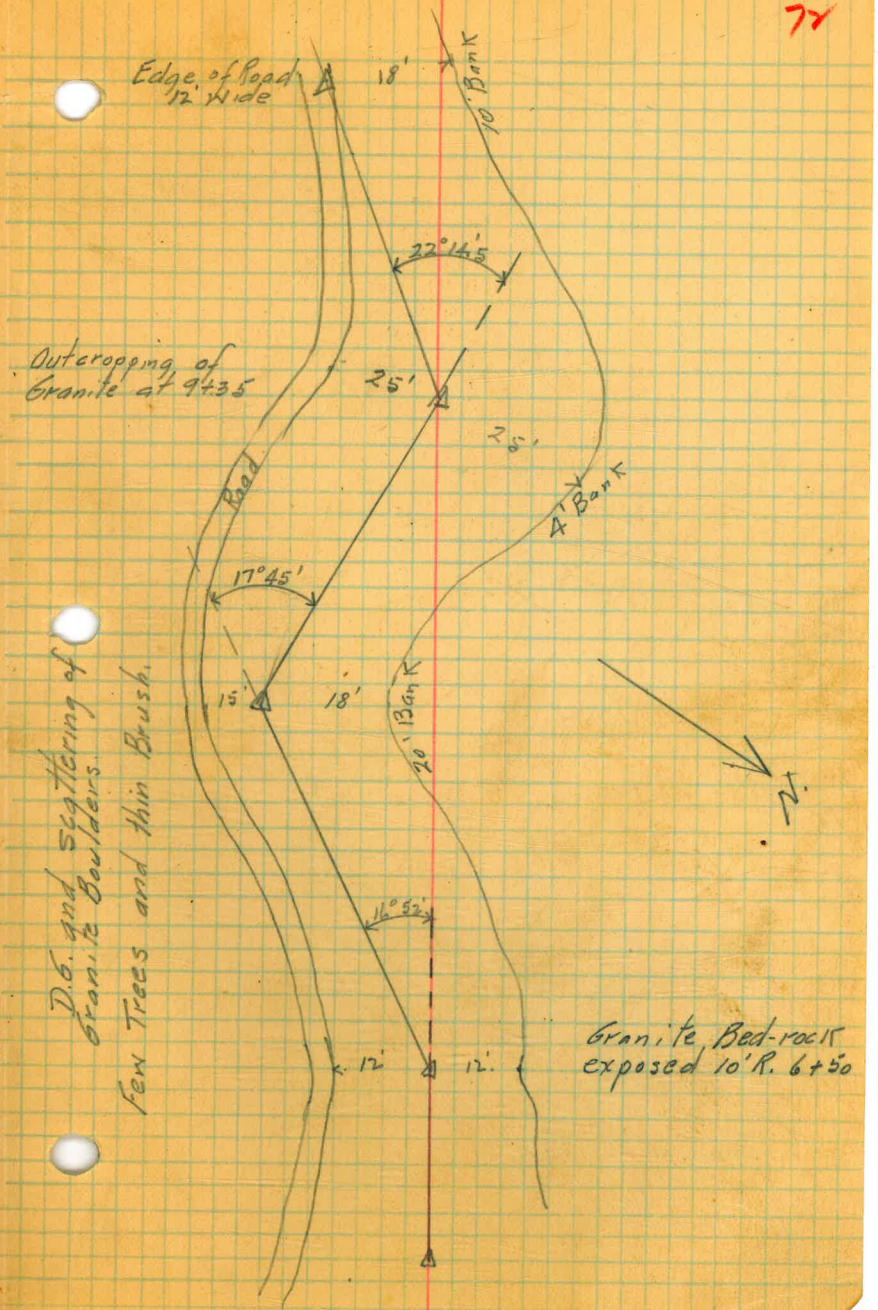


Sept. 19, 1927

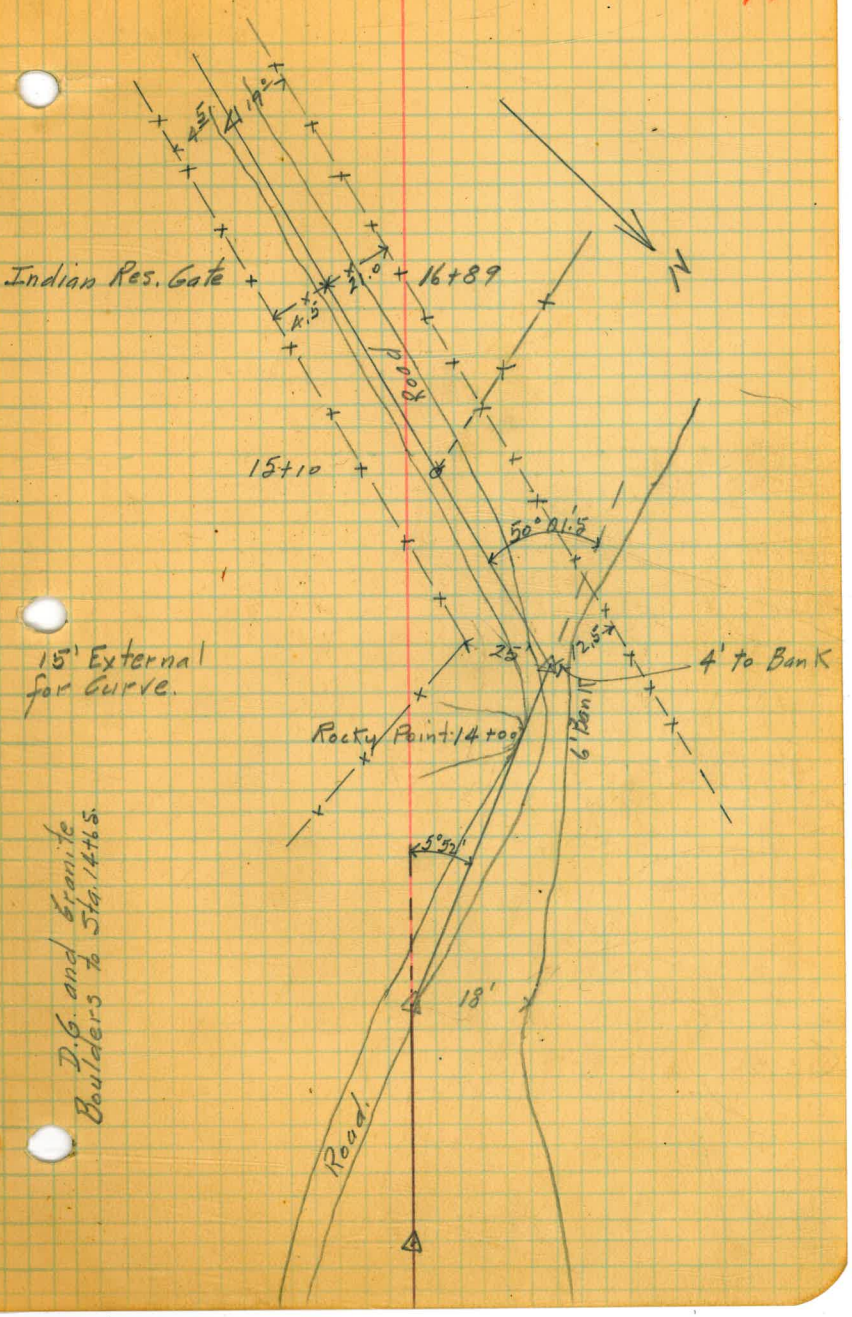
(5)

71

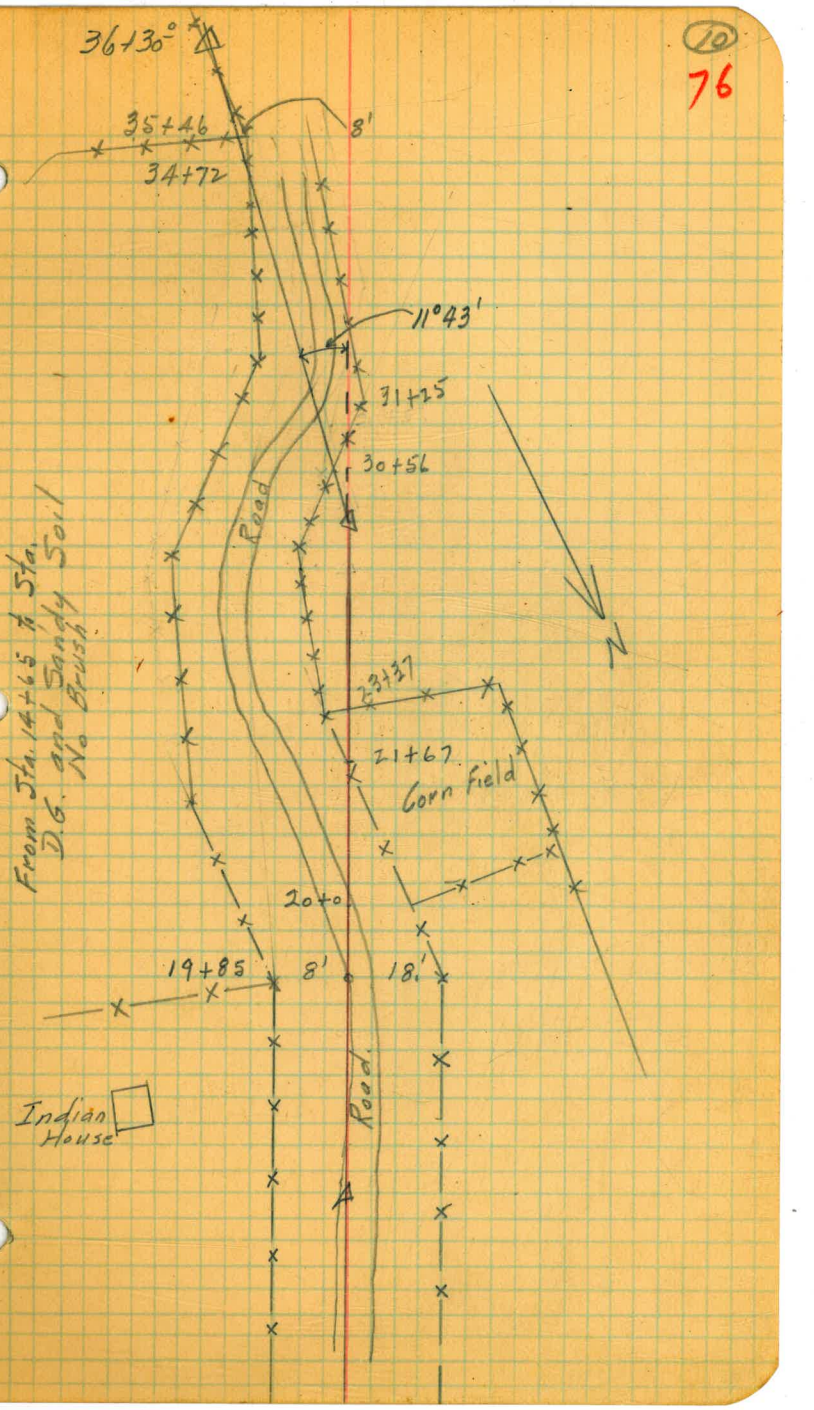
Sta.	Hor. Δ.	Dist.	Bearing	Mag.
10+45	Δ			
		110.0'	S80°03'W	5.66°00'W
9+35	Δ 22°14.5 L			
		160.0'	N77°42.5W	5.88°30'W
7+75	Δ 17°45' R			
		112.0'	S84°32.5'W	5.70°20'W
6+63	Δ 16°52' L			
		188.0'	N75°35.5W	
4+75				



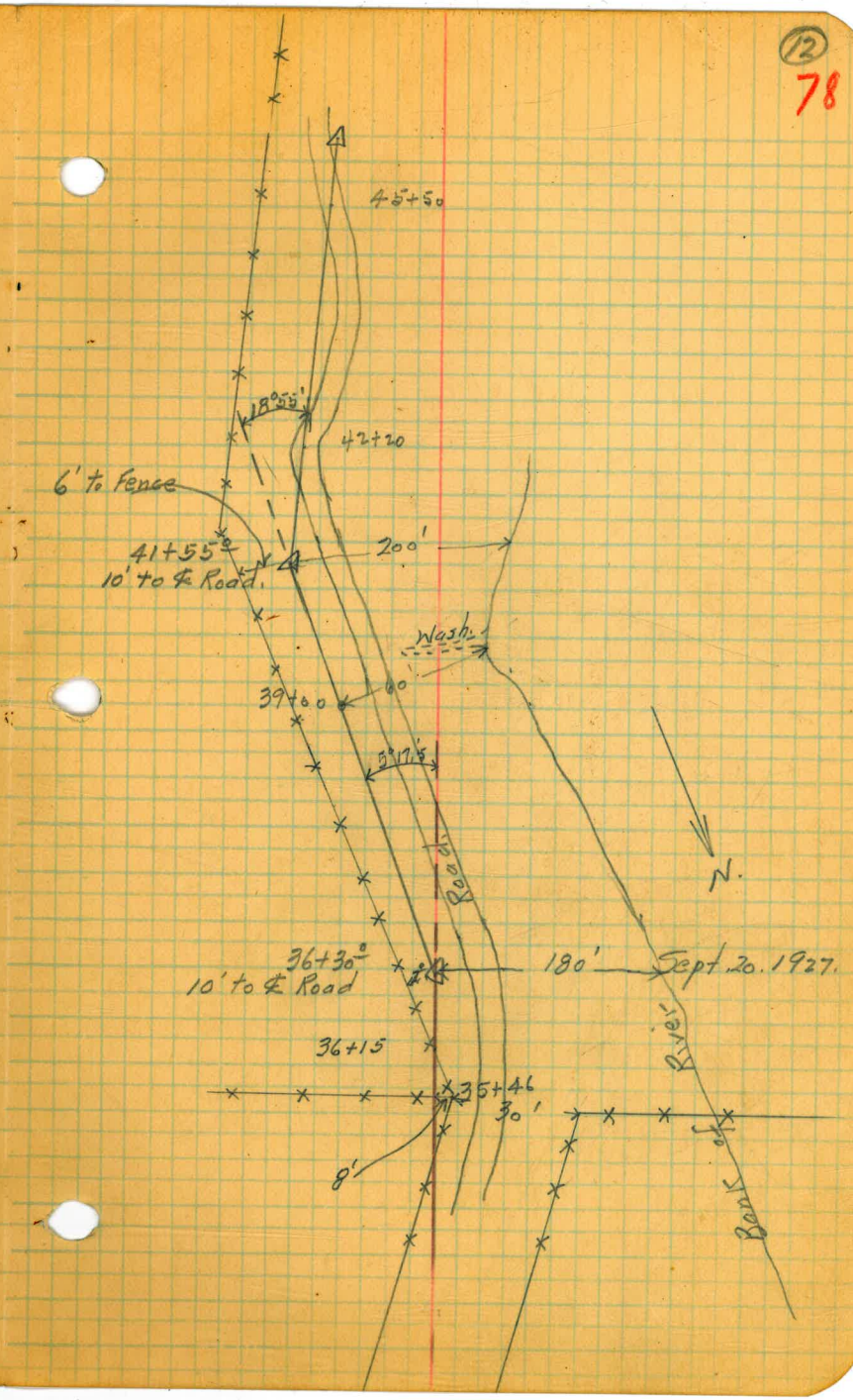
Sta.	Hor. Δ	Dist.	Bearing.	Mag.
17+65 P.O.T.				
		1535.0'	S35°53.5'W	5.21°20'W
14+65	Δ 5°01.5' L.			
		420.0'	S85°55'W	5.71°40'W
10+45	Δ 5°52' R			
		110.0'	S80° 03.0'W	5.66°0'W
9+35	Δ			



Sta.	Hor. Δ	Dist.	Bearing.	Mag.
		630.0'	S24°10.5'W	S.9°30'W
30+00	Δ 11°43'L.			
		1535.0'		
17+65	P.O.T.			



Sta.	Hor. Δ	Dist.	Bearing	Mag.
45+75 = Δ			S60°45'W	
		420.0		
			S37°45'W	S.23°20'W.
41+55 = Δ	18°55'R.		S37°45'W	
		525.0		
			S18°53'W	S.4°20'W
36+30 = Δ	5°17.5L.		S13°35'W	
		630.0'		
			S24°10.5'W	
30+00 = Δ			S24°10.5'W	

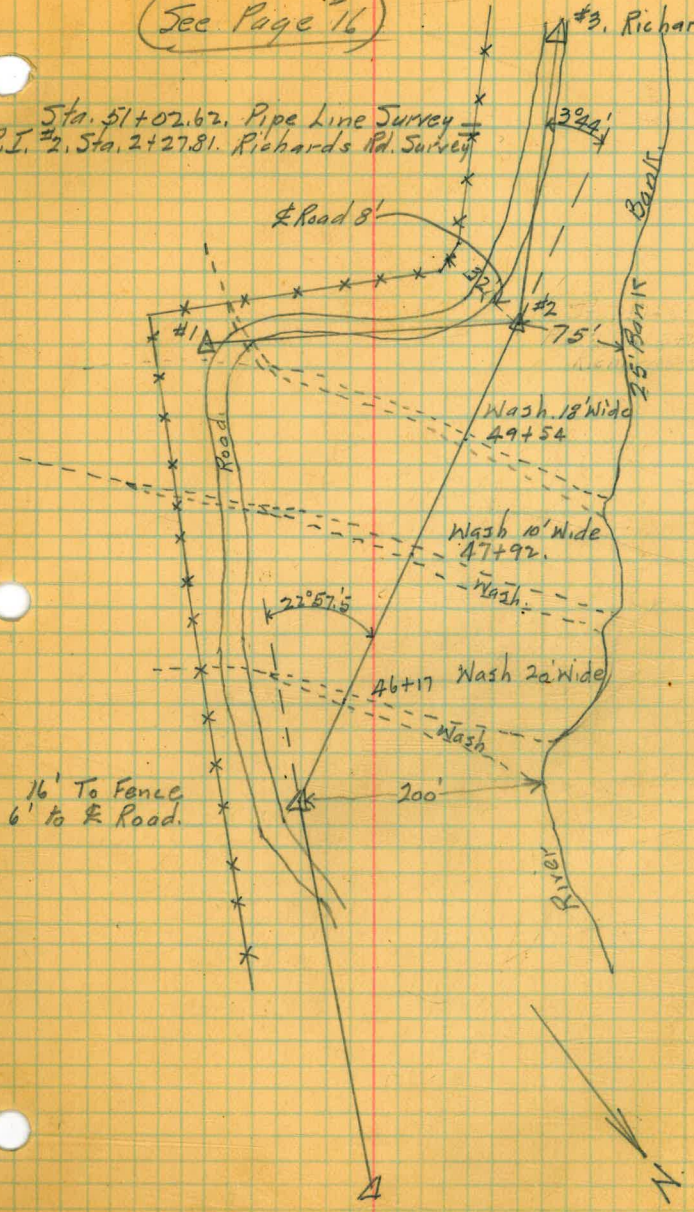


(13)
79

Sta.	Hor. Δ	Dist.	Bearing	Mag.
54+05.68= P.I. #3.				
			S57°01.5'W	S.42°45'W
51+02.62	Δ=3°44' L.			
P.I. #2.				
		527.62'		
			S60°45.5'W	S.46°30'W
45+75°	Δ 22°57.5 R.			
			S37°48.0'W	
41+55°				

(See Page #16)

= Sta. 51+02.62. Pipe Line Survey
= P.I. #2. Sta. 2+27.81. Richards Rd. Survey



(15)
81

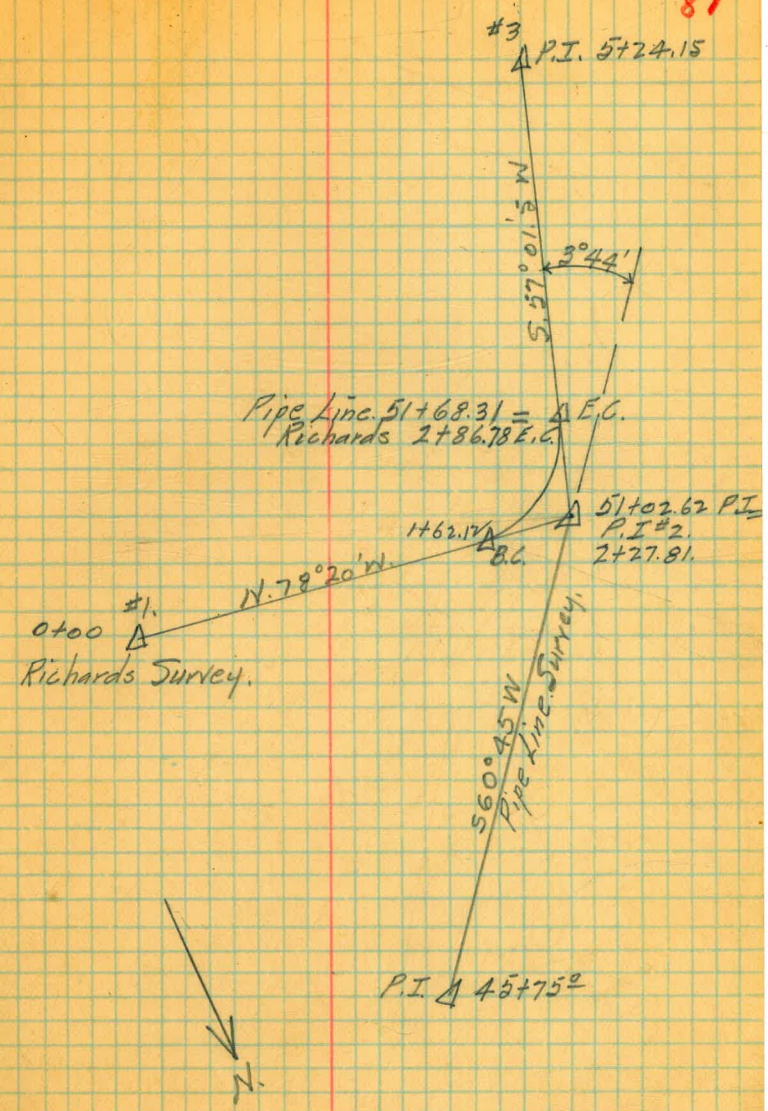
Richards Curve Data.

P.I. #2. $\Delta = 44°38'5$

$R = 160$

$T = 65.69$

$L = 124.66$



83

A Copy of Richards Notes of re-location of El Capitan Road.

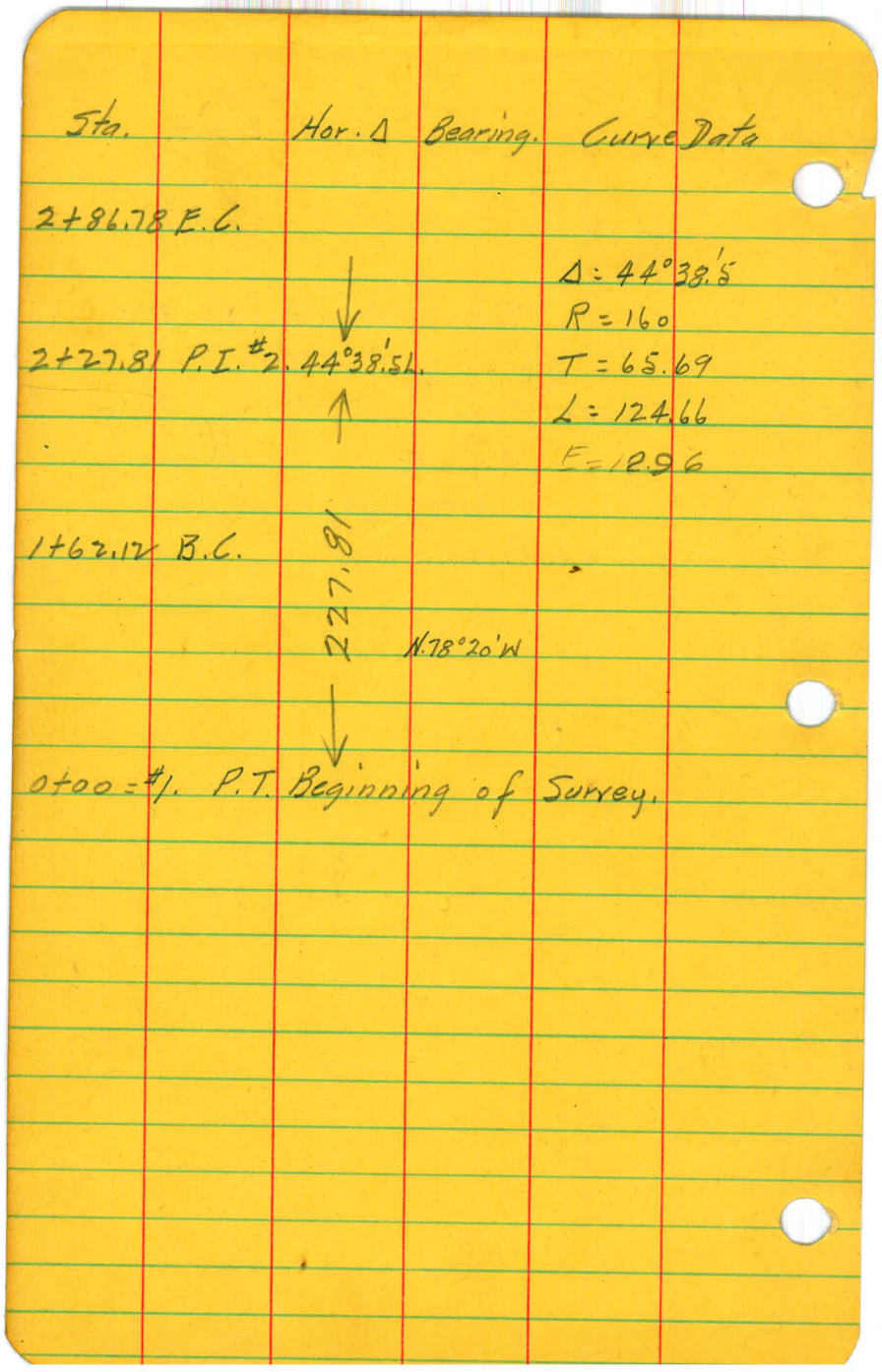
County Survey Number = R.S. 389.
(Formerly O.S. #56.)

County Field Book #113 and #113A.

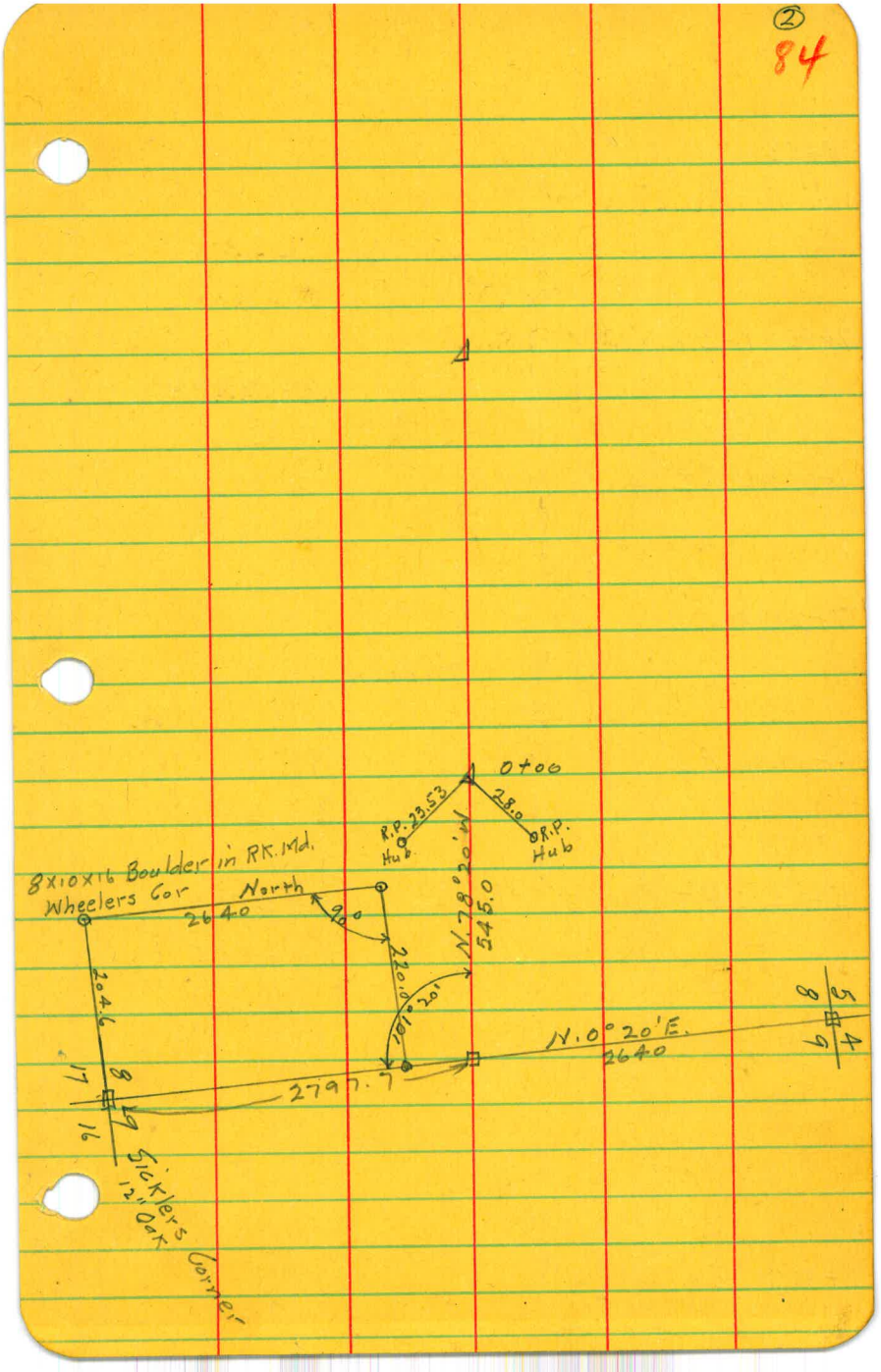
Copy by Converse.

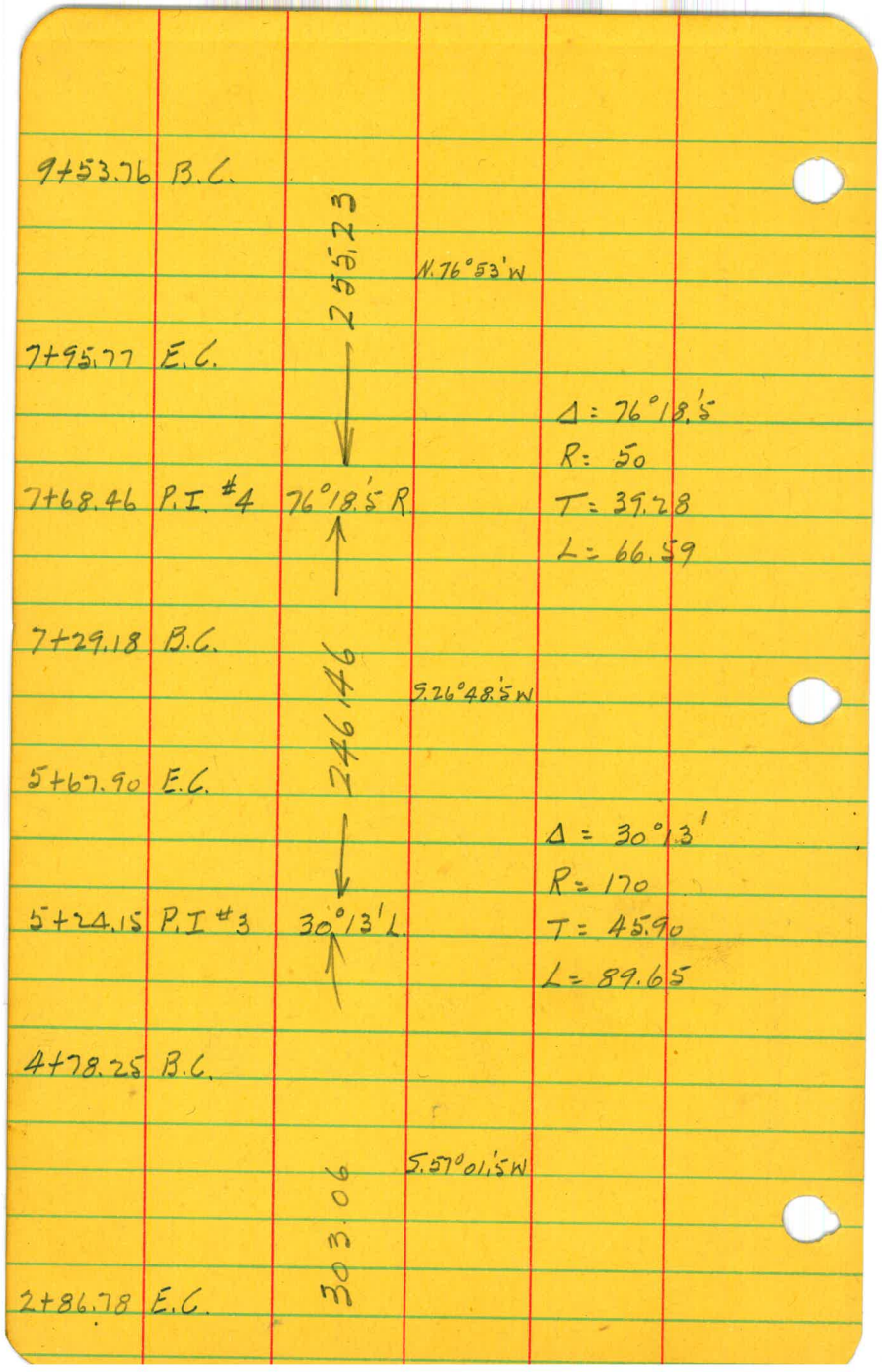
Sept. 22. 1927.

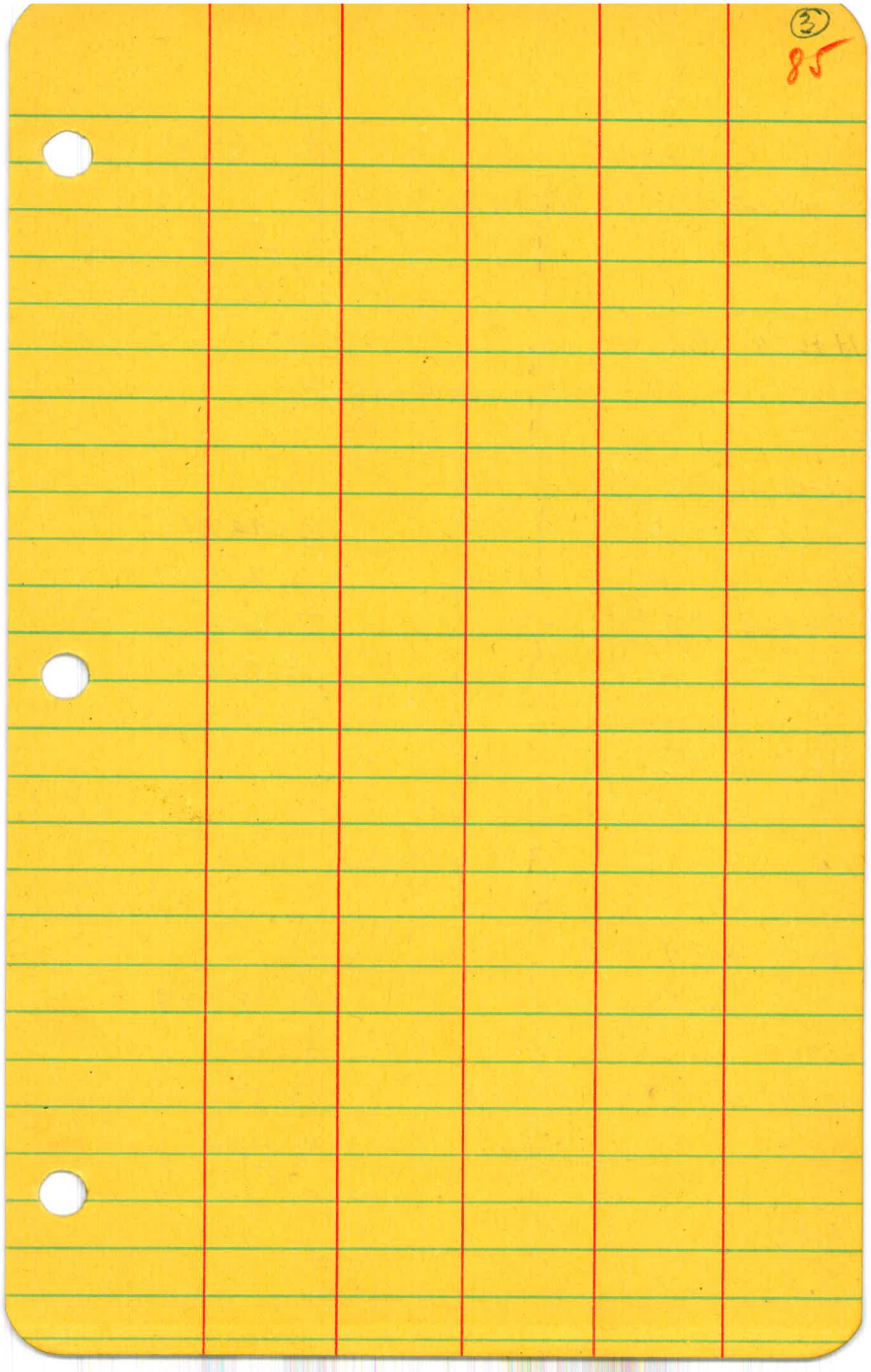
Page 1 - 21.

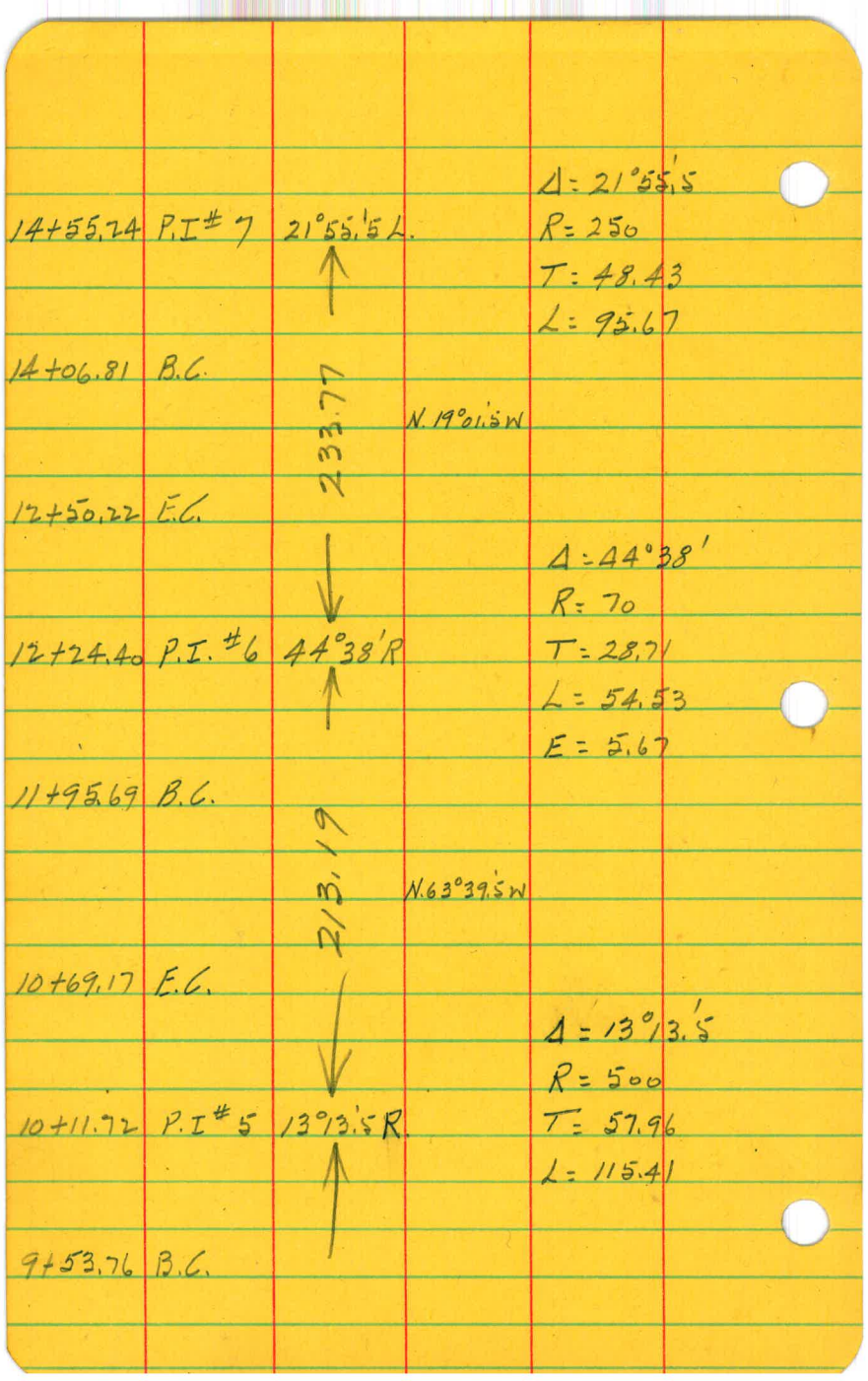

Sta.
Hor. Δ
Bearing.
Curve Data
2+86.78 E.C.
Δ = 44°38.5'
R = 160
2+27.81 P.I. #2. 44°38.5'L.
T = 65.69
L = 124.66
E = 12.96
1+62.12 B.C.
227.91
N.78°20'W
0+00 = #1. P.T. Beginning of Survey.

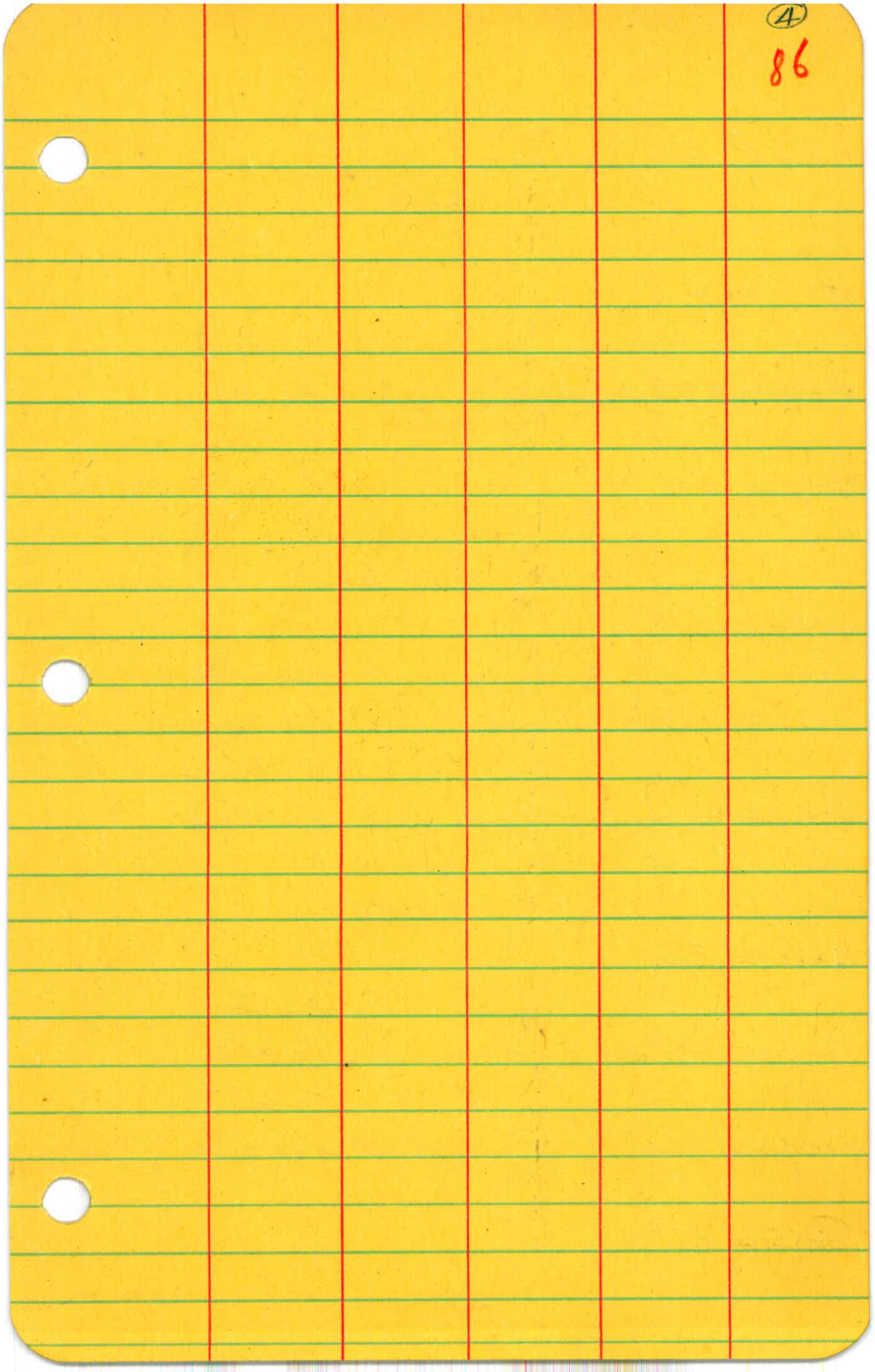
(2)
84

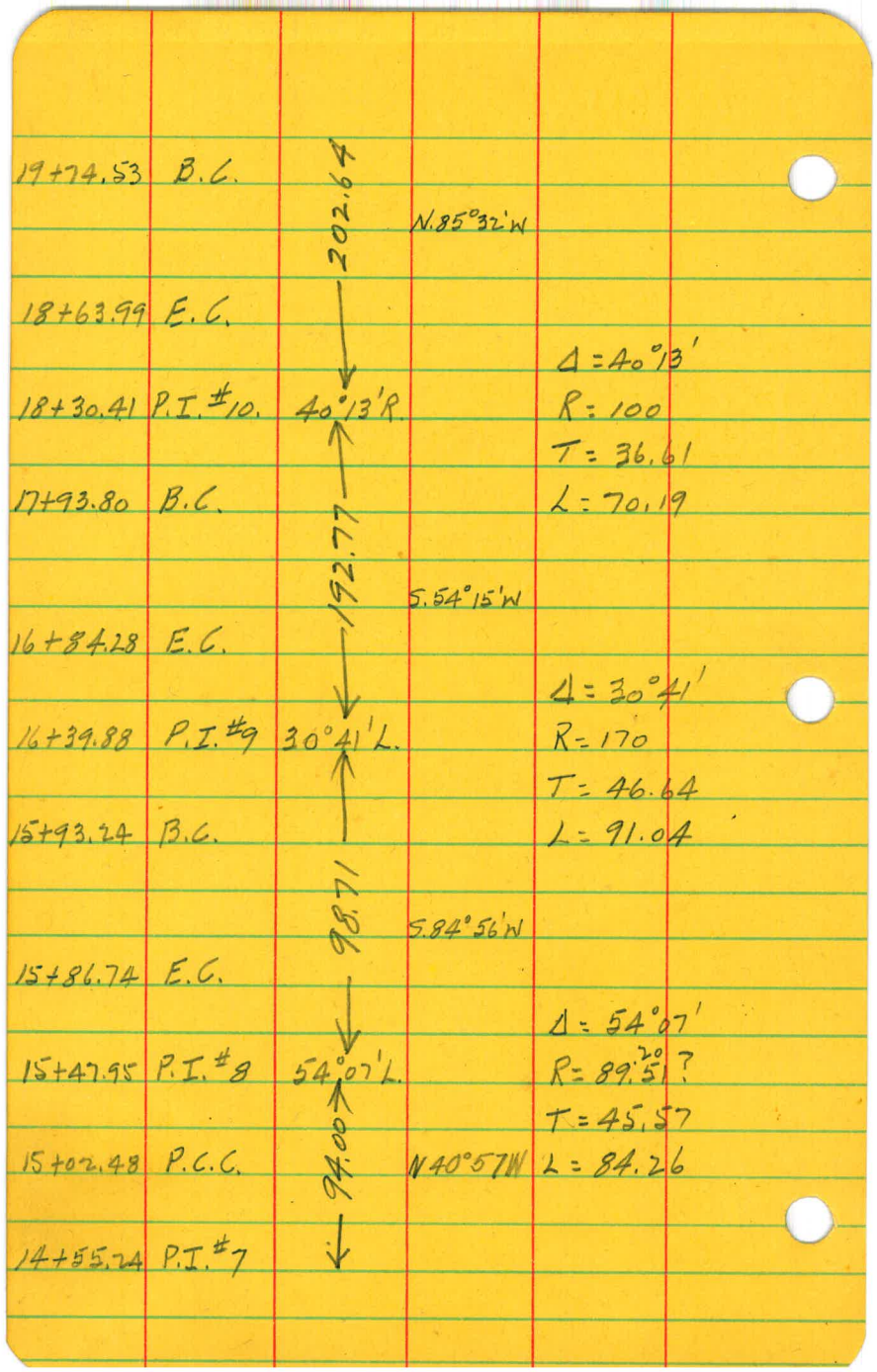

0+00
R.P. 23.53
Hub
28.0
R.P.
Hub
N. 78° 20' W.
545.0
8x10x16 Boulder in RK. Md.
Wheelers Cor
North
2640
90°
2204.6
220.0
101° 20'
N. 0° 20' E.
2640
2797.7
17
8
16
Sickler's
12" Oak
Corner
5
8
4
9

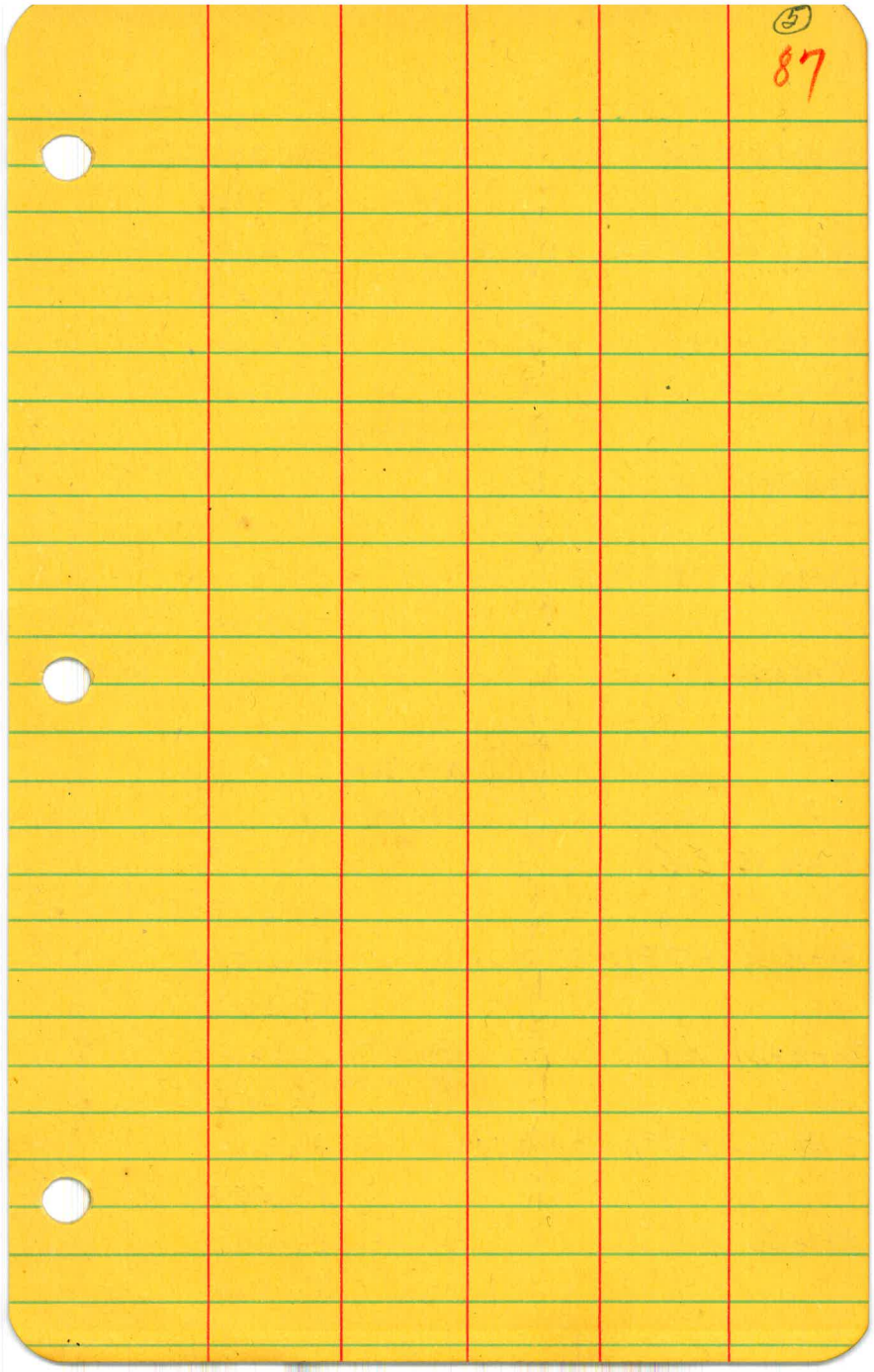

9+53.76 B.C.
295.23
N.76°53'W
7+95.77 E.C.
Δ = 76°18.5'
R = 50
7+68.46 P.I. #4
76°18.5' R.
T = 39.28
L = 66.59
7+29.18 B.C.
246.46
S.26°48.5'W
5+67.90 E.C.
Δ = 30°13'
R = 170
5+24.15 P.I. #3
30°13' L.
T = 45.90
L = 89.65
4+78.25 B.C.
303.06
S.57°01.5'W
2+86.78 E.C.

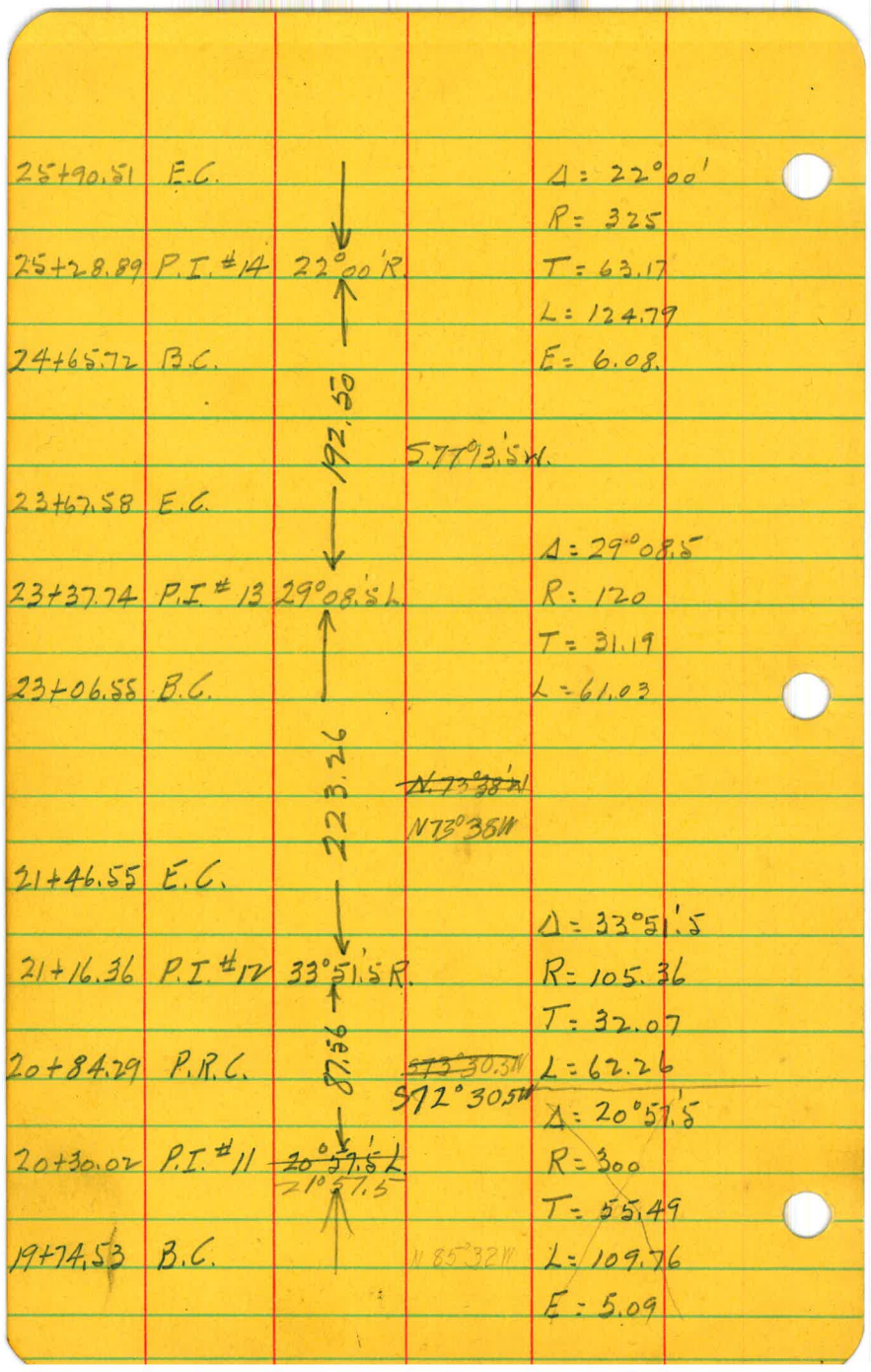

(3)
85


14+55.74 P.I.# 7 21°55.'5 L.
Δ = 21°55.'5
R = 250
T = 48.43
L = 95.67
14+06.81 B.C.
233.77
N. 19°01.'5 W
12+50.22 E.C.
Δ = 44°38'
R = 70
T = 28.71
L = 54.53
E = 5.67
12+24.40 P.I. #6 44°38'R
11+95.69 B.C.
213.19
N. 63°39.'5 W
10+69.17 E.C.
Δ = 13°13.'5
R = 500
T = 57.96
L = 115.41
10+11.72 P.I.# 5 13°13.'5 R.
9+53.76 B.C.


④
86


19+74.53 B.C.
202.64
N.85°32'W
18+63.99 E.C.
Δ = 40°13'
18+30.41 P.I. #10. 40°13'R.
R = 100
T = 36.61
17+93.80 B.C.
L = 70.19
192.77
5.54°15'W
16+84.28 E.C.
Δ = 30°41'
16+39.88 P.I. #9 30°41'L.
R = 170
T = 46.64
15+93.24 B.C.
L = 91.04
98.71
5.84°56'W
15+86.74 E.C.
Δ = 54°07'
15+47.95 P.I. #8 54°07'L.
R = 89.20?
T = 45.57
15+02.48 P.C.C.
94.00
N40°57W
L = 84.26
14+55.24 P.I. #7


5
87


25+90.51 E.C.
Δ = 22°00'
R = 325
25+28.89 P.I. #14 22°00'R.
T = 63.17
L = 124.79
24+65.72 B.C.
E = 6.08.
192.50
S.77°13.5'W.
23+67.58 E.C.
Δ = 29°08.5'
23+37.74 P.I. #13 29°08.5'L.
R = 120
T = 31.19
23+06.58 B.C.
L = 61.03
223.26
~~N.73°38'W~~
N73°38'W
21+46.55 E.C.
Δ = 33°51.5'
21+16.36 P.I. #12 33°51.5'R.
R = 105.36
T = 32.07
97.96
20+84.29 P.R.C.
~~S73°30.3'W~~
S72°30.5'W
L = 62.26
Δ = 20°57.5'
20+30.02 P.I. #11 ~~20°57.5'L~~ 21°57.5'
R = 300
T = 55.49
19+74.53 B.C.
N 85°32'W
L = 109.76
E = 5.09

Correction to PI#11

Sta	Angle	Bearing
20+30.02	21°57.5	N85° 32'W

Δ = 21° 57.5
R = 286.03'
T = 55.49
L = 109.62

Sta 21+84.15 = Equation
Sta 21+84.29

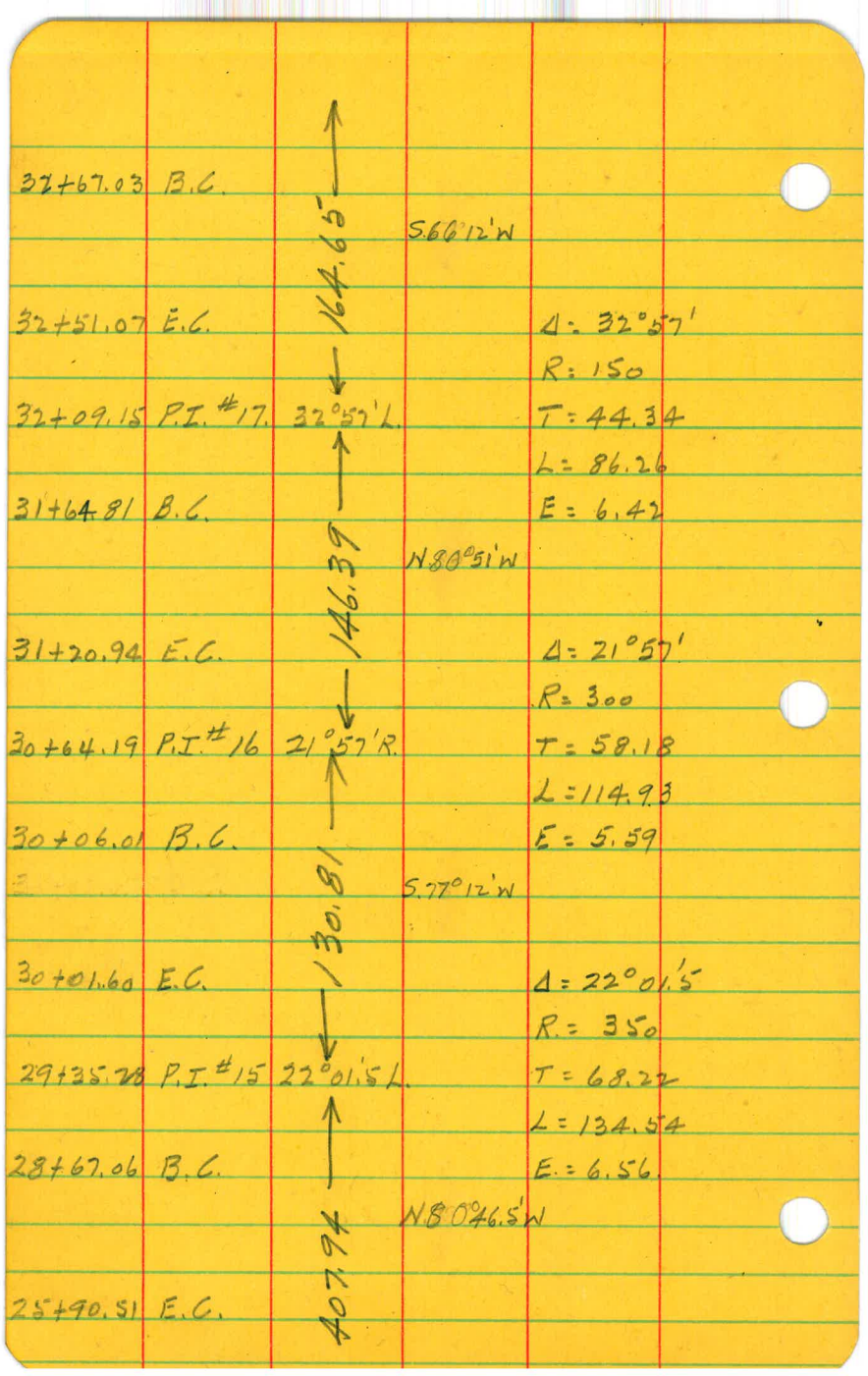
Correction RCP - 72°30.5 Δ 21°57.5

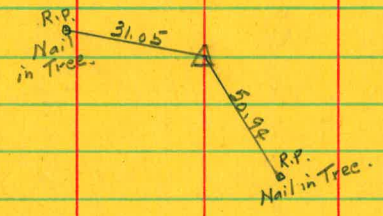
20+30.02 PI #11 R=286.03

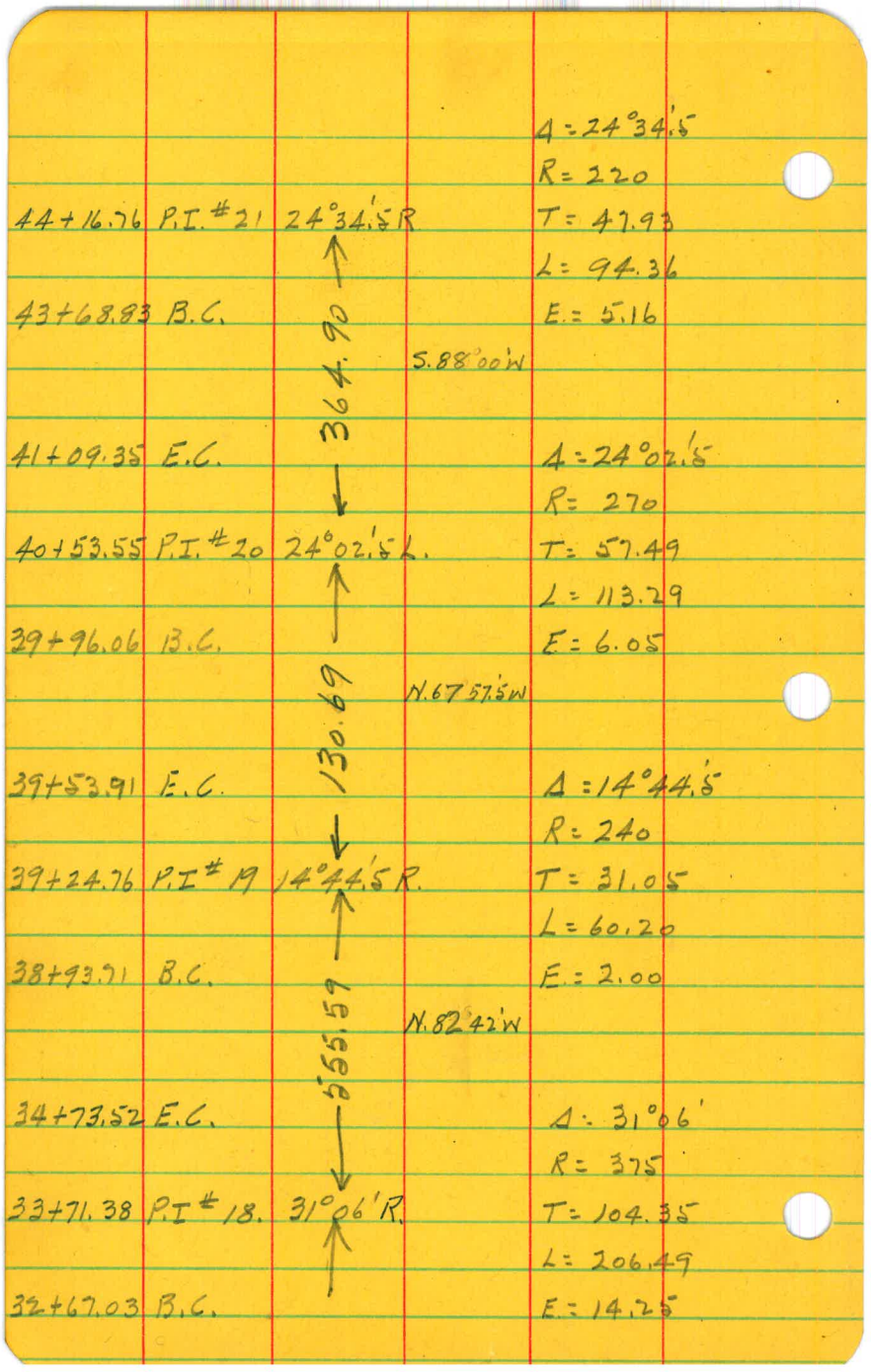
T=55.49

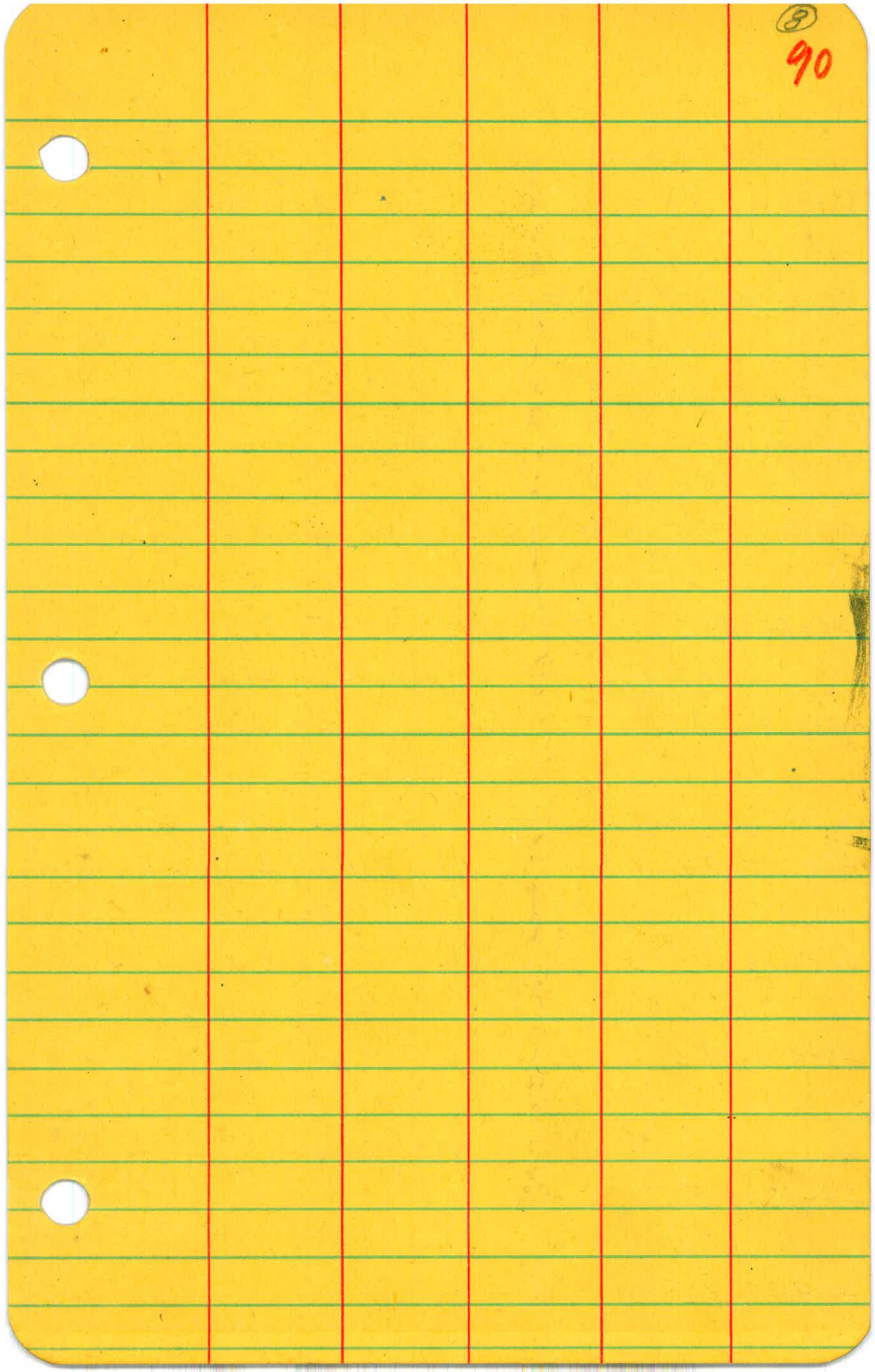
85°32 L=109.62

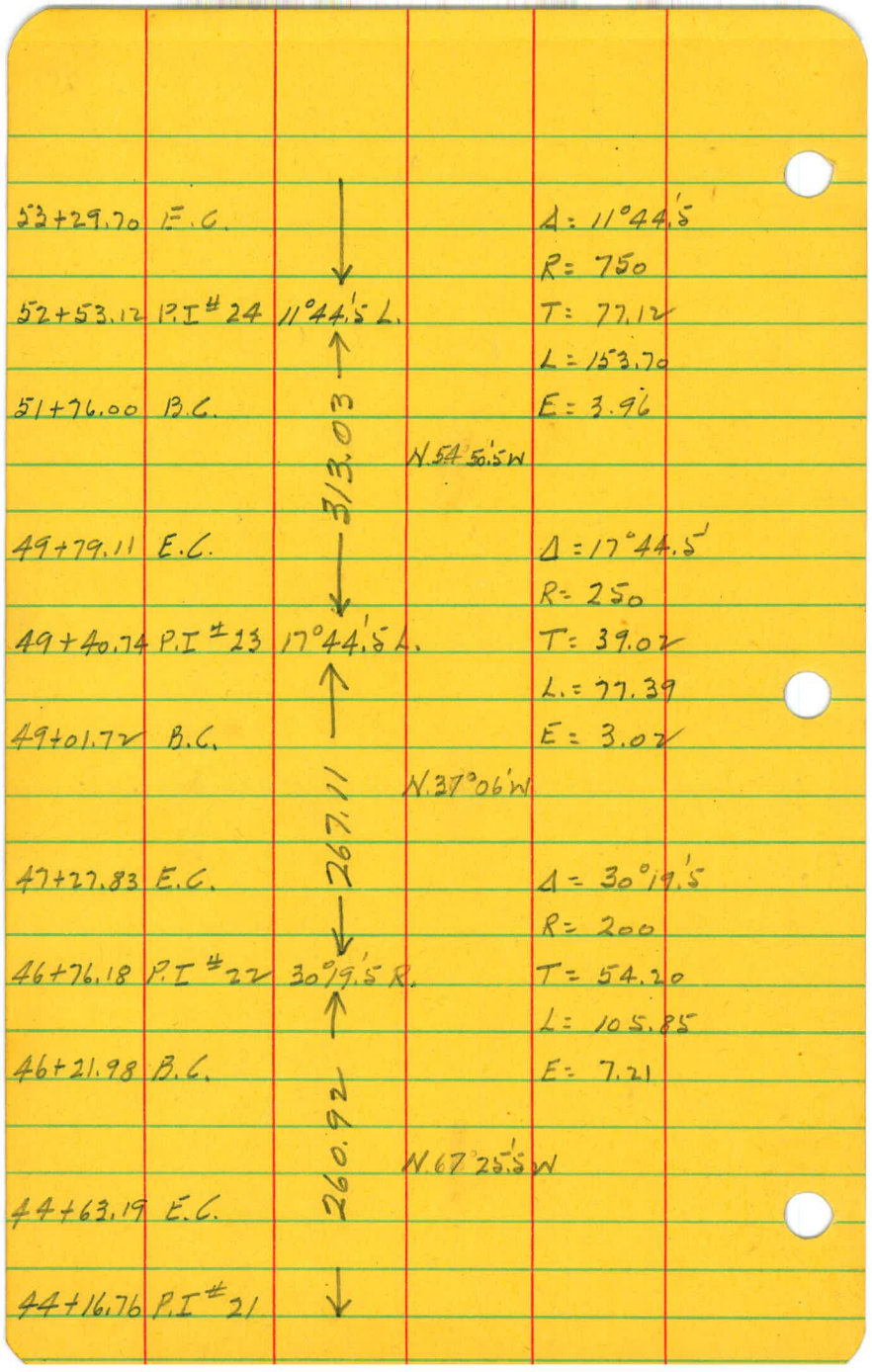
Equation 21+84.15=
21+84.29

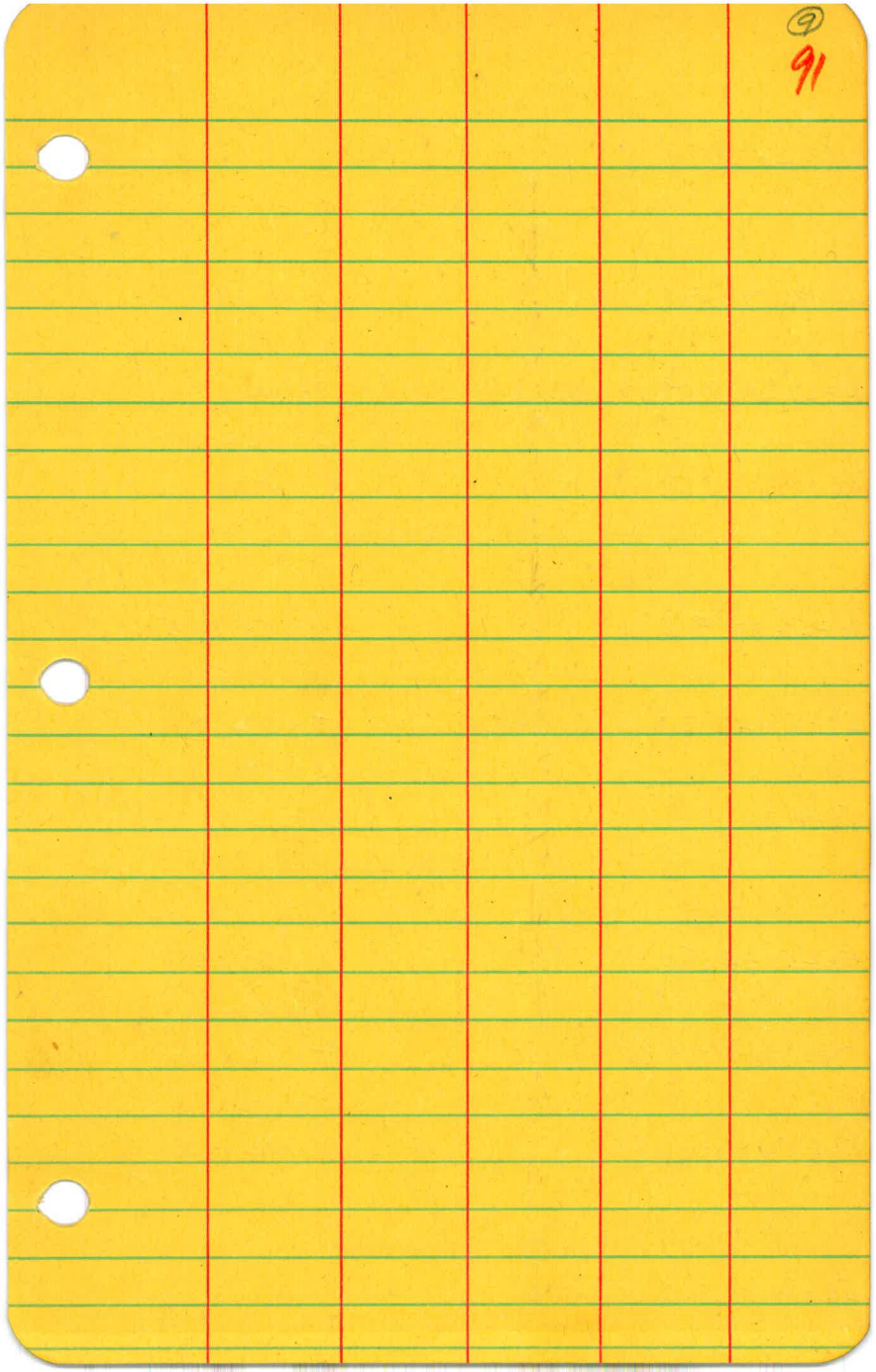

32+67.03 B.C.
S.66°12'W
164.65
32+51.07 E.C.
Δ = 32°57'
R = 150
32+09.15 P.I. #17 32°57'L.
T = 44.34
L = 86.26
31+64.81 B.C.
E = 6.42
N.80°51'W
146.39
31+20.94 E.C.
Δ = 21°57'
R = 300
30+64.19 P.I. #16 21°57'R.
T = 58.18
L = 114.93
30+06.01 B.C.
E = 5.59
S.77°12'W
130.91
30+01.60 E.C.
Δ = 22°01.5'
R = 350
29+35.78 P.I. #15 22°01.5'L.
T = 68.22
L = 134.54
28+67.06 B.C.
E = 6.56
N.80°46.5'W
407.94
25+90.51 E.C.

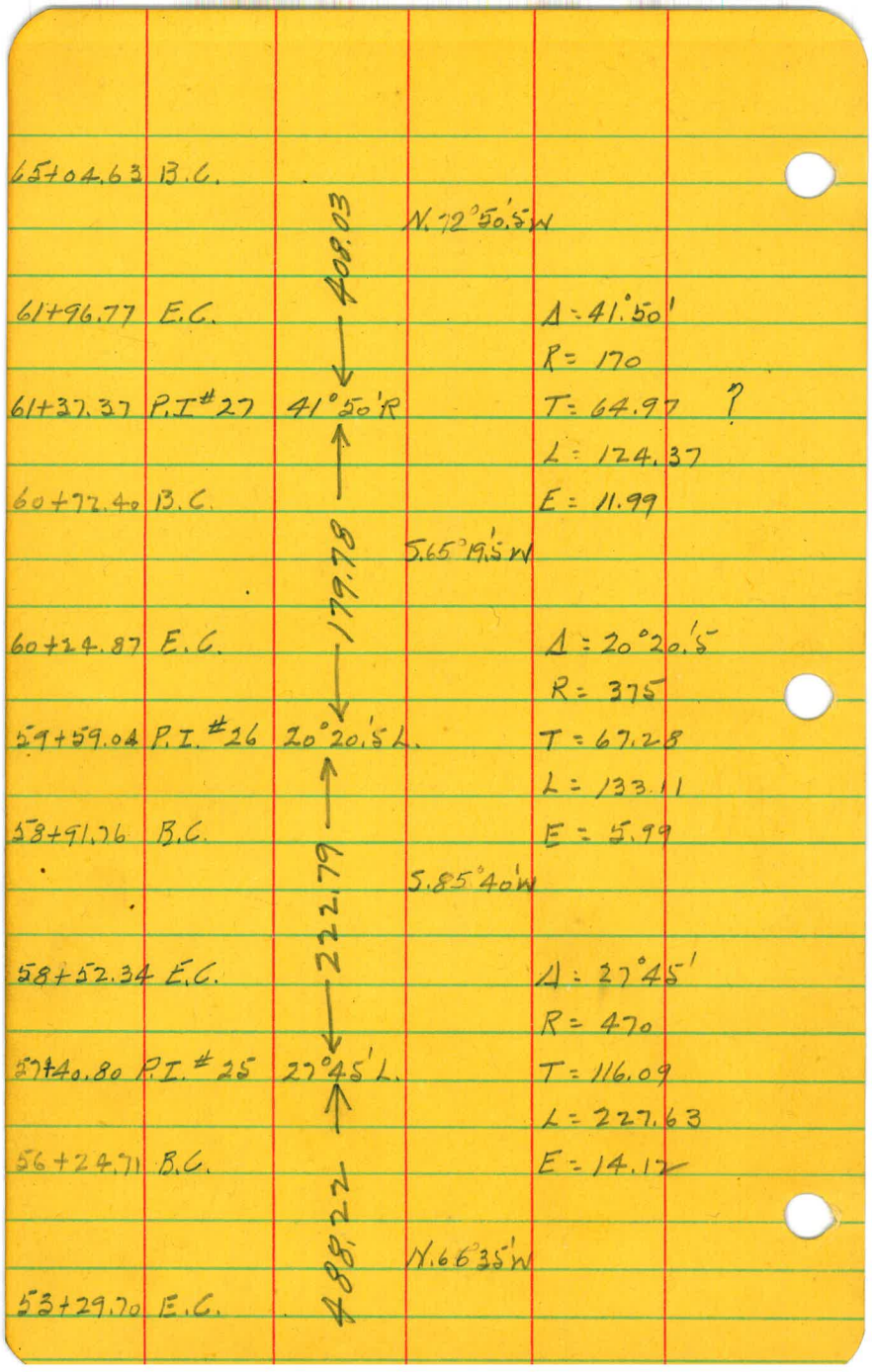

R.P.
Nail
in Tree.
31.05
50.98
R.P.
Nail in Tree.


44+16.76 P.I. #21 24°34.5 R
43+68.83 B.C.
364.90
5.88°00'W
41+09.35 E.C.
40+53.55 P.I. #20 24°02.5 L.
39+96.06 B.C.
130.69
N.67°57.5W
39+53.91 E.C.
39+24.76 P.I. #19 14°44.5 R.
38+93.71 B.C.
555.59
N.82°42'W
34+73.52 E.C.
33+71.38 P.I. #18. 31°06' R.
32+67.03 B.C.
Δ=24°34.5
R=220
T=47.93
L=94.36
E.=5.16
Δ=24°02.5
R=270
T=57.49
L=113.29
E=6.05
Δ=14°44.5
R=240
T=31.05
L=60.20
E.=2.00
Δ=31°06'
R=375
T=104.35
L=206.49
E.=14.25


90

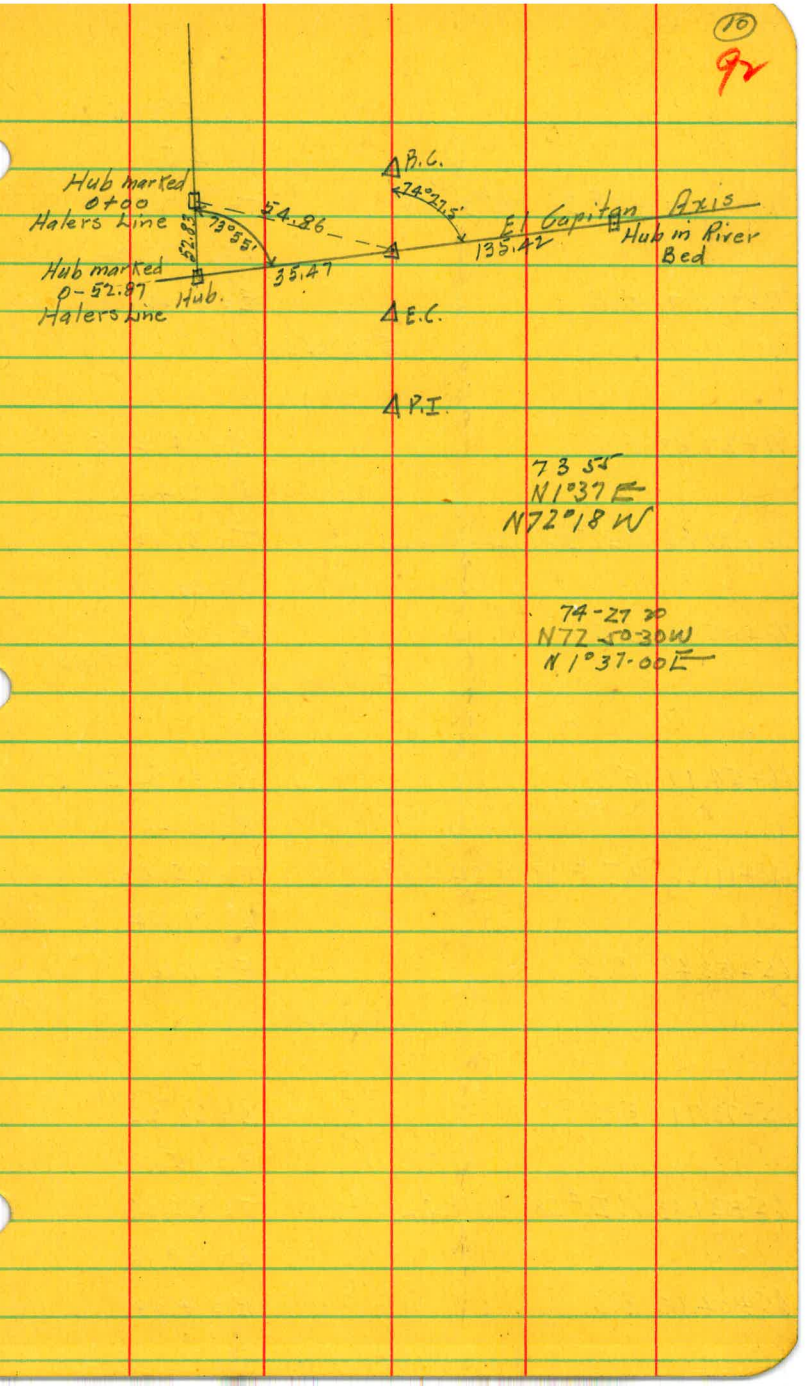

53+29.70 E.C.
52+53.12 P.I # 24 11°44.5' L.
51+76.00 B.C.
313.03
N.54°50.5'W
49+79.11 E.C.
49+40.74 P.I # 23 17°44.5' L.
49+01.72 B.C.
367.11
N.37°06'W
47+27.83 E.C.
46+76.18 P.I # 22 30°19.5' R.
46+21.98 B.C.
260.92
N.67°25.5'W
44+63.19 E.C.
44+16.76 P.I # 21
Δ = 11°44.5'
R = 750
T = 77.12
L = 153.70
E = 3.96
Δ = 17°44.5'
R = 250
T = 39.07
L = 77.39
E = 3.07
Δ = 30°19.5'
R = 200
T = 54.20
L = 105.85
E = 7.21


9
91


65+04.63 B.C.
N. 72°50.5'W
408.03
61+96.77 E.C.
Δ = 41°50'
R = 170
61+37.37 P.I. #27 41°50'R
T = 64.97 ?
L = 124.37
E = 11.99
60+72.40 B.C.
5.65°19.5'W
179.78
60+24.87 E.C.
Δ = 20°20.5'
R = 375
59+59.04 P.I. #26 20°20.5'L.
T = 67.28
L = 133.11
58+91.26 B.C.
E = 5.99
5.85°40'W
222.79
58+52.34 E.C.
Δ = 27°45'
R = 470
57+40.80 P.I. #25 27°45'L.
T = 116.09
L = 227.63
56+24.71 B.C.
E = 14.17
488.22
N.66°35'W
53+29.70 E.C.

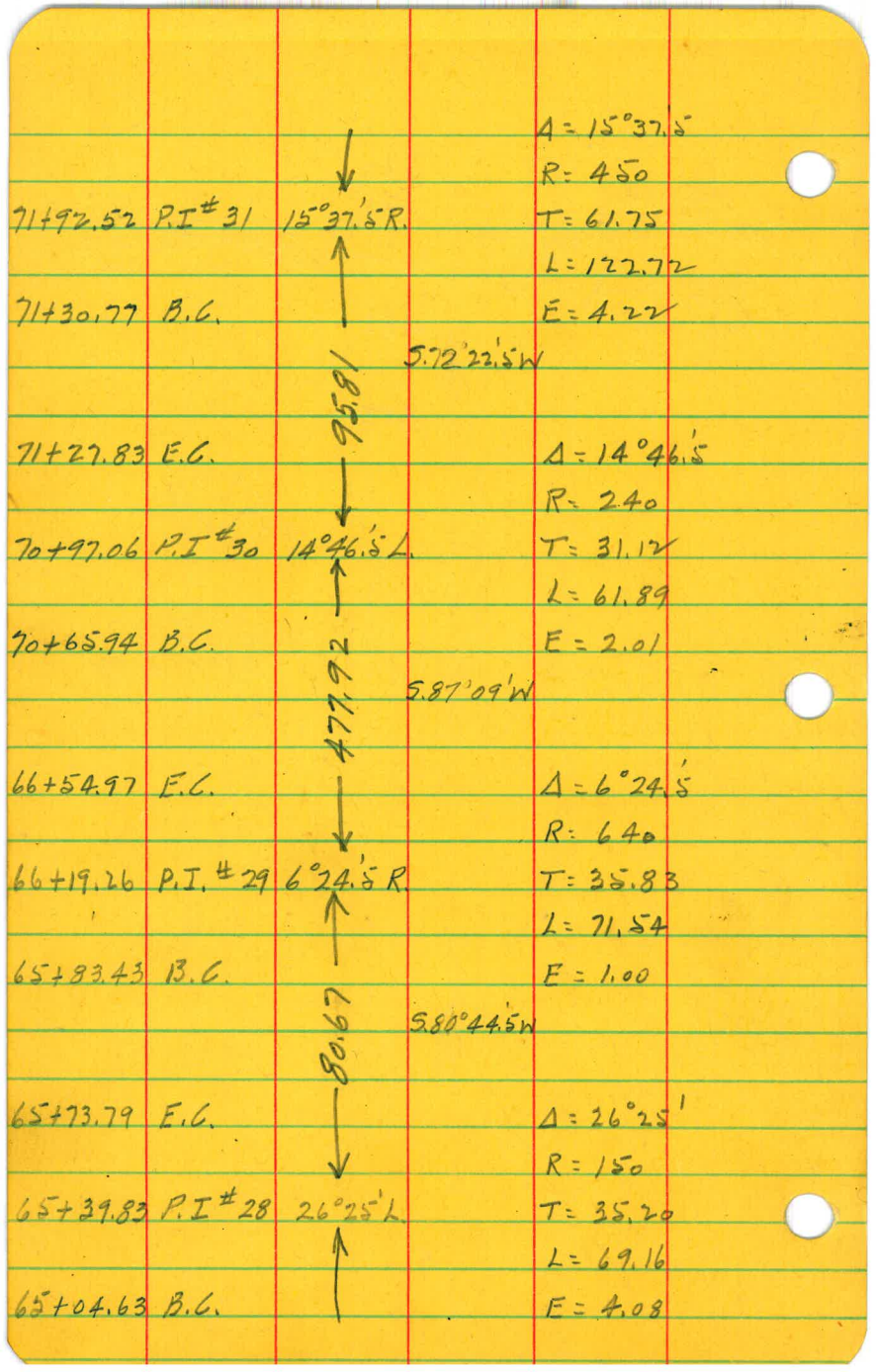
(10)

9r



73 55'
N1°37 E
N72°18 W

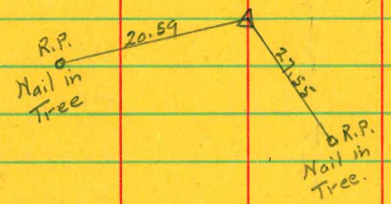
74-27 30
N72-50-30W
N 1°37-00E

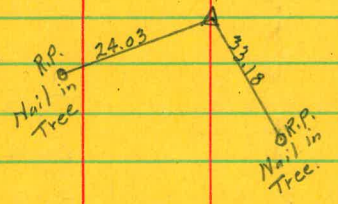

71+92.52 P.I # 31 15°37.5' R.
71+30.77 B.C.
5.72°22.5'W
95.91
71+27.83 E.C.
70+97.06 P.I # 30 14°46.5' L.
70+65.94 B.C.
5.87°09'W
477.92
66+54.97 E.C.
66+19.26 P.I. # 29 6°24.5' R.
65+83.43 B.C.
5.80°44.5'W
69.08
65+73.79 E.C.
65+39.83 P.I # 28 26°25' L.
65+04.63 B.C.
Δ = 15°37.5'
R = 450
T = 61.75
L = 122.72
E = 4.22
Δ = 14°46.5'
R = 240
T = 31.12
L = 61.89
E = 2.01
Δ = 6°24.5'
R = 640
T = 35.83
L = 71.54
E = 1.00
Δ = 26°25'
R = 150
T = 35.20
L = 69.16
E = 4.08

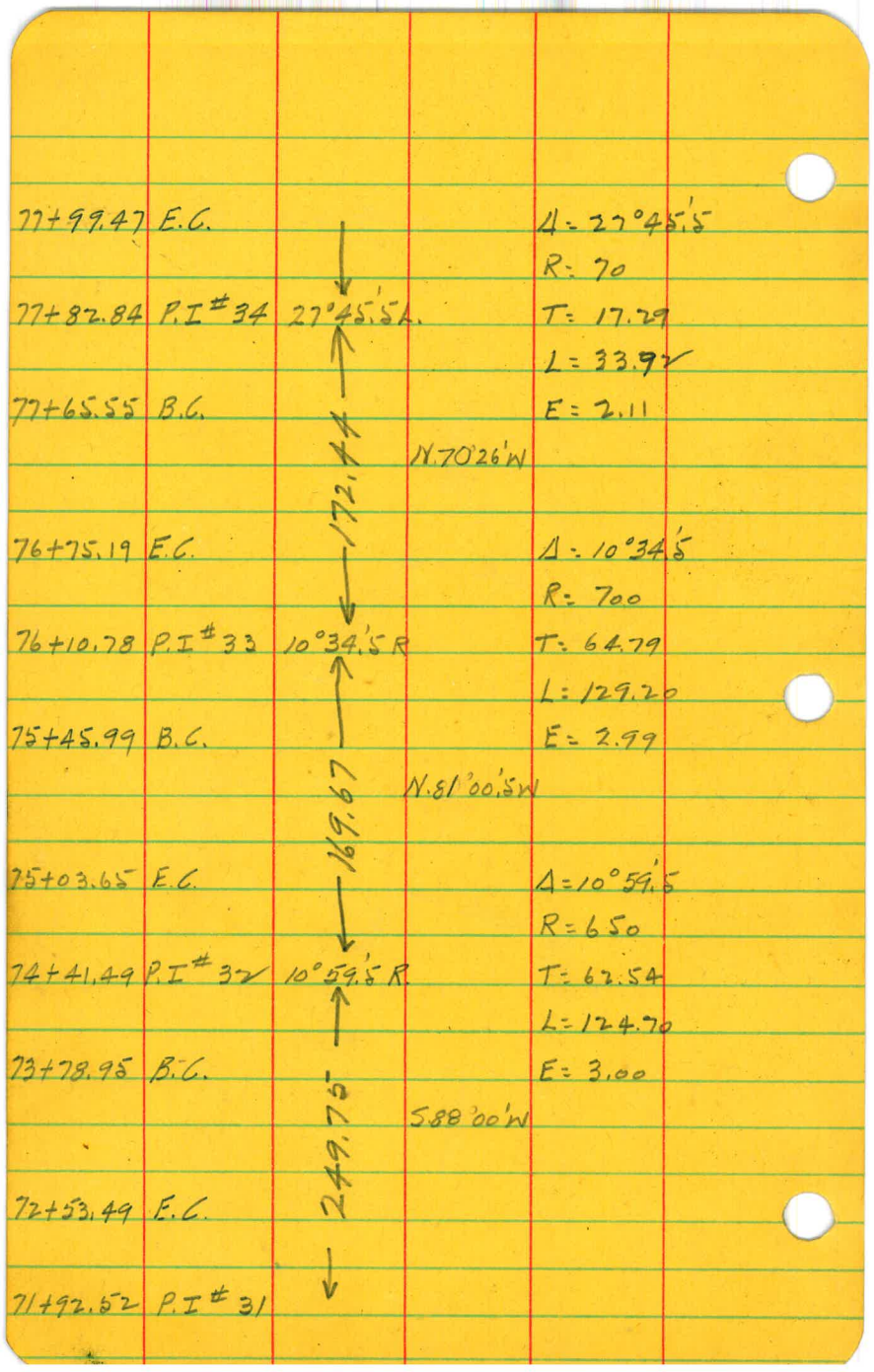
(11)

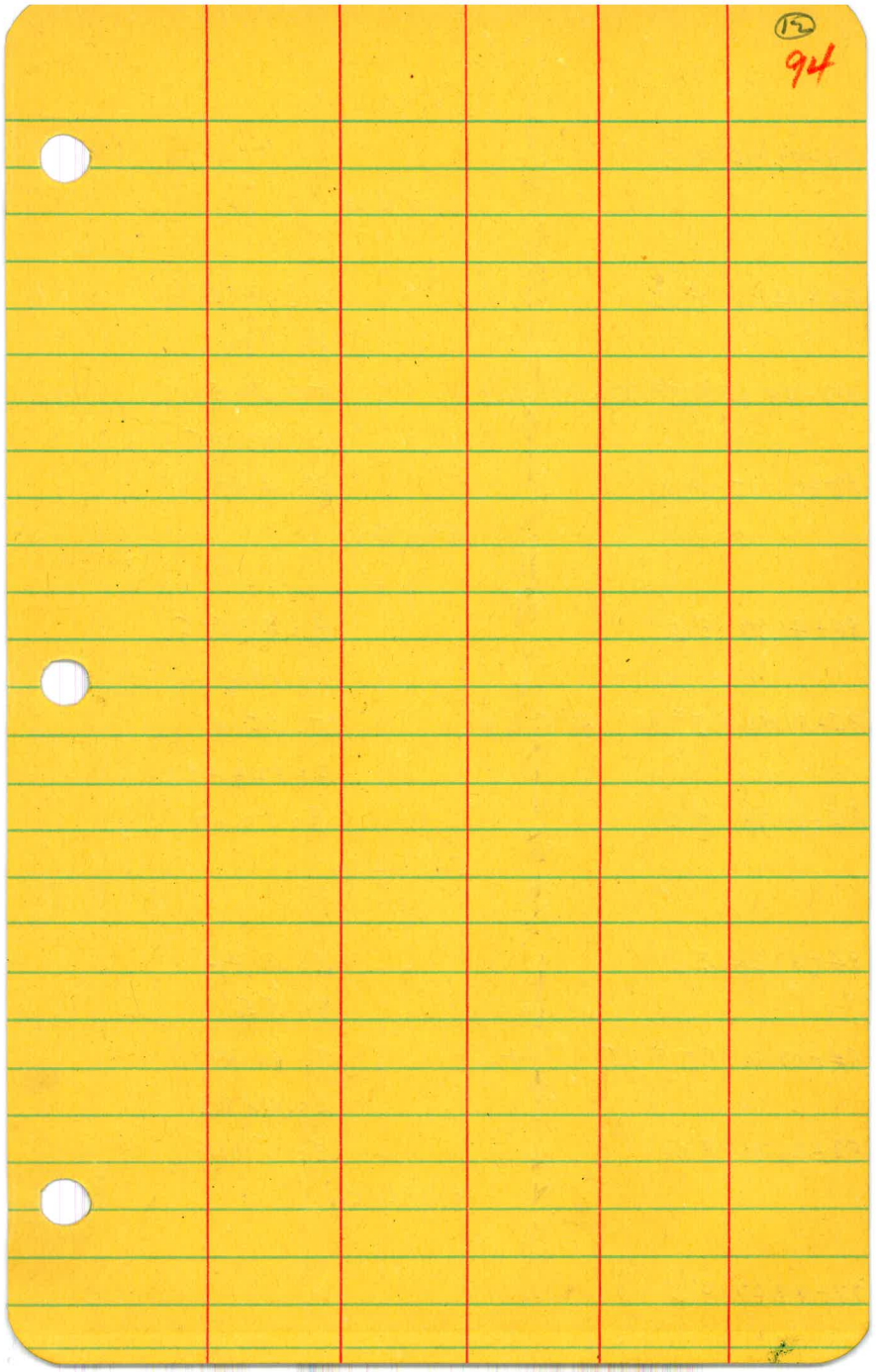
93

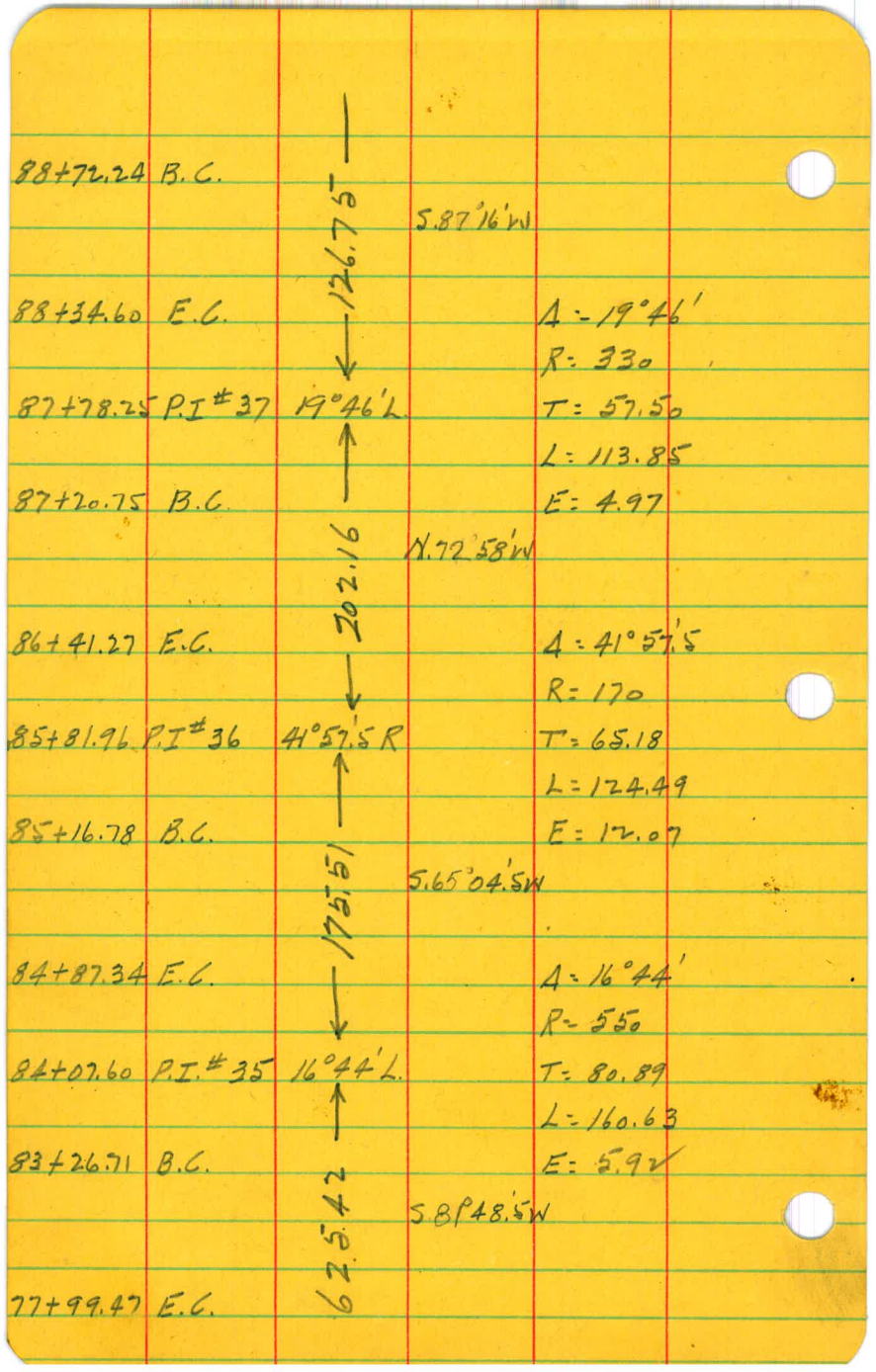
△ P.I. = 7+99.8 P.I. Pipe Line.





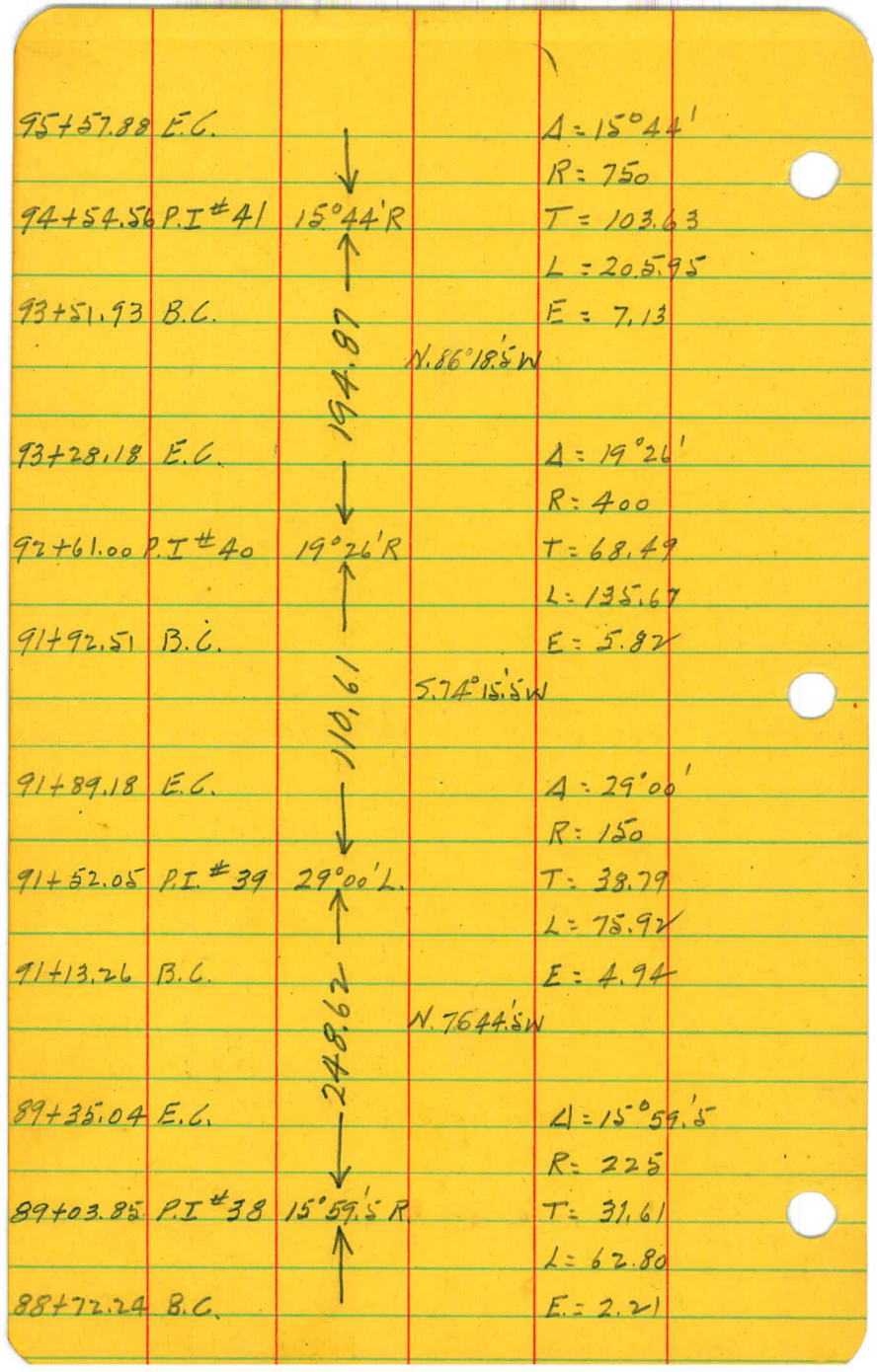

77+99.47 E.C.
77+82.84 P.I # 34
27°45.5' L.
77+65.55 B.C.
N.70°26'W
172.44
76+75.19 E.C.
76+10.78 P.I # 33
10°34.5' R
75+45.99 B.C.
N.81°00.5'W
169.67
75+03.65 E.C.
74+41.49 P.I # 32
10°59.5' R
73+78.95 B.C.
S.88°00'W
249.75
72+53.49 E.C.
71+92.52 P.I # 31
Δ = 27°45.5'
R = 70
T = 17.29
L = 33.92
E = 2.11
Δ = 10°34.5'
R = 700
T = 64.79
L = 129.20
E = 2.99
Δ = 10°59.5'
R = 650
T = 62.54
L = 124.70
E = 3.00

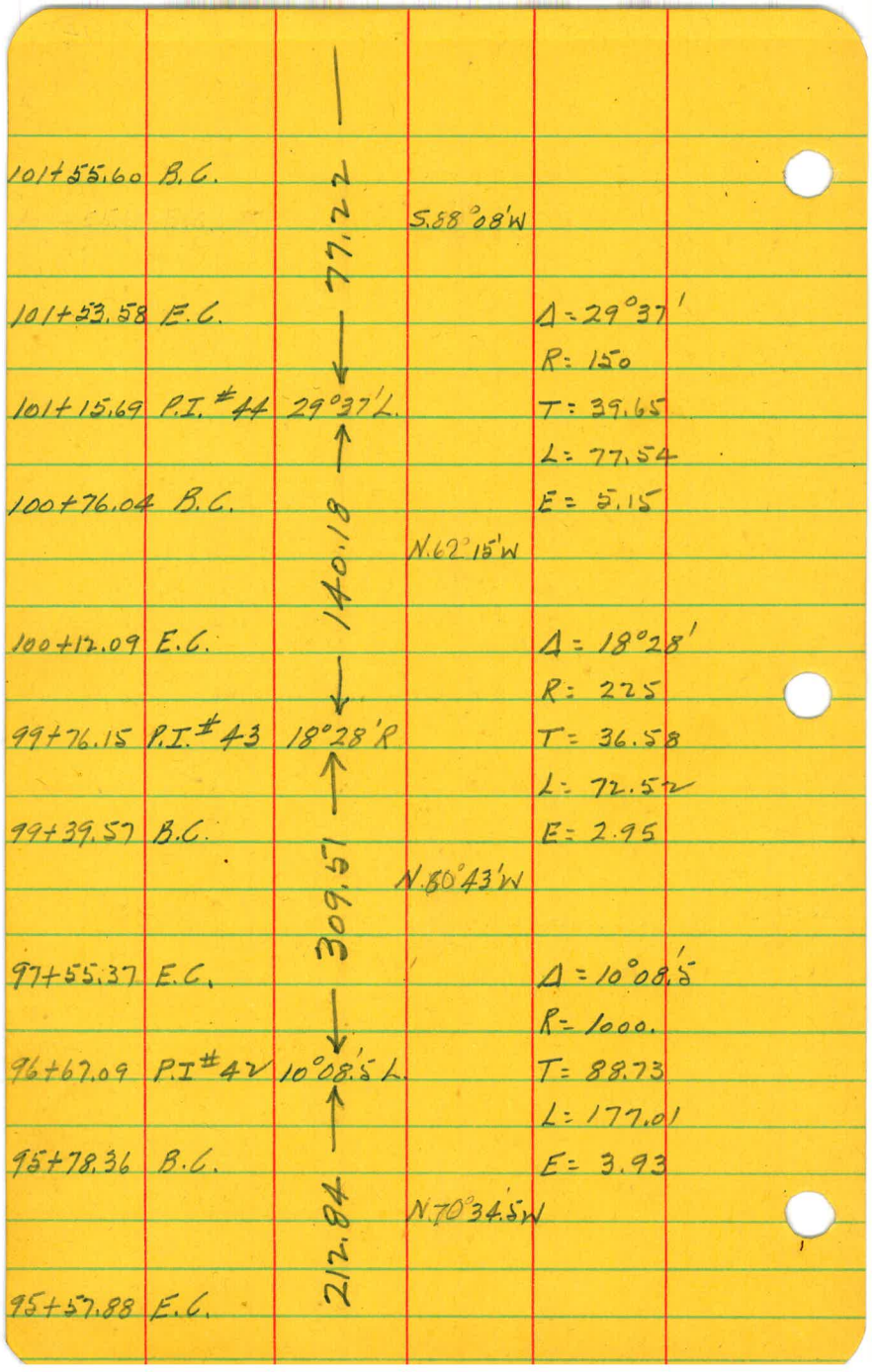

94

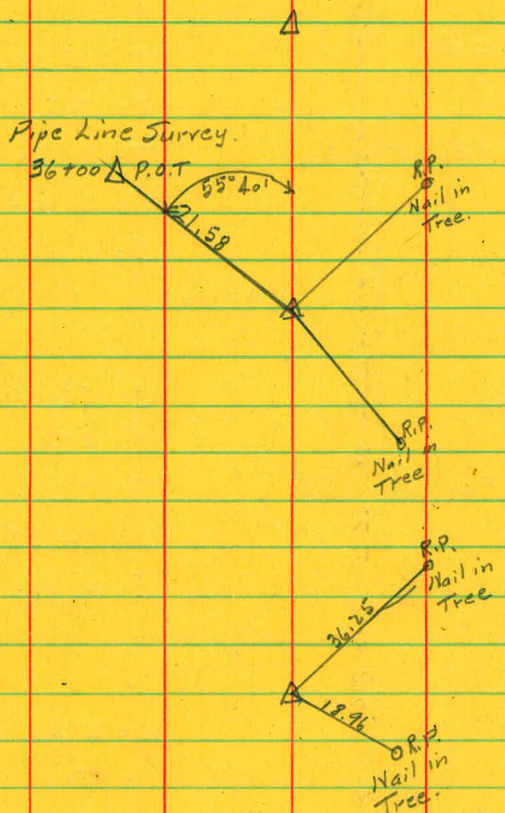

88+72.24 B.C.
126.75
S.87°16'W
88+34.60 E.C.
Δ = 19°46'
R = 330
87+78.25 P.I #37 19°46'L
T = 57.50
L = 113.85
87+20.75 B.C.
E = 4.97
202.16
N.72°58'W
86+41.27 E.C.
Δ = 41°57.5'
R = 170
85+81.96 P.I #36 41°57.5'R
T = 65.18
L = 124.49
85+16.78 B.C.
E = 12.07
176.51
S.65°04.5'W
84+87.34 E.C.
Δ = 16°44'
R = 550
84+07.60 P.I. #35 16°44'L
T = 80.89
L = 160.63
83+26.71 B.C.
E = 5.92
625.42
S.81°48.5'W
77+99.47 E.C.

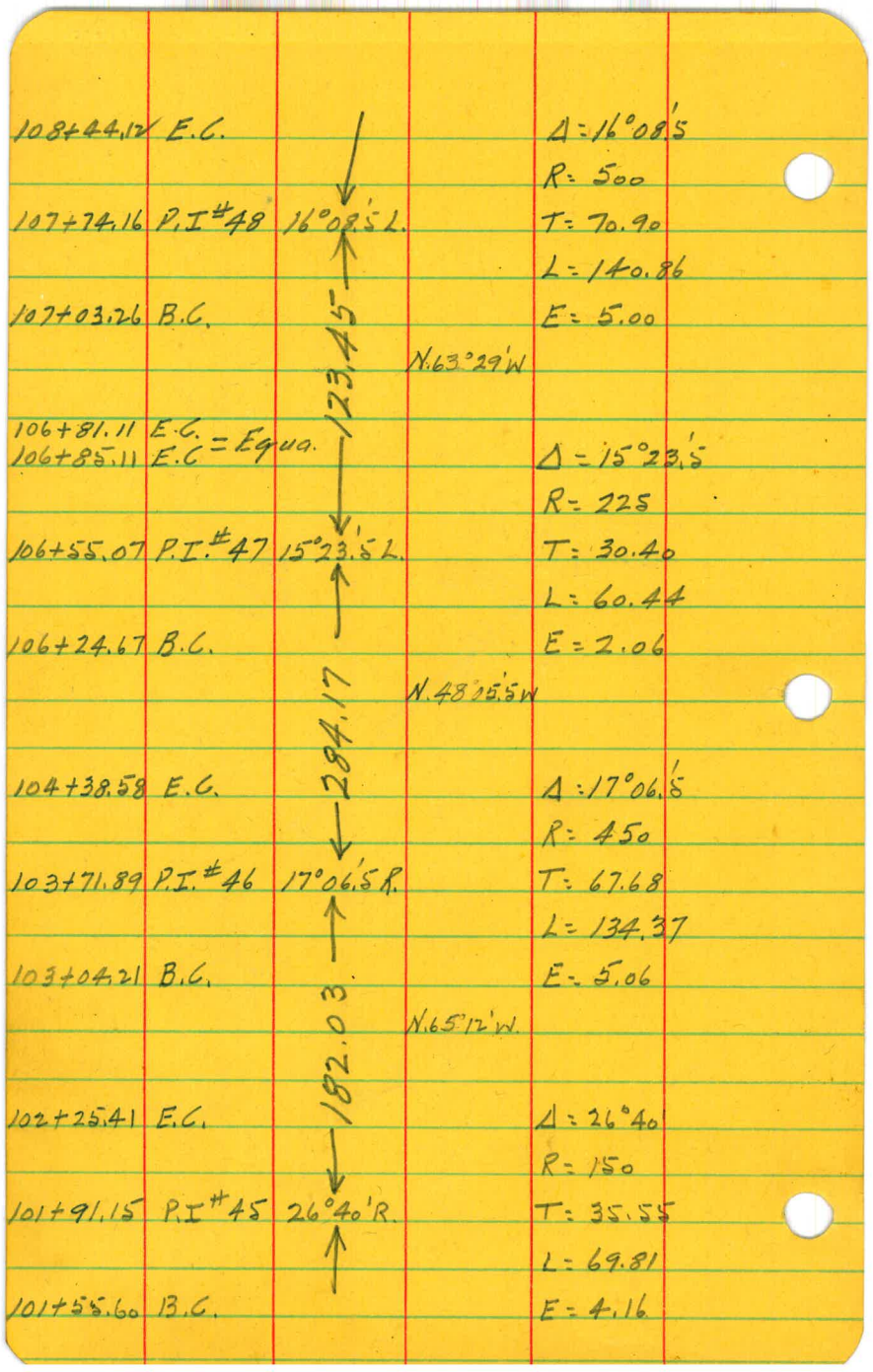
(13)
95

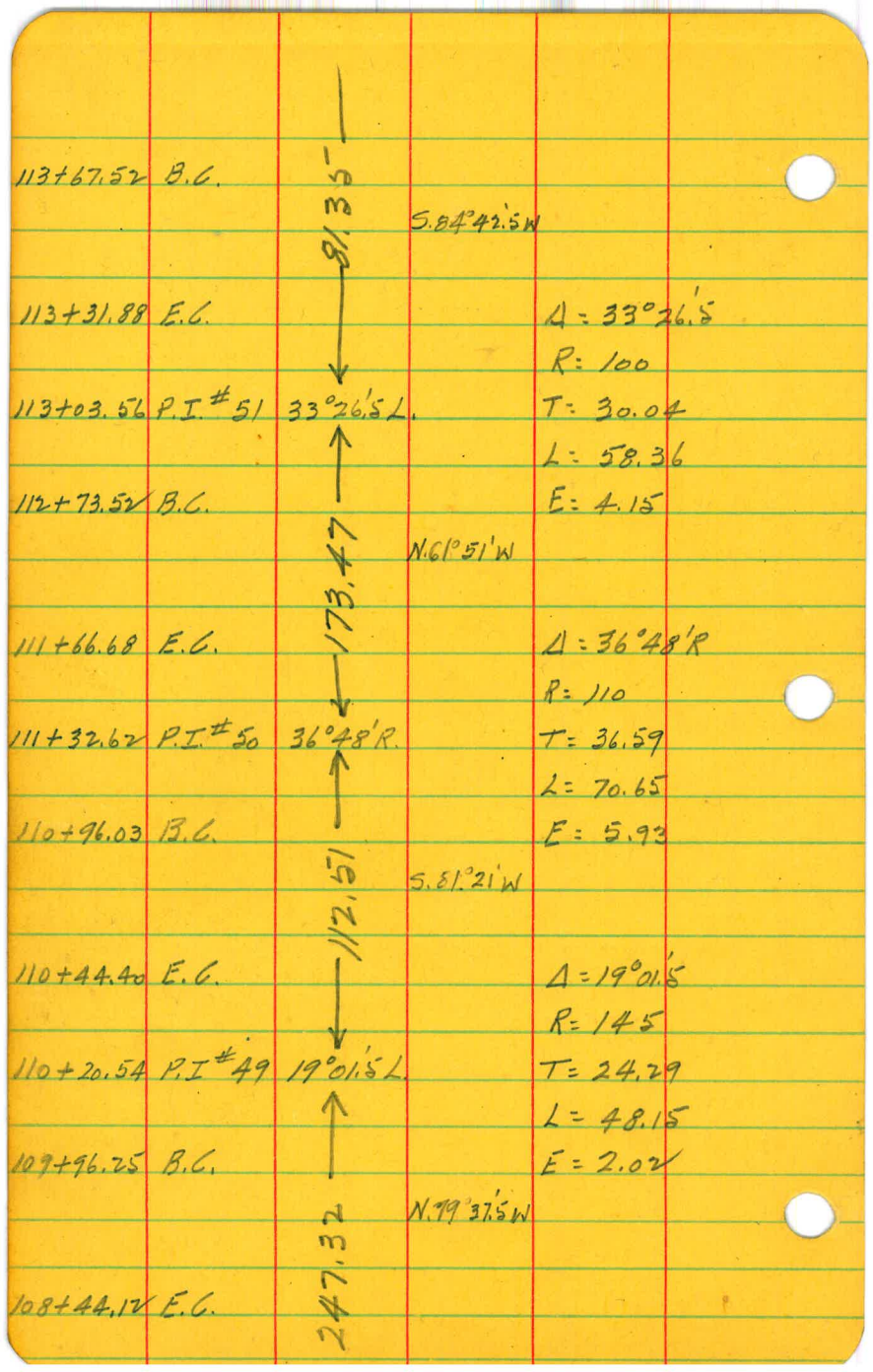
△ P.I = 21+81.2 P.I. Pipe Line

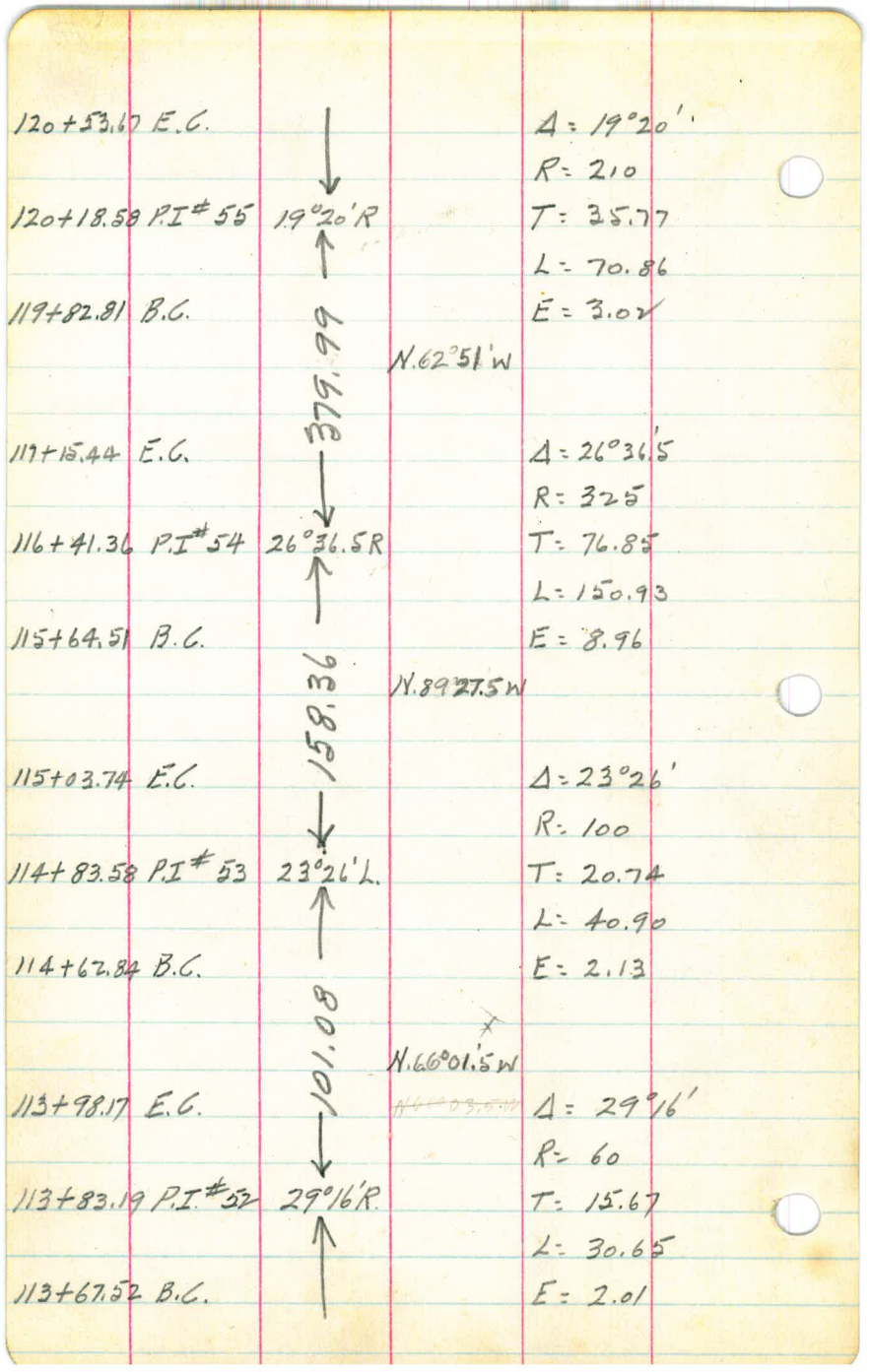

95+57.88 E.C.
94+54.56 P.I #41 15°44'R
93+51.93 B.C.
194.97
N.86°18.5'W
93+28.18 E.C.
92+61.00 P.I #40 19°26'R
91+92.51 B.C.
110.61
S.74°15.5'W
91+89.18 E.C.
91+52.05 P.I #39 29°00'L.
91+13.26 B.C.
248.62
N.76°44.5'W
89+35.04 E.C.
89+03.85 P.I #38 15°59.5'R
88+72.24 B.C.
Δ = 15°44'
R = 750
T = 103.63
L = 205.95
E = 7.13
Δ = 19°26'
R = 400
T = 68.49
L = 135.67
E = 5.82
Δ = 29°00'
R = 150
T = 38.79
L = 75.92
E = 4.94
Δ = 15°59.5'
R = 225
T = 31.61
L = 62.80
E = 2.21


101+55.60 B.C.
S.88°08'W
77.22
101+53.58 E.C.
Δ = 29°37'
R = 150
101+15.69 P.I. #44 29°37' L.
T = 39.65
L = 77.54
E = 5.15
100+76.04 B.C.
N.62°15'W
140.19
100+17.09 E.C.
Δ = 18°28'
R = 225
99+76.15 P.I. #43 18°28' R
T = 36.58
L = 72.52
E = 2.95
99+39.57 B.C.
N.80°43'W
309.51
97+55.37 E.C.
Δ = 10°08.5'
R = 1000.
96+67.09 P.I. #42 10°08.5' L.
T = 88.73
L = 177.01
E = 3.93
95+78.36 B.C.
N.70°34.5'W
212.84
95+57.88 E.C.


Pipe Line Survey.
36+00 P.O.T
55° 40'
21.58
R.P.
Nail in
Tree.
R.P.
Nail in
Tree
R.P.
Nail in
Tree
36.25
18.96
R.P.
Nail in
Tree.

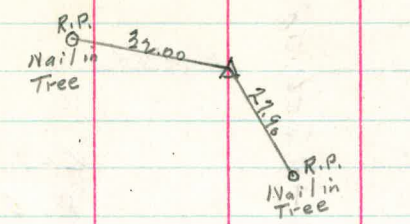

108+44.12 E.C.
107+74.16 P.I. #48 16°08.5' L.
107+03.26 B.C.
123.45'
N.63°29'W
106+81.11 E.C.
106+85.11 E.C. = Equa.
106+55.07 P.I. #47 15°23.5' L.
106+24.67 B.C.
294.17
N.48°15.5'W
104+38.58 E.C.
103+71.89 P.I. #46 17°06.5' R.
103+04.21 B.C.
182.03'
N.65°12'W.
102+25.41 E.C.
101+91.15 P.I. #45 26°40' R.
101+55.60 B.C.
Δ = 16°08.5'
R = 500
T = 70.90
L = 140.86
E = 5.00
Δ = 15°23.5'
R = 225
T = 30.40
L = 60.44
E = 2.06
Δ = 17°06.5'
R = 450
T = 67.68
L = 134.37
E = 5.06
Δ = 26°40'
R = 150
T = 35.55
L = 69.81
E = 4.16


113+67.52 B.C.
91.35
S.84°42.5'W
113+31.88 E.C.
Δ = 33°26.5'
R = 100
113+03.56 P.I. #51 33°26.5'L.
T = 30.04
L = 58.36
112+73.52 B.C.
E = 4.15
173.47
N.61°51'W
111+66.68 E.C.
Δ = 36°48'R
R = 110
111+32.62 P.I. #50 36°48'R.
T = 36.59
L = 70.65
110+96.03 B.C.
E = 5.93
112.51
S.81°21'W
110+44.40 E.C.
Δ = 19°01.5'
R = 145
110+20.54 P.I. #49 19°01.5'L.
T = 24.29
L = 48.15
109+96.25 B.C.
E = 2.02
247.32
N.79°37.5'W
108+44.17 E.C.

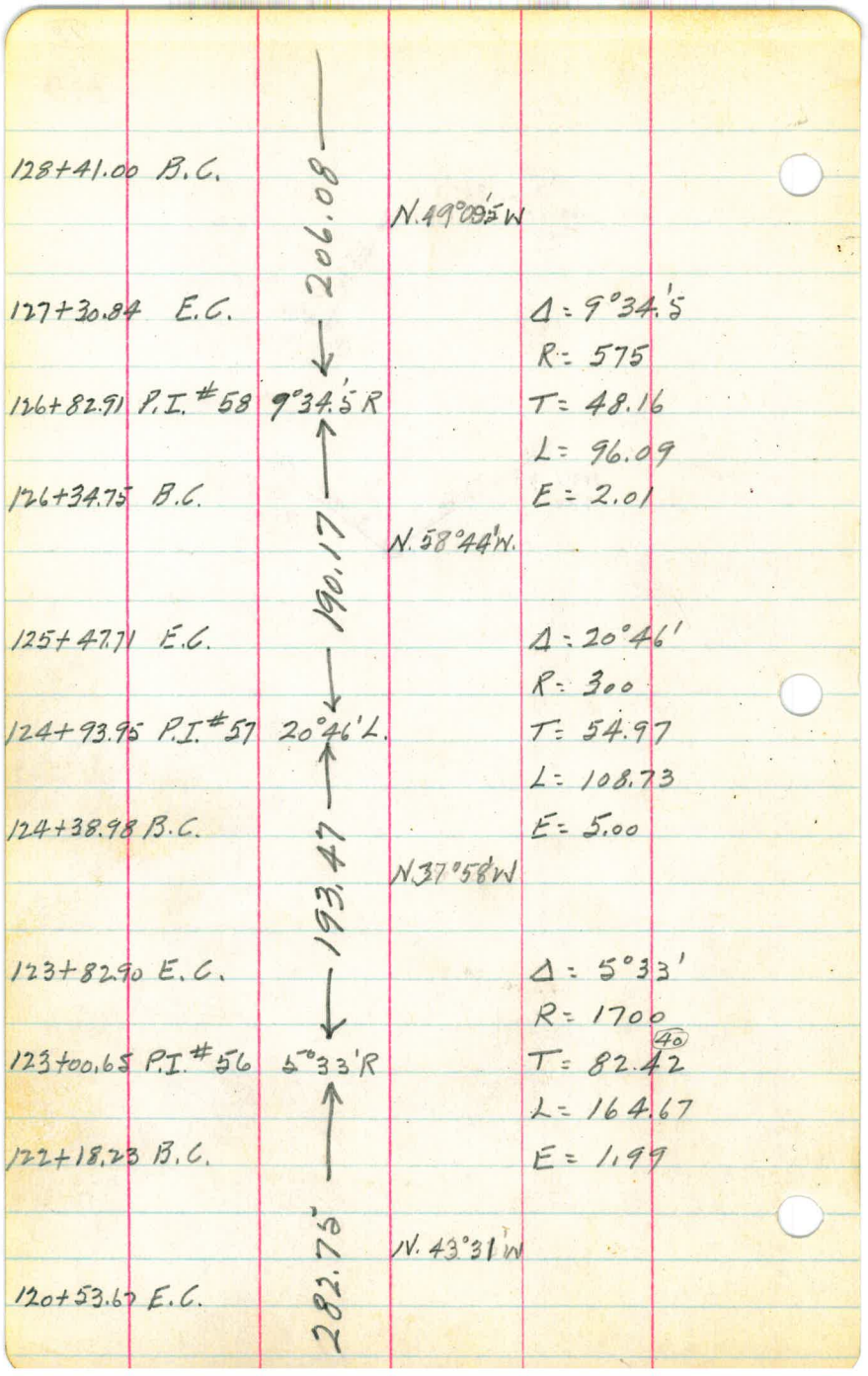

120+53.67 E.C.
120+18.58 P.I # 55
19°20' R
119+82.81 B.C.
N. 62°51' W
379.99
119+15.44 E.C.
116+41.36 P.I # 54
26°36.5 R
115+64.51 B.C.
N. 89°27.5 W
158.93
115+03.74 E.C.
114+83.58 P.I # 53
23°26' L.
114+62.84 B.C.
N. 66°01.5' W
101.08
113+98.17 E.C.
113+83.19 P.I # 52
29°16' R
113+67.52 B.C.
Δ = 19°20'
R = 210
T = 35.77
L = 70.86
E = 3.02
Δ = 26°36.5'
R = 325
T = 76.85
L = 150.93
E = 8.96
Δ = 23°26'
R = 100
T = 20.74
L = 40.90
E = 2.13
Δ = 29°16'
R = 60
T = 15.67
L = 30.65
E = 2.01

(18)

100

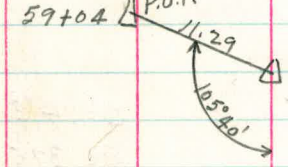

R.P.
Nail in
Tree
32.00
27.69
R.P.
Nail in
Tree

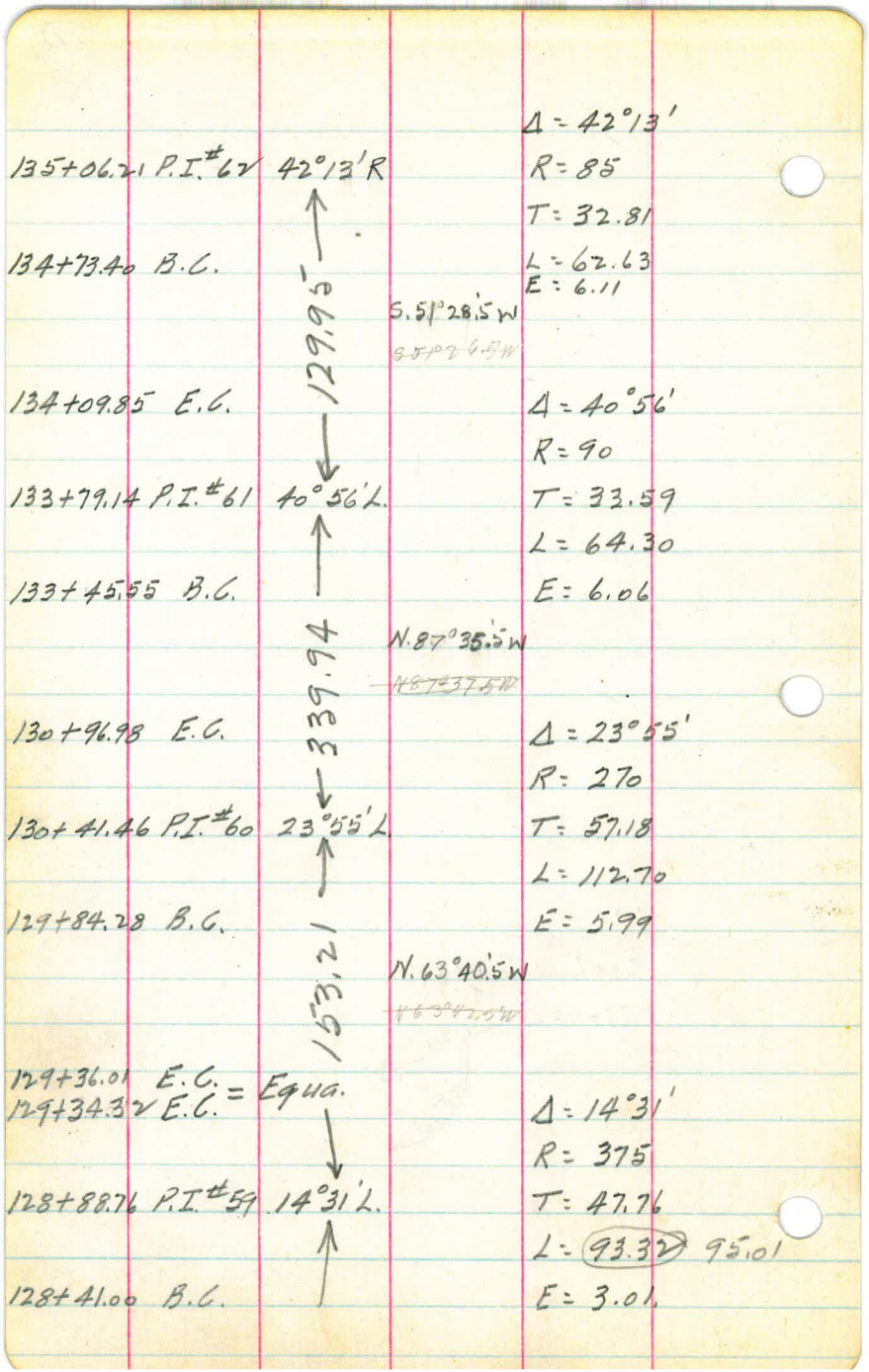

R.P.
Nail in
Tree
27.58
30.97
R.P.
Nail in
Tree


128+41.00 B.C.
206.08
N. 49°09'5W
127+30.84 E.C.
Δ = 9°34.'5
R = 575
126+82.91 P.I. #58 9°34.'5 R
T = 48.16
L = 96.09
126+34.75 B.C.
E = 2.01
190.17
N. 58°44'W.
125+47.71 E.C.
Δ = 20°46'
R = 300
124+93.95 P.I. #57 20°46'L.
T = 54.97
L = 108.73
124+38.98 B.C.
E = 5.00
193.47
N. 37°58W
123+82.90 E.C.
Δ = 5°33'
R = 1700
123+00.65 P.I. #56 5°33'R
T = 82.42 (40)
L = 164.67
122+18.23 B.C.
E = 1.99
282.75'
N. 43°31'W
120+53.67 E.C.

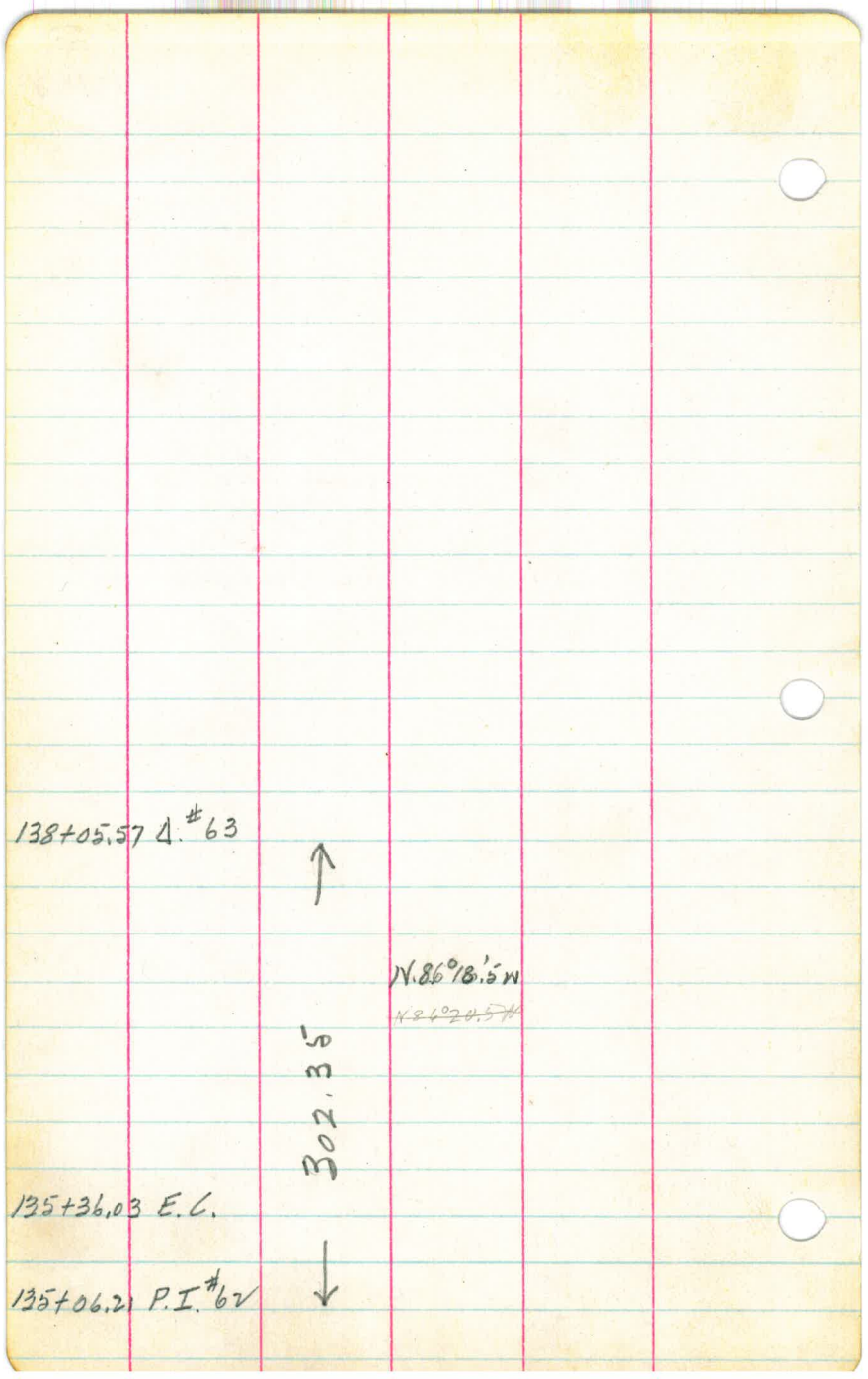
Pipe Line Survey

59+04 P.O.T.

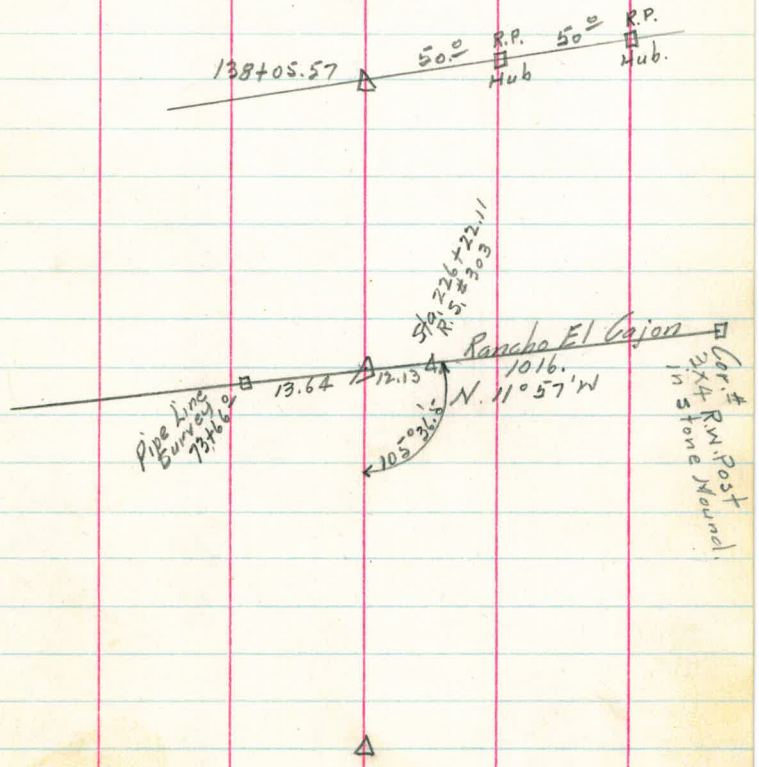


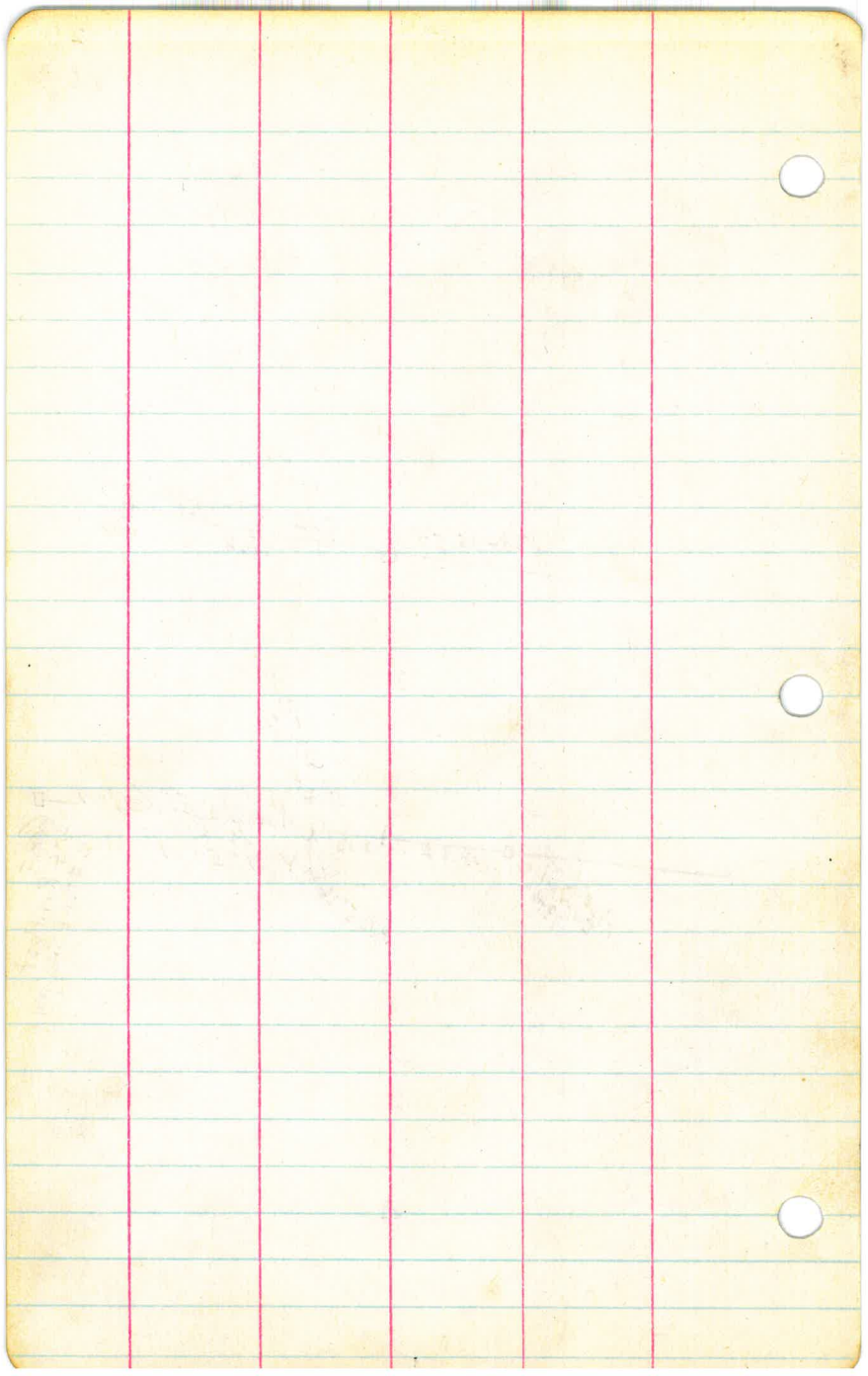

135+06.21 P.I. #62 42°13'R
Δ = 42°13'
R = 85
T = 32.81
L = 62.63
E = 6.11
134+73.40 B.C.
S. 51°28.5' W
129.95'
134+09.85 E.C.
Δ = 40°56'
R = 90
133+79.14 P.I. #61 40°56'L.
T = 33.59
L = 64.30
E = 6.06
133+45.55 B.C.
N. 87°35.5' W
339.94
130+96.98 E.C.
Δ = 23°55'
R = 270
130+41.46 P.I. #60 23°55'L.
T = 57.18
L = 112.70
E = 5.99
129+84.28 B.C.
N. 63°40.5' W
153.21
129+36.01 E.C.
129+34.32 E.C. = Equa.
Δ = 14°31'
R = 375
128+88.76 P.I. #59 14°31'L.
T = 47.76
L = 93.32 95.01
128+41.00 B.C.
E = 3.01

10V


138+05.57 Δ. #63
N.86°18.5'W
N.86°20.5'W
302.35'
135+36.03 E.C.
135+06.21 P.I. #62

103


138+05.57
50.00
R.P.
Hub
50.00
R.P.
Hub.
Sta. 226+22.11
R.S. #303
Rancho El Cajon
1016.
N. 11°57'W
13.64
12.13
Pipe Line
Survey
73+46.0
105°31.5'
Cor. #
2"x4" R.W. Post
in stone Mound.



(1)
104

Levels from E.C. 2+86.78 Richards Road Survey, = Sta. 51+68.31 - Pipe Line Survey to Sta. 0+00 on Pipe Line Survey, which point is on Axis of El Capitan Dam Site #3.

Sept. 1927.

Converse.

Rauner

McBain.

Pages 1-6.

B.M.				612.16	
	8.06	620.22			
51+68.31			3.4	616.8	
51			5.1	615.1	
50			8.4	611.8	
49+63			13.7	606.5	
49+54			22.6	597.6	
49+45			14.0	606.2	
49			7.8	612.4	
48			8.6	611.6	
47+97			9.2	611.0	
47+92			14.2	606.0	
47+87			9.1	611.1	
47			5.6	614.6	
46+27			7.1	613.1	
46+17			13.5	606.7	
46			7.0	613.2	
45+85			4.8	615.4	
45+75			4.3	615.9	
45			4.6	615.6	
44			5.0	615.2	
T.P.			6.36	613.86	
	4.57	618.43			
43			4.6	613.8	
42			5.1	613.3	

B.M. Established by Converse.
Nail Top Oak Stump 45' R Sta 2+75
Richards Road Survey.

P.O.T. 51+68.31 Pipe Line Survey
EC. 2+86.78 Richards Road Survey

Sept. 20, 1927.

Bottom Wash.

Bottom Wash.

Bottom Wash.

P.I.

		618.43		
41+55			4.3	614.1
41			3.4	615.0
40+70			7.0	611.4
40			7.2	611.2
39			9.2	609.2
38			9.2	609.2
T.P.			9.23	609.20
	5.97	615.17		
37			5.0	610.2
36+30			4.6	610.6
36			6.1	609.1
35			8.3	606.9
34			6.0	609.2
33			5.7	609.5
T.P.			6.77	608.40
	6.29	614.69		
32			5.1	609.6
31			6.5	608.2
30			5.5	609.2
29			2.5	612.2
28			3.6	611.1
27			5.2	609.5
T.P.			5.05	609.64
B.M			3.30	611.39

P.I.

P.I.

Nail in Oak Tree 25'L. Sta. 29+85

T.P.				609.64	
	8.38	618.02			
26			8.1	609.9	
25			7.0	611.0	
24			6.6	611.4	
23			5.5	612.5	
22			4.7	613.3	
21			2.3	615.7	
T.P.			2.25	615.77	
	11.25	627.02			
20			9.5	617.5	
19			7.0	620.0	
18			4.6	622.4	
17+65			4.3	622.7	
17			6.0	621.0	
16			7.8	619.2	
15			9.2	617.8	
T.P.			9.26	617.76	
	3.95	621.71			
14+65			5.0	616.7	
14			4.7	617.0	
			11.5	610.2	
13			3.5	618.2	
T.P.			0.47	621.24	
	8.06	629.30			

④

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P. I.

High Water Mark in S.D. River opp. Sta. 14.

		629.30		
12.			7.4	621.9
11+45			3.7	625.6
11			4.4	624.9
B.M.			4.63	624.67
10			3.0	626.3
9+35			4.0	625.3
T.P.			5.88	623.42
	4.83	628.25		
9			3.8	624.4
8			4.3	623.9
7+75			4.6	623.6
7			5.4	622.8
6+63			6.4	621.8
T.P.			6.44	621.81
	7.11	628.92		
6			4.0	624.9
5+70			3.0	625.9
5+50			7.6	621.3
5+35			3.6	625.3
5			2.4	626.5
4+75			2.0	626.9
4			6.7	622.2
T.P.			7.17	621.75
	5.26	627.01		
B.M.			5.67	621.34

P.I.

Nail in Oak Tree 3'R. Sta. 11+50

P.I.

On Hub 6+63.2

Nail in Oak Tree 7'R. Sta. 1+71

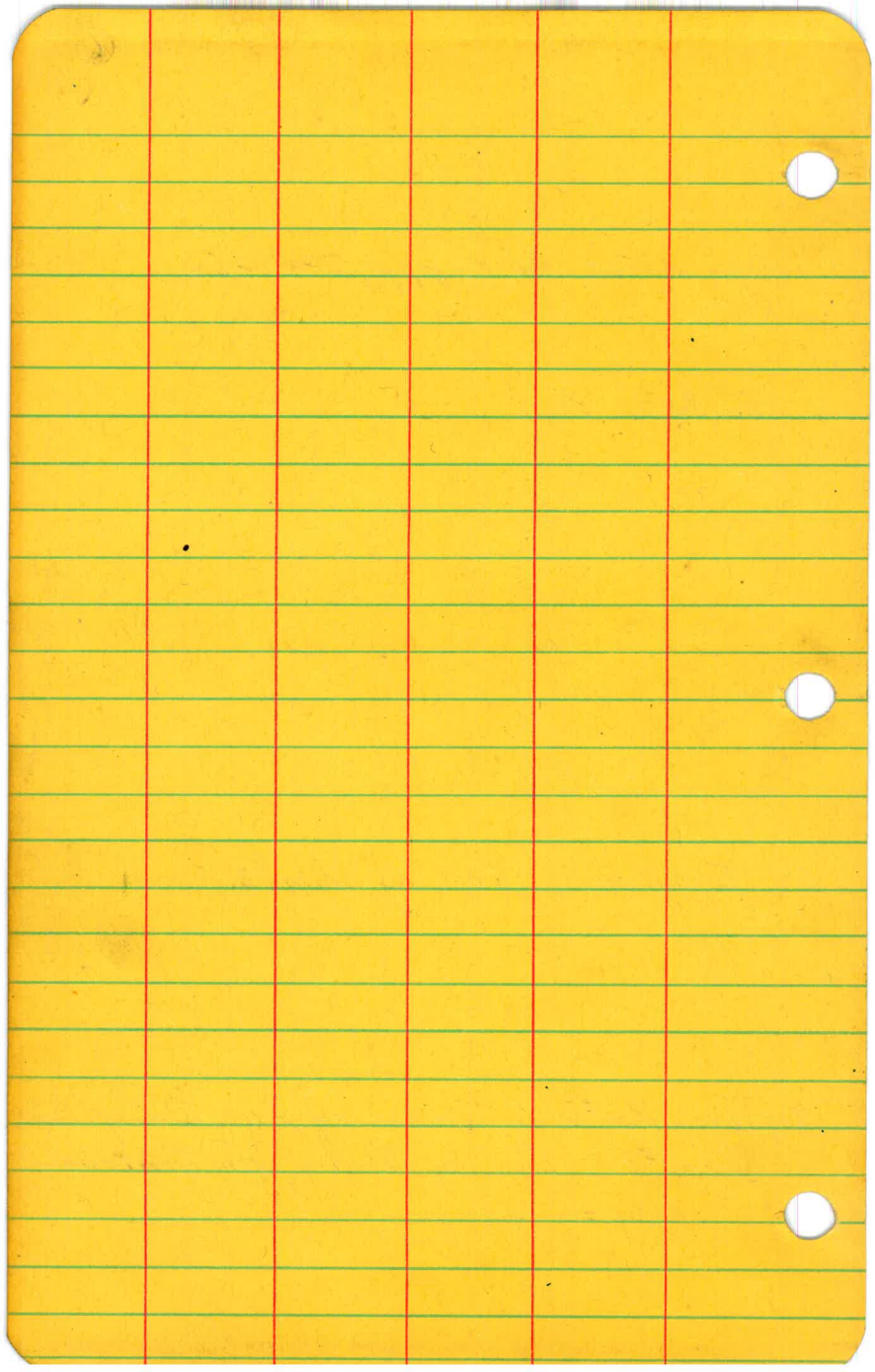
		627.01		
3			4.5	622.5
2			4.3	622.7
			10.5	616.5
1+71 4			4.8	622.2
1+40			7.4	619.6
1+20			+2.1	629.1
1			2.7	624.3
0+60			7.0	620.0
T.P.			1.01	626.00
	11.39	637.39		
0+45			14.2	623.2
0+42			8.5	628.9
0+27.			5.0	632.4
T.P.			0.63	636.76
	12.59	649.32		
0+00			12.4	636.9
T.P.			0.22	649.10
	11.05	660.15		
T.P.			0.67	659.48
	8.65	668.13		
Pin #3.			5.37	662.76

High Water Mark opp. Sta. 1+50
P.I.

On Rocky Point

On Temporary Axis of Dam #3.

Top Iron Pin #3 on Temporary Axis El Capitan
Dam #3. Elev. by Stadia from Contour
Survey = 662.6



(1)
110

Cross Sections of
Right-of-way on Richards
El Capitan County Road
Survey. Sta. 10+00 to
Sta. 138+05.57. (El Monte
Ranch East Line.)
Page 1-29.
Sept.-Oct. 1927.
Converse
Duermit
Rouner
McBain.

Sta.	Elev.
10+00	598.3
+35	597.2
+60	595.4
11.	590.5
+85	581.1
12.	579.4
+25	581.9
+50	586.7

Sept. 27. 1927

III

Left.		℄	Right
598.9	598.5		598.1
+0.6 / 20.0	+0.2 R. / 7.0	R.	-0.2 / 20.0
598.1	597.0		598.0
+0.9 / 20.0	-0.2 R / 8.0	R.	+0.8 / 20.0
596.9	596.5	595.0	597.4	588.0
+1.5 / 20.0	+1.1 / 12.5	-0.4 R / 8.0 R.	+2.0 / 10.0	-7.4 / 20.0
590.0	590.5	590.5	587.9	585.2
-0.5 / 20.0	0.0 R / 10.5	0.0 R. / 3.0	-2.6 / 13.0	-5.3 / 20.0
581.9	581.9	588.6
+0.8 R / 24.0	+0.8 R / 16.0	-2.5 / 20.0
581.4	580.9	579.1
+2.0 R / 31.0	+1.5 R / 20.0	-0.3 / 20.0
585.1	584.8	581.1	579.8
+3.2 R / 20.0	+2.9 R / 10.0	-0.8 / 16.0	-2.1 / 20.0
596.5	587.7	583.5	590.9
+9.8 / 20.0	+1.0 R / 11.5 R.	-3.2 / 8.5	-5.8 / 20.0

Sta.	Elev.
13	594.3
+25	596.7
14	601.7
+55	605.2
15	605.1
+48	605.7
16	607.1
+40	608.2

	L		℄		R	
584.0	581.3	574.7		574.4	567.3	563.3
+9.7 / 20.0	+7.2 / 13.0	R +0.4 / 10.5	0	R +0.1 / 4.8	-7.0 / 15.0	-11.0 / 20.0
		577.4				
Borrow Pit		+0.7 / 20.0	0			
612.0	608.6	602.4		602.1	593.3	588.6
+10.3 / 20.0	+6.9 / 8.7	R +0.4 / 2.0	0	R +0.4 / 5.5	-6.2 / 15.0	-13.1 / 20.0
613.9	611.3	603.3		603.4	598.9	596.8 598.9
+8.2 / 20.0	+6.3 / 13.0	R +0.3 / 5.0	0	R +0.2 / 6.0	-6.3 / 9.0	-8.4 / 13.5 -16.3 / 20.0
612.8	608.5	603.4		603.0		596.8
+7.7 / 20.0	+3.4 / 7.7	R +0.3 / 4.7	0	R -0.1 / 5.0		-8.3 / 20.0
614.5	610.3	603.9		603.9	603.4	598.5
+8.8 / 20.0	+4.6 / 7.7	R +0.2 / 4.0	0	R +0.2 / 4.5	-2.3 / 12.0	-7.2 / 20.0
615.9	612.4	607.4		607.3		598.9
+8.8 / 20.0	+5.3 / 11.0	R +0.3 / 4.3	0	R +0.2 / 5.5		-8.2 / 20.0
615.8	613.2	608.0		608.6	606.7	601.0
+7.6 / 20.0	+5.0 / 13.0	R +0.6 / 5.8	0	R +0.4 / 2.5	-1.5 / 11.0	-7.2 / 20.0

Sta.	Elev.
17.	608.8
18	609.4
+30	609.2
19	609.6
20	610.7
+30	611.3
21	612.3
+16	612.8

Sept. 28, 1927

L.		℄		R.	
614.0	613.8	609.0	R 608.8	607.7	602.3
+5.2	+5.0	+0.2 R	0.0	-5.1	-6.3
20.0	11.0	3.5	4.5	16.5	20.0
620.9	618.0	609.2	R 609.3		601.9
+11.5	+8.6	+0.1 R	-0.1		-7.5
20.0	14.0	6.6	5.0		20.0
621.2	619.1	609.3	R. 609.7	602.0	600.0
+12.0	+9.9	+0.3 R	-0.5	-7.2	-9.2
20.0	15.0	3.3	5.0	17.0	20.0
623.1	616.9	609.7	R 609.6	608.2	598.9
+13.5	+7.3	+0.1 R	0.0	-1.4	-11.2
20.0	11.5	4.4	2.0	7.7	20.0
624.2	619.3	611.3	R 610.7	605.3	600.7
+13.5	+8.8	+0.6 R	0.0	-5.2	-10.0
20.0	10.5	5.7	2.9	12.2	20.0
625.0	621.4	611.4	R. 611.2	610.0	599.3
+13.7	+10.1	+0.1 R.	0.0	-1.3	-11.8
20.0	11.0	4.0	4.0	9.0	20.0
629.3	624.4	612.5	R. 612.5		609.3
+17.0	+12.1	+0.2 R.	+0.2		-8.0
20.0	12.6	2.8	9.0		20.0
625.6	621.7	613.3	R 612.6		604.1
+12.8	+8.9	+0.5 R	-0.2		-8.7
20.0	13.7	6.0	5.7		20.0

Sta.	Elev.
22	612.1
+60	609.5
23	610.8
+38	609.7
24	607.7
25	605.0
+29	604.5
+63	604.0

L.		E		R.	
626.8	620.7	612.4	R. 612.2		602.4
+14.7	+8.6	+0.3	+0.1		-9.7
20.0	10.6	7.0	2.2		20.0
620.3	611.2	610.6	604.9		597.1
+10.8	+1.7	+1.1	-4.6		-12.4
20.0	11.0 R	3.0 R	8.0		20.0
623.9	620.6	610.9			597.1
+13.1	+9.8	+0.1			-13.7
20.0	13.4	10.0 R.	R.		20.0
623.8	619.3	610.2	608.8	609.3	604.0
+14.1	+9.6	+0.5	+0.1	-0.4	-5.7
20.0	10.0	5.0 R.	4.0 R	10.5	20.0
618.3	614.1	608.1	607.8		598.3
+10.6	+7.0	+0.4	+0.1		-9.4
20.0	13.2	6.5 R	3.3 R		20.0
616.8	610.5		605.1	604.1	601.5
+11.8	+5.5		+0.1	-0.3	-3.5
20.0	5.7	R.	9.0 R	14.4	20.0
611.2	608.2	605.1	604.5	603.8	600.1
+6.7	+3.7	+0.6	0.0	-0.7	-4.4
20.0	10.7	6.5 R	4.2 R	11.6	20.0
607.4	604.1	604.2	604.3		598.0
+3.4	+0.7	+0.2	+0.3		-6.0
20.0	13.5	6.7 R	3.3 R		20.0

Sta.	Elev.
26	603.8
+64	601.9
27	600.7
+55	598.6
28	598.2
29	597.4
+35	596.8
30	595.6

L.		℄		R.	
611.9	609.8	604.4	603.8		597.5
+8.1	+6.0	+0.6	0.0		-6.3
20.0	12.7	8.5 R	5.0 R		20.0
613.1	609.7	602.6	602.8		596.6
+11.2	+7.8	+0.7	+0.1		-5.3
20.0	11.3	5.0 R	7.8 R		20.0
614.5	609.2	603.7	600.6		594.2
+13.8	+8.5	+3.0	-0.1		-6.5
20.0	11.0	5.4 R.	6.5 R		20.0
612.1		599.6			585.8
13.5		+1.0			-12.8
20.0		10.5 R	R		20.0
611.2	607.3	590.6			585.0
+13.0	+9.1	+0.4			-13.2
20.0	14.7	9.0 R.	R		20.0
606.6	603.6	597.4	596.9		583.7
+9.2	+6.2	0.0	-0.5		-11.7
20.0	12.4	7.4 R.	5.5 R		20.0
606.5		597.1	596.9	595.5	588.7
+9.7		+0.3	0.0	-1.3	-8.1
20.0		6.0 R	4.6 R	10.2	20.0
601.9	599.7	596.6	595.6		590.6
+6.2	+4.1	+1.0	0.0		-5.0
20.0	11.8	8.0 R.	6.5 R.		20.0

Sta.	Elev.
+64	595.2
31	596.0
32+09	601.7
33	600.2
34	598.7
35	597.1
36	599.5
37	598.4

L.		℄		R.	
601.2	596.2	595.2	595.1		591.7
+6.0	+1.0	0.0	-0.1		-3.5
20.0	11.8	6.0 R	4.0 R		20.0
606.0	601.2	596.8	596.0	594.9	592.5
+10.0	+5.2	+0.8	0.0	-1.1	-3.5
20.0	7.0	3.8 R	6.6 R	14.7	20.0
608.0	606.9	602.2	601.7		597.9
+6.3	+5.2	+0.5	0.0		-3.8
20.0	15.0	6.0 R	7.0 R		20.0
602.9		600.8	600.3		597.7
+2.7		+0.6	+0.1		-2.5
20.0		8.4 R	8.3 R		20.0
602.3		599.9	598.8		597.6
+3.6		+1.2	+0.1		-1.1
20.0		3.3 R	10.0 R.		20.0
599.9		597.6			592.9
+2.8		+0.5			-4.2
20.0		7.5 R.	R.		20.0
606.9		603.0	599.1		596.9
+7.4		+3.5	-0.4		-2.6
20.0		6.0	11.6 R		20.0
604.3	601.1	598.6	598.6		594.0
+5.9	+3.3	+0.2	+0.2		-4.4
20.0	10.4	5.0 R	7.4 R		20.0

Sta.	Elev.
38	599.7
+60	599.5
39	598.6
+25	598.4
+60	599.9
40	597.V
+55	597.3
41	594.9

L.		℄		R.	
610.8	605.7	600.0	600.0		594.4
+11.1	+6.0	+0.3	+0.3		-5.3
20.0	8.4	1.7 R	9.4 R.		20.0
612.5		608.6	598.8		596.1
+13.0		+9.1	-0.7		-3.4
20.0		11.3 R	14.8 R		20.0
604.1	603.2	598.9	598.5	595.6	593.1
+5.5	+4.6	+0.3	-0.1	-3.0	-5.5
20.0	14.0	8.5 R.	7.4 R	10.8	20.0
600.1		598.8	598.2	595.7	590.7
+1.7		+0.4	-0.2	-3.2	-7.7
20.0		7.8 R	7.7 R.	10.7	20.0
604.6	602.9	600.4	599.9	597.6	595.9
+4.7	+3.0	+0.5	0.0	-2.3	-4.0
20.0	10.4	4.0 R	8.8 R	12.8	20.0
603.7	602.0	597.5	597.2	594.7	592.9
+6.5	+4.8	+0.3	0.0	-2.5	-4.3
20.0	14.0	7.8 R	7.2 R	12.4	20.0
605.1	601.6	597.7	597.2		590.7
+7.8	+4.3	+0.4	-0.1		-6.6
20.0	12.0	5.0 R	6.0 R		20.0
603.6	600.2	595.4	595.0	589.6	587.6
+8.7	+5.3	+0.5	+0.1	-5.3	-7.3
20.0	10.0	5.0 R	8.2 R	14.8	20.0

Sta.	Elev.
42	591.1
43	588.5
44	589.5
45	589.7
46	590.8
47	590.5
48	581.6
49	576.2

	L.			R.	
600.4 +9.3 20.0		591.6 +0.6 3.5 R.	591.1 0.0 6.3 R.		590.3 -0.8 20.0
599.2 +10.7 20.0	594.9 +6.4 12.6	588.8 +0.3 5.5 R.	588.5 -0.2 6.3 R	585.4 -3.1 11.0	582.2 -6.3 20.0
598.3 +8.8 20.0	593.9 +4.3 8.0	589.8 +0.3 2.7 R.	589.2 -0.3 8.3 R	586.0 -3.5 12.6	582.5 -7.0 20.0
599.7 +10.0 20.0	596.2 +6.5 13.2	590.2 +0.5 6.7 R	589.9 +0.2 3.4 R	587.2 -2.5 7.0	578.4 -11.3 20.0
601.6 +10.8 20.0	598.1 +7.3 11.4	591.3 +0.5 8.0 R	590.8 0.0 4.8 R		581.7 -9.1 20.0
603.3 +12.8 20.0	598.6 +8.1 8.5	590.9 +0.4 5.0 R	590.7 +0.2 8.0 R		581.9 -8.6 20.0
589.6 +8.0 20.0		582.0 +0.4 13.0 R	576.1 -5.5 12.4 R		574.0 -7.6 20.0
590.2 +14.0 20.0	581.7 +5.5 11.6	576.3 +0.1 3.5 R	576.4 +0.2 7.7 R	575.7 -0.5 13.5	565.6 -10.6 20.0

Sta.	Elev.
+40	575.8
50	577.5
+50	577.4
51	577.3
52	576.7
+50	576.8
53	576.9
54	580.6

L.		℄		R.	
586.8		576.0	575.8	572.2	568.7
+11.0		+0.2	0.0	-3.6	-7.1
20.0		4.3	6.3	12.4	20.0
		R	R		
582.2		577.5	571.4	572.3	568.2
+4.7	+4.1	0.0	-6.1	-5.2	-9.3
20.0	15.3	12.5	7.3	H.W.M.	20.0
		R	R.		
585.7	583.0	577.5	577.4	571.5	566.1
+8.3	+5.6	+0.1	0.0	-5.9	-11.3
20.0	12.0	4.1	6.3	12.6	20.0
		R	R		
582.0		578.0	577.1	573.1	569.6
+4.7		+0.7	-0.2	-4.2	-7.7
20.0		9.0	6.6	10.7	20.0
		R	R		
582.2		577.1	576.7		571.0
+5.5		+0.4	0.0		-5.7
20.0		5.3	7.0		20.0
		R	R.		
580.5	579.0	576.9	576.6		574.5
+3.7	+2.2	+0.1	-0.2		-2.3
20.0	12.6	10.0	8.4		20.0
		R	R		
581.6	580.0	577.4	577.0		574.1
+4.7	+3.1	+0.5	+0.1		-2.8
20.0	10.5	7.7	5.5		20.0
		R	R		
583.1	580.9	586.6	576.5		
+2.5	+0.2	+6.	-1.1		
20	15.3	7 R	20		
	R				

Sta.		Elev			
55		579.8			
56		576.7			
57		574.6			
58		575.8			
59		574.6			
60		578.6			
61		580.3			
450		579.6			

L		℄		R	
	591.2 +1.4 20	580.3 +0.5 6.5 R	580.3 +0.5 3.0 R	579.4 −0.1 20	
	591.6 +4.9 20	577.3 +0.6 7.5 R	577.1 +0.9 5.0 R	576.7 0.0 20	
582.4 +7.8 20	578.5 +3.9 11.0	574.8 +0.2 4.5 R	574.6 0.0 R 5.5	573.7 −0.9 20	
582.9 +7.1 20	581.0 +5.2 15	576.1 +0.3 5.0 R	575.9 +0.1 5.0 R	572.2 −3.6 20	
582.6 +6.0 20.	579.3 +2.7 10.0	576.9 +0.3 5.0 R	576.6 0.0 5.7 R	581.1 4.5 20.	
586.5 +7.9 20.	581.5 +3.2 9.0	579.1 +0.5 5.0 R	578.9 +0.3 5.5 R	578.6 0.0 10.3	575.1 −3.5 20.
589.8 +9.5 20.	583.9 +3.6 9.0	580.8 +0.5 4.7 R	580.0 +0.5 4.6 R	581.2 +0.9 9.5	577.9 −2.1 16. 577.5 −2.8 20
584.9 +5.3 20	583.0 +3.4 10.0	580.2 +0.6 4.4 R	579.3 −.3 4.6 R	579.2 −0.4 10.	576.1 −3.5 20

Sta.	Elev.
62	577.9
+76	572.0
63	560.6
+22	569.8
+25	564.7
+82	563.1
64	558.9
+57	566.0

L					
	581.7	578.0	578.2	575.0	574.4
	+3.8 / 20	+ 0.1 / R 10.0 R	+0.3 / 3.0	-2.9 / 13.	-3.5 / 20
574.4 574.7	573.1	572.8	562.7	559.0	558.9
+2.4 / 20. +2.7 / 15.6	+1.1 / 12.3 R	+0.8 / 4.0 R	- 9.3 / 3.0	-13.0 / 10.	-13.1 / 20.
573.3	572.3	561.6	557.9	557.8	
+12.7 / 20 R	+ 11.7 / 11.0 R	+10. / 2.0	- 2.7 / 8.5	-2.8 / 20	
	572.6	572.1	561.5	562.4	557.4
	+2.8 / 27. R	+12.3 / 15.5 R	- 5.3 / 1.0	-7.4 / 6.0	-12.8 / 7.0 -12.3 / 20.
573.1	572.5	570.1	562.7	557.7	557.5
+8.4 / 27. R	+7.8 / 16.0 R	+ 5.4 / 1.	- 2.0 / 6.6	-7.0 / 7.5	-7.2 / 20.
570.8 570.5	570.0	566.2	560.4	556.6	556.5
+7.7 / 29. R +7.4 / 20 R	+6.9 / 12.	+3.1 / 10.	- 2.7 / 3.0	-6.5 / 10.	-6.6 / 20.
569.7 569.6	568.9	562.4	556.9	556.9	
+ 10.8 / 27. R +10.7 / 17. R	+10. / 7.0	+ 3.5 / 4.0	- 2.0 / 11.	-2.0 / 20.	
572.7	569.1	568.9	558.3	556.2	
+ 6.7 / 20.	+ 3.1 / 13.6 R	+2.9 / 4.6 R	- 2.7 / 4.5	-9.8 / 20.	

Sta.	Elev	
65	568.3	
+40	568.7	H.W.M. 565.7
+83	572.7	
66	573.6	
+55	575.8	
67	573.6	
68	570.0	
69	569.0	

12

	L	℄	R		
	574.1	568.3	568.0	564.4	556.9 556.9
	+5.8 / 20	0.0 / 11.R	-0.3 / 3.0	-3.9 / 9.0	-11.4 / 15.5 -11.4 / 20
579.4	575.2	569.4	568.6	563.2	560.7
+10.7 / 20.	+6.5 / 14	+0.2 / 8.0 R	-0.1 / 5.0 R	-5.5 / 10.5	-8.0 / 20
~~581.1~~ 581.8	577.3	573.0	572.7	568.7	565.4
+8.4 / 20	+4.6 / 10.0	+0.3 / 4.7 R	0.0 / 6.0 R	-4.0 / 13.5	-7.3 / 20.
579.1	576.9	573.7	573.8	570.3	568.6
+5.5 / 20.	+3.3 / 12.5	+0.1 / 4.0 R	+0.8 / 5.0 R	-3.3 / 17.5	-5.0 / 20.
580.5	579.4	576.3	576.3	572.7	
+4.7 / 20	+3.6 / 12.3	+0.5 / 5.5 R	+0.5 / 4.5 R	-3.1 / 20.	
	579.2	574.8	574.1	571.1	
	+5.6 / 20.	+1.2 / 6.0 R	+0.5 / 8.5 R	-2.5 / 20.	
573.7	572.8	570.6	569.9	562.0	
+3.2 / 20.	+2.8 / 15.0	+0.6 / 11.0 R	-0.1 / 5.5	-8.0 / 20	
575.2	573.0	569.5	569.1	564.3	561.3
+6.2 / 20.	+4.0 / 15.	+0.5 / 11.0 R	+0.1 / 3.0	-4.7 / 11.	-7.2 / 20

Sta.	Elev.
70	569.9
+97	569.0
72	570.0
73	568.7
74	567.6
+41	567.0
75+04	568.2
+46	568.3

123

L		℄	R	
571.3	573.9	570.3	570.2	565.2
+7.4	+4.0	+0.4	+0.3	-4.7
20	6.0	2.0 R	8.0 R	20
576.3	573.6	569.7	568.9	567.3	559.7
+7.3	+4.6	+0.2	-0.2	-1.7	-9.3
20	11.0	4.6 R	3.0 R	10.	20.
574.0	572.6	570.7	569.6	566.4
+4.0	+2.6	+0.7	-0.4	-3.6
20	13.5	7.0 R	7.5 R	20.
		573.1	568.6	565.4
		+4.4	-0.1	-3.3
		20 R	7.0 R	20.
573.9	572.5	567.8	568.1	565.2
+6.3	+4.9	+0.2	+0.5	-2.4
20	16.5	8.9 R	5.0	20.
573.8	571.3	P 567.6	567.1	565.2	565.0
+6.8	4.3	0.6	+0.1	-1.8	-2.0
20.	12.5	7.4 R	5.5 R	14.5	20.
572.9	570.7	568.0	568.4	568.3	564.7
+4.7	+2.5	+0.6	+0.2	+0.1	-3.5
20	8.4	3.5 R	7.5 R	13.0	20.
573.8	571.5	568.9	568.6	568.7	564.6
+5.5	+3.2	+0.6	+0.3	-0.1	-3.7
20.	11.	4.5 R	6.3 R	9.5	20.

Sta.		Elev.			
76					
+1					
+11		566.9			
+22		570.2			
+77		568.1			
+66		566.4			
+83		565.7			
78		565.5			
79		565.6			
80		563.2			

	L	℄	R	
578.1	571.0	571.0	557.6	554.9
+11.2	+4.1	+4.1	-9.3	-12.
20	16.4 R	7.4 R	13.	20
575.3	570.0	570.9	569.0	559.2
+5.1	-0.2	+0.2	-1.2	H.W.M. 562.0 -11.
20.	13.7 R	4. R	4.5	20.
570.3	575.0	568.9	568.1	567.9 561.8
+10.2	+6.9	+0.8	00	-0.2 -6.3
20.	12.5	5.2 R	6.0 R	10.5 20.
575.5	572.9	566.9	566.4	559.1 558.2
+9.1	+6.5	+0.5	00	-7.3 -8.2
20.	11.7	5.0 R	5.5	12.0 20.
585.3	580.7	566.2		
+19.6	+15.2	+0.5	over large rock	
20.	12.0	R 5.0		
576.1 575.8	570.9	566.2	565.2	565.2 556.8
+10.6 +10.3	+5.4	+0.7	-0.3	-0.3 -8.7
20. 16.	10.5	3.0 R	7.0 R	12. 20.
	570.2	566.0	565.5	565.6 563.6
	+4.6	+0.4	-0.1	0.0 -2.0
	20.	5.2 R	5.3 R	12.5 20.
		564.9	563.3	560.6
		+1.2 R	+0.1	-2.6
		20.	9.7 R	20

Sta.	Elev	
81	563.6	H.W.M. 561.6
82	563.9	
+80	563.2	
83	565.5	
84+07	568.1	
85	568.1	
+82	569.6	
86	570.0	

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L ℄ R

570.3 +6.7 20.	568.1 +4.5 12.3	563.9 +0.3 6.5R	563.7 +0.1 4.5	563.2 -0.4 11.	559.4 -4.2 20.
567.8 +3.9 20	567.1 +3.2 17.5	564.2 +0.3 R 12.R	563.7 -0.2 6.0	561.3 -2.6 11.0	560.5 -3.4 20.0
564.0 +0.8 20.	564.9 +1.7 16.0R	564.4 +1.2 6.5R	559.2 -4.0 20		
	568.9 +3.4 20.	565.5 0.0 R 9.0R	565.8 +0.3 9.5	561.2 -4.3 20.	
571.9 +3.8 20.	570.7 +2.6 10.5	568.6 +0.5 5.0R	568.1 0.0 6.5R	565.6 -2.5 20.	
575.1 +7.0 20.	571.8 +3.7 10.0	568.3 +0.2 6.0R	568.1 0.0 4.5R	568.0 -0.1 9.5	565.1 -3.0 20
573.0 +3.4 20	570.0 +0.4 12.0	569.8 +0.2 6.R	569.7 +0.1 5.5R	566.2 -3.4 15.	565.9 -3.7 20.
576.8 +6.8 20.	574.4 +4.4 13.	570.0 +0.0 8.0	570.0 0.0 5.0R	569.8 -0.2 7.3R	565.8 -4.2 20

Sta.		Elev.			
86					
+41		571.5			
87		574.5			
+78		580.0			
88		580.5			
89		588.6			
+35		590.3			
90		584.6			
91		576.6			

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	L		℄		R	
	582.0		577.5	571.6	568.2	
	+10.5		+6.0 R	+0.1	−3.3	
	20.		6.0	11.0 R	20.0	
	587.0		581.6	575.5	576.2	573.9
	+12.5		+7.1	+1.0	+1.2	−0.7
	20.		7.0 R	8.0 R	14.0	20
589.5	585.0		580.3	580.0	571.7	
+9.5	+5.0		+0.3	0.0	−8.3	
20	10.0		4.5 R	6.5 R.	2.0	
591.0	585.5		580.9	581.3	574.1	
+10.5	+5.0		+0.4	+0.8	−6.4	
20.	7.5		4.5 R	6.5 R	20.	
598.4	592.7		589.2	589.6	581.0	
+9.8	+7.1		+0.6	+1.0	−7.6	
20.0	15.0		8.5 R	4.0 R	20.	
600.3	595.3		590.8	590.5	590.5	587.6
+10.0	+5.0		+0.5	+0.2	+0.2	−2.7
20.	9.5		4.0 R	6.5 R	13.2	20.
	597.6		590.6	585.7	582.6	
	+13		+6.0 R	+0.6	−2.0	
	20.		3.0	11. R	20	
589.3	582.5		576.9	576.7	569.2	
+12.7	+5.9		+0.3	0.1	−7.4	
20	8.4		5.3 R	6.2 R	20.	

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Sta. 91		Elev.		
+ 13		576.0		
+ 52		573.1		
+ 89		571.0		
92+00		570.3		
+61		565.6		
93+00		563.1		
+ 52		560.9		
94+00		559.4		
+55		558.6		

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589.6	586.8 L	576.6	576.4 R	570.0
+12 6 / 20 0	+10 8 / 16 5	+0 6 / 7 5	+0 4 / 6 2	-7 0 / 20 0
581.2	580.0	573.3	573.4	564.1
+14 1 / 20 0	+6 9 / 8 0	+0 2 / 4 5	+0 3 / 5 4	-9 0 / 20 0
583.1	579.0	571.0	570.4	571.9	565.0
+12 1 / 20 0	+8 0 / 11 6	0 0 / 7 2	+0 4 / 6 5	+0 9 / 10 8	-6 0 / 20 0
583.0	577.3	570.3	570.7	570.0	565.6
+12 7 / 20 0	+7 0 / 10 7	0 0 / 7 5	+0 4 / 7 0	-0 3 / 13 0	-4 7 / 20 0
574.1	571.6	566.5	566.2	566.2	560.6
+8 5 / 20 0	+6 0 / 12 7	+0 9 / 10 0	+0 6 / 5 2	+0 6 / 10 4	-5 0 / 20 0
571.6	568.1	563.6	563.4	559.7
+8 5 / 20 0	+5 0 / 9 6	+0 5 / 5 7	+0 3 / 7 9	-3 4 / 20 0
564.7	561.2	560.7	557.1
+3 8 / 20 0	+0 3 / 6 6	-0 2 / 5 0	-3 8 / 20 0
563.9	560.1	559.4	557.7
+4 5 / 20 0	+0 7 / 5 0	0 0 / 7 0	-1 7 / 20 0
562.6	559.1	558.8	555.0
+4 0 / 20 0	+0 5 / 7 4	+0 2 / 4 4	-3 6 / 20 0

Sta.		Elev			
95+00		558.3			
+58		559.7			
+78		561.0			
96+00		560.9			
+67		557.1			
97+00		555.1			
98+00		552.6			
99+00		551.5			

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L		E		R	
565.3	561.3	558.9	558.3	555.5	
+7 20	+3 8	+0 6 3 8	0 8 3	-2 8 20	
564.5	563.5	560.0	560.1	557.1	
+4 8 20	+3 8 14	+0 3 8 5	+0 4 4 5	-2 6 20	
565.5	563.7	561.4	561.5	561.8	558.2
+4 5 20	2 7 10 4	+0 4 7	+0 2 3 8	+0 8 9 4	-2 8 20
564.9	564.0	561.2	561.2	562.0	559.1
+4 0 20	+3 1 9 8	+0 3 5 4	+0 3 4 4	+1 1 12 2	-1 8 20
	562.1	557.8	557.1		553.1
	+5 0 20	+0 7 6 2	0 0 4 2		-4 0 20
	560.7	555.6	555.0	554.3	552.1
	+5 6 20	+0 6 3 3	-0 1 6 7	-0 8 14 2	-3 0 20
	556.6	553.4	552.1		550.3
	+4 0 20	+0 8 5 5	-0 5 5 0		-2 3 20
	554.4	551.9	551.2		546.9
	+2 9 20	+0 4 7 3	-0 3 6 2		-4 6 20

Sta.	Elev.
99+76	550.7
100+00	550.0
+76	548.7
101	548.5
+16	548.3
+54	548.1
+91	548.0
102	547.9

129

L	C	R	
554.2	551.3	550.3	546.3
+3 5 / 20	+0 6 / 10 5	−0 4 / 7 3	−4 7 / 20
553.2	550.5	550.0	545.5
+3 2 / 20	+0 5 / 6 5	0 / 5	−4 5 / 20
554.8	549.1	548.8	544.9
+6 1 / 20	+0 4 / 4 8	+0 1 / 4 5	−4 3 / 20
552.6	548.8	548.8	543.2
+4 1 / 20	+0 3 / 6 4	+0 3 / 2 6	−5 3 / 20
557.6	553.3	548.6	548.6	543.7
+9 3 / 20	+5 0 / 6 3	+0 3 / 4 7	+0 3 / 7 3	−4 6 / 20
552.0	549.2		543.7
+3 9 / 20	+1 1 / 13 5		−4 9 / 20
557.4	548.3	548.2	543.0
9 4 / 20	+0 3 / 5 7	+0 2 / 4 8	−5 0 / 20
557.5	548.4	547.9	543.0
9 6 / 20	+0 5 / 6 0	0 / 5 0	−4 9 / 20

Sta.	Elev
103+00	548.8
+72	547.1
104	545.2
+39	542.9
105	541.9
106	538.9
+25	538.4
+55	538.7

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L		℄	R
564.1	549.8	548.8	538.3
+15 3	+1 0	0 0	−10 5
20 0	7 0	5 0	20 0
563.9	547.3	547.1	536.3
+16 8	+0 3	0 0	−10 8
20 0	8 0	4 0	20 0
554.2	545.7		533.8
+9 0	+0 5		−11 4
20 2	12 7		20 0
558.0	543.4	542.3	538.3
+15 1	+0 5	−0 6	−4 6
20 0	7 0	6 3	20 0
553.0	542.2	541.2	538.9
11 1	+0 3	−0 7	−3 0
20 0	9 3	10 0	20 0
553.6	539.5	538.7	532.8
+14 7	+0 6	−0 2	−6 1
20 0	11 3	8 8	20 0
549.6	538.2		532.1
+11 2	−0 2		−6 3
20 0	12 7		20 0
544.2	539.0		532.0
+5 5	+0 3		−6 7
20 0	15 6		20 0

Sta.	Elev.
106+85 ℄ = 106+81 ℄ Equa.	538.5
107	538.6
+74	537.5
108	537.5
+44	537.6
109	537.3
110	536.4
+20	536.0

131

L	C		R
542.3	538.8	538.3	531.6
+3 9	+0 3	−0 2	−6 9
20 0	8 6	3 8	20 0
547.1	538.9	538.5	531.7
+8 5	+0 3	−0 1	−6 9
20 0	8 5	4 2	20 0
544.4	540.3	537.5	537.5	532.1
+6 9	+2 8	0 0	0 0	−5 4
20 0	10 0	5 8	6 0	20 0
	542.2	537.6	536.6	533.3
	+4 7	+0 1	−0 9	−4 2
	20 0	4 6	9 5	20 0
	542.3	537.6	~~537.1~~ 537.5	535.1
	+4 7	0 0	−0 1	−1 9
	20 0	8 3	6 6	20 0
542.9	540.3	537.5	537.1	537.3
+5 6	+3 0	+0 2	−0 2	0 0
20 0	15 0	9 6	5 7	20 0
	542.8	536.3	536.4	534.3
+	6 9	−0 1	0 0	−2 1
	20 0	3 0	6 9	20 0
540.7	538.4	536.0	535.8	533.6
+4 7	+2 4	0 0	−0 2	−2 4
20 0	11 8	4 2	5 3	20 0

Sta.	Elev
110+45	536.0
111+00	536.6
+33	536.2
+67	535.2
112	534.4
+74	532.7
113+04	533.2
+32	533.5

137

L	℄		R
542.7	536.2	535.7	533.8
+6 7 / 20	+0 2 / 5 2	-0 3 / 7 2	-2 2 / 20
542.0	536.9	536.8	535.0
+5 1 / 20	+0 3 / 9	+0 2 / 4 3	-1 6 / 20
542.4	536.2	536.1	535.3
6 2 / 20	0 / 8 2	-0 1 / 6 3	-0 9 / 20
539.2	535.1	535.2	534.2
+4 / 20	-0 1 / 5	0 / 4 3	-1 / 20
537.3	534.4	534.2	534.~
+2 9 / 20	0 / 7 8	-0 2 / 4	-0 2 / 20
539.7	533.1	532.9	535.2
+7 / 20	+0 4 / 7 6	+0 2 / 5 8	+2 5 / 20
539.2	538.2	533.4	533.0	535.6
+6 / 20	+5 / 12 8	+0 2 / 4 8	-0 2 / 5 4	+2 4 / 20
538.3	537.2	533.8	532.5	534.9
+4 8 / 20	+3 2 / 10 3	+0 3 / 3 2	-1 / 13	+1 4 / 20

Sta.	Elev
113+83	537.0
114+00	537.0
+63	538.2
+84	537.8
115	537.4
+65	537.0
116+00	536.6
+41	536.1
117+00	536.0

133

	L		E	R.	
539.3	539.7	537.2	536.6	531.4	
+2 3 / 20	+1 7 / 9 3	+0 2 / 8 5	−0 1 / 4 5	−5 6 / 20	
	539.5	537.4	534.0	532.0	
	+2 5 / 20	+0 1 / 9	−3 0 / 7	−5 0 / 20	
	540.4	538.6	538.3	531.4	
	+2 2 / 20	+0 1 / 3 9	+0 1 / 5	−6 8 / 20	
	540.2	538.2	537.8	531.7	
	+2 1 / 20	+0 1 / 5	0 / 9 1	−6 1 / 20	
	540.4	537.7	537.4	533.3	532.2
	+3 0 / 20	+0 3 / 6 6	0 / 6	−4 1 / 14 1	−5 2 / 20
	537.8	537.2	537.2	536.2	
	+0 8 / 20	+0 2 / 7 1	+0 2 / 4 7	−0 8 / 20	
	537.2		537.0	537.1	
	+0 6 / 20		+0 1 / 9	+0 5 / 20	
	536.2		536.2	536.1	
	+0 1 / 20		+0 1 / 7 3	0 / 20	
	535.9	536.2	536.3	535.6	
	−0 1 / 20	+0 2 / 8 8	+0 3 / 9 3	−0 4 / 20	

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Sta.	Elev.
119+00	535.5
+50	535.7
119+00	538.6
+83	534.8
120+00	534.7
+19	534.8
+54	533.9
121+00	533.4

134

L		E		R
537.5	535.7	535.7	534.5	
+2 20	+0 8 3	+0 6 5	−1 20	
540.7	536.0	535.8	535.4	
+5 20	+0 3 7	+0 1 4 7	−0 3 20	
539.3		538.5	536.1	
+0 7 20		−0 1 5 3	−2 5 20	
535.8	534.9		534.2	
+1 20	+0 1 8 3		−0 6 20	
533.2	534.9		535.4	
−1 5 20	+0 2 4 7		+0 7 20	
535.3	535.0	535.0	533.0	
+0 7 20	+0 2 6 7	+0 2 7 5	−1 8 20	
535.4	534.3	533.9	532.4	
+1 5 20	+0 9 7 7	0 2 6 0	−1 5 20	
535.4	534.1	533.4	531.4	
+2 20	+0 7 7 3	0 2 6 2	−2 20	

Sta.	Elev.
122+00	532.1
+18	531.9
123+00	530.1
+83	529.4
124	528.7
+39	527.4
+94	527.5
125+48	529.8

135

	L 537.1		℄ 532.3	R 529.7	
	+5 / 20		+0 / 11	−2 / 20	
	536.6	534.3	531.7	530.1	
	+4 / 20	+2 / 7	−0 / 7	−1 / 20	
	536.1	530.6	530.5	525.9	
	+6 / 20	+0 / 8	+0 / 7	−4 / 20	
543.9	538.9	529.7	529.4	526.3	523.9
+14 / 20	+9 / 12	+0 / 7	0 / 3	−3 / 10	−5 / 20
543.9	537.1	528.9	528.8	523.9	522.0
15 / 20	+8 / 8	+0 / 5	+0 / 3	−4 / 15	−6 / 20
541.8	538.7	527.4	527.4	521.9	521.4
14 / 20	+10 / 10	0 / 5	0 / 3	−6 / 12	−6 / 20
538.9	537.4	527.8	527.6	521.5	521.3
+11 / 20	+9 / 10	+0 / 5	+0 / 4	−6 / 16	−6 / 20
536.5	532.5	530.1	529.9	523.5	522.3
+6 / 20	+2 / 5	+0 / 4	+0 / 5	−6 / 16	−7 / 20

Sta.		Elev.
126+00		531.0
+35		530.6
+83		530.5
127+00		531.1
128+00		530.9
+41		531.4
+89		531.3
129+00		531.3
+34.32 = +36.01	E.C.	531.1

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537.0 +6 0 20 0	533.1 +2 1 5 6	531.1 +0 1 5 4	530.9 −0 1 5 5	526.3 −4 7 20 0	
533.6 +3 0 20 0	532.4 +1 8 8 5	530.9 +0 3 8 1	528.6 −2 0 6 0	528.0 −2 6 20 0	
	533.0 +2 5 20 0	530.9 +0 4 9 0	530.6 +0 1 6 0	528.4 −2 1 20 0	
	533.6 +2 5 20 0	531.4 +0 3 6 0	531.4 +0 3 9 0	530.1 −1 0 18 0	528.1 −3 0 20 0
	532.4 +1 5 20 0	530.9 0 0 3 4	530.8 −0 1 6 0	529.0 −1 9 9 8	527.4 −3 5 20 0
	536.2 +4 8 20 0	531.5 +0 1 6 0	531.5 +0 1 7 2	526.3 −5 1 20 0	
539.1 +7 8 20 0	534.0 +2 7 7 8	531.7 +0 4 5 3	531.3 0 0 6 5	528.2 −3 1 10 2	526.3 −5 0 20 0
539.9 +8 6 20 0	534.3 +3 0 8 0	531.8 +0 5 5 3	531.2 −0 1 7 0	528.3 −3 0 11 0	526.4 −4 9 20 0
541.1 +10 8 20 0	534.7 +3 6 7 3	531.5 +0 4 3 5	531.2 +0 1 6 2	527.4 −3 7 13 3	527.1 −4 0 20 0

Sta.		Elev.
130+00		530.4
+41		530.8
131		531.6
132		534.1
+40		534.8
133		540.4
+45		542.0
+79	P.I.	542.6
134		542.5

137

541.0 +10 6 20 0	535.6 +5 2 12 8	530.2 −0 2 7 5	530.4 0 0 3 5	529.2 −1 2 20 0
538.8 +8 0 20 0	529.9 −2 9 9 9	530.7 −0 1 7 8	530.8 0 0 4 5	529.9 −0 9 20 0
543.1 +11 5 20 0	539.2 +7 6 15 5	534.2 +2 6 4 0	531.6 0 0 9 7	531.9 −0 3 20 0
	535.4 +1 3 20 0	534.4 +0 3 10 0		532.8 −1 3 20 0
	536.0 +1 2 20 0	535.2 +0 4 9 3		533.4 −1 4 20 0
548.4 +8 0 20 0	546.4 +6 0 11 0	540.9 +0 5 7 8	540.3 −0 1 4 7	531.2 −9 2 20 0
	549.3 7 3 20 0	545.5 +3 5 2 0	542.2 +0 2 12 0	538.5 −3 5 20 0
548.1 +5 5 20 0	546.1 +3 5 8 7	542.5 −0 1 6 0	542.7 +0 1 6 5	537.5 −5 1 20 0
547.9 +5 4 20 0	546.0 +3 5 11 4	543.0 +0 5 8 9	542.5 0 0 5 0	536.7 −5 8 20 0

Sta.	Elev.	
134+73	543.4	
135	544.5	
+36	544.5	
136	544.7	
+60	546.2	
137	544.6	
138	539.0	
+05 57	538.5	— Gate El Monte Rancho.

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	R		L		
549.2 +4 8 20 0	546.3 +2 9 12 4	543.5 +0 1 6 3	543.2 −0 2 7 2	540.0 −2 6 20 0	
549.7 +5 2 20 0	548.3 +3 8 13 2	545.1 +0 6 7 8	544.3 −0 2 6 0	542.4 −2 1 10 6	540.2 −4 3 20 0
550.9 +6 4 20 0	548.3 +3 8 11 2	545.2 +0 2 6 2	544.6 +0 1 3 7	541.0 −3 5 12 2	539.1 −5 1 20 0
550.9 +6 2 20 0	548.3 +3 6 8 8	545.2 +0 5 3 8	544.8 +0 1 8 4	542.7 −2 0 14 0	541.9 −2 8 20 0
	548.2 +2 0 20 0	546.3 +0 1 6 4	545.6 −0 6 7 3	544.5 −1 7 20 0	
	545.9 +1 3 20 0	545.0 +0 4 7 6	543.9 −0 7 6 6	543.6 −1 0 20 0	
541.8 +2 8 20 0	540.0 +1 0 15 0	539.3 +0 3 7 5	539.0 0 0 7 8	538.6 −0 4 20 0	
	540.0 +1 5 20 0	538.7 +0 2 8 0	538.5 0 0 6 5	537.9 −0 6 20 0