

W 293

First Cross Sections

1870-1880

# 293

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*ENGINEERING and DRAFTING SUPPLIES*

IRVING PARK STATION

CHICAGO, ILL.  
**MICROFILMED**

JAN 11 1965

O.R.-S.D. 2nd. Main Pipe Line.  
City Datum.

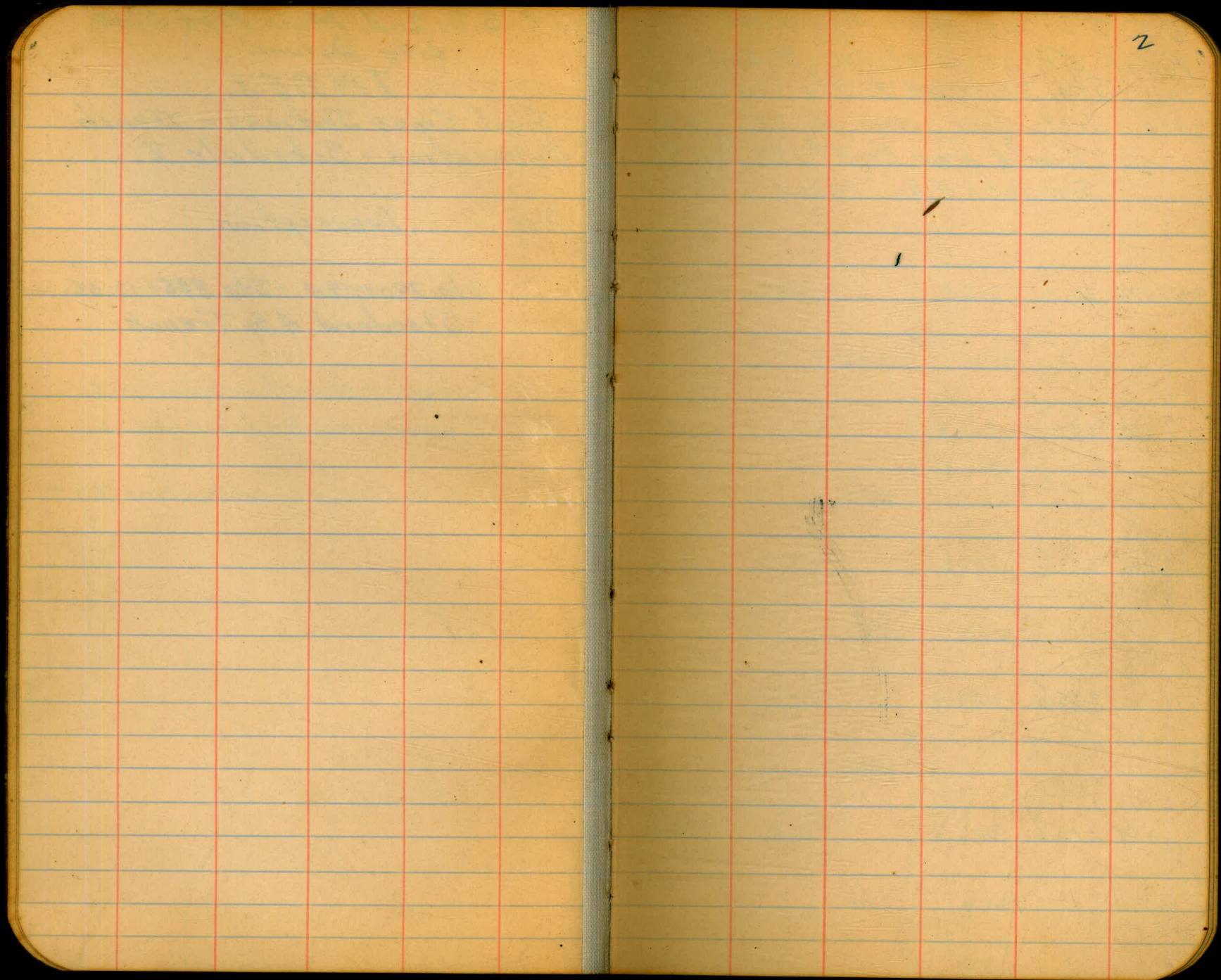
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Excavation - Schedule I.

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MICROFILMED

JAN 1 1982



2

O.R. - S.D. 2nd. Main Pipe Line  
 Final Cross Sections - Schedule I  
 Sta. 790+09.4 to Sta. 855+12.05

Sta Grade Elev Dist L.C.  $\frac{1}{4}$   
 Contd. from Book #292, Page 79,  
 Standard 4.50 Trench.

790+09.4 360.8 365.5 4.7 4.7 4.7 21.15 ✓

15.6 ✓

22.275 ✓ 12.87 ✓

+25 358.0 363.7 5.2 23.40 ✓

25 ✓

23.40 ✓ 21.67 ✓

+50 353.7 358.9 5.2 23.40 ✓

50 ✓

21.60 ✓ 40.00 ✓

791 345.0 349.4 4.4 19.80 ✓

25 ✓

22.05 ✓ 20.42 ✓

+25 340.6 346.0 5.4 24.30 ✓

5.0 ✓

26.11 ✓ 4.84 ✓

Chd. T.M.M.  
 Calc. M.D.B.  
 ✓ W.H.S.

✓ A.C.L.  
 Calc. M.D.B. of  
 99.80 ✓

1/22/30 Converse - Notes  
 Clear + Warm Hill - Grades  
 Elliott -  $\pi$   
 Simpson - Sick  
 Walton

R.C. End Area Av. Area Cu Yds

Sta	Grade	Elev	Dist	L.C.	Q.	R.C.		
+30	339.7	345.9		6.2	6.2	6.2	27.91	
			6.				25.66	5.70
+36	338.6	343.8			5.2		23.40	
			31.				24.97	28.67
+67	332.8	338.7			5.9		26.55	
			33.				25.88	31.63
792	326.6	332.2			5.6		25.20	
			25.				23.40	21.67
+25	322.0	326.8			4.8		21.60	
			25.				22.73	21.05
+50	315.7	321.0			5.3		23.85	
			15.				22.05	12.25

Chd. T.M.M.  
 Calc. W.H.S.  
 ✓ M.R.E.

P.A.C.L.  
 Calc. M.R.E.  
 120.97

+65 312.0 ✓ 316.5

4.5 ✓

20.25 ✓

16.1 ✓

18.68 ✓

11.07 ✓

+81 308.0 ✓ 311.8

3.8 ✓

17.10 ✓

8.2 ✓

8.55 ✓

2.60 ✓

+89.2 308.0 ✓ 308.0

0.0 ✓

0.0 ✓

41.2 ✓

0. ✓

0.0 ✓

793+30.5 308.0 ✓ 308.0

0.0 ✓

0.0 ✓

19.5 ✓

5.62 ✓

4.06 ✓

+50 308.0 ✓ 310.5

2.5 ✓

11.25 ✓

21. ✓

15.30 ✓

11.90 ✓

+71 308.0 ✓ 312.3

4.3 ✓

19.35 ✓

29. ✓

Chd. T.M.M.

22.05 ✓

23.68 ✓

Calc. M.A.S.  
✓ - w.H.S.

✓ A.C.L.

Calc. M.A.S. of  
53.31 ✓

794 309.8 ✓ 315.3 ✓

5.5 ✓

24.75 ✓✓

50. ✓

22.73 ✓  
42.09 ✓✓

+50 312.9 ✓ 317.5 ✓

4.6 ✓

20.70 ✓✓

50. ✓

20.25 ✓  
37.50 ✓✓

795 316.1 ✓ 320.5 ✓

4.4 ✓

19.80 ✓✓

50. ✓

22.50 ✓  
41.67 ✓✓

+50 319.2 ✓ 324.8 ✓

5.6 ✓

25.20 ✓✓

25. ✓

23.62 ✓  
21.87 ✓✓

+75 322.2 ✓ 327.1 ✓

4.9 ✓

22.05 ✓✓

25. ✓

22.50 ✓  
20.83 ✓✓

796 325.2 ✓ 330.3 ✓

5.1 ✓

22.95 ✓✓

20. ✓

21.83 ✓  
16.17 ✓✓calc. - w. H.S.  
✓ M.D.E

P.A.C.I.

Calc M.D.E ✓  
180.13 ✓



+20	327.7 <sup>✓</sup>	332.3	4.6	20.70 <sup>✓✓</sup>	21.60 <sup>✓</sup>	8.00 <sup>✓✓</sup>
					21.83 <sup>✓</sup>	8.89 <sup>✓</sup>
			10.✓			
+30	328.9 <sup>✓</sup>	333.9	5.0 <sup>✓</sup>	22.50 <sup>✓</sup>		
					23.62 <sup>✓</sup>	17.50 <sup>✓</sup>
			20.✓			
+50	331.3 <sup>✓</sup>	336.8	5.5	24.75 <sup>✓</sup>		
					25.88 <sup>✓</sup>	47.91 <sup>✓</sup>
			50.✓			47.93 <sup>✓</sup>
797	337.4 <sup>✓</sup>	343.4	6.0	27.00 <sup>✓</sup>		
					28.20 <sup>✓</sup>	46.67 <sup>✓</sup>
			50.✓			
+50	343.4 <sup>✓</sup>	348.6	5.2 <sup>✓</sup>	23.40 <sup>✓</sup>		
					24.75 <sup>✓</sup>	45.83 <sup>✓</sup>
			50.✓			
798	347.3 <sup>✓</sup>	353.1	5.8	26.10 <sup>✓</sup>		
					21.15 <sup>✓</sup>	25.07 <sup>✓</sup>
			32.✓			
					190.98 <sup>✓</sup>	

Chd. T.M.M.  
Calc M.D.E.  
✓ - W.H.S.

FALL.

Calc M.D.E. of  
190.98<sup>✓</sup>

+32 349.7 ✓ 353.3

3.6 ✓

18. ✓

16.20 ✓

20.03 ✓ 13.35 ✓

+50 351.2 ✓ 356.5

5.3 ✓

50. ✓

23.85 ✓

24.97 ✓ 46.24 ✓

799 355.0 ✓ 360.8

5.8 ✓

25. ✓

26.10 ✓

25.43 ✓ 23.55 ✓

+25 357.0 ✓ 362.5

5.5 ✓

25. ✓

29.75 ✓

27.71 ✓ 25.66 ✓

+50 358.9 ✓ 366.3

6.2 ✓  
2.30 ✓ 7.4 ✓

20. ✓

6.2 ✓  
2.30 ✓ 30.67 ✓

26.58 ✓ 19.69 ✓

+70 360.5 ✓ 365.5

5.0 ✓

19.9 ✓

22.50 ✓

22.05 ✓ 16.25 ✓

Chd. T.M.M.  
calc. - w. H.S.  
M.R.E

Calc M.R.E  
144.74 ✓

+89.9 362.0 366.8

4.8

21.60 ✓

10.1 ✓

22.73 ✓

8.50 ✓

800

362.0 367.3

5.3

23.85 ✓

19.9 ✓

22.95 ✓

16.92 ✓

+19.9 362.0 366.9

4.9

22.05 ✓

30. ✓

23.90 ✓

26.00 ✓

+49.9 361.1 366.6

5.5

24.75 ✓

29.9 ✓

25.65 ✓

28.41 ✓

+79.8 358.4 364.3

5.9

26.55 ✓

13.2 ✓

25.20 ✓

12.32 ✓

+93 356.7 362.0

5.3

23.85 ✓

16.4 ✓

25.42 ✓

15.44 ✓

Chd. T.M.M.  
Calc. M.A.B.  
✓ - W.H.S.

CALL

M.A.B.

107.59 ✓

801+09.4 354.0 ✓ 360.0 6.0 ✓

15.6 ✓

27.00 ✓

26.10 ✓ 15.08 ✓

+25 351.2 ✓ 356.8 5.6 ✓

25.0 ✓

25.20 ✓

24.525 ✓  
24.57 ✓  
22.71 ✓  
22.75 ✓

+50 346.8 ✓ 352.1 5.3 ✓

25. ✓

23.85 ✓

25.43 ✓ 23.55 ✓

+75 342.3 ✓ 348.3 6.0 ✓

15. ✓

27.00 ✓

28.82 ✓ 16.01 ✓

+90 339.6 ✓ 346.3 6.7 ✓

6.7 ✓  
2.3 ✓

7.5 ✓  
2.63 ✓

30.64 ✓

10. ✓

36.09 ✓ 13.37 ✓

802 337.8 ✓ 346.8 9.0 ✓

8.2 ✓  
2.8 ✓

9.0 ✓  
3.0 ✓

41.55 ✓

12. ✓

36.65 ✓ 16.29 ✓  
107.01 ✓

Chd. T.M.M.  
calc. - w.H.S.  
M.B.E.  
VALL.  
Calc M.B.E.

End Area, Av. End Ar. Cu. yds.

+12 335.6 342.6

$\frac{7.0}{2.5}$  7.0

$\frac{7.0}{2.5}$  31.75 ✓

9.04 ✓

30.06 ✓ 10.06 ✓

802 +21.04 334.0 340.3  
800 + 66.20

$\frac{6.3}{2.33}$  6.3

$\frac{6.3}{2.33}$  28.37 ✓

↑  
Expansion

0.0

28.37 ✓ 0.0 ✓

800 + 66.20 334.0 340.3

$\frac{6.3}{2.33}$  6.3

$\frac{6.3}{2.33}$  28.37 ✓

8.8 ✓

29.82 ✓ 9.72 ✓

+75 332.7 339.6

$\frac{6.9}{2.48}$  6.9

$\frac{6.9}{2.48}$  31.26 ✓

25.1 ✓

29.13 ✓ 26.97 ✓

801 329.2 335.2

6.0

27.00 ✓

25.1 ✓

24.75 ✓ 22.92 ✓

+25 325.6 330.6

5.0

22.50 ✓

25.1 ✓

21.83 ✓ 20.21 ✓

Chd. T.M.M.  
Calc. M.D.E.  
V - W.H.S.

109.88 89.88 ✓

+50 ✓ 323.0 327.7 4.7 ✓

↑  
50. ✓

21.15 ✓

21.15 ✓ 39.17 ✓

802 317.8 ✓ 322.5 4.7 ✓

14.6 ✓

21.15 ✓

21.825 ✓ 11.80 ✓

+14.6 316.3 ✓ 321.3 5.0 ✓

10.4 ✓

22.50 ✓

24.30 ✓ 9.36 ✓

+25 315.2 ✓ 321.0 5.8 ✓

50. ✓

26.10 ✓

25.88 ✓ 47.93 ✓

+75 312.4 ✓ 318.1 5.7 ✓

25. ✓

25.65 ✓

24.08 ✓ 22.30 ✓

803 311.0 ✓ 316.0 5.0 ✓

17. ✓

22.50 ✓

22.28 ✓ 19.03 ✓

Chd. T.M.M.  
calc. w. H.S.  
M.D.S.

FA.C.L.  
Calc. M.D.B.  
144.59 ✓

+17 310.0<sup>✓</sup> 314.94.9 4.9<sup>✓</sup>4.9 22.05<sup>✓</sup>7.0<sup>✓</sup>17.95<sup>✓</sup> 4.65<sup>✓</sup>+24 309.7<sup>✓</sup> Pipe  
313.2 $\frac{2.6}{2.25}$  3.5<sup>✓</sup> $\frac{2.7}{2.25}$  13.84<sup>✓</sup>26.1<sup>✓</sup>14.74<sup>✓</sup> 14.19<sup>✓</sup>+50 308.2<sup>✓</sup> Pipe  
312.3 $\frac{2.8}{2.25}$  4.1 $\frac{2.9}{2.25}$  15.64<sup>✓</sup>25.1<sup>✓</sup>18.28<sup>✓</sup> 16.93<sup>✓</sup>+75 306.8<sup>✓</sup> Pipe  
311.6 $\frac{3.7}{2.25}$  4.8<sup>✓</sup> $\frac{5.3}{2.25}$  20.93<sup>✓</sup>25.1<sup>✓</sup>21.94<sup>✓</sup> 20.31<sup>✓</sup>804 305.4<sup>✓</sup> Pipe  
310.6 $\frac{4.7}{2.25}$  5.2<sup>✓</sup> $\frac{5.3}{2.25}$  22.95<sup>✓</sup>10.1<sup>✓</sup>23.52<sup>✓</sup> 8.71<sup>✓</sup>+10 304.8<sup>✓</sup> 310.1 $\frac{4.8}{2.25}$  5.3<sup>✓</sup> $\frac{6.0}{2.25}$  24.08<sup>✓</sup>5.1<sup>✓</sup>

Chd. T.M.M.

Calc M.A.B.

- w.H.S.

26.51<sup>✓</sup>

A.C.L.

Calc M.A.B.

4.91<sup>✓</sup>69.70<sup>✓</sup>

+15	304.3 ✓	310.6		$\frac{6.8}{2.45}$	6.3 ✓	$\frac{6.3}{2.33}$	28.95 ✓		
			24.8 ✓					30.86 ✓	28.35 ✓
+27.8	301.7 ✓	308.9		$\frac{7.2}{2.55}$	7.2 ✓	$\frac{7.2}{2.55}$	32.76 ✓		
			7.2 ✓					31.52 ✓	8.91 ✓
+47	300.6 ✓	307.3		$\frac{6.7}{2.43}$	6.7 ✓	$\frac{6.7}{2.43}$	30.28 ✓		
			3. ✓					26.47 ✓	2.94 ✓
+50	300.1 ✓	304.7		$\frac{4.6}{2.25}$	4.6 ✓	$\frac{6.4}{2.35}$	22.66 ✓		
			15. ✓					25.28 ✓	14.04 ✓
+65	297.7 ✓	303.7		$\frac{6.0}{2.25}$	6.0 ✓	$\frac{6.8}{2.45}$	27.90 ✓		
			20. ✓					28.60 ✓	21.19 ✓
+85	294.6 ✓	301.1		$\frac{6.5}{2.38}$	6.5 ✓	$\frac{6.5}{2.38}$	29.31 ✓		
			15. ✓					28.16 ✓	15.64 ✓

Chd. T.M.M.

Calc. W.H.S.  
M.B.

I.A.C.L.

Calc. M.H.P.

Total 90.57 ✓



805	292.2 <sup>r</sup>	298.2	$\frac{6.0}{2.25}$	6.0	$\frac{6.0}{2.25}$	27.00 <sup>✓</sup>	
				35.1 <sup>✓</sup>		27.00 <sup>✓</sup>	35.10 <sup>✓</sup>
+35.1	286.8 <sup>✓</sup>	292.8	$\frac{6.0}{2.25}$	6.0	$\frac{6.0}{2.25}$	27.00 <sup>✓</sup>	
				22.9 <sup>✓</sup>		28.88 <sup>✓</sup>	24.49 <sup>✓</sup>
+58	285.0 <sup>r</sup>	291.8	$\frac{6.8}{2.45}$	6.8	$\frac{6.8}{2.45}$	30.76 <sup>✓</sup>	
				7 <sup>✓</sup>		30.52 <sup>✓</sup>	29.1 <sup>✓</sup>
+65	284.4 <sup>✓</sup>	291.1	$\frac{6.7}{2.43}$	6.7	$\frac{6.7}{2.43}$	30.28 <sup>✓</sup>	
				10 <sup>✓</sup>		24.36 <sup>✓</sup>	9.02 <sup>✓</sup>
+75	284.4 <sup>✓</sup>	288.5		4.1		18.45 <sup>✓</sup>	
				25 <sup>✓</sup>		15.98 <sup>✓</sup>	14.80 <sup>✓</sup>
806	284.4 <sup>r</sup>	287.4		3.0		13.50 <sup>✓</sup>	
				20 <sup>✓</sup>		18.67 <sup>✓</sup>	13.83 <sup>✓</sup>
						Chd. T.M.M.	
						Calc. M.R.S.	
						- W.H.S.	
						Calc. M.R.P.	
						105.15 <sup>✓</sup>	

806 + 20 284.4 ✓ 289.7

5.3 ✓

23.85 ✓

5. ✓

29.35 ✓

5.44 ✓

+25 284.4 ✓ 292.0

$\frac{7.6}{2.65}$  ✓

7.6 ✓

$\frac{7.6}{2.65}$  ✓

34.84 ✓

10. ✓

37.53 ✓

13.90 ✓

+35 284.4 ✓ 292.7

$\frac{8.3}{2.83}$  ✓

8.3 ✓

$\frac{7.4}{3.10}$  ✓

40.23 ✓

29.9 ✓

36.45 ✓

40.37 ✓

+64.9 286.1 ✓ 292.7

$\frac{8.6}{2.9}$  ✓

6.6 ✓

$\frac{7.0}{2.5}$  ✓

32.67 ✓

35.1 ✓

25.17 ✓

32.72 ✓

807 290.2 ✓ 293.1

$\frac{6.0}{2.25}$  ✓

2.9 ✓

$\frac{3.9}{2.25}$  ✓

17.66 ✓

35. ✓

16.03 ✓

20.78 ✓

+35 294.3 ✓ 297.0

$\frac{3.7}{2.25}$  ✓

2.7 ✓

$\frac{3.7}{2.25}$  ✓

19.40 ✓

30. ✓

Calc. T.M.M.

17.60 ✓

19.56 ✓

Calc. w. H.S.  
-M.D.E

P.C.L.

Calc. m.d.e.  
132.77 ✓

+65	296.0 <sup>✓</sup>	300.0	$\frac{6.0}{2.25}$ ✓	4.0 <sup>✓</sup>	$\frac{4.5}{2.25}$ ✓	20.81 <sup>✓</sup>	0 <sup>✓</sup>	20.53 <sup>✓</sup>	26.61 <sup>✓</sup>
808	296.0 <sup>✓</sup>	299.5	$\frac{5.5}{2.25}$ ✓	3.5	$\frac{5.5}{2.25}$ ✓	20.25 <sup>✓</sup>	0 <sup>✓</sup>	21.53 <sup>✓</sup>	39.87 <sup>✓</sup>
+50	296.1 <sup>✓</sup>	300.0	$\frac{5.4}{2.25}$ ✓	3.9	$\frac{7.4}{2.6}$ ✓	22.81 <sup>✓</sup>	0 <sup>✓</sup>	21.34 <sup>✓</sup>	39.52 <sup>✓</sup>
809	296.1 <sup>✓</sup>	300.0	$\frac{4.6}{2.25}$ ✓	3.9	$\frac{4.4}{1.8}$ $\frac{6.6}{3.0}$ $\frac{6.8}{2.45}$	19.87 <sup>✓</sup>	0 <sup>✓</sup>	21.57 <sup>✓</sup>	39.94 <sup>✓</sup>
+50	296.1 <sup>✓</sup>	300.3	$\frac{6.8}{2.45}$ $\frac{6.6}{2.0}$ $\frac{5.0}{1.8}$	4.2	$\frac{5.4}{1.7}$ $\frac{7.0}{1.9}$ $\frac{7.4}{2.6}$	23.27 <sup>✓</sup>	0 <sup>✓</sup>	23.17 <sup>✓</sup>	42.91 <sup>✓</sup>
810	296.1 <sup>✓</sup>	300.1	$\frac{8.1}{2.78}$ $\frac{7.8}{2.3}$ $\frac{5.2}{2.0}$	4.0	$\frac{5.0}{1.8}$ $\frac{7.8}{2.0}$ $\frac{8.1}{2.78}$	23.07 <sup>✓</sup>	0 <sup>✓</sup>	22.53 <sup>✓</sup>	41.72 <sup>✓</sup>
						Chd. T.M.M.	22.53 <sup>✓</sup>	ACCL.	41.72 <sup>✓</sup>
						Calc. M.A.S.		Calc. M.A.S.	
						W.H.S.			230.57 <sup>2x</sup>

+50 296.2 ✓ 299.8

$$\frac{8.2}{2.80} \frac{8.0}{2.2} \frac{4.8}{2.0} 3.6$$

$$\frac{4.7}{1.8} \frac{8.0}{2.0} \frac{8.3}{2.83}$$

21.99 ✓

25. ✓

20.90 ✓

19.35 ✓

✓

+75 296.2 ✓ 299.7

$$\frac{8.0}{2.75} \frac{7.7}{2.2} \frac{4.7}{2.0} 3.5$$

$$\frac{4.7}{2.0} \frac{6.0}{2.25}$$

19.80 ✓

25. ✓

19.19 ✓

17.77 ✓

✓

811 296.2 ✓ 299.4

$$\frac{8.3}{2.83} \frac{8.0}{2.2} \frac{4.2}{2.0} 3.2$$

$$\frac{4.1}{2.0} \frac{7.3}{2.25} \frac{7.6}{2.65}$$

18.59 ✓

50. ✓

17.13 ✓

31.72 ✓

M.R.E. ✓

~~17.14~~~~31.77~~

+50 296.2 ✓ 298.9

$$\frac{7.0}{2.5} \frac{3.8}{2.0} 2.7$$

$$\frac{3.6}{1.7} \frac{5.0}{2.0} \frac{6.0}{2.25}$$
~~15.60~~ ✓ A.C.L.  
 15.67 ✓

~~17.14~~ ✓ ch. 1/1/30

~~31.77~~ ✓ L.M.H. M.R.G.

30. ✓

Note - X sec. ends here. → ?

2.25

15.57 ✓

17.30 ✓

+80 296.2 ✓ 298.7

$$\frac{2.6}{2.65} \frac{3.6}{2.0} 2.5$$

$$\frac{3.5}{1.6} \frac{6.1}{2.0} \frac{6.4}{2.25}$$

15.97 ✓

15.47 ✓

ch. 1/1/30

L.M.H. M.R.G.

20. ✓

~~14.52~~ ✓  
~~14.55~~

10.76 ✓

812 296.3 ✓ 298.3

$$\frac{7.6}{2.65} \frac{7.0}{2.3} \frac{3.4}{1.8} 2.0$$

$$\frac{3.3}{2.0} \frac{4.4}{2.25}$$

13.56 ✓

13.62 ✓

50. ✓

11.38 ✓

21.07 ✓

Chd. T.M.M.

A.C.L. ✓

Calc. w.H.S.

Calc. M.R.G.

117.97 ✓

+50 296.3<sup>✓</sup> 297.6

$\frac{6.0}{2.25}$  2.4 1.3

$\frac{2.4}{2.0}$   $\frac{3.5}{2.25}$

9.19<sup>✓</sup>

50.:

10.42<sup>✓</sup>

19.30<sup>✓</sup>

813 296.3<sup>✓</sup> 298.2

$\frac{6.5}{2.38}$  2.7 1.9

$\frac{3.0}{1.8}$   $\frac{4.4}{2.25}$

~~11.61~~ 11.66<sup>✓</sup> ch. 7/1/30<sup>✓</sup> A.C.L. L.H.H. M.D.S.

50.:

13.32<sup>✓</sup>

24.67<sup>✓</sup>

+50 296.3<sup>✓</sup> 298.9

$\frac{7.1}{2.53}$  3.6 2.6

$\frac{3.6}{1.8}$   $\frac{7.2}{2.55}$

~~14.85~~ 14.99<sup>✓</sup> ch. 7/1/30<sup>✓</sup> L.H.H. M.D.S. A.C.L.

35.:

16.96<sup>✓</sup>

21.99<sup>✓</sup>

+85 296.4<sup>✓</sup> 300.1

$\frac{8.7}{2.93}$  4.5 3.7

$\frac{4.5}{2.0}$   $\frac{8.3}{2.83}$

~~18.71~~ 18.93<sup>✓</sup> A.C.L.

29.9.:

24.76<sup>✓</sup>

27.42<sup>✓</sup>

814 +14.9 298.0<sup>✓</sup> 303.6

$\frac{9.5}{3.13}$  6.8 5.6

$\frac{6.7}{1.8}$   $\frac{9.4}{2.5}$   $\frac{9.4}{3.1}$

30.59<sup>✓</sup>

35.:

28.85<sup>✓</sup>

37.51<sup>✓</sup>

+50 301.9<sup>✓</sup> 307.2

$\frac{6.4}{2.35}$  5.3

$\frac{6.4}{2.7}$   $\frac{8.7}{2.4}$   $\frac{8.7}{2.93}$

27.12<sup>✓</sup>

50.:

29.36<sup>✓</sup>

54.37<sup>✓</sup>

Chd. T.M.M.

Cole M.R.S.

W.H.S.

A.C.L.

M.D.S.

185.26<sup>✓</sup>

815 307.4 ✓ 313.1  $\frac{10.3}{3.33} \frac{10.0}{2.6} \frac{6.8}{2.0} 5.7$

42.2 ✓

$\frac{6.7}{2.0} \frac{9.3}{2.5} \frac{9.3}{3.08} 31.60$  ✓ ✓

28.38 ✓ 44.36 ✓

+42.2 312.0 ✓ 316.9  $\frac{2.7}{2.68} \frac{6.0}{2.0} 4.9$

30. ✓

$\frac{6.0}{2.0} \frac{7.1}{2.53} 25.15$  ✓ ✓

27.35 ✓ 30.39 ✓

+72.2 313.8 ✓ 319.3  $\frac{7.4}{3.7} \frac{9.0}{2.6} \frac{6.8}{1.8} 5.5$

27.8 ✓

$\frac{6.7}{2.0} \frac{7.5}{2.63} 29.55$  ✓ ✓ L.H.H.

33.61 ✓ 34.61 ✓

816 314.0 ✓ 320.6  $\frac{11.4}{3.6} \frac{11.0}{3.0} \frac{8.3}{1.8} 6.6$

50. ✓

$\frac{8.0}{1.8} \frac{9.0}{3.0} \frac{9.7}{3.05} 37.68$  ✓ ✓ L.H.H.

40.90 ✓ 75.74 ✓

+50 314.4 ✓ 322.2  $\frac{11.7}{3.68} \frac{11.2}{3.0} \frac{9.5}{2.0} 7.3$

15. ✓

$\frac{8.9}{2.0} \frac{10.8}{3.0} \frac{10.8}{3.45} 49.11$  ✓ ✓ L.H.H.

46.26 ✓ 25.70 ✓

+65 314.5 ✓ 322.7  $\frac{13.0}{4.0} \frac{13.0}{3.0} \frac{9.4}{2.0} 8.2$

5. ✓

$\frac{9.6}{1.8} \frac{10.7}{2.5} \frac{10.7}{3.43} 48.90$  ✓ ✓

40.07 ✓ 7.42 ✓

Chd. Tm. M.  
Calc. w. H.S.  
M.D. 60

V.A.L.L.  
Calc. M.D. 8  
198.22 218.22 ✓

+70 314.5 ✓ 321.5

$\frac{7.0}{2.5}$  7.0

7. ✓

$\frac{7.0}{2.5}$  31.75 ✓

28.93 ✓ 7.50 ✓

+77 314.6 ✓ 320.4

5.8 ✓

26.10 ✓

8.2 ✓

26.32 ✓ 7.99 ✓

+85.2 314.7 ✓ 320.6

5.9 ✓

26.55 ✓

↑  
14.8 ✓

26.78 ✓ 14.68 ✓

817

314.8 ✓ 320.8

Parlement

6.0 ✓

27.00 ✓

19. ✓

26.10 ✓ 18.37 ✓

+19 315.0 ✓ 320.6

5.6 ✓

25.20 ✓

7. ✓

26.10 ✓ 6.77 ✓

+26 315.0 ✓ 321.0

$\frac{6.0}{2.25}$  6.0

4. ✓

$\frac{6.0}{2.25}$  27.00 ✓

Chd. T.M.M.  
Calc. M.D.S.  
V.W.H.S.

33.26 ✓  
4.93 ✓  
4.78 ✓  
60.24 ✓

+30	315.0 <sup>✓</sup>	323.6		$\frac{7.6}{3.15}$	8.6 <sup>✓</sup>	$\frac{7.0}{2.5}$	39.52 <sup>✓</sup>		
			5.0 <sup>✓</sup>				42.33 <sup>✓</sup>	7.84 <sup>✓</sup>	
+35	315.1 <sup>✓</sup>	324.0		$\frac{11.0}{3.50}$	8.9 <sup>✓</sup>	$\frac{8.8}{2.95}$	45.15 <sup>✓</sup>		
			4.0 <sup>✓</sup>				53.72 <sup>✓</sup>	7.96 <sup>✓</sup>	
+39	315.1 <sup>✓</sup>	327.0		$\frac{11.9}{3.73}$	11.9 <sup>✓</sup>	$\frac{11.9}{3.73}$	62.28 <sup>✓</sup>		
			11.0 <sup>✓</sup>				61.16 <sup>✓</sup>	24.92 <sup>✓</sup>	
+50	315.2 <sup>✓</sup>	326.8		$\frac{11.6}{3.65}$	11.6 <sup>✓</sup>	$\frac{11.6}{3.65}$	60.04 <sup>✓</sup>		
			30.0 <sup>✓</sup>				51.39 <sup>✓</sup>	57.10 <sup>✓</sup>	
+80	315.4 <sup>✓</sup>	324.4		$\frac{9.0}{3.0}$	9.0 <sup>✓</sup>	$\frac{9.0}{3.0}$	42.75 <sup>✓</sup>		
			20.0 <sup>✓</sup>				33.93 <sup>✓</sup>	25.13 <sup>✓</sup>	
218	315.6 <sup>✓</sup>	322.0		$\frac{6.4}{2.85}$	6.4 <sup>✓</sup>	$\frac{3.1}{2.75}$	25.11 <sup>✓</sup>		
			15.0 <sup>✓</sup>				26.06 <sup>✓</sup>	14.48 <sup>✓</sup>	
							137.43 <sup>✓</sup>		

Wood Stave Pipe

Chd. T.M.M.  
Calc. - W.H.S.  
M.P.G.

26.06  
A.C.L.  
M.A.B.  
137.43<sup>✓</sup>



+15	314.9 <sup>✓</sup>	320.9		$\frac{6.0}{2.25}$ ✓	6.0 <sup>-</sup>	$\frac{6.0}{2.25}$ ✓	27.00 <sup>✓</sup>		
			45. ✓				24.52 <sup>✓</sup>	40.87 <sup>✓</sup>	9
+60	313.0 <sup>✓</sup>	317.9			4.9 <sup>-</sup>		22.05 <sup>✓</sup>		
			29.9 <sup>✓</sup>				21.83 <sup>✓</sup>	24.17 <sup>✓</sup>	9
+89.9	310.2 <sup>✓</sup>	315.0			4.8 <sup>-</sup>		21.60 <sup>✓</sup>		
			20.1 <sup>✓</sup>				22.50 <sup>✓</sup>	16.75 <sup>✓</sup>	9
819+10	307.3 <sup>✓</sup>	312.5			5.2 <sup>-</sup>		23.40 <sup>✓</sup>		
			15. ✓				24.30 <sup>✓</sup>	13.50 <sup>✓</sup>	9
+25	305.1 <sup>✓</sup>	310.7			5.6 <sup>-</sup>		25.20 <sup>✓</sup>		
			10. ✓				26.10 <sup>✓</sup>	9.67 <sup>✓</sup>	9
+35	303.7 <sup>✓</sup>	319.7			6.0 <sup>-</sup>		27.00 <sup>✓</sup>		
			15. ✓				27.00 <sup>✓</sup>	15.00 <sup>✓</sup>	9
							119.96 <sup>✓</sup>		

Wood Stave Pipe

Chd. T.M.M.  
Calc. M.R.G.  
✓ - W.H.S.

27.00<sup>✓</sup>  
✓ A.C.L.  
M.R.G.

119.96<sup>✓</sup>

+50 301.5 ✓ 307.5 6.0 ✓

27.00 ✓

35. ✓

24.53 ✓ 31.80 ✓

+85 296.5 ✓ 301.4 4.9 ✓

22.05 ✓

15. ✓

22.50 ✓ 12.50 ✓

820 294.3 ✓ 299.4 5.1 ✓

22.95 ✓

Wood Stave Pipe

30.0 ✓

24.97 ✓ 27.79 ✓

+30 290.0 ✓ 296.0 6.0 ✓

27.00 ✓

10.0 ✓

30.14 ✓ 11.16 ✓

+40 288.5 ✓ 295.8  $\frac{7.3}{2.58}$  7.3 ✓

$\frac{7.3}{2.58}$  33.28 ✓

10. ✓

31.78 ✓ 11.77 ✓

+50 287.1 ✓ 293.8  $\frac{6.7}{2.43}$  6.7 ✓

$\frac{6.7}{2.43}$  30.28 ✓

35.1 ✓

33.38 ✓ 43.39 ✓

Chd. T.M.M.  
col. - w. H.S.  
M.R.G.

138.36 ✓

+85.1

282.1 ✓

290.0

Wood Stake Pile

 $\frac{7.7}{2.73}$  ✓

7.9 ✓

 $\frac{7.7}{2.73}$  ✓

36.47 ✓

4.9 ✓

29.91 ✓

5.43 ✓

+90

281.5 ✓

286.2 ✓

↓

 $\frac{8.5}{2.88}$  $\frac{5.4}{1.8}$ 

4.7 ✓

 $\frac{5.0}{1.8}$  $\frac{7.2}{2.55}$ 

23.36 ✓

10. ✓

23.93 ✓

8.86 ✓

821

280.5 ✓

285.4

 $\frac{7.7}{2.68}$  $\frac{5.5}{1.8}$ 

4.9 ✓

 $\frac{6.0}{2.75}$ 

24.49 ✓

15. ✓

27.31 ✓

15.17 ✓

+15

279.0 ✓

285.4

 $\frac{7.5}{2.63}$  ✓

6.4 ✓

 $\frac{6.4}{2.35}$ 

30.13 ✓

35. ✓

26.54 ✓

34.40 ✓

+50

277.7 ✓

282.5

 $\frac{6.0}{2.75}$ 

4.8 ✓

 $\frac{4.8}{2.75}$ 

22.95 ✓

50. ✓

19.40 ✓

35.93 ✓

822

275.7 ✓

279.0

 $\frac{4.2}{2.75}$ 

3.3 ✓

 $\frac{3.3}{2.25}$ 

15.86 ✓

50. ✓

15.58 ✓

28.85 ✓

Chd. T.M.M.

Calc. M.R.C.

v. - w.H.S.

P.A.C.L.

M.R.C.

128.64 ✓

+50 273.8<sup>✓</sup> 277.0

$\frac{4.0}{2.25}$

3.2<sup>✓</sup>

$\frac{3.2}{2.25}$

15.30<sup>✓</sup>

50. ✓

15.87<sup>✓</sup>

29.39<sup>✓</sup>

823 271.9<sup>✓</sup> 275.3

$\frac{4.4}{2.25}$

3.4<sup>✓</sup>

$\frac{3.4}{2.25}$

16.43<sup>✓</sup>

50. ✓

16.84<sup>✓</sup>

31.19<sup>✓</sup>

+50 269.9<sup>✓</sup> 273.0

$\frac{6.8}{2.45}$   $\frac{3.8}{1.2}$

3.1<sup>✓</sup>

$\frac{3.8}{2.25}$

17.25<sup>✓</sup>

6. ✓

15.26<sup>✓</sup>

3.39<sup>✓</sup>

+56 269.9<sup>✓</sup> 272.8

$\frac{3.0}{2.25}$

2.9<sup>✓</sup>

$\frac{3.0}{2.25}$

13.28<sup>✓</sup>

4. ✓

22.02<sup>✓</sup>

3.26<sup>✓</sup>

+60 269.9<sup>✓</sup> 276.7

$\frac{6.8}{2.45}$

6.8<sup>✓</sup>

$\frac{6.8}{2.45}$

30.76<sup>✓</sup>

15. ✓

28.88<sup>✓</sup>

16.04<sup>✓</sup>

+75 269.9<sup>✓</sup> 275.8

$\frac{6.0}{2.25}$

6.0<sup>✓</sup>

$\frac{6.0}{2.25}$

27.00<sup>✓</sup>

15. ✓

25.88<sup>✓</sup>

14.38<sup>✓</sup>

Wood Stave Pipe

Chd. T.M.M.

Calc. - w. H.S.  
- M.P.E.

A.C.L.

M.P.E.

97.65<sup>✓</sup>

+90	269.8 ✓	275.3		5.5 ✓		24.75 ✓		
			Wood Stake Pipe				23.85 ✓	53.00 ✓
			60 ✓					
824+50	269.7 ✓	274.8		5.1 ✓		22.95 ✓		
			10 ✓				22.27 ✓	8.25 ✓
+60	269.7 ✓	274.5	↓	4.8 ✓		21.60 ✓		
			1. ✓				18.28 ✓	0.68 ✓
+61	269.7 ✓	272.8		3.1 ✓	$\frac{3.0}{2.25}$	19.96 ✓		
			44. ✓				16.93 ✓	27.59 ✓
825+05	269.6 ✓	273.2		3.6 ✓	$\frac{3.6}{2.25}$	18.90 ✓		
			22. ✓				17.78 ✓	14.49 ✓
+27	269.6 ✓	273.0		3.4 ✓	$\frac{3.4}{2.25}$	16.65 ✓		
			1. ✓				19.80 ✓	0.73 ✓
							104.74 ✓	

Chd. T.M.M.  
Calc. M.H.B.  
V. - W.H.S.

M.A.B.  
104.74 ✓

+28	269.6 <sup>✓</sup>	274.7	↑	$\frac{5.1}{2.25}$	5.1 <sup>✓</sup>	$\frac{5.1}{2.25}$	22.95 <sup>✓</sup>			
				2.1 <sup>✓</sup>			25.89 <sup>✓</sup>	1.92 <sup>✓</sup>		
+30	269.6 <sup>✓</sup>	276.0		$\frac{6.4}{2.35}$	6.4 <sup>✓</sup>	$\frac{6.4}{2.35}$	28.84 <sup>✓</sup>			
				20.1 <sup>✓</sup>			30.78 <sup>✓</sup>	22.80 <sup>✓</sup>		
+50	269.5 <sup>✓</sup>	276.2	Wood Store Pipe	$\frac{7.9}{2.73}$	6.7 <sup>✓</sup>	$\frac{7.5}{2.63}$	<del>32.76</del> 32.70 <sup>✓</sup>			
				50.1 <sup>✓</sup>				34.18 <sup>✓</sup>	63.30 <sup>✓</sup>	
826	269.4 <sup>✓</sup>	277.1			$\frac{7.8}{2.7}$	7.7 <sup>✓</sup>	$\frac{7.8}{2.7}$	<del>35.61</del> 35.65 <sup>✓</sup>		
				12.1 <sup>✓</sup>				35.50 <sup>✓</sup>	15.78 <sup>✓</sup>	
+12	269.4 <sup>✓</sup>	276.8			$\frac{7.4}{2.6}$	7.4 <sup>✓</sup>	$\frac{8.6}{2.9}$	<del>35.38</del> 35.35 <sup>✓</sup>		
				27.9 <sup>✓</sup>			34.63 <sup>✓</sup>	35.78 <sup>✓</sup>		
+39.9	269.4 <sup>✓</sup>	276.5		$\frac{7.2}{2.55}$	7.1 <sup>✓</sup>	$\frac{8.3}{2.83}$	33.90 <sup>✓</sup>			
				20.1 <sup>✓</sup>			32.83 <sup>✓</sup>	29.44 <sup>✓</sup>		
								164.02 <sup>✓</sup>		

Chd. T.M.M.  
Calc. W.H.S.  
M.R.6

W.H.S.  
M.R.6

+60 268.5 ✓ 275.4

$\frac{6.8}{2.45}$  ✓

6.9 ✓

$\frac{7.4}{2.6}$

31.76 ✓

9.9 ✓

30.53 ✓

✓

11.19 ✓

+69.9 268.1 ✓ 274.6

$\frac{6.5}{2.38}$

6.5 ✓

$\frac{6.5}{2.38}$

29.31 ✓

29.8 ✓

28.71 ✓  
29.91 ✓

31.69 ✓  
33.01 ✓

+99.7 264.3 ✓ 270.8

$\frac{6.5}{2.38}$

6.5 ✓

$\frac{5.5}{2.25}$

28.12 ✓  
30.50 ✓

Pipe

30.3 ✓

29.91 ✓  
31.75 ✓

32.89 ✓  
35.63 ✓

827+30 259.3 ✓ 266.3

$\frac{7.0}{2.5}$  ✓

7.0 ✓

$\frac{6.0}{2.25}$

30.50 ✓  
33.00 ✓

Store

20 ✓

28.75 ✓  
30.00 ✓

21.30 ✓  
22.22 ✓

+50 255.9 ✓ 261.9

$\frac{6.0}{2.25}$

6.0 ✓

$\frac{6.0}{2.25}$

27.00 ✓

Wood

15 ✓

27.12 ✓

15.07 ✓

+65 253.4 ✓ 259.4

$\frac{7.0}{2.5}$  ✓

6.0 ✓

$\frac{5.2}{2.25}$

27.23 ✓

35 ✓

25.14 ✓

32.59 ✓

Chd. T. m. m.  
Calc. m. R.  
✓. w. H. S.

VALL.  
Mid.

149.77 144.73 ✓

828	247.6	253.1	$\frac{5.5}{2.25}$	5.5	$\frac{4.0}{2.25}$	23.06		
				10.3		21.66	8.26	
+10.3	245.8	250.4	$\frac{5.1}{2.25}$	4.6	$\frac{3.7}{2.25}$	20.25		
				29.4		23.62	25.72	
+39.7	239.7	245.7	$\frac{6.0}{2.25}$	6.0	$\frac{6.0}{2.25}$	27.00		
				17.3		32.35	20.73	
+57	234.6	242.6	$\frac{9.5}{3.13}$	8.0	$\frac{7.0}{2.5}$	37.69		
				11.5		35.15	14.97	
+68.5	231.3	238.9	$\frac{8.2}{2.8}$	7.6	$\frac{5.2}{2.25}$	32.62		
				30.4		33.01	37.17	
+72.1	230.7	238.2	$\frac{8.2}{2.8}$	7.5	$\frac{5.5}{2.25}$			

Pipe  
Stave  
Wood

238

Chd. T.M.M.  
Calc. - w.H.S.  
M.R.E  
Calc. M.D.S.  
VALL  
10.6.85 ex



8	+98.9	222.3 ✓	229.8		$\frac{8.0}{2.75}$ ✓	7.5	$\frac{6.3}{2.33}$ ✓	33.40 ✓		
				13.1 ✓					27.95 ✓	13.56 ✓
829+12		219.6 ✓	224.6		$\frac{5.0}{2.25}$ ✓	5.0	$\frac{5.0}{2.25}$ ✓	22.50 ✓		
				9. ✓					21.83 ✓	7.28 ✓
+21		217.8 ✓	222.5	Pipe		4.7		21.15 ✓		
				7.3 ✓					24.07 ✓	6.51 ✓
+28.3		216.3 ✓	222.3	Stave		6.0		27.00 ✓		
				29.7 ✓					29.38 ✓	<u>37.32</u> ✓ <del>32.92</del>
+58		212.9 ✓	219.9	Wood	$\frac{7.0}{2.15}$ ✓	7.0	$\frac{7.0}{2.15}$ ✓	31.75 ✓		
				7. ✓					29.37 ✓	7.61 ✓
+65		212.5 ✓	218.5			6.0		27.00 ✓		
				7. ✓					24.75 ✓	6.42 ✓
									Calc. M.R.G. ✓	73.70 ✓
									Calc. M.R.G. ✓	
									✓ - w.H.S.	

Chd. T.M.M.  
Calc. M.R.G.  
✓ - w.H.S.

Calc. M.R.G.

73.70 ✓

1/23/30  
 Clear + Cool.  
 Converse - Notes  
 Hill - Grades  
 Elliott - \*  
 Simpson - \*  
 Walton -

37

8	+72	212.2 ✓	217.2	5.0 ✓	
			16.1 ✓		
	+88.1	211.5 ✓	216.9	5.4 ✓	
			11.9 ✓		
830		211.5 ✓	217.5	6.0 ✓	
			15. ✓		
	+15	211.6 ✓	216.9	5.3	
			15. ✓		
	+30	211.6 ✓	217.6	6.0	
			20. ✓		
	+50	211.7 ✓	217.9	6.2	
			$\frac{6.2}{2.3}$	6.2	
			40. ✓		

Wood Stave Pipe

22.50 ✓		
23.40 ✓	13.95 ✓	
24.30 ✓		
25.65 ✓	11.31 ✓	
27.00 ✓		
25.43 ✓	14.13 ✓	
23.85 ✓		
25.42 ✓	14.12 ✓	
27.00 ✓		
27.46 ✓	20.34 ✓	
$\frac{6.2}{2.3}$	27.91 ✓	
28.61 ✓	42.39 ✓	
	116.24 ✓	

Chd. T.M.M.  
 calc. w. H.S.  
 M.R.E.

P.L.L.  
 M.R.E.

+90	211.7 <sup>✓</sup>	218.2	$\frac{6.5}{2.38}$ ✓	6.5 <sup>✓</sup>	$\frac{6.5}{2.38}$ ✓	29.31 <sup>✓</sup>		
				10.1 <sup>✓</sup>		27.03 <sup>✓</sup>	10.01 <sup>✓</sup>	
831	211.8 <sup>✓</sup>	217.3		5.5 <sup>✓</sup>		24.75 <sup>✓</sup>		
				15.1 <sup>✓</sup>		23.85 <sup>✓</sup>	13.25 <sup>✓</sup>	
+15	211.8 <sup>✓</sup>	216.9		5.1 <sup>✓</sup>		22.95 <sup>✓</sup>		
				5.1 <sup>✓</sup>		26.37 <sup>✓</sup>	4.88 <sup>✓</sup>	
+20	211.8 <sup>✓</sup>	218.4	$\frac{6.6}{2.4}$ ✓	6.6 <sup>✓</sup>	$\frac{6.6}{2.4}$ ✓	29.79 <sup>✓</sup>		
				30.1 <sup>✓</sup>		28.85 <sup>✓</sup>	32.06 <sup>✓</sup>	
+50	211.9 <sup>✓</sup>	218.1	$\frac{6.2}{2.3}$ ✓	6.2 <sup>✓</sup>	$\frac{6.2}{2.3}$ ✓	27.91 <sup>✓</sup>		
				5.1 <sup>✓</sup>		27.45 <sup>✓</sup>	5.08 <sup>✓</sup>	
+55	211.9 <sup>✓</sup>	217.9	$\frac{6.0}{2.25}$ ✓	6.0 <sup>✓</sup>	$\frac{6.0}{2.25}$ ✓	27.00 <sup>✓</sup>		
				10.1 <sup>✓</sup>		28.16 <sup>✓</sup>	10.43 <sup>✓</sup>	
						75.71 <sup>✓</sup>		

Wood Store Pipe

Chd. T.M.M.  
Calc. M.H.E.  
- W.H.S.

M.A.E.

+65	211.9 <sup>✓</sup>	218.4		$\frac{6.5}{2.38}$	6.5 <sup>✓</sup>	$\frac{6.5}{2.38}$	29.31 <sup>✓</sup>		
			35.✓					29.79 <sup>✓</sup>	38.62 <sup>✓</sup>
832	212.0 <sup>✓</sup>	218.7		$\frac{6.7}{2.43}$	6.7 <sup>✓</sup>	$\frac{6.7}{2.43}$	30.28 <sup>✓</sup>		
			50.✓					29.56 <sup>✓</sup>	54.74 <sup>✓</sup>
+50	212.1 <sup>✓</sup>	218.5		$\frac{6.4}{2.35}$	6.4 <sup>✓</sup>	$\frac{6.4}{2.35}$	28.84 <sup>✓</sup>		
			25.✓					27.92 <sup>✓</sup>	25.85 <sup>✓</sup>
+75	212.2 <sup>✓</sup>	218.2		$\frac{6.0}{2.25}$	6.0 <sup>✓</sup>	$\frac{6.0}{2.25}$	27.00 <sup>✓</sup>		
			10.✓					24.98 <sup>✓</sup>	9.25 <sup>✓</sup>
+85	212.2 <sup>✓</sup>	217.3		$\frac{5.1}{2.25}$	5.1 <sup>✓</sup>	$\frac{5.1}{2.25}$	22.95 <sup>✓</sup>		
			15.✓					23.90 <sup>✓</sup>	13.00 <sup>✓</sup>
833	212.2 <sup>✓</sup>	217.5			5.3 <sup>✓</sup>		23.85 <sup>✓</sup>		
			12.5.✓					25.88 <sup>✓</sup>	11.98 <sup>✓</sup>
								153.44 <sup>✓</sup>	

Chd. T.M.M.  
Calc - w. H.S.  
M.N.G.

ALL  
Calc M.N.G.  
153.44

+12.5 212.2<sup>✓</sup> 218.4 $\frac{6.2}{2.3}$  6.2<sup>✓</sup> $\frac{6.2}{2.3}$ 27.91<sup>✓</sup>37.5<sup>✓</sup>27.45<sup>✓</sup>38.13<sup>✓</sup>+50 214.4<sup>✓</sup> 220.4 $\frac{6.0}{2.25}$  6.0<sup>✓</sup> $\frac{6.0}{2.25}$ 27.00<sup>✓</sup>10.0<sup>✓</sup>27.00<sup>✓</sup>10.00<sup>✓</sup>+60 215.0<sup>✓</sup> 221.06.0<sup>✓</sup>27.00<sup>✓</sup>

Stare Pipe

10.0<sup>✓</sup>26.10<sup>✓</sup>9.67<sup>✓</sup>+70 215.6<sup>✓</sup> 221.2<sup>Top Pipe</sup>5.6 5.6<sup>✓</sup>5.6 25.20<sup>✓</sup>

Wood

30.0<sup>✓</sup>24.64<sup>✓</sup>27.38<sup>✓</sup>834 217.3<sup>✓</sup> 223.1<sup>Top Pipe</sup>5.0 5.8<sup>✓</sup>4.8 24.08<sup>✓</sup>12.5<sup>✓</sup>24.64<sup>✓</sup>11.41<sup>✓</sup>+12.5 218.1<sup>✓</sup> 224.1<sup>T. Pipe</sup>5.0 6.0<sup>✓</sup>5.4 25.20<sup>✓</sup>15.5<sup>✓</sup>25.43<sup>✓</sup>14.60<sup>✓</sup>Chd. T.M.M.  
Calc. M.H.S.  
W.H.S.P.C.L.  
M.H.S.11.19<sup>✓</sup>

+28 ✓ T. Pipe  
219.4 225.1

5.7 ✓ 5.7

5.7 25.65 ✓

7.0 ✓

27.52 ✓ 7.13 ✓

+35 ✓  
220.0 226.9

$\frac{6.3}{2.33}$  ✓ 6.9

$\frac{6.0}{2.25}$  29.40 ✓

15.0 ✓

27.92 ✓ 15.51 ✓

+50 ✓  
221.2 227.3

$\frac{6.0}{2.25}$  6.1

$\frac{5.3}{2.25}$  26.44 ✓

40.0 ✓

26.61 ✓ 39.42 ✓

+90 ✓  
224.6 230.8

$\frac{6.2}{2.3}$  ✓ 6.2

$\frac{5.2}{2.25}$  26.78 ✓

14.7 ✓

28.53 ✓ 15.53 ✓

835 +04.7 ✓  
225.8 232.5

$\frac{6.7}{2.43}$  ✓ 6.7

$\frac{6.7}{2.43}$  30.28 ✓

15.3 ✓

28.64 ✓ 16.23 ✓

+20 ✓  
227.7 233.7

$\frac{6.0}{2.25}$  6.0

$\frac{6.0}{2.25}$  27.00 ✓

14.5 ✓

26.33 ✓ 14.14 ✓

Chd. T.M.M.  
Calc. m.R.E.

A.L.L.  
107.96 ✓  
~~108.46~~

+34.5 ✓	229.5 ✓	235.2		$\frac{5.7}{2.25}$ ✓	5.7 ✓	$\frac{5.7}{2.25}$ ✓	25.65 ✓		
			15.5 ✓				24.30 ✓	13.95 ✓	
+50	232.6 ✓	237.7			5.1 ✓		22.95 ✓		
			13.9 ✓				22.50 ✓	11.58 ✓	
+63.9 ✓	235.4 ✓	240.3			4.9 ✓		22.05 ✓		
			18.1 ✓				21.60 ✓	14.98 ✓	
+82	240.5 ✓	245.2			4.7 ✓		21.15 ✓		
			10.8 ✓				20.93 ✓	8.37 ✓	
+92.8	243.6 ✓	248.2			4.6 ✓		20.70 ✓		
			22.2 ✓				21.37 ✓	17.58 ✓	
836+15	251.7 ✓	256.6			4.9 ✓		22.05 ✓		
			5.9 ✓				23.01 ✓	5.03 ✓	
								70.99 ✓	

Chd. T.M.M.

Calc. W.H.S.

M.A.E.

P.A.L.L.

+20.9	253.9 ✓	259.3		$\frac{5.4}{2.25}$ ✓	5.4 ✓	$\frac{5.1}{2.25}$ ✓	23.96 ✓		
								✓	✓
			16.3 ✓					22.44 ✓	13.55 ✓

+37.2	260.6 ✓	265.4		$\frac{5.1}{2.25}$ ✓	4.8 ✓	$\frac{3.9}{2.25}$ ✓	20.93 ✓		
								✓	✓
			13.8 ✓					22.00 ✓	11.24 ✓

+51	265.7 ✓	270.9	Stave Pipe	$\frac{6.0}{2.25}$ ✓	5.2 ✓	$\frac{4.1}{2.25}$ ✓	23.06 ✓		
				14.4 ✓					✓
								24.06 ✓	12.83 ✓

+65.4	270.9 ✓	276.6	Wood	$\frac{6.4}{2.25}$ ✓	5.7 ✓	$\frac{4.5}{2.25}$ ✓	25.07 ✓		
				14.6 ✓					✓
								26.33 ✓	14.24 ✓

+80	274.9 ✓	281.1		$\frac{6.6}{2.4}$ ✓	6.2 ✓	$\frac{5.5}{2.25}$ ✓	27.58 ✓		
								✓	✓
			14.3 ✓					26.61 ✓	14.09 ✓

+94.3	278.9 ✓	284.7		$\frac{5.8}{2.25}$ ✓	5.8 ✓	$\frac{5.4}{2.25}$ ✓	25.65 ✓		
			15.7 ✓					✓	✓
								27.97 ✓	16.26 ✓

Chd. T.M.M.  $\frac{1.45}{1.45}$  ✓  
 Calc. - w. H.S.  $\frac{1.45}{1.45}$  ✓  
 M.A.E.  $\frac{1.45}{1.45}$  ✓  
 67.40 82.21 ✓



+95.7 279.2 285.2  $\frac{6.0}{2.25}$  6.0  $\frac{5.6}{2.25}$

44.3 ✓

837+10 281.9 ✓ 288.6  $\frac{6.7}{2.43}$  6.7 ✓  $\frac{6.7}{2.43}$  30.28 ✓

15.2 ✓

27.06 ✓ 15.23 ✓

+25.2 284.9 ✓ 290.2  $\frac{5.3}{2.25}$  5.3 ✓  $\frac{5.3}{2.25}$  23.85 ✓

11.8 ✓

~~25.13~~ ✓ ~~10.99~~ ✓  
~~25.05~~ ✓ ~~10.95~~ ✓

+37 286.3 ✓ 292.3  $\frac{6.0}{2.25}$  6.0 ✓  $\frac{5.5}{2.25}$  26.44 ✓

18. ✓

24.75 ✓ 16.50 ✓

+55 288.4 ✓ 293.6  $\frac{5.4}{2.25}$  5.2 ✓  $\frac{4.7}{2.25}$  23.06 ✓

10. ✓

23.73 ✓ 8.79 ✓

+65 289.2 ✓ 294.8  $\frac{5.6}{2.25}$  5.6 ✓  $\frac{4.9}{2.25}$  24.41 ✓

35. ✓

22.84 ✓ 29.61 ✓

Chd. T.M.M.

calc. - w. H.S.

M.R.E

A.L.L.

M.R.S

81.12 ✓

Star Pipe

Wood

838	292.0	296.9		$\frac{4.7}{2.25}$	4.9	$\frac{4.4}{2.25}$	21.26 ✓		
			20. ✓					21.43 ✓	15.87 ✓
+20	293.6	298.4		$\frac{4.8}{2.25}$	4.8 ✓	$\frac{4.8}{2.25}$	21.60 ✓		
			5. ✓					20.02 ✓	3.71 ✓
+25	294.0	298.1	Pipe	$\frac{4.1}{2.25}$	4.1 ✓	$\frac{4.1}{2.25}$	18.45 ✓		
			5 Stave						
			10. ✓					18.68 ✓	6.92 ✓
+35	294.8	299.0	Pipe	4.2 ✓	4.2	4.2	18.90 ✓		
			Wood						
			29.8 ✓					21.88 ✓	29.15 ✓
+64.8	298.5	304.0		6.0	5.5 ✓	5.1	24.86 ✓		
			11.2 ✓					26.10 ✓	10.83 ✓
+76	300.4	306.9		6.0	6.5 ✓	5.3	27.34 ✓		
			12. ✓					26.72 ✓	11.88 ✓

Chd. T.M.M.  
 calc. - w.H.S.  
 M.A.S.  
 ALL.  
 M.A.S.A.  
 73.36

+88 302.4<sup>✓</sup> 308.4 6.0 6.0 5.2 26.10<sup>✓</sup>  
 5. ✓ 27.07<sup>✓</sup> 5.01<sup>✓</sup>

+93 303.2<sup>✓</sup> 309.4  $\frac{6.0}{2.25}$  6.2  $\frac{6.5}{2.38}$  28.03<sup>✓</sup>  
 7. ✓ 26.16<sup>✓</sup> 6.78<sup>✓</sup>

839 304.4<sup>✓</sup> 309.8 5.4 5.4 5.4 24.30<sup>✓</sup>  
 4. ✓ 24.53<sup>✓</sup> 3.63<sup>✓</sup>

+04 304.8<sup>✓</sup> 310.3 5.5 5.5 5.5 24.75<sup>✓</sup>  
 6. ✓ 27.22<sup>✓</sup> 6.05<sup>✓</sup>

+10 305.5<sup>✓</sup> 312.7  $\frac{6.0}{2.25}$  7.2  $\frac{6.0}{2.25}$  29.70<sup>✓</sup>  
 10. ✓ 31.07<sup>✓</sup> 11.51<sup>✓</sup>

+20 306.6<sup>✓</sup> 314.3  $\frac{6.7}{2.43}$  7.7  $\frac{6.5}{2.38}$  32.44<sup>✓</sup>  
 10. ✓ 29.05<sup>✓</sup> 10.76<sup>✓</sup>  
~~10.77~~

Chd. T.M.M.  
 Calc. w.H.S.  
 M.A.E  
 M.A.E  
 43.74<sup>✓</sup>

+30 307.6 313.3 5.7 5.7 5.7 25.65 ✓

20. ✓

26.32 ✓ 19.50 ✓

+50 309.8 315.8 6.0 6.0 6.0 27.00 ✓

20. ✓

25.88 ✓ 19.27 ✓

+70.1 312.0 317.5 5.5 5.5 5.5 24.75 ✓

Pipe  
Stairc  
Wood

19.9 ✓

24.52 ✓ 18.07 ✓

+90 313.3 318.7 5.4 5.4 5.4 24.30 ✓

10. ✓

25.65 ✓ 9.50 ✓

840. 314.0 320.0 6.0 6.0 6.0 27.00 ✓

10. ✓

23.85 ✓ 8.83 ✓

+10 313.9 318.5 4.6 4.6 4.6 20.70 ✓

20. ✓

21.26 ✓ 15.75 ✓

Chd. T.M.M.  
calc. - w.H.S.  
M.O.S.

90.92 ✓

+30	313.6	318.2		$\frac{5.6}{2.25}$	4.6	$\frac{4.6}{2.25}$	21.82		
			12.					24.70	10.98
+42	313.0	319.4		$\frac{6.4}{2.35}$	6.4	$\frac{5.3}{2.25}$	27.58		
			33.					28.65	35.02
+75	311.3	318.1		$\frac{7.3}{2.58}$	6.8	$\frac{5.4}{2.25}$	29.72		
			8.					27.69	8.20
+83	310.9	316.6			5.7		25.65		
			11.					26.10	10.63
+94	310.3	316.2			5.9		26.55		
			6.					24.02	5.34
841	310.0	314.4		$\frac{5.9}{2.25}$	4.4	$\frac{4.4}{2.25}$	21.49		
			12.					23.37	10.39
								80.56	

Chd. T.M.M.  
calc. w.H.S.  
M.R.R.

ACL.

+12 309.4 ✓ 314.9 ✓  $\frac{7.0}{2.5}$  ✓ 5.5 ✓ 4.5 25.25 ✓

30 ✓

24.10 ✓ 2.68 ✓

+15 309.2 ✓ 314.3 ✓ 5.1 ✓ 22.95 ✓

35 ✓

24.97 ✓ 32.37 ✓

+50 307.4 ✓ 313.4 ✓ 6.0 ✓ 27.00 ✓

50 ✓

27.63 ✓ 26.13 ✓ 54.87 ✓

842 304.8 ✓ 311.9 ✓  $\frac{7.1}{2.53}$  ✓ 7.1 ✓ 7.1  $\frac{7.1}{2.53}$  ✓ 32.26 ✓

50 ✓

27.83 ✓ 51.54 ✓

+50 305.7 ✓ 310.9 ✓ 5.2 ✓ 23.40 ✓

30 ✓

26.12 ✓ 29.02 ✓

+80 306.2 ✓ 312.6 ✓  $\frac{6.4}{2.35}$  ✓ 6.4 ✓ 6.4  $\frac{6.4}{2.35}$  ✓ 28.84 ✓

20 ✓

27.47 ✓ 20.35 ✓

Chd. T.M.M. calc. - w.H.S. 190.83 ✓  
~~200.83~~

Wood Stave Pipe

843	306.6 <sup>✓</sup>	312.4		5.8 <sup>✓</sup>		26.10 <sup>✓</sup>		
			12.0 <sup>✓</sup>				30.21 <sup>✓</sup>	13.43 <sup>✓</sup>
+12	306.8 <sup>✓</sup>	314.3		$\frac{7.5}{2.63}$ <sup>✓</sup>	7.5 <sup>✓</sup>	$\frac{7.5}{2.63}$ <sup>✓</sup>	34.32 <sup>✓</sup>	
			Pipe 38.0 <sup>✓</sup>				33.03 <sup>✓</sup>	46.49 <sup>✓</sup>
+50	307.5 <sup>✓</sup>	314.5		$\frac{7.0}{2.5}$ <sup>✓</sup>	7.0 <sup>✓</sup>	$\frac{7.0}{2.5}$ <sup>✓</sup>	31.75 <sup>✓</sup>	
			Stair 32.0 <sup>✓</sup>				30.53 <sup>✓</sup>	36.18 <sup>✓</sup>
+82	307.6 <sup>✓</sup>	314.1		$\frac{6.5}{2.38}$ <sup>✓</sup>	6.5 <sup>✓</sup>	$\frac{6.5}{2.38}$ <sup>✓</sup>	29.31 <sup>✓</sup>	
			Wood 5.0 <sup>✓</sup>				32.37 <sup>✓</sup>	5.99 <sup>✓</sup>
+87	307.6 <sup>✓</sup>	315.9		$\frac{7.3}{2.58}$ <sup>✓</sup>	8.3 <sup>✓</sup>	$\frac{7.0}{2.5}$ <sup>✓</sup>	35.43 <sup>✓</sup>	
			13.0 <sup>✓</sup>				34.84 <sup>✓</sup>	16.77 <sup>✓</sup>
844	307.6 <sup>✓</sup>	315.6		$\frac{7.6}{2.65}$ <sup>✓</sup>	8.0 <sup>✓</sup>	$\frac{6.4}{2.35}$ <sup>✓</sup>	34.25 <sup>✓</sup>	
			8.0 <sup>✓</sup>				32.13 <sup>✓</sup>	9.52 <sup>✓</sup>

Chd. T.M.M.

calc - w. H.S.

✓ M.D.E.

✓ A.C.L.

128.38 ✓

+08 307.7 314.7

$\frac{6.4}{2.35}$  7.0

$\frac{6.2}{2.3}$  30.00 ✓

9.0

26.47 ✓ 8.82 ✓

+17 307.7 312.8

5.1 5.1

5.1 22.95 ✓

25.0

21.38 ✓ 19.80 ✓

+42 307.8 312.2

4.4 4.4

4.4 19.80 ✓

5.0

24.60 ✓ 4.56 ✓

+47 307.8 314.7

$\frac{6.3}{2.33}$  6.9

$\frac{6.0}{2.25}$  29.40 ✓

7.0

28.48 ✓ 7.38 ✓

+54 307.8 314.3

$\frac{6.0}{2.25}$  6.5

$\frac{5.5}{2.25}$  27.56 ✓

6.0

24.35 ✓ 5.41 ✓

+60 307.8 312.5

4.7 4.7

4.7 21.15 ✓

6.0

23.75 ✓ 5.28 ✓

Chd. T.M.M.  
calc. w. H.S.  
✓ M.D.E.

51.25 ✓

32



+66 307.8 ✓ 313.9

$\frac{7.1}{2.53}$  ✓ 6.1 ✓

$\frac{4.1}{2.25}$  ✓ 26.34 ✓

10.0 ✓

24.59 ✓ 9.11 ✓

+76 307.9 ✓ 313.3

$\frac{6.0}{2.25}$  ✓ 5.4 ✓

$\frac{3.5}{2.25}$  ✓ 22.84 ✓

11.0 ✓

25.86 ✓ 10.54 ✓

+87 307.9 ✓ 314.8

$\frac{6.7}{2.43}$  ✓ 6.9 ✓

$\frac{5.1}{2.25}$  ✓ 28.88 ✓

Pipe  
Stave  
Wood

6.0 ✓

29.53 ✓  
29.02 ✓ 6.56 ✓

+93 307.9 ✓ 315.1

$\frac{6.8}{2.45}$  ✓ 7.2 ✓

$\frac{5.5}{2.25}$  ✓ 30.16 ✓

12.0 ✓

25.99 ✓ 11.55 ✓

845 +05 308.0 ✓ 313.0

$\frac{4.4}{2.25}$  ✓ 5.0 ✓

$\frac{5.0}{2.25}$  ✓ 21.82 ✓

7.0 ✓

22.50 ✓ 5.83 ✓

+12 308.0 ✓ 313.6

$\frac{4.2}{2.25}$  ✓ 5.6 ✓

$\frac{5.2}{2.25}$  ✓ 23.18 ✓

8.0 ✓

21.07 ✓ 6.23 ✓  
49.82 ✓

Chd. T.M.M.  
Calc. w.H.S.  
- M.R.E

+20	308.0	312.2	4.2	4.2	4.2	18.90 ✓		
			6.0				21.71 ✓	4.82 ✓
+26	308.0	314.0	$\frac{5.0}{2.25}$ ✓	6.0	$\frac{4.8}{2.25}$ ✓	24.52 ✓		
			24.0				24.13 ✓	21.45 ✓
+50	308.1	313.9	$\frac{4.8}{2.25}$ ✓	5.8	$\frac{4.7}{2.25}$ ✓	23.74 ✓		
			12.0				25.37 ✓	11.28 ✓
+62	307.2	313.9	$\frac{5.0}{2.25}$ ✓	6.7	$\frac{5.6}{2.25}$ ✓	27.00 ✓		
			8.0				22.00 ✓	6.52 ✓
+70	306.6	310.2	$\frac{4.3}{2.25}$ ✓	3.6	$\frac{3.6}{2.25}$ ✓	16.99 ✓		
			8.0				23.00 ✓	6.81 ✓
+78	306.0	312.9	$\frac{6.0}{2.25}$ ✓	6.9	$\frac{6.0}{2.25}$ ✓	29.02 ✓		
			17.0				28.91 ✓	18.20 ✓

Chd. T.M.M.  
 C910-w.H.S.  
 ✓ M.B.S.

✓ P.C.L.  
 69.08 ✓

+95 304.7 311.5

$\frac{6.0}{2.25}$

6.8

$\frac{6.0}{2.25}$

28.80 ✓

29.9 ✓

29.42 ✓

32.58 ✓

846+24.9 301.4 308.0

$\frac{7.4}{2.6}$

6.6

$\frac{6.0}{2.25}$

30.04 ✓

29.5 ✓

30.83 ✓

33.68 ✓

+544 296.1 303.3

$\frac{7.5}{2.63}$

7.2

$\frac{6.0}{2.25}$

31.62 ✓

26.4 ✓

36.31 ✓

35.50 ✓

+80.8 290.4 299.1

$\frac{8.7}{2.93}$

8.7

$\frac{8.7}{2.93}$

40.99 ✓

10.2 ✓

40.76 ✓

15.40 ✓

+91 288.6 297.4

$\frac{8.8}{2.95}$

8.8

$\frac{8.1}{2.78}$

40.53 ✓

9.0 ✓

37.95 ✓

12.65 ✓

847 287.0 294.7

$\frac{7.7}{2.68}$

7.7

$\frac{7.7}{2.68}$

35.38 ✓

10.4 ✓

33.32 ✓

12.83 ✓

142.64 ✓

Chd. T.M.M.  
care - w. H.S.  
✓ M.D.S.

Wood Stake Pipe

+10.4 285.2 292.2

 $\frac{7.2}{2.55}$ 

7.0

 $\frac{6.4}{2.35}$ 

31.25

14.6

27.55 14.90

+25 283.6 288.9

5.3

23.85

15.2

23.85 13.43

+40.2 281.9 287.2

5.3

23.85

Pipe

14.8

25.42 13.93

+55 281.3 287.3

6.0

27.00

Stave

15.2

28.16 15.85

Wood

+70.2 280.7 287.2

 $\frac{6.5}{2.38}$ 

6.5

 $\frac{6.5}{2.38}$ 

29.31

29.8

32.34 35.69

248 280.5 288.2

 $\frac{7.7}{2.68}$ 

7.7

 $\frac{7.7}{2.68}$ 

35.38

16.0

33.57 19.89  
A.L.L.  
113.69Chd. T.M.M.  
Calc. by H.S.  
M.D.E.

+16 280.4 ✓ 287.4

$\frac{7.0}{2.5}$  ✓

7.0 ✓

$\frac{7.0}{2.5}$  ✓

31.75 ✓

39.0 ✓

30.29 ✓ 43.75 ✓

+55 280.1 ✓ 286.5

$\frac{6.4}{2.35}$  ✓

6.4 ✓

$\frac{6.4}{2.35}$  ✓

28.84 ✓

20.0 ✓

25.45 ✓ 18.85 ✓

+75 280.0 ✓ 284.9

4.9

4.9 ✓

4.9

22.05 ✓

Pipe  
Stave  
Wood

10.0 ✓

25.21 ✓ 9.34 ✓

+85 277.2 ✓ 283.8

$\frac{6.3}{2.33}$  ✓

6.3 ✓

$\frac{6.3}{2.33}$  ✓

28.37 ✓

10.0 ✓

29.32 ✓ 10.86 ✓

+95 274.3 ✓ 281.0

$\frac{6.7}{2.43}$  ✓

6.7 ✓

$\frac{6.7}{2.43}$  ✓

30.28 ✓

22.0 ✓

30.77 ✓ 35.07 ✓

849 +17 268.1 ✓ 275.0

$\frac{6.9}{2.48}$  ✓

6.9 ✓

$\frac{6.9}{2.48}$  ✓

31.26 ✓

33.0 ✓

25.53 ✓  
20.53 ✓  
P.A.C.L.  
31.20 ✓  
139.07 ✓

Chd. T.M.M.  
calc. w. H.S.  
M.A.E.

+50 258.7 263.1

4.4

19.80 ✓

17.0 ✓

19.80 ✓ 17.47 ✓

+67 253.9 258.3

4.4

19.80 ✓

15.0 ✓

20.48 ✓ 11.38 ✓

+82 249.7 254.4

4.7

21.15 ✓

13.0 ✓

25.95 ✓ 12.49 ✓

+95 246.0 252.8

6.8  
2.45 ✓ 6.8

6.8  
2.45 ✓ 30.76 ✓

15.0 ✓

27.98 ✓ 15.54 ✓

850+10 245.7 251.3

5.6

25.20 ✓

15.0 ✓

24.98 ✓ 13.88 ✓

+25 245.3 250.8

5.5

24.75 ✓

25.0 ✓

22.50 ✓ 20.83 ✓  
86.59 ✓

Chd. T.M.M.  
calc - w. H.S.  
- m. 08

+50 244.7 249.2 4.5 ✓

20.25 ✓

50.0 ✓

20.70 ✓ 38.33 ✓

851 243.6 ✓ 248.3 4.7 ✓

50.0 ✓

21.15 ✓

23.62 ✓ 43.74 ✓

+50 242.4 ✓ 248.2 5.8 ✓

50.0 ✓

26.10 ✓

28.93 ✓ 21.43 ✓

20.0 ✓

+70 241.9 ✓ 248.9 7.0 ✓  
2.0  
2.5 ✓

31.75 ✓  
7.0  
2.5 ✓

5.0 ✓

29.67 ✓ 5.49 ✓

+75 241.8 ✓ 247.3 7.5 ✓  
2.63 ✓ 7.5  
1.5 5.5 ✓  
1.0 5.5 ✓

27.60 ✓  
6.0  
2.25 ✓

8.0 ✓

29.31 ✓ 8.68 ✓

+83 241.6 ✓ 248.0 7.9 ✓  
2.73 ✓ 8.0  
1.5 6.6 ✓  
1.0 6.4 ✓

31.01 ✓  
6.4  
2.35 ✓

2.0 ✓

Chd. T.M.M. 29.23 ✓ 2.17 ✓  
A.C.L.  
Calc. w. H.S. 119.84 ✓  
M. D. 8

+85 241.6 247.7

$\frac{6.1}{2.28}$

6.1

$\frac{6.1}{2.28}$

27.45

11.0

29.10

11.86

+96 241.3 248.1

$\frac{6.8}{2.45}$

6.8

$\frac{6.8}{2.45}$

30.76

4.0

27.08

4.01

852 241.2 246.4

5.2

23.40

10.0

23.18

8.59

+10 241.0 246.1

5.1

22.95

10.0

19.80

7.33

+20 244.2 247.9

3.7

16.65

10.0

20.25

7.50

+30 247.4 252.7

5.3

23.85

8.0

26.46

7.84

Chd. Tm. M.

Calc. w. H.S.

M.R. 8

47.13



+38 250.0<sup>✓</sup> 255.8 $\frac{8.5}{2.88}$  5.8<sup>✓</sup> $\frac{5.8}{2.25}$  29.07<sup>✓</sup>10.0<sup>-</sup>~~28.85~~<sup>✓</sup>29.11<sup>✓</sup>10.69<sup>✓</sup>+48 253.3<sup>✓</sup> 258.8 $\frac{8.6}{2.9}$   $\frac{8.4}{2.3}$   $\frac{6.5}{1.6}$  5.5<sup>✓</sup> $\frac{6.5}{2.38}$ ~~28.64~~<sup>✓</sup>29.16<sup>✓</sup>19.0<sup>-</sup>~~29.60~~<sup>✓</sup>29.92<sup>✓</sup>20.87<sup>✓</sup>+67 259.4<sup>✓</sup> 264.7 $\frac{10.0}{3.25}$   $\frac{10.0}{3.0}$   $\frac{7.0}{2.3}$  5.3<sup>✓</sup> $\frac{6.3}{1.5}$   $\frac{9.5}{2.30}$   $\frac{9.5}{3.73}$ 30.68<sup>✓</sup>8.0<sup>-</sup>32.59<sup>✓</sup>~~32.00~~<sup>✓</sup>32.53<sup>✓</sup>9.66<sup>✓</sup>~~9.18~~<sup>✓</sup>+75 262.0<sup>✓</sup> 268.3 $\frac{10.4}{3.35}$   $\frac{10.4}{2.4}$   $\frac{7.5}{2.0}$  6.3<sup>✓</sup> $\frac{7.1}{1.7}$   $\frac{9.1}{3.03}$ ~~35.33~~<sup>✓</sup>34.38<sup>✓</sup>~~34.51~~<sup>✓</sup>32.74<sup>✓</sup>~~31.65~~<sup>✓</sup>32.18<sup>✓</sup>29.85<sup>✓</sup>~~30.23~~<sup>✓</sup>25.0<sup>-</sup>853 272.2<sup>✓</sup> 278.2 $\frac{9.8}{3.2}$   $\frac{9.6}{2.8}$   $\frac{6.2}{2.0}$  6.0<sup>✓</sup> $\frac{7.0}{2.2}$   $\frac{9.0}{3.0}$ 29.97<sup>✓</sup>25.0<sup>-</sup>~~32.73~~<sup>✓</sup>34.65<sup>✓</sup>30.39<sup>✓</sup>30.31<sup>✓</sup>+25 282.4<sup>✓</sup> 289.7 $\frac{9.0}{3.0}$   $\frac{8.4}{2.5}$   $\frac{6.9}{2.0}$  7.3<sup>✓</sup> $\frac{8.5}{2.0}$   $\frac{8.6}{2.9}$ ~~35.50~~<sup>✓</sup>39.33<sup>✓</sup>

Chd. T.M.M.

~~32.85~~<sup>✓</sup>

A.C.L.

30.43<sup>✓</sup>

Calc. M.R.E.

34.77<sup>✓</sup>~~132.34~~<sup>✓</sup>131.80<sup>✓</sup>25.0<sup>-</sup>

+50 293.6 299.7

$$\frac{8.5}{2.88} \frac{8.1}{2.5} \frac{6.4}{1.7} \frac{6.1}{1.7}$$
 $\frac{7.4}{2.6}$ 

30.22 ✓

1.0 ✓

31.69 ✓

1.17 ✓

+51 294.0 301.4

$$\frac{8.4}{2.85} \frac{8.1}{2.5} \frac{6.3}{2.0} \frac{7.4}{2.0}$$
 $\frac{7.7}{2.68}$ 

33.16 ✓

11.0 ✓

33.22 ✓

13.53 ✓

+62 299.0 306.3

 $\frac{7.3}{2.58}$ 

7.3 ✓

 $\frac{7.3}{2.58}$ 

33.28 ✓

10.4 ✓

34.59 ✓

13.32 ✓

+72.4 303.6 311.4

 $\frac{7.8}{2.7}$ 

7.8 ✓

 $\frac{7.8}{2.7}$ 

35.91 ✓

13.9 ✓

31.01 ✓

15.96 ✓

+86.3 309.3 315.1

5.8 ✓

5.8 ✓

5.8 ✓

26.10 ✓

Wood Stave Pipe

8.7 ✓

25.87 ✓

8.34 ✓

+95 312.1 317.8

5.7 ✓

25.65 ✓

5.6 ✓

22.73 ✓

4.71 ✓

 Chd. T.M.M.  
 Calc. M.D.B.

57.03 ✓

854+00.6 314.0 ✓ 318.4

4.4 ✓

19.80 ✓

14.5 ✓

19.57 ✓ 10.51 ✓

+15.1 317.6 ✓ 321.9

4.3 ✓

19.35 ✓

4.9 ✓

21.38 ✓ 388 ✓  
4.02

+20 318.4 ✓ 323.6

5.2 ✓

23.40 ✓

Pipe  
Stave

9.9 ✓

22.50 ✓ 8.25 ✓

+29.9 320.2 ✓ 325.0

4.8 ✓

21.60 ✓

Wood

20.1 ✓

21.99 ✓ 16.37 ✓

+50 322.0 ✓ 327.9

5.7

4.9 ✓

4.4

22.39 ✓

16.0 ✓

21.38 ✓ 12.67 ✓

+66 325.2 ✓ 329.5

5.2

4.3 ✓

4.3

20.36 ✓

9.0 ✓

Chd. M. M.

Calc M. M. B.

21.80 ✓ 7.27 ✓  
V.R.C.L.59.13  
58.95 ✓

337.0  
E-1 330.6  
855 + 03 = 58

339.35  
1.85  
341.20  
5.6  
335.6

+75 326.5 ✓ 330.7

7.3 6.8 4.2 4.2 ✓  
2.58 1.0 0.5

4.2 ✓  
2.25 23.24

15.0 :

+90 328.6 ✓ 333.8

7.1 ✓  
2.53 5.2

4.0  
2.25

24.07 ✓  
24.04

23.64 ✓ 13.13 ✓

Wood Store Pipe

10.0 :

855 Revised → 329.5 ✓  
330.1 334.6

5.4 ✓  
4.0 5.1 ✓  
2.25 4.5

3.4  
4.0  
2.25

20.03 ✓  
22.72

20.03 ✓  
23.38 7.42 ✓

3.5 ✓  
12.05  
8.55 ✓

19.57 ✓

19.80 ✓  
2.57 ✓  
28.38  
25.91 ✓ 8.21 ✓

+12.05 330.6 ✓ 336.9  
337.8

7.8  
8.7  
2.95  
2.70

5.8  
6.7  
2.45  
2.25

32.26 ✓  
34.04

VAL. 33.22  
31.33 ✓

End Schedule #1.

855 + 035 330.6 335.0

5.3  
2.25

3.3  
2.25

19.57

Total cu. Yds. in  
Book 293 = 6170.40 ✓ P.C.L.  
additions not checked.

Figured  
Twice P.C.L.  
with  
6170.40  
Additions checked  
in the Book  
10/18/30 J.M.M.

Chd. T.M.M.  
Calc. M.R.B.

11/21/30 P.B.  
59

Summary  
Excavation - 2nd Main Pip Line

Book No	Page	Cuyards Excavation	
285	77	10,034. <sup>02</sup>	- 6.55 cu yds
286	79	13,292. <sup>24</sup>	
287	78	15,304. <sup>02</sup>	
288	71	10,196. <sup>86</sup>	
289	78	8,946. <sup>48</sup>	
289A	10	2,968. <sup>13</sup>	
290	73	8,741. <sup>25</sup>	
291	44	11,343. <sup>34</sup>	
292	79	12,545. <sup>22</sup>	
293	58	6,170. <sup>40</sup>	
		99,541. <sup>96</sup>	
		Add (see note) 1,429. <sup>24</sup>	
		<u>100,971.<sup>20</sup></u>	
		Excavated by City Forces 6.55	
		<u>Total Excavation 100,964.<sup>65</sup></u>	cu yds

Note. All trench excavation computations in these field books 285-293 inclusive are based on width of trench taken inside diameter of pipe + 18". Correction to be added because outside diameter of pipe should have been used as basis for width of trench computation, Total 54" trench (page 69) =  $44,547.81 \times \frac{55}{54} = 45,372.74$  cu yds, an addition of 824.93 cu yds. Total of 58" trench (page 69) =  $35,051.<sup>10</sup> \times \frac{59}{58} = 35,655.<sup>41</sup>$ , an addition of 604.31 cu yds, total addition to be made because of 1" additional width  $604.31 + 824.93 = 1,429.24$  cu yds.

Note. For Backfill summary see Page 61.

Areas of Western Pipe & Steel  
Company backfill to be used for  
Computations of final backfill schedule I



$$4.5 \times 2.0417 = 9.18765$$

$$\text{segment} = 4.52683$$

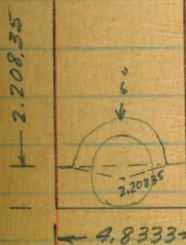
$$54'' \text{ Trench } 13.71448$$

$$+ 1'' \quad .17007$$

$$55'' \text{ Trench} = 13.88455 \text{ sq. ft.}$$

The above calc. by A.C.L. copied from  
original sheets by M.D.C. 4/25/30.

Calculations of Area by P.B. = 13.8843 sq. ft.



$$4.8333 \times 2.20835 = 10.67362$$

$$\text{segment} \quad 5.47115$$

$$58'' \text{ Trench } 16.14477$$

$$+ 1'' \quad .18402$$

$$59'' \text{ Trench} = 16.32879$$

The above calc. by A.C.L. copied from  
original sheets by M.D.C. 4/25/30.

Calculations of Above area by P.B. = 16.32875 sq. ft.

Otay Res. San Diego 2nd Main Pipeline

Backfill Schedule I

61

Nov. 13, 1930.

Summary.

55" Trench backfill (page 69)	23,891.41 C.Y.
59" Trench backfill (page 69)	15,888.07
Portal Cuts backfill (page 70)	2,013.68
Deep Cuts backfill (page 68)	2,459.58

Total backfill Schedule I 44,252.74 C.Y.

checked Main Office 11/21/30 P.B.

Olay Reservoir San Diego 2nd Main Pipe Line  
Pavement Replaced Schedule I

Oct 21, 1930 LV

These notes taken  
from City Street Insp. Davis's  
final report & by M.R.G.  
11/24/30

St. Name	Sta.	Mile	Kind	Sq. Feet Relaid	OK'd for Estimate	Sq. Feet of 4x4 Mesh
54th St.	817+02	15.5	Concrete	201.	201.	402.
Brdway.	754+39	14.3	Concrete	558.	558.	1116.
Ridge Way	652+51	12.4	Concrete	1000.	300.	592.
Bonita Ave.	470+23	8.9	"	224.	224.	448.
Bach Ave.	704+09	13.3	"	533.	533.	1066.
Imperial	678+51	12.9	Asphalt	160 base 261 top	Ave. 210	—
65th St.	683+72	13.0	"	194 base 211 top	Ave. 203	—
Overlap of steel mesh total						226
						2229

3850  
253  
4103  
Ave. \*

Extra W.O. #3 - 264 Sq. ft. concrete sidewalk Imperial Ave.

Extra W.O. #2 - 4103 Sq. ft. 4x4" steel mesh

Extra W.O. #1 - Excavation at Sta. 525+00 \$38.75

Summary

E.W.O. #1 - Excavation at sta 525+00 = \$38.75

E.W.O. #2 - 4103 sq' of 4x4" Mesh @ \$.0721 = 295.82

E.W.O. #3 - 264 sq' of sidewalk @ \$.20 = 52.80

\$387.37

+ 15% of \$387.57 = 58.10

Pavement relaid 2229 sq' @ \$.45 = 1003.05

\$1448.52

\* Note: on steel mesh, prior agreement between contractor & main office was on basis of 3 rolls of 4"x4" mesh 7' wide & 200' long = 4200 sq' at \$.0521 sq' + \$.02 per sq' for footage that was to be laid, balance not laid to be taken into stock of Department at equivalent price of mesh in place

4200 sq' in 3 rolls

- 3850 sq' laid

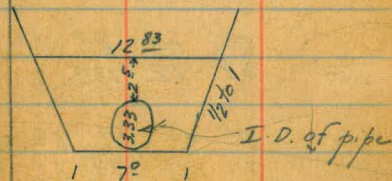
350 sq' Bal. not laid but delivered to Chollas 10/27/30

$\frac{350 \times .0521}{.0721} = 253$  sq' at equivalent price of mesh in place



Book #	Sta. to Sta.	Excavation	W.P. & Steel Co. Backfill	Hazard Co. Backfill
293	855+12 <sup>05</sup> 790+09 <sup>4</sup>	6,170.4	6,617.5 x 13.9445 = 3,417.69	2,752.71
292	790+09 <sup>8</sup> 680+17 <sup>5</sup>	11,713.63	10,728.6 x 13.9445 + 22 = 5,540.92	6,172.71
291	680+17 <sup>5</sup> 630+00	5,984.31	5,017.5 x 13.9445 + 22 = 2,541.35	3,392.96
290	630+00 536+09	8,746.5	8,970.9 x 13.9445 + 22 = 4,633.14	4,113.36
289+289A	536+09 430+50	11,932.97	10,439. x " " = 5,391.36	6,541.61
288	430+50 331+00	10,196.86	9,750.0 x 16.4176 + 27 = 6,050.19	4,146.67
287	331+00 299+09 <sup>2</sup>	3,623.3	3,196.3 x " " = 1,943.54	1,679.76
*	299+09 <sup>2</sup> 298+17 <sup>8</sup>		92.3 x 1.5326 = 141.46	
*	286+99 285+44		155.0 x 1.5326 = 237.55	
287	285+44 225+92	6,350.2	5,795.2 x 16.4176 + 27 = 3,523.83	2,826.37
*	225+92 224+30 <sup>2</sup>		179.64 x 1.5326 = 275.32	
*	205+10 <sup>7</sup> 204+18 <sup>2</sup>		92. x 1.5326 = 141.00	
286	204+18 <sup>2</sup> 192+76 <sup>2</sup>	1,416.82	1,142.5 x 16.4176 + 27 = 694.71	722.11
*	192+76 <sup>2</sup> 192+31 <sup>5</sup>		44.7 x 1.5326 = 68.51	
*	171+95 <sup>5</sup> 171+14		85.0 x 1.5326 = 130.27	
*	170+72 167+75 <sup>1</sup>		296.9 x 1.5326 = 455.03	
*	145+83 <sup>1</sup> 142+25		365.5 x 1.5326 = 560.17	
286	142+25 135+77	717.26	608.8 x 16.4176 + 27 = 390.19	347.07
	135+77 129+30		See pages 64 to 66	993.03
286	129+30 77+83.2	5,155.78	4,932.7 x 16.4176 + 27 = 2,999.37	2,156.41
	77+83 <sup>2</sup> 74+00 <sup>4</sup>		See page 66 to 68	1,463.15
285	74+00 <sup>4</sup> 1+70 <sup>0</sup>	7,590.88	7,060.4 x 16.4176 + 27 = 3,297.74	

Note: For standard trench backfill this formula was used,  
 Cu. Yds backfill =  $\frac{(\text{Total Cu. Yds Excavation}) - (\text{Lineal ft. of excavation} \times \text{pipe Co. Bk.})}{27}$   
 Lineal ft. of excavation does not include trestles, pipe Co. backfill based on Drawings W.D. 206+207.  
 For tunnel entrance & exit trenches, 2 1/2' of cover over pipe, this formula was used, Cu. Yds. backfill = (Lineal ft. of backfill x Cu. Yds per lineal ft.), in which the backfill is carried to the outside wall of tunnel wells.



Total backfill  $\frac{12.83 + 7.0}{2} \times 5.83 = 57.80$   
 Pipe Co. backfill 16.42  
 41.38  
 $\frac{41.38}{27} = 1.5326$  Cu. Yds. per Lin. ft

\* Portal Cuts.

Total Backfill  
 Foreward to page 69

42,614.97 Cu. Yds  
 Calc. W.P. & Steel Co. & Hazard Co.

Otay Res. S.D. 2<sup>nd</sup> Main Pipeline  
 Back fill Sta. 129+30 to 135+77

For original ground use Book 291 p. 40  
 For final ground use " p47(64)

Sta.		End Area	Average Area	Cu. Yds
129+30	0° 36 48 4° 0° 2.41 2.41 0 2.41 2.41	20.79	31.75	23.52
129+50	0° 27 28 42 12 0° 75 10 4 0 6 5	42.73	54.21	50.19
129+75	0° 26 66 46 40 30 03 0° 10 12 135 6 2 0 55 5	65.70	59.53	55.12
130+00	0° 03 52 49 20 05 0° 5 10 11 3 0 4 4	53.35	59.60	55.19
130+25	05 06 71 46 30 08 0° 5 10 14 3 0 4 25	65.85	62.83	58.18
130+50	0° 03 65 43 32 09 0° 25 95 13 3 0 4 25	59.82	57.96	42.93
130+70	0° 02 58 46 29 0° 5 10 13 4 0 4	56.10	59.05	34.99
130+86	0° 04 26 62 42 31 06 0° 29 98 12 12 2 0 4 4	62.00	63.46	32.91
131+00	0° 03 59 42 31 11 0° 25 12 135 2 0 4 35	64.92	68.94	127.67
131+50	0° 46 69 65 33 11 0° 7 135 135 6 0 4 3	72.95	69.77	129.20
132+00	0° 38 64 60 43 13 11 0° 5 11 115 4 0 5 5 4	66.60	61.99	57.40
132+25	0° 21 27 60 48 32 13 0° 4 8 12 135 3 0 4 4	57.38	57.16	46.57
		56.95		

132+47

$$\begin{array}{r} 00 \ 16 \ 22 \ 64 \ 44 \ 32 \ 05 \ 00 \\ 65 \ 75 \ 11 \ 13 \ 4 \ 0 \ 5 \ 4 \end{array}$$

56.95

69.55 66.97

132+73

$$\begin{array}{r} 00 \ 23 \ 32 \ 74 \ 73 \ 38 \ 15 \ 00 \\ 6 \ 85 \ 13 \ 14 \ 6 \ 0 \ 4 \ 4 \end{array}$$

82.15

76.40 76.40

133+00

$$\begin{array}{r} 00 \ 20 \ 29 \ 67 \ 61 \ 35 \ 17 \ 00 \\ 75 \ 8 \ 13 \ 13 \ 5 \ 0 \ 3 \ 3 \end{array}$$

70.65

68.03 125.98

133+50

$$\begin{array}{r} 00 \ 21 \ 38 \ 65 \ 59 \ 47 \ 24 \ 00 \\ 5 \ 6 \ 12 \ 13 \ 35 \ 0 \ 3 \ 4 \end{array}$$

65.40

55.12 102.07

134+00

$$\begin{array}{r} 00 \ 14 \ 30 \ 45 \ 42 \ 29 \ 10 \ 00 \\ 5 \ 7 \ 125 \ 125 \ 3 \ 0 \ 3 \ 40 \end{array}$$

44.83

47.67 30.01

134+17

$$\begin{array}{r} 00 \ 05 \ 42 \ 53 \ 47 \ 38 \ 16 \ 00 \\ 25 \ 5 \ 115 \ 115 \ 2 \ 0 \ 4 \ 35 \end{array}$$

50.50

45.52 21.92

134+30

$$\begin{array}{r} 00 \ 11 \ 51 \ 46 \ 30 \ 16 \ 00 \\ 25 \ 6 \ 115 \ 3 \ 0 \ 3 \ 3 \end{array}$$

40.55

45.98 64.08

134+67<sup>63</sup>

$$\begin{array}{r} 00 \ 25 \ 43 \ 55 \ 41 \ 30 \ 09 \ 00 \\ 75 \ 95 \ 12 \ 125 \ 2 \ 0 \ 4 \ 3 \end{array}$$

51.40

46.95 26.10

134+82<sup>64</sup>

$$\begin{array}{r} 00 \ 44 \ 40 \ 30 \ 09 \ 00 \\ 8 \ 9 \ 2 \ 0 \ 5 \ 4 \end{array}$$

42.50

39.02 21.56

134+97<sup>56</sup>

$$\begin{array}{r} 00 \ 04 \ 64 \ 34 \ 32 \ 03 \ 00 \\ 25 \ 7 \ 9 \ 6 \ 0 \ 5 \ 5 \end{array}$$

35.55

40.95 22.43

135+12<sup>35</sup>

$$\begin{array}{r} 00 \ 14 \ 53 \ 70 \ 70 \ 38 \ 36 \ 08 \ 00 \\ 25 \ 65 \ 10 \ 102 \ 9 \ 5 \ 0 \ 6 \ 7 \end{array}$$

46.35

54.34 45.59

135+35

$$\begin{array}{r} 00 \ 12 \ 71 \ 43 \ 36 \ 37 \ 38 \ 05 \ 00 \\ 25 \ 7 \ 85 \ 45 \ 0 \ 5 \ 9 \ 85 \ 25 \end{array}$$

62.32

57.38 31.88

52.45

Otay Reservoir

San Diego 2nd Main Pipeline

Backfill Cont.

Sta.	0°	35	50	45	38	36	36	29	0°
135+50	5	9	9	6	0	5	75	65	3
135+77	0°	44	42	50	0°				
	291	291	0	291	291				

End Area	Ave. Area	Cu. Yds.
52.45		
37.58	37.58	
22.70		

Western P. & S. Co Backfill (647.0)(16.4176) = 27

Total all backfill 1386.44 Cu. Yds.  
- 393.41

Total Hazard & Co. 993.03 Cu. Yds Back fill. See p. 68

Calc. M. A. E.

Chkd. by Main office.

Backfill Sta 74+00 to 77+83

Sections taken from

Field book #285 pages 71 to 78

74+00 <sup>49</sup>	0°	53	56	53	0°				
29.03	291	291	0	291	291				
74+29 <sup>47</sup>	0°	09	80	72	72	30	08	0°	
14.73	4	95	10	0	1	8	5	35	
74+44 <sup>20</sup>	0°	58	72	72	72	37	30	13	0°
14.77	85	10	10	0	15	8	8	5	25
74+58 <sup>97</sup>	0°	25	33	88	75	63	63	30	29
8.01	3	85	14	175	10	0	1	7	65
74+66 <sup>98</sup>	0°	20	24	96	72	64	30	26	12
6.02	3	7	12	20	10	0	7	65	47
74+73	0°	18	82	70	65	31	22	0°	
10.	35	125	145	10	0	7	65	4	
74+83	0°	83	65	58	29	10	0°		
5.8	12	15	1	0	5	6	3		

26.32		
67.11	72.16	
107.90		
106.85	58.29	
105.80		
109.98	60.16	
114.17		
115.11	34.15	
116.06		
115.02	25.65	
113.98		
116.74	43.24	
119.50		
114.63	24.62	

109.75

1 74+888  
11.2

0° 12 86 67.52 21 08 00  
7 12 125 2 0 6 55 5

109.75

120.33 49.91

13 75+00  
18.8

0° 20 113 91 53 16 05 00  
75 13 135 6 0 6 55 5

130.92

142.73 99.38

75+188  
31.2

0° 18 22 146 43 14 00  
6 95 155 155 0 6 55

154.53

152.90 176.68

75+50  
50

0° 12 20 147 55 19 08 00  
4 10 145 147 0 5 5 35

151.28

141.89 262.76

76+00  
9.

0° 26 34 152 60 24 10 00  
6 65 12 135 0 5 5 4

132.50

138.38 46.13

76+09  
9.

0° 24 38 142 180 73 24 19 00  
5 65 115 115 15 0 6 6 5

144.25

129.95 43.32

76+18  
32

0° 21 42 128 68 20 00  
45 55 11 11 0 6 6

115.65

109.39 129.65

76+50  
25

0° 21 32 118 55 15 00  
6 65 11 105 0 6 6

103.13

124.50 115.28

76+75  
31.25

0° 23 25 147 61 18 00  
5 7 13 125 0 75 6

145.88

136.04 157.45

77+0625  
6.75

0° 22 28 122 57 19 00  
75 85 12 12 0 7 6

126.20

122.45 30.61

77+13  
8.20

0° 20 35 128 51 21 00  
7 8 125 13 0 55 55

118.70

120.68 36.65

77+212  
14.9

0° 25 35 129 50 19 00  
65 9 13 15 0 6 55

122.65

122.35 67.52

122.05

77+36<sup>1</sup>      0° 1' 22 3° 11° 9° 5° 19 16 12 0°  
               3 9 9<sup>5</sup> 14<sup>5</sup> 15 10 0 6 6 4 2<sup>5</sup>      122.05

77+50<sup>2</sup>      0° 4<sup>8</sup> 4<sup>8</sup> 6<sup>9</sup> 12<sup>4</sup> 10<sup>9</sup> 6<sup>9</sup> 4° 3<sup>9</sup> 3<sup>8</sup> 0°  
               10.1      2<sup>5</sup> 9 14 19 20 15 0 6 4<sup>2</sup> 3<sup>5</sup> 2<sup>5</sup>      129.00

77+61      0° 2<sup>8</sup> 7<sup>2</sup> 7<sup>2</sup> 12<sup>4</sup> 6<sup>5</sup> 2<sup>2</sup> 4<sup>3</sup> 0°  
               22.2      3 3<sup>5</sup> 10 18<sup>5</sup> 20 0 6 3 2      94.85

77+83<sup>2</sup>      0° 6° 8° 6<sup>2</sup> 5° 0°  
               2<sup>4</sup> 2<sup>4</sup> 2<sup>9</sup> 0 2<sup>4</sup> 2<sup>4</sup>      30.71

Sta 74100<sup>2</sup> to 77+83<sup>2</sup>  
 Western P. & S. Co Backfill (382.76)

27

Total of all backfill 1695.90 Cu. Yds  
 (16.4176)      - 232.75 Cu. Yds

Hazard Co. Backfill 1463.15 Cu. Yds

Calc. M. D. & Chkd by Main Office.

Note: These computations were based on W. P. & S. Co. back fill area of 16.4176 c.f., this area 16.2387 should have been used, computations thus:

Total of all backfill page 66 1386.44

Total " " this page 1695.90

Total all backfill Deep cuts 3082.34 c.y.

W. P. & S. Co. (382.76 + 647.) x  $16.2387$  <sup>32.87</sup> - 622.76

27

2,459.58 c.y.

Total backfill of Deep Cuts →

Otay Reservoir San Diego 2nd Main Pipe Line  
Backfill Schedule I: 69

Forwarded from page 63.

Book #	54" Trench		Lineal ft.	
	Sta to Sta	Excavation	Excavation	Excavation
293.	855+12 <sup>2</sup>	790+09 <sup>4</sup>	6,170.4	6,617.5
292	790+09 <sup>4</sup>	680+17 <sup>2</sup>	11,713.63	10,728.6
291	680+17 <sup>2</sup>	630+00	5,984.31	5,017.5
290	630+00	536+09	8,746.5	8,970.9
289+289A	536+09	430+50	11,932.97	10,439
Total			49,547.81	41,773.5

Hazard Co. Backfill	Note: Original field calculations based on 54" trench width, should have been 55" (see page 59), also W.P.+S.Co. Area was based on W.D. 206 instead of <del>12888</del> as shown on page 60. Computation = 45,372.74 C.Y. excavation - $\frac{41,773.5 \times 13.8843}{27}$ , W.P.+S. backfill = 23,891.41 Cu. yds of backfill an increase of 918.06 C.Y. to be added.
2,752.71	
6,172.71	
3,392.96	
4,113.36	
6,541.61	
22,973.35	Cu. yds. original figures
918.06	Addition
23,891.41	Cu. yds. total backfill of 55" trench

Book #	58" Trench		Lineal ft. Exc.	
	Sta to Sta	Excavation	Excavation	Excavation
288	430+50	331+00	10,196.86	9,950.0
287	331+00	299+09 <sup>1</sup>	3,623.3	3,196.3
"	285+44	225+92	6,350.2	5,795.2
286	209+18 <sup>2</sup>	192+76 <sup>2</sup>	1416.82	1142.5
"	192+25	135+77	717.26	608.8
"	129+30	77+83 <sup>2</sup>	5,155.78	4,932.7
285	74+00 <sup>49</sup>	1+70	7,590.88	7,060.4
			35,051.10	32,682.9

Hazard Co. Backfill	Note: Original field calculations based on 58" trench width, should have been 59" (see page 59), also W.P.+S.Co. area was based on W.D. 207 instead of $\frac{16,3287}{95}$ as shown on page 60. Computation = 35,051.10 Cu. yds. excavation - $\frac{32,685.9 \times 16,3287}{27}$ , W.P.+S.Co. backfill = 15,888.07 Cu. yds. of backfill, an increase of 711.94 Cu. yds
4,146.67	
1,679.76	
2,826.37	
722.11	
347.07	
2,156.41	
3,297.74	
15,176.13	Cu. yds. original figures.
711.94	Addition
15,888.07	Cu. yds. total backfill of 59" trench

Continued p. 70

Otay Reservoir San Diego 209 Main Pipe Line  
 Backfill Schedule I (cont from p. 69)

Tunnel/Portal Cuts.

Sta. to Sta.	lin. feet of backfill.	Hazard Co. Backfill.
299+09 <sup>2</sup> 298+17 <sup>4</sup>	92.3	141.46
286+99 285+44	155.	237.55
225+92 224+30 <sup>2</sup>	179.64	275.32
205+102 204+18 <sup>2</sup>	92.	141.00
192+76 <sup>2</sup> 192+31 <sup>5</sup>	44.7	68.51
171+95 <sup>5</sup> 171+14	85.	130.27
170+72 167+75 <sup>1</sup>	296.9	455.03
145+83 <sup>1</sup> 142+25	365.5	560.17
	<u>1311.04</u>	

2,009.31 Cu. Yds. original field figures.

4.37 Addition (See note)

2,013.68 Cu. Yds total back fill of Portal Cuts.

Note: original field computations based on W.D. drawing 207 for W.P. & Steel Co. back fill. 16.3287, as shown on page 60, should have been used. Thus, Total backfill area,  $57.80 - 16.3287 = 2,013.68$  an increase <sup>27</sup> of 4.37 Cu. Yds





72



74

75





B.M. 339.35  
9.15  
 343.50  
5.5  
 855 335.0 330.1 C. 4.9  
1.7  
 103.5 338.8 320.6 C. 8.2

349.50

6.2

337.3 320.6 C. 6.7

343.5

1.6

338.9 C. 8.7



DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder  
take for any width roadway, slope 1 to 1.  
If ground is nearly level, the cut or fill at any  
stake is located by the double entry method in  
left column and top row. The number in  
of table in same row and column gives distance

**IMPROVED TABLES  
AND  
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of  
any other degree, divide by degree of curve and  
add correction found in column of corrections.  
Degree of curve with a given  $T$  may be found  
by dividing tangent (or external), opposite  $T$   
given tangent (or external).  
The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
length divided by twice the radius.

34.63  
12.05  
22.58

9.3  
31  
62  
56  
11.8

9.3  
36  
57  
37  
92

85  
31  
54  
19  
73

86  
2  
66  
53  
119

88  
19  
59  
26  
85

95  
24  
71  
13  
84

99  
36  
63  
2  
83

89  
36  
63  
27  
90

104

2.6  
330.6  
2.6  
328.0

Wrong % of grade 821+15 to 823+50  
should be 3.856%

Why short grade at 828+70  
" " " " 836+94.  
850+50 - Graded Street - only 4.4 cut.

3.9  
3213  
3252  
3209  
48

3 850  
821+15      398  
235 ) 9.06  
      705  
      2010  
      2115  
      1950  
      1880  
      700

1626  
104  
6504  
1626  
169104      3.8  
2010

3256  
17  
3239  
41  
2280