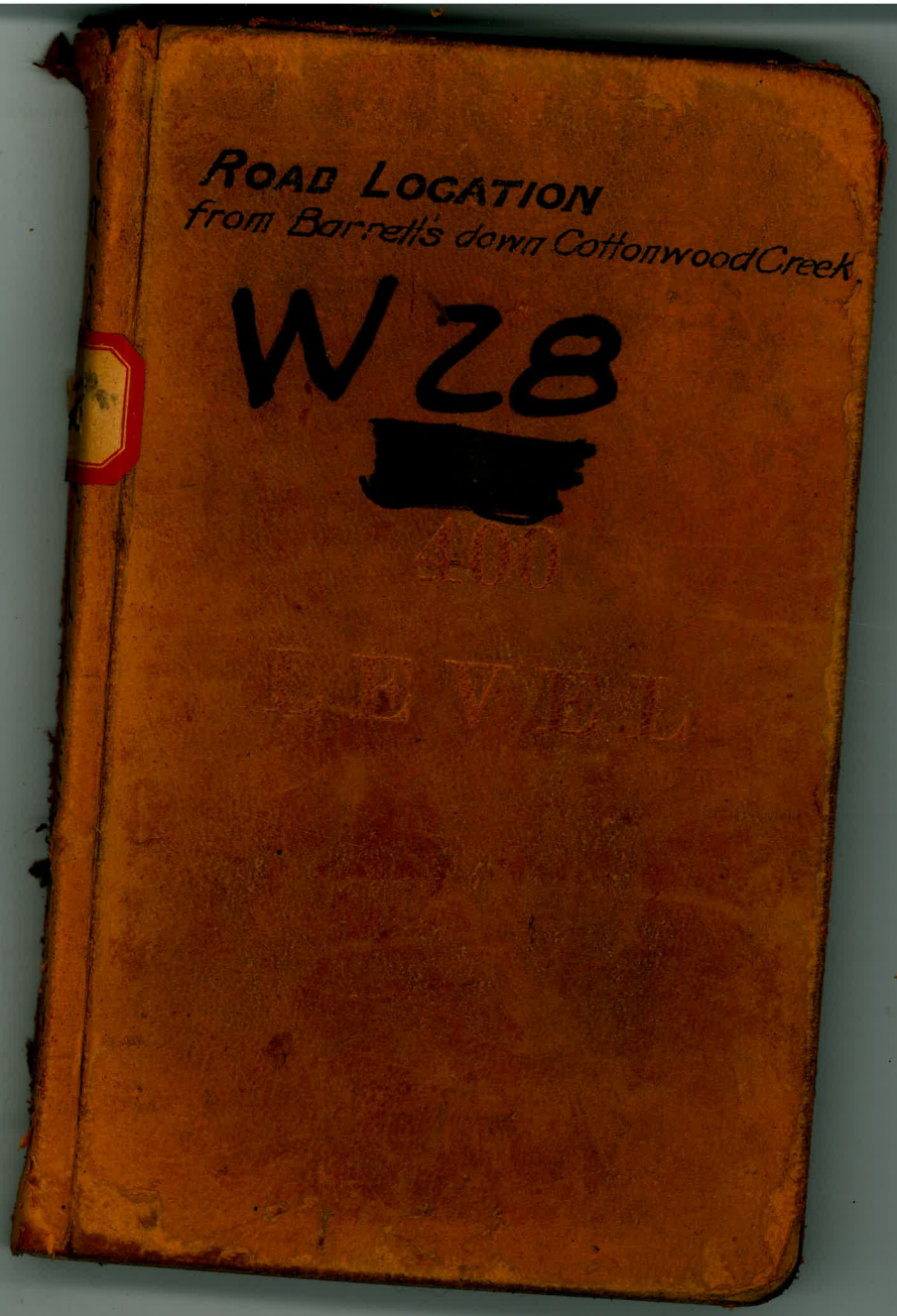

ROAD LOCATION
from Barnett's down Cottonwood Creek.
W28
[redacted]
400
LEVEL

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

Minutes	Lks.	Minutes	Lks.	Minutes	Lks.
1	2⅓	21	49	41	95⅔
2	4⅔	22	51⅓	42	98
3	7	23	53⅔	43	100⅓
4	9⅓	24	56	44	102⅔
5	11⅔	25	58⅓	45	105
6	14	26	60⅔	46	107⅓
7	16⅓	27	63	47	109⅔
8	18⅔	28	65⅓	48	112
9	21	29	67⅔	49	114⅓
10	23⅓	30	70	50	116⅔
11	25⅔	31	72⅓	51	119
12	28	32	74⅔	52	121⅓
13	30⅓	33	77	53	123⅔
14	32⅔	34	79⅓	54	126
15	35	35	81⅔	55	128⅓
16	37⅓	36	84	56	130⅓
17	39⅔	37	86⅓	57	133
18	42	38	88⅔	58	135⅓
19	44⅓	39	91	59	137⅔
20	46⅔	40	93⅓	60	140

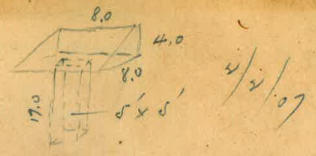
TABLE FOR RUNNING ON SLOPES.

The following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links
o		o		o		o	
4	0.24	11	.88	18	5.14	25	10.54
5	0.38	12	.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0 98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

MICROFILMED
MAR 0 1965
MICROFILMED

13+30 1.85
12+75 2.34



2/2/07

Shaft. No 1

Index

1st Location 0 - 83+75 pp 1-25
Upper Trial Line 75+50 - 91 26-27

Sewering Grade 44 - 66+21
pp 35-42

Tying New Line to Old
43

MICROFILMED
JAN 0 1985

Lvg. P Road from Garrett Dam. down Cottonwood Canon

	3.04	1601.21		1598.173
0			5.2	1596.0
+ 25			6.7	
+ 50			8.2	1593.0
+ 75			9.7	91.5
1+00			11.2	1590.0
+25			12.7	88.5
①	0.62	1589.91	11.82	1589.39
+50			2.9	87.0
+75			4.4	85.5
2+00			5.9	84.0
+25			7.4	82.5
+50			8.9	
+75			10.4	
3+00			11.9	1578.0
②	1.35	1578.29	12.97	1576.94

Cottonwood Canon Jan. 17 1907

13.M. on E. side of Canon N. of E. end of Garrett dam site

From Sta 0. to Sta 7 6% grade

0.0 (Estimate Feb. 7, 1907)

Earth.	8.0 cut	+ 6.0
Earth.	12.0 "	+ 7.0
Earth. + Boulders.	13.0 "	+ 8.0
Earth. + Boulders.	12.0 "	+ 6.0
Earth + Boulders	16.0 "	+ 10.7

				1578.29				
3+25			1.8	1576.5				
+50			3.3	75.0		Loose Rock	9.0 ave	+8.7
+75			4.8					
4+00			6.3	72.0		Solid "	10.0 "	+10.6
+25			7.8					
+50			9.3			Solid "	15.0 "	+14.0
+75			10.8					
⊙	0.02	1565.87	12.22	1565.85		Sa.S Solid "	15.0 "	+8.5
5+50			4.9	1563.0		" "	8.0 "	+12.0
+75								
6+00			5.9	60.0		Solid Rock.	6.0 "	+8.5
+25								
+50			8.9	57.0		"	22.0 "	+9.5
+75								
7+00			11.9	54.0		"	4.0 "	+9.0
⊙			12.10	1553.77				

Rock Loose Solid to Sta. 5+00

	7.63	1556.40		1553.77			
7+25				52.75			
+50			4.9	51.50	Solid Rock.	4.0 ave	+ 6.0
+75							
8+00			7.4	49.0	Earth & Bouldrs.	9.0 "	+ 7.0
⊙	1.99	1545.80	12.59	1543.81			
+50			10.2	46.0	" "	14.0 "	+ 9.0
+75			1.3	44.5			
9+00			2.8	43.0	Large Bouldrs.	15.0	+ 10.0
+25			4.3	41.5			
+50			5.8	40.0	" "	9.0	+ 11.0
+75			7.3	38.5			
10+00			8.8	37.0	Solid Rock.	12.0	+ 4.0
⊙	1.62	1535.93	11.49	1534.31			
	8.77	1536.72	7.98	1527.95	B.M., N.9 2. 1528.07		
+25			1.2	1535.5	Solid Rock	4.0	+ 15
+50			2.7	1534.0		2.0	+ 8.0

		1536.72			
75			4.2	1532.5	
11+00			5.7	1531.0	✓
+25			7.22	29.50	✓
+50			7.22	29.50	Earth. ✓14.0 +7.0
+75			7.22	29.50	
	2.18	1536.28		1528.07	0.M. 4/22
12+00			2.3	1528.0	
+25			3.8	26.5	
⊙	4.09	1527.59	12.75	1517.50	
+50			+3.4	25.0	
+75			+1.9	23.5	
13+00			+0.4	22.0	
+25			not det.		
+50			2.6	19.0	

Earth. & Boulders. 12.0 ave. +10.0

Cross Flume at Sta. 7+60 Elev. of Top of Floor of Flume 1523.44. From Top of floor to Top of floor plank = 4'11" Grade of road at Flume crossing is 6 Ft. above Flume floor.

From Sta. 5+00 8.0 ave +5.0

85% of Road finished to Sta. 12, (4/22/07)

0.0 0.0

		1521.59			
13+75			4.1	1517.5	
14+00			5.6	16.0	
			7.1		
+ 50			8.6	18.0	
	1.71	1531.77		1530.06	B. M. No 3. (Time Loc.)
	1.20	1520.63	12.37	1519.40	
	1.60	1509.37	12.86	1507.77	
+ 75			+ 2.1	11.5	
15+00			+ .6	1510.0	
+ 25			.9	08.8	
+ 50			2.2	7.0	
+ 75			3.9	5.3	
16+00			5.2	1504.0	From Sta. 16. to Sta 20+75 at %
+ 25			6.9	2.3	1503.0
+ 50			8.2	1.0	1502.0

Jan, 17. 1907
" 7th "

		1509.37			
16+75			9.9	1499.5	1501.
17+00			11.4	98.0	1500.
	1.00	1498.36	12.01	1497.36	
+ 25			1.9	96.5	1499.
+ 50			3.4	95.0	1498
+ 75			4.9	93.5	97.
18+00			6.4	92.0	96.
+ 25			7.9	90.5	95
+ 50			9.4	89.0	94
⊙			12.20	1486.16	
	8.80	1494.96			
+ 75			2.0	1493.	93.
19+00			3.0	92.	92
+ 25			4.0		91
+ 50			5.0		90
+ 75			6.0		89
20+00			7.0		88

Lightens out from Sta 16

Jan. 14, 1907.

		1494.96		
20+25			8.0	87.
+50			9.0	86.
+75			10.0	1485.
⊙	1.16	1496.00	0.12	1494.84
21+00				83.5
+25			14.0	82.0
+50			14.9	81.1
+75			15.5	80.5
22+00			17.0	79.0
+25				77.5
⊙	1.28	1484.78	10.0	76.5
+50			12.50	1483.50
+75				72.5
23+00			11.8	73
⊙	1.37	1493.94	13.3	71.5
+25			17.21	1477.57
			3.9	70.

not Ex.

From 20+75 to Sta 6%

From Sta 23+25 run Grade to Sta 25

8

		1473.94		
23+50			8.4	1468.5
+75			6.9	67.0
24+00			8.4	65.5
⊙	1.08	1476.98	12.07	1461.87
+25			+1.0	62.0
+75			2.0	61.0
25+00			3.5	59.5
+25			5.0	58.0
+50			6.5	56.5
+75			8.0	56.0
26+00			9.5	53.5
	-0.01	1450. 1469.99	12.96	1469.99
+25			+2.0	52.0
+50			+0.5	50.5
+75			1.0	49.0
27+00			2.5	47.5

Revised

for page 9.

Monday Jan 21, 1907

		1429.98			
27+25			4.0	1426.0	
+50			5.5		
+75			7.0	423.0	
			10.58	1439.40	
28+00				41.5	
	12.68	1464.67		1429.99	
	11.61	1473.57	0.71	1461.98	
23+50			3.57		1470.0
+75					"
24+00					"
+25					"
+50					"
+75					"
25+00			3.60		"
+25			6.1		68.5
+50			6.6		66.0

10					
		1473.57			
25+75			8.1		1465.5
26+00			9.6		64.0
+25			11.1		62.5
+50			12.6		61.0
⊙	5.64	1467.60	11.61	1461.96	
+75			8.1		59.5
27+00			9.6		58.0
+25			11.1		56.5
+50			12.6		55.0
⊙	0.30	1455.91	11.99	1455.61	
+75			2.4		53.5
28+00			3.9		52.0
⊙	7.38	1454.02	11.24	1442.67	
+25				1.5	50.5
+50				3.0	49.0
+75				4.5	47.5
29+00				6.0	46.0

11

		1452.02			
	2.45	1446.86	7.61	1444.41	
29+25			7.4		1444.5
+50			3.9		43.0
+75			5.4		41.5
30+00			6.9		40.0
+25			8.4		38.5
+50			9.9		37.0
+75			11.4		35.5
31+00			12.9		34.0
⊙	5.06	1440.02	11.90	1434.96	
+25			7.5		32.5
+50			9.0		31.0
+75			10.5		29.5
32+00			12.0		28.0
⊙	2.47	1431.99	10.82	1429.50	
+25			5.5		26.5
+50			7.0		25.0

level from 32+50 to 33+50

12					
		1431.97			
32+75			8.5	1423.5	1425.00
33+00			10.0	22.0	25.
+25				22.0	25 level
+50			10.0	22.0	14 25 ⊙
⊙	0.50	1420.45	12.04	1419.95	
+75			0.0	20.5	
34+00			1.5	19.0	1422
+25			3.0	17.5	
+50			4.5	16.0	1419
+75			6.0	14.5	
35+00			7.5	13.0	1416
+25			9.0	11.5	
+50			10.5	10.0	1413.
+75			12.0	8.5	
36+00			13.5	7.0	1410
⊙	1.50	1410.71	17.24	1409.21	
+25			5.7	1405.5	

(est. from 35+25 to 36 not set incl. 07)

from 36+25 4% grade to Sta 44 to Sta 42 4.74% →

		1410.71			
36+50			6.2		1404.5
+75			7.2		3.5
37+00			8.2		2.5
37+25			9.2		1.5
+50			10.2		1400.5
⊙	2.34	1402.58	10.44	1400.24	
+75			3.1		1399.5
38+00			4.1		98.5
+25			5.1		97.5
+50			6.1		96.5
+75			7.1		95.5
39+00			8.1		94.6
+25			9.1		93.5
+50			10.1		92.5
+75			11.1		91.5
40+00			12.1		90.5
⊙	1.16	1391.13	12.61	1389.97	
+25			1.6		89.5

			6.9 37-39+50	
	10.9	1396.7		1395.5
1404				
1400.0				
	6.5			
	11	1403.5		1392.5

		1391.13			
L0+50			2.6		1388.5
+75			3.6		87.5
L1+00			4.6		86.5
+25			5.6		85.5
+50			6.6		84.5
+75			7.6		83.5
L2+00			8.6		82.5
⊙	10.50	1389.51	12.12	1379.01	
+25			7.0		82.5
+50			7.0		
+75			7.0		
L3+00			7.0		
+25			7.0		
+50			7.0		
+75			7.0		
L4+00			7.0		1382.5
+25			7.0		82.5

1390

From ⊙ Sta 42 level to Sta. 45

Tuesday, Jan. 22, 1907

		1389.57			
44+50			7.0		1382.5
+75			7.0		
45+00			7.0		1382.5
+25			8.5		81.0
+50			10.0		79.5
* ⊙	1.99	1379.44	12.06	1377.45	
+75	✓		1.4		78.0
46+00	✓		2.9		76.5
+25	✓		4.4		75.0
+50	✓		5.9		73.5
+75	✓		7.4		72.0
47+00	✓		8.9		70.5
+25	✓		10.4		69.0
+50	✓		11.9		67.5
+75	✓		13.4		66.0
⊙	1.76	1368.90	12.30	1367.14	
48+00			4.4		64.5

From Sta 45. 67 ft. Sta.

		1368.90			
48+25			5.9		1363.0
+50			7.4		61.5
+75			8.9		60.0
49+00			10.4		58.5
+25			11.9		57.0
⊙	1.60	1358.50	12.00	1356.90	
+50			3.0		55.5
+75			4.5		54.0
50+00			6.0		52.5
+25			7.5		51.0
+50			9.0		49.5
⊙	2.12	1349.40	11.12	1346.68	
+75			1.4		48.0
51+00			2.9		46.5
+25			4.4		45.0
+50			5.9		43.5
+75			7.4		42.0

Hash carries consideratly water 4x4. culvert.

Rocky Point

17

		1349.40			
51+00 ✓			8.9		1340.5
+ 25 ✓			10.4		39.0
+ 50			11.9		37.5
⊙	0.37	1337.67	12.10	1337.30	
⊙	3.36	1330.63	10:40	1327.27	
53+00			+ 3.9		34.5
⊙	10.78	1336.35	5.06	1325.57	
+ 25 ✓			3.3		33.0
+ 50 ✓			4.8		31.5
+ 75			6.3		30.0
54+00			7.8		28.5
+ 25			9.3		
+ 50			10.8		
+ 75			12.3		24.0
⊙	1.46	1326.98	10.83	1325.52	
55+00			4.5		24.5
+ 25			6.0		21.0

		1326.98			
55+50 ✓			7.5		1319.5
+75 ✓			9.0		18.0
56+00 ✓			10.5		16.5
⊙	0.88	1315.68	12.18	1314.80	
+25 ✓			0.7		15.0
+50 ✓			2.2		13.5
+75 ✓			3.7		12.0
57+00 ✓			5.2		10.5
+25 ✓			6.7		9.0
+50 ✓			8.2		7.5
+75 ✓			9.7		6.0
58+00 ✓			11.2		4.5
+25 ✓			12.7		3.0
⊙	2.95	1306.50	12.13	1303.65	
+50			5.0		1.5
+75			6.5		1300.0
59+00			8.0		1298.5

		1306.80			
59+25			9.5		1297.0
+50			11.0		95.5
+75			12.5		94.0
⊙	0.29	1296.09	10.70	1295.80	
60+00			3.6		92.5
+25			5.1		91.0
+50			6.6		89.5
+75			8.1		88.0
61+00			9.6		86.5
⊙	0.53	1285.79	10.82	1285.26	
+25			0.8		85.0
+50			2.3		83.5
+75			3.8		82.0
62+00			5.3		80.5 Not exact Main + x + channel.
+30			7.1		78.7
+50			8.3		77.5
+75			9.8		76.0

		1285.79			
63+00			11.3		1274.5
+25			12.8		73.0
⊙	1.09	1274.23	12.65	1273.14	
+50			9.7		71.5
+75			4.2		70.0
64+00			5.7		68.5
+25			7.2		67.0
+50			8.7		65.5
+75			10.2		64.0
65+00			11.7		62.5
+25			12.2		61.0
⊙	1.21	1263.05	12.39	1261.84	
+50			3.5		59.5
+75			5.0		58.0
66+00			6.5		56.5
+25			8.0		55.0
⊙			11.07	1251.98	

From Sta 64 to Sta 69+50 From notes.

	2.00	1253.98		1251.98	
66+50			0.5		1253.5
+75			2.0		52.0
67+00			3.5		50.5
+25			5.0		49.0
+50			6.5		47.5
+75			8.0		46.0
68+00			9.5		44.5
+25			11.0		43.0
⊙	2.99	1246.17	10.80	1243.18	
+50			4.7		41.5
+75			6.2		40.0
69+00			7.7		38.5
+25			9.2		37.0
+50			10.7		35.5
⊙	0.44	1234.61	12.00	1234.17	
+75			0.6		34.0
70+00			2.1		32.5

Dry wash no water running this year. 2x2 tox

		1234.61			
70+25			3.6		1231.0
+50			5.1		29.5
+75			6.6		28.0
71+00			8.1		26.5
⊙	4.06	1230.13	8.53	1226.08	
+25			5.1		25.0
+50			6.6		23.5
+75			8.1		22.0
72+00			9.6		20.5
⊙	0.80	1220.44	10.49	1219.64	
+25			1.4		19.0
+50			2.9		17.5
+75			4.4		16.0
73+00			5.9		14.5
+25			7.4		13.0
+50			8.9		11.5
+75			10.4		10.0

June, 23. 1907

		1220.44			
24+00			11.9		1208.5
⊙	1.17	1210.26	11.35	1209.09	
+25			3.3		7.0
+50			4.8		5.5
+75			6.2		4.0
25+00			7.8		2.5
+25			9.3		1.0
* ⊙	4.26	1207.98	6.64	1203.62	
+50			8.5		1199.5
+75			10.0		98.0
26+00			11.5		96.5
+25			13.0		95.0
⊙	2.59	1197.63	12.94	1195.04	
+50			4.1		93.5
+75			5.6		92.0
27+00			7.1		90.5
+25			8.6		89.0

24

		1197.63			
77+50			10.1		1187.5
+75			11.6		86.0
78+00			13.1		84.5
⊙	0.94	1186.84	11.72	1185.90	
+25	✓		3.8		83.0
+50	✓		5.3		81.5
+75	✓		6.8		80.0
79+00	✓		8.3		78.5
+25	✓		9.8		77.0
+50	✓		11.3		75.5
+75	✓		12.8		74.0
⊙	0.80	1175.24	12.40	1174.44	
80+00			4.7		72.5
+25			4.2		71.0
+50			5.7		69.5
+75			7.2		68.0
81+00			8.7		66.5

		1175.24			
81+25			10.2		1165.0
+50			11.7		63.5
+75			13.2		62.0
⊙	0.08	1163.19	12.13	1163.11	
82+00			2.7		60.5
+25			4.8		58.4
+50			6.9		56.3
83+00			8.7		54.5
+25			10.2		
+50			11.7		
+75			13.2		1150.0
⊙			12.90	1150.29	

See page 26. For a trial line from Sta 75+50 to a point opposite Sta 83+75 at Elv. of about 50 above Sta. 83+75 of Lower Line. The object is to avoid several bad Inlet crossings by raising the line at this point.

Upper Trial line.

		1202.94		
75+50.			3.44	1199.50
76				
+50				
77				1199.50
+50				
78				1199.5
+50				
79+00				1199.5
+50			3.44	
⊙	4.67	1202.35	5.26	1197.68
80.			4.85	1199.50
+50				
⊙	7.75	1205.23	4.87	1197.48
84			5.73	1199.5
+50				
			3.60	1201.63

Sta. of Sta 83+75 of lower line

	5.84	1207.47		1201.63	
85+00			8.0		1199.5
+50					
86+10					
+50			8.0		1199.5
87+00			11.0		96.5
⊙	0.13	1195.63	11.97	1195.50	
+50			2.1		93.5
88+00			5.1		90.5
+50			8.1		87.5
89+00			11.1		84.5
⊙	2.15	1185.65	12.13	1183.50	
+50			4.1		81.5
90+00			7.1		
+53			10.1		
91+00			13.1		

From Sta. 86+50 6%

Retracement from Sta. 20.

20	12.61	1500.61		1488.00		Elev at Sta. 20
19+75			11.6		1489.0	
+50			10.6		90.0	
+25			9.6		91.0	
19			8.6		92.0	
+75			7.6		93.0	
+50			6.6		94.0	
+25			5.6		95.0	
18			4.6		96.0	
⊙	3.35	1503.73	0.43	1500.38		
17+75			6.7		97.0	
17+50	6.40	1504.40		1498.0		
+25			5.4		99.0	
17			4.4		1500.0	
16+75			3.4		1501.0	
+50			2.4		2.0	
+25			1.4		3.0	

		1504.40			
	12.10	1514.88	1.62	1502.78	
15+75			9.44		1505.35
+50			7.9		7.0
+25			6.44		
15.			4.9		
14+75			3.44		11.5
+50			1.9		
+25			0.44		14.5
⊙	11.18	1526.76	1.30	1513.58	
14				8.8	1516.0
13+75				7.3	
+50				5.8	
+25				4.3	
13.				2.8	

30

Feb. 28, 1907

Retracement

	11.17	1481.17			1470	Sta. 22+25
22+00			9.7		71.5	
22+75			4.7	76.5	73.0	+ 3.5
⊙	12.97	1494.06	0.08	1481.09		
+50					74.5	
+25			8.8	85.2	76.0	+ 9.2
22			0.9	83.1	77.5	+ 15.6
21+75			6.6	87.4	79.	+ 8.4
+50			7.0	87.	80.5	+ 6.5
+25			4.7	89.3	82.0	+ 7.3
21			2.2	91.8	83.5	+ 8.3
20+75			5.7	88.3	85.0	+ 3.3
+50			3.8	90.2	86.	+ 4.2
+25			6.5	87.5	87	+ 0.5
20			5.0	89.	88	+ 1.0

31

28+75	11.23	1458.73		1447.50	
			45	1445.28	
28				6.7	1452.0
					50.5
+50			9.8	48.9	49.0
+75			11.2		47.5
29			11.9	46.8	46.
⊙	0.69	1447.50	11.92	1446.81	
+25			2.9	44.6	44.5
+50			4.7	42.8	43.
+75			1.8	45.7	41.5
⊙	4.41	1451.34	0.57	1446.93	
30					40
+25			7.5	43.8	38.5
+50			1.3		1437.0
	0.95	1439.29	13.00	1438.34	
+75			57	33.6	35.5
31					1434.0

3/15/07

Ground at Sta

	+ 0.8	
	− 0.2	1439.3
	+ 4.2	1433.9
	+ 5.3	39.2
		.8
	− 1.9	39.3

Retacument from Sta 42

42+00	11.35	111.35		100.00		Ground level
41+75			10.35		101	
+50			9.35		102	
+25			8.35		103	
41			7.35		104	
+75			6.35		105	
+50			5.35		106	
+25			5.6 4.35	5.7	107	F1.3
40			3.35		108	
+75			2.35		109	
+50			1.35		110	
⊙ +~~25~~			0.43	110.92		
~~39~~	11.63	122.55				
39+25				11.55	112	
39				10.55	112	
+75				9.55		
+50				8.55		

38+50		122.55	7.55	115
+25			7.55	115
38+00			6.55	
+75			5.55	
+50			4.55	
⊙			2.85	119.70
	5.8	125.5		
37+00			1.8	123.7
+25			2.975	
50			4.150	
75			5.325	
38			~~6.50~~	
+25			~~7.675~~	
⊙	4.50	121.13	8.87	116.63
38			2.13	119
+25			3.30	
+50			4.48	

		121.13			
38+75			5.65		
39			6.83	114.3	F 2.4
+25			8.005		
+50			9.18		
+75			10.35		
40			11.53		
+25			12.70		
+50			~~13.88~~	107.25	
⊙	1.15	110.06	12.22	108.91	
40+50			7.00 2.81	107.25	F 4.2
+75			3.985		
41			5.160		104.74
+25			6.33		
+50			7.51		
+75			8.685		
42			9.86	100.20	1382.2

Sewing Grade on Road from Barrett
Commencing at Sta 44+00

44		1382.50	
	6.47	1388.97	
+50			1379.00
+75			
T.P.		12.04	1376.93
	13.66	1380.59	
45			
+25			
+50			1372.0
+75			
46			
T.P		12.35	1368.24
	1.62	1369.86	
+25			
+50			1365.0
+75			
47			
+25			

Down down Cottonwood Creek Canyon

Apr. 6. 1907.

Sew. B. Harris,
N. L. Hall
R. Wheeler
Max. Watson
Ford Beebe
"Bill" Kuhnle

9.97	
11.72	
5.09	1/0
6.84	
8.59	
10.34	
12.09	
3.11	
4.86	
6.61	
8.36	
10.11	

36.

		1369.86			
47+50				1358.	11.86
T.P.			11.80	1158.06	
	6.38	1364.44			
+75					8.19
48				1354.5	9.94
T.P.			12.40	1352.04	
	3.00	1355.04			
+25					2.29
+50				1351.00	4.04
+75					5.79
49					7.54
+25					9.29
+50				1344.00	11.04
+75					12.79
T.P.			11.08	1343.96	
	0.45	1344.41			
50				1340.50	3.91

1.10

37

1344.41

50+75					5.66
+50				1337.00	7.41
+75					9.16
51					10.91
+75					12.66
T.P.			12.62	1331.79	
	3.77	1335.56			
+50				1330.00	5.56
+75					7.31
52					9.06
+75					10.81
+50				1323.00	12.56
T.P.			12.61	1323.95	
	6.05	1329.00			
+75					7.75
53					9.50
+75					11.75

1/10

38						
		1329.00				
53+50				1316.00	13.00	
T.P.			11.27	1317.73		
	365	1321.38				
+75					7.13	
54					8.88	
+25					10.63	
+50				1309.00	12.38	
T.P.			12.12	1309.26		
	4.73	1313.99				
+75					6.74	
55					8.49	
+25					10.24	
+50				1302.00	11.99	
T.P.			11.76	1302.23		
	0.12	1302.35				
+75					2.10	
56					3.85	

0.11

		1302.35				
56+25					5.60	
+50				1295.0	7.35	+3.1
+75					9.10	
57					10.85	+3.3
T.P.			17.32	1290.03		
	2.62	1297.65				
+25					2.1	1.0
+60				1287.30	5.35	
+75					6.40	
58					8.15	
+25					9.90	
+50				1281.00	11.65	
+75					13.40	
T.P.			12.41	1280.24		
	8.73	1288.97				
59				1277.50	11.47	
+25					13.22	

40

1288.97

T.P.			12.18	1276.79		
	1.75	1278.54				
59+50					1274.00	4.54
+75						6.29
60						8.04
+25						9.79
+50					1267.00	11.54
+75						13.29
T.P.			17.59	1265.95		
	1.27	1267.22				
61					1263.50	3.72
+25					1261.75	5.47
+50					1260.64	6.58
+75						6.58
62						6.58
+38						6.58
+77						6.58

0.10

0.0

× × ×

#1						
		1267.22				
62+77				1260.64	6.58	
63				1259.14		
T.P.			9.68	1257.54		
	0.76	1258.30				
+25				57.52	0.78	
+50				55.90	2.40	
+75				54.27	4.03	
64				52.65	5.65	
+25				51.02	7.28	
+50				49.40	8.90	
+75				47.77	10.53	
65				46.15	12.15	
T.P.			11.46	1246.84		
	0.93	1247.77				
+25				44.52	3.25	
+50				42.90	4.87	
+75				41.27	6.50	

-6.5

42

1247.77

66 1239.65 8.12

+21 9.38 1238.39 38.25 9.49 × = T.P. on Rock.

Shelf around Island

.237 1240.76

+50 39.00 1.76

+75 37.50 3.3 ✓

67 abandoned 36.00 4.8 ✓

+25 34.50 6.3 ✓

+50 33.00 7.8 ✓

+75 31.50 9.3 ✓

68 30.00 10.8 ✓

+25 28.50 12.3 ✓

⊙ 12.51 1238.25

1.46 1239.71

+50 27.00 2.7 ✓

+75 25.50 4.2 ✓

69 24.00 5.7 ✓

+25 22.50 7.2 ✓

1/50

1/50

Tying new line to Old.

	12.90	1241.15	1228.25
66+75			1239.0
67			
+25			
+50			
+75			
68			
+27			

Apr. 9th 1907.

= T.P. on page 42

2.15

0.0

Sam B. Hamm
R. Wheeler
Max Watson
Ford Beebe
Geo. Sanders
"Bill" Kerkum

= Sta 69 Old line

Trial line from 75+50 to

			1174.44
	11.46	1185.92	
⊙		1.17	1184.75
	12.36	1197.11	
⊙		1.21	1195.90
	7.01	1202.91	
76+75			1199.50
77			1197.75

Apr 9. 1907. Witte

= T.P. on 1st location near Sta. 79+75
Kings elev. 1174.44

3.41 This Trial line ties on to Kings "Upper Trial line" at this Sta.

5.16

0.0

		1202.91					
77+25				1196.00	6.91		
⊙			9.02	1193.89 ✓			
	1.73	1195.62 ✓					
+50				1194.25	1.37		
+75				1192.50	3.12		
⊙			13.20	1182.42 ✓			
	8.34	1190.76 ✓					
78				1190.75	.01	0.1	mor sat
+25				1189.00	1.76		
+50				1187.25	3.51		
+75				1185.50	5.26		
79				1183.75	7.01		
+25				1182.00	8.76		
+50				1180.25	10.51		
+75				1178.50	12.26		
			12.73	1178.03 ✓			
	2.42	1180.45 ✓					

#5.						
		1180.45				
80				1176.75	3.70	
+25				1175.00	5.45	
+50				1173.25	7.20	
+75				1171.50	8.95	
81				1169.75	10.70	-1.0
+25				1168.00	12.45	
⊙			12.38	1168.07		
	1.13	1169.20				
+50				1166.25	2.95	
+75				1164.50	4.70	
82				1162.75	6.45	
+25				1161.00	8.20	
+50				61.00	8.20	
+92				61.00	8.20	
83				61.00	8.20	-0.0
+25				61.00	8.20	
+50				61.00		

Set with a 4.16 rod from #3 (1165.16)
on next page

#6						
—		1169.20				
83 +75				1161.00		Sur with H.16 rod from #1 Record
⊙			0.65	1168.55 ✓		
	5.27	1173.82 ✓				
⊙			11.31	1162.44 ✓		
	2.72	1165.16 ✓				
84				1161.00	#16	
⊙			7.10	1158.06 ✓		1.00
	6.37	1164.43 ✓				
+25				1161.00	3.43	
+45				61.00	3.43	
+90				61.00	3.43	
85				61.00	3.43	
+25				61.00	3.43	
+50				61.00	3.43	
+75				61.00	3.43	
86				61.00	3.43	
+25				1159.25	5.18	0.17 X

47.

1164.43

86+50				1157.50	6.93
+75				1155.75	8.68
87				1154.68	10.43
+25				1152.25	12.18
⊙			9.93	1154.50 ✓	
	3.20	1157.70 ✓			
+50				1150.50	7.20
+75				1148.75	8.95 ✓
88				1147.00	10.70 ✓
+25				1145.25	12.45 ✓
⊙			18.11	1145.59 ✓	
	4.62	1150.21 ✓			
+50				1143.50	6.71 ✓
+75				1141.75	8.46
89				1140.00	10.21 ✓
+75				1138.25	11.96 ✓
+50					13.71 ✓

1:10

mur ouest galerie acquéreur 2x+ calvert.

+8.

1150.

12.10 1138.11 ✓

2.03 1140.14 ✓

89+75		1134.75	5.39 ✓
90			
+25		1133.0	7.14 ✓
+50		1131.25	8.89 ✓
+75		1129.50	10.64 ✓
⊙	12.51 1127.63 ✓	1127.75	12.39 ✓
	1.55 1129.18 ✓		
91		1126.65	3.48 ✓ +0.9
+28		1124.25	6.09 ✓
+35			5.93 +2.3
+46		1123.5	6.70
+88		1120.75	9.64
92		1119.20	10.48
+33		1117.45	12.19
+40		1115.5	13.29

1 / 10

49

		11.94			
⊙			12.74	1116.74 ✓	
	2.19	1118.93 ✓			
92+50				1115.50	3.43 not over - in gully
+75				1113.75	5.18 ✓
93				1112.00	6.93 ✓
+25				1110.25	8.68 ✓
+50				1108.50	10.43 ✓
+75				1106.75	12.68 ✓
⊙			12.45	1106.48 ✓	
	1.85	1108.33 ✓			
94				1105.00	3.33 ✓
+25				1103.25	5.08 ✓
+50				1101.50	6.83 ✓
+75				1099.75	8.58 ✓
95				1098.00	10.33 ✓
+12			9.0	1099.33	= Sta. 94 of King line

50/ Retracement of Kings Run.

		1108.33		
⊙			9.98	1099.35	= Sta 94 Kings Run
	5.65	1105.00		
			12.21	1092.79	= Sta 95 - "
⊙			12.22	1092.78	
	2.22	1095.00		
			6.40	1088.60	= Sta 96
			11.30	1083.70	= Sta 97
⊙			12.85	1082.15	
	1.86	1084.01		
			9.00	1075.01	= Sta 98
			10.50	1073.51	Sta 99
⊙			12.69	1071.32	
	4.26	1075.58		
			6.70	1068.88	Sta 100.
⊙			6.63	1068.95	Reference Pr.

903

Sta 95				1098.0
	3.20	1101.15		1097.95
95 +50				1095.2
96				1093.7
+50				1090.5
97				1085.5
⊙	5.72	1094.63	17.24	1088.91
+50				1086.2
98				1083.7
+50				1081.3
⊙	2.49	1085.07	12.05	1082.58
99				1079.0
+50				1076.6
100				1074.2
⊙	4.96	1077.85	12.18	1072.89
+50				1071.8
101				1069.5
Reference Pt. on Preceding Page			8.82	1069.03
		1077.77		

= Point at 95 Set to an average grade of Decimal stations

5.6	
7.9	
10.3	
12.7	
	1+75
8.5	
10.9	
13.3	
6.1	
8.8	
10.9	
6.0	
8.4	

May 10th 1907

S.B. Harris
R. Ernest
Max Watson
Ford Bourbon
Geo Sauer
W.M. Moss
R. Mitchell (Examiner)

on Rock - base 97+03

Peg 2' R 98+37

peg line 100+11

(Showing that original Elev. was 0.08' high)

Hence now H.I.

52

101					(1069.4)
		1077.77			
101+50			10.4		1065.7
Bm.			9.13	1068.64	
⊙	3.09	1068.40	12.66	1065.31	
102			3.8	1064.6	
+50			5.6	1062.8	
103			6.9	1061.5	
+50					1058.0
⊙	0.44	1056.73	12.11	1056.29	
104					1054.5
+50					1051.
105					1047.5
+50					1044.0
⊙	2.13	1046.41	12.45	1044.28	
106					1040.5
+50					1037.0
107					1033.5
⊙	1.95	1036.13	12.23	1034.18	

119	+1.5		
		Top of Granite Boulder 36' L	101+50
		peg 3' L	101+60
10.4			
		peg Iron	103+52
2.2		Continued from 105+50	
5.7		May 11th 1907.	
9.2		Same Crew.	
12.7			
		peg	105+50
5.9			
9.4			
12.9			
		peg 3' R	107+24

53

		1036.13								
107	+50				1030.0	6.1				
108					1026.5	9.6				
	+50				1027.0	18.1				
⊙		0.29	1024.15	12.37	1023.16			Rock	3' R.	105+56
109					1019.5	4.7	1/10			
	+31			10.1	1014.1					
	+50			17.4	1006.7	1016.0	-9.3	Bottom of gulch		
	+75			24	1021.8	1014.25	9.9	+7.5		
110				7.6	1016.6	1012.5	11.7	+4.1		
⊙		1.47	1017.95	12.67	1011.48			Rock	6' L	110+24
	+50					1009.0	4.0			
111						1006.5	7.5			
	+50					1002.0	11.0			
⊙		0.63	1001.31	12.27	1000.68			Dry	hill	111+71
112						999.5	2.8			
	+50					995.0	6.3			
113						991.5	9.8			

54

1001.31

113+50				998.0	
⊙	3.44	992.08	12.67	988.64	
114			4.8	987.3	
+50			6.2	985.9	
115			4.9	987.2	
⊙	5.10	992.46	4.72	987.36	
+50			7.1	985.4	
116			10.5	982.0	
+50			11.5	981.0	
117			11.9	980.6	
+50			11.6	980.9	
+35			11.79	980.67	

133

Rock 113+50

Reg 115+00

= 114 = T.P. at Sta 114 on line up from Cottonwood.

55

56

39+50	3.95	103.95			
TP	3.10	101.48	5.57	98.38	
T.P	1.52	90.60	12.4	89.08	
43+80			11.6		
T.P	2.51	92.28	0.83	89.77	
T.P	2.89	83.57	11.60	80.68	
T.P.	1.25	72.23	12.60	70.97	
45+50			8.22	~~8.2~~	64.00
T.P.	0.73	60.54	12.41	59.81	
47+75			10.04	3	50.50
T.P.	2.80	50.33	13.01	47.53	
49+25			8.83		41.50
T.P ~~51+00~~	9.44	57.62	2.15	48.18	
51+00			1.98	55.64	
T.P	1.46	46.26	11.82	45.80	31.00
T.P.	5.04	38.90	12.40	33.86	

Upper Road
Lower Road

58

60+75	1.16	101.6		100
	0.05	88.75	12.94	88.7

Station	Sta.	Lower Target	Corrected Rod
300	1	0.xx	1x.78
	x	0.51	1x49
L 10.7	3	0.53	1x47
	4	0.9x	1x.08
	5	1.x0	11.80
	6	1.61	11.39
	7	1.77	11.x3
	8	x.06	10.94
	9	x.x1	10.79
	10	x.40	10.60
	△	x.45	10.55
	11	x.4x	10.58
	1x	x.38	10.6x
	13	x.x3	10.77
	14	189	11.11
	15	x.06	10.94
	16	7.45 7.5x	11.03

Station	Sta.	Lower Target	Corrected Rod
300	17	1.87	11.13
	18	1.98	11.0x
	19	x.01	10.99
	x0	x.14	1086
	x1	1.89	11.11
	xx	1.77	11.x3
	x3	1.47	11.53
	x4	1.x4	11.76
	x5	1.07	11.93
	x6	0.58+	1x4x

Station	Sta.	Lower Target	Corrected Rod
290	1	6.85 6.85	1x30
	x	1.01	11.99
	3	1.28	11.7x
	4	1.55	11.45
	5	x.00	11.00
	6	x.16	10.84
	7	x.x0	10.80
	8	x.19	10.81
	9	x.18	10.8x
	10	x.05	10.95
	11	x.19	10.81
	1x	x.x9	10.71
	13	x.17	10.83
	14	7.53 7.55	10.9x
	15	7.45 7.53	11.0x
	16	x.0x	10.98
	17	x.31	10.69

Station	Sta.	Lower Target	Corrected Rod
290	18	x.4x	10.58
	△	x.39	10.61
	19	x.3x	10.68
	x0	x.04	10.96
	x1	x.00	11.00
	xx	1.6x	11.38
	x3	1.31	11.69
	x4	0.97	1x.03

Contour	Sta	Lower Target	Corrected Rod
280	1	1.07	11.98
	2	0.90	12.10
	3	1.43	11.57
	4	1.82	11.18
	5	1.96	11.04
	6	2.26	10.74
	7	2.49	10.51
	8	2.79	10.21
	9	2.77+	10.23
	10	2.53	10.47
	11	2.61	10.39
	12	2.48	10.52
	13	2.46	10.54
	14	2.58	10.42
	15	2.46	10.54
L 3.0	16	2.49	10.51
	17	2.57	10.43

Contour	Sta	Lower Target	Corrected Rod
280	18	2.53	10.47
	19	2.42	10.58
	20	2.20	10.80
	21	1.74	11.26
	22	1.47	11.53
	23	1.25	11.75

Contour	Sta	Lower Target	Corrected Rod
270	1	1.56	11.44
	2	1.83	11.17
R.07	3	2.04	10.96
	4	2.50	10.50
	5	2.76	10.24
	6	2.89	10.11
	7	2.98	10.02
	8	2.85	10.15
	9	2.77	10.23
	10	2.94	10.06
	11	2.87	10.13
	12	2.82	10.18
	13	3.15	9.85
	14	3.22	9.78
	15	3.38	9.62
	△	3.30	9.70
	16	3.13	9.87

Contour	Sta	Lower Target	Corrected Rod
270	17	2.90	10.10
	18	2.44	10.56
	19	2.28	10.72
	20	2.30	10.70
	21	1.95	11.05
	22	1.70	11.30
	23	1.52	11.48

Contour	Sta	Lower Target	Correct Rod
260	1	1.87	11.13
	2	2.39	10.61
	3	2.50	10.50
	4	2.65	10.35
	5	3.00	10.00
	6	3.31	9.69
	7	3.40	9.60
	8	3.89	9.11
	9	3.86	9.14
	10	3.60	9.40
	11	3.36	9.64
	12	3.33	9.67
	13	3.28	9.72
	14	3.24	9.76
	15	3.20	9.80
	16	3.27	9.73
	17	3.30	9.70

Contour	Sta	Lower Target	Correct Rod
260	18	3.25	9.75
R15	19	3.05	9.95
	20	2.35	10.65
	21	2.25	10.75
	22	2.10	10.90

Contour	Sta	Lower Target	Correct Rod
250	1	2.36	10.64
	2	2.60	10.40
	3	2.82	10.18
	4	3.10	9.90
	5	3.39	9.61
	6	3.51	9.49
	7	3.72	9.28
	8	4.14	8.86
	9	4.33	8.67
	10	4.00	9.00
	11	3.73	9.27
	12	3.78	9.22
	13	3.75	9.25
	14	3.62	9.38
	15	3.74	9.26
	16	3.77	9.23
	17	3.60	9.40

Contour	Sta	Lower Target	Correct Rod
250	18	3.54	9.46
	19	3.69	9.31
	20	3.56	9.44
	21	3.34	9.66
	22	3.02	9.98
	23	2.75	10.25
	24	2.60	10.40

Criterion	Sta	Lower Target	Corrected Rod
240	1	3.14	9.86
	2	3.44	9.56
	3	3.67+1	9.34
	4	3.78+1	9.23
	5	3.83	9.17
	6	4.05	8.95
	7	3.96	9.04
	8	4.04	8.96
	9	4.03	8.97
	10	3.93	9.07
	11	4.09	8.91
	12	4.09	8.91
	13	4.09	8.91
	14	4.16	8.84
	15	4.21	8.79
	16	4.44	8.56
	17	4.38+1	8.63

Criterion	Sta	Lower Target	Corrected Rod
240	18	4.60	8.40
	19	4.40	8.60
	20	4.01	899
	21	3.83	917
	22	3.61	939
	23	3.42	958
	24	3.26	974
	25	2.81	1019
	26	2.55	1045

Criterion	Sta	Lower Target	Corrected Rod
230	1	3.14	9.86
	2	3.55	9.45
	3	3.68	9.32
	4	3.97	9.03
	5	4.09	8.91
	6	4.44	8.56
	7	4.61	8.39
	8	4.85+4	8.15+4 8.19
	9	5.10+1.7	7.92
	10	5.06	7.94
	11	4.83+3	8.20
	12	4.76	8.24
	13	4.67	833
	14	4.68	832
	15	4.62	838
	16	4.48	852
	17	4.55	8.45

Criterion	Sta	Lower Target	Corrected Rod
230	18	4.47	853
	19	4.48	852
	20	4.54	846
	21	4.40	860
	22	4.29	871
	23	4.10	890

Contour	Sta	Lower Target	Corrected Rod
220	1	4.10	8.90
	2	4.57	843
	3	4.64	836
	4	4.57	843
	5	4.74	826
	6	4.69	831
	7	4.59	841
	8	4.76	824
	9	4.85	815
	10	4.85	815
	11	4.86	814
	12	5.15	785
	13	5.22	778
	14	5.26	774
	15	4.98	802
	16	4.73	827
	17	4.55	845
220	18	4.48	852
	19	4.16	884
	20	4.02	898
	21	3.87	913
	22	3.75	925
	23	3.45	955
	24	3.31	969

Contour	Sta	Lower Target	Corrected Rod
210	1	3.77	9.23
	2	4.05	895
	3	4.33	867
	4	4.33	867
	5	4.52	848
	6	4.47-1.8	8.53
	7	4.88	812
	8	5.04	796
211	9	5.12	788
	10	5.59	741
	11	5.76	724
	△	5.77	723
	12	5.83	717
	13	5.78	722
	14	5.68	732
	15	5.59	741
	16	5.39	761
210	17	5.22	7.78
	18	5.33	767
	19	5.30	770
	20	5.29	771
	21	5.07	793
	22	5.08	792
	23	4.99	801
	24	5.05	795
	25	4.95	805
	26	4.78	822
	27	4.58	842

65

200				200			
	1	4.83	8.17		17	5.29	7.71
	2	5.08	7.92		18	5.09	7.91
	3	5.09	7.91	R 30	19	4.98	8.02
	4	5.18	7.82		20	5.08+26	7.92+26
	5	5.09	7.91		21	4.74	8.26
	6	5.30	7.70		22	4.62	8.38
	7	5.22	7.78		23	4.38	8.62
	8	5.38	7.62		24	4.18	8.82
	9	5.52	7.48		25	3.93	9.07
	10	5.36	7.64				
	11	5.51	7.49				
	12	5.67	7.33				
	13	5.97	7.03				
	14	6.07	6.93				
	△	5.98	7.02				
	15	5.98	7.02				
	16	5.70	7.30				

190				190			
	1	4.10	8.90		17	5.43	7.57
	2	4.24	8.76		18	5.49	7.51
	3	4.54	8.46		19	5.58	7.42
	4	4.63	8.37		20	5.56	7.44
	5	4.76	8.24		21	5.40	7.60
	6	5.09+13	7.91+13		22	5.43	7.57
	7	5.20	7.80		23	5.40	7.60
	8	5.50	7.50		24	5.18+2	7.82+2
	9	6.11	6.89		25	5.29+1	7.71+1
	10	6.21	6.79		26	5.19	7.81
	△	6.24	6.76		27	5.21	7.79
	11	6.24	6.76		28	5.01	7.99
	12	6.20	6.80				
	13	6.11	6.89				
	14	5.94	7.06				
	15	5.79	7.21				
	16	5.67	7.33				

West Side -

Contour	Sta	Tower Target	Correct Rod	Contour	Sta	Tower Target	Correct Rod
		6.64					
350	1	6.67	12.69	350	18	1.14	11.86
		6.76					
	2	6.74	12.50		19	0.99+6	12.01+6
	3	0.74	12.28				
	4	0.55	12.45				
	5	0.81	12.19				
	6	1.06	11.94				
	7	1.15	11.85				
	8	0.87	12.13				
	9	1.09	11.91				
	10	1.15	11.85				
	11	1.00	12.00				
	12	0.85	12.15				
		6.87					
	13	6.86	12.77				
	14	0.75	12.25				
	15	0.83	12.17				
	16	1.04	11.96				
	17	1.23	11.77				

Feb. 25, 1907

Contour	Sta	Tower Target	Correct Rod	Contour	Sta	Tower Target	Correct Rod
340	1	1.05	11.95	340	18	1.00	12.00
	2	1.25	11.75		19	0.86	12.14
	3	1.37-5.	11.63-5.		20	0.74	12.26
	4	1.10	11.90		21	0.90	12.10
	5	1.11	11.89		22	0.92	12.08
	6	0.90	12.10		△	0.68	12.32
	7	0.87	12.13		23	0.64	12.36
						6.58	
4.5 L	8	0.86	12.14		24	6.63	12.79
	9	0.93	12.07				
	10	1.18	11.82				
	11	1.15	11.85				
	12	1.38	11.62				
	13	1.06	11.94				
	14	1.20	11.80				
	15	1.01	11.99				
	16	1.25	11.75				
	17	1.21	11.79				

330	1	6.73 6.74	17.53	330	17	1.03	11.97	320	1	1.37	11.68	320	17	1.28	11.72
	2	061	17.39		18	1.08	11.92		2	1.50+3.5	11.50+3.5				
	3	1.01	11.99		19	1.25	11.75		3	1.34+4	11.66+4				
	4	1.00	17.00		20	1.20	11.80		4	1.32	11.68				
	4	1.12	11.88		21	1.21	11.79		5	1.25	11.75				
	5	118	11.82						6	1.28	11.72				
	6	0.94	12.06						7	1.20	11.80				
	7	1.08	11.92						8	1.36	11.64				
	8	1.07-4	11.93-4						9	1.44	11.56				
	9	1.46	11.54						10	1.36	11.64				
	10	1.38-2	11.62-2						11	1.31	11.69				
	11	1.20	11.80						12	1.15	11.85				
	12	1.22	11.78						13	1.36	11.64				
	13	1.37	11.63						14	1.39	11.61				
	14	1.26	11.74						4	133	11.67				
	15	1.01	11.99						15	1.29	11.71				
	16	1.00	17.00						16	0.95	17.05				

310	1	1.34	11.66	310	17	1.36	10.64
	2	1.26	11.74			1.76	11.24
	3	1.44	11.56		18	1.33	10.67
	4	1.61	11.39			1.73	11.27
	5	1.64	11.36		19	1.22	10.78
	6	1.59	11.41			1.64	11.36
	7	1.71	11.29				
	8	1.60	11.40				
	9	1.75	11.25				
	10	1.72	11.28				
	11	1.74	11.26				
	12	1.59	11.41				
	13	1.66	11.34				
	14	1.61	11.39				
	15	1.62	11.38				
	16	1.73	11.27				
		1.61	11.39				

		1.39	10.61				
300	1	1.85	11.15	300	18	1.21	10.79
		1.45	10.55				
	2	1.87	11.13		△	1.21	10.79
		1.42	10.58				
	3	1.85	11.15		19	1.13	10.87
		1.22	10.77				
	4	1.77	11.23		20	1.81	11.19
		1.54	10.46				
	5	1.02	10.98		21	1.88	11.12
		1.38	10.62				
	6	1.84	11.16				
		1.38	10.62				
	7	1.83	11.17				
	8	1.74	11.26				
	9	1.76	11.24				
	10	1.99	11.01				
	11	1.89	11.11				
	12	1.96+1.7	11.04+1.7				
	13	1.97	11.03				
	14	1.96	11.04				
	15	1.88	11.12				
	16	2.12	10.88				
	17	2.13	10.87				

290	1	7.32	10.68	290	18	7.49	10.51	280	1	7.56	10.44	280	19	7.64	10.36
						7.08	10.92			7.17	10.83				
	2	7.38	10.62			7.53	10.47		2	7.65+3.	10.35+3.		△	7.67	10.33
					19	7.17	10.83			7.23+3.	10.77+3.				
	3	7.28	10.72			7.38	10.62		3	7.80	10.20		20	7.69	10.31
					20	1.98	11.02			7.33	10.67				
	4	7.39	10.61			7.58	10.42		4	7.59	10.41		21	7.63	10.37
					21	7.16	10.84			7.19	10.81				
	5	7.61	10.39			7.51	10.49		5	7.55	10.45		22	7.31	10.69
					22					7.10	10.90				
	△	7.60	10.40						6	7.24	10.76		23	7.39	10.61
	6	7.58	10.42							7.65+3	10.35+3				
									7	7.29+3.	10.71+3.		24	7.35	10.65
	7	7.45	10.55						8	7.14	10.86				
	8	7.43	10.57						9	7.26	10.74				
	9	7.15	10.85						10	7.44	10.56				
	10	7.32	10.68						11	7.22	10.78				
	11	7.26	10.74						12	7.34	10.66				
	12	7.03	10.97						13	7.28	10.72				
	13	7.12	10.88						14	7.52	10.48				
	14	7.12	10.88						15	7.56	10.44				
	15	7.27	10.73						16	7.35	10.65				
	16	7.09	10.91						17	7.43	10.57				
	17	7.06	10.94						18	7.49	10.51				

270	1	2.87	10.18	270	18	2.79	10.21
	2	2.85	10.15		19	2.76	10.24
	3	2.74	10.26		20	2.84	10.16
	4	2.99	10.01		21	2.81	10.19
	5	3.23	9.77		22	2.66	10.34
	△	3.33	9.67		23	2.73	10.27
	6	3.26	9.74		24	2.88	10.12
	7	3.05	9.95		25	2.92	10.28
	8	3.07	9.93		26	2.73	10.27
	9	2.98	10.02				
	10	3.13	9.87				
	11	3.13	9.87				
	12	2.89	10.11				
	13	2.93	10.07				
	14	2.83	10.17				
	15	2.95	10.05				
	16	2.80	10.20				
	17	2.80	10.20				

260	1	2.91	10.09	260	18	3.50	9.50
	2	2.88	10.12		19	3.42	9.58
	3	2.96	10.04		20	3.25	9.75
	4	2.78	10.22		21	3.03	9.97
	5	2.98	10.02		22	3.12	9.88
	6	2.98	10.02		23	3.12	9.88
	7	2.91	10.09				
	8	2.92	10.08				
	9	2.84	10.16				
	10	2.95	10.05				
	11	3.09	9.91				
	12	3.35	9.65				
	13	3.34	9.66				
	14	3.15	9.85				
	15	3.39	9.61				
	16	3.55	9.45				
	17	3.55	9.45				
	△	3.54	9.46				

250				250			
	1	3.38	9.62		18	3.06	9.94
	2	3.37	9.63		19	3.05	9.95
	3	3.26	9.74		20	3.18	9.82
	4	3.23	9.77		21	3.19	9.81
	5	3.52	9.48		22	2.93	10.07
	6	3.70	9.30		23	2.98	10.02
	7	3.82	9.18		24	3.04	9.96
	Δ	3.82	9.18		25	2.98	10.02
	8	3.77	9.23		26	3.03	9.97
	9	3.39	9.61				
	10	3.60	9.40				
	11	3.59	9.41				
	12	3.40	9.60				
	13	3.30	9.70				
	14	3.22	9.78				
	15	3.18	9.82				
	16	3.06	9.94				
	17	3.00	10.00				

240				240			
	1	3.22	9.78		19	3.79	9.21
	2	3.15	9.85		20	4.02	8.98
	3	3.25	9.75		Δ	4.04	8.96
	4	3.35	9.65		21	4.03	8.97
	5	3.09-2	9.91-2		22	3.95	9.05
	6	3.02	9.98		23	3.74	9.26
	7	3.25	9.75		24	3.47	9.53
	8	3.31	9.69		25	3.59	9.41
	9	3.16	9.84		26	3.52	9.48
	10	3.23	9.77		27	3.46	9.54
	11	3.23	9.77				
	12	3.32	9.68				
	13	3.35	9.65				
	14	3.46	9.54				
	15	3.55	9.45				
	16	3.78	9.22				
	17	3.78	9.22				
	18	3.66	9.34				

72

230				230			
	1	4.69	8.31		19	4.47	8.53
	2	4.72	8.28		20	4.56	8.44
	3	4.72	8.28		21	4.47	8.53
	4	4.63	8.37		22	4.41	8.59
	5	4.61	8.39		23	4.45	8.55
	6	5.02	7.98				
	7	5.20	7.80				
	8	5.33	7.67				
	9	5.27	7.73				
	10	4.96	8.04				
	11	4.93	8.07				
	12	5.08	7.92				
	13	5.07	7.93				
	14	4.72	8.28				
	15	4.62	8.38				
	16	4.54	8.46				
	17	4.47	8.53				
	18	4.52	8.48				

220				220			
	1	4.55	8.45		19	5.46	7.54
	2	4.55	8.45		20	5.51	7.49
	3	4.62+6.	8.38+6.		△	5.45	7.55
	4	4.68+11.7	8.32+11.7		22	5.43	7.57
	5	4.50+1	8.50+1		23	5.37	7.63
	6	4.61	8.39		24	5.04	7.96
	7	4.68	8.32		25	4.75	8.25
	8	4.61	8.39		26	4.86	8.14
	9	4.61	8.39		27	4.85	8.15
	10	4.69	8.31		28	4.91	8.09
	11	4.69	8.31		29	4.80	8.20
	12	4.94	8.06				
	13	4.81	8.19				
	14	4.89	8.11				
	15	5.26	7.74				
	16	5.37	7.63				
	17	5.31	7.69				
	18	5.25	7.75				

73

210	1	4.90	8.10	210	15	4.96	8.04
	2	5.07	7.93		16	4.96	8.04
		4.94	8.06		17	4.83	8.17
		5.02	7.98		18	4.80	8.20
	3	5.06	7.94		19	4.82	8.18
	4	4.97	8.03		20	4.55	8.45
		5.10	7.90		21	4.60	8.40
	5	5.19	7.81		22	4.69	8.31
	6	5.58	7.42		23	4.74	8.26
	7	5.74	7.26		24	4.69	8.31
	8	5.78	7.22				
		5.77	7.23				
	9	5.64	7.36				
	10	5.43	7.57				
	11	5.56	7.44				
	12	5.54	7.46				
	13	5.42	7.58				
	14	5.11	7.89				

200	1	5.07	7.93
	2	5.03-4	7.97-4.
	3	5.04	7.96
	4	5.09	7.91
	5	4.89	8.11
	6	4.97	8.03
	7	5.18	7.82
	8	5.17	7.83
	9	5.35	7.65
	10	5.41	7.59
	11	5.62	7.38
	12	5.87	7.13
	13	5.88	7.12
	14	5.96	7.04

74 3/18/07

East Side.

350	1	6.01 5.96	1403	340	1	5.94 5.92	1414	340	18	6.13 6.11	1376	300	1	0.15	1285
	2	6.10 6.09	1381		2	6.16 6.15	1369		19	6.00 6.01	1399		2	6.62 6.61	1277
	3	6.24 6.26	1350		3	6.31 6.30	1339					~~9.01~~	3	0.10	1260
	4	6.44 6.46	1310		4	6.44 6.43	1313						4	6.81 6.80	1239
	5	6.55 6.56	1289		5	0.25	1295						5	0.12	1288
	6	6.56 6.54	1290		6	0.26	1274						6	1.41	1159
	7	6.47 6.42	1311		6	0.25	1295					~~1.01~~	7	1.49	1151
	8	6.42 6.40	1318		7	6.45 6.44	1311						8	1.90	1110
	9	6.50 6.47	1303	~~0.51~~	8	6.39 6.37	1324						9	1.98	1102
	10	6.46 6.48	1306		9	0.10	1290						10	2.20	1080
	11	6.35 6.34	1331		10	0.16	1284						△	2.22	1078
	12	6.42 6.41	1317		11	6.54 6.52+50	1294+50						11	2.25	1075
	△	6.55 6.54	1291		12	0.23	1277						12	2.17	1083
	13	6.53 6.51	1296		13	0.17	1283						13	2.01	1096
	14	6.52 6.50	1298		14	6.64 6.62	1274						14	1.88	1117
	15	6.38 6.38	1324		15	0.18	1282						15	2.02	1098
	16	6.25 6.24	1351		16	6.49 6.51	1300						16	2.01+2.0	1099+2.
	17	5.88 5.85	1427		17	6.32 6.33	1335						17	1.85+1.5	1115+1.5

East Side

300	18	1.88	1117	290	1	6.86 6.85
	19	2.05	1095		2	0.97
	20	2.03	1097		3	1.28
	21	1.92	1108		4	1.48
	22	1.71	1129		5	2.03
	23	1.41	1159		6	2.08
	24	1.20	1180		7	2.14
	25	0.97	1203		8	2.14
	26	0.59	1241		9	2.13
					10	2.01
					11	2.12
					12	2.30
					13	2.17
					14	7.57 7.57
					15	7.50 7.51
					16	2.04
					17	2.29
					18	2.42

1229						
1203						
1172						
1152						
1097						
1092						
1086						
1086						
1087						
1099						
1088						
1070						
1083						
1086						
1099						
1096						
1071						
1058						

East Side

290	△	2.42	1058			
	19	2.34	1066			
	20	2.08	1092			
	21	1.99	1101			
	22	1.63	1137			
	23	1.34	1166			
	24	0.95	1205			
	25	0.55	1245			
230	5	4.11	889			
220	18	4.49	851			

West Side

240	6	4.36	864
	7	4.34	866
250	21	4.24	876
	22	3.94	906

127	8	2	118+40	8	2
					E
26	8	1	118	8	1
125	8	1	117	8	1
					E
124	8	2	116	8	1
123	8	2	115	8	1
+65	8	1	114	8	1
+15	0	0	113	8	1
122	8	1	112	6	1
+85	0	0	111+55	16	3
+25	0	0	111	8	2
		E			
121	8	1	110+50	0	0
+55	8	2	110	8	1
120	8	1	109+40	14	3.5
					E
+60	8	1	109	8	2
					E
+30	8	2	108	8	2
					E
119	0	0	107	8	2
118+65	0	0	106	8	2

105	8	2.5	90	18	0
		E			
104	9.5	2.5	89+35	18	15
103	9.5	5	+90	0	8
					E
102	8	4.5	+55	0	0
		E			
101	8	2.5	+20	11	16
					E
100	8	2.5	88+10	7	11
		E			
99	8	2.5	+95	9	18
98	8	2.5	+75	0	0
		E			
97	8	2	+60	0	0
		E			
96	8	2	+45	10	17
					E
		E			
95	8	1	+35	0	0
		E			
94	8	2	87+15	24	15
		E			
93	8	2	+95	0	0
+60	0	0	+55	16	0
		E			
92+20	0	0	+30	16	4 9 16
					E
91	8	14 22	86	19	8.7
		E			
90+35	0	0	85+04	0	0

June 1 1907

County Road Job #44

Johnsons Camp.

Sta	Width	Heighth	Sta	Width	Heighth
35+50			42+50	7.5	3.7
36	14.5	27 (26) E 34	43+15	5	L.R. 2
+50	13	18 (16) L.R. 26	+16	10	8 L.R.
+85	10	21 (17) R. 28	+50	14	L.R. 3.5
37+13	13.5	39.5 (34) 47	43+90	0	0
+35	17	43 (37) R. 54	43+10	0	0
+60	16	34 (27) R. 45	+40	13.8	E 7.9
38+66	0	0	+65	11	E 4
39+18	0	L.R. 0	44	9.7	E 4.
+23	15	D. 5.	44+50	12	L.R. 5.
+50	14	R & E. 13	45	9	L.R. 5.5
32+75	12.5	D. 5.4	+50	14	L.R. 8.7
Old Road Cut		R.	33+75	14	L.R. 7
+50	0	0	33+95	16	E
41	12	6.5	33+75	0	L.R. 0
+50	8.4	5.5	34+50	15	L.R. (41) 45 53
+70	0	0	Vert. H. 8'		
42+00	12	R. (23) 34 E 5	35+	11	
42+25	9.4	R. (24) 36 E 3	35+40	18	
49			49+56	0	0 L.R.
+16	10	8 L.R.	50	15	2' Dup. E
51+17	0	0			
+50	3.8	3 E			
+88	5.5	5 E			
52	6.5	11 E			
+20	6	4 E			
+50	5.4	6 E			
52+80	5	4.5 E			
53	3	3 E			
53+32	0	0			
55+0	0	0			
+20	4.3	3 E			
55+39	0	0			

18 Bringing up 3 Benches from new elevation of 44+50.

44+50	10.38	1389.38		1379.00			
+25					1380.75	863	
T.P.			4.71	1384.67			
	17.33	1397.00					
BM			0.32	1396.68			
	11.75	1408.43					
T.P.			0.03	1408.40			
	12.28	1420.68					
T.P.			1.75	1418.93			
	17.595	1431.52					
BM			2.10	1429.42			
	12.95	1442.37					
T.P.			0.92	1441.45			
	12.51	1453.96					
T.P.			1.32	1452.64			
	6.73	1459.37					
BM			5.21	1454.16			

Apr. 9th 1907.

R. Wurzer
Max Walsh
Ford Beebe
Geo. Lane

39+61	On Rock	
34+12	On Rock	
30+03	On Rock	

	12.53	1162.82		1150.29
	12.04	1174.53	0.31	1162.51
	12.71	1186.60	0.64	1173.89
	37.36		.75	
	95		0.05	1186.55
	36.31			9.18
	1150.29			1195.73
	1186.60			3.04
				1192.69
				10.15
				1202.84
	1202.84			
	3.85	1201.36	5.30	1197.51
	2.85	1202.94	2.42	1199.09
		3.44		
	11	1403.5		1392.5
			.7	1402.8
	10.9	1413.7		
37.5			8.5	
37+0			5.5	1408.2
B.M.			.3	1413.4
	1.6	1415.0		
35450			0.0	1415.0

	137+52	8	2
	137	8	2
	136	8	2
	135	8	1
	134	8	1
	133	8	2
	132	0	6
	131	8	1
	130	8	1.5
Ou. Rock	129	8	2
	128	18	1

79

80

12 chains

Road Work 9-10-11-12-13

101.90 = 16

16+25

2.9

3.9

4.9

5.9

10.52	1538.49	1547.95	
8,7	1545.8	1.40	1537.1
		1.3	1535
		2.8	1530
		1.5	
		1.3	

100

83775 = 1150

16725 97.50

6 100 = 1052.50

97.50 66+50 1238.

3350. 175.50

16.50

50.00

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		

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