

295

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Schedule I

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IRVING PARK STATION

CHICAGO, ILL.
MICROFILMED

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2nd M.P.L.

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COPY 1 X 100

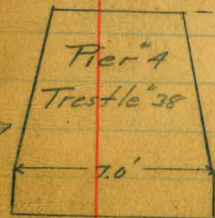
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TRESTLES

Sta.	Trestle	Pier	Ground Eler.	Grade Eler.	Footing Eler.	Dimension Base of Pier	Height	Excav. C.Y.	Concrete C.Y.	lbs. Reinf. Steel	bbls. Cement
793	39	1	306.5	308.0	303.2	26' x 6.02'	5.3'	1.91	1.87	112.5	
		2	306.0	"	302.5	2.83 x 6.25	6.0	2.29	2.36	122.5	
		3	307.3	"	307.7	2.10 x 5.52	3.8	1.11	1.06	89.5	
Trestle walk			2 pcs 2" x 16" x 15" = 90.67 F.B.M.					5.31	5.27	323.5	7.5
768	38	1	320.8	329.0	317.7	3.10 x 6.52	6.8	2.32	2.98	138.5	
		2	316.6	"	311.3	4.0 x 7.0	13.2	5.50	4.53	282.5	
		3	317.2	"	313.0	4.0 x 7.0	11.5	4.36	4.05	243.5	
		4	318.1	"	314.1	4.3 x 7.0	10.4	4.46	6.56	208.5	
		5	323.0	"	318.4	2.9 x 6.28	6.1	3.10	2.43	124.5	
Trestle walk			4 pcs 2" x 16" x 15" = 177.78 F.B.M.					19.74	20.55	995.5	26.5

Note i-6 batter stopped when pier length reached 7.0' to keep within Right of Way



Area at pt. 8.3 below top = 25.2 sq. ft.
 " " base = 30.1 sq. ft.

$$\frac{25.2 + 30.1}{2} \times 2.1 = 2.15 \text{ C.Y.}$$

716	37	1	251.1	256.0	246.8	1.07 x 7.0	9.7	4.54	5.87	197.5	
		2	246.6	"	242.7	4.0 x 7.0	13.8	4.07	4.75	300.5	
		3	246.7	"	242.2	4.0 x 7.0	19.3	4.36	4.90	308.5	
		4	251.7	"	247.6	3.8 x 7.2	8.9	4.15	5.00	183.5	
Trestle walk			3 pcs 2" x 16" x 15" = 134.22 F.B.M.					17.09	20.46	1988.5	31.3

Note For piers adjacent to old wood structure a minimum depth of about 4 feet was used for footing.

chkd by
A.L.L.

Trestles (cont.)

2

Sta.	Trestle	Pier	Ground Elev.	Grade Elev.	Footing Elev.	Dimens. Base of Pier	Height	Excav. C.Y.	Concrete C.Y.	Reinf. Steel	bbls. Cement
691	36	1	245.6	245.6	242.0	2.2' x 5.62'	4.1	1.15 [§]	1.20 [§]	88.✓	
		2	241.4	"	236.5	4.03' x 7.0	9.6	3.90 [§]	5.62 ^W	195.✓	
		3	237.9	"	232.5	5.37' x 7.0	13.6	6.25 [§]	10.57 [§]	257.✓	
		4	234.4	"	228.5	4.0' x 7.0	17.6	6.12 [§]	5.85 ^W	365.✓	
		5	234.7	"	231.4	4.0' x 7.0	14.7	3.42 [§]	5.02 ^W	310.✓	
		6	239.1	"	235.5	4.37' x 7.0	10.6	3.48 [§]	6.68 [§]	209.✓	
		7	243.6	"	240.4	2.73' x 6.15	5.7	1.50 [§]	2.14 [§]	117.✓	
Trestle walk			6 pcs. 2" x 16" x 15"	7 "	264.89 [§]	F.B.M.	Poured 6/11/30 - 6/19/30	25.82 [§]	37.1 ^W	1541.✓	56.5

Note On several piers footings carried about 2 feet below grade shown on drawings on account of soft adobe.

With exception of Piers 4 & 5 of above Trestle material excavated on same batter as piers, excavation yardage computed accordingly.

621440	35	1	241.8	242.87	236.6	3.47' x 6.88	7.9	5.57 [§]	4.00 [§]	166.✓	
		2	241.9	242.87	237.7	2.73' x 6.15	5.7	2.61 [§]	2.14 [§]	117.✓	
Trestle walk			1 pc. 2" x 16" x 15"	2 pcs. 2" x 16" x 16"	47.11 [§]	F.B.M.	Poured 6/19/30 - 6/19/30	8.18 [§]	6.14 [§]	283.5	9.4

✓§.

chkd by
A.L.

Trestles (cont.)

Sta.	Trestle	Pier	Ground Elev.	Grade Elev.	Footing Elev.	Dimens. of base	Height	Excav. C.Y.	Concrete C.Y.	Reinf. steel	bbls. Cement
614+70	"34	1	369.6	370.66	367.3	213 x 535	3.9	1.01 ^{8.✓}	1.10 ^{3.✓}	90.✓	
		2	369.9	370.63	368.0	1.87 x 5.28	3.1	0.69 ^{8.✓}	0.76 ^{3.✓}	79.✓	
	Trestle walk	1 pc. 2" x 16" x 16"		47.11	F.B.M.	Poured 6/18/30-6/19/30		1.70 ^{3.✓}	1.86 ^{3.✓}	169.✓	2.5
612	33	1	367.0	371.22	364.0	3.40 x 6.82	7.7	3.01 ^{8.✓}	3.80 ^{3.✓}	164.✓	
		2	366.1	371.19	362.0	4.07 x 7.18	9.7	4.62 ^{8.✓}	6.09 ^{3.✓}	195.✓	
		3	368.3	371.16	364.9	3.10 x 6.52	6.8	2.54 ^{3.✓}	2.98 ^{8.✓}	138.✓	
	Trestle walk	2 pcs. 2" x 16" x 16"		90.67	F.B.M.	Poured 6/19/30-6/20/30		10.17 ^{8.✓}	12.87 ^{3.✓}	497.✓	16.0
607+50	32	1	324.6	328.04	320.0	3.67 x 7.08	8.5	4.43 ^{8.✓}	4.63 ^{3.✓}	177.✓	
		2	323.6	328.84	319.0	4.26 x 7.68	10.3	5.57 ^{8.✓}	6.92 ^{3.✓}	205.✓	
		3	322.7	329.65	320.0	4.20 x 7.62	10.1	3.20 ^{8.✓}	6.64 ^{3.✓}	202.✓	
		4	327.4	330.45	323.0	3.5 x 6.92	8.0	3.96 ^{8.✓}	4.10 ^{3.✓}	167.✓	
		5	328.8	331.26	326.0	2.77 x 6.18	5.8	1.78 ^{8.✓}	2.21 ^{3.✓}	120.✓	
	Trestle walk	4 pcs. 2" x 16" x 16"		177.78	F.B.M.	Poured 6/18/30-6/19/30		18.93 ^{8.✓}	24.50 ^{3.✓}	871.✓	36.2

calc. *M.E.* ch. *M.E.*
 ch. *M.E.* ch. *M.E.* chkd *M.E.*

chkd by
A.C.L.

Trestles (cont.)

5

Sta.	Trestle Pier	Ground Elev.	Grade Elev.	Footing Elev.	Dimension at base	Height	Excav. C.Y.	Concr. C.Y.	Reinf. Steel	Bbb. Cement	
567+50	"26	1	331.9	332.16	329.0	207 x 5.42	3.7	1.22 ^{s.v.}	1.01 ^{s.v.}	88'	
		2	329.3	330.92	327.0	230 x 5.72	4.4	1.12 ^{s.v.}	1.35 ^{s.v.}	98'	
		3	328.0	330.33	324.0	310 x 6.52	6.8	2.99 ^{s.v.}	2.98 ^{s.v.}	135'	
		4	330.1	330.00	327.0	200 x 5.42	3.5	1.24 ^{s.v.}	0.92 ^{s.v.}	85'	
	Trestle Walk	3 pcs 2" x 16" x 15"		=		134.22 ^{s.} F.B.M.	Paired 7/13/30 - 7/15/30	6.57 ^{s.v.}	6.26 ^{s.}	406'	9.8

560+50	"25	1	264.3	266.05	261.0	270 x 6.12	5.6	2.02 ^{s.v.}	2.07 ^{s.v.}	117'	
		2	263.7	266.50	261.0	283 x 6.25	6.0	1.77 ^{s.v.}	2.35 ^{s.v.}	123'	
		3	265.5	266.95	263.5	213 x 5.55	3.9	0.88 ^{s.v.}	1.10 ^{s.v.}	91'	
	Trestle Walk	2 pcs 2" x 16" x 15"		=		90.67 ^{s.} F.B.M.	Paired 7/16/30 - 7/17/30	4.67 ^{s.v.}	5.52 ^{s.}	331'	8.4

549+50	"24	1	272.1	273.09	270.0	203 x 5.95	3.6	0.98 ^{s.v.}	0.97 ^{s.v.}	80'	
		2	268.1	273.16	264.5	390 x 7.32	9.2	4.12 ^{s.v.}	5.35 ^{s.v.}	186'	
		3	268.2	273.51	265.0	383 x 7.25	9.0	3.29 ^{s.v.}	5.21 ^{s.v.}	183'	
		4	272.9	274.14	270.0	237 x 5.78	4.6	1.97 ^{s.v.}	1.46 ^{s.v.}	102'	
	Trestle Walk	3 pcs 2" x 16" x 15"		=		134.22 ^{s.}	Paired 7/9/30 - 7/11/30	9.86 ^{s.v.}	13.09 ^{s.}	557'	20.3

Calc. J.H.H. Calc. J.H.H.

Chkd. J.H.H.

Chkd by
A.C.L.

Trestles (cont.)

6

Sta.	Trestle	Pier	Ground Elev.	Grade Elev.	Footing Elev.	Dimens. of base	Height	Excav. C.Y.	Concr. C.Y.	Rein. Steel	Bbls. Cement
548+70	"23	1	274.6	275.02	273.0	1.66x5.08	2.5	0.50 ⁸	0.53 ⁸	70.4	
		2	274.6	274.20	271.5	1.90x5.32	3.2	1.16 ⁸	0.80 ⁸	80.4	
	Trestle Walk		1 pc 2" x 16" x 15" 2 pcs 2" x 16" x 16" =		47.11 F.B.M.	Poured 7/14/30-7/14/30		1.66 ⁸	1.35 ⁸	150.4	2.1
516+50	"22	1	170.0	170.31	168.0	1.76x5.18	2.8	0.67 ⁸	0.64 ⁸	74.4	
		2	167.5	170.00	169.5	2.83x6.25	6.0	1.96 ⁸	2.33 ⁸	124.4	
		3	168.2	170.00	165.0	2.67x6.08	5.5	1.92 ⁸	2.00 ⁸	116.4	
		4	170.4	170.33	167.0	2.10x5.52	3.8	1.46 ⁸	1.06 ⁸	89.4	
	Trestle Walk		3 pcs 2" x 16" x 15" 4 pcs 2" x 16" x 16" =		134.22 F.B.M.	Poured 7/12/30-7/12/30		6.01 ⁸	6.05 ⁸	403.4	9.3
493+50	"21	1	141.5	142.65	139.0	2.23x5.65	4.2	1.17 ⁸	1.25 ⁸	95.4	
		2	142.1	143.40	139.5	2.30x5.72	4.4	1.27 ⁸	1.35 ⁸	98.4	
	Trestle Walk		1 pc 2" x 16" x 15" 2 pcs 2" x 16" x 16" =		47.11 F.B.M.			2.44 ⁸	2.60 ⁸	193.4	4.0
492+40	"20	1	141.5	140.66	135.0	2.90x6.32	6.2	4.41 ⁸	2.50 ⁸	125.4	
		2	139.0	140.77	135.0	2.93x6.35	6.3	2.76 ⁸	2.58 ⁸	128.4	
	Trestle Walk		1 pc 2" x 16" x 15" 2 pcs 2" x 16" x 16" =		47.11			7.17 ⁸	5.08 ⁸	253.4	7.8
								chkd M.R. G.	chkd W.H.		

chkd by
A.C.L.

Sta.	Trestle	Pier	Ground Elev.	Grade Elev.	Footings Elev.
270+50	"18"	1	354.1	357.14	351.4
		2	357.2	"	348.9
		3	358.1	"	352.8
	Trestle Walk		2 pcs 2" x 16" x 15" 3 pcs 2" x 16" x 16"	=	90.67 FBM

260	"17"	1	363.6	365.15	361.4
		2	361.4	366.28	357.8
		3	363.0	367.40	359.9
		4	368.8	368.52	366.6
	Trestle Walk		3 pcs 2" x 16" x 15" 4 pcs 2" x 16" x 16"	=	134.72 FBM

257+50	"16"	1	367.2	368.08	364.0
		2	361.4	368.29	359.0
		3	361.3	368.40	359.2
		4	365.4	368.56	363.0
		5	368.7	368.70	367.4
	Trestle Walk		4 pcs 2" x 16" x 15" 5 pcs 2" x 16" x 16"	=	177.78 FBM

136+50	"15"	1	365.0	368.0	363.0
		2	364.0	"	360.0
		3	367.7	"	365.5
	Trestle Walk		2 pcs 2" x 16" x 15" 3 pcs 2" x 16" x 16"	=	90.67

Dimens. of base	Height	Excav. C.Y.	Concr. C.Y.	Reinf. Steel	BBLs Cement
293 x 6.60	6.3	1.93	2.68	130'	
370 x 7.43	8.8	2.38	5.16	184'	
477 x 6.13	4.9	1.29	1.70	105'	
		5.60	9.54	419'	14.6
230 x 5.97	4.4	1.12	1.41	99'	
387 x 7.83	9.1	3.89	5.52	186'	
353 x 7.29	8.1	2.92	4.36	171'	
166 x 5.33	2.5	0.72	0.56	70'	
		8.65	12.19	526'	18.1
			11.85		
240 x 6.07	4.7	1.73	1.58	104'	
413 x 7.80	9.9	2.86	6.58	202'	
417 x 7.83	10.0	2.78	6.72	203'	
290 x 6.57	6.2	1.69	2.60	126'	
160 x 5.27	2.3	0.53	0.51	52'	
		9.59	17.99	687'	27.5
270 x 6.87	5.6	1.27	2.16	117'	
370 x 7.37	8.6	4.04	4.92	179'	
187 x 5.63	3.1	0.84	0.79	77'	
		6.15	7.87	373'	12.0
		J.C.B.	Calc. J.H.H.	J.C.B.	
		chkd M.D.G.	chkd W.H.		

chkd by
A.C.L.

Sta.	Trestle	Pier	Ground Elev.	Grade Elev.	Footings Elev.	Dimens. of base	Height	Excav. C.Y.	Concr. C.Y.	Reinht. Steel	Bbs cement
119+60	" 14	1	329.2	330.0	322.0	370x7.37	8.6	7.27	4.92	179.	
		2	328.8	"	322.0	370x7.37	8.6	6.82	4.92	179.	
	Trestle Walk		1pc 2"x16"x15" 2pc 2"x16"x16"	=	47.11 F.B.M.			14.145	9.84	358.	15.1
112+70	" 13	1	383.3	384.0	381.5	187x5.53	3.1	0.69	0.79	77.	
		2	380.5	"	378.5	287x6.53	6.1	1.39	2.5-2	123.	
		3	380.9	"	378.5	287x6.53	6.1	1.67	2.5-2	123.	
		4	383.6	"	381.5	187x5.53	3.1	0.80	0.79	79.	
	Trestle Walk		3pc 2"x16"x15" 4pc 2"x16"x16"	=	134.22 F.B.M.			4.553	6.62	402.	10.1
110+10	" 12	1	364.2	364.0	360.5	220x5.87	4.1	1.77	1.25	192.	
		2	365.5	"	361.0	203x5.70	3.6	1.93	1.01	86.	
	Trestle Walk		1pc 2"x16"x15" 2pc 2"x16"x16"	=	47.11 F.B.M.			3.70	2.26	178.	3.5
105+00	" 11	1	309.5	312.0	307.0	270x6.37	5.6	1.59	2.16	117.	
		2	308.8	"	304.0	370x7.37	8.6	4.85	4.92	179.	
		3	308.8	"	304.0	370x7.37	8.6	4.85	4.92	179.	
		4	311.1	"	309.0	203x5.70	3.6	0.90	1.01	86.	
	Trestle Walk		3pc 2"x16"x15" 4pc 2"x16"x16"	=	134.22 F.B.M.			14.198	13.01	561.	19.9
98+50	" 10	1	348.8	352.0	346.0	303x6.70	6.6	2.11	2.93	132.	
		2	347.5	"	344.0	370x7.37	8.6	3.53	4.92	179.	
	Trestle Walk		1pc 2"x16"x15" 2pc 2"x16"x16"	=	47.11 F.B.M.			5.64	7.85	311.	12.0

calc. T.H.H.
chkd. M.H.R.S.

calc. T.H.H.
chkd. M.H.R.S.

J.C.B.
chkd. M.H.

1

12.826

ch. Kcd by
A.C.L.

Sta.	Trestle	Pier	Ground Elev.	Grade Elev.	Footing Elev.	Pier base	Height	Excav. c.v.	Concr. c.v.	Rent. Steel	Bbls. Cement
98+00	#9	1	324.7	328.0	323.5	253X620	5.1	0.70	1.82	110.	
		2	322.8	"	319.5	387X7.53	9.1	3.56	5.52	187.	
		3	325.3	"	323.5	253X620	5.1	1.05	1.82	110.	
Trestle Walk			2 pcs 2"X16"X15" 3 pcs 2"X16"X16" =		90.67 F.B.M.			5.315	9.16	407.	14.0
81+50	#8	1	329.0	330.0	326.5	220X587	4.1	1.19	1.25	93.	
		2	329.2	"	327.0	203X570	3.6	0.94	1.01	86.	
		Trestle Walk			1 pc 2"X16"X15" 2 pcs 2"X16"X16" =		47.11 F.B.M.			2.13	2.26
72+20	#7	1	336.2	339.0	334.5	253X620	5.1	0.99	1.82	110.	
		2	335.2	"	330.5	387X7.53	9.1	5.07	5.52	187.	
		3	337.5	"	335.5	220X587	4.1	0.96	1.25	93.	
Trestle Walk			2 pcs 2"X16"X15" 3 pcs 2"X16"X16" =		90.67 F.B.M.			7.02	8.59	390.	13.1
67+50	#6	1	310.9	312.0	305.5	320X687	7.1	4.40	3.37	143.	
		2	310.8	"	305.0	337X703	7.6	5.09	3.84	152.	
		Trestle Walk			1 pc 2"X16"X15" 2 pcs 2"X16"X16" =		47.11 F.B.M.			9.49	7.21
60+50	#5	1	339.0	340.0	335.0	270X637	5.6	2.55	2.16	116.	
		2	338.5	"	333.5	320X687	7.1	4.07	3.37	143.	
		Trestle Walk			1 pc 2"X16"X15" 2 pcs 2"X16"X16" =		47.11 F.B.M.			6.62	5.53
33+10	#4	1	353.5	354.0	350.5	220X587	4.1	1.43	1.25	93.	
		2	353.7	"	351.5	187X553	3.1	0.84	0.79	79.	
		Trestle Walk			1 pc 2"X16"X15" 2 pcs 2"X16"X16" =		47.11 F.B.M.			2.27	2.04

CAI. J.C.B.E.
 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

Sta.	Trestle	Pier	Ground Elev.	Grade Elev.	Footing Elev.	Dimens. at base	Height	Excav. cu.	Concr. cu.	Reinft. steel	Bbls cement
29 ⁺ +30	"3	1	337.8	338.0	335.0	2.03 x 5.70	3.6	1.20 ^{cu}	1.01 ^{cu}	85 ^{lb}	
		2	337.1	"	334.0	2.37 x 6.03	4.6	1.64 ^{cu}	1.5 ^{cu}	100 ^{lb}	
		3	338.0	"	336.0	1.70 x 5.37	2.6	0.68 ^{cu}	0.59 ^{cu}	74 ^{lb}	
	Trestle Walk				90.67 F.B.M.			3.52 ^{cu}	3.12 ^{cu}	259 ^{lb}	4.8
			2 pcs 2" x 16" x 15'								
			3 pcs 2" x 16" x 16" =								
10+80	"2	1	335.9	336.32	332.0	2.47 x 6.13	4.9	2.19 ^{cu}	1.70 ^{cu}	105 ^{lb}	
		2	335.2	336.06	331.5	2.57 x 6.23	5.2	2.19 ^{cu}	1.89 ^{cu}	110 ^{lb}	
	Trestle Walk				47.11 F.B.M.			4.38 ^{cu}	3.59 ^{cu}	215 ^{lb}	5.5
			1 pc 2" x 16" x 15'								
			2 pcs 2" x 16" x 16" =								
			Total to here 3,209.78								
1+30	"1				395.66						
		1	390.9	"	387.1	3.87 x 7.53	9.1	4.10 ^{cu}	5.52 ^{cu}	185 ^{lb}	
		2	389.8	"	385.4	4.43 x 8.10	10.8	5.85 ^{cu}	7.92 ^{cu}	212 ^{lb}	
		3	388.7	"	384.5	4.73 x 8.40	11.7	6.18 ^{cu}	9.41 ^{cu}	225 ^{lb}	
		4	389.2	"	387.2	3.83 x 7.50	9.0	2.13 ^{cu}	5.90 ^{cu}	183 ^{lb}	
	Trestle Walk				134.22 F.B.M.			18.26 ^{cu}	28.25 ^{cu}	805 ^{lb}	41.0
			3 pcs 2" x 16" x 15'								
			4 pcs 2" x 16" x 16" =								
			Totals all trestles by M.D.B. 10/31/30					2.93.02 ^{cu}	340.88 ^{cu}	15,807 ^{lb}	509.41.
			chk'd M.D.B. 11/10/30						341.98 ^{cu}		

Note - Steel in each separate Pier not checked. A.C.L.

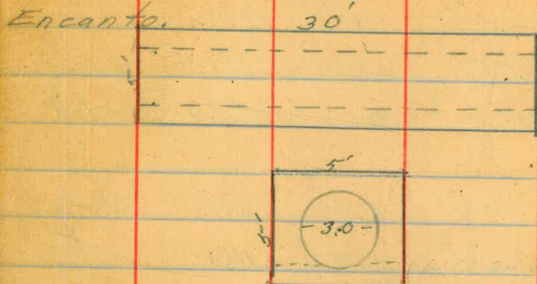
chk'd by
A.C.L.

MISCELLANEOUS CONCRETE STRUCTURES

11

Hill 1930

Concr. encasement at R.R. undercrossing



Concrete

$$\text{End area of concr.} = 5 \times 5 = 25 \text{ sq ft.}$$

$$\text{" " " pipe } (1.5)^2 \times 3.1416 = 7.06 \text{ "}$$

$$\text{Net end area} = 25.0 - 7.06 = 17.94 \text{ sq ft.}$$

$$\text{Concrete content} = \frac{17.94 \times 30.0}{27} = 19.93 \text{ Cu. Yds.}$$

$$\text{Reinforcing - } 8 \frac{1}{2} \text{ \# bars } 25' \text{ long} = 200 \text{ \#}$$

$$30 \text{ " " " } 4.5 \text{ " " " } = 135 \text{ \#}$$

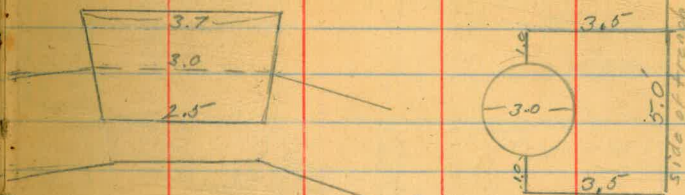
$$335 \text{ \# steel at } 0.85 \text{ \# lbs per foot} = 285 \text{ \# lbs.}$$

$$\text{Cement} = 25.1 \text{ bbls.}$$

Calc. T.H.B.
Chkd. M.R.E.

chkd by
A.L.L.

Pipe Anchor Block at Sta 508+93



Concrete

$$\text{Total content of block} = 3.1 \times 3.5 \times 5.0 = 54.25 \text{ cu. ft.}$$

$$\text{Content displaced by pipe} = (1.5)^2 \times 3.1416 \times 2.75 = 9.71 \text{ cu. ft.}$$

$$\frac{54.25 - 9.71}{27} = 1.65 \text{ Cu. Yds.}$$

Reint. steel

$$5 \text{ - } 5 \frac{1}{8} \text{ \# bars } 5.33' \text{ long} = 26.65 \text{ \#}$$

$$26.65 \text{ feet at } 1.33 \text{ \# lbs per foot} = 35 \text{ \# lbs.}$$

$$\text{Cement } 2.2 \text{ bbls.}$$

Structure Excav.

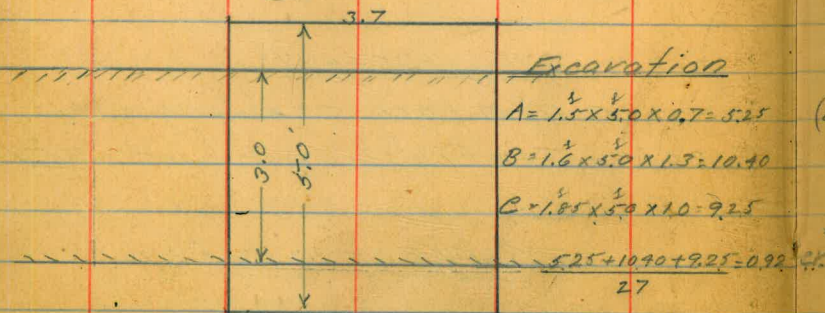
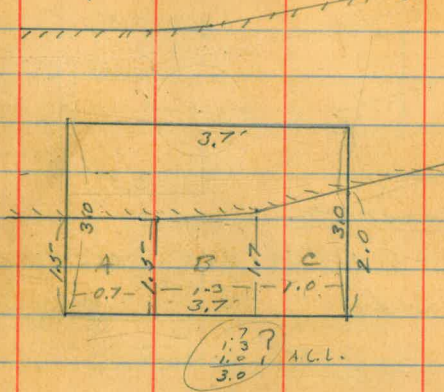
$$\frac{3.1 \times 3.5 \times 1.0}{27} = 0.40 \text{ Cu. Yds.}$$

Calc. T.H.B.
Chkd. M.R.E.

chkd by
A.L.L.

Misc. Concr. structures (cont.)

Pipe Anchor at 469+95
(As constructed)



Excavation

$$A = 1.5 \times 5.0 \times 0.7 = 5.25$$

$$B = 1.6 \times 5.0 \times 1.3 = 10.40$$

$$C = 1.85 \times 5.0 \times 1.0 = 9.25$$

$$5.25 + 10.40 + 9.25 = 24.90$$

Concrete

$$3.7 \times 5.0 \times 3.0 = 55.5 \text{ cu. ft.}$$

$$\text{supplanted by pipe} = 9.18 \text{ cu. ft.}$$

$$55.5 - 9.18 = 1.7.2 \text{ Cu Yds.}$$

Reinforcing Steel

$$5 \text{ } \# \frac{5}{8} \text{ bars } 5.5' \text{ long} = 27.5'$$

$$27.5 \text{ feet at } 1.33 \text{ lbs per foot} = 37 \text{ lbs}$$

$$\text{Cement } 2.2 \text{ bbls}$$

chkd by
A.L.L.

chkd by

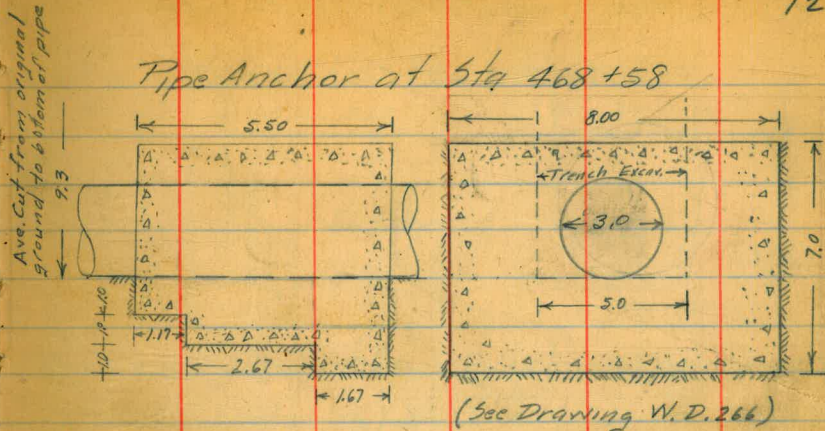
$$156.5' \text{ of } \frac{3}{4} \text{ at } 1.91 \text{ lbs per ft} = 299 \text{ lbs.}$$

chkd by

Comold. M. D. E. 11/28/30

chkd. by
A.L.L.

Pipe Anchor at Sta 468+58



Excavation

$$1 \times \frac{5.5 \times 8}{27} = 1.63$$

$$1 \times \frac{4.33 \times 8}{27} = 1.28$$

$$1 \times \frac{1.67 \times 8}{27} = 0.49$$

$$\left(\frac{5.5 \times 8 \times 9.3}{27} \right) - \left(\frac{5 \times 5.5 \times 9.3}{27} \right) = 5.68$$

$$\text{Total Exc. } 9.08 \text{ Cu. yds}$$

Concrete

$$1 \times \frac{5.5 \times 8}{27} = 1.63$$

$$1 \times \frac{4.33 \times 8}{27} = 1.28$$

$$1 \times \frac{1.67 \times 8}{27} = 0.49$$

$$\left(\frac{8 \times 4 \times 5.5}{27} \right) - \left(\frac{15^2 \times 3.1416 \times 5.5}{27} \right) = 5.08$$

$$\text{Total Concrete } 8.48 \text{ Cu. yds}$$

Reinforcing Steel

$$\text{"A" bars } 8 \times 8.71' = 69.7'$$

$$\text{"B" bars } 5 \times 6.16' = 30.8'$$

$$\text{"C" bars } 8 \times 7.0' = 56.0'$$

$$156.5'$$

$$156.5' \text{ of } \frac{3}{4} \text{ at } 1.91 \text{ lbs per ft} = 299 \text{ lbs.}$$

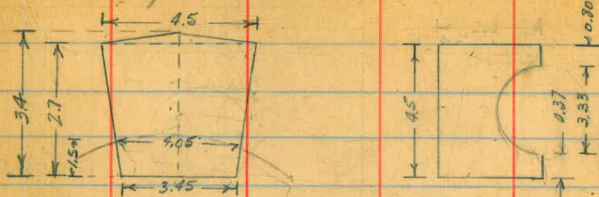
chkd by

Comold. M. D. E. 11/28/30

chkd. by
A.L.L.

Misc. Concrete Structures (cont.)

Pipe Anchor at Sta 286+67



$$\text{Concrete } \left(\frac{3.45 + 4.5}{2} \times 2.7 \times 4.5 \right) + (0.7 \times 2.25 \times 4.5) - \left(\frac{1.67 \times 3.1416 \times 3.75}{2} \right) = 144 \text{ Cu. Yds.}$$

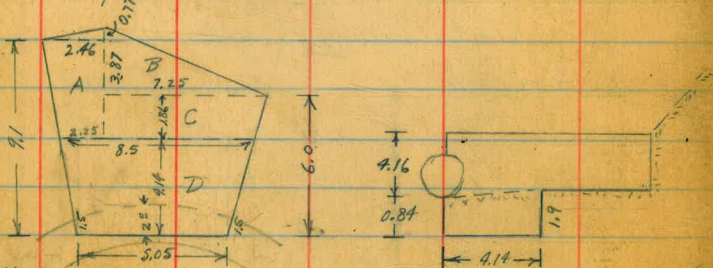
$$\text{Steel } 5 - 3/4 \text{ } \# \text{ } 5.33 \text{ Long} = 26.65 \text{ at } 1.91 \text{ lbs per ft.} = 51 \text{ Lbs}$$

$$\text{Excavation } \left(\frac{3.45 + 4.5}{2} \times 2.7 \times 0.37 \right) + (0.7 \times 2.25 \times 0.37) \div 27 = 0.17 \text{ Cu. Yds.}$$

$$\text{Cement } 8 \text{ sacks} = 2.06 \text{ bbls.}$$

Comptd M.R.S. 10/29/30 - chd J.H.H.

Pipe Anchor Sta. 224+85



Ave. Depth of A, B, C = 3.1
Ave. Depth of D = 5.0

$$\text{Concrete } \left(\frac{8.5 + 5.05}{2} \times 4.14 \times 5 \right) + \left(\frac{2.25 + 6.25}{2} \times 1.86 \times 3.1 \right) + \left(\frac{3.27 \times 7.25 \times 3.1}{2} \right) + \left(\frac{2.46 + 2.25}{2} \times 5.73 \times 3.1 \right) + \left(\frac{2.46 \times 0.77 \times 3.1}{2} \right) - \left(\frac{4.94 \times 3.1416 \times 5.68}{2} \right) \div 27 = 8.86 \text{ Cu. Yds.}$$

$$\text{Steel } 10 - 3/4 \text{ } \# \text{ } 5.33 \text{ Long} = 53.3 \text{ at } 1.91 \text{ lbs per ft.} = 102 \text{ Lbs.}$$

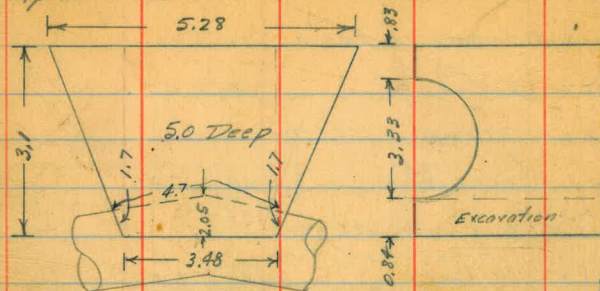
$$\text{Excavation } \left(\frac{8.5 + 5.05}{2} \right) \times 4.14 \times \left(\frac{0.84 + 1.9}{2} \right) \div 27 = 1.42 \text{ Cu. Yds.}$$

$$\text{Cement } 43 \text{ sacks} = 10.75 \text{ bbls.}$$

Comptd M.R.S.
chd J.H.H.

chkd. by
A.C.L.

Pipe Anchor Sta 145+47.87



$$\text{Concrete } \left(\frac{5.28 + 3.48}{2} \times 3.1 \times 5 \right) - (5.02 \times 4.09) \div 27 = 1.76 \text{ Cu. Yds.}$$

$$\text{Excavation } \left(\frac{5.28 + 3.48}{2} \times 3.1 \times 0.84 \right) \div 27 = 0.42 \text{ Cu. Yds.}$$

$$\text{Cement } 10 \text{ sacks} = 2.5 \text{ bbls.}$$

$$\text{Steel } 6 - 3/4 \text{ } \# \text{ } 5.33 \text{ Long at } 1.91 \text{ lbs per ft.} = 61 \text{ Lbs.}$$

Calc. M.R.S.

chd J.H.H.

Misc. Concrete Structures Continued on Page 37

ch. by
A.C.L.

STEEL PIPE 36"

Hill 1930

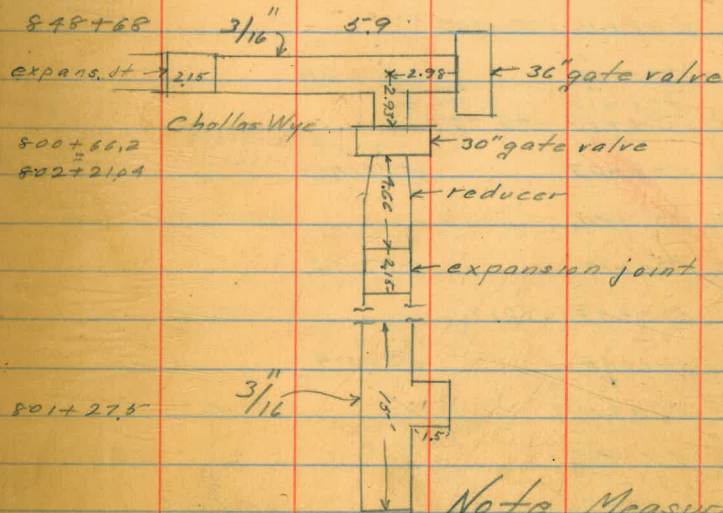
SPECIALS

14

Station to	Station	3/16" Lin.ft.	1/4" Lin.ft.	5/16" Lin.ft.	3/8" Lin.ft.
855+12.05	853+73.70	142.65			
853+73.70	846+22.20		768.07		
846+22.20	838+80	768.10			
838+80	819+13.5		1965.40		
819+13.5	814+25		985.09		
814+25	804+17		1009.13		
804+17	759+02	4676.96			
759+02	749+20		999.90		
749+20	718+79	3062.56			
718+79	713+88		503.42		
713+88	696+78	1721.60			
696+78	682+00		1487.30		
682+00	679+90		209.20		
679+90	674+47		553.00		
674+47	627+11	4751.50			
627+11	617+78		945.50		
617+78	596+55	2151.30			
596+55	590+08		658.92		

(cont. on next page)

Station	3/16" Lin.ft.	1/4" Lin.ft.	5/16" Lin.ft.	3/8" Lin.ft.
852+10	27.5			
849+95	34.25			
848+68	5.9			
expans. jt	2.15			
800+66.2				
802+21.4				
801+27.5				
769+50	5.22			
768+64	18.35			
767+75	11.62			
754+38	20.00			
748+54	25.60			
718+45	20.43			
691+00	12.12			
680+17	30.08			
671+02	31.20			
620+17	14.87			
616+25	23.40			
615+94	14.10			



Note Measurement of specials discontinued as it was impossible to determine exact length on account of wrapping.

STEEL PIPE 36" (cont.)

Station to Station	3/16" Lin. Ft.	1/4" Lin. Ft.	5/16" Lin. Ft.	3/8" Lin. Ft.
590+08 563+40	270.15			
563+40 558+90		469.35		
558+90 551+11	795.02			
551+11 536+65		1951.90		
536+65 535+18	149.97			
535+18 534+88	179.97			
534+88 529+83		541.19		
529+83 522+96			705.67	
522+96 520+10		292.10		
520+10 512+98			718.70	
512+98 571+18		179.84		
571+18 490+30			2109.40	
490+30 461+62				2890.97
461+62 450+22			1148.53	
450+22 439+92		1036.79		
439+92 430+45	948.33			
	22,355.23	12,852.11	4,891.50	2,890.97

40" PIPE

430+45 411+20	1930.64			
411+20 405+ ³³ 84		591.90		
405+ ³³ 84 397+84		621.90		
397+84 394+80			772.15	
394+80 395+10			742.15	
395+10 362.04	3286.05	314.20		
362+04 360+68	3316.05	284.20		
360+68 352+53			137.65	
352+53 350+50				824.50
			205.95	

SPECIALS

15

Station	3/16" Lin. Ft.	1/4" Lin. Ft.	5/16" Lin. Ft.	3/8" Lin. Ft.
608+10	12.10			

STEEL PIPE 40" (cont)

16

Station to Station	^{3/16} Lin. ft.	^{1/4} Lin. ft.	^{5/16} Lin. ft.	^{3/8} Lin. ft.
350+50	344+53	606.95		
344+53	342+25		228.73	
342+25	330+74	1167.95		
330+74	328+22		257.45	
328+22	318+55	974.08		
318+55	312+73		587.70	
312+73	311+24	149.80		
311+24	309+06		226.40	
309+06	298+20	1094.10		
298+20	286+98		Tunnel #4 1126.43	
286+98	227+56	5979.37		
227+56	224+31	343.70		
224+31	205+00		Tunnel #3 1931.50	
205+00	192+03	1303.75		
192+03	171+97		Tunnel #2 2009.52	
171+97	167+84	413.45		
167+84	145+70		Tunnel #1 2221.73	
145+70	106+08	3991.66		
106+08	103+83		230.35	
103+83	68+06	3660.15		
68+06	66+53		158.76	
66+53	51+94	1485.92		
51+94	39+05		1305.84	

STEEL PIPE 40" (cont)

Station to Station	3/16" Lin. Ft.	1/4" Lin. Ft.	5/16" Lin. Ft.
39+05 21+86	1755.20		
21+86 19+25		275.41	
19+25 1+17	1832.21		
	30,799.45	11,809.52	772.15

Note ^{51+33.5} ~~at~~ ~~the~~ ~~End~~ ~~of~~ ~~the~~ ~~Branch~~
at ~~the~~ ~~End~~ ~~of~~ ~~the~~ ~~Plant~~

2

18

APPURTENANCES

Reducers, Tees, Wyes and Expansion Joints 20

Item 18	Item 19	Item 20	Item 21	Item 22
40" x 36" x 1/4"	40" x 30" x 1/4"	40" x 28" x 1/4"	36" x 30" x 1/4"	36" x 28" x 1/4"
reducer	reducer	reducer	reducer	reducer

Item 23	Item 24	Item 25	Item 26	Item 27
36" x 36" x 20"	40" x 40" x 36"	36" x 36" x 36"	40" expansion	36" expansion
Tee	wye	Tee	joints	joints

800+82
800+66.2
802+21.09
802+16
802+10
801+27
658

1

1

1

1

1

2

discontinued

Appurtenances (cont.)

Station	Item 28 36" gate valve	Item 29 30" gate valve	Item 30 28" gate valve
800+6620			
802+2101	1	1	
658		1	

Item 31 4" air valve private R/W	Item 32 4" air valve Sts. & Road	Item 33 4" blow off trestles	Item 34 4" blow off trestles	Item 40 4" pipe
855+08	2			
				10.75

~~discontinued~~

Byler
King
OTTEN

ELEV'S. OF VARIOUS METERS
GAGES & VALVES

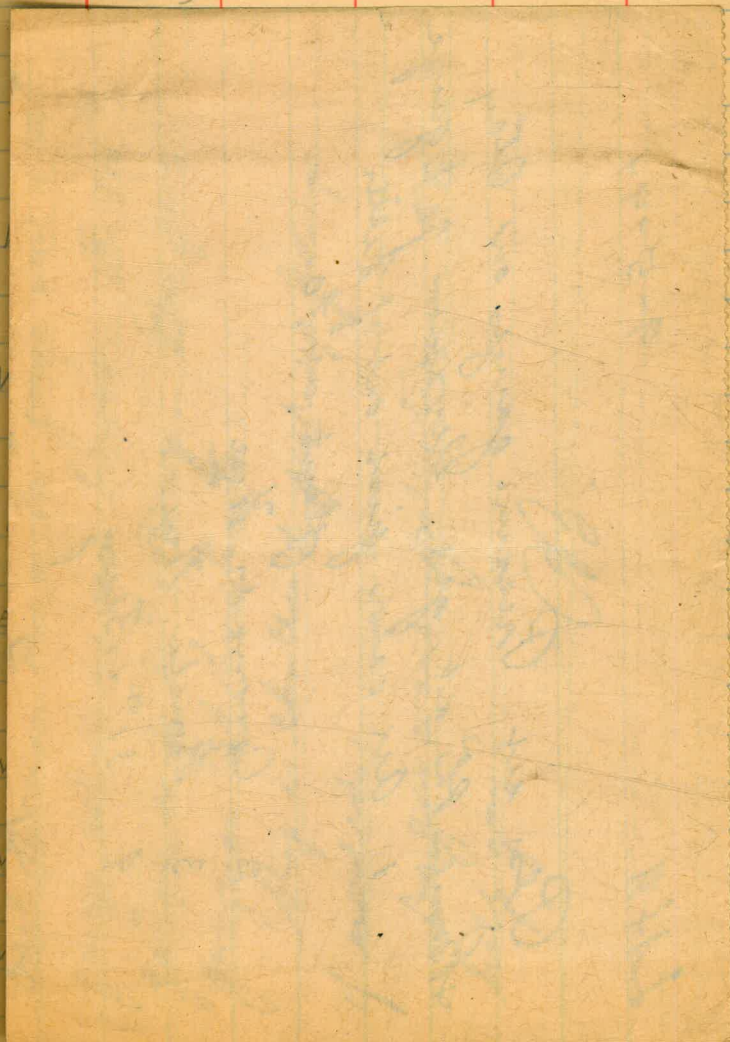
22

1-26-44

OTAY FILTER PLANT

	B.S.	H.I.	F.S.	ELEV.	LOCATIONS
	3.53	408.28		404.75	B.M. Cross on end of Small retaining Wall S.W. COR. Main Bldg.
T.P.			0.00	408.28	
	12.20	420.48			
BRISTOL Press. Meter			1.10	419.38	
WASH Water Meter			0.69	419.79	
Center Table gauge			1.31	419.17	
Sparkling Wash gauge			0.83	419.65	
CHlor. Press. ga.			0.96	419.52	E.W.
WASH Press. ga.			0.95	419.53	E.W.
Domestic Press ga.			0.84	419.64	E.W.
HVD. Valve Press gauge			0.84	419.64	E.W.

(Continued)



LHA

9-5-44

Please set Pressure gauges on Stay
+ Bould PL at get Elevation of gauge

1. Air valve just out of Filter
plant at 50.

2. Coronado Wye.

3. Bould Wye

4. 31st + Bldg

Earl Thomas has a 200th gauge and a 100th
gauge which we can borrow. The 200th
gauge is for 31st + Bldg. Please put
gauges on 24 hr charts:

Stop at Challen to pick up fittings
if needed.

Do you want patrolman to
help you?

AB.

Byler
King
OTTEN

ELEV'S. OF VARIOUS METERS
GAGES & VALVES

22

1-26-44

OTAY FILTER PLANT

	B.S.	H.I.	F.S.	ELEV.	LOCATIONS
	3.53	408.28		404.75	B.M. Cross on end of Small retaining wall S.W. COR. Main Bldg.
T.P.			0.00	408.28	
	12.20	420.48			
BRISTOL Press. Meter			1.10	419.38	West Wall in office SO. END Main Bldg.
WASH Water Meter			0.69	419.79	W. Wall in office SO. END Main Bldg.
Center Table gauge			1.31	419.17	Center Table OPER. FLOOR
SPARKING Wash gauge			0.83	419.65	E. Wall CENTR. OPER. FLOOR.
CHLOR. Press. ga.			0.96	419.52	E. Wall in office SO. END Main Bldg.
WASH Press. ga.			0.95	419.53	E. Wall in office SO. END. Main Bldg.
Domestic Press ga.			0.84	419.64	E. Wall in office SO. END. Main Bldg.
HVD. Valve Press gauge			0.84	419.64	E. Wall in office SO. END Main Bldg.

(Continued)

Elev's. Meters Etc. (Cont.)

23

O'Day Filter Plant

CHLORINE HOUSE

	3.05	407.80	404.75	B.M. "X" ON SO. END of retaining wall near S.W. Cor. Main Bldg.
No. Chlorine gauge		2.74	405.06	No. gauge
" "		2.75	405.05	Center gauge
So. " "		2.81	404.99	So. gauge
Floor Elev.				

PUMP HOUSE

	0.03	396.43	395.80	B.M. ON steel dowel in most westerly of two 12"X12" concrete piers west of stand by pump house
Pressure gauge		4.38	392.0	ON 8" WASH line
Pressure gauge		5.08	391.3	ON 3" D.M. line
Pressure gauge		8.85	387.6	ON 1 1/2" chlor. line
Floor El.		10.7	385.7	

(Continued)

ELEV'S. METERS ETC. OTAV FILTER
PLANT (CONT.)

24

Emergency Standby Plant

396.43

Pressure gauge

4.1

392.3

1 1/2" Chlor line

Pressure gauge

3.2

393.2

2" Domestic line

Floor Elev.

5.2

391.2

Addtl. Elevs on Pipes Otago P. Plant

B.M. 4.23 407.77 403.54

2.00 405.77

8.88 398.89

12.98 394.79

8.8 399.0

9.2 398.6

10.1 397.7

12.8 395.0

XON END Retaining Wall S.W. Cor. Filter House

Top 36" Pipe at Pt A

Top 40" " " " A

Concrete Floor at Pt. A

Top 40" Pipe at Pt. 36" 40" JOIN

Top stem ON bypass Gate ON 40" PL

Top stem ON Blow off Gate ON 40" PL

Ground Elev. at Blow off

Byler King
often
1-26-44

LEVELS FOR ESTABLISHING B.M.
ON OTAY DAM

27

	B.S.	I.I.	F.S.	ELEV.	B.M.
	12.90	417.65			404.75
T.P.			0.06	417.59	ON 2" PIPE UNION
	12.63	430.22			
T.P.			0.56	429.66	ON ROCK
	12.37	442.03			
T.P.			0.03	442.0	ON ROCK NEAR ROAD
	12.85	454.85			
T.P.			0.29	454.56	ON ROCK SO. OF ROAD NEAR 1 st CABIN
	12.81	467.37			
T.P.			0.20	467.17	ON ROCK IN ROAD
	12.84	480.01			
T.P.			0.17	479.84	ON ROCK IN ROAD
	12.00	491.84			
T.P.			0.26	491.58	ON ROCK IN ROAD.
	12.05	503.63			
T.P.			0.18	503.45	ON ROCK NO SIDE ROAD
	12.13	515.58			
T.P.			0.22	515.36	ON ROCK SO SIDE ROAD
	12.44	527.80			
T.P.			0.23	527.57	ON ROCK E. OF FLAGPOLE
	11.01	538.58			
			9.34	529.24	ON N.E. COR. TOP OF FLAGPOLE base
T.P.			5.61	532.97	
	0.51	533.48			
T.P.					

SEE PAGE 22

520.2/4
528.56

	533.48		
T.P.	0.84	521.30	13.02 520.46
T.P.	0.15	509.12	12.63 508.67
T.P.	4.34	503.19	10.27 498.85
B.M.	4.31	502.33	5.17 498.02
			0.79 501.54
	Check Back		
			498.02
T.P.	11.69	509.71	0.42 509.29
	13.03	522.32	
T.P.			0.13 522.19
	12.42	534.61	
T.P.			1.96 532.65
	6.70	539.35	
TP			10.11 529.24
	0.56	529.80	
T.P.			13.01 516.79
	0.40	517.19	
			13.05 504.14
T.P.	0.08	504.22	

ON ROCK IN \angle of Road

ON ROCK IN \angle of Road

ON ROCK $\&$ Road. 30' from gate

Set B.M. ON So. end of westerly Ist BEAM
UNDER gage tower Top Lower Ody Dam
Pointer on water height gage.

B.M. ON DAM

ON ROCK IN \angle Road

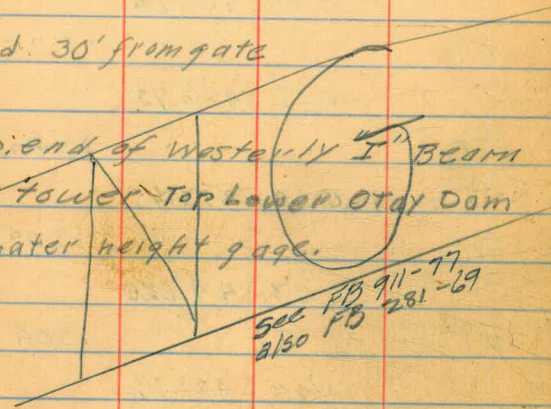
ON ROCK $\&$ Road

ON ROCK $\&$ Road

ON flag pole base (check)

ON ROCK $\&$ Road

ON ROCK So.



See PB 911-77
also PB 281-69

		504.22			
T.P.			12.69	491.53	on Rock No. Side of Road
	0.21	491.74			
T.P.			12.99	478.75	on Rock so. Side of Road.
	0.54	479.29			
T.P.			12.78	466.51	on Rock E Road
	0.27	466.78			
T.P.			13.10	453.68	on Rock so. Side Road
	0.23	453.91			
T.P.			13.09	440.82	on Rock W. of Road
	0.38	441.20			
T.P.			13.04	428.16	on Rock near Tel.
	0.00	428.16			
T.P.			12.44	415.72	
	1.13	416.85			
B.M.			12.11	404.74	404.75 (check)

MISCELLANEOUS STRUCTURE EXCAVATION

30

Connection at Lantana $1 \times 2.8 \times 4.0 = 0.42 \text{ C.Y.}$
27

8" x 16" connec's at 54th St. $1.5 \times 3.0 \times 5.0 \times 2 = 1.66 \text{ C.Y.}$
27

Expans. jt. at sta. 800+82 $1.5 \times 6.0 \times 6.0 + 1.0 \times 5.0 \times 6.0 = 3.11 \text{ C.Y.}$
27

Expans. jt. at sta. 802+10 same as above 3.11 C.Y.

Tee, sta. 801+28 $2.7 \times 4.5 \times 5.0 = 2.25 \text{ C.Y.}$
27

Anchor 10' West of P.L. 802+21.00 = 800+66.20
 $1.3 \times 5.5 \times 8.6 + 1.0 \times 6.7 \times 8.6 = 4.41 \text{ C.Y.}$
27

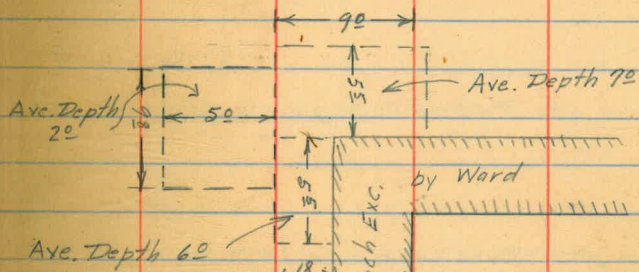
Anchor & Expansion Jt. 802+10 $(6 \times 6 \times 5.6) - (4.5 \times 4.2 \times 6) = 3.27 \text{ C.Y.}$
27

Calc. M.P.S.
Chkd. M.P.S.

15.12

Structure Exc. at Gate Valve

Sta 802+21.00 = 800+66.20



$$(9.0' \times 7.0' \times 5.5') + (9.8' \times 5.0' \times 2') + (1.8' \times 5.5' \times 6.0') = 18.66 \text{ C.Y.}$$

27

Calc. M.P.S.
Chkd. M.P.S.

Note: This Excav. was checked from figures as given. A.C.L.

Structure Excar. (cont.)

Blowoff at sta. 774+20 - $\frac{2.0 \times 2.5 \times 5.0}{27} = 0.93$ s.

4" connection sta. 742+81 = $\frac{1.2 \times 2.3 \times 5.0}{27} = 0.51$ s.

2" connection sta. 733+25 = $\frac{1.0 \times 2.4 \times 5.0}{27} = 0.44$ s.

10" connection sta. 707+08 = $\frac{1.5 \times 4.0 \times 5.0}{27} = 1.11$ s.

Excavation for 10" connection at sta. 700 thru error in work order - same dimensions as above = 1.11

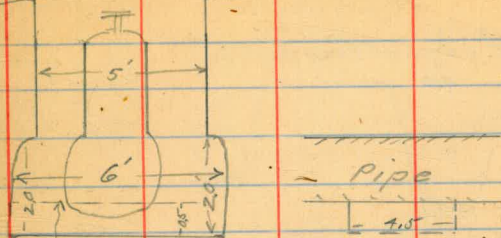
6" connections sta. ⁶⁷⁸⁺³⁵ $\frac{2.0 \times 5.0 \times 5.0 \times 2}{27} = 3.70$ s.

Expans. jt. at sta. 658+30 = $\frac{1.5 \times 6.0 \times 6.0}{27} + \frac{1.0 \times 5.0 \times 6.0}{27} = 3.11$ s.

Expans. jt. at sta. 657+20 - same as above 3.11

Note: This Excavation was checked from figures as given. A.C.L. ^{Calc. 1/10/06} Chkd M.D.G. 14.04 s.

Gate valve at sta. 657+93



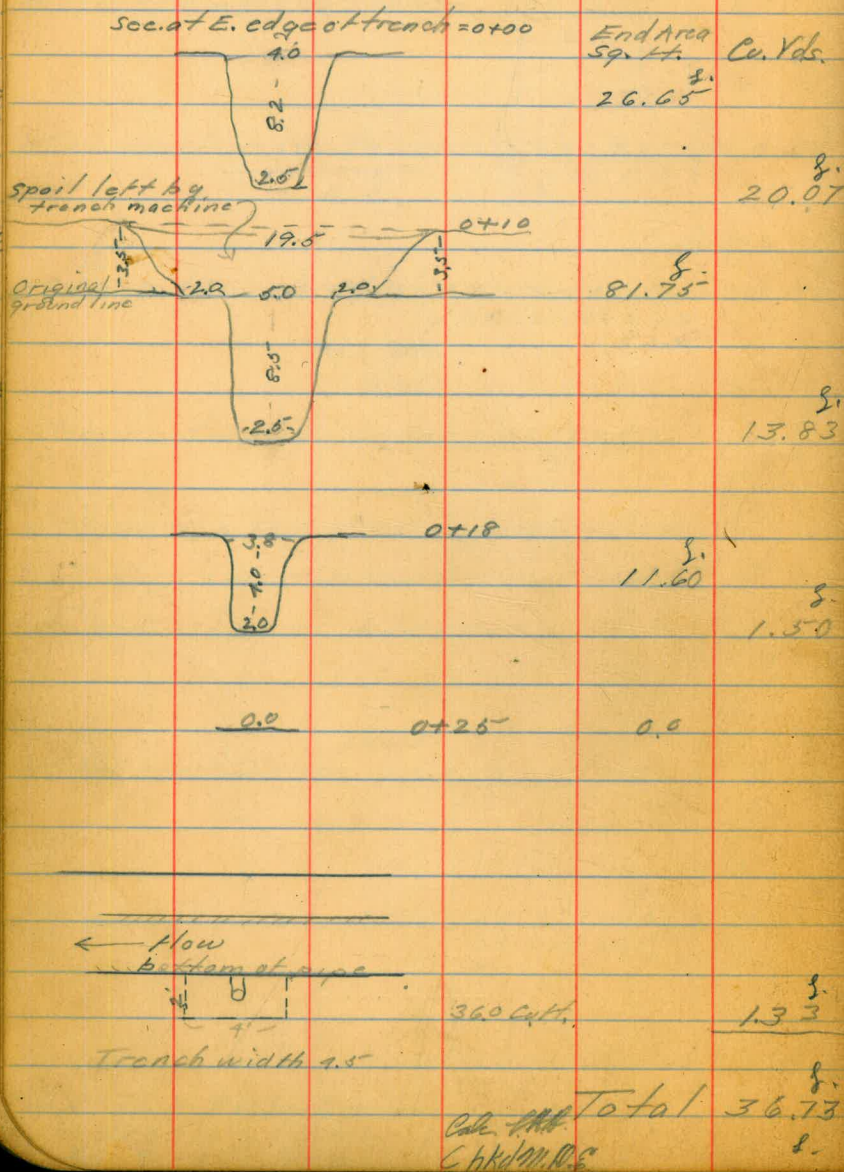
Pipe grade

$\frac{0.5 \times 5.0 \times 4.5}{27} + \frac{2.0 \times 4.5 \times 0.5 \times 2}{27} = 0.76$ C.Y. s.

Calc. 1/10/06
Chkd M.D.G.

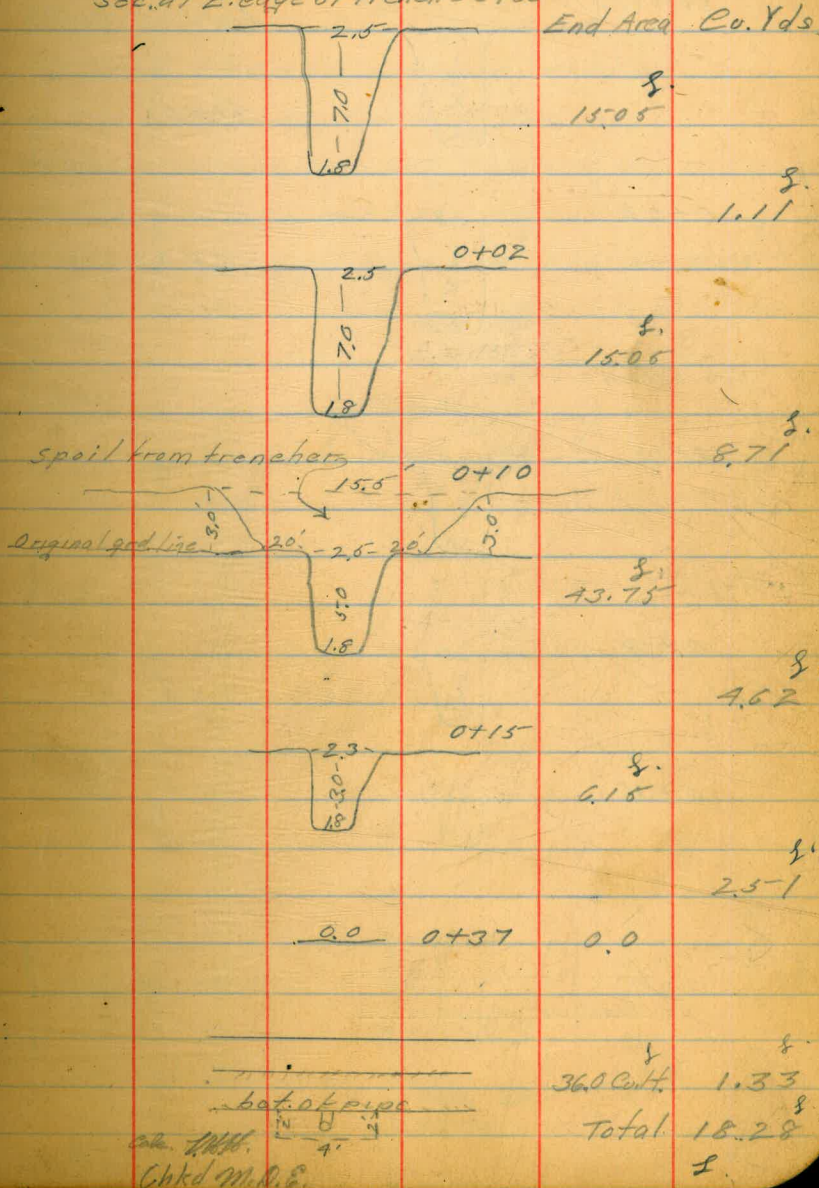
Structure Excavation (cont.)

Blow off at sta. 650



Blow off at sta 646+50

Sec. at E. edge of trench = 0+00



Structure Excavation (cont.)

Blowoff at sta. 636+65

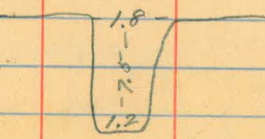
0+00 = E side of trench



End Area Cu. Yds.
s.
11.25
s.
0.83

1" connections at stations
657+00, 634+25, 615+08, 508+16,
507+23, 502+06, 501+15, 500+36,
197+95, 195+40, 154+10, 356+00, 312+15 (2' canose)
277+24, 238+80, 13+28.

0+02

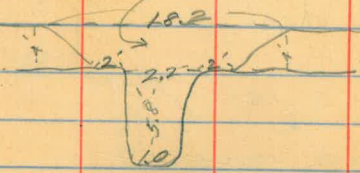


s.
11.25

Ar. dimens. $\frac{1.0 \times 2.4 \times 50}{27} = 0.44 \times 16 = 7.04$ Cu. yds.

Calc. ~~11/11~~
Chkd M.D.E.

Spoil from trencher



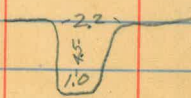
s.
10.27

0+10

s.
58.08

s.
9.67

0+18



s.
7.20

0+36



s.
3.57
s.
3.50

bat. of pipe
16' x 16'

360 Cu. ft. 1.33

Calc. ~~11/11~~
Chkd M.D.E.

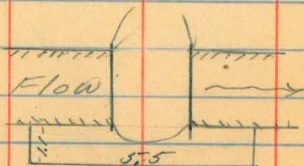
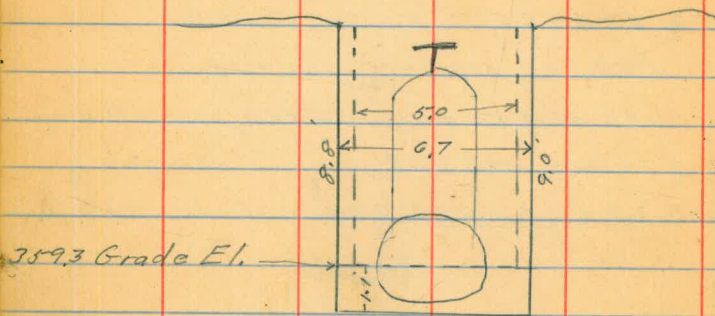
Total 25.67

s.

s.

Structure Excav. (cont.)

Gate Valve at sta. 430+51



$$5.5 \times 5.0 \times 1.1 = 30.25 \text{ cu. ft.}$$

$$5.5 \times 8.8 \times 0.85 = 41.14 \text{ " "}$$

$$5.5 \times 9.0 \times 0.85 = 42.08 \text{ " "}$$

$$113.47 \text{ cu. ft.} = 420 \text{ C.Y.}$$

calc. T.H.H.
ckd M.R.E.

34

Exp. joint at 430+88

$$\left. \begin{array}{l} 1.7 \times 5.0 \times 6.0 \\ 1.5 \times 5.0 \times 6.0 \end{array} \right\} \div 27 =$$

cu. yds.
3.56

Exp. joint at 429+69

$$\left. \begin{array}{l} 1.6 \times 5.0 \times 4.1 \\ 1.7 \times 4.8 \times 4.1 \end{array} \right\} \div 27 =$$

2.07

5.63

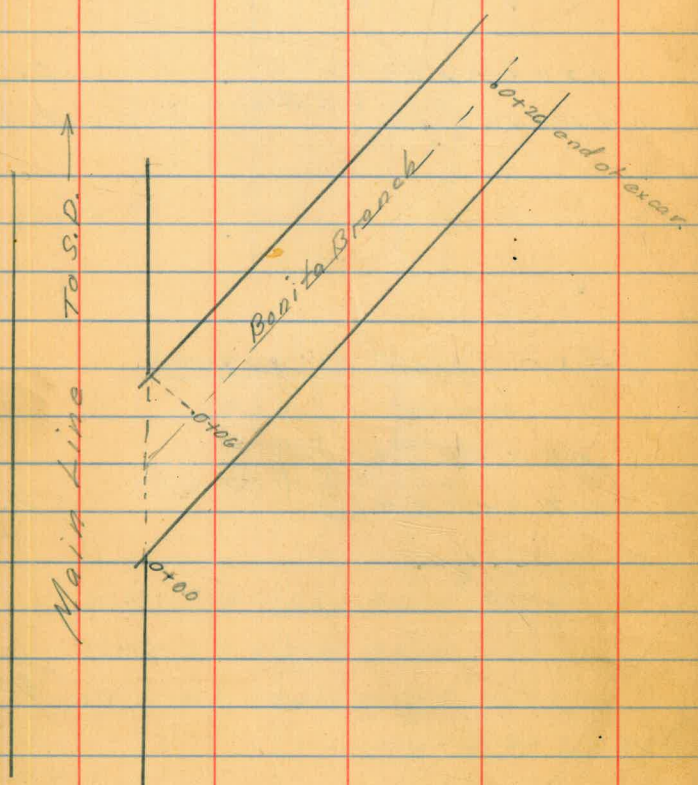
calc. T.H.H.

ckd M.R.E.

L.

Structure Excav. (cont.)

Bonita Wye Branch



Station	End Area	Cu. Yds.
Intersect. S.D. line of branch with M.L. 0+00	0.0	0.0
0+06	58.50	6.50
0+10	64.31	9.10
0+13	52.80	6.51
0+21	36.36	13.21
0+24	22.00	3.24
0+25	0.00	0.41
		38.97

calc. I.H.B.
Chkd M.R.E.

Structure Excav. (cont.)

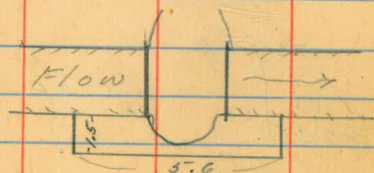
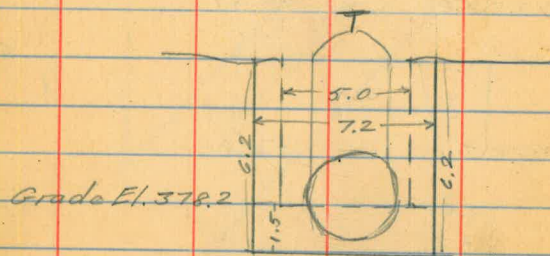
36

Exp. joint at 307+24

$$\left. \begin{array}{l} 2.0 \times 6.0 \times 3.7 \\ 2.0 \times 6.5 \times 3.7 \end{array} \right\} \div 27 =$$

Cu. Yds.
3.15

Gate Valve at 306+21



$$\left. \begin{array}{l} 6.2 \times 5.6 \times 2.2 \\ 5.0 \times 5.6 \times 1.5 \end{array} \right\} \div 27 =$$

Cu. Yds.
1.38

Exp. joint at 305+20

$$\left. \begin{array}{l} 1.8 \times 5.0 \times 4.0 \\ 2.0 \times 4.5 \times 4.0 \end{array} \right\} \div 27 =$$

Cu. Yds.
2.67

calc. T.H.B. chkd M.R.E.

10.20

Exp. jt. at 136+94

$$\left. \begin{array}{l} 1.5 \times 5.0 \times 4.0 \\ 1.5 \times 4.8 \times 4.0 \end{array} \right\} \div 27$$

Cu. Yds.

2.18

6" connection at 135+88

$$\frac{2.0 \times 2.0 \times 1.0}{27} =$$

Cu. Yds.

0.15

6" connection at 135+65

$$\frac{1.0 \times 1.0 \times 1.0}{27} =$$

Cu. Yds.

0.04

Gate Valve at 135+81

$$\left. \begin{array}{l} \text{S. side } 4.8 \times 4.1 \times 1.5 \\ \text{N. " } 6.5 \times 4.0 \times 0.8 \\ \text{Bottom } 5.0 \times 5.0 \times 0.9 \end{array} \right\} \div 27 =$$

Cu. Yds.

2.70

Exp. jt. at 134+50

$$\frac{1.0 \times 4.0 \times 6.0}{27} =$$

Cu. Yds.

0.89

5.96

Calc. T.H.B.
Chkd M.R.E.

Miscellaneous Concrete Structures 37
(Cont)

Venturi Meter Tube Box at Sta 5+19 (Drawing WD273)

Concrete

Walls $32' \times 0.5' \times 8' = 128.0 \text{ Cu.ft.}$

Floor $7' \times 10' \times 0.5' = 35.0 \text{ Cu.ft.}$

Pier $\frac{(1.8 \times 2.4) + (1.1 \times 2.0)}{2} \times 1.85 = 6.03 \text{ Cu.ft.}$
 169.03 Cu.ft.

Supplanted by pipes

$(1.17^2 \times 3.1416 \times 0.5) + (1.0^2 \times 3.1416 \times 0.5) = 3.72 \text{ Cu.ft.}$

hd seat $2' \times 3' \times 3' = 1.29 \text{ Cu.ft.}$

$169.03 - 5.01 = 164.02$

6.07 C.Y. Conc.

Steel

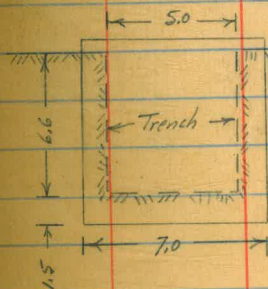
27 pcs $\frac{3}{8}'' \times 6.75' = 182.25$

24 pcs $\frac{3}{8}'' \times 9.75' = 234.0$

34 pcs $\frac{3}{8}'' \times 8.25' = 280.5$

$3.696.75 \text{ at } .38 \text{ lbs./ft.} = 265 \text{ lbs}$

Excavation



$\frac{(8.1 \times 7.0 \times 1.0) - (6.6 \times 5.0 \times 1.0)}{27} = 8.78 \text{ C.Y.}$

Cement 34 sacks

= 8.5 bbls.

6" Concrete Conduit Pipe F.W.O.

= 13 lin. ft.

Ladder Rungs

= 5

Calc. M.P.B.
and T.H.H.

chd. A.C.L.

Excavation + Drain tile at Exit Tunnel # 4

Sta.	Depth x Width	Cu. Yds.	
0+00	1.0 x 1.7	8.0	0+00 →
		0.49	
0+06	1.6 x 1.7	1.91	
0+27	1.3 x 1.7	2.33	
0+64	0.7 x 1.7	0.06	
0+66	0.3 x 1.7	2.57	
0+82	4.8 x 1.7	3.59	
1+02	0.9 x 1.7 End Pipe	0.34	0+66 →
1+14	0.0		
Total Exc.		11.29 ³ Cu. Y.	← 13' ± →
		102' of 6" tile.	

6" tile drain

2nd Main Pipe Line

Comptd M.A.C.
Ch. 2/11/11

Structure Exc. (cont)

Excavation and Tile Ent. Tunnel #3

Sta	Depth x Width	Cu. yds
0+00	1.0 x 1.67	8.106'
0+10.7	2.2 x 1.67	8.438'
0+50	1.4 x 1.67	8.247'
0+92	0.5 x 1.67	8.215'
1+50	0.7 x 1.67	8.199'
1+90	0.9 x 1.67	8.260'
2+50	0.5 x 1.67	8.139'
3+00	0.4 x 1.67	8.058'
3+03.5	5.0 x 1.67	8.226'
3+10	6.2 x 1.67	8.479'
3+22	6.7 x 1.67	8.492'
3+37	3.9 x 1.67	8.144'
3+49	0.0	8.

30.03 Cu. yds total excavation.

205+10 = 0+00

209+18 = 0+92

202+10 = 3+00

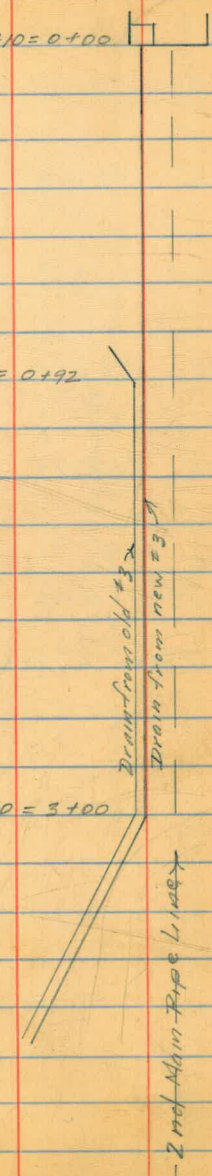
3+49

For old Tunnel 261

For New Tunnel 348

609 lineal ft. of 6" tile.

Completed 11/11/02



Excavation + Tile Exit Tunnel #2		
Sta.	Depth x Width	Cu. Yds.
192+315	1.0 x 1.7	3.50
192+76	1.5 x 1.7	2.83
193+06	1.5 x 1.7	1.87
193+23	2.0 x 1.7	3.78
193+53	2.0 x 1.7	0.19
193+56	0.0	0.0
Total Exc.		12.17 Cu. Yds
Total 6" pipe		123 Lin. ft.

2nd Main Pipe Line

Compld. M.D.E. 10/29/30
 Chkd. ~~W.B.~~ S.

Excavation + Tile Entrance Tunnel #1		
Sta.	Depth x Width	Cu. Yds.
145+90	1.0 x 1.5	1.20
145+74	1.7 x 1.5	6.37
145+00	1.4 x 1.5	16.11
143+00	1.5 x 1.5	8.75
141+50	0.6 x 1.5	0.19
141+49	6.2 x 1.5	1.95
141+43	5.5 x 1.5	1.94
141+36	4.5 x 1.5	0.61
141+32	1.0 x 1.5	0.06
141+30	0.0	0.0
Total Exc.		39.18 Cu. Yds
Total 6" pipe		459 Lin. ft.

2nd Main Pipe Line
 Drain tile

Compld. M.D.E.
 Chkd. ~~W.B.~~ I.

TOTAL QUANTITIES

Structure Excavation ✓	606.11	Cu. Yds.
Douglas Fir lumber ✓	3,344	M.B.M.
Concrete	391.89	Cu. Yds.
Reinforcing Steel ✓	16,942	Libs.
Cement	573.05	Bbls.
6" Concrete Drain Pipe	1293	Lin. ft.

Calc. M.R.S. 11/2/30
Chad 2/15/30

TRESTLE QUANTITIES AND MISC. STRUCTURES 02

Structure -	from Page this vol.	Cu. Yds. Concrete	Bbls. Cement	Summarized by A.C.L. 11/19/30
Trestle No. 39	1	5.28	7.5	1.42
" 38		20.55	25.5	1.24
" 37		20.46	31.3	1.53
" 36		37.12	56.5	1.52
" 35		6.14	9.4	1.53
" 34		1.86	2.5	1.34
" 33		12.87	16.0	1.24
" 32		24.50	36.2	1.48
" 31		3.03	4.5	1.49
" 30	No Trestle #29	2.25	3.50	1.56
" 28		6.25	9.5	1.52
" 27		5.14	7.9	1.54
" 26		6.26	9.8	1.57
" 25		5.52	8.4	1.52
" 24		13.09	20.3	1.56
" 23		1.35	2.1	1.56
" 22		6.05	9.3	1.54
" 21		2.60	4.0	1.54
" 20	No Trestle #19	5.08	7.8	1.54
" 18		9.54	14.6	1.53
" 17		11.85	18.1	1.53
" 16		17.99	27.5	1.53
" 15		7.87	12.0	1.52
		232.65	344.20	Sub. Totals

(over)

TRESTLE QUANTITIES AND MISC. STRUCTURES - (CONT.)

Structure -	Cu. yds.	Bbls.	Brl. for work
	Concrete	Cement	
	232.65	324.20	
Trestle No. 14	9.84	15.1	1.53
" " 13	6.62	10.1	1.53
" " 12	2.26	3.5	1.55
" " 11	13.01	19.9	1.53
" " 10	7.85	12.0	1.53
" " 9	9.16	14.0	1.53
" " 8	2.26	3.6	1.59
" " 7	8.59	13.1	1.53
" " 6	7.21	11.0	1.53
" " 5	5.53	8.5	1.54
" " 4	2.04	3.1	1.52
" " 3	3.12	4.8	1.54
" " 2	3.59	5.5	1.53
" " 1	28.25	41.0	1.45
Concrete Box under P.R. Encanto	19.93	25.1	1.26
Anchor Block Sta. 508+93	1.65	2.2	1.33
Anchor Block Sta. 469+95	1.72	2.2	1.28
" " " 468+58	8.48	10.4	1.23
" " " 286+67	1.44	2.0	1.39
" " " 224+85	8.86	10.75	1.21
" " " 145+47 ⁸⁷	1.76	2.50	1.42
Venturi Meter Tube Box Sta. 5+19	6.07	8.5	1.40
Totals -	391.89	573.05	1.46

TRESTLE QUANTITIES AND MISC. STRUCTURES

Structure -	structure	Lumber	Reinforcing	Summarized by A.C.L. 11/19/30
	Excavation Cu. Yds.	F.B.M.	steel Pounds.	
Trestle No. 39	5.31	90.67	323	
" " 38	19.74	177.78	995	
" " 37	17.09	134.22	988	
" " 36	25.82	264.89	1541	
" " 35	8.18	47.11	283	
" " 34	1.70	47.11	169	
" " 33	10.17	90.67	497	
" " 32	18.93	177.78	871	
" " 31	4.08	47.11	201	
" " 30	3.02	—	180	
No Trestle No. 29				
" " 28	5.71	134.22	415	
" " 27	5.68	47.11	255	
" " 26	6.57	134.22	406	
" " 25	4.67	90.67	331	
" " 24	9.86	134.22	557	
" " 23	1.66	—	150	
" " 22	6.01	134.22	403	
" " 21	2.44	47.11	193	
" " 20	7.17	—	253	
No Trestle No. 19				
" " 18	5.60	90.67	419	
" " 17	8.65	134.22	526	
" " 16	9.59	177.78	687	
" " 15	6.15	90.67	373	
Sub Totals	193.80	2292.45	14,016	

TRESTLE QUANTITIES AND MISC. STRUCTURES (CONT.)

Structure	Structure Excavation Cu. Yds.	Lumber F.B.M.	Reinforcing Steel Pounds	Br. for wood
	193.80	2292.45	11,016	
Trestle No. 14	14.14	47.11	358	
" " 13	4.55	134.22	402	
" " 12	3.70	47.11	178	
" " 11	12.19	134.22	561	
" " 10	5.64	47.11	311	
" " 9	5.31	90.67	407	
" " 8	2.13	47.11	179	
" " 7	7.02	90.67	390	
" " 6	9.49	47.11	295	
" " 5	6.62	47.11	259	
" " 4	2.27	47.11	172	
" " 3	3.52	90.67	259	
" " 2	4.38	47.11	215	
" " 1	18.26	134.22	805	
Concrete Box Under RR Excavate	—	—	285	
Anchor Block Sta 508+93	0.40	—	35	
" " " 469+95	0.92	—	37	
" " " 468+58	9.08	—	299	
" " " 286+67	0.17	—	51	
" " " 224+85	1.42	—	102	
" " " 145+47 ⁸⁷	0.42	—	61	
Venturi Meter Tube Box Station	8.78	—	265	
* See Next Page -	24.90	—	—	
Totals	606.11	3,344 F.B.M.	16,942 lbs.	



MISC. STRUCTURES (CONT.) **

Structure -	Excavation Cu. Yds.	Tile Drain
See Page # 30 for Detail	15.12	
" " # 30 " "	18.66	
" " # 31 " "	14.02	
" " # 31 " "	0.75	
" " # 32 " "	36.73	
" " # 32 " "	18.28	
" " # 33 " "	25.67	
" " # 33 " "	7.04	
" " # 34 " "	4.20	
" " # 34 " "	5.63	
" " # 35 " "	38.97	
" " # 36 " "	10.20	
" " # 36 " "	5.96	
Tile Drain Tunnel #4 Page # 38	11.29	102 ft.
" " " # 3 " 39	30.03	609
" " " # 2 " 40	12.17	123
" " " # 1 " 40	37.18	459
	291.90	1293 ft. Total
		6" Drain

4. Profile - 36th St Revision - Boston, Birch, Vesta, Main.

B.M.	11.46	50.70		39.30
TP	1.81	50.54	1.97	48.73
81+00			6.7	43.8
+150 ⁷ f.			7.6	42.9
+50			10.0	40.5
82			12.2	38.3
+50			12.5	38.0
TP - Set B.M.	0.11	37.74	12.91	37.63
83			0.5	37.2
+50			2.3	35.4
84			3.8	33.9
+50			5.7	32.0
85			6.3	31.4
+50			7.2	30.5
86			9.6	28.1
+50			9.8	27.9
87			10.8	26.9
+50			13.0	25.7
TP	0.30	25.39	12.65	25.09
87+65			0.3	25.1
88+00			3.8	21.6
+50			10.2	15.2
TP	0.18	12.62	12.95	12.44
89			1.6	11.0
+50			4.2	8.4

Top F. Hyd. S. E. Cor. 36th & Northwood

Nail in power pole 8' R+83+30

On hub - 87+24³⁰

9/27/41
Soper
Brooks
Hodgson

45

12.62

90+00			6.1	6.5
+50			6.7	5.9
+64			9.3	3.3
+66			11.3	1.3
90+76 ⁷⁴			11.8	0.8
			5.7	6.9
			11.1	1.5
90+79			7.0	5.6
91+00			5.6	7.0
TP	3.98	10.73	5.87	6.75
91+50			4.1	6.6
92			4.2	6.5
+25			4.3	6.4
+42			1.1	9.6
+50			5.7	5.0
+55			9.1	1.6
+62			9.0	1.7
+68			4.2	6.5
93			4.9	5.8
+50 ⁴⁵			5.2	5.5
94			5.6	5.1
+30			4.9	5.8
+50			0.7	10.0
+60			7.6	3.1
+78			7.5	3.2

Rim sewer M.H 29' Rt 90+64
H.h. " " " "

(spoil pile from drain ditch)

{ in drain ditch

(spoil pile from drain ditch at Rt of E.)

10-73

94	180		5.8	4.9
95			4.9	5.8
95	1288 ^x		4.6	6.1
TI	6.22	13.16	3.79	6.94
			7.9	5.3
			16.5	-3.3
			11.5	1.7
95	150		6.9	6.3
96			6.7	6.5
+ 50			6.5	6.7
97			6.1	7.1
+ 50			5.8	7.4
98			5.6	7.6
+ 50			5.2	8.0
99			4.8	8.4
			9.8	3.4
+ 50			4.4	8.8
100			3.9	9.3
+ 50			3.3	9.9
101			2.6	10.6
+ 50			2.0	11.2
102			1.2	12.0
+ 50			0.5	12.7
TI	9.76	22.62	0.30	12.86
103			9.5	13.1

Set B.M. nail in power pole 46' LT 95+43

Rim of sewer M.H. 39' LT 95+15

F.L. " " " " " "

F.L. line 36" Conc. culv. 25' RT 95+09

F.L. 36" Conc. Culv. 35' RT 99+00

22.62

103	150		9.0	13.6
104			8.4	14.2
	+50		7.8	14.8
105			7.2	15.4
	+50		6.6	16.0
106			5.9	16.7
	+50		5.0	17.6
107			4.0	18.6
	+50		2.6	20.0
108			1.0	21.6
	+44 ³⁰	L	0.0	22.6
	+50		0.1	22.5
109			0.7	21.9
	IP	184 24.22	0.24	22.38
	+50		2.6	21.6
110			3.1	21.1
			3.3	20.9
			9.2	15.0
110	150		3.3	20.9
111			3.8	20.4
	+50		4.2	20.0
112			4.5	19.7
	+50		5.0	19.2
113			5.6	18.6
	+50		6.2	18.0

Rin sewer M. H. 5⁴ Rt 110 + 29³
 F.L. " " " "

24.22

114+00			6.7	17.5
			6.7	17.5
114+50			7.4	16.8
115			8.0	16.2
.50			8.5	15.7
116			9.0	15.2
TP	5.77	21.35	8.64	15.58
.50			6.1	15.3
117			5.2	16.2
.50			4.7	17.7
118			4.0	17.4
.50			4.0	17.4
119			4.6	16.8
.50			5.6	15.8
TP	4.82	19.78	6.39	14.96
TP	3.88	18.62	5.04	14.74
			5.16	13.52
B.M.	3.22	18.80		15.58
120 @ Main			3.2	15.6
121			5.3	13.5
122			6.9	11.9
123			8.8	10.0
124			10.2	8.6
FP	5.97	14.47	10.30	8.50

Rim sewer M.H. 5' RT 114+09 (covered with tar)

Set B.M. Point on curb return 25' LT 116+45

B.P. in curb S.W. Cor Main & Una.

Profile West of Main will probably change (Road is dug up for caving)

14.47

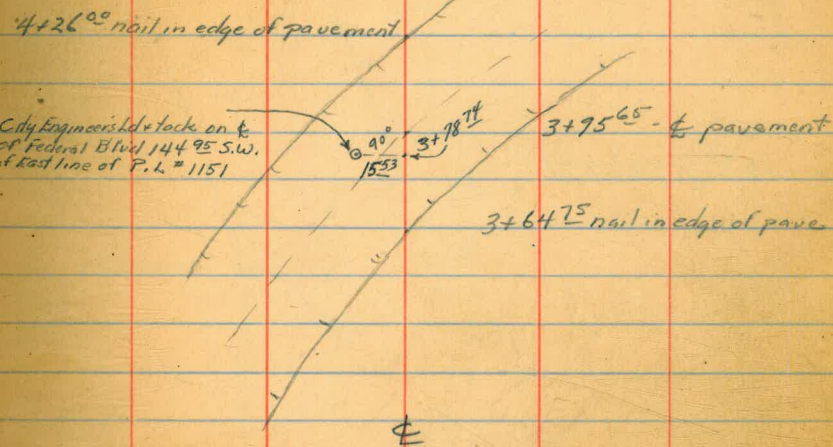
125	5.3	9.2	✓
126	4.7	9.8	✓
127	4.7	9.8	✓
128	5.0	9.5	✓
129	5.7	8.8	✓
+61	6.1	8.4	✓
	4.14	10.33	✓

Set B.M. Nail in guy pole

Relocation of 36th St pipeline on Federal Blvd. - Sta 2+90⁷³ to 9+15⁸³

10/16/41
Soper
Brook's
Hodgeson

51



3+58³⁵ L. 31°50' L

3+58³⁵ ← 37 →

3+50 ← 42 →

3+00 ← 57 →

2+50 ← 6° →

6°

Edge of Conc. Pave

2+09⁷³ - P.O.T.

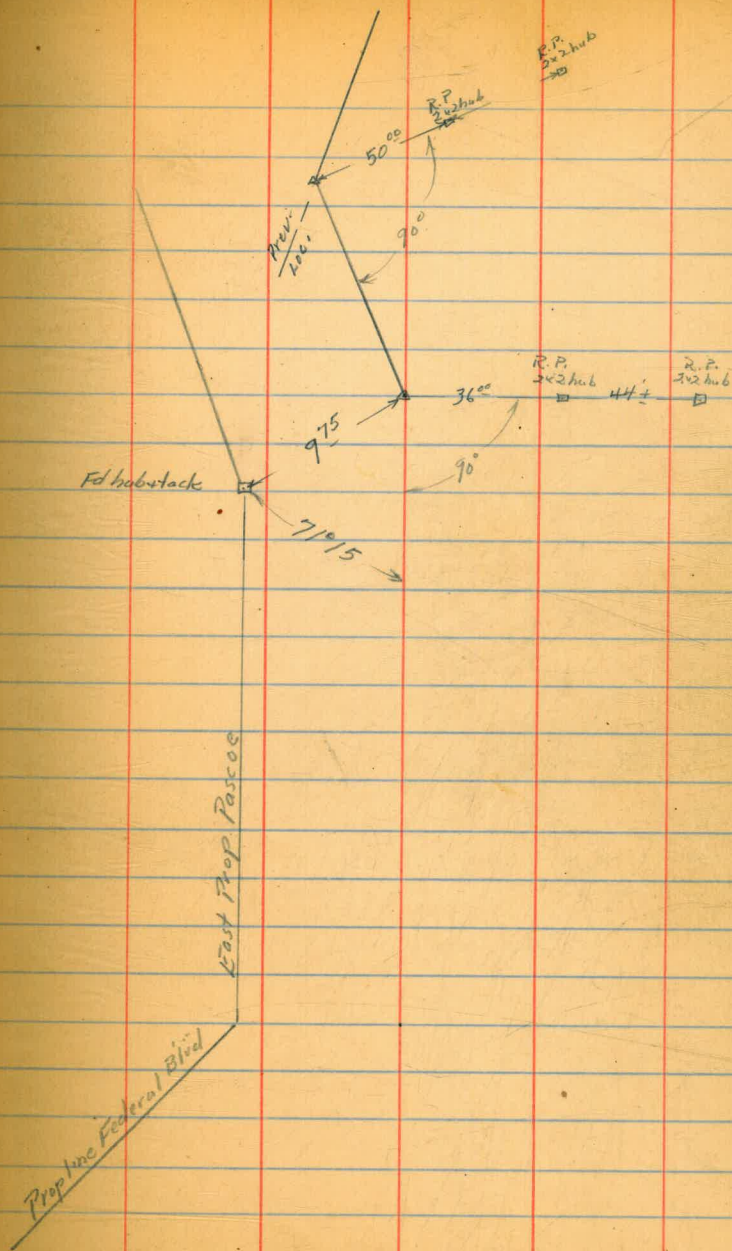
Cont'd from Book 289A page 77

Cont'd in Book # 289A - page 61

8+22 65° Ahead
9+15 85° Back \angle 25° 41' Rt to previous loc. - 10' west
of Pueblo lat line

6+10 41° \angle 34° 00' Lt

4+46 25° P.O.T



Profile 36th St Relocation Sta 2+09⁷³ - 9+15⁸⁵

B.M.	11.28	62.22		50.94
2+09 ⁷³			4.7	57.5
+50			5.2	57.0
3+00			5.7	56.5
+50			5.9	56.3
+58 ³⁵			5.9	56.3
-64 ⁷			5.9	56.3
+95 ⁵			5.5	56.7
4+36			5.9	56.3
+42			5.2	57.0
+46 ²			3.6	58.6
TP	12.37	74.56	0.03	62.19
4+52			10.0	64.6
5+00			4.1	70.5
TP	11.03	85.13	0.46	74.10
+25			8.7	76.4
+50			5.7	79.4
+68			4.4	80.7
6+00			6.0	79.1
+104 ¹ L			4.5	80.0
TP	12.63	97.34	0.42	84.71
6+50			11.5	85.8
7+00			3.9	93.4

Top of 1/2" pipe 10/4 1+13⁸ (1st alignment)

Edge of Pave.

φ " "

Edge " "

For final cross-sections page 79

LT	±	RT
71.3		63.1
3.3		12.5
12.0		12.1
81.1		21
4.0		33
10		66.6
78.9		18.5
6.2		23
7		69.9
85.1		15.2
2.0		24
10		73.3
85.1		11.8
0.8		21
6		76.5
85.1		6.6
0.0		15
3.0		
17		
7		
89.8		87.1
7.5		10.2
10		15
94.0		94.0
3.3		3.3
11		15

10/17/41
Soper
Brooks
Hedgecock

		97.34		
TP	12.10	109.33 ✓	0.11	97.23 ✓
7+50			8.6	100.7 ✓
8+00			2.0	107.3 ✓
TP	12.38	121.19 ✓	0.52	108.81 ✓
8+60			4.1	17.1 ✓
TP	12.02	133.06 ✓	0.15	121.04 ✓
8+90			11.2	21.9 ✓
9+00			8.2	24.9 ✓
9+15 ^{Back}				
8+22 ^{Ahead}			5.6	127.4 ✓
			2.2	130.9 ✓

Cont'd in Book 291 page 51

	LT		RT
110.3			107.6
+1.0			1.7
10			12
127.8			117.4
+6.6			3.8
20			10
			122.3
			10.8
			12
			124.1
			9.0
			10

ck on old Sta 8+50 Rec elev. 130.9

Slope stakes for bench excavation - bench grade is 10 feet above pipe grade, 15' base width, 1/4 to 1 slope.

Station	Offset	Top of Bench	Top of Pipe
17+00	7.3	162.4	155.1
17+50	5.1	157.3	152.2
16+88	8.7	153.7	142.00
17+00	7.3	155.1	148.7
1736	5.0	157.4	148.7
1754	5.3	157.1	149.3
1772	7.5	154.9	149.3
18+00	12.6	149.8	148.0

Bench grade 10' above pipe grade

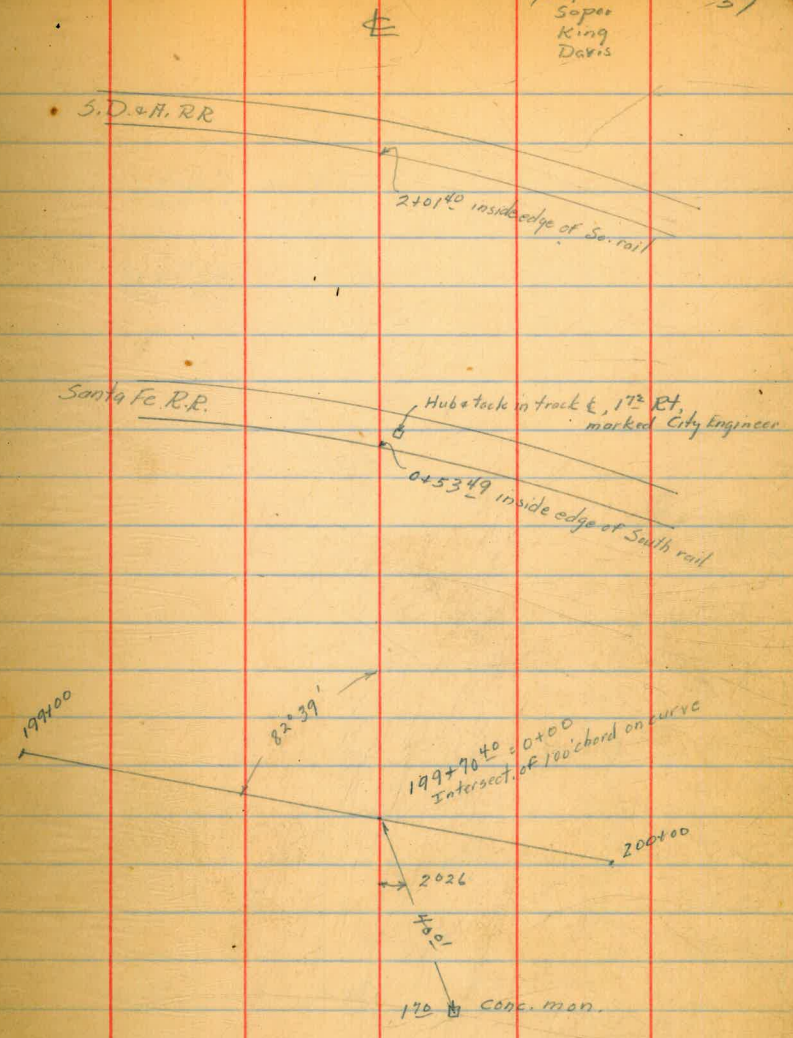
Rec. 157.3

Lt	Center	Rt
$\frac{C110}{102}$	112	$\frac{C118}{105}$
$\frac{C92}{92}$	94	$\frac{C96}{92}$
$\frac{C86}{96}$	87	$\frac{C86}{96}$
$\frac{C69}{92}$	78	$\frac{C82}{96}$
$\frac{C49}{82}$	56	$\frac{C62}{92}$
$\frac{C13}{72}$	18	$\frac{C24}{82}$

Pipeline location, from Sheltons location on Harbor Drive,
North on Vesta St. to intersection with 36th St location

0+00

5/27/42
Soper
King
Davis 57



3+68.3
water S.V. 6.3 →

3+51.5
Sewer M.H. 16.3 →

3+23 - F.H.H.
14.3 Rt



9+43.17 EC.

$\Delta 110^{\circ}00'$
R. 400
T. 3852
L. 76.79

~~8+88.71 $\Delta 15^{\circ}35'$ RT~~

8+66.38 BC.

8+62.29 EC.

$\Delta 10^{\circ}58'$
R. 400
T. 3810
L. 76.56

~~7+95.80 $\Delta 15^{\circ}35'$ RT~~

7+85.73 BC.

Oil Paving
Paving

to Vesta

1000

185

9+18.6

8+20

30

50

7+86 Sew. M.H. 16³

7+78⁵ water s.v. 6²

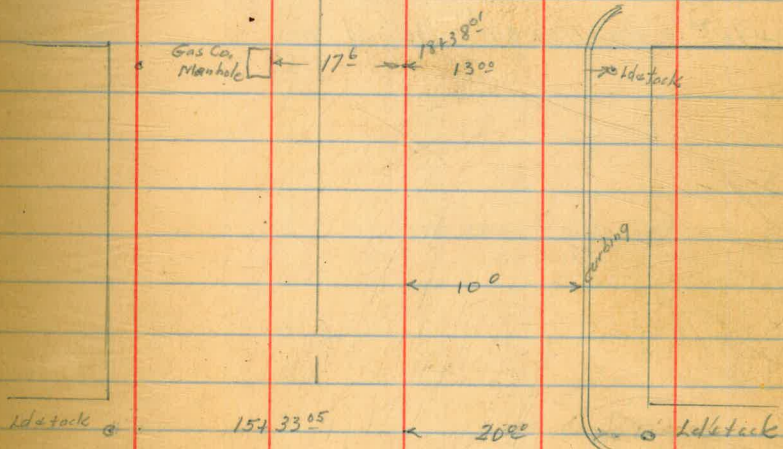
curb & gutter

E

Main St

18738⁰¹ P.O.T.

15433⁰⁵ P.O.T.



Filbert St

10⁰⁰
K. Resda St.

23+78³⁸ = Sta. 115+07³⁸ - 36th St line

⊕

⊙

⊙ 2402⁸⁰, G.V. 1^o RT

1000

⊕ Vesta St.

⊙ 18+65⁶⁵ G.V. 0⁶⁵ RT

⊕

Profile - Vesta St. Loc.

B.M.	2.24	12.37	10.33	✓
TP	3.95	11.32	5.20	7.37 ✓
set B.M.			3.38	7.94 ✓
			4.43	6.89 ✓
0+00			6.3	5.0 ✓
0+39			5.2	6.1 ✓
0+45			6.9	4.4 ✓
0+50			5.4	5.9 ✓
0+53 ⁴			4.62	6.70 ✓
0+58 ²			4.48	6.84 ✓
0+60			5.2	6.10 ✓
0+65			6.5	4.8 ✓
0+69			6.4	4.9 ✓
0+72			4.7	6.6 ✓
1+00			5.0	6.3 ✓
1+05			4.8	6.5 } ✓
1+10			6.2	5.1 } ✓
1+50			5.7	5.6 ✓
1+81			5.4	5.9 ✓
1+87			4.9	6.4 ✓
1+94			9.1	2.2 ✓
1+99			6.9	4.4 ✓

Nail in guy pole (page 50) 21 Rt 10+92 (new sta.)

Nail in telephone pole, 14 Rt 1+05
 ck on top of rail 198+50, Shalhas loc. Rec. 7^o

Top of rail

" " "

	11.32	✓		
2+00			6.9	4.4 ✓
2+01 ⁴			6.30	5.0 ✓
2+06 ¹			6.29	5.03 ✓
2+08			6.9	4.4 ✓
2+13			8.7	2.6 ✓
2+22			5.2	6.1 ✓
2+50			4.9	6.4 ✓
3+00			5.1	6.2 ✓
3+50			4.9	6.4 ✓
4+00			5.1	6.2 ✓
4+50			4.8	6.5 ✓
5+00			4.7	6.6 ✓
5+50			4.5	6.8 ✓
TP	6.10	13.42	4.00	7.32 ✓
6+00			6.4	7.0 ✓
6+50			6.2	7.2 ✓

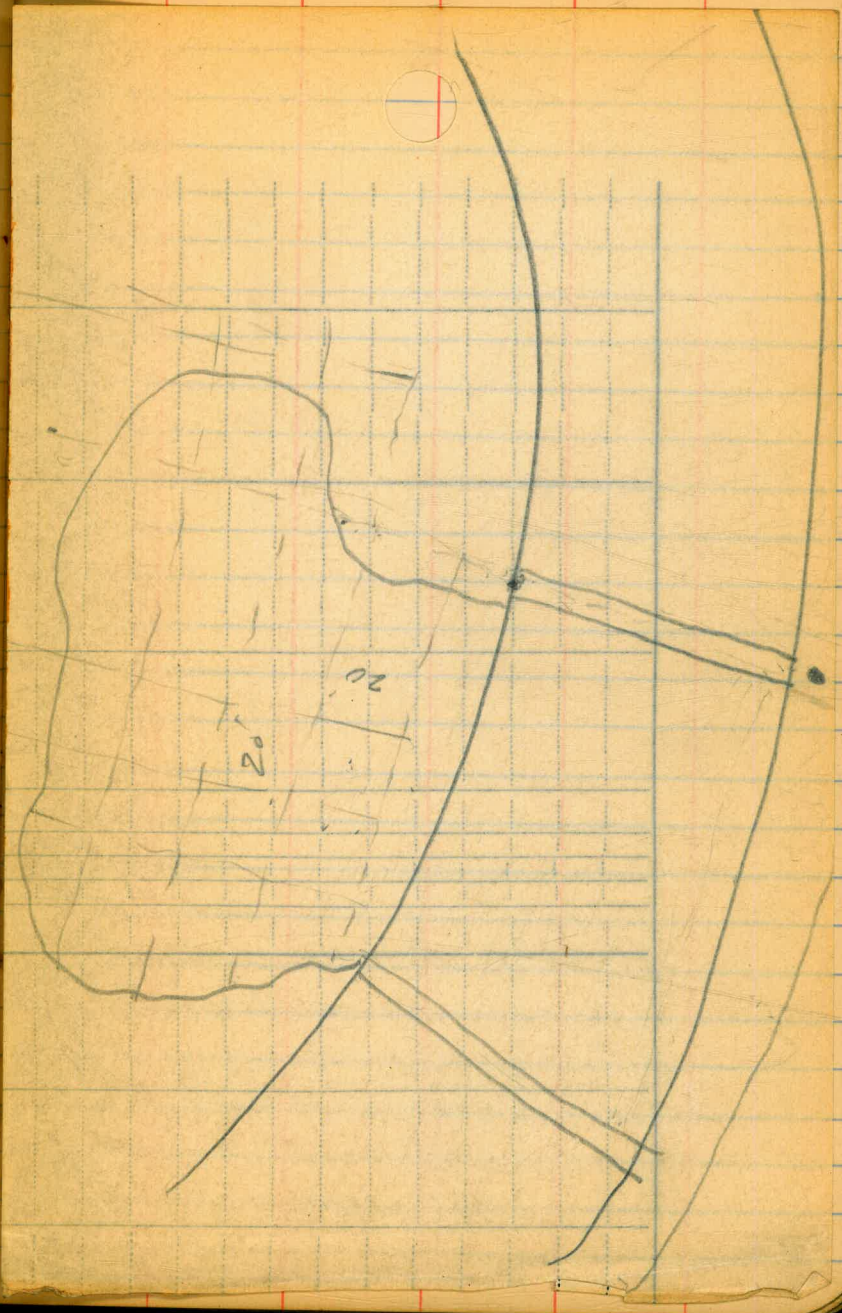
Top of rail

" " "

13.42 ✓

7400	6.1	7.3	✓
7450	6.0	7.4	✓
7495 ⁸⁰	5.8	7.6	✓
8200	5.7	7.7	✓
+50	5.6	7.8	✓
8488 ⁷¹	5.3	8.1	✓
9200	5.1	8.3	✓
+50	4.9	8.5	✓
10	4.4	9.0	✓
+50	4.1	9.3	✓
11	3.5	9.9	✓
+50	3.3	10.1	✓

64



13.42 ✓

7400	6.1	7.3	✓
7450	6.0	7.4	✓
7495 ⁸⁰	5.8	7.6	✓
8200	5.7	7.7	✓
+50	5.6	7.8	✓
8488 ⁷¹	5.3	8.1	✓
9200	5.1	8.3	✓
+50	4.9	8.5	✓
10	4.4	9.0	✓
+50	4.1	9.3	✓
11	3.5	9.9	✓
+50	3.3	10.1	✓

		13.42 ✓			
12+00			3.4	10.0	✓
TP	5.23	14.83	3.82	9.60	✓
12+50			4.9	9.9	✓
13			5.0	9.8	✓
+50			5.2	9.6	✓
14			5.4	9.4	✓
+50			6.1	8.7	✓
+69			6.5	8.3	✓
15			5.5	9.3	✓
+26			5.7	9.1	✓
+50			5.2	9.6	✓
16			4.4	10.4	✓
+50			3.4	11.4	✓

14.83 ✓

17+06 2.5 12.3 ✓

+50 1.7 13.1 ✓

18 1.0 13.8 ✓

TP 9.01 22.93 0.91 13.92 ✓

18+50 8.0 14.9 ✓

18+81 7.3 15.6 ✓

± Main

19+00 7.4 15.5 ✓

19+09 7.4 15.5 ✓

+50 6.6 16.3 ✓

20 5.8 17.1 ✓

+50 5.5 17.4 ✓

21 5.8 17.1 ✓

+50 6.6 16.3 ✓

22.93 ✓

22+00

7.0 15.9 ✓

+40

7.9 15.0 ✓

+50

7.9 15.0 ✓

+72

7.7 15.2 ✓

23

8.0 14.9 ✓

23+28

7.3 15.6 ✓

+50

7.0 15.9 ✓

+78³⁸

6.7 16.2 ✓

ck on B.M.

12.0

7.32

15.61

✓ Rec. 1558

Point on curb return, 20' Rt 22+36 - Old sta 116+45 (page 49)

Profile - 36th St - after benching

B.M.	10.47	61.41		50.94
4+30			4.8	56.6
+40			4.5	56.9
+50			3.1	58.3
TP	13.04	73.46	0.99	60.42
4+70			10.5	63.0
+80			8.7	64.8
5+00			6.3	67.2
+50			0.0	73.5
TP	12.83	86.20	0.09	73.37
6+00			6.6	79.6
+50			0.0	86.2
TP	12.97	99.07	0.10	86.10
7+00			5.3	93.8
TP	12.84	111.91	0.00	99.07
7+50			11.6	100.3
8+00			4.1	107.8
TP	12.83	124.38	0.36	111.55
8+50			9.0	115.4
9+00			0.5	123.9
TP	12.96	137.17	0.17	124.21
9+15 ⁸⁵ back			10.4	126.8
8+22 ⁶⁵ ahead			6.0	131.2
TP	12.70	149.64	0.23	136.94
9+00			11.5	138.1

6/22/42

Rt. Seper
Davis

68.

Lt.

Note: From sta 4+30 to 15+40 was benched off by
H. Foster. From 16+30 to 25+58, moved by City crew

For final sections page 79

149.64

9+50			7.9	141.7	✓
10+00			6.2	143.4	✓
+50			4.6	145.0	✓
11+00			4.2	145.4	✓
+50			4.3	145.3	✓
12+00			3.7	145.9	✓
+50			3.4	146.2	✓
13+00			5.3	144.3	✓
+50			9.4	140.2	✓
TP	0.73	139.86	10.51	139.13	✓
14+00			3.5	136.4	✓
+50			7.2	132.7	✓
15+00			12.6	127.3	✓
TP	1.13	128.01	12.98	126.88	✓
15+40			5.2	122.8	✓
B.M.			5.61	122.40	Rec. 122.41
16+30			5.6	122.4	✓
17+00			4.1	123.9	✓
18+00			4.5	123.5	✓
19+00			5.9	122.1	✓
20+00			9.9	118.1	✓
TP	0.49	118.41	10.09	117.92	✓
21+00			5.4	113.0	✓
22+00			10.2	108.2	✓
TP	1.12	106.77	12.76	105.65	✓

Pave. covered with dirt,
 B.P. in curb N.W. Cor. 36th & Market.

6/24/42
Soper
King
Davis

70

106.77

23+00			2.8	104.0	
24+00			5.8	101.0	
25+00			8.7	98.1	
			2.56	104.21	
B.M.	0.21	104.42			
25+25 ⁸⁸ A			6.9	97.5	
+38			7.0	97.4	
+41			5.5	98.9	
+45			5.5	98.9	
+50			10.0	94.4	
TP	4.55	97.83	11.14	93.28	
25+55			6.2	91.6	
+94			12.5	85.3	
26+00			11.2	86.6	
+28 ⁰⁷ A			6.6	91.2	
+50			8.9	88.9	
27			12.0	85.8	
+25			9.7	88.1	
+50			8.4	89.4	
+58			7.9	89.9	
+67			1.6	96.2	
+71			1.7	96.1	
+75			3.3	94.5	
28+02 ⁰⁰ back			5.2	92.6	
28+03 ⁸⁸ ahead			6.6	91.2	Rec. 91.2

Set temporary B.M. Nailing guy pole 40' lt 23+60
& Profile over line revision - 25+25⁸⁸ to 28+02

dirtwalk

bottom of draw

dirtwalk

36th St line revision, 25+25⁸⁸ to 28+03⁸⁸

28+03⁸⁸ ahead
28+02⁸⁹ back

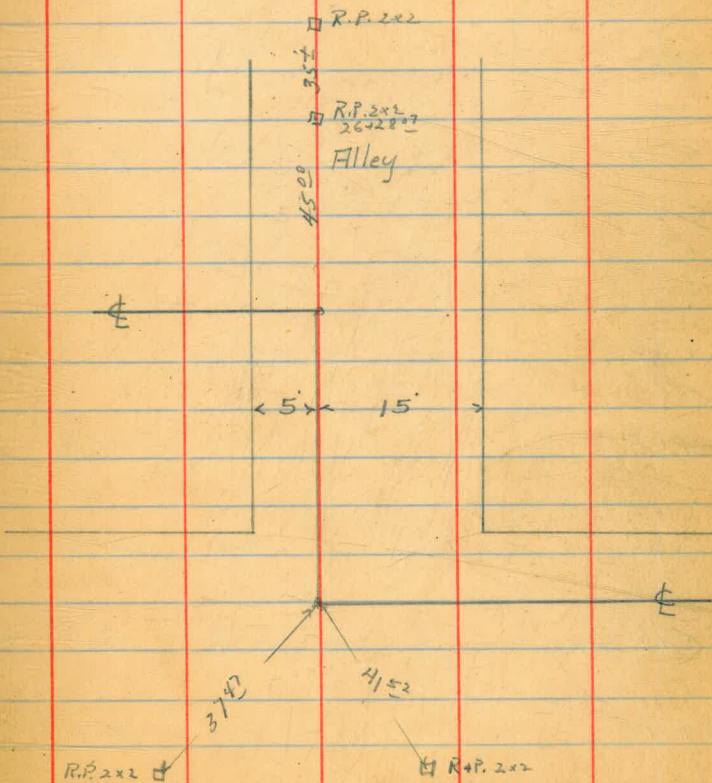
26+28⁰⁷ Δ 90°05' Lt

25+25⁸⁸ Δ 90°36' Rt

6/23/42

Soper
King
Davis

71



7/16/42

72

Super
leveling
DaulsProfile - 6' offsets to left - 36th St. P.L. Loc.

B.M. 10.40 61.34 50.94 Grade Cut

0+00	2.4	58.9	51.88	7.1	
0+04 Beginning of work		58.9	51.91	7.0	
0+50	2.7	58.6	53.13	5.5	
0+75 x	3.1	58.2	53.80	4.4	
1+00	3.1	58.2	53.65	4.5	
1+50	3.5	57.8	53.35	4.4	
2+00	3.7	57.6	53.05	4.5	
2+50	4.2	57.1	52.75	4.3	
3+00	4.6	56.7	52.45	4.2	(on Pavc)
3+50	4.9	56.4	52.15	4.2	"
3+58 ³⁵ Ax	4.9	56.4	52.10	4.3	" (bisection of L)
3+90 x	4.6	56.7	51.00	5.7	"
4+10 x	4.9	56.4	51.00	5.4	"

61.34

4+30 x 4.5 56.8' 51.70 5.1' hub

4+50 x 2.8 58.5' 53.10 5.4'

TP 12.93 73.49' 0.78 60.56'

4+70 x 10.1 63.4' 55.20 8.2'

5+00 x 6.0 67.5' 59.40 8.1'

TP 12.17 85.36' 0.30 73.19'

5+50 11.6 73.8' 66.95 6.8'

6+00 x 5.7 79.7' 74.50 5.2'

+10⁴ Δ 4.4 81.0' 76.00 5.0' (bisection of angle)

TP 12.60 97.88' 0.08 85.28'

6+50 ? 81.70 ?

7+00 4.3 93.6' 88.90 4.7'

TP 12.41 109.71' 0.58 97.30'

7+50 8.9 100.8' 96.10 4.7'

7/22/42
Super
King
Davis

74

	109.71				
8+00 x		1.7	108.0	103.30	4.7
TP	12.69	121.96	0.44	109.27	
8+50		6.4	115.6	111.37	4.2
TP	8.45	130.02	0.39	129.57	
9+00		6.1	123.9	119.44	4.5
9+15 ⁸⁵ back 8+22 ⁶⁵ ahead x		3.2	126.8	122.80	4.8 (bisection of angle)
TP	12.53	139.32	3.23	126.79	on & hub 9+15 ⁸⁵ = 8+22 ⁶⁵
8+50		8.0	131.3	126.33	5.0
8+75 x		4.2	135.1	130.30	4.8
9+00 x		1.0	138.3	133.30	5.0
TP	10.51	149.52	0.31	139.01	
9+25 x		8.9	140.6	135.50	5.1
9+75 x		6.7	142.8	138.70	4.1
10+25 x		5.0	144.5	140.70	3.8

149.52

140.3
136.8
3.5

5.7

75

10475 x 4.3 145.2 141.80 3.4

11400 4.2 145.3 141.80 3.5

150 4.1 145.4 141.80 3.6

12 x 3.6 145.9 141.80 4.1

150 x 3.5 146.0 140.70 5.3

13 x 5.0 144.5 138.00 6.5

150 9.2 140.3 134.13 6.2

TP 0.94 141.27 9.19 140.33

14 4.7 136.6 130.26 6.3

150 8.4 132.9 126.40 6.5

14490 x 12.7 128.6 123.30 5.3

TP 0.66 129.23 12.70 128.57

	129.23					
15+10	x	3.1	126.1	121.20	4.9	
+30	x	5.5	123.7	118.60	5.1	
+50		6.7	122.5	118.60	3.9	X on Parc
16+60	x	6.7	122.5	118.60	3.9	X on Parc
TP	3.76	126.18	6.81	122.42		
16+50		3.1	123.1	118.50	4.6	
17		2.4	123.8	118.40	5.4	
+50		2.1	124.1	118.30	5.8	
18		2.5	123.7	118.20	5.5	
+50		3.2	123.0	118.10	4.9	
19	x	3.8	122.4	118.00	4.4	
+50		5.3	120.9	116.00	4.9	

126.18

20	+00	X		7.6	118.6	114.00	4.6
	+50			10.1	116.1	111.50	4.6
21				13.7	113.5	109.00	4.5
	IP	0.50	113.94	12.74	113.44		
21	+50			3.3	110.6	106.50	4.1
22		X		5.4	108.5	104.00	4.5
	+50			7.4	106.5	102.00	4.5
23				9.4	104.5	100.00	4.5
	+50			11.0	102.9	98.00	4.9
	IP	2.66	105.57	11.03	102.91		
24	+00			4.2	101.4	96.00	5.4
	+50	X		5.9	99.7	94.00	5.7
25				7.2	98.4		
25	+50			8.0	97.6		
ck on B.M.				1.37	104.20		

Rec.
104.21

Cont'd in Book 601-A page 1

Elev. of existing 8" C.I.P. on Market St. (from G.V.)

B.M.	4.96	127.37	122.41	-24 for 6" V		
			6.25	121.12	118.7	bott. pipe
			5.62	121.75	119.4	bott. pipe

78

Top of stem of 8" G.V. 22 RT 154843
" " " " 9⁵ Lt 12842

X-section after benching

(For - From of elev.)
see page 68

7/27/42
Super
12.09
Davis

(79)

LT	Elev.	RT
5400	$\frac{+0^3}{13}$ 672	$\frac{-1^2}{15}$
+25	$\frac{+12^2}{12}$ $\frac{+0^5}{11^5}$ 700	$\frac{0^2}{15}$
+50	$\frac{+13^2}{14}$ $\frac{+0^5}{12}$ 735	$\frac{0.0}{10}$
+68	$\frac{+11^2}{13}$ $\frac{+1^0}{11^5}$ 752	$\frac{0.0}{15}$
6400	$\frac{+7^0}{12}$ $\frac{0^0}{11}$ 796	$\frac{0.0}{15}$
+50	$\frac{+13^2}{10}$ $\frac{+0^3}{9}$ 863	$\frac{0.0}{15}$
7400	$\frac{+1^2}{12}$ $\frac{+0^2}{14}$ 938	$\frac{+0^3}{15}$
8400	$\frac{+5^0}{19}$ $\frac{+0^5}{17}$ 1078	$\frac{+0^2}{15}$
+60	$\frac{+6^5}{14}$ $\frac{+0^2}{11}$ 1172	$\frac{+1^2}{15}$
+78	$\frac{+4^0}{13}$ $\frac{+0^2}{11}$ 1223	$\frac{0.0}{15}$
9400	$\frac{+2^8}{13}$ $\frac{+0^3}{12}$ 1239	$\frac{0.0}{15}$

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

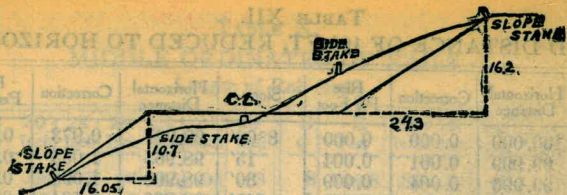
Distance of slope stake from side or shoulder stake for any width roadway, slope 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not level, the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point and line of stake should cut target.

IMPROVED TABLES AND INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE $1\frac{1}{2}$ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

477.52
 417.75
 79.57
 497.32
 404.75
 92.57
 116.45
 3.55
 18.81
 22.36

Intersect Birch & Vesta, 108+4430

⁴⁷
108+72830 tie to 7 pt. E side of
Vesta

115+66.32 tie to 7 point on N.
side of Dalbergia

New A = 108+4930

prop 108+7730

120
122
24
120.1

18.96
120 +
+ 347.17
486.13

497.32

529.24
404.75
124.49