

285



Final Cross Sections

LEVEL BOOK

16.380 F

0100 - 77-88.2

W 285

~~85~~

285

285

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

MICROFILMED

JAN 11 1965

O.R. - S.D. 2nd. Main Pipe Line.
U.S.G.S. Datum.

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Final Cross Sections - Trench
Excavation - Schedule I.

Page	Description
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MICROFILMED

JAN 1 1962

O.R.-S.D. 2nd Main Pipe Line.
 "A" Line - Final Cross Sections.
 Sta. 0+00 to Sta.

Sta.	Grade	Elev.	Dist.	L.C.	¢
0+00	395.66	395.66			0.0
0+03	395.66	395.66	1.0		0.0
0+04	395.66	401.7			6.0
+09.6	395.66	401.7	5.6		6.0
+25	395.7 395.66	403.3	15.1		7.6
+75	395.7 393.22	399.6	50.0		3.9
+77	395.7 393.1	399.1	13.0		3.4
0+90	395.7	395.7	123.0		0.0

92" Trench

Jan. 2, 1930. Converse - Notes.
 Clear + Warm. Hill - Grades.
 Elliott -
 Simpson
 Walton
 Av. End Area C.V.

R.C.	End Area	Av. End Area	C.V.
	0.0		
	0.0		
	28.98	14.49	0.54
	28.98		6.01
	28.98		6.01
	26.82	23.91	13.64
	36.75	32.87	18.70
	20.24	33.25	31.48
	13.65	27.97	0.95
	11.90	28.98	2.22
	5.95	15.94	2.86
Chd. Trm. M.	0.00		13.38
Y.A.L.			

End areas calc. by
 L.B. from 0+00 to
 .70+94.

~~Moved by
 City Forces.~~

~~Figures for
 (Not figured) trench?~~

Schedule II
 Structure Exc.

Schedule I
 Trench Exc.

Sta.	Grade	Elev	Dist.	L.C.	±	R.C.	End Area	Ar. End Area	e.Y.
1+00	395.7 ✓ 392.00	392.6			↓ 0.0 0.6		0.0 ✓ 2.89		
			↓ 40.0				0.0 ✓ 1.45	0.0 ✓ 0.21 ✓	
1+04	395.7 ✓ 392.00	392.00			↓ 0.0		0.0 ✓		
			↓ 53.4				0.0 ✓		
1+57.4	395.7 ✓ 392.00	392.00			↓ 0.0		0.0 ✓		
			↓ 12.6				0.0 ✓ 8.70	0.0 ✓ 7.06 ✓	
1+70	395.7 ✓ 392.00	395.6			↓ 0.0 3.6		0.0 ✓ 12.39 ✓		
			↓ 15.0				14.11 ✓ 24.74 ✓	2.28 ✓ 12.08 ✓	
1+85	395.7 ✓ 392.00	397.4			↓ 1.7 5.4		8.21 ✓ 26.08 ✓		
			↓ 15.0				9.66 ✓ 27.53 ✓	5.37 ✓ 15.29 ✓	
2+00	395.7 ✓ 392.00	398.0			↓ 2.3 6.0		11.11 ✓ 28.98 ✓		
			↓ 30.0				12.07 ✓ 29.97 ✓	13.41 ✓ 33.30 ✓	

Chd. T.M.M.

yes so state them in
for page.

Leading

first hand

~~6.6~~
2.4

~~0.0~~
1.8

Sta.	Grade	Elev.	Dist.	L.C.	¢	R.C.	End Area	Av. End Area	C.V.
2+30	395.17 395.00	398.4	20.0%	6.4 2.7	2.7 6.4	6.4 2.5	13.04 33.75	22.00 38.50	16.30 28.52
+ 50	394.16 395.00	401.0	25.0%	7.3 6.4	6.4 9.0	9.0 3.2	30.95 48.06	29.97 48.87	27.75 37.84
+ 75	393.3 395.00	399.3	25.0%	7.3 6.0	6.0 7.3	7.3 2.7	28.98 35.67	28.98 32.32	26.83 29.95
3+00	at. ✓ 392.00	398.00	25.0%	6.0 2.4	6.0	6.0 2.4	28.98	21.88 23.01	23.01
3+25	390.70	395.0	15.0%		4.3		20.77	24.87 13.82	13.82
+ 40	389.9	395.9	10.0% PAL.	6.0 2.4	6.0	6.0 2.4	28.98	28.98	10.73

Chd. T.M.M.

Sta.	Grade	Elev.	Dist.	L.C.	±	R.C.	End. Area	Av. End Area	C.V.
3+50	✓ 389.4	395.4	✓ 25.0	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	✓ 28.98	✓ 28.36	✓ 23.48
+75	✓ 388.1	392.6	✓ 25.0		✓ 4.5		✓ 21.71		
4+00	✓ 386.8	392.5	✓ 50.0		✓ 5.7		✓ 27.53		
+50	✓ 384.76	390.0	✓ 50.0		✓ 5.8		✓ 28.01		
5+00	✓ 383.85	389.9	✓ 35.0	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	✓ 28.98	✓ 28.50	✓ 52.78
+35	✓ 383.6	390.8	✓ 55.0	✓ $\frac{7.4}{2.7}$	✓ 7.2	✓ $\frac{7.4}{2.8}$	✓ 35.42	✓ 32.20	✓ 41.74
			✓ VAL.				Chd. T.M.M.	✓ 35.64	✓ 72.10

Sta.	Grade		L.C.	±	R.C.	End Area	Av End Area	C.Y.
5+90	383.2	390.5	$\frac{7.3}{2.7}$	7.3	$\frac{7.3}{2.7}$	35.67	33.83	12.53
		10.0						
6+00	383.15	389.8	$\frac{6.6}{2.6}$	6.6	$\frac{6.6}{2.6}$	31.98	30.48	11.29
		10.0						
+10	383.1	389.1	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98	26.81	9.93
		10.0						
+20	383.0	388.1		5.1		24.63	25.84	57.72
		60.0						
+80	382.6	388.2		5.6		27.05	28.02	10.38
		10.0						
+90	382.5	388.5	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98	28.98	10.73
		10.0						
		VAL.						

Chd. T. M. M.

Sta.	Grade	Elev.	Dist.	L.C.	±
7+00	✓ 382.45	388.5	✓ 50.0 ²	✓ 6.0	
+50	✓ 382.10	387.5	✓ 15.0 ²	✓ 5.4	
+65	✓ 381.4	387.1	✓ 35.0 ²	✓ 5.7	
8	✓ 379.7	384.2	✓ 25.0 ²	✓ 4.5	
+25	✓ 378.5	383.5	✓ 20.0 ²	✓ 5.0	
+45	✓ 377.6	383.6	✓ 9.9 ² VPL.	✓ 6.0 2.4	

R.C.

6

End Area	Av. End Area	C.Y.
28.98 [✓]	27.53 [✓]	50.98 [✓]
26.08 [✓]	26.81 [✓]	14.89 [✓]
27.53 [✓]	24.63 [✓]	31.93 [✓]
21.74 [✓]	22.98 [✓]	21.25 [✓]
24.15 [✓]	26.56 [✓]	19.67 [✓]
28.98 [✓]	29.97 [✓]	10.99 [✓]

Chd. T.M. 711.

			L.C.	±
8 + 54.9	377.07	383.5	$\frac{6.4}{2.5}$	6.4
			15.1	
+ 70	375.8	383.4	$\frac{7.6}{2.8}$	7.6
			10.0	
+ 80	374.9	382.4	$\frac{7.5}{2.8}$	7.5
			4.75	
+ 84.75	374.55	381.5	$\frac{6.9}{2.6}$	6.9
			15.25	
9 + 00	372.2	378.2	$\frac{6.0}{3.4}$	6.0
			14.38	
+ 14.38	369.9	374.8		4.9
			29.22	
			V.P.	

	End Area	End Area	C.V.
	$\frac{6.4}{2.5}$	30.95	
		34.30	19.18
	$\frac{7.6}{2.8}$	37.64	
		37.21	13.78
	$\frac{7.5}{2.8}$	36.78	
		35.15	6.18
	$\frac{6.9}{2.6}$	33.52	
		31.25	17.65
	$\frac{6.0}{3.4}$	28.98	
		26.33	14.02
		23.67	
	Chd. T.M.M.	23.91	25.88

L.C. \$

9+43.60 363.05 368.0

5.0

21.4²

+65 357.2 363.0

5.8

26.65²

+91.65 349.97 355.0

5.0

29.22²

10+20.87 343.19 348.3

5.1

29.65²

10+50.52 338.63 341.5

2.9

25.28²

10+75.80 336.32 336.3

0.0

26.6²

V.A.L.

R.C.

8

End Area ^{Av.} End Area C.Y.24.15²26.08² 20.67²28.01²26.08² 26.74²24.15²24.39² 26.40²24.63²19.32² 21.22²14.01²7.01² 6.56²0.0²

Chd. T.M.M.

0.0² 0.0²

L.G. Σ

R.G.

9

End Area End Area C.V.

✓ 11+02.4	✓ 336.28	336.3	✓ 8.03 ²	✓ 0.0
+10.43	✓ 336.27	337.3	✓ 29.57 ²	✓ 1.0
+10	✓ 337.3	339.5	✓ 35.0 ²	✓ 2.2
+75	✓ 338.6	343.6	✓ 25.0 ²	✓ 5.0
12+00	✓ 339.5	345.5	✓ 27.0 ²	✓ 6.0
+27	✓ 340.5	345.7	✓ 17.83 ²	✓ 5.2

✓
V.P.L.

0.0 ✓	2.11 ✓	0.72 ✓
1.83 ✓	7.73 ✓	8.47 ✓
10.63 ✓	17.39 ✓	22.57 ✓
24.15 ✓	26.86 ✓	24.59 ✓
28.98 ✓	27.05 ✓	27.05 ✓
25.12 ✓	20.77 ✓	13.72 ✓

Chd. T.M. 71.

Sta.	Grade	Elev.	Dist.	L.C.	Σ	P.C.	End Area	End Area	C.V.
12+44.83	✓ 341.1	344.5			✓ 3.4		16.42 ✓		
			✓ 2.17	✓ 2			11.59 ✓	0.93 ✓	✓ 10
+47.	✓ 341.3	342.7			✓ 1.4		6.76 ✓		
			✓ 17.79	✓ 2			13.53 ✓	6.41 ✓	✓ 10
+59.79	✓ 342.16	346.4			✓ 4.2		20.29 ✓		
			✓ 14.86	✓ 2			24.64 ✓	13.56 ✓	✓ 10
+74.65	✓ 344.21	350.2			✓ $\frac{6.0}{2.4}$	✓ 6.0	28.98 ✓		
			✓ 14.69	✓ 2		✓ $\frac{6.0}{2.4}$	37.97 ✓	20.66 ✓	✓ 10
+89.34	✓ 347.26	356.5			✓ $\frac{9.2}{3.2}$	✓ 9.2	16.96 ✓		
			✓ 5.66	✓ 2		✓ $\frac{9.2}{3.2}$	57.33 ✓	10.76 ✓	✓ 10
+95	✓ 348.5	359.0			✓ $\frac{10.5}{3.5}$	✓ 10.5	55.75 ✓		
			✓ 8.79	✓ 2		✓ $\frac{10.5}{3.5}$	49.48 ✓	16.11 ✓	✓ 10

Chd. T.M.M.

Total to here

55 on 7th
Schedule 11 Incl

✓ A.C.L.
1090.44
1083.89

Sta.	Grade	Elev.	Dist	L.C.	±	R.C.	End Area	Av. End Area	C.Y.
13+03.79	351.30	359.9	6.21 ²	$\frac{8.6}{3.1}$	8.6	$\frac{8.6}{3.1}$	43.20 ²	38.36 ²	8.82 ²
+10	353.3	360.2	50.0 ²	$\frac{6.9}{2.6}$	6.9	$\frac{6.9}{2.6}$	33.52 ²	37.46 ²	69.37 ²
+60	369.1	377.4	25.47 ²	$\frac{8.3}{3.0}$	8.3	$\frac{8.3}{3.0}$	11.40 ²	37.20 ²	35.02 ²
+88.42	377.1	383.9	29.16 ²	$\frac{6.8}{2.6}$	6.8	$\frac{6.8}{2.6}$	33.00 ²	30.99 ²	33.47 ²
14+14.58	384.12	390.1	17.16 ²	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98 ²	28.50 ²	13.32 ²
+27.26	386.30	397.1	14.88 ²		5.8		28.01 ²	27.05 ²	14.91 ²

Chd. T.M.M.

14+A2.08 388.22 393.6

14.98

5.4

End Area End Area C.V.
26.08

+57.06 389.05 394.0

15.0

5.0

25.11 13.93
24.15

+72.06 388.80 393.7

27.94
27.96

4.9

23.91 13.28
23.67
25.36 26.24
~~26.26~~

15+00 387.3 392.9

50.0

5.6

27.05
28.02 51.89

+50 384.5 390.5

50.0

6.0
2.4

6.0

6.0
2.4

28.98
30.73 56.91

16+00 381.8 388.5

50.0
A.L.

6.7
2.6

6.7

6.7
2.6

32.48
30.73 56.91

Chd. T.M.M.

Sta.			L.C.	£	R.C.	End Area	Av. End Area	C.V.
16+50	✓ 379.1	385.1	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	28.98 ✓		
			✓ 50.0 ✓				30.22 ✓	5-5.96 ✓
17+00	✓ 376.4	382.9	✓ $\frac{6.5}{2.5}$	✓ 6.5	✓ $\frac{6.5}{2.5}$	31.15 ✓		
			✓ 25.0 ✓				30.21 ✓	27.97 ✓
+25	✓ 375.0	381.0	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	28.98 ✓		
			✓ 59.41 ✓				26.33 ✓	5-7.94 ✓
+84.4)	✓ 371.76	376.7		✓ 4.9		23.67 ✓		
			✓ 14.94 ✓				25.60 ✓	14.17 ✓
+99.35	✓ 370.45	376.1		✓ 5.7		27.53 ✓		
			✓ 14.82 ✓				28.26 ✓	15.51 ✓
18+14.17	✓ 368.14	374.1	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	28.98 ✓		
			✓ 14.63 ✓					
			✓ A.L.				32.87 ✓	17.81 ✓

Chd. T.M.M.

Sta	End Area	Av. End Area	C.V.	L.C.	±	P.C.	End Area	Av. End Area	C.V.
18+28.80	364.84	372.3		$\frac{7.2}{2.7}$	7.5	$\frac{7.8}{2.9}$	36.77		
			9.20				39.70	13.53	
+38	362.1	370.6		$\frac{8.2}{3.0}$	8.5	$\frac{8.8}{3.1}$	42.63		
			5.18				40.54	7.78	
+43.18	360.6	368.4		$\frac{7.6}{2.8}$	7.8	$\frac{8.0}{2.9}$	38.45		
			14.06				41.78	21.76	
+57.24	355.3	364.2		$\frac{8.6}{3.1}$	8.7	$\frac{9.2}{3.2}$	45.11		
			13.72				46.33	23.54	
+70.96	349.11	358.4		$\frac{9.0}{3.2}$	9.3	$\frac{9.5}{3.3}$	47.54		
			16.04				38.26	22.73	
+87	341.3	347.3		$\frac{5.8}{2.4}$	6.0	$\frac{6.2}{2.5}$	28.98		
			13.0				27.77	13.37	
			A.L.				Chd. Tm. M.		

Sta.	Grade	Elev.	L.C.	±	P.C.	End Area	Av. End Area	C.V.
19+00	334.9 336.0	340.4		5.5		26.57		
			30.0				25.12	27.91
+30	320.3	325.2		4.9		23.67		
			20.0				26.57	19.68
							26.33	19.50
+50	310.5	316.5	6.1 6.0 2.4	6.1 6.0	6.1 6.0 2.1	29.46 28.98		
			25.0				27.83	25.77
							33.38	32.76
+75	301.1 298.2	306.5	4.9 4.8 2.9 2.41	5.9 5.3	6.0 6.0 2.91	26.20 41.78		
			29.09				30.46	32.82
							33.34	32.70
20+04.09	288.7 284.0	295.8	6.3 6.0 3.9 2.49	7.1 11.8	8.0 8.0 4.1 2.91	34.72 65.70		
			25.91				33.03	31.70
							48.42	46.56
+30	284.0	290.5	6.3 2.5	6.5	6.6 2.6	31.34		
			32.0					
			P.L.				30.16	35.75

Grade Change
See finish stake book for grades

Chd. T.M.M.

Sta.	Grade	Elev.	Dist.	L.C.	±	R.C.	End Area	End Area	C.V.
20+62	284.0 ✓	290.0	5.0 ✓	$\frac{6.0}{2.4}$ ✓	6.0 ✓	$\frac{6.0}{2.4}$ ✓	28.98 ✓	26.08 ✓	7.83 ✓
+67	284.0 ✓	288.8	12.0 ✓		4.8 ✓		23.18 ✓		
+79	284.0 ✓	289.3	11.0 ✓		5.3 ✓		25.60 ✓	24.39 ✓	10.84 ✓
+80	284.0 ✓	291.0	15.56 ✓	$\frac{7.2}{2.7}$ ✓	7.0 ✓	$\frac{6.8}{2.6}$ ✓	34.04 ✓	32.00 ✓	18.44 ✓
+95.56	284.0 289.6 ✓	295.8	19.44 ✓	$\frac{7.0}{4.1}$ $\frac{12.6}{2.66}$ ✓	$\frac{6.2}{11.8}$ ✓	$\frac{5.4}{3.7}$ $\frac{11.0}{2.41}$ ✓	$\frac{29.96}{65.88}$ ✓	$\frac{29.84}{58.84}$ ✓	$\frac{21.49}{21.54}$ ✓
21+15	284.0 296.6 ✓	302.8	15.0 ✓ P.A.L.	$\frac{6.9}{3.5}$ $\frac{10.7}{2.56}$ ✓	$\frac{6.2}{10.0}$ ✓	$\frac{5.7}{3.5}$ $\frac{9.5}{2.41}$ ✓	$\frac{29.86}{52.10}$ ✓	$\frac{29.78}{58.84}$ ✓	$\frac{13.96}{13.91}$ ✓

Chd. T.M.M.

Grade change

Grade Change →

			L.C.	±	R.C.	End Area	End Area	Q.V.
21+30	$\frac{302.0}{297.5}$	305.9	$\frac{4.1}{6.7}$ <u>2.6</u>	$\frac{3.8}{6.4}$	$\frac{3.4}{6.0}$ <u>2.4</u>	18.24 ✓ 30.82 ✓	23.35 ✓ 31.65 ✓	17.30 ✓ 23.11 ✓
			20.0 ✓					
+50	$\frac{309.2}{308.5}$	315.2	$\frac{6.2}{7.0}$ <u>2.7</u> 2.16	$\frac{5.9}{6.7}$	$\frac{5.6}{6.4}$ <u>2.5</u> 2.41	28.46 ✓ 32.47 ✓		
			50.0 ✓					
22+00	$\frac{331.00}{331.00}$	338.1	$\frac{7.6}{2.8}$	7.1	$\frac{6.9}{2.6}$	34.97 ✓		
			18.0 ✓					
+18	$\frac{339.10}{339.10}$	348.3	$\frac{6.6}{2.6}$	6.3	$\frac{6.0}{2.4}$	30.45 ✓		
			32.0 ✓					
+50	$\frac{353.5}{353.5}$	361.2	$\frac{7.9}{2.9}$	7.7	$\frac{7.6}{2.8}$	38.05 ✓		
			12.0 ✓					
+62	$\frac{358.9}{358.9}$	365.2	$\frac{6.8}{2.6}$	6.3	$\frac{6.0}{2.4}$	30.69 ✓		
			10.0 ✓					
			2 P.L.					
						39.07 ✓	14.17 ✓	

Chd. T.M.M.

L.C.

£

P.C.

22+72 ✓
363.4 ✓ 372.8 ✓ $\frac{9.7}{3.3}$

9.4

 $\frac{8.6}{3.1}$ End Area ^{Av.} End Area C.Y.

47.75 ✓

12.89 ✓

12.71 ✓

+80 ✓
367.0 ✓ 374.8 ✓ $\frac{8.5}{3.0}$

7.8

 $\frac{7.0}{2.7}$

38.33 ✓

33.66 ✓

1.99 ✓

+84 ✓
368.8 ✓ 374.8 ✓ $\frac{6.0}{2.4}$

6.0

 $\frac{6.0}{2.4}$

28.98 ✓

21.25 ✓

12.59 ✓

23 ✓
376.0 ✓ 378.8 ✓

2.8

13.52 ✓

30.0 ✓

19.08 ✓

21.20 ✓

+30 ✓
377.5 ✓ 382.6 ✓

5.1

24.63 ✓

15.0 ✓

23.43 ✓

13.02 ✓

+45 ✓
378.25 ✓ 382.8 ✓

4.6

22.22 ✓

15.0 ✓

Chd. T.M.M.

25.60 ✓

14.22 ✓

✓ P.L.

23+60	379.0	385.0	40.0
24+00	381.0	388.0	25.0
+75	382.25	389.4	25.0
+50	383.5	390.3	20.0
+70	384.5	392.0	20.0
+90	385.5	391.5	10.0

P.L.

$\frac{6.0}{2.4}$	6.0	$\frac{7.0}{2.7}$	7.2	$\frac{6.5}{2.5}$	6.8	$\frac{7.2}{2.7}$	7.5	$\frac{6.0}{2.4}$	6.0
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End Area	End Area	C.V.
28.98	31.60	16.81
31.21	34.70	32.13
35.18	34.15	31.62
33.11	31.80	25.78
36.48	32.73	21.24
28.98	27.05	10.02

Chd. T.M.M

Sta.	Grade		L.C.	±	R.C.	End Area	Av. End Area	C.V.
25+00	386.00	391.2		5.2		25.12		
			18.0				27.05	18.03
+18	385.6	391.6		6.0		28.98		
			17.0				32.63	20.54
+35	385.3	392.7		7.4		36.28		
			15.0				36.18	20.10
+50	385.0	392.4		7.4		36.08		
			10.0				33.83	12.53
+60	384.8	391.2		6.4		31.57		
			40.0				30.28	14.86
26+00	384.1	390.1		6.0		28.98		
			40.0				28.98	12.93

V.A.L.

Chd. T.M.M.

2596.83
A.C.C.

Total to here 2596.83
7/9/30
Total to here 2805.80
A.C.C.

End Area ^{Ar.} End Area C.F.

26 + 40 383.2 389.2

6.0
2.4

6.0

6.0
2.4

28.98

14.81

25.80 14.04

+54.81 383.0 387.6

4.6

22.22

29.95

22.70 25.18

+84.76 381.3 386.1

4.8

23.18

15.24

23.43 13.22

27 + 00 379.2 384.1

4.9

23.67

14.49

21.26 11.41

+14.49 377.3 381.2

3.9

18.84

29.35

20.29 22.06

+43.84 371.05 375.5

4.5

21.74

16.16
V.A.L.

25.36 15.18

Chd. T.M.M.

Sta.	Grade	Elev.	Dist	L.C.	±	R.C.	End Area	End Area	C.V.
27+60	↓	366.8	372.8	↓	6.0	↓	28.98	29.72	27.52
			18.0	$\frac{6.0}{2.4}$		$\frac{6.0}{2.4}$			
+85	↓	366.2	366.5	↓	6.3	↓	30.45	29.72	16.57
			15.0	$\frac{6.3}{2.5}$		$\frac{6.3}{2.5}$			
28+00	↓	356.2	362.2	↓	6.0	↓	28.98	28.26	25.12
			24.0	$\frac{6.0}{2.4}$		$\frac{6.0}{2.4}$			
+24	↓	350.9	356.6	↓	5.7	↓	27.53	28.26	11.51
			11.0						
+35	↓	348.5	354.5	↓	6.0	↓	28.98	32.88	18.27
			15.0	$\frac{6.0}{2.4}$		$\frac{6.0}{2.4}$			
+50	↓	345.2	352.7	↓	7.5	↓	36.78	34.38	13.29
			10.44	$\frac{7.5}{2.8}$		$\frac{7.5}{2.8}$			
			17.4						

Chd. T.M.M.

L.C.

±

R.G.

End Area ^{AV} End Area C.V.

28 + 60.44 342.9 349.5

$\frac{6.6}{2.6}$

6.6

$\frac{6.6}{2.6}$

31.98

14.75

3048 16.65

+ 75.19 340.17 346.2

$\frac{6.0}{2.4}$

6.0

$\frac{6.0}{2.4}$

28.98

14.91

25.84 14.27

+ 90.10 338.50 343.2

4.7

22.70

14.99

15.70 8.72

29 + 05.09 338.0 339.8

1.8

8.89

9.01

1.35 1.75

+ 14.1 338.0 338.0

0.0

0.0

31.1

0.0 0.0

+ 45.2 338.0 338.0

0.0

0.0

4.75
P.L.

Chd. T.M.M.

0.73 0.11

Sta.	Grade	Elev.	Dist.	L.C.	±
29+49.45	338.0	338.3			0.3
			29.96		
+79.41	339.2	342.6			3.4
			14.59		
+94	341.0	344.6			3.6
			15.18		
30 +09.18	342.94	348.2			5.3
			5.82		
+15	344.1	350.1		$\frac{6.0}{2.4}$	6.0
			5.0		
+20	345.7	351.0			5.9
			6.0		
			PA L.		

End Area ^{Ar.} End Area C.V.

1.45 ✓

8.94 ✓

9.92 ✓

16.12 ✓

16.91 ✓

9.17 ✓

17.39 ✓

21.50 ✓

12.09 ✓

25.60 ✓

27.29 ✓

5.88 ✓

28.98 ✓

28.74 ✓

5.32 ✓

28.50 ✓

27.53 ✓

6.12 ✓

Chd. T.M.M.

Sta.	Grade	Elev.	Dist.	L.C.	±	P.C.
30+26	346.3	351.8	17.53		5.5	
+38.53	349.1	354.5	28.77		5.4	
+67.30	357.6	363.6	17.7	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$
+85	361.9	368.3	15.0	$\frac{5.7}{2.4}$	6.4	$\frac{7.3}{2.7}$
31	365.5	371.8	25.63	$\frac{5.4}{2.4}$	6.3	$\frac{6.9}{2.6}$
+25.63	371.7	378.2	14.37	$\frac{5.5}{2.4}$	6.5	$\frac{8.0}{2.9}$
			A.L.			

End Area	Av. End Area	C.V.
26.57		
26.33		12.22
26.08		
27.53		29.33
28.98		
30.09		19.73
31.20		
30.65		17.03
30.10		
31.11		29.53
32.11		
34.40		18.31

Chd. T.M.M.

L.C.

£

R.C.

End Area ^{Av} End Area C.V.

31 + 40 ✓
372.8 ✓ 380.3 ✓

✓
6.2
2.5

7.5

✓
8.7
3.1

36.68 ✓

15.53 ✓

35.24 ✓
20.27 ✓

+55.53 ✓
374.1 ✓ 381.1 ✓

✓
5.8
2.4

7.0

✓
8.0
2.9

33.80 ✓

30.0 ✓

31.39 ✓
34.88 ✓

+85.53 ✓
374.1 ✓ 380.1 ✓

✓
6.0
2.4

6.0

✓
6.0
2.4

28.98 ✓

29.90 ✓

25.36 ✓
28.08 ✓

32 + 15.43 ✓
371.7 ✓ 376.2 ✓

4.5

21.74 ✓

9.57 ✓

23.19 ✓
8.22 ✓

+25 ✓
369.3 ✓ 374.4 ✓

5.1

24.63 ✓

10.0 ✓

26.81 ✓
9.93 ✓

+35 ✓
366.9 ✓ 372.9 ✓

✓
6.0
2.4

6.0

✓
6.0
2.4

28.98 ✓

5.0 ✓
A.L.

Chd. T.M.M. 30.06 ✓
5.57 ✓

L.C. \$

R.G. Jan. 3. 1930 Converse - Notes
Clear + Warm. Hill - Grades
Elliott - K
Simpson
Walton
End. Area End Area C.V.

27

32740 365.7 372.2

5.2
2.4

6.5

7.5
2.8

31.13

10.0

30.06 11.13

+50 363.2 369.2

6.0
2.4

6.0

6.0
2.4

28.98

6.0

28.98 6.44

+56 361.7 367.7

6.0
2.4

6.0

6.0
2.4

28.98

12.0

28.98 12.88

+68 358.8 364.8

6.0

28.98

19.5

28.98 20.93

+87.50 354.0 360.0

6.0

28.98

12.5

20.29 9.39

33+00 354.0 356.4

2.4

11.59

5.90
P.L.

5.80 1.27

Chd. T.M.M.

33 + 05.90 ↓
354.0 354.0

17.10 ✓

✓
0.0

+23.0 ↓
354.0 354.0

25.0 ✓

✓
0.0

+48 ↓
354.0 360.0

2.0 ✓

6.0
2.4

✓
6.0

6.0
2.4

28.98 ✓

+50 ↓
354.0 360.6

33.0 ✓

6.6
2.6

✓
6.6

6.6
2.6

31.98 ✓

+83 ↓
364.6 372.3

5.0 ✓

6.8
2.6

✓
7.7

9.1
3.2

38.61 ✓

+88 ↓
366.2 370.9

9.0 ✓
A.L.

✓
4.7

22.70 ✓

Chd. TIMM.

30.86 ✓ 10.29 ✓

End Area ^{Av} End Area C.V.

0.0 ✓

0.0 ✓ 0.0 ✓

0.0 ✓

14.49 ✓ 13.42 ✓

30.48 ✓ 2.26 ✓

35.30 ✓ 43.14 ✓

30.66 ✓ 5.68 ✓

33+97 369.0 ✓ 377.0

L.C. ✓
 $\frac{6.9}{2.6}$ 8.0

13.0 ✓

34+10 373.2 ✓ 380.5

✓
 $\frac{6.7}{2.6}$ 7.3

2.38 ✓

+17.38 375.6 ✓ 381.6

✓
 $\frac{6.0}{2.4}$ 6.0

28.9 ✓

+46.28 383.6 ✓ 388.7

✓
 5.1

13.7 ✓

+60 386.2 ✓ 392.2

✓
 $\frac{6.0}{2.4}$ 6.0

10.0 ✓

+70 388.2 ✓ 396.2

✓
 $\frac{6.6}{2.6}$ 8.0

5.72 ✓
 %AL

R.C.

End Area End Area^{Av} C.V.

✓
 $\frac{8.7}{3.1}$ 39.02 ✓

37.08 ✓ 17.85 ✓

✓
 $\frac{7.5}{2.8}$ 35.17 ✓

32.06 ✓ 8.76 ✓

✓
 $\frac{6.0}{2.4}$ 28.98 ✓

26.81 ✓ 28.70 ✓

24.03 ✓

26.81 ✓ 13.62 ✓

✓
 $\frac{6.0}{2.4}$ 28.98 ✓

33.88 ✓ 12.55 ✓

✓
 $\frac{8.8}{3.1}$ 38.77 ✓

37.80 ✓ 8.01 ✓

Chd. T.M.M.

3359.23 A.L.L.
~~3358.22~~
 Total to here
 7/9/30
 Total to here
 3568.20 P.C.L.

L.C.

£

P.C.

End Area ^{Ar} End Area C.V.

34+75.72 389.4 397.0

 $\frac{6.6}{2.6}$

7.6

 $\frac{8.2}{3.0}$

36.83

19.28²32.91⁰ 23.50²

+95 391.6 397.6

 $\frac{6.0}{2.4}$

6.0

 $\frac{6.0}{2.4}$

28.98

10.52²28.26⁰ 11.01⁰

35+05.52 392.8 398.5

5.7

27.53²4.48²28.26⁰ 4.69²

+10 393.0 399.0

 $\frac{6.0}{2.4}$

6.0

 $\frac{6.0}{2.4}$

28.98

5.0²32.88⁰ 6.09²

+15 393.2 400.7

 $\frac{7.5}{2.8}$

7.5

 $\frac{7.5}{2.8}$

36.78

20.5²37.78⁰ 28.68²

+35.5 394.0 401.8

 $\frac{7.6}{2.8}$

7.8

 $\frac{8.2}{3.0}$

38.78

9.5²
A.L.42.60⁰ 14.99²

Chd. T.M.M.

			L.C.	±
35+45	394.0	403.0	$\frac{8.9}{3.1}$	9.0
		18.0		
+63	394.0	402.5	$\frac{7.6}{2.8}$	8.5
		27.0		
+90	394.0	400.0	$\frac{5.4}{2.4}$	6.0
		20.0		
36+10	394.0	400.0	$\frac{5.7}{2.4}$	6.0
		10.0		
+20	394.0	400.9	$\frac{6.7}{2.5}$	6.9
		15.0		
+35	394.0	402.3	$\frac{7.3}{2.7}$	8.3
		19.8		
		VAL.		

	End Area	End Area	C.V.
	$\frac{9.6}{3.3}$	76.41	
		11.40	29.60
	$\frac{9.3}{3.2}$	42.39	
		35.63	35.63
	$\frac{6.5}{2.5}$	28.86	
		28.86	21.38
	$\frac{6.7}{2.5}$	28.86	
		31.20	11.56
	$\frac{7.6}{2.8}$	33.59	
		37.07	20.59
	$\frac{8.8}{3.1}$	40.59	
		45.84	33.62
	Chd. T.M.M.		

			L.G.	±	R.G.	End Area	End Area ^{Ar.}	C.V.
36+54.8	394.0	403.9	$\frac{8.5}{3.0}$	9.9	$\frac{11.0}{3.7}$	51.08		
		29.98				16.91	52.09	
+84.78	392.9	401.2	$\frac{7.7}{2.8}$	8.3	$\frac{9.8}{3.4}$	42.73		
		15.22				45.37	23.69	
37+00	391.2	400.6	$\frac{9.0}{3.2}$	9.4	$\frac{9.8}{3.4}$	48.40		
		14.59				45.96	24.84	
+14.59	389.5	398.1	$\frac{7.9}{2.9}$	8.6	$\frac{9.5}{3.3}$	43.51		
		7.41				36.24	9.94	
+22	388.1	394.1	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98		
		12.0	2.41			23.18	10.30	
+34	385.9	389.5		3.6		17.39		
		10.07				20.53	7.66	
		✓ A.L.				✓ A.C.L.		

37+44.07 384.0 388.9

5.93°

4.9

End Area ^{Av.} End Area C.Y.
23.67

+50 381.6 387.6

5.0°

$\frac{5.5}{2.4}$

6.0

$\frac{6.9}{2.6}$

29.47

26.57 5.84

+55 379.6 387.8

20.0°

$\frac{7.2}{2.7}$

8.2

$\frac{9.5}{3.3}$

41.25

35.36 6.55

+75 371.6 380.0

25.0°

$\frac{7.4}{2.8}$

8.4

$\frac{9.0}{3.2}$

41.99

41.32 30.61
41.37 30.64

38+00 361.6 367.6

50.0°

$\frac{6.0}{2.4}$

6.0

$\frac{6.0}{2.4}$

28.98

35.18 32.57
35.24 32.63

+50 343.6 349.6

33.0°

$\frac{6.0}{2.4}$

6.0

$\frac{6.0}{2.4}$

28.98

28.98 53.67

28.02 34.25

✓ P.C.L.

Sta.	Grade	Elev.	Dist	L.C.	±	R.C.	End Area	End Area ^{Av.}	C.V.
38+83	↓	333.3	338.9		✓		27.05		
			17.0				28.02	17.64	
39+00	↓	328.0	334.0		✓		28.98		
			50.0				28.98	53.67	
+50	↓	315.2	321.2		✓		28.98		
			10.0				28.98	10.73	
+60	↓	313.1	319.1		✓		28.98		
			10.0				17.87	6.62	
+70	↓	311.1	312.5		✓		6.76		
			8.0				17.87	5.29	
+78	↓	309.4	315.4		✓		28.98		
			22.0	6.0 2.4	✓	6.0 2.4	29.71	24.21	
							∅		

∅

			L.C.	±	P.C.	End Area	^{Av.} End Area	C.V.
40+00	304.9 ✓	311.1	$\frac{6.0}{2.4}$	6.0 ✓	$\frac{6.8}{2.6}$	30.71 ✓		
		50.0 ✓				29.89 ✓	55.38 ✓	
+50	294.6 ✓	300.6	$\frac{5.7}{2.4}$	6.0 ✓	$\frac{6.6}{2.6}$	29.37 ✓		
		25.0 ✓				30.67 ✓	28.40 ✓	
+75	289.4 ✓	296.0	$\frac{6.2}{2.5}$	6.6 ✓	$\frac{7.0}{2.7}$	32.00 ✓		
		15.0 ✓				30.61 ✓	17.01 ✓	
41+00	286.4 ✓	292.4	$\frac{5.8}{2.4}$	6.0 ✓	$\frac{6.4}{2.5}$	27.22 ✓		
		10.0 ✓				28.14 ✓	10.42 ✓	
41+00	284.3 ✓	289.9		5.6 ✓		27.05 ✓		
		25.0 ✓				26.33 ✓	24.38 ✓	
+25	279.15 ✓	284.5		5.3 ✓		25.60 ✓		
		5.0 ✓				27.29 ✓	5.05 ✓	

P.R.C.L.

			L.C.	±	R.C.	End Area	End Area	C.V.
41+30	✓ 272.7	283.7	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	28.98 ✓		
			✓ 20.0 ✓			38.77 ✓	26.51 ✓	
41+50	✓ 271.6	280.1	✓ $\frac{8.5}{3.0}$	✓ 8.5	✓ $\frac{8.5}{3.0}$	42.60 ✓		
			✓ 15.0 ✓			49.18 ✓	27.33 ✓	
+65	✓ 267.0	277.5	✓ $\frac{10.5}{3.5}$	✓ 10.5	✓ $\frac{10.5}{3.5}$	55.75 ✓		
			✓ 15.0 ✓			57.19 ✓	31.77 ✓	
+80	✓ 262.5	273.4	✓ $\frac{10.9}{3.6}$	✓ 10.9	✓ $\frac{10.9}{3.6}$	58.62 ✓		
			✓ 5.0 ✓			53.47 ✓	9.90 ✓	
+85	✓ 261.0	270.4	✓ $\frac{9.4}{3.3}$	✓ 9.4	✓ $\frac{9.4}{3.3}$	48.26 ✓		
			✓ 5.0 ✓			38.62 ✓	7.15 ✓	
+90	✓ 261.0	267.0	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	28.98 ✓		
			✓ 35.0 ✓			28.26 ✓	36.63 ✓	

P.A.C.L.

			L.C.	Σ	R.C.	End Area	End Area ^{AK}	C.V.
42+25	261.0	266.7		5.7		27.53		
			5.0°				26.08	1.83
+30	261.1	266.2		5.1		24.63		
			10.0°				24.81	9.93
+40	261.3	267.3		$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98	
			10.0°				34.60	12.81
+50	261.5	269.6		$\frac{8.1}{2.9}$	8.1	$\frac{8.1}{2.9}$	40.21	
			50.0°				39.34	72.85
43+00	262.5	270.3		$\frac{7.8}{2.9}$	7.8	$\frac{7.8}{2.9}$	38.47	
			50.0°				36.26	67.15
+50	263.5	270.5		$\frac{7.0}{2.7}$	7.0	$\frac{7.0}{2.7}$	34.05	
			50.0°				32.50	60.19

			L.C.	Σ	R.C.	End Area	End Area	C.V.
44+00	264.5	270.9	$\frac{6.4}{2.5}$	6.4	$\frac{6.4}{2.5}$	30.95		
			50.0			29.97	53.50	
+50	265.5	271.5	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98		
			25.0			28.98	26.83	
+75	266.0	272.0	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98		
			25.0			27.78	25.72	
+5	268.5	274.0		5.5		26.57		
			25.0			27.78	25.72	
+25	271.0	277.1		6.0		28.98		
			25.0			28.74	26.61	
+50	273.5	279.4		5.9		28.00		
			50.0			26.81	49.65	

✓A.C.L

End Area ^{Av.} End Area C.V.

46+00 ✓
278.5 283.7

✓
5.2

25.12 ✓

✓
10.03 ✓

26.33 ✓ 9.78 ✓

+10.03 ✓
279.5 285.2

✓
5.7

27.53 ✓

✓
29.52 ✓

25.36 ✓ 27.73 ✓

+39.55 ✓
284.8 289.6

✓
4.8

23.18 ✓

✓
14.35 ✓

23.43 ✓ 12.75 ✓

+53.9 ✓
288.4 293.3

✓
4.9

23.67 ✓

✓
6.1 ✓

26.33 ✓ 5.95 ✓

+60 ✓
289.8 295.8

✓
6.0
2.4

✓
6.0

✓
6.0
2.4 28.98 ✓

✓
7.0 ✓

31.79 ✓ 8.24 ✓

+67 ✓
291.3 298.4

✓
7.1
2.7

✓
7.1

✓
7.1
2.7 31.59 ✓

✓
16.19 ✓

31.79 ✓ 19.06 ✓

4813.64 A.C.L.
Total to here 4807.63
7/9/30
Total to here 5022.61
A.C.L.

L.C.

F

R.C.

Ar.
End Area End Area C.V.

46 +83.19 294.8 300.8

 $\frac{6.0}{2.4}$

6.0

 $\frac{6.0}{2.4}$

28.98

 $\frac{16.81}{2}$ $\frac{27.78}{2}$ $\frac{17.30}{2}$

47 297.1 302.6

5.5

26.57

 $\frac{12.93}{2}$ $\frac{27.05}{2}$ $\frac{12.95}{2}$

+12.93 298.8 304.5

5.7

27.53

 $\frac{4.07}{2}$ $\frac{28.26}{2}$ $\frac{7.26}{2}$

+17 299.0 305.0

 $\frac{6.0}{2.4}$

6.0

 $\frac{6.0}{2.4}$

28.98

 $\frac{8.0}{2}$ $\frac{32.33}{2}$ $\frac{9.58}{2}$

+25 299.4 306.7

 $\frac{7.3}{2.7}$

7.3

 $\frac{7.3}{2.7}$

35.67

 $\frac{17.9}{2}$ $\frac{36.79}{2}$ $\frac{24.39}{2}$

+42.9 300.3 308.0

 $\frac{7.7}{2.8}$

7.7

 $\frac{7.7}{2.8}$

37.90

 $\frac{17.1}{2}$ $\frac{40.55}{2}$ $\frac{25.68}{2}$

A.C.L.

Ar.
End. Area End. Area C.V.

47+60
299.7
308.3

12.9

L.C.
8.6
3.1

8.6

P.C.
8.6
3.1

73.20

40.55 19.37

+72.9
299.3
307.0

17.1

7.7
2.8

7.7

7.7
2.8

37.90

33.98 22.79

+90
297.3
304.3

12.7

7.0
2.7

7.0

7.0
2.7

34.05

34.59 16.27

48+02.7
295.8
303.0

12.3

7.2
2.7

7.2

7.2
2.7

35.12

32.05 14.60

+15
293.8
299.8

7.0

6.0
2.4

6.0

6.0
2.4

28.98

27.29 7.08

+22
292.7
298.0

13.16

5.3

25.60

23.84 12.59

V.A.C.L.

48+35.16 ✓
290.6 296.0

✓
19.84 ✓

✓
5.4

+55 ✓
288.7 294.7

✓
10.0 ✓

✓
 $\frac{6.0}{2.4}$ 6.0

+65.0 ✓
287.7 294.0

✓
49.6 ✓

✓
 $\frac{6.3}{2.5}$ 6.3

49+14.6 ✓
286.1 292.6

✓
10.4 ✓

✓
 $\frac{6.5}{2.5}$ 6.5

+25 ✓
286.1 292.7

✓
19.6 ✓

✓
 $\frac{6.0}{2.4}$ 6.0

+44.6 ✓
286.1 289.3

✓
5.4 ✓

✓
3.2

End Area ^{Av} End Area C.V.

26.08 ✓

27.53 ✓ 20.23 ✓

28.98 ✓

29.72 ✓ 11.00 ✓

30.45 ✓

30.95 ✓ 56.86 ✓

31.15 ✓

30.22 ✓ 11.64 ✓
~~28.22~~ ~~9.71~~

28.98 ✓

22.22 ✓ 16.13 ✓

15.46 ✓

22.22 ✓ 4.44 ✓

✓ P.L.L.

			L.C.	Σ
49+50	286.5 ✓	292.5		6.0
			24.5 ✓	
+74.5	288.3 ✓	293.8		5.5
			17.5 ✓	
+92	290.9 ✓	295.3		4.4
			12.2 ✓	
50+04.2	292.7 ✓	298.0		5.3
			29.3 ✓	
+33.5	299.2 ✓	305.2	$\frac{6.0}{2.4}$	6.0
			16.5 ✓	
+50	303.5 ✓	310.6	$\frac{7.1}{2.7}$	7.1
			6.0 ✓	

End Area	^{AV} End Area	C.V.
28.98 ✓		
27.78 ✓		25.21 ✓
26.57 ✓		
23.91 ✓		15.50 ✓
21.25 ✓		
23.73 ✓		10.59 ✓
25.60 ✓		
27.29 ✓		29.61 ✓
28.98 ✓		
31.79 ✓		19.43 ✓
34.59 ✓		
37.69 ✓		8.38 ✓
V.A.C.L.		

50 + 56

304.6 312.8

$\frac{8.2}{3.0}$

8.2

$\frac{8.2}{3.0}$

40.79

11.0

41.39 16.86

+ 67

306.6 315.0

$\frac{8.4}{3.0}$

8.4

$\frac{8.4}{3.0}$

41.99

18.0

38.49 23.66

+ 85

309.8 315.8

$\frac{6.0}{2.4}$

6.0

$\frac{6.0}{2.4}$

28.98

15.0

27.29 15.16

51 + 00

312.5 317.8

5.3

25.60

15.0

27.29 15.16

+ 15

315.2 321.2

$\frac{6.0}{2.4}$

6.0

$\frac{6.0}{2.4}$

28.98

10.0

30.99 11.48

+ 25

317.0 323.8

$\frac{6.8}{2.6}$

6.8

$\frac{6.8}{2.6}$

33.00

17.0

30.99 19.57

of A.C.L.

End Area ^{Av.} End Area C.V.

			L.C.	±	P.C.	End Area	End Area ^{Av}	C.V.
51 +42	✓ 320.4	✓ 326.4	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	✓ 28.98	✓ 26.81	✓ 7.94
+50	✓ 322.0	✓ 327.1	✓ 8.0	✓ 5.1	✓ 27.63	✓ 26.81	✓ 9.93	
+60	✓ 324.0	✓ 330.0	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	✓ 28.98	✓ 30.48	✓ 33.81
+90	✓ 330.0	✓ 336.6	✓ $\frac{6.0}{2.5}$	✓ 6.6	✓ $\frac{7.0}{2.7}$	✓ 31.98	✓ 34.73	✓ 12.86
52+00	✓ 332.0	✓ 339.7	✓ $\frac{7.0}{2.7}$	✓ 7.7	✓ $\frac{8.1}{2.9}$	✓ 37.48	✓ 38.34	✓ 14.20
+110	✓ 334.8	✓ 342.7	✓ $\frac{7.3}{2.7}$	✓ 7.9	✓ $\frac{8.6}{3.1}$	✓ 39.19	✓ 39.70	✓ 26.47
							✓ 39.74	✓ 26.49
						✓ A.C.L.		

52+28

339.8

348.0

$$\frac{7.4}{2.8}$$

8.2

$$\frac{8.6}{3.1}$$

$$\frac{40.20}{70.29}$$

$$\frac{\text{Av. End Area}}{\text{End Area C.V.}}$$

10.0

$$\frac{35.08}{35.12}$$

$$\frac{12.99}{13.07}$$

+38

342.6

348.8

$$\frac{6.2}{2.5}$$

6.2

$$\frac{6.2}{2.5}$$

29.95

17.0

$$\frac{29.77}{29.77}$$

$$\frac{13.10}{13.10}$$

+50

346.0

352.0

$$\frac{6.0}{2.4}$$

6.0

$$\frac{6.0}{2.4}$$

28.98

40.0

$$\frac{31.12}{31.12}$$

$$\frac{16.10}{16.10}$$

+90

357.2

364.1

$$\frac{6.0}{2.4}$$

6.9

$$\frac{7.6}{2.8}$$

33.25

10.0

$$\frac{31.12}{31.12}$$

$$\frac{11.53}{11.53}$$

53+00

360.0

366.0

$$\frac{6.0}{2.4}$$

6.0

$$\frac{6.0}{2.4}$$

28.98

5.0

$$\frac{28.81}{28.81}$$

$$\frac{7.96}{7.96}$$

+05

361.2

366.3

5.1

24.03

26.12

$$\frac{24.03}{24.03}$$

$$\frac{23.83}{23.83}$$

L.C.

±

R.C.

53+31.12 ✓
367.5 ✓
372.6✓
6.88^o✓
5.1Av.
End Area End Area C.V.21.63^o+38 ✓
369.0 ✓
375.0✓
8.0^o✓
 $\frac{6.0}{2.4}$ ✓
6.0✓
 $\frac{6.0}{2.4}$ 28.98^o26.81^o ✓
6.83^o ✓+46 ✓
370.6 ✓
378.6✓
14.49^o✓
 $\frac{7.0}{2.7}$ ✓
8.0✓
 $\frac{8.4}{3.0}$ 38.75^o
~~38.975~~33.87 ✓
~~33.98~~ 10.04 ✓
~~10.07~~+60.49 ✓
373.6 ✓
380.9✓
14.51^o✓
 $\frac{6.7}{2.6}$ ✓
7.3✓
 $\frac{8.1}{2.9}$ 35.93^o ✓37.34 ✓
~~37.45~~ 20.04 ✓
20.10+75 ✓
375.8 ✓
381.8✓
15.12^o✓
 $\frac{6.0}{2.4}$ ✓
6.0✓
 $\frac{6.0}{2.4}$ 28.98^o ✓32.46^o ✓
17.44^o ✓+90.2 ✓
378.0 ✓
383.1✓
29.8^o✓
5.121.63^o ✓26.81^o ✓
15.09^o ✓25.12^o ✓
27.73^o ✓

%A.C.L.

L.C.

E

R.C.

49

54+20.0 ✓
380.7 ✓ 386.0✓
10.0°✓
5.3+30 ✓
381.3 ✓ 387.3✓
20.0°✓
6.0+50 ✓
382.5 ✓ 389.0✓
25.0°✓
5.5+75 ✓
384.0 ✓ 389.9✓
15.0°✓
4.9+90 ✓
384.0 ✓ 389.0✓
10.0°✓
5.055+00 ✓
384.0 ✓ 390.0✓
20.0°✓
6.0End. Area ^{Av.} End. Area C.V.

25.60 ✓

27.29 ✓ 10.11 ✓

28.98 ✓

27.78 ✓ 20.58 ✓

26.57 ✓

25.12 ✓ 23.26 ✓

23.67 ✓

23.91 ✓ 13.28 ✓

24.15 ✓

26.57 ✓ 9.84 ✓

28.98 ✓

27.53 ✓ 20.39 ✓

V.A.L.L.

55+20 ✓
384.0 389.4

✓
30.0

L.G. E
✓
5.4

End Area ^{Av} End Area C.V.
26.08 ✓

26.08 ✓ 28.98 ✓

+50 ✓
384.1 389.5

✓
50.0

✓
5.4

26.08 ✓

25.12 ✓ 16.52 ✓

56+00 ✓
384.2 389.2

✓
30.0

✓
5.0

27.15 ✓

27.15 ✓ 26.83 ✓

+30 ✓
384.2 389.2

✓
10.0

✓
5.0

27.15 ✓

26.57 ✓ 9.84 ✓

+40 ✓
384.2 390.2

✓
10.0

✓
 $\frac{6.0}{2.4}$ 6.0

✓
 $\frac{6.0}{2.4}$

28.98 ✓

30.87 ✓ 11.43 ✓

+50 ✓
384.2 391.0

✓
15.0

✓
 $\frac{6.0}{2.4}$ 6.8

✓
 $\frac{7.4}{2.8}$

32.75 ✓

30.87 ✓ 17.15 ✓

✓
A.C.L.

✓
5884.51 A.C.L.
Total to here 5870.28
7/9/30
Total to here
6093.48 A.C.L.

L.C.

±

P.C.

56+65 ✓
383.9 ✓ 389.9 $\frac{6.0}{2.4}$

6.0 ✓

 $\frac{6.0}{2.4}$

28.98 ✓

10.0 ✓

27.78 ✓ 10.29 ✓

+75 ✓
383.7 ✓ 389.2

5.5 ✓

26.57 ✓

10.0 ✓

27.78 ✓ 10.29 ✓

+85 ✓
383.5 ✓ 389.5

6.0 ✓

28.98 ✓

15.0 ✓

28.98 ✓ 16.10 ✓

57+00 ✓
383.2 ✓ 389.2

6.0 ✓

28.98 ✓

25.0 ✓

27.78 ✓ 25.72 ✓

+25 ✓
382.7 ✓ 388.2

5.5 ✓

26.57 ✓

25.0 ✓

26.57 ✓ 24.60 ✓

+50 ✓
382.2 ✓ 389.7

5.5 ✓

26.57 ✓

25.0 ✓

27.78 ✓ 25.72 ✓

P.C.L.

57+75

381.6 ✓

387.6

25.0 ✓

6.0 ✓

28.98 ✓

Av. End Area End Area C.V.

28.02 ✓ 25.94 ✓

58+00

381.1 ✓

386.7

50.0 ✓

5.6 ✓

27.05 ✓

26.57 ✓ 19.20 ✓

+50

380.0 ✓

385.4

19.9 ✓

5.4 ✓

26.08 ✓

26.08 ✓ 19.22 ✓

+69.9

379.6 ✓

385.0

18.1 ✓

5.4 ✓

26.08 ✓

27.53 ✓ 18.76 ✓

+88

378.5 ✓

384.5

6.0 ✓
2.4

6.0 ✓

6.0 ✓
2.4

28.98 ✓

11.1 ✓

31.79 ✓ 13.07 ✓

+99.9

377.8 ✓

384.9

6.8 ✓
2.6

7.1 ✓

7.4 ✓
2.8

34.60 ✓

15.1 ✓

40.63 ✓
40.60 22.71 ✓

V.A.L.L.

			L.C.	±
59+15	375.6 ✓	384.9	$\frac{8.5}{3.0}$ ✓	9.3 ✓
			14.6 ✓	
+29.6	373.7 ✓	381.9	$\frac{7.7}{2.8}$ ✓	8.2 ✓
			10.4 ✓	
+40	371.8 ✓	377.8	$\frac{6.0}{2.4}$ ✓	6.0 ✓
			10.0 ✓	
+50	370.0 ✓	375.0		5.0 ✓
			15.0 ✓	
+65	363.1 ✓	369.1	$\frac{6.0}{2.4}$ ✓	6.0 ✓
			35.0 ✓	
60+00	346.9 ✓	353.9	$\frac{7.0}{2.7}$ ✓	7.0 ✓
			15.0 ✓	

	End Area	Av. End Area	C.V.
	46.65 ✓	15.60 ✓	
	43.80 ✓	13.75 ✓	23.68 ✓
			23.66 ✓
	40.99 ✓	10.90 ✓	
	34.96 ✓	31.91 ✓	13.47 ✓
			13.46 ✓
	28.98 ✓		
	26.57 ✓	9.84 ✓	
	24.15 ✓		
	26.57 ✓	14.76 ✓	
	28.98 ✓		
	31.52 ✓	40.86 ✓	
	34.05 ✓		
	36.55 ✓	20.31 ✓	
	V.A.C.L		

L.C.

Σ

60+15.0 ✓
340.0 ✓
347.9

✓
 $\frac{7.9}{2.9}$

✓
7.9

✓
5.0²

+26 ✓
340.0 ✓
346.0

✓
 $\frac{6.0}{2.4}$

✓
6.0

✓
19.2²

+39.2 ✓
340.0 ✓
340.0

✓
0.0

✓
29.5²

+68.7 ✓
340.0 ✓
340.0

✓
0.0

✓
8.9²

+77.6 ✓
340.0 ✓
343.8

✓
3.8

✓
22.4²

61+00 ✓
347.4 ✓
351.9

✓
4.5

✓
20.0²

P.C.

54

End Area ^{Av} End Area C.V.

✓
 $\frac{7.9}{2.9}$

✓
37.05²

✓
37.02² ✓
6.30²

✓
 $\frac{6.0}{2.4}$

✓
28.98²

✓
14.19² ✓
10.30²

✓
0.0²

✓
0.0² ✓
0.0²

✓
0.0²

✓
9.18² ✓
3.03²

✓
18.35²

✓
20.05² ✓
16.63²

✓
21.74²

✓
A.C.L. 25.36² ✓
18.79²

61+20	354.1 ✓	360.1	15.7 ✓	6.0 ✓
+35.7	359.3 ✓	364.0	23.3 ✓	4.7 ✓
+59	365.4 ✓	371.4	5.8 ✓	6.0 ✓
+64.8	366.9 ✓	372.9	18.2 ✓	6.0 ✓
+83	370.5 ✓	375.5	17.0 ✓	5.0 ✓
62	373.9 ✓	379.9	18.16 ✓	6.0 ✓
			$\frac{6.0}{2.4}$	

End Area	Av. End Area	C.Y.
28.98 ✓		
23.84 ✓	15.03 ✓	
22.70 ✓		
28.98 ✓	22.30 ✓	
28.98 ✓	6.23 ✓	
28.98 ✓		
26.57 ✓	17.91 ✓	
24.16 ✓		
26.57 ✓	16.73 ✓	
28.98 ✓		
✓A.C.L.	33.08 ✓	22.25 ✓
	33.07	23.24

L.C. E

R.G.

62+18.16 377.5 385.2

 $\frac{7.2}{2.7}$

7.7

 $\frac{7.7}{2.8}$ End Area ^{Av.} End Area C.Y.

37.19

37.15

33.08

33.07

26.72

26.75

+40 381.0 387.0

 $\frac{6.0}{2.4}$

6.0

 $\frac{6.0}{2.4}$

28.98

33.08

33.07

26.72

26.75

21.84

7.8

28.02

8.09

+47.8 382.2 387.8

5.6

27.05

17.2

26.81

17.08

+65 383.8 389.3

5.5

26.57

12.7

26.85

12.16

+77.7 385.0 390.2

5.2

26.12

30.0

26.33

29.26

63+07.7 385.8 391.5

5.7

27.33

15.3

A.C.L.

28.26

16.01

63+23 385.7 391.7

9.0²

$\frac{6.0}{2.4}$

6.0

$\frac{6.0}{2.4}$

End Area ^{Ar.} End Area C.V.

28.98⁹

31.79⁹ 10.60⁹

+32 385.7 392.8

18.0²

$\frac{6.8}{2.6}$

7.1

$\frac{7.4}{2.8}$

34.60⁹

33.80⁹ 22.53⁹

+50 385.6 392.4

45.2²

$\frac{6.4}{2.5}$

6.8

$\frac{7.2}{2.7}$

32.99⁹

30.99⁹ 51.88⁹

+95.2 385.4 391.4

8.8²

$\frac{5.6}{2.4}$

6.0

$\frac{6.4}{2.5}$

28.98⁹

32.05⁹ 10.45⁹

64+04 384.7 391.9

26.0²

$\frac{6.8}{2.6}$

7.2

$\frac{7.6}{2.8}$

35.11⁹

34.65⁹ 33.37⁹

+30 382.6 389.5

25.0²

$\frac{6.7}{2.6}$

6.9

$\frac{7.6}{2.8}$

34.15⁹

V.A.C.L. 32.15⁹ 29.77⁹

			L.C.	£	P.C.	End Area	Av. End Area	C.V.
64+55	380.6	387.2	$\frac{6.3}{2.5}$	6.6	$\frac{7.0}{2.7}$	32.12		
		29.8				33.23	36.68	
+84.8	377.2	384.2	$\frac{6.6}{2.6}$	7.0	$\frac{7.6}{2.8}$	34.33		
		15.2				32.90	18.52	
65+00	374.2	380.7	$\frac{6.0}{2.4}$	6.5	$\frac{7.0}{2.7}$	31.16		
		7.0				30.22	7.83	
+07	372.9	378.9	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98		
		7.2				27.53	7.34	
+14.2	371.6	377.0		5.4		26.08		
		29.1				26.08	28.11	
+43.3	364.0	369.4		5.4		26.08		
		42.3				P.C.L.	27.53	43.13

L.C.

±

R.C.

End Area ^{Ar} End Area C.V.

65+85.6	✓ 351.3	357.3	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	28.98 ✓	32.87 ✓	34.45 ✓
		28.3 ✓						
66+13.9	✓ 341.3	348.9	✓ $\frac{7.2}{2.7}$	✓ 7.6	✓ $\frac{7.6}{2.8}$	36.76 ✓	37.61 ✓	21.03 ✓
		15.1 ✓						
+29	✓ 335.1	342.9	✓ $\frac{7.6}{2.8}$	✓ 7.8	✓ $\frac{8.0}{2.9}$	38.45 ✓	33.72 ✓	12.19 ✓
		10.0 ✓						
+39	✓ 321.0	337.0	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	28.98 ✓	25.60 ✓	13.27 ✓
		14.0 ✓						
+53	✓ 325.2	329.8		✓ 4.6		22.22 ✓	25.60 ✓	16.12 ✓
		17.0 ✓						
+70	✓ 318.2	324.2	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	28.98 ✓	33.22 ✓	18.46 ✓
		15.0 ✓				✓ A.C.L.	33.21 ✓	18.45 ✓

			L.C.	£	R.C.	End Area	Ar. End Area	C.Y.
66+85	✓ 312.0	319.6	✓ $\frac{6.8}{2.6}$	✓ 7.6	✓ $\frac{8.5}{3.0}$	✓ 37.47 37.13	✓ 33.22 33.21	✓ 9.84
			✓ 8.0					
+93	✓ 312.0	318.0	✓ $\frac{6.0}{2.4}$	✓ 6.0	✓ $\frac{6.0}{2.4}$	✓ 28.98		
			✓ 32.0				✓ 18.60	✓ 22.04
67+25	✓ 312.0	313.7		✓ 1.7		✓ 8.21		
			✓ 16.7				✓ 1.11	✓ 2.57
+41.7	✓ 312.0	312.0		✓ 0.0		✓ 0.0		
			✓ 22.7				✓ 0.0	✓ 0.0
+64.4	✓ 312.0	312.0		✓ 0.0		✓ 0.0		
			✓ 5.6				✓ 1.35	✓ 9.02
+70	✓ 312.0	313.8		✓ 1.8		✓ 8.62		
			✓ 10.0				✓ 16.18	✓ 5.99

✓A.C.L.

Total to here: 6999.07 A.C.L.
 6993.06
 M.H.D. 8
 7/9/30
 Total to here
 7208.04 A.C.L.

			L.C.	±	P.C.	End Area	End Area ^{Av.}	C.Y.
67+80	316.4	321.3		4.9		23.67		
			20.0 ²				22.46	16.67
68+00	325.3	329.7		4.4		21.25		
			16.0 ²				25.12	17.89
+16	332.3	338.3		6.0		28.98		
			$\frac{6.0}{2.4}$				30.93	11.46
			10.0 ²					
+26	336.8	343.6		6.8		32.87		
			$\frac{6.9}{2.6}$				36.68	16.30
			12.0 ²					
+38	342.0	350.1		8.1		40.48		
			$\frac{8.5}{3.0}$				37.20	31.97
			23.2 ²					
+61.2	352.3	359.2		6.9		33.91		
			$\frac{7.5}{2.8}$				33.94	
			13.8 ²					
							31.09	16.08
							31.46	

A.C.L.

			L.C.	±	P.C.	End Area	Ar. End Area	C.Y.
68+75	357.2	363.2	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98	25.36	13.62
			16.5					
+89.5	362.4	366.9		4.5		21.74		
			35.5				23.43	30.81
69+25	372.4	377.6		5.2		25.12		
			28.6				22.22	23.54
+53.6	380.4	384.4		4.0		19.32		
			16.4				24.15	14.67
+70	382.7	388.7	$\frac{6.0}{2.4}$	6.0	$\frac{6.0}{2.4}$	28.98		
			15.0				30.22	10.79
+85	384.8	391.3	$\frac{6.5}{2.5}$	6.5	$\frac{6.5}{2.5}$	31.45		
			19.7				30.22	22.05

V.H.C.L.

			L.C.	£	R.C.	End Area	Av. End Area	C.V.
70+04.7	387.6 ✓	393.6	$\frac{6.0}{2.4}$ ✓	6.0 ✓	$\frac{6.0}{2.4}$ ✓	28.98 ✓		
		15.3 ✓				31.79 ✓	18.01 ✓	
+20	388.2 ✓	395.3	$\frac{7.1}{2.7}$ ✓	7.1 ✓	$\frac{7.1}{2.7}$ ✓	31.59 ✓		
		14.7 ✓				33.80 ✓	18.10 ✓	
+34.7	388.7 ✓	395.5	$\frac{6.8}{2.6}$ ✓	6.8 ✓	$\frac{6.8}{2.6}$ ✓	33.00 ✓		
		15.3 ✓				33.80 ✓	19.15 ✓	
+50	388.1 ✓	395.2	$\frac{7.1}{2.7}$ ✓	7.1 ✓	$\frac{7.1}{2.7}$ ✓	34.59 ✓		
		14.7 ✓				32.52 ✓	17.71 ✓	
+64.7	387.6 ✓	393.9	$\frac{6.3}{2.5}$ ✓	6.3 ✓	$\frac{6.3}{2.5}$ ✓	30.15 ✓		
		10.3 ✓				30.15 ✓	11.62 ✓	
+75	385.7 ✓	392.0	$\frac{6.3}{2.5}$ ✓	6.3 ✓	$\frac{6.3}{2.5}$ ✓	30.15 ✓		
		19.2 ✓				29.72 ✓	21.13 ✓	

✓ A.C.L.

Clear + Warm - Feb. 4. 1930
 Converse - Notes
 Hill - Grades
 Elliott - " "
 Walton
 Simpson

End Area

70 + 94.2 ✓
 382.1 ✓ 388.1

15.8 °

✓
 $\frac{6.0}{2.4}$ ✓ 6.0 ✓

✓
 $\frac{6.0}{2.4}$ ✓ 28.98 ✓

71 + 10 ✓
 374.2 ✓ 382.4

18.0 °

✓
 $\frac{8.2}{2.96}$ ✓ 8.2 ✓

✓
 $\frac{8.2}{2.96}$ ✓ 40.79 ✓

+28 ✓
 365.1 ✓ 372.3

22.0 °

✓
 $\frac{7.2}{2.71}$ ✓ 7.2 ✓

✓
 $\frac{7.2}{2.71}$ ✓ 35.12 ✓

+50 ✓
 354.1 ✓ 363.3

14.0 °

✓
 $\frac{9.2}{3.21}$ ✓ 9.2 ✓

✓
 $\frac{9.2}{3.21}$ ✓ 46.96 ✓

+64 ✓
 347.0 ✓ 355.9

16.0 °

✓
 $\frac{8.9}{3.14}$ ✓ 8.9 ✓

✓
 $\frac{8.9}{3.14}$ ✓ 45.07 ✓

+80 ✓
 339.0 ✓ 347.0

16.8 °

✓
 $\frac{8.0}{2.91}$ ✓ 8.0 ✓

✓
 $\frac{8.0}{2.91}$ ✓ 39.62 ✓

34.89 ✓ 20.42 ✓

37.96 ✓ 25.31 ✓

41.04 ✓ 33.44 ✓

46.02 ✓ 23.86 ✓

42.35 ✓ 25.10 ✓

19.81 ✓ 12.33 ✓

✓ A.C.L.

calc. by
 W.H.S.

71+96.8 339.0[✓] 339.0

0.0[✓]

0.0[✓]

43.0[✓]

0.00[✓]

0.00[✓]

72+39.8 339.0[✓] 339.0

0.0[✓]

0.0

15.2[✓]

12.80[✓]

7.21[✓]

+55 339.0[✓] 344.3

5.3[✓]

25.60[✓]

26.0[✓]

28.77[✓]

27.70[✓]

+81 344.7[✓] 351.2

$\frac{5.4}{2.41}$ [✓]

6.5[✓]

$\frac{8.0}{2.91}$ [✓]

31.94[✓]

12.0[✓]

26.60[✓]

11.82[✓]

+93 347.4[✓] 351.8

$\frac{4.4}{2.41}$ [✓]

4.4[✓]

$\frac{4.4}{2.41}$ [✓]

21.25[✓]

7.0[✓]

31.07

8.06[✓]

73 349.0[✓] 357.7

$\frac{6.8}{2.61}$ [✓]

8.7[✓]

$\frac{8.2}{3.09}$ [✓]

40.89[✓]
46.76[✓]

34.01

~~8.82~~

130[✓]

36.69[✓]

17.67[✓]

V.A.C.L.

39.12

~~18.83~~

72.46

Calc. by
W.M.S.

73+13

351.8 ✓

358.4

 $\frac{6.4}{2.51}$ ✓

6.6 ✓

12.0 ✓

+25

354.5 ✓

361.3

 $\frac{6.8}{2.61}$ ✓

6.8 ✓

10.0 ✓

+35

357.5 ✓

363.2

 $\frac{5.7}{2.41}$ ✓

5.7 ✓

15.0 ✓

+50

362.0 ✓

368.8

 $\frac{6.8}{2.61}$ ✓

6.8 ✓

12.0 ✓

+67

365.6 ✓

373.6

 $\frac{8.0}{2.91}$ ✓

8.0 ✓

18.0 ✓

~~told from here see page 77~~

+80

371.0

377.8

 $\frac{6.8}{2.61}$ ✓

6.8 ✓

12.1 ✓

 $\frac{7.2}{2.71}$ ✓

32.49 ✓

31.47

32.74 ✓

32.24

14.55 ✓

14.33

 $\frac{6.8}{2.61}$ ✓

33.00 ✓

 $\frac{5.7}{2.41}$ ✓

27.53 ✓

30.27 ✓

11.21 ✓

 $\frac{6.8}{2.61}$ ✓

33.00 ✓

30.27 ✓

16.82 ✓

 $\frac{8.0}{2.91}$ ✓

39.62 ✓

36.31 ✓

16.14 ✓

 $\frac{6.8}{2.61}$ ✓

33.00 ✓

36.31 ✓

24.21 ✓

✓ A.C.L.

30.51 ✓

13.67 ✓

96.60 ✓

Calc. by
W.H.S.

Sta	Grade	Elev	Dist	Lft. Cut	Rt. Cut
73	+92.1	374.6	380.4	5.8 2.41	5.8 2.41

Standard trench 377.1 ✓ 382.7
74+00 382.2 388.2

Continued on page 75 this book.

May 28, 1930

Elliott & Notes
Jacobsen &
Bailey Tape

12' trench Vertical cuts. (Notes: all cuts

29.4

Begin 12' trench.
74+50 387.7 393.4

29.9

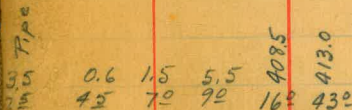
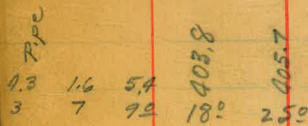
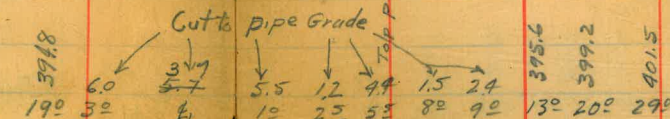
74
75+80 391.1 392.5

75+10 392.3 392.7

40.0

Lt.

Rt.



✓ A.C.L.

27.17
28.50

8.39
30.72

26.32
28.98

Total to here 765.81
m. D.S. 10/1/30
7883.12

checked my figures
here
7/9/30
A.C.L.

Calc. By
W.H.S.

67

A.C.L.
10/1/30

7883.12

765.81

7/9/30

shown are to A.P.S.D 2nd N. 10' grade)

Additional sections
taken out from 3' on the left
and 9' on the right July 2, 1930
Elliott
Soper
Bailey

Station	4	392.5	393.4	420.2	418.3	415.0	414.8	49	13	0.9	3.7	Pipe
75+50 ⁹	4	392.5	393.4	40° 24'	18° 12'	30	15	2.5				
				49.6								
76+00	4	392.5	395.3	422.4	418.2	416.7	7.0	3.7	2.8	3.5	Top pipe	
				48° 34'	15° 30'	15						
76+07	4	392.5	396.0	421.5	412.0	405.0	6.0	3.7	3.4	2.5	Pipe	
				50° 22'	7° 30'	15						
76+15	4	392.5	396.6	421.5	417.2	416.5	5.0		4.1	3.6	Pipe	
				50° 40'	15° 30'							
				10.								
76+25	4	392.5	394.3	421.7	417.9	417.0	417.0	3.7	1.8	3.4	Pipe	
				48° 39'	22° 16'	32						
				25.								
76+50	4	392.5	394.1	421.8	417.1	416.7	6.9	1.8	1.6	3.5	Pipe	
				32° 23'	15° 30'	12						
				50								
77+00	4	392.5	395.2	417.2	413.0	410.4	7.9	6.5	3.0	2.7	Pipe	
				32° 20'	8° 30'	15	12					
				14.9								

Station	3.8	6.9	416.0	417.7	419.6	421.5
	72	92	20°	27°	30°	50
			R.I.			
			418.9	421.0	420.7	
	40	8.1	22°	32°	50°	
	62	92				
			412.0	416.4	421.8	
	39	7.5	20°	46°	60°	
	62	92				
			419.1	421.0	421.8	
	3.8	7.0	22°	33°	50	
	62	92				
			418.9	421.5	422.2	
	3.0	5.0	7.4	22°	30°	50°
	4	8	92			
			417.4	420.0	422.8	
	2.7	3.1	8.3	20°	30°	60°
	52	62	92			
			403.5	408.7	409.3	
	2.3	2.8	10.1	15°	19°	30°
	52	62	92			

				LT	Pipe	RT		
77+142	⁴ 392.5	393.0	413.0	409.1	7.2 6.4 0.5	1.2 1.5 4.5 7.2	404.2	403.2
			372 120	30 15	4 25	45 60 65 90	150	310
			15.					
77+292	³ 391.9	393.5	409.4		6.6 4.8 1.6	1.0 1.2 5.5 5.9	399.4	399.7
			240	30 15	4 35	50 65 75 90	150	220
			14.9					
Vertical cut, 77+448	¹ 390.2	394.1	405.7	405.0	8.0 6.7 3.9 2.4 5.7	2.5 2.8 4.7	376.5	397.2
			27	150 30 15	4 20 45	60 75 90	150	230
			14.7					
Standard trench 77+595	387.4	392.4	403.4	397.0	8.8 8.5 5.0 5.0	387.1	392.8	
			180	70 31.6 10	4 2.91 12.	140 190		
			13.7					
77+832	381.9	388.1			8.0 6.2	5.0		
					2.91 4	2.41		

Continued in Book #286 page 2

399.14 - B.M. #19

11.76 410.90

New Pipe
Grade75+03⁰⁶ 393.92 $\frac{15^2}{12^2}$

10.35

421.25

T.P.

0.00

410.90

75+18¹¹ 394.49 $\frac{16^8}{12^2}$

75+50 394.50

 $\frac{10^4}{13^6}$

76+00 394.50

 $\frac{20^8}{13^2}$ 76+09⁰ 394.50 $\frac{12^4}{11^6}$ 76+18⁰ 394.50 $\frac{17^6}{12^2}$

76+50 394.50

 $\frac{22^0}{14^2}$

77+00

 $\frac{17^2}{12^2}$

Aug 19, 1930

Elliott
Soper
Barley

Lt.

74+67⁴⁰ 367.2

(Standard Trench)
74+00⁴⁴ 377.1

Pay for Yds Moved
(10' bottom 6' vert. + 1/4 to 1)
74+29⁴⁷ 384.7

74+49² 387.4

74+58⁹⁷ 390.13

74+66⁹⁸ 391.0

7.6 8.0 8.4
2.81 3.01

S.I. S.I.
5.0 5.3 5.6 5.3 3.6
5.0 2.41 2.41 7.0

S.I.
9.3 9.3 5.0 4.5 6.3 5.3 0.0
20 14. 5.0 4.0 5.0 5.0

S.I.
8.5 7.6 6.6 6.0 5.6 0.0
25 14. 5.2 2.0 6.0

Slope Indicators
12.7 10.0 9.2 5.2 3.6 0.3 0.0
25 14 7.3 3.0 5.0 6.7

S.I.
14.7 14.5 11.5 9.0 6.5 0.9 0.0
20 18. 13. 5.8 5.5 6.5

9/22/30

Simpson
Sober
Remmer

71

Final Cross sections

Lt. cut $\frac{1}{2}$ Rt. cut

$\frac{8^0}{10^0}$ $\frac{2^9}{9^5}$ $\frac{0^0}{7^0}$ $\frac{0^0}{2^5}$ $\frac{0^0}{5^0}$ $\frac{3^0}{7^0}$

Crossed

$\frac{5^8}{10^0}$ $\frac{0^0}{8^5}$ $\frac{0^0}{2^5}$ $\frac{1^0}{5^0}$ $\frac{1^0}{8^0}$

$\frac{12^5}{19^5}$ $\frac{3^3}{14^0}$ $\frac{2^5}{8^5}$ $\frac{0^0}{3^2}$ $\frac{0^0}{2^5}$ $\frac{1^0}{4^5}$ $\frac{2^0}{6^5}$

$\frac{15^2}{18^5}$ $\frac{2^4}{12^0}$ $\frac{2^0}{7^0}$ $\frac{0^0}{3^0}$ $\frac{0^0}{3^0}$ $\frac{1^0}{4^5}$ $\frac{2^0}{6^5}$

9/22/30

72

Lit.

Q R1

Final Cross sections

74+73 391.7 ✓

14.7 15.1 12.0
20. 12. 10.

S.I.
9.8 9.6 7.2 0.0 0.0
6.0 2. 5.0 6.3

4. cut R R1 cut
 $\frac{14.7}{16.5}$ $\frac{18}{12.5}$ $\frac{0.0}{3.5}$ $\frac{0}{4}$ $\frac{2}{6.5}$

+83 392.8 ✓

S.I.
9.8 7.6 5.7 3.2 0.0 0.0
20. 5.4 3.0 5.0 6.0

$\frac{9.0}{12.5}$ $\frac{0.0}{12.0}$ $\frac{0.0}{3.0}$ $\frac{1.0}{6.0}$

+88 393.4 ✓

S.I.
11.5 9.6 6.0 2.5 0.0
20 5.9 3.5 4.5

$\frac{10.3}{12.5}$ $\frac{1.0}{12.0}$ $\frac{0.0}{7.0}$ $\frac{0.0}{5.0}$ $\frac{0.0}{5.5}$

75+00 393.8 ✓

15.5 16.0 14.8
30. 20. 12.

S.I.
14.8 14.7 8.2 3.0 0.0 0.0
7.2 5. 4. 2.5 3.7 5.7

$\frac{15.6}{13.5}$ $\frac{2.0}{13.0}$ $\frac{0.0}{7.5}$ $\frac{0.0}{5.0}$ $\frac{0.0}{5.5}$

6
Fine graded

75+18 394.5

19.6 19.4 19.4
30. 20. 18.

S.I.
17.1 16.7 15.0 7.6 2.4 0.0
10. 7.8 5.5 2.5 4.0

$\frac{19.6}{15.5}$ $\frac{2.0}{15.5}$ $\frac{1.8}{9.5}$ $\frac{0.0}{6.0}$ $\frac{0.0}{5.5}$

75+50 394.5

25.6 23.7 23.0 20.6
30. 20. 16. 12.

S.I.
20.6 18.7 7.4 0.0
8.6 6.0 4.0

$\frac{21.7}{14.5}$ $\frac{2.0}{14.5}$ $\frac{1.7}{10.0}$ $\frac{0.0}{4.0}$ $\frac{0.0}{3.5}$ $\frac{1.0}{7.0}$

~~75+88 394.5~~

$\frac{23.5}{15.5}$ $\frac{3.8}{15.5}$ $\frac{2.9}{10.0}$ $\frac{1.3}{8.5}$ $\frac{0.0}{2.5}$ $\frac{0.0}{3.5}$ $\frac{1.0}{5.0}$

9/24/30

73

Final Cross sections

76+00 394.5

Slope Intersection

23.7	22.2	22.1	20.9	8.4	7.3	1.3	0.8
30.	20.	9.	8.7		1.5	3.0	5.5

Lft. cut.				Rt. cut.	
$\frac{22^1}{13^0}$	$\frac{3^1}{12^0}$	$\frac{2^6}{6^5}$	$\frac{0^0}{6^0}$	$\frac{0^0}{4^0}$	$\frac{0^0}{6^0}$

+09 394.5

S.I.

17.3	16.3	12.2	10.0	7.5	1.4	0.0
25.	20.	6.6	2.0		3.0	5.5

$\frac{14^2}{11^5}$	$\frac{3^8}{11^5}$	$\frac{2^4}{6^5}$	$\frac{0^0}{5^0}$	$\frac{0^0}{5^0}$	$\frac{1^2}{6^0}$
---------------------	--------------------	-------------------	-------------------	-------------------	-------------------

+18 394.5

S.I.

22.4	22.2	22.0	17.7	15.0	7.3	2.3	1.8	1.8
30.	20.	9.5	7.9	5.0		2.0	5.5	7.0

$\frac{22^3}{11^0}$	$\frac{4^7}{11^0}$	$\frac{2^1}{5^2}$	$\frac{0^0}{4^5}$	$\frac{0^0}{6^0}$
---------------------	--------------------	-------------------	-------------------	-------------------

+50 394.5

S.I.

28.2	25.1	24.0	22.2	22.0	7.6	5.0	0.4	0.0
30.	22.	20.	15.	9.0		2.0	4.0	5.7

$\frac{22^2}{10^5}$	$\frac{3^2}{11^0}$	$\frac{2^1}{6^5}$	$\frac{0^0}{6^0}$	$\frac{0^0}{6^0}$
---------------------	--------------------	-------------------	-------------------	-------------------

76+75 394.5

S.I.

26.2	24.6	21.0	20.4	20.1	8.6	1.2	0.0
30.	20.	15.	8.6	7.5		2.7	5.7

$\frac{20^7}{13^0}$	$\frac{2^5}{13^0}$	$\frac{2^3}{7^0}$	$\frac{0^0}{5^0}$	$\frac{0^0}{6^0}$
---------------------	--------------------	-------------------	-------------------	-------------------

77+06²⁵ 394.5

S.I.

19.7	18.7	16.2	15.7	8.8	5.8	4.2	0.0
25	20	7.6	5.0		1.0	2.0	4.5

$\frac{17^1}{12^0}$	$\frac{2^0}{12^0}$	$\frac{2^2}{8^5}$	$\frac{0^0}{7^5}$	$\frac{0^0}{6^0}$
---------------------	--------------------	-------------------	-------------------	-------------------

77+13 394.2

Slope Intersection

17.5	15.0	8.4	4.4	0.0
20	7.2		3.0	4.0

9/24/30

16 ⁵	3 ⁵	2 ⁰	0 ⁰	0 ⁰
13 ⁵	12 ⁵	8 ²	7 ²	5 ⁵

77+21² 393.9 ✓

S.I.

16.3	15.3	10.4	7.4	4.9	0.0
20.	12.0	6.1		2.0	4.0

15 ³	3 ⁵	2 ⁵	0 ⁰	0 ⁰
15 ⁰	13 ⁵	9 ²	6 ⁵	5 ⁵

77+36¹ 392.2 ✓

S.I.

14.0	13.0	12.2	6.9	5.7	0.9	0.9
20.	15.	6.6		2.5	4.5	5.5

13 ⁰	3 ⁰	2 ⁷	1 ²	0 ⁰	0 ⁰	1 ²	1 ⁰	
15 ⁰	14 ⁵	9 ⁵	9 ²	3 ⁰		2 ⁵	4 ²	6 ⁰

+50² 389.4

S.I.

15.9	14.3	10.6	7.8	7.6	6.7	3.0	3.0
20.	11.5	6.2	2.0		3.0	4.7	5.9

15 ⁸	6 ²	4 ²	4 ⁸	0 ⁰	0 ⁰	3 ⁰	3 ⁹	
17 ⁰	19 ⁰	14 ⁰	9 ⁰	2 ⁵		2 ⁵	3 ⁵	4 ²

77+61 387.1

S.I.

13.9	10.0	8.7	5.7	5.6	4.5
15	6.0		1.0	4.5	6.5

16 ⁷	7 ²	7 ²	2 ⁸	0 ⁰	0 ⁰	4 ³	5 ¹	
20 ²	18 ⁵	10 ²	3 ⁵	3 ²		2 ⁰	3 ⁰	6 ⁰

Standard trench

 77+82.2 381.9

8.0	6 ²	5 ⁰
2.91	0	2.41

X sections thru cut from Sta
 Complete sections taken from originals
 Pay for all dirt moved.
 Continued from page 67

74+00⁰⁰ to 74+83⁰⁰
 in this book page 71 to 74

Standard Trench	Dist	Lit.	Cl.	Rt.	End Area	Ave. Area	Cu. Yds						
74+00 ⁰⁰	29.03	0 ⁰⁰ 2.41	5.3 2.91	5.6 2.41	573.50 ⁰⁰ 241.51	26.32	54.44 58.53						
74+2947	14.73	0 ⁰⁰ 4.9	0 ⁰⁰ 9.5	8 ⁰⁰ 10.	5 ⁰⁰ 5.	4 ⁵⁰ 4.	6 ³⁰ 6.3	53.08 5. 5. 3.5	0 ⁰⁰ 3.5	82.55	80.53	43.93	
74+442	14.77	0 ⁰⁰ 8.5	5 ⁸⁰ 10.	6 ⁶⁰ 5.2	6 ⁰⁰ 6.2	5 ⁶⁰ 2.	1 ³⁰ 5.	0 ⁰⁰ 2.5	0 ⁰⁰ 2.5	78.50	103.29	56.50	
74+5897	8.01	0 ⁰⁰ 3.0	2 ⁵⁰ 8.5	3 ³⁰ 14.	1 ²⁵ 19.5	1 ⁰⁰ 14.	9 ²⁰ 7.3	5 ²⁰ 5.3	3 ⁶⁰ 3.0	12 4.5	128.08	132.07	39.18
74+6698	6.02	0 ⁰⁰ 3.	2 ⁰⁰ 7.	2 ⁵⁰ 12.	1 ⁵⁰ 18.5	1 ⁴⁵ 18.	1 ¹⁵ 13.	9 ⁰⁰ 5.8	6 ⁵⁰ 6.5	1 ²⁰ 4.2	136.05	146.62	32.69
74+73		0 ⁰⁰ 3.5	1 ⁸⁰ 12.5	1 ⁴⁰ 16.5	1 ¹⁰ 12.	1 ²⁰ 10.	9 ⁸⁰ 6.	9 ⁶⁰ 2.	7 ²⁰ 7.2	0 ⁰⁰ 5.0	157.18	133.16	49.32
74+83		0 ⁰⁰ 12.0	9 ⁰⁰ 12.5	7 ⁶⁰ 5.4	5 ⁷⁰ 5.7	3 ²⁰ 3.	0 ⁰⁰ 5.	3 ²⁰ 3.5	0 ⁰⁰ 5.	109.14	115.54	24.82	
74+888		0 ⁰⁰ 7.	1 ²⁰ 12.0	1 ⁰⁰ 12.5	7 ⁶⁰ 5.3	6 ⁰⁰ 6.0	2 ⁵⁰ 3.5	0 ⁰⁰ 4.5	2 ⁵⁰ 3.5	121.94	155.69	64.58	

Comptd. M.D.E.

75+00

0° 2° 15° 14° 14° 14° 8° 3° 0°
7° 13 13° 12. 7.2 5. 2° 32

189.44 ✓

212.69 ✓

148.10 ✓

75+188

0° 18 22 19° 17° 17° 16° 15° 7° 2° 0°
6° 9° 15° 15° 15. 10. 7.8 5.2 2° 40

235.94 ✓

244.81 ✓

282.89 ✓

75+50

0° 17 2° 21 20° 20° 18° 7° 0°
4° 10° 14° 14° 12. 8° 6. 4°

253.68 ✓

233.06 ✓

431.59 ✓

76+00

4° 0° 26 34 22° 22° 20° 8° 7° 13 12 0°
6° 6° 12° 13° 9° 8° 15 3° 5° 4°

212.43 ✓

171.74 ✓

57.25 ✓

76+09

0° 24 38 14° 12° 10° 7° 14 0°
5° 6° 11° 11° 6° 2. 3° 5°

131.04 ✓

148.56 ✓

49.52 ✓

76+18

0° 24 42 22° 22° 17° 15° 7° 23 18 18 0°
4° 5° 11. 11. 9° 7.9 5. 2. 5° 6° 6°

166.08 ✓

172.34 ✓

204.25 ✓

76+50

0° 24 33 22° 22° 7° 5° 0° 0°
6° 6° 11. 10° 9. 2. 4. 5°

178.59 ✓

198.62 ✓

184.21 ✓

183.91 ✓

Computed M. D. E. 11. 57

76+75

0° 23 25 20 20 20 8° 12 00
5. 7. 13. 13. 86 7.5 27 57

(219.31) A.C.L.
218.65 (201.60) (233.33)
201.17 232.84

77+0625

0° 22 28 17 16 15 88 52 42 09
75 85 120 120 75 50 10 20 45

(183.90)
183.68 (182.69) (45.67)
182.59 45.65

77+13

0° 20 35 16 15 84 44 00
70 80 125 135 75 30 40

181.49
170.24 51.70

77+212

0° 25 35 15 15 10 74 49 00
65 9. 13. 15. 12. 61 2. 4.

158.98
162.69 89.78

77+361

0° 11 27 30 13 12 69 57 12 00
30 90 95 145 15. 60 25 4. 25

166.40
176.84 96.93

77+50?

0° 48 48 69 158 143 100 78 70 62 39 38 00
25 90 140 190 190 115 62 2. 30 42 35 25

187.27
168.69 63.10

77+61

0° 28 72 72 162 139 100 82 57 56 45 31 43 00
30 35 100 185 200 150 60 10 45 65 60 30 20

150.10
90.40 74.33

Standard Trench
77+832

0° 60 80 62 50 00
241 241 241 241 241

30.71
2381.40
7645.81
10,027.21
10/19/30
2382.20
7651.82
10,034.02
A.C.L.

Continued in Book 286

Total from 74+00 to 77+832
Comptd. M. D. S.

Otoy Res. to San Diego Second Main Pipe line
Back Fill cross sections

Grade	Lf. cut.	$\frac{1}{2}$	Rt. cut.
74+29 ²⁷	384.7	$\frac{8^{\circ}}{10^{\circ}}$	7 ³ $\frac{7^{\circ}}{1^{\circ}}$ $\frac{3^{\circ}}{8^{\circ}}$ <small>no slope</small>
74+44 ²⁰	387.4	$\frac{7^{\circ}}{10^{\circ}}$	7 ² $\frac{7^{\circ}}{15^{\circ}}$ $\frac{3^{\circ}}{8^{\circ}}$ <small>no slope</small>
74+52 ²⁷	390.13	NG. $\frac{9^{\circ}}{20^{\circ}}$ $\frac{12^{\circ}}{10^{\circ}}$ $\frac{7.5^{\circ}}{10^{\circ}}$	6 ³ $\frac{6^{\circ}}{10^{\circ}}$ $\frac{3^{\circ}}{7^{\circ}}$
74+66 ²⁰	391.0	$\frac{7^{\circ}}{20^{\circ}}$ $\frac{7^{\circ}}{10^{\circ}}$	6 ⁴ $\frac{3^{\circ}}{7^{\circ}}$
74+73	391.7	NG. $\frac{9^{\circ}}{20^{\circ}}$ $\frac{7^{\circ}}{10^{\circ}}$	6 ⁶ $\frac{3^{\circ}}{7^{\circ}}$
74+83	392.8	$\frac{8^{\circ}}{15^{\circ}}$ $\frac{6^{\circ}}{10^{\circ}}$	5 ⁸ $\frac{2^{\circ}}{5^{\circ}}$
74+88 ²	393.4	$\frac{8^{\circ}}{12^{\circ}}$ $\frac{6^{\circ}}{20^{\circ}}$	5 ² $\frac{2^{\circ}}{6^{\circ}}$
75+00	393.8	$\frac{11^{\circ}}{13^{\circ}}$ $\frac{9^{\circ}}{6^{\circ}}$	5 ³ $\frac{16^{\circ}}{6^{\circ}}$
75+18 ^E	394.5	$\frac{14^{\circ}}{15^{\circ}}$	4 ⁹ $\frac{1^{\circ}}{6^{\circ}}$
75+50	394.5	$\frac{14^{\circ}}{14^{\circ}}$	5 ⁵ $\frac{1^{\circ}}{5^{\circ}}$
76+00	394.5	$\frac{15^{\circ}}{13^{\circ}}$	6 ⁰ $\frac{2^{\circ}}{5^{\circ}}$

11/12/30
Simpson
Saber
Rem m 29

Grade	Lf. cut.	$\frac{1}{2}$	Rt. cut.
76+09	394.5	$\frac{18^{\circ}}{15^{\circ}}$	7 ³ $\frac{2^{\circ}}{6^{\circ}}$
76+18	394.5	$\frac{12^{\circ}}{10^{\circ}}$	6 ⁸ $\frac{2^{\circ}}{6^{\circ}}$
76+50	394.5	$\frac{11^{\circ}}{10^{\circ}}$	5 ⁵ $\frac{1^{\circ}}{6^{\circ}}$
76+75	394.5	$\frac{14^{\circ}}{12^{\circ}}$	6 ¹ $\frac{1^{\circ}}{7^{\circ}}$
77+06 ²⁵	394.5	$\frac{12^{\circ}}{12^{\circ}}$	5 ² $\frac{1^{\circ}}{7^{\circ}}$
77+13	394.2	$\frac{12^{\circ}}{13^{\circ}}$	5 ¹ $\frac{2^{\circ}}{5^{\circ}}$
77+21 ²	393.9	$\frac{12^{\circ}}{15^{\circ}}$	5 ⁰ $\frac{1^{\circ}}{6^{\circ}}$
77+36 ⁴	392.2	$\frac{11^{\circ}}{15^{\circ}}$ $\frac{9^{\circ}}{10^{\circ}}$	5 ⁶ $\frac{1^{\circ}}{6^{\circ}}$
77+50 ²	389.4	$\frac{12^{\circ}}{20^{\circ}}$ $\frac{10^{\circ}}{15^{\circ}}$	6 ⁴ $\frac{4^{\circ}}{6^{\circ}}$
77+61	387.1	$\frac{12^{\circ}}{20^{\circ}}$	6 ⁵ $\frac{2^{\circ}}{6^{\circ}}$

Standard trench
77+83³

399.14 = 8 M = 19

4.30	703.74		
		7.30	399.14
5.05	704.19		
		0.51	703.68
12.00	415.68		
	97.5		
	21.2		
	8.5		
	12.7		

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

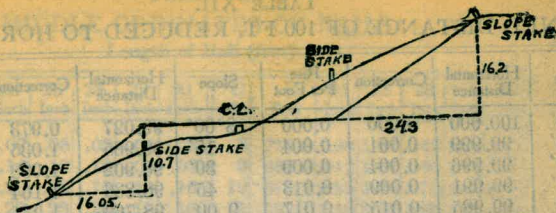
of table in same row and column gives distance from side stake to slope stake. If ground is not

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

29.06
30
59.04

395.66
6
401.66

18 + 70.96 = 349.12

40
18
58 4.83
10 2.41
12

check 28.50
" 17.99
" 19.50