

BARRETT-DULZURA  
COND. LINE.

W27

~~██████████~~

400

LEVEL

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

Dulzura Conduit  
Book No 3

June 1907

MINUTES	LKS.	MINUTES	LKS.	MINUTES	LKS.
1.....	2 $\frac{1}{3}$	21.....	49	41.....	95 $\frac{2}{3}$
2.....	4 $\frac{2}{3}$	22.....	51 $\frac{1}{3}$	42.....	98
3.....	7	23.....	53 $\frac{2}{3}$	43.....	100 $\frac{1}{3}$
4.....	9 $\frac{1}{3}$	24.....	56	44.....	102 $\frac{2}{3}$
5.....	11 $\frac{2}{3}$	25.....	58 $\frac{1}{3}$	45.....	105
6.....	14	26.....	60 $\frac{2}{3}$	46.....	107 $\frac{1}{3}$
7.....	16 $\frac{1}{3}$	27.....	63	47.....	109 $\frac{2}{3}$
8.....	18 $\frac{2}{3}$	28.....	65 $\frac{1}{3}$	48.....	112
9.....	21	29.....	67 $\frac{2}{3}$	49.....	114 $\frac{1}{3}$
10.....	23 $\frac{1}{3}$	30.....	70	50.....	116 $\frac{2}{3}$
11.....	25 $\frac{2}{3}$	31.....	72 $\frac{1}{3}$	51.....	119
12.....	28	32.....	74 $\frac{2}{3}$	52.....	121 $\frac{1}{3}$
13.....	30 $\frac{1}{3}$	33.....	77	53.....	123 $\frac{2}{3}$
14.....	32 $\frac{2}{3}$	34.....	79 $\frac{1}{3}$	54.....	126
15.....	35	35.....	81 $\frac{2}{3}$	55.....	128 $\frac{1}{3}$
16.....	37 $\frac{1}{3}$	36.....	84	56.....	130 $\frac{2}{3}$
17.....	39 $\frac{2}{3}$	37.....	86 $\frac{1}{3}$	57.....	133
18.....	42	38.....	88 $\frac{2}{3}$	58.....	135 $\frac{1}{3}$
19.....	44 $\frac{1}{3}$	39.....	91	59.....	137 $\frac{2}{3}$
20.....	46 $\frac{2}{3}$	40.....	93 $\frac{1}{3}$	60.....	140

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links
0		0		0	
11	1.88	18	5.14	25	10.54
0.38	2.24	19	5.76	26	11.26
0.55	2.63	20	6.42	27	12.24
0.76	3.06	21	7.11	28	13.37
8	3.53	22	7.85	29	14.34
9	4.02	23	8.64	30	15.47
10	4.56	24	9.47	35	22.07

MICROFILMED  
JAN 6 1980

533

.08

42.64

2

1464.00

42.64

1506.64

Index =  
Cont. Book No 2 - June - 1907

Continuation of "B" line 1-37

Dulzura Summit to Dam Cut 39-41

Continuation of S. line

Continued Book No. 2  
June 1907

357 +60	11.7	827	14884	stake - 5.7
0	11.42	8293		
952 - 1492.45				
+60	8.0	845	8842	- 3.9
35'	6.2	863	8846	- 2.1
+20	5.0	875	8835	- .09
+40	4.09		8826	
+60	4.11		8824	
+60	4.13		8832	
359	4.15		8830	
+20	4.17		8828	
+40	4.19		8826	
+60	4.21		8824	
+80	4.23		8822	
360	4.25		8820	
+20	4.27		8818	
+40	4.29		8816	

Bushy Floor with opening of Boulder.

CP

2.

1492.45

0

296 148949

2.52 1492.01

360+60

3.87

1488.14

Stake

+80

389

8812

361

391

8810

+20

393

8808

+40

395

8806

+60

397

8804

+80

399

8802

B.M. 43

4.75

148726

.013 High (1487.273) = B.M. 32 Eaten Sing  
pr with 11' + 361+80

362

4.01

8800

+20

4.03

8798

0

4.75

148726

11.53 1499.09

440

6.4

92.7

8796

Stake

+5.3

+60

1.52

149756

8794

Sub

+10.7

6.52 1504.09

File with 100 Boulders

\*

1504.095

362+80	29	14912	148792	Stake	+13.3
363	41	1500.0	8790	"	+12.1
+20	86	955	8788	"	+7.6
+40	124	14919.55	8786	hub	+4.1

5225 1497.180

+60	9.34		8784	Stake	
+80	336		8782	on top of RR	-33
364	131	1484.1	8780	Stake	-37
+20	130	842	8778		-36
+40	942		8776		
+60	72	90.0	8774		+2.3

0.53 1496.65

0.53 1497.18

	944		8774		
0	1160	1495.51			

0.08 1495.66

0	7235	1479.425			
---	------	----------	--	--	--

Our saddle cutting out long stems

Commenced work  
Sta 364+60  
6-27-07

W. K. Hall  
Fred. W. West  
Marshall  
Geo. Sam  
Fred. Bull  
S. W. Mas

@ 00

= P.P. on Boulder

= grade for Sta 364+60 on hub

0.215 1478.640

1478.425

10.90

1467.74

hut

(Upper 149.75) = grade, 364+60 after dropping 20

364+80

10.92

67.72

Saki

365+56

10.99

67.65

364+80 - 365+56 across bench, west

366

11.04

67.60

+70

11.11

67.52

Sill passes over gulch and bench (12' high)

367

11.14

67.52

+60

11.19

67.45

o

7.84 1470.80

on III

367+40

2.05 1472.85

368

5.45

67.40

on Rk

+50

5.50

67.35

Saki

369

5.55

67.30

+50

5.60

67.25

370

5.65

67.20

o

4.34 1468.51

6.89 1475.40

So: stations from here on

Dismantled and shipped out

CO



147540

656 1468.84

Check Savels from Bm 32 - Bm 32

Eaten in

= Pay P on Pk in water gulet

1242 1499.68

148726

2105 1497.575

448 1502.055

820 1493.915

393 1497.645

1005 1496.640

= Chk on left page 3

1160 1476.045

684 1492.905

9085 1474.820

= Pay P on Pk south of water gulet

6.

0.885 1485.705

1484.820

1.95 1473.745

0.30 1474.045

Sta 370+50

6.90

1467.15

Stake

371

6.95

67.10

+50

7.00

67.00

Mk with

372

7.05

67.00

Stake

+50

7.10

66.95

on Ken Pt

373

11.9

1462.2

66.90

Stake

-4.7

+50

11.5

62.6

66.85

on Ken Pt

-4.3

374

7.25

66.80

Stake

+50

7.30

66.75

375

7.35

66.70

+60

7.40

66.65

376

7.45

66.60

0

8.15 1465.860

5.80 1471.66

+50

5.11

66.5

Blumen Camp  
North of each  
water of each

= P.P. on Rick side  
from check levels  
on previous page

Slump Position  
Saddle Hill

0.05

on Pt rpp 38

147.66

377	516	1466.50	Stake
+50	521	6645	"
378	526	6640	"
+50	531	6635	"
379	536	6630	"
+50	541	6625	"
380	546	6620	"

927 1462.39

0

072 1470.94

1280 1483.74

+55	27	81.5	6615	+15.3
+80	10	82.7	6612	+16.6
391 +10	0.8	82.9	6610	+16.8
+45	113	72.4	6605	+6.3
+70	96	74.1	6603	+8.1
0	1280	1470.94		

130 1492.14

attribution of wages, Gulcher & Cluff & Simpson

Pr. by Cluff

CO

	147214		
		9.76	146238 ✓
	1014 147253		146239
382 +10		658	146601
+50		659	6595
383		663	6590
+50		669	656
384		673	6580
0		889	146364
	641 1470.08		
+50		430	6575
385		436	6570
+50		440	6565
386		445	6560
0		449	146556
	10.88 147644		
+50		10.99	6555
387		1094	6550

✓ 472.52

announced work 384 +00  
 6-20-07  
 N.W. Hall  
 P. W. Smith  
 Mar. 1880  
 2nd floor  
 Mt. St. Ann  
 = Red Pt beyond cliffs  
 litho

30° Dip - granite and shale

384 +33  
 6' 1" 384 +33

1476.44

387+50	1099	1465.45
388+20	11.06	6535
+50	11.09	6535
389	11.14	6520
+50	11.19	6525
390	11.24	6525
0	11.30	1465.34

Stake

387+50 - 388+20 = straight line on zig-zag

814 147348

+50	8.33	6515
391	838	6510
+50	842	6505
392	841	6500
+50	853	6495
393+15	859	6491
+50	863	6485
394	868	6480
+50	873	6475

peg

390

CP

392+50 - 393+15 straight line  
12' guth

147348

395	875	146470
+50	883	6425
396 +05	888	6440
+60	894	6454
397	898	6450
+50	903	6445
0	891	146457

685 147142

398	702	6440
+50	707	6435
399	712	6430
+50	717	6425
400	722	6420
+50	727	6415
401	732	6410
+50	737	6405
402	742	6400

Stake

395 + 50 - 396 + 05 across 18' gully

396 + 05 - 396 + 60 " 18' gully

peg

391 + 50

CO

- 0.35 c

edge of road

		1471.42			
3	402 +50		747	1463.95	Stak
	403		752	6390	"
3	+50		757	6385	"
	0		7.60	1463.92	
3		702 1470.84			
	404		7.04	6380	
	+50		7.09	6375	
	405		7.14	6370	
	+50		7.19	6365	
	406		7.24	6360	
	+50		7.29	6355	
	407		7.34	6350	
	+50		7.39	6345	
	408		7.44	6340	
	+50		7.49	6335	
	409		7.54	6330	
	+50		7.59	6325	

34

403 +50

*(Handwritten signature or scribble)*

1470.84

410 764 146320

Stake

+50 769 626

411 774 630

+50 779 635

0 787 146297

894 147191

412 891 630

+50 896 6295

412 901 630

+50 906 635

0 712 146479

952 147431

3m. 45 995 146436

414 1181 626

+50 1186 6275

415 1164 6270

+55 1166 626

pxg 413 + 70

on Bldg 5' L+ 413 + 93

CP

415 - 415 + 55 flatish wood 18 dur



13

1474.31

416		1171	1462.60
+50		1176	6255
417		1151	6250
+50		1156	6245
418		1191	6240
+25			
+50		1196	6235
419		1201	6230
+50		1206	6225
420		1211	6220
+50		1216	6215
0		1191	1462.40
8	9.11	1471.51	
421		941	6210
+50		946	6205
422		951	6200
+50		956	6195

Stake

417 - 417 + 50 = 15' sandy wash

= shallow wash 8' deep

on p49

419 + 50

C10

422 - 422 + 50 across 12' gutter

1471.51

423

9.61

146190

State

+50

9.61

6185

424

9.71

6180

0

9.73

146178

req

14704+00

1235 1474.13

+50

1238

6175

425

1243

6170

+50

1248

6165

426

3.2

14709

6160

+9.3

0

3.0

1471.03

Curt Thorne Pass

426

1261 1483.44

+50

6.0

7.76

6155

+16.01

0

2.03

1481.61

426+75

1034 1491.95

427

7.0

14860

6150

+23.5

+50

2.4

14896

6145

+28.1

428 +75

4.9

1497.1

6140

+25.7

= Summit

= county road

1491.95

426 +50

10.3

1481.7 1461.3

+20.3

429

14.7

77.3 61.30

+16.0

0

12.11

1479.84

peg

428.47

194 1481.78

+50

5

5.8

1476.0 61.25

+14.7

430

9.6

1472.2 61.20

+14.0

0

12.77

1469.01

0.10

1469.11

+50

3.8

1465.3 61.5

4.1

+85

7.99

61.2

grade on bank - 5 feet 1/2 cut

431

8.01

61.10

Stake

+50

9.06

61.05

432

8.11

61.00

*Loop*

+50

8.16

60.95

0

8.34

1460.77

peg

432.66

6.19

1466.96

433

12.7

54.3

60.90

- 6.6

1466.96

434

1460.90

+50

123 547 6075

Bon 46

1067 1456.29

10788 1467.078

+69

638 6073

Stake

435

628 6070

+50

643 6065

0

881 1468.465

1067 1469.135

436

854 6060

+50

859 6055

437

864 6050

+50

869 6045

438 +50

874 6040

+35

5.7 634 6035

+50

7.0 62.1 6030

0

6.825 1462.310

Commenced work at 434+69

6-30-07

Ch. H. Hall

R. W. M. H. H.

Max Watson

E. W. H. H.

(Mike H. H.)

100'

432+50 + 434+60

- 6.1

swale/depression

on Bldr 15' LT 434+05

per 6' LT 435+68

0.00

+3.0

+ 1.7

per 438+50

1086 1472.37 1462.31

439 104 62.0 1460.30 + 1.7

+50 87 64.2 6025 + 39

440 41 68.3 6030 + 8.1

+50 19 70.5 6015 + 10.2

441 56 66.8 6010 + 6.7

+55 12.32 6025

442 12.37 6000

+50 12.42 5995

0 12.35 1460.02

slowly  
cur

1108 1471.02

443 11.12 5990

+50 11.7 5985

444 11.22 5980

+60 11.28 5974

445 11.32 5970

+50 11.37 5965

0 11.47 1461.44 11.26 1459.96

219

442 + 50

444 - 444 + 60 = 7' gully

219

445 + 50

1461.44

446 130 48.4 1459.60

+50 200 41.4 5955

447 84 53.0 5950

+50 63 58.1 5945

448 2.04 5940

0 1308 1467.55 - 692 1454.52

+50 8.20 5935

449 125 5930

+50 130 5925

450 135 5920

+50 140 5915

451 145 5910

+50 150 5905

452 155 5900

0 1176 1470.65 866 1458.89

+50 142 66.5 5995

0 1207 1479.95 1765 1461.88

- 11.2

- 18.2

- 6.5

- 4.4

129 15 14 449 +00

ep's

129 452

+ 7.5

1452 +00

1479955

453 99 70.1 145890 + 112

+50 57 74.3 5885 + 75.4

454 49 75.1 5890 + 16.3

+50 90 71.0 5885 + 12.2

o 183 1469445 1234 1467615 peg 454 + 80

455 40 65.4 5870 + 6.7

+50 10.80 5865

456 10.85 5860

+50 10.90 5855

457 10.95 5850

+50 11.00 5845

o 681 1466815 944 1460005 peg 10 Pt 457 + 50

458 + 15 8.43 5830

+50 8.47 5825

459 8.52 5820

+50 8.57 5815

o 296 1460442 937 1457440 peg 10 Pt 459 + 65

457 + 50 - 458 + 15 = 20' Swath

COO

460		97	507	145820
+50		110	494	5815
461		51	553	5810
+50		79	575	5815
+90		54	55.0	5800
+105		127	477	5800
+15		96	50.8	57900
Bm 47		1243	1447.99	
+50		56	54.8	5785
464		2.62		5785
0	371	1459.93	1220	145622
+60		2.19		5778
465		223		5770
		495	145498	
+50		228		5765
466		233		5760
0	1230	1467.05	527	1454.66

1460/2

Plan of Qualls with central ridge

- 7.5  
- 8.8  
- 2.8  
- 0.6  
- 3.0  
- 10.3  
- 7.1  
- 3.1

= highest pt on central ridge

(Depth point 22 feet)

on Boulder

on low of block, big pond 30' x 763 + 10

P=9 20 L+ 463 + 50

= 2 x 3 hat with lath guard  
50' north of fuel cor.

CS



1467.05

466 + 50		9.50	1457.55
467		9.55	5750
+ 50		9.60	5700
468		9.65	5740
+ 25		9.67	5715
469 + 25		9.77	5725
⊙	355	1468.20	240
+ 50		10.95	575
470		11.00	5700
+ 50		11.05	570
471		11.10	5710
+ 50		11.15	5705
472		11.20	5700
+ 25		11.22	5695
+ 85		11.29	5692
473		11.30	5690
+ 30		11.35	5655

5.20

Along Fence Line

468 + 25 - 469 + 25 = 25' dug holes

= hub 5' north of fence post  
west of gutter

472 + 25 - 473 + 85 = 11' gutter

146820

0 5.58 146251 11.27 145693

474 6.01 145600

+50 6.06 5675

475 6.11 5671

+50 6.16 565

476 6.21 560

0 6.50 145631

565

check on line from Eaton Bm W1

1.51 1461063 1486273

12.59 1475493

0.69 1476183

11.67 1464513

3.33 145964 145631

476 +50 307 145655

477 314 46.00

peg

473+50

CS

enpr/PR

476+13

7-2-07

M H Hall

R. W. West

S W Moss

Robt. Watson

Mike (Station)

CS

145964

477 +50

319

145646

478

322

8640

+65

329

8636

479

334

8630

0

2276 1457365

4.25 1461.615

+50

337

8628

480

342

8620

+50

347

8616

481

352

8610

+50

357

8604

482

362

8600

+50

367

8594

0

267 1458945

6.26 1465305

483

371

8590

+50

376

8584

478-479+65 across gulet.

on PK

on PK

on PK

5.4+ 479+05

on PK

PK

4.27 482+65

EW

on PK

21.

1465305

484

951 145580

+50

956 5575

485

961 5570

o

9255 1462020 1200 1452765

on PK 20kt 485+35

+50

637 5561

574 442

5560

+50

4.6

574

5555

+15

on PK party

487

4.0

580

5550

+25

+50

657 5545

o

520 145682

on PK 60 487+50

1465115

005

on PK

488

972 6540

+50

977 5535

489

982 5530

+50

987 5525

490

992 5520

+50

997 5515

1465.115

○	5.833	1464.005	6964	1458.150		
#91				8.91	1455.10	
	+50			8.96	5500	
#92				9.01	5500	
	+50			9.06	5495	
#93				9.11	5490	
	+50			9.16	5485	
#94				9.21	5480	

PK 4 P+ 1190+140

○	7.895	1464.150	7.75	1456.235		
	+50			9.40	5475	
#95				9.45	5470	
	+50			9.50	5465	
#96				9.55	5460	
	+50			9.60	5455	
#97				9.65	5450	

hnt 12 P+ 494+20

CO

○	10.67	1465.29	9.53	1454.62		
	+50			10.84	5445	

hnt 11 P+ 497

1465.29

+98	10.89	5440
+75	10.96	5433
+89	10.99	5430
+50	11.04	5425
+86	11.07	5422
500. +35	11.12	5417
+50	11.14	5415
501	11.19	5410
+50	11.24	5405
502	11.29	5400

$498 - 498 + 75 = 20'$  gully

across gully

across gully

Prm 48 2.35 1462.94

= old top on ground 35 ft 501 + 80

123 1464.17

v.

+50	10.22	5395
503	10.27	5390
+50	10.32	5385
504	10.37	5380
+50	10.42	5375

m.p.k

27

1464.17

528 1465.515 4.435 1449.735

505 11.32 1453.70

+50 11.37 5365

506 11.42 5360

+50 11.47 5355

507 +50 11.57 5345

508 11.62 5340

across 15' gulch

509 994 1463.685 11.27 1453.745

+50 10.34 5335

509 10.39 5330

+50 10.44 5325

510 10.49 5320

+50 10.54 5315

511 10.59 5310

@ 90

512 849 1465.705 6.47 1459.215

+50 12.66 5305

pen 309+ 510+60

512 12.71 53.01

1465.705

S12 +50

12.76

1452.95

S13

12.81

52.90

+50

12.86

52.85

S14

12.91

52.80

0

104.8

1463.645

12.54

1453.165

+50

10.90

52.75

S15

10.95

52.70

+50

11.00

52.65

S16

11.05

52.60

+75

11.12

52.53

S17

11.15

52.50

0

555

1459.585

9.61

1454.035

+50

7.14

52.45

S18

7.19

52.40

+50

7.24

52.35

S19

7.29

52.30

+50

7.34

52.25

1217.73  
46.143  
1638.73

719

S14 +50

S16 - S14 + 75 = 52' valley

775  
152.00

page

S17

S17 + 00

*Bob*

on 1/11



1459.58

Ref. Pr.

9.795 1449.790

6.365 1464.950 1.00 1458.585

1.46 1463.49

7.16 1456.95 1449.79

520

+60

3.1 539

475 1452.20

521

+50

485 5210

490 5205

00

12.09 1465.95 209 1453.86

522

7.0 590

52.00 +7.0

12.24 1477.82 037 1465.58

+50

124 65.4

51.95 +13.4

523

69 70.9

51.90 +19.0

+50

74 70.4

51.8 +18.5

524

52 72.6

51.90 +20.8

11.47 1484.65 464 1473.18

continued work at Sta 522+00

7-3-07

Ref. Pr. M.H. Hall  
Ref. Water on 210m, D.G. Hall

on RR 45' Lt 519+65

1463.873 = 513m 45

Ref. Pr. above

not set

on RR 3' Lt 521+25

West side of cut

on RR 2' Lt 524

148460

524 +50 10.1 74.6

525 6.6 78.1

o 1188 149092 5.61 1479.04

+50 10.7 80.2

526 6.7 84.2

+50 3.2 87.7

o 11635 1500835 1.72 1480.20

527 10.1 90.7

+50 6.4 94.4

528 2.3 98.5

o 1187 151232 0.38 1500.450

o +50 8.9 03.4

529 3.4 08.9

o 10.700 1521415 1.61 1510.71

+50 6.4 15.0

o 12075 1531360 2.13 1519.285

530 8.8 22.6

1451.75 +228

5170 +26.4

5165 +28.5

5160 +32.6

5155 +36.1

5150 +39.2

5145 +42.9

5140

Peg 6' Lt 525+00

- South side of Camp Road

PK 12' R 526+70

Peg 528+10

Peg 529+16

Peg 529+77

1531.36

0	11855	1572.005	121	1530.15	hub	530+421
530+50			109	31.1		
+80			69	36.1	= Chr Campo Red	
0	12085	1550.290	370	1538.505	hub	531+00
531+50			26	47.8		
0	1157	1566.605	1355	1549.035	hub	531+44
0	12255	1569.785	3.075	1559.530	hub	+97
0			205	1567.735	hub	532+35
	1088	1578.675				
0			063	1577.985	hub	+70
	1176	1589.745				
0			077	1588.975	hub	533+14
	12125	1601.100				
0			0895	1600.205	hub	+64
	12.00	1612.205				
0			0885	1611.320		534+26
	12.45	1623.77				535

61.59

83.09

21.50

1623.77

0 3.47 1620.30

10.10 1630.40

4.1 1626.3

0 10.41 1619.99

2.80 1622.79

0 11.20 1611.59

1.54 1613.13

0 11.86 1601.27

1.42 1602.69

0 10.61 1592.08

1.71 1593.79

0 11.64 1582.15

1.17 1583.32

0 12.49 1570.83

0.97 1571.80

0 11.41 1560.39

1.79 1562.18

Hub. 534+77

Summit

Hub. 535+95

Hub. 536+35

Hub. 536+61

Hub. 536+80

Hub. 537+10

Hub. 537+40

Hub. 537+75

10.00

98.68

1562.18

0 12.62 1549.56

1.46 1551.02

0 11.97 1539.05

0.94 1539.99

0 12.55 1527.44

1.05 1528.49

0 12.68 1515.81

0.34 1516.15

0 12.07 1504.08

0.78 1504.86

12.00

1492.86

0 12.43 1492.43

1.09 1493.52

0 12.54 1480.98

2.39 1483.37

0 11.82 1471.55

1.95 1473.50

Hub 538+12

" 538+50

" 538+85

CO

" 539+20

" 539+65

Gulchi 539+60

Hub 540

Hub S R 541

" 541+75

1473.50

B.M. 49

9.04 1464.46

Tack on Sycamore Tree 6" Dia. - E. B.M. 46 Elev. 1464.473

4.50

1468.00

End of line. (80' contour) 541+95

0.92 1465.38

11.29 1454.09

2.83 1456.92

14

543+88

7.12

1449.30

End of line (60' Contour)

1/4/07

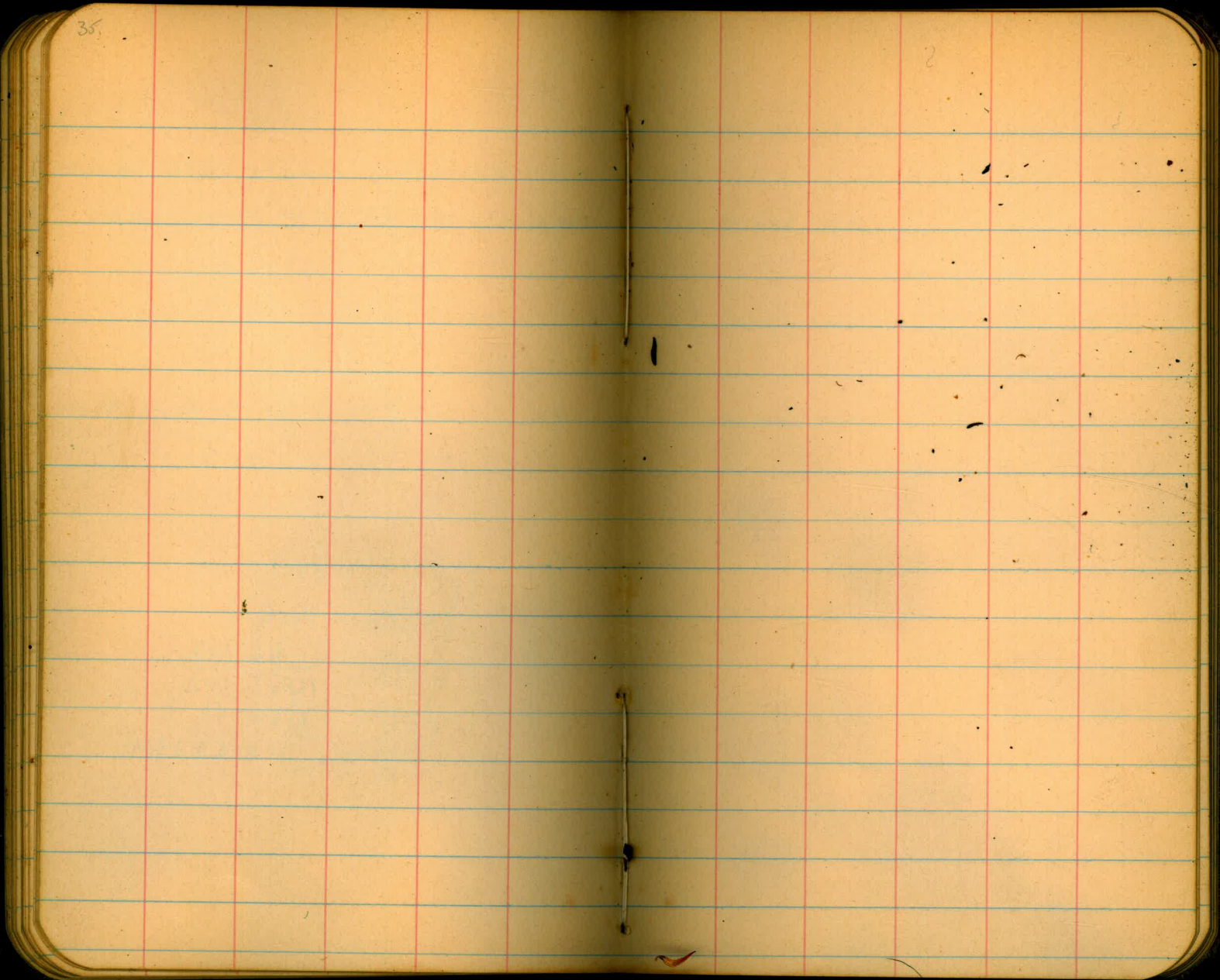
C

Eaten = 1419

Eaten 46.143  
1465.143

Wares 1464.46

Difference 0.683 feet.



1528.72

= R.M. #1. 120' to Tunnel entrance = Sta. 0.

12.36 1541.08

1528.72

0

9.57 1531.51

On rock

4.22 1535.73

0

3.17 1532.54

" "

5.16 1537.70

0

5.35 1532.35

" "

1.18 1533.53

0

10.63 1522.90

1.19 1524.09

0

9.58 1514.51

1.43 1515.94

10+00

10.74

1505.20

11

10.64

05.30

12

10.54

05.40

13

10.44

05.50

+50

10.39

0

2.44

1513.50



1513.50

7.88 1521.38

7.88 1513.50 15.75 1505.60

0.25 1513.75

14

8.15 1505.60

Rock Bluff Barrett Dam site (upper)

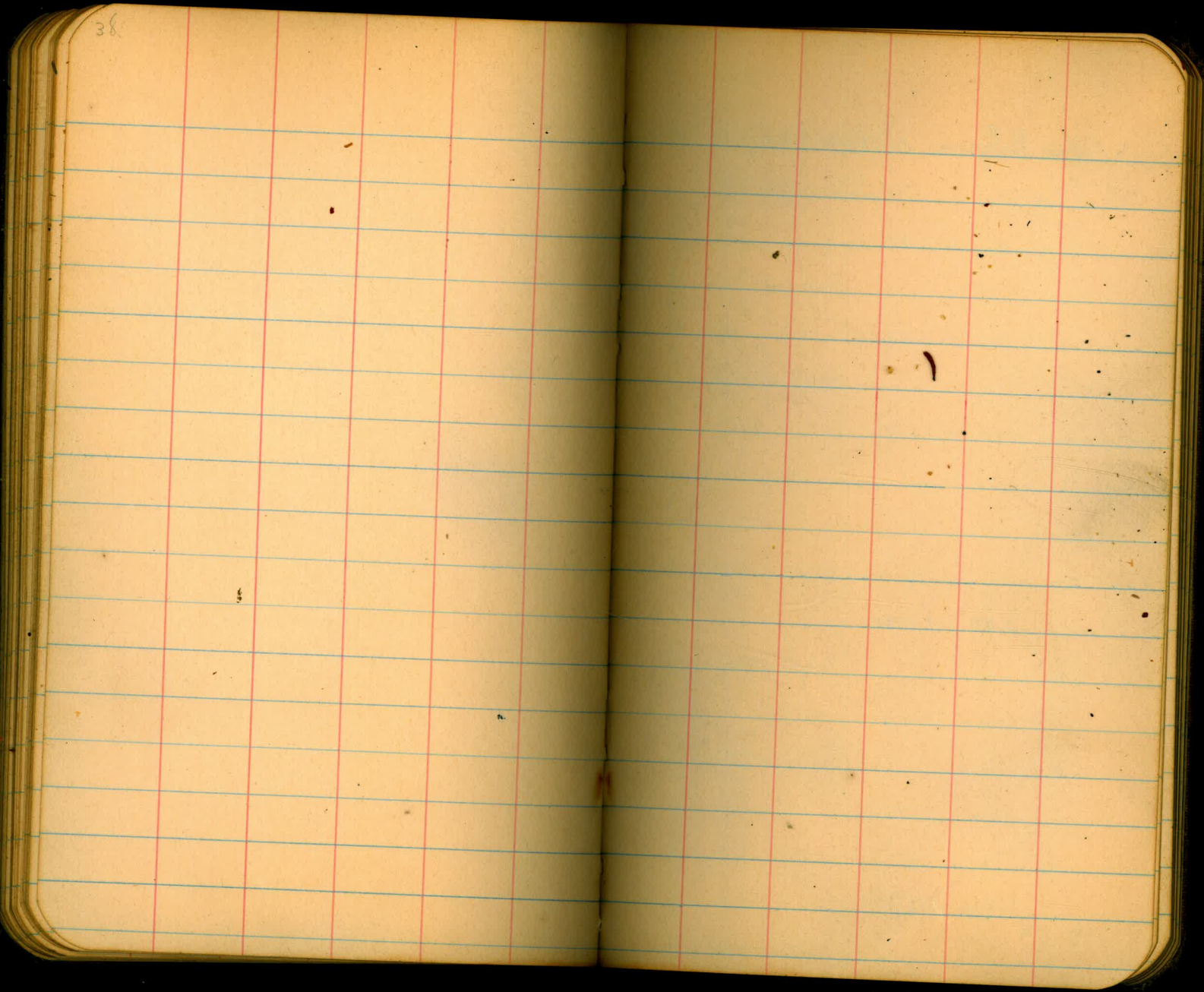
15

8.05 .70

16

7.95 .80

4.23 1507.52



# Maui Sulphur Summit to Dawn Oct July 13 1907.

4508

Hall  
Harriman  
Co. Recs.

T.P. 5' A 521+15

48.02      53.10      1453.86

1.06    1454.92

0      5.14    1449.78

12.55    1462.33

0      11.38    1450.95

10.20    1461.15

2700

5200 = 818

1452.70

0      7.44    1451.71

8.84    1460.55

0      7.31    1457.24

7+00

6.50    1457.74

0      8.68    1449.06

3.39    1452.45

0      5.85    1446.60

5.48    1452.08

0      3.30    1448.78

18+00

CRW  
✓  
14.7.97

66.3621.83

3.53

11.10

1459.88

1448.78

4253

149231

9.7

20+00

Gulch

Dana Cut.

2.32

1457.56

20+50

12.29

1470.25

1.88

1468.37

21+48

On rock

9.15

1477.52

2.82

1474.70

22+25

12.10

1486.80

2.95

1483.85

23+17

Beginning of cut.

12.35

1496.60

1.31

1495.29

25+17

6.23

1521.52

9.0

26+17

Summit

1499.52

4.12

1497.40

26+78

Old B 2m #150

1.69

1499.09

7.43

1497.66

28+78

0.65

1492.31

C O O

41

6.02

23.16

1498.31

0

9.41

1482.90

31+78

3.90

1486.90

4.6

1482.2

33+78

West end of Davis Cut

0

8.11

1478.69

64+78

2.12

1486.81

5.66

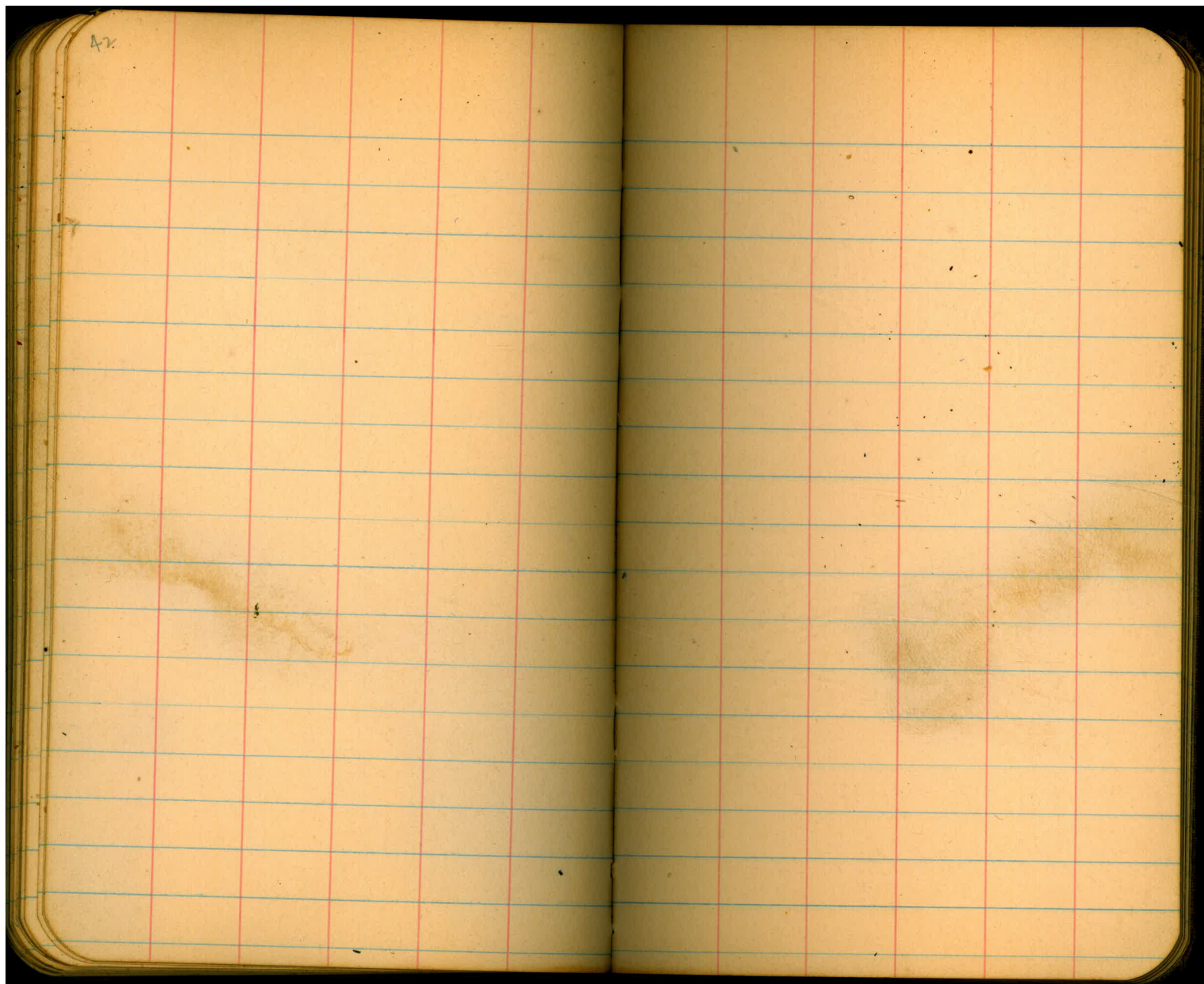
1475.15

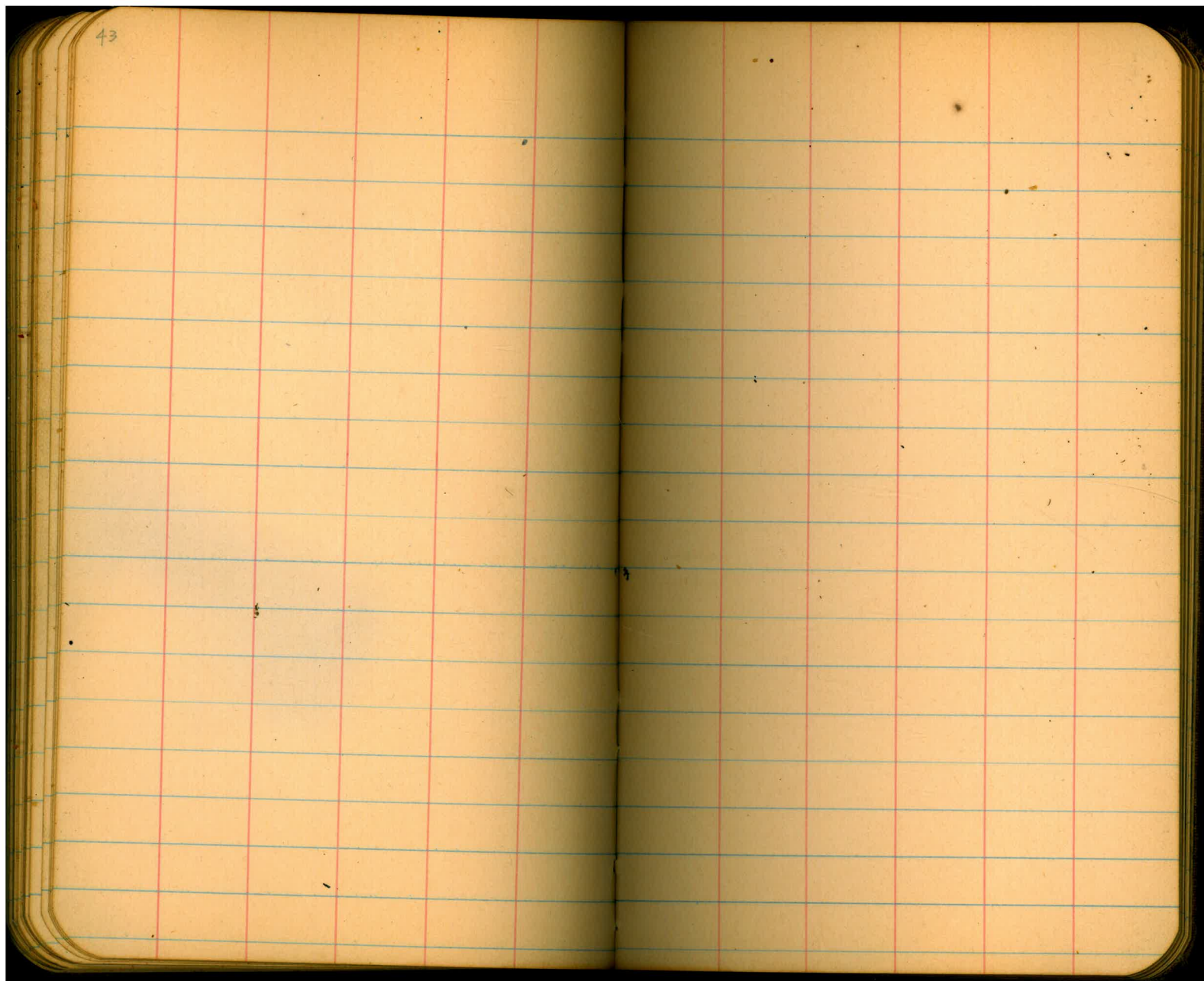
37+49

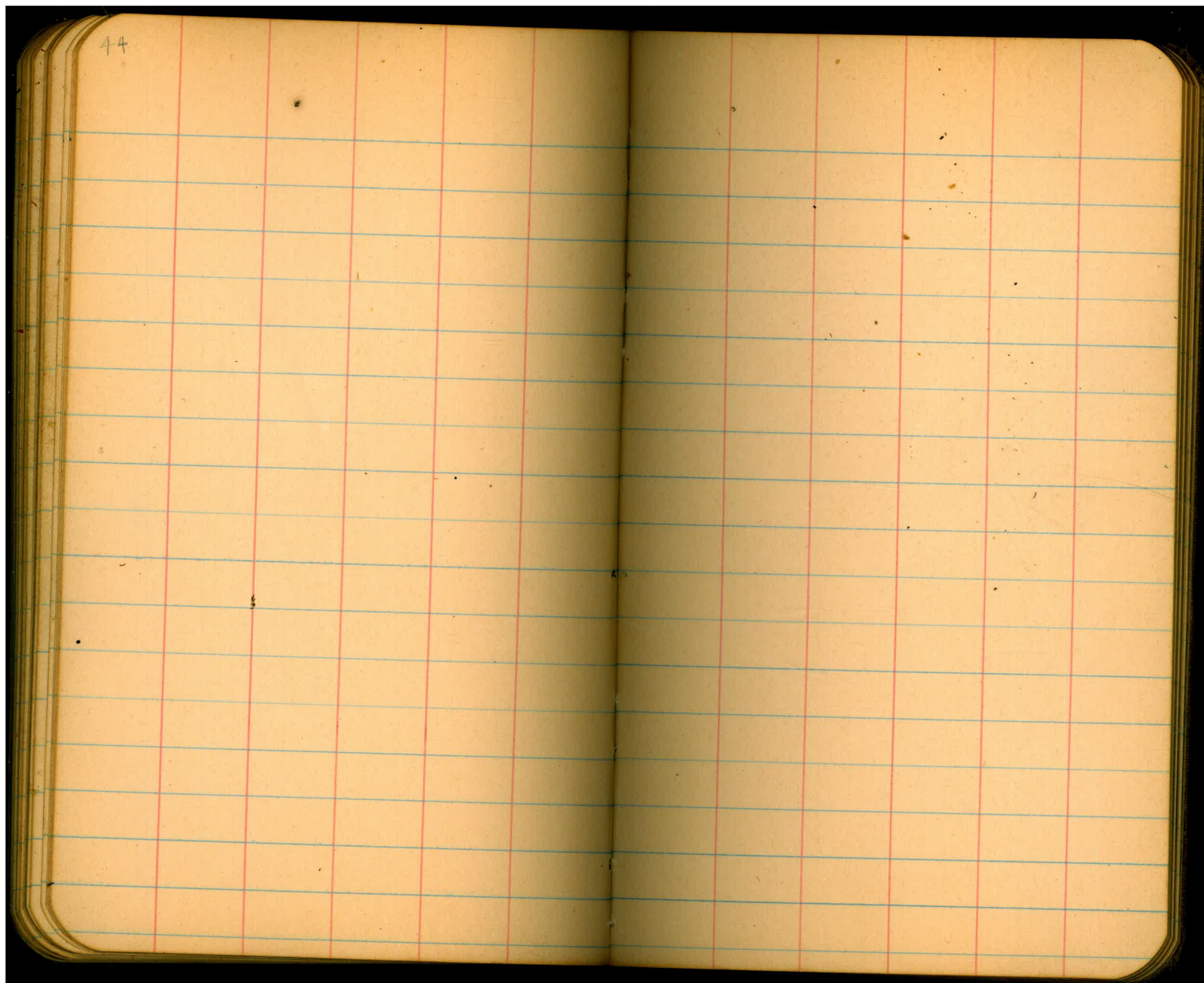
On Boulder & dia among brush

& boulders in line with cut

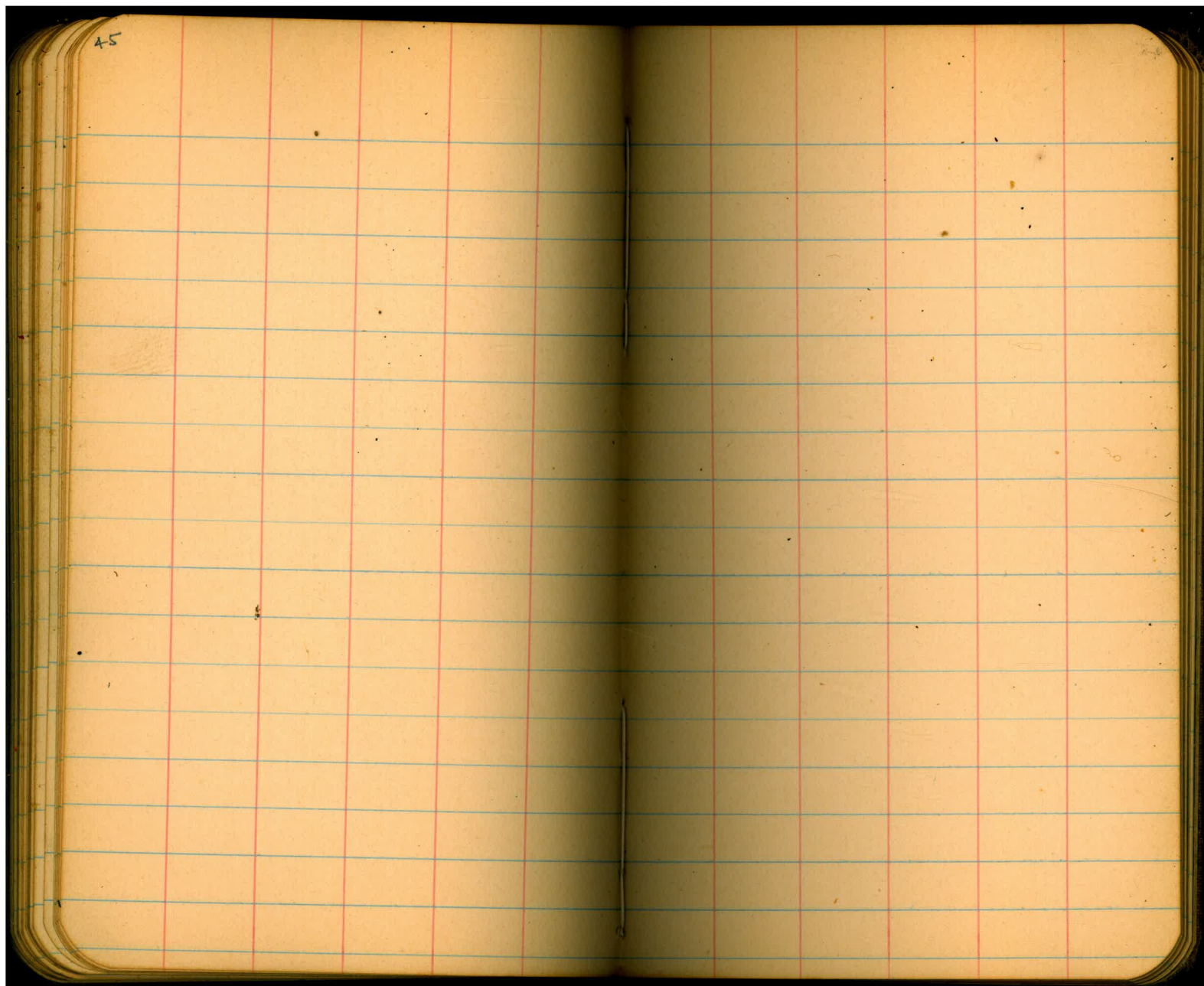
CS<sup>erw.</sup>

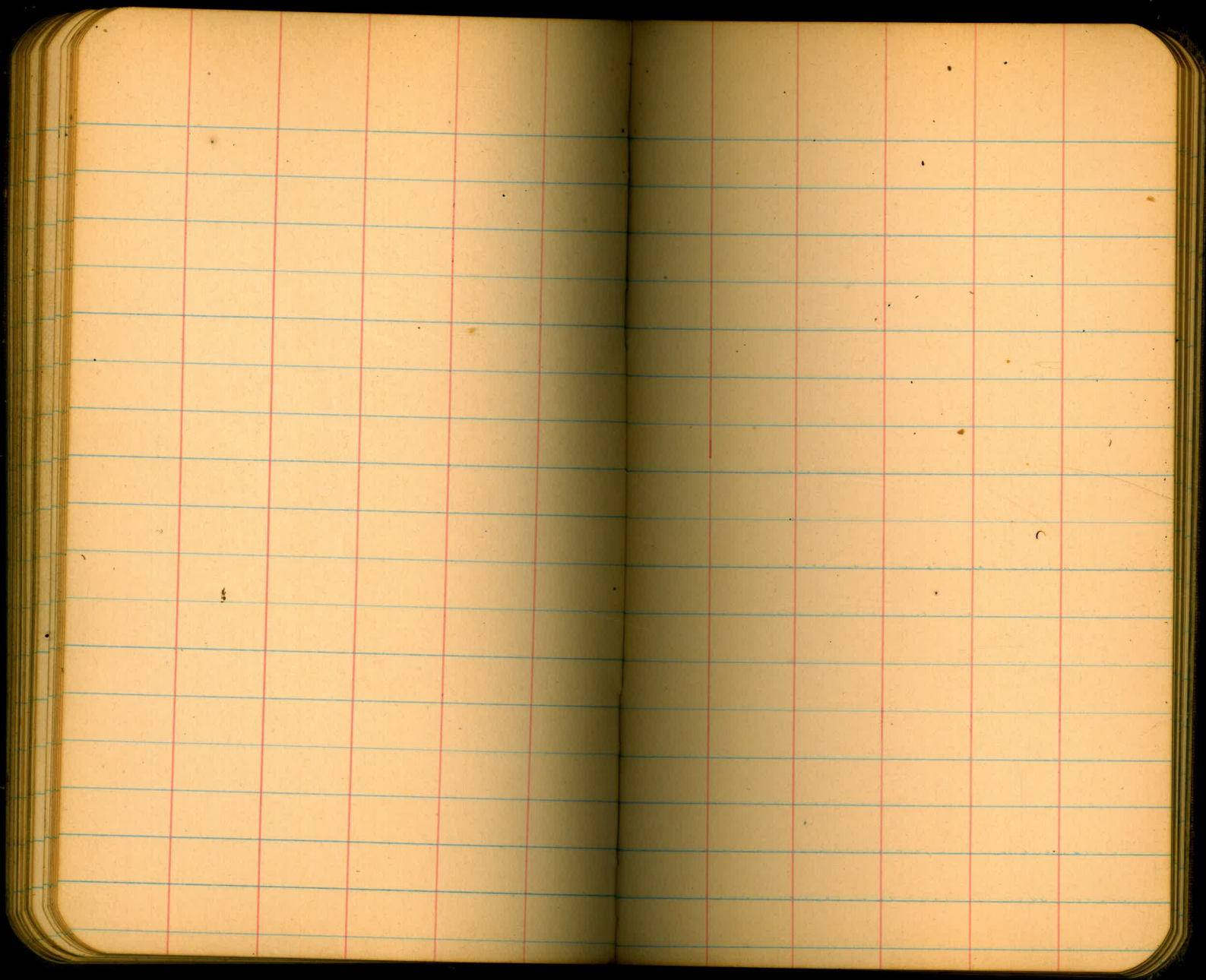












Sta.	Grad.		
355	8870	445	1479.70
360	8820	450	79.20
365	8770	455	78.70
370	8720	460	78.20
375	8670	465	77.70
380	8620	470	77.20
385	8570	475	76.70
390	8520	480	76.20
395	8470	485	75.70
400	8420	490	75.20
405	8370	495	74.70
410	8320	500	74.20
415	8270	505	73.70
420	8220	510	73.20
425	8170	515	72.70
430	8120	520	72.20
435	8070	525	71.70
440	8020	530	

B.M. 40 - on Bedr 4' L + 420 + 75  
 $1427.04 + 46.143 = 1473.183$

B.M. 41 - on limb of  $\pi$  431 + 15  
 near 3rd June post  
 $1440.13 + 46.143 = 1486.273$

B.M. 42 - on large Bedr .5  $\pi$  441 + 25  
 $1429.59 + 46.143 = 1475.733$

B.M. 43 - on limb 9' L + 451 + 20  
 $1423.78 + 46.143 = 1470.223$

B.M. 44 - on Bedr. 25' L + 459 + 95  
 $1417.40 + 46.143 = 1463.543$

B.M. 45 on oak tree 15" dia 3' L + 460 + 70  
 $1425.95 + 46.143 = 1472.093$

B.M. 46 - on Sycamore tree 6" dia  
 2' L + 464 + 60  
 $1418.33 + 46.143 = 1464.473$

$$\begin{array}{r} 1464.00 \\ 17.84 \\ \hline 1481.84 \end{array}$$

$$\begin{array}{r} 1477.68 \\ 17.84 \\ \hline 1495.52 \end{array}$$

$$\begin{array}{r} 1495.52 \\ 17.84 \\ \hline 1513.36 \end{array}$$

513.36

Degrees. 89, 88, 87, 86, 85, 84, 83, 82, 81, 80, 79, 78, 77, 76, 75, 74, 73, 72, 71, 70, 69, 68, 67, 66, 65, 64, 63, 62, 61, 60, 59, 58, 57, 56, 55, 54, 53, 52, 51, 50, 49, 48, 47, 46, 45

Bench on Eaton line

B.M. 32 - on bench 10' h<sup>t</sup> 340 + 28

$$1441.13 + 46.143 = 1487.273$$

B.M. 33 - on bench 10' h<sup>t</sup> 350 + 80

$$1438.67 + 46.143 = 1484.813$$

B.M. 34 - on rock ledge 11' h<sup>t</sup> 360 + 60

$$1446.15 + 46.143 = 1492.293$$

B.M. 35 - on hub at 369 + 29

$$1436.19 + 46.143 = 1482.333$$

B.M. 36 - on hub 4' h<sup>t</sup> 380 + 20

$$1439.55 + 46.143 = 1485.693$$

B.M. 37 - on rock 15' h<sup>t</sup> 388 + 30

$$1445.40 + 46.143 = 1491.543$$

B.M. 38 - on hub 50' h<sup>t</sup> 401 + 10

$$1430.76 + 46.143 = 1476.903$$

B.M. 39 - on hub 7' h<sup>t</sup> 412 + 13

$$1419.96 + 46.143 = 1466.103$$

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.52	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.

Published by H. S. CROCKER COMPANY, Stationers, Drawing Materials, Mathematical Instruments, etc., San Francisco.