

326

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326

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358

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

INDEX

El Capitan Pipe Line survey
from Dam Site to Lakeside 1-79
Transit Notes on
Original Line. 1931 Survey.

9/11/31

Converse Hill
Simpson
Weather - clear + hot

2

Sta. Angle Mag. Calc.

S. 87° W / S 87° 40' W

0+00 5° 38' 30"
2° 49' L

131.56

6. W. C.
0+71.90 E.C.

+71.06 E.C.

-1+31.40 12° 40'
6° 20' R6. W. C.
-1+71.06 B.C.

0+91.90 B.C.

39.66
54.24

West N 89° 31' W

P.L. -1+31.4

A 6° 20' R

D 8'

T 39.66

L 79.16

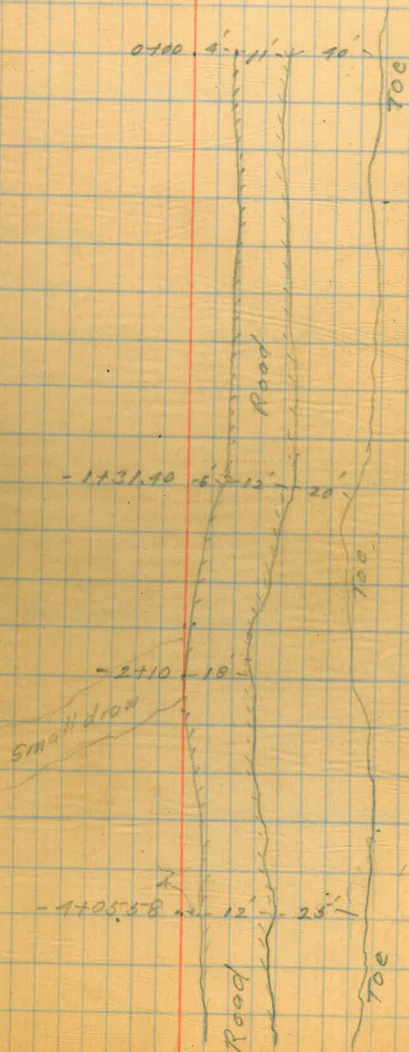
R 71.678

274.18

S 84° W / S 84° 09' W

-1+05.58 26° 00'
13° 00' L91.9
313.6

61.62



Sta. Angle Mag. B. Calc. B.

Small draw 3719

S 83-30 W S 64-07 W

2451.43 EC.

R1. 1794.62

+51.43 4°33' L Δ 9°07'

+25 3°30' D 8°

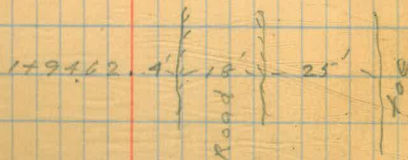
2400 2°30' T 57.16

+75 1°30' L 113.96

+50 0°30' R 716.78

123.05

1794.62 18° 14' 9°07' R



1737.17 BC.

S 73-30 W S 75-00 W

1711.44 EC.

R1. 0472.14

Δ 12°40'

D 16'

T 39.87

L 79.17

R. 359.26

72.14

0472.14 12°-40' L



0432.27 BC.

7/5/31

Converse Weather-clear & hot
Hill
Simpson

Sta. Angle Mag. B. Calc. B.

N66°30'W N66°30'W

6459.40 E.C.

E.C. 947' P.I. 6429.06

+75 8°38' Δ 19°34' R

+50 6°33' D 16'

6429.06 ^{39°08'30"} 19°34' R

+25 4°38' T 61.95

107.76

6400 2°38' L 122.29

+75 0°38' R 359.26

5467.11 B.C.

N86°30'W N86°04'W

5421.30 ^{6°-1130"} 3°-21' L

117.81

5421.30 5' 17' 50' 100

N83°W N82°43'W

4786.21 E.C.

E.C. 4621.035 P.I. 4786.21

+50 5°28' Δ 13°10'

+25 4°28' D 8'

4704.35 ^{26°20'} 13°10' R

+100 3°08' T 82.72

210.07

+75 2°08' L 164.58

+50 1°08' R 716.78

4704.35 18' 12' 40' 100

3421.63 B.C.

Sta. Angle Mag. B. Calc. B
S 74°30' W S 74°00' E W

11773.28 EC.

P.I. 11733.80

A 7°00' L

11733.80 14°00'
7°00' L

D 8

232.41

11733.80 .6' 15' 30' 700

T 4802

10785.78 BE.

L 8750

R 716.78

wash 10739

S 81° W S 81°05' W

9401.39 4°55' R

104.78

9401.39 .8' 16' 40' 700

S 76°30' W S 76°10' W

8457.89 EC.

EC 18°40' P.I. 8402.50

+50 17°24' A 37°20'

+25 13°24' D 32°

8402.50 74°-40'
37°-20' L

8400 9°24' T 61.28

175.05

8402.50 12' 13' 700

+75 6°24' L 116.97

+50 1°24' R 181.4

7441.22 BE.

Sta. Angle Mag B. Calc. B.

S66°W S66°14'W

14+19.12 E.C.

EC. 1327' P.I. 13+65.85

14+00 10°49' Δ 26°14' L

13+65.85 26°14' L

+75 7°49' D 24

+50 4°49' T 56.01

+25 1°49' L 109.31

13+09.81 B.C.

R 240.49

N87°W N87°32'W

12+94.37 E.C.

P.I. 12+37.76

EC. 9°10' Δ 18°20' R

+75 7°37' D 16

12+37.76 18°20' R

+50 5°37' T 57.97

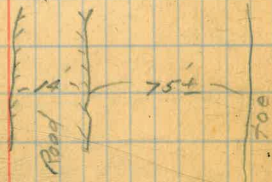
+25 3°37' L 114.58

12+00 P.37 R 359.26

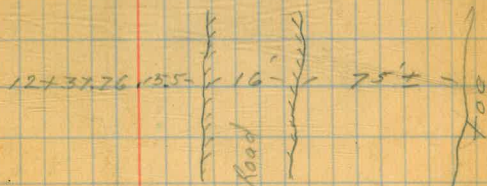
11+79.79 B.C.

Instrument off

129.45'



112.50'



9/2/31

Sta. Angle Mag. B Calc. B_d

S82°W S82-14W

EC. 12°00'

18+54.96 EC.

+50 11-37 P1. 17+813.2

+25 9-37 Δ 24°

18+00 7-37 D 16°

17+81.32 24°00' L

+75 5-37 T 76.36

+50 3-57 L 150.0

+25 1-37 R 359.26

17+04.96 BC.

17+00.64 P.O.T.

N74°W N73-46W

16+42.52 EC.

EC. 20°00' P1. 15+83.57

+25 17-12 Δ 10°

16+00 13-12 D 32°

15+83.57 80°00'
40°00' R

+75 9-12 T 66.12

+50 5-12 L 125.0

+25 1-12 R 181.46

15+17.52 BC.

Converse Weather - clear + hot
Hill
Simpson

7

80.68

17+813.2 3.5-10

100±

Road

Road

Road

124.14

17+00.64 4-17

100±

Road

Road

Road

220.96

15+83.57 7-18

100±

Road

Road

Road

Sta. Angle Mag. B. Calc. B.

8°-28' N 81-30 W N 81-00 W
20+24.25 1°-14 L

N 77-30 W N 76-46 W

19+91.88 E.C.

P.I. 19+71.65

Δ 6°-30 L

D 16

19+71.65 6°-30 L

T 20.40

L 40.63

R 35.26

19+51.25 B.C.

N 70° W N 70-16 W

19+43.93 E.C.

P.I. 19+02.38

Δ 27°-30 L

E.C. 13-45 D 32°

19+02.38 27°-30 R

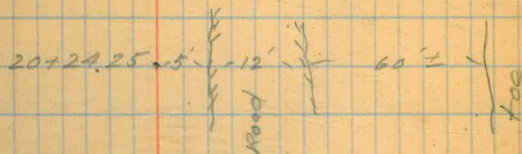
+25 10.13 T 44.37

19+00 6-43 L 85.94

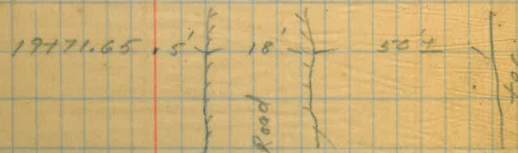
+75 2°-43 R 181.40

18+57.99 B.C.

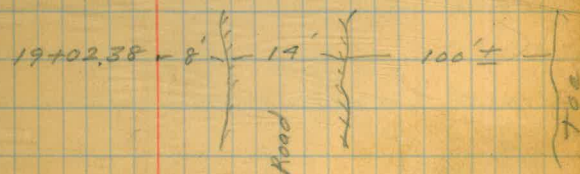
52.77 ✓



72.11 ✓



123.78 ✓



Sta. Angle Mag. B. Calc. B.
N 72° W N 72° 41 W

25400.97 E.C. EC. 7-23 P.I. 24455.23

25400 7-18 Δ 14° 46'

29-32
24455.23 14°-46' R

+75 5-18 D 16°

179.35 ✓

24455.23 ... 6'

+50 3-18 T 46.55

24408.68 B.C.

+25 1-18 L 92.29

R 359.26

N 87-27 W

23414.01 E.C.

P.I. 22476.41

Δ 12° 07'

D 16

24° 14' 30"
22476.41 12°-07' R

T 38.13

131.93 ✓

22476.41 ... 3'

L 75.73

R 359.26

22438.28 B.C.

S 80-30 W S 80-26 W

EC. 9-17

22400 9-02 P.I. 21445.88

22403.20 E.C.

+75 7-02 Δ 18° 34'

+50 5-02 D 16

37°-08' 30"
21445.88 18°-34' L

+25 3-02 T 58.72

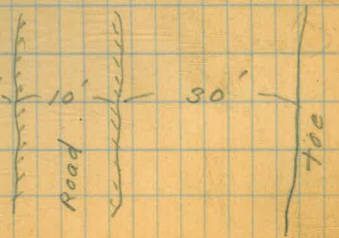
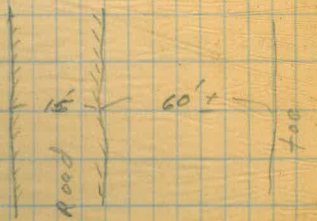
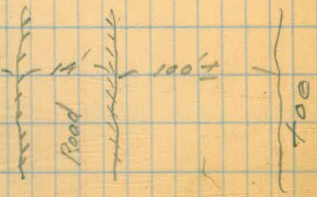
121.63 ✓

21445.88 ... 6'

21400 1° 02' L 116.04

R 359.26

20487.16 B.C.



9/9/31

Converse Clear hot
Hill
Simpson

10

sta. Angle Mag. B. Calc. B.
N58° W N58-31W

30+09.03 E.C.

P.I. 29+69.66

A 26°

52°-00'

E.C. 13°00' D 32°

29+69.66 26°00' R

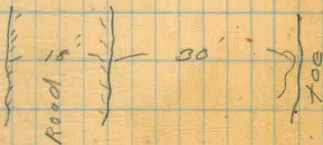
30+00 11-33 T 41.88

176.84 ✓

29+69.66

+75 7-33 L 89.25

+50 3-33' R 181.40



29+27.78 B.C.

N84-30W N84-31W

28+35.61 E.C.

P.I. 27+92.98

A 6°-50' L

D 8°

13°-10'

27+92.98 6°50' L

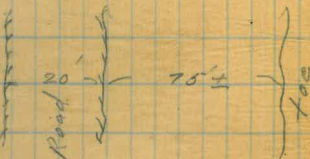
T 92.79

187.59 ✓

27+92.98

L 85.12

R. 716.78

Cleveland Nat.
Forest sign
27+95 ⊕

27+50.19 B.C.

N77° W N77-41W

26+05.39 10°00' 5°00' L

150.97 ✓

26+05.39



Sta. Angle Mag. B. Calc. P.
N60-30W N61-39W

33+31.07 EC.

P1. 32+95.50

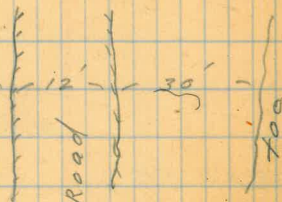
A 5°42' R

11°-24'
32+95.50 5°42' R

D 8°

121.22[✓]

32+95.50



32+59.82 BC.

T 33.68

L 71.25

R 716.78

N66-30W N67-21W

32+16.32 EC.

P1. 31+75.72

A 19-50 R

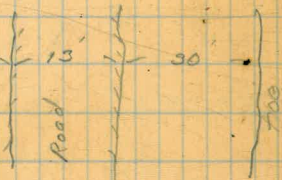
EC. 9-55 D 24°

39°40'-30"
31+75.72 19°-50' R

32+00 7-58 T 42.04

94.23[✓]

31+75.72



+75 7-58 L 82.64

+50 1°-58 R 240.19

31+33.68 BC.

N86° W N87-11W

31+27.84 EC.

P1. 30+84.61

EC. 14°-20' A 28°40' L

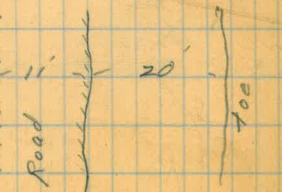
+25 13-55 D 32°

57°-20'
30+84.61 28°40' L

31+00 9-53 T 46.35

117.46[✓]

30+84.61



+75 5-53 L 89.58

+50 1°-53 R 181.10

30+38.26 BC.

Sta. Angle Mag. B. Calc. B.

N52°W N52-55W

34+98.27 E.C.

P.I. 34+63.98

Δ 9°-06' L

D 16°

34+63.98 18°-12'
9°-06' L

T 28.69

L 56.88

R 359.20

66.59 ✓

34+63.98



34+35.39 B.C.

N43° W N43-49W

34+25.85 E.C.

P.I. 33+98.58

Δ 17°-50' R

D 32°

33+98.58 35°-39'-30"
17°-50' R

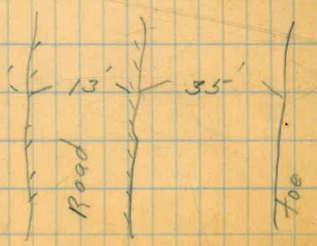
T 28.46

103.19 ✓

L 55.73

R 181.4

33+98.58



33+70.12 B.C.

Sta Angle Mag. B. Calc. B.

N66-30W N67-01W

37+38.32

P1. 36+83.39

FC. 6°38' Δ 13°-16L

+25 5-50 D 12°

36+83.39 Δ 13°-16L
26°-32'

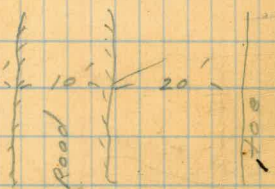
37+00 4-20 T 55.63

73.06

+75 2-50 L 110.55

+50 12-20 R 478.34

36+83.39



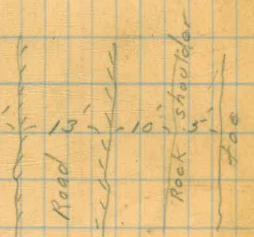
36+27.76

N53°W N53-45W

36+10.33 10°00'
5°00' L

67.75

36+10.33



N48°W N48-15W

35+42.58 8°19'-30"
4°-10' R

78.90

35+42.58



9/10/31 Converse clear + warm
Hill
Simpson.

1A

Sta. Angle Mag. B. Calc. B.

N77°W N76-59W

39+17.05 EC.

P.L. 38+91.43

A 6°-10' R

D 12°

T 25.77

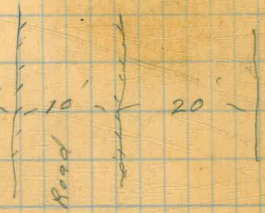
92.59

L 57.39

R 478.34

38+91.43 12°-20'
6°-10' R

38+91.43-6 10' 20'



38+65.66 BC.

N83°W N83-09W

38+49.76 EC.

P.L. 37+99.85

EC. 8°-04' A 16°-08' L

+75 905 D 16°

+50 4-05 T 50.92

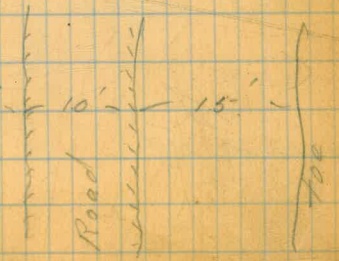
117.16

+75 2°-05' L 100.83

+50 0-05 R 359.26

37+99.85 32°-16'
16°-08' L

37+99.85-7 10' 15'



37+48.93 BC.

Sta. Angle Mag. B. Calc. B.

N66°W N66-49W

41+67.16 E.C.

P.I. 41+16.21

E.C. 17°10' Δ 34°20'R

+50 14-22 D 32°

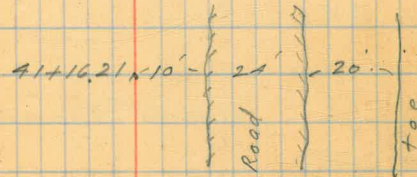
41+16.21 68°39-39"
34°20'R

+25 10-22 T 56.04

114.71

41+00 6-22 L 107.29

+75 2°22' R 181.90



40+60.17 B.C.

S78-30W S78-51W

40+52.98 E.C.

P.I. 40+03.77

E.C. 12°05' Δ 29°10'L

+50 11-43 D 24°

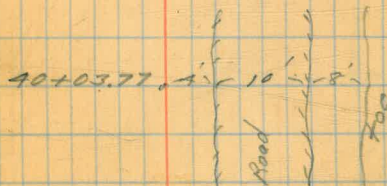
40+03.77 48°20'
29°10'L

+25 8-43 T 51.48

112.49

40+00 5-43 L 100.69

+75 2°43' R 240.49



39+52.29 B.C.

Sta. Angle Mag. B. Cole. B.
 N70°W N68.59W P.I. 43+84.83

44+20.78 EC. EC. 11:50 Δ 23°40' R
 44+00 830 D 32°
 43+84.83 47°19'30" 23°40' R 475 4:30 T 38.01
 450 0°:30' L 73.96
 43+46.82 BC. R 181.40

105.57



S86°W S87.21W

43+34.72 EC. P.I. 42+83.93
 EC. 17:00 Δ 34° L
 42+00 830 D 32°
 42+83.93 68°00' 34°00' L 43+00 11:27 T 55.46
 475 7:27 L 106.25
 450 3°:27 R 121.40

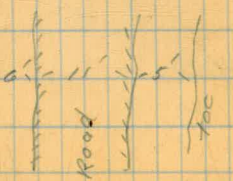
92.80



N59.30W N58.39W

42+11.69 EC. P.I. 41+91.42
 Δ 8°10' R
 D 20°
 41+91.42 16°-20' 8°10' R 41+00 6:00 T 20.56
 L 40.83
 R 287.94

80.00



41+70.86 BC.

Sta. Angle Mag. B. Calc. B.

N75°W N74°09W

46+45.51 E.C.

P.I. 46+10.33

Δ 11°20'R

D 16°

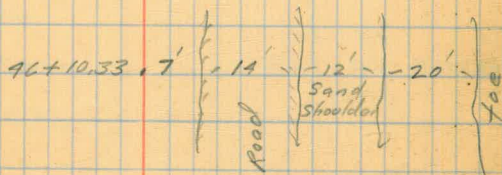
46+10.33 22°-40',
11°-20'R

T 35.65

137.56

L 70.83

R. 359.26



45+74.68 B.C.

N86°30W N85°29W

45+24.86 E.C.

P.I. 44+73.83

E.C. 8-15 Δ 16°30'L

45+00 6-16 D 16

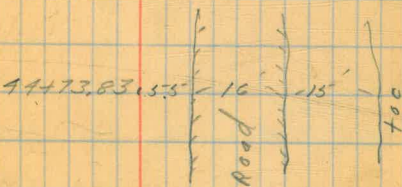
44+73.83 33°-00',
16°-30'L

+75 4-16 T 52.09

91.06

+50 2-16 L 103.12

+25 0°-16 R. 359.26



44+21.74 B.C.

Sta. Angle Mag. B Calc. B

N38-30W N37-29W ✓

EC. 12-25'

51+21.58 EC.

51+00 10-41 P.I. 50+75.47

+75 8-11 Δ 24°50'

+50 6-41 D 16°

19°40'
50+75.47 24°50' R

+25 4-11 T 79.10

342.99

50+00 2-41 L 155.21

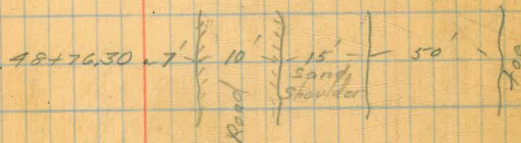
+75 0-11 R 359.26

49+66.37 BC.



48+76.30 P.O.T.

~~P.O.W.~~ 48+93



N63-30W N62-19W

47+52.05 EC.

P.I. 47+03.01

EC. 5-55 Δ 11°50' R

+50 5-48 D 12°

23°40'
47+03.01 11°50' R

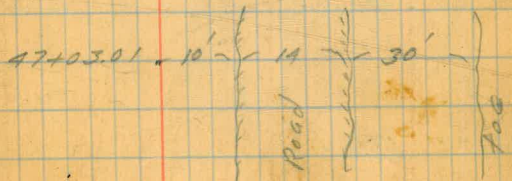
+25 4-18 T 49.57

93.15

47+00 2-18 L 98.61

+75 1-18 R 478.34

46+53.11 BC.



9/11/31

Converse Clear + warm
Hill
Simpson

19

Sta. Angle Mag. B. Calc. B.

N37-30W N37-24W

53+35.07 E.C.

P.I. 52+97.06

Δ 12-15 R

E.C. 6'-07 1/2" D 16"

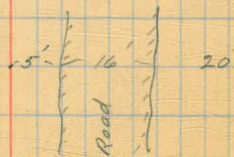
52+97.06 24°-30'
12°-15' R

+25 5-19 T 38.35

123.42

53+00 3-19 L 76.56

+75 1°-19' R 359.26



Toe (change)

52+58.51 B.C.

N50-30W N42-39W

52+11.93 E.C.

P.I. 51+74.18

Δ 12-10 L

E.C. 6'-05" D 16"

51+74.18 24°-20'-30"
12°-10' L

52+00 5-08 T 38.29

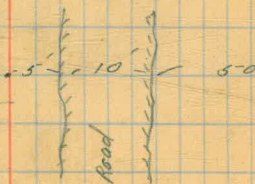
131.70

+75 3-08 L 76.09

+50 2-08' R 359.26

Draw

51+74.18



Toe

51+35.89 B.C.

Sta. Angle Mag. B. Calc. B.

N48°W N48°00'W

57+35.83 E.C.

P.I. 56+95.04

Δ 9°50'R

19°39'30"

E.C. 12-55' D 12°

56+95.04 7°50'R

+25 4-16' T 41.15

236.63

56+95.04-8'

57+00 2-96 L 81.94

+75 1°16' R. 47834

56+33.89 B.C.



N57-30W N57-50W

54+91.10 E.C.

P.I. 54+59.94

Δ 20°26'L

40°51'30"

D 32°

54+59.94 20°26'L

T 32.69

163.42

L 63.85

R 181.4

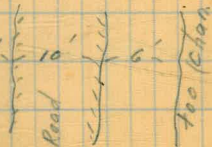
old line P.I. 61+35.5

24°30'15"

N56°25' W (minor)
N56°25' W

3°23'

54+59.94



54+27.25 B.C.

old line P.I. 60+61.2

Sta.	Angle	Mag. B.	Calc. B.
		S84-30W	S84-36W
		EC. 11°-17'	
61+27.00	EC.	+25 11-02	P1. 60+80.95
		61+00 2-02	A 22°-34L
60+80.95	15°-08' 22°-34L	+75 5-02	D 24°
		+50 2°-02'	T 47.98
60+32.97	BC.		L 94.02
			R 240.19

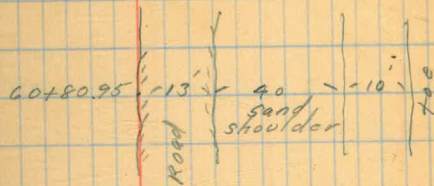
N72-50W

		EC. 12°-25'	
59+93.47	EC.	+75 10-56	P1. 59+17.36
		+50 2-56	A 24°-50'L
		+25 6-56	D 16°
59+17.36	49°-10' 24°-50L	59+00 1-56	T 79.10
		+75 2-56	L 155.21
		+50 0-56	R. 359.26
58+38.26	BC.		

58+38.53 P.O.T.

166.58

222.68



Sta. Angle Mag. B. Calc. B.

N81°W N80-59W

62+81.52 E.C.

P.I. 62+83.78

Δ 6°-15' R

D 12'

62+53.48 13°-30'
6°-15' R

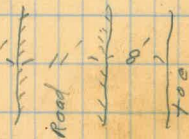
T 28.21

79.30

L 56.25

R 178.34

62+53.48 - 6'



62+25.27 B.C.

N88-30W N87-44W

62+06.23 E.C.

P.I. 61+74.39

Δ 7°-10' R

D 12'

61+74.39 15°-20'
7°-10' R

T 32.05

95.37

L 63.89

R 178.34

61+74.39 - 5'



Flat for 40'

61+42.34 B.C.

9/12/30

Converse Clearwarm
Hill
Simpson
Remman

2A

Sta. Angle Mag. B. Calc. B.

N83-30W N82-59W

65+31.14 E.C.

E.C. 22°05' P.I. 64+98.10

+20 18-11 Δ 74°10'R

+10 15-11 D 60°

88-19-30°

64+98.10 44°10'R

65+00 12-11 T 90.57

158.72

64+98.10 -12' 13' 20'

+90 9-11 L 73.61

+80 6-11 R 100.0

64+57.53 B.C.

+70 3-11

S52-30W S52-51W

63+82.00 E.C.

P.I. 63+47.68

E.C. 23°05' Δ 46°10'L

+80 22-29 D 60°

92°-20'

63+47.68 46°10'L

+90 19-29 T 42.62

94.37

63+47.68 13' 14' 25' 700

+60 16-29 L 76.94

+50 13-29 R 100.0

63+05.06 B.C.

+40 10-29

+30 7-29

+20 4-29

Sta. Angle Mag. B. Calc. B.
S80°W S80-11W

69+97.17 E.C.

P.I. 69+47.27

EC 12°20' Δ 29°40' L

+75 9°38' D 27°

69+47.27 19°-20'
29°40' L

+50 6°38' T 52.58

+25 3°38' L 102.78

69+00 0°38' R 240.99



68+94.69 B.C.

N75-30W N75-09W

67+23.86 E.C.

P.I. 67+85.60

Δ 12°20' R

D 16°

67+85.60 21°-40'
12°20' R

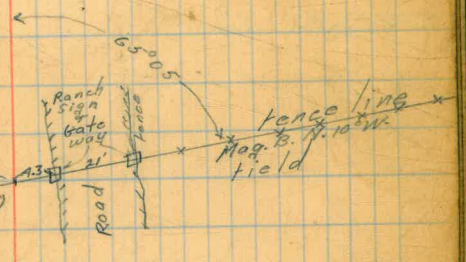
T 36.82

L 72.08

R 359.26

215.69

About E. Boundary of El Monte Ranch



67+96.78 B.C.

N87-30W N87-29W

65+69.21 9°00'
1°-30' L

79.34

Sta. Angle Mag. B. Calc. B.

N52°W N52°09W

72+99.62 E.C.

P.I. 72+54.70

Δ 22° R

E.C. 11°00' D 21°

72+54.70 44°00' 22°00' R

+75 8-03 T 46.75

+50 5-03 L 91.67

+25 2-03 R 240.49

72+07.95 B.C.



N74-30W N74-09W

71+75.91 E.C.

P.I. 71+23.76

E.C. 12°50' Δ 25°40' R

+50 9-43 D 21°

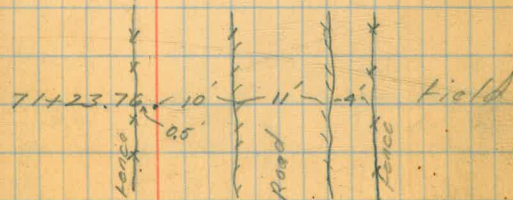
71+23.76 51°20' 25°40' R

+25 6-43 T 57.79

71+00 3-13 L 106.94

+75 0-43 R 240.49

70+68.97 B.C.



9/19/30

Converse clear + warm
Hill
Simpson
Romney

27

Sta. Angle Mag. B. Calc. B.

N 58° W N 57-42 W

77+81.82 E.C.

E.C. 1833 1/2' P.I. 77+10.32

+75 11-06 Δ 23° 17' R

+50 9-06 D 16°

77+10.32 16°-33' 30"
23°-17' R

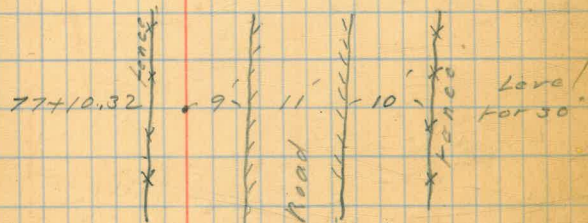
+25 7-06 T 74.02

77+00 5-06 L 145.52

+75 3-06 R 359.26

76+36.30 B.C.

+50 1° 06'



N 81-30 W N 80-59 W

75+37.52 E.C.

P.I. 74+49.66

E.C. 14° 25' Δ 28° 50' L

+25 13-25 D 16°

74+49.66 57°-40'
28°-50' L

75+00 11-25 T 92.35

+75 9-25 L 180.21

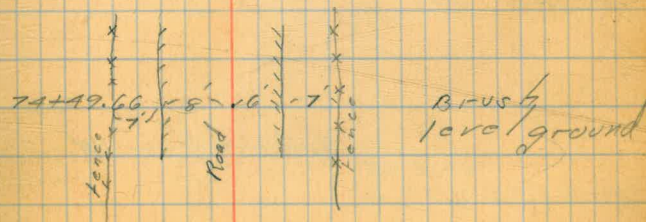
+50 7-25 R 359.26

73+57.31 B.C.

+25 5-25

74+00 3-25

+75 1° 25'



Sta. Angle Mag. B. Calc. B.

80+10.34 $4^{\circ}-08'$ $2^{\circ}04' L$ $N72-30W$ $N71-55W$

79+94.32 E.C. $N70^{\circ}W$ $N69-51W$ P.I. 79+58.10

$\Delta 11^{\circ}40'R$

79+58.10 $23^{\circ}-20'$ $11^{\circ}-40' L$ E.C. 5250' D 16'

+78 4-17 T 36.70

+60 2-17 L 72.92

+25 0-17 R 359.26

79+21.40 B.C.

78+68.90 $0^{\circ}58'-30''$ $0^{\circ}29' L$ $N58-30W$ $N58-11W$

Sta. Angle Mag. B. Calc. B.

N60°W N58-05W

82+37.27 EC.

P1. 82+07.23

A 9°-10L

D 16°

T 30.38

L 60.42

R 359.26

82+07.23 19°-20,
9°-40 L

81+76.85 BC.

N58-30W N58-25W

81+45.55 EC.

P1. 81+0369

A 13°-30R

D 16°

T 42.52

L 84.38

R 359.26

81+03.69 27°-00',
13°-30 R

80+61.07 BC.

Sta. Angle Mag B Calc B.

N74°W N74-27W

83+80.78 EC.

P.I. 83+49.52

Δ 20°30L

D 32°

T 32.80

L 64.06

R 181.4

46°59'30"

83+49.52 20°30L

83+16.72 B.C.

N46°W N53-57W

82+94.71 EC.

P.I. 82+73.03

Δ 14°08R

D 32

T 22.19

L 44.17

R 181.10

28°16'

82+73.03 14°08R

82+50.54 B.C.

Sta. Angle Mag. B. Calc. B.
N57°W N57-31W

86+19.58 E.C.

P.I. 86+29.56

A 6°-26'R

D 16°

T 20.19

L 40.21

R 359.26

12-52-30
86+29.56 6°-26'R

86+09.37 B.C.

3°-40'
85+69.19 1°-50'L
N63-30W N63-57W

85+17.16 E.C.
N62°W N62-07W

P.I. 84+78.90

A 12°-20'R

D 16

T 38.82

L 77.08

R 359.26

21°-40'
84+78.90 12°-20'R

84+10.08 B.C.

Sta. Angle Mag. B. Calc. B.

N53-30W N53-33W

88+25.04 E.C.

P.I. 87+82.06

A 13°-52' L

E.C. 6-56' D 16°

87+82.06 27°-44' 13°-52' L

88+00 4-56' T 43.69

+75 2-56' L 86.67

+50 0°-56' R 959.26

87+38.37 B.C.

N39°W N39-41W

87+16.76 E.C.

P.I. 86+89.99

A 17°-50' R

D 32°

86+89.99 35°-10' 17°-50' R

T 28.46

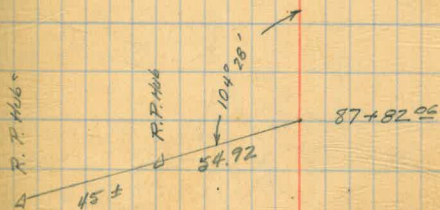
L 53.73

R 1814

86+61.03 B.C.

T.P. from 87+82 to 103+65 Set Jan 8, 1932
G.W. Converse Chief
Elliott T. notes
Simpson
Howden

32



9/15/30

Converse clear + warm
Hill
Simpson
Remmen

33

N72-30W N72-37W

92+21.98 E.C.

P.I. 91+92.45

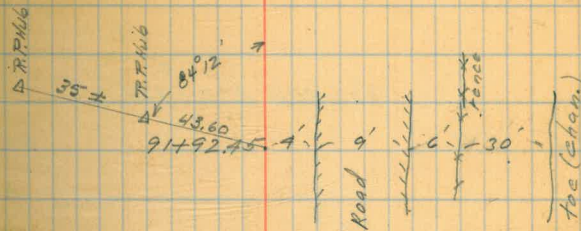
 Δ 9°-30' L

D 16°

T 29.85

L 39.38

R 369.26

91+92.45 19°-00'
9°-30' L

91+02.60 B.C.

N63-30W N63-07W

91+43.69 E.C.

P.I. 91+18.28

 Δ 12°-20' L

D 29°

T 25.98

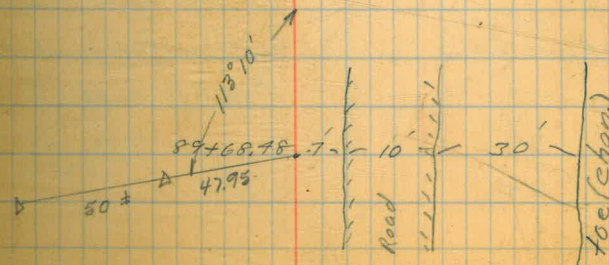
L 51.39

R 290.49

91+18.28 24°-40'
12°-20' L

90+92.30 B.C.

N51° W N50-47W

89+68.48 5°-32'
2°-46' R

Sta. Angle Mag. B. Calc. B.

N72-30W N73-07W

91+27.41 E.C.

P.I. 93+89.10

 Δ 15-30 R

D 20°

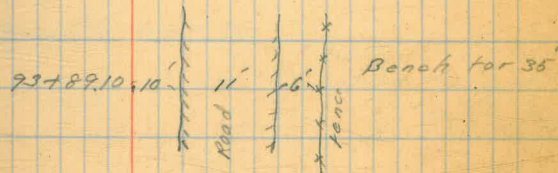
93+89.10 15-30 R

T 39.19

L 77.50

R 287.94

93+99.91 B.C.



N88-30W N88-37W

93+12.96 E.C.

P.I. 92+93.45

E.C. 8-10 Δ 16° L

+25 6-34 D 16°

92+93.45 32°00' L

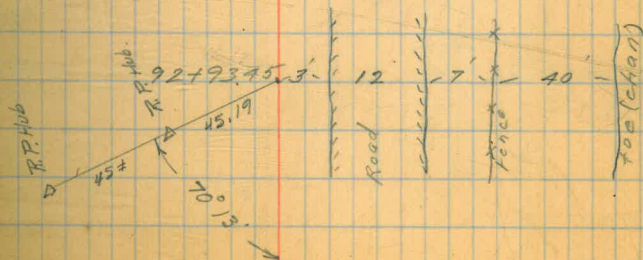
16°00' L

93+00 4-34 T 50.49

+75 2-34 L 100.00

+80 0°34' R 359.24

92+12.96 B.C.



Sta. Angle Mag. B. Cak. B.

98+81.25 8°36'
7°18' R

N77-30W N77-59W

97+47.92 P.O.T.

96+22.30 E.C.

95+93.81 18°-19'-30"
9°-10' L

95+65.01 B.C.

Pl. 95+93.81

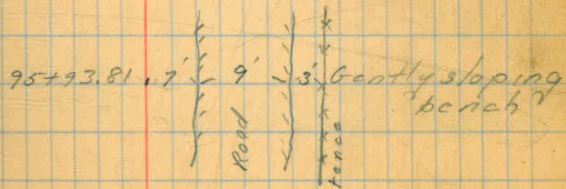
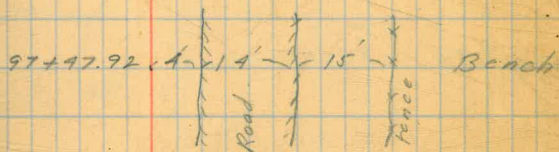
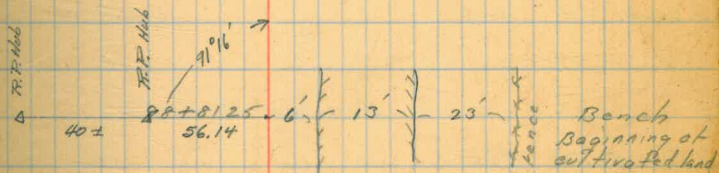
Δ 9-10 L

D 16'

T 29.80

L 57.25

R 359.26



Sta. Angle Mag. B Calc. P.
N10°W N11-31W

104+35.50	EC.	EC. 11-27	P.I. 103+65.3
		+25 10-37	
		109+00 8-37	Δ 22°54R
		+75 6-37	
103+65.13	22°54R	+50 4-37	D 16
		+25 2-37	T 72.76
102+92.37	BC.	102+00 0-37	L 143.13
			R 357.26

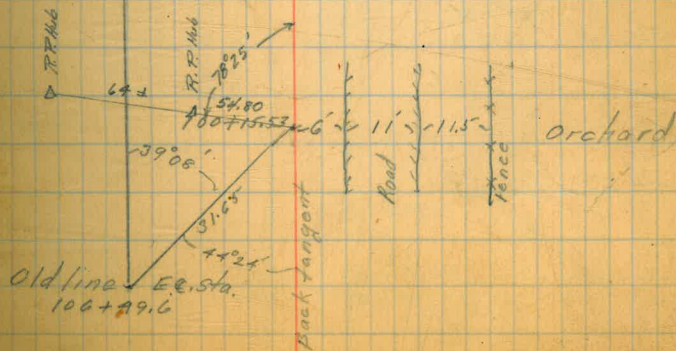
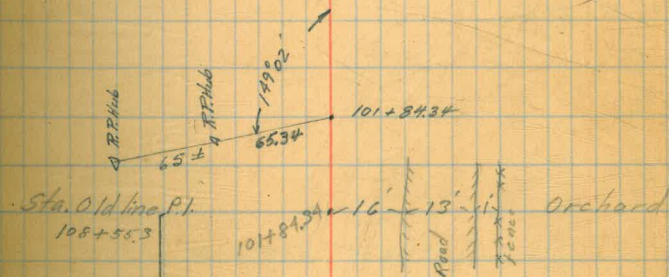
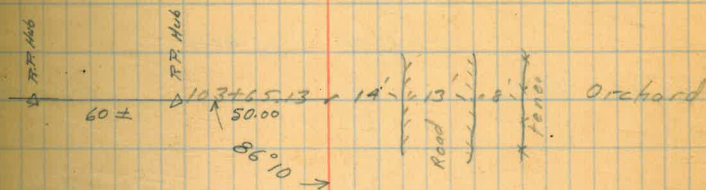
N33-30W N39-25W

102+41.39	EC.	EC. 19-11	P.I. 101+84.34
		+25 16-40	Δ 38°34R
		101+00 12-40	D 32°
		+75 8-40	T 63.47
		+50 4-40	L 120.52
		+25 0-40	R 181.90

101+20.87 BC.

N72-30W N72-59W

100+15.53 10°00'
5°00'R



9/16/31

Converse
Hill
Simpson
Remmen

87

Sta. Angle Mag. B. Calc. B.

S 85° W S 83 47 W

111709.36 EC.

P.L. 110784.02

Δ 6°-06 L

D 12°

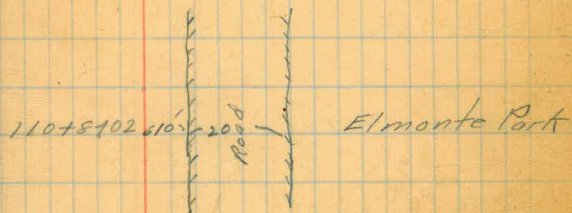
T 25.99

L 50.83

R 478.39

12° 12' 1
110784.02 6°-06 L

110758.53 B.C.



N 89° W S 89°-53 W

107765.57 EC.

P.L. 107746.64

Δ 76°-36 L

D Actual
Arc

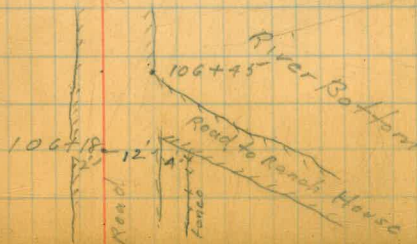
T 28.91

L 46.84

R 39.23

157°-12'
107746.64 78°-36 L

107718.63 B.C.



Sta Angle Mag. B. Calc. B.

129+39.97 $6^{\circ}-50'$
 $3^{\circ}-25'$ S. 41° W S 40-27 W

125+24.29 P.O.T.

S. 45° W S 43-52 W

E.C. 19-57 1/2'

+25 19-00

121+00 17-00

121+37.10 E.C.

+75 15-00 R 1, 120+18.08

+50 13-00 Δ 39° 55'

+25 11-00 D 16°

120+18.08 39° 55'

120+00 9-00 T 130.46

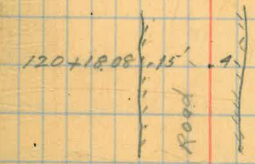
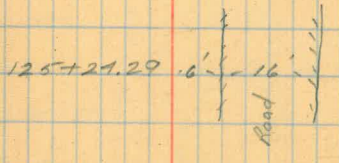
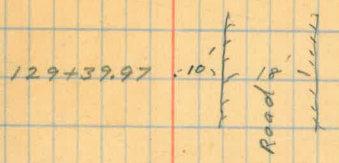
+75 7-00 L 219.98

+50 5-00 R 359.26

118+67.02 B.C.

+25 3-00

119+00 1-00'



S47°E S46-49 E

136+89.72 E.C.

E.C. 16-13' R.I. 136+24.52

+75 14-27 Δ 32°26' L

+50 11-27 D 24°

136+24.52 64°52'
32°26' L

+25 8-27 T 69.94

+262.93

136+00 5-27 L 135.14

+75 2-27' R 240.99

135+54.62 B.C.



S14-30E S14-23 E

133+37.56 E.C.

R.I. 132+87.09

Δ 54°50' L

E.C. 27-25' D 48

132+87.09 109°40'
54°50' L

+25 24-24 T 63.77

+350.73

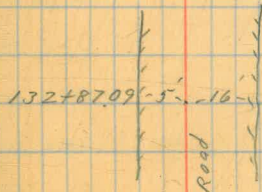
133+00 18-24 L 114.24

+75 12-24 R 122.93

+50 6-24

132+23.32 B.C.

12" CONC. WATER PIPE 133+94



9/17/30

Converse clear-warm
Hill
Simpson
Remmen

40

Sta. Angle Mag. B Calc. B.

S 59° W S 53-39 W

141+59.98 E.C.

P.I. 140+70.00

E.C. 14.47' Δ 29°-34 R

+50 13-59 D 16°

+25 11-59 T 94.81

140+70.00 ^{59° 08'} 29°-34 R

141+00 9-59 L 187.79

* 744.25

140+70.0

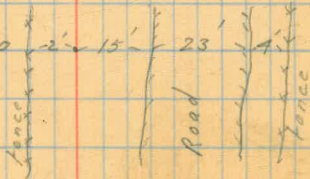
+75 7-59 R 359.26

+50 5-59

+25 3-59

139+75.19 B.C.

140+00 1°-59'



S. 21° W S 21-05 W

139+29.68 E.C.

P.I. 138+82.71

E.C. 35-27' Δ 70-54 R

+20 32-33 D 60°

139+00 26-33 T 76.20

* 211.52 v

138+82.71 ^{141' 48'} 70°-54 R

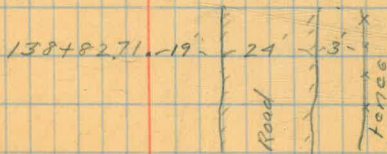
+50 20-33 L 118.17

+60 14-33 R 100.0

+40 8-33

+20 2°-33'

138+11.51 B.C.



Sta. Angle Mag. B. Calc. B.
S. 23° W S 24-11 W

153+29.18 E.C.

P.I. 152+86.81

Δ 13° 40' L

D 16°

T 43.08

L 85.42

R 359.26

152+86.81 $\begin{matrix} 27^{\circ}-20' \\ 13^{\circ}-40' L \end{matrix}$

x 170.61

152+86.81 S.S. 21'

152+43.76 B.C.

S 38° W S 37-51 W

151+61.53 $\begin{matrix} 8^{\circ}-53'-70'' \\ 4^{\circ}-27' L \end{matrix}$

x 125.28

151+61.53 S.S. 21'

148+80.07 E.C.

E.C. 5° 40' P.I. 148+80.07

+75 5-28 A 11° 21' L

+50 4-28 D 8°

+25 3-28 T 71.23

148+00 2-28 L 141.88

+75 1-28 R 716.78

+50 0-28

148+09.92 $\begin{matrix} 22^{\circ}-42' \\ 11^{\circ}-21' L \end{matrix}$

x 352.69

148+09.92 S.S. 12'-12'

147+38.19 B.C.

B.C. 3'-22'

146+55 Road

Sta Angle Mag. B. Calc B.

42

S. 50-30W S 50-55W

156+27.97 EC.

P.I. 156+04.95

A 7° 24' L

D 16°

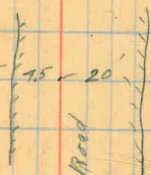
T 23.23

L 46.26

R 359.26

x 81.0

156+04.95 45-20'



156+04.95 7° 24' L

14-18'

155+81.72 BC.

S. 52-30W S 52-19W

155+59.78 EC.

EC. 17° 01'

150 18-17 P.I. 154+86.74

725 14-17 A 34° 08' R

155+00 12-17 D 16°

775 10-17 T 110.29

750 8-17 L 213.33

725 6-17 R 359.26

154+00 4-17

775 2-17

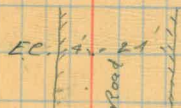
750 0-17

154+56.74 34° 08' R

68° 16'

x 155.46

154+56.74 13-28'



153+46.45 BC.

BC. 13-24'

Road

Sta. Angle Mag. B. Calc. B.

S 28° W S 28-33 W

158+46.53 E.C.

P. 1. 158+22.49

Δ 13°-10' L

D 28°

T 24.77

L 48.81

R 206.68

158+22.49
27°-20'
13°-10' L

x 146.76

158+22.49

Road

157+97.78 B.C.

S 41-30 W S 42-13 W

157+46.76
9°-00'
7°-30' L

x 76.03

157+46.76

Road

S 46° W S 46-43 W

156+85.74
8°-24'-30"
7°-12' L

x 60.72

156+85.74

Road

Sta. Angle Mag. B. Cole. B.

S48-50W S49-19W

15 162+7721 E.C.

P1 162+5037

Δ 13°02' L

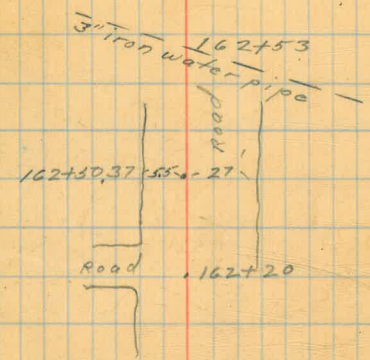
D 24'

162+50.37 26°04' 13°02' L ✓

T 27.47 + 287.37

L 57.31

R. 240.49



15 162+2290 B.C.

S61-30W S62-21W

160+19.04 E.C.

P1 159+68.52

E.C. 1655' Δ 33°48' R

159+68.52 67°36' 33°48' R

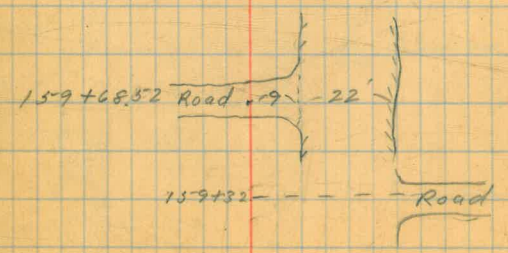
160+00 13.51 D 32'

+75 9.51 T 33.11

+ 286.44

+50 5.51 L 105.63

+25 1.51 R. 181.9

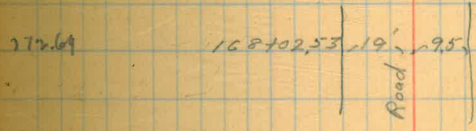


159+13.91 B.C.

sta. Angle Mag. B. Calc. B.

S52°W S52-43W

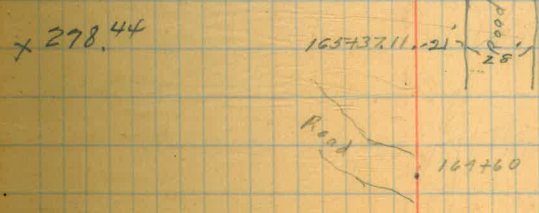
168+77.12 EC.	EC. 20-30' P.I. 168+02.53
	+50 16-59 Δ 41°L
	+25 13-41 D 26°
168+02.53 82°00' 41°00' L ↓	168+00 10-29 T 83.10
	+25 7-14 L 157.69
	+50 3-59 R 222.27
167+19.13 BC.	+25 0-44



166+76
2" iron water pipe

N87°W N86-17W

166+11.60 EC.	EC. 22-12'
	+25 20-32 P.I. 165+37.11
	166+00 18-02 Δ 49°24'R
	+75 15-32 D 20
165+37.11 49°24'R ↓	+50 13-02 T 117.51
	+25 10-32 L 222.00
	165+00 8-02 R 287.94
164+19.60 B.C.	+75 5-32
	+50 3°02'
	+25 0-32'



9/18/30

Converse
Hill
Simpson
Remmen

46

Sta. Angle Mag. B. Calc. B.
S 32-30 W S 33-30 W

174+83.76 EC.

P.I. 174+37.09

 Δ 9° 22' L

D 10°

T 47.00

L 93.67

R 573.69

174+72
3" iron water pipe

174+37.09 6' - 17'

Road

174+37.09 18° 44' ↓
9° 22' L

173+90.09 B.C.

S 42-30 W S 42-52 W

171+90.11 5° 11' ↓
2° 37' L

171+90.11 4' - 20'

Road

S 45° W S 45-29 W

169+96.75 EC.

P.I. 169+66.71

 Δ 7° 11' L

D 12°

T 30.24

L 60.28

R 478.34

169+66.71 15' - 21'

Road

169+66.71 14° 28' ↓
7° 11' L

169+36.47 B.C.

Sta. Angle Mag. B Calc. B.

181+27.84 $40^{\circ}42'36''$
 $2^{\circ}21'R$ S. 36-30W S37-25W

177+05.01 $3^{\circ}08'30''$
 $1^{\circ}34'R$ S34-30W S35-04W

97

pow. pole 183+78

pow. pole 182+33

181+27.84 $0^{\circ}42'29''$
Road

180+35.5
3" iron sewer pipe

pow. pole 180+00

Road 179+43

pow. pole 178+50

Road 177+78

8" Cer. iron sewer pipe
177+14.5

pow. pole 177+05.01
Road

Road 176+53

Sta. Angle Mag. B. Calc. B.

185+31.09 P.O.T

S 36° 30' W S 37° 25' W

pow. pole 197+03

pow. pole 195+66

15" concrete water pipe - 194+27.6 Note not in use.

pow. pole 194+21

pow. pole 192+83

pow. pole 191+43

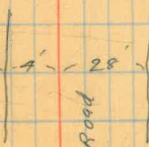
pow. pole 189+82

pow. pole 188+32

pow. pole 186+82

186+31.09

pow. pole



Road 184+00

Sta. Angle Mag. B. Calc. B.

202+81.81 P.O.T.

S 83-30 W S 89-33 W

200+69.13 E.C.

P.I. 200+16.37

E.C. 23°34' Δ 47°08' R

+50 12-11 D 40°

200+15.37 94°16' 47°08' R

+25 14-11 T 63.77

200+00 9-11 L 117.83

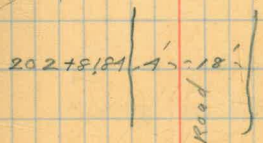
+75 1-11 R 146.19

199+51.60 B.C.

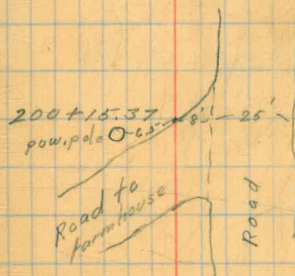
pow. pole O 204+72

Road 203+25

pow. pole O 203+12



pow. pole O 201+53



pow. pole O 198+68

Sta. Angle Mag. B. Calc. B

50

Road . 211755

pow.
pole O . 211708

pow.
pole O . 209748

14" cast iron culv. = -209716

. 209712

Road to
farmhouse

. 208738

12" concrete pipe drain
208712

pow.
pole O . 207787

pow.
pole O . 206732

Road . 205789

205787
2" iron water pipe

Sta. Angle Mag. B. Calc. B.

N43-30W N42-53W

215+62.49 E.C.

P.I. 215+24.94

 Δ 12° 06' R

D 16'

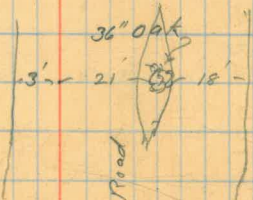
T 38.08

L 75.63

R 359.26

215+24.94 $\begin{matrix} 24^\circ 12' \\ 12^\circ 06' R \end{matrix}$

214+86.86 B.C.



214+03
 12" 8" 10" iron culvert
 26.5
 4'

N55-30W N59-59W

212+56.24 E.C.

E.C. 20'-11" P.I. 211+96.64

+50 19-14 Δ 40° 28' R

+25 15-14 D 32'

211+00 11-14 T 68.86

+76 7-14 L 126.46

+50 3-14 R 181.40

211+96.64 $\begin{matrix} 80^\circ-36'-30'' \\ 40^\circ-28' R \end{matrix}$

211+29.78 B.C.

211+96.64 11-6" 31-

Road

9/24/30 Conners clear-hot
Hill
Mattoon
Remmen

52

Sta Angle Mag. B Calc. B.

S 61° W 560-58 W

218+77.27 E.C.

P.I. 218+22.73

Δ 8° 45' L

D 8°

T 57.83

L 109.37

R 716.78

17°-30'
218+22.73 8°-45' L

218+22.73 } 7' - 24' }

217+67.90 B.C.

S 70° W 569-43 W

217+60.67 E.C.

E.C. 33° 42' P.I. 217+09.79

+50 31.02 Δ 67° 24' L

+25 24.17 D 50°

217+00 18-32 T 78.84

+75 12-17 L 134.80

+50 6-02 R 118.21

134-48,
217+04.71 67° 24' L

217+09.79 } 28' - 7' }

216+25.87 B.C.

B.C. } 5' - 25' }

Road

Sta Angle Mag. B. Calc B.

✓
S 80° W S 79-38 W

223+70.90 EC.

P.I. 223+19.70

EC 22° 08' Δ 44° 16' L

+50 17-57 D 40

48° 31' 30"

223+19.70 44° 16' L

+25 12-57 T 59.16

223+00 7-57 L 110.66

176 2°-57' R. 146.19

222+60.24 BC.

✓
N 55-30 W N 56-06 W

221+33.24 EC.

EC. 31° 28'

+25 29-14 P.I. 220+68.79

221+00 24-29 Δ 62° 56' R

+75 19-14 D 42°

125° 52'

220+68.79 62° 56' R

+50 13-59 T 85.39

+25 8-14 L 149.84

220+00 3°-29' R = 139.51
6.146

219+83.40 BC.

138.71 ✓

EC. 4. - 20' }

223+19.70 } 16' - 15' }

BC. 4.55 - 23.5 }

road

EC. 3.5 - 28' }

220+68.79 - 14' } 25' }

220+22
- 2" water pipe

BC. 3.5 - 25' }

Sta. Angle Mag. B. Calc. B

S 86° W S 85-31 W

225+83.28 E.C.

P.I. 225+54.79

Δ 9°-10' R

D 16'

225+54.79 18°-20'
9°-10' R

T 28.80

225+54.79 | A - 22'

L 57.29

R 359.20

225+25.99 B.C.

S 76-30 W S 76-21 W

224+50.15 6°-34'
3°-17' L

224+50.15 | A - 18'

Road

101.74

79.64

Sta. Angle Mag. B Calc. B.

S 27-30 W S 27-09 W

228+53.14 EC.

Pl. 228+13.95

Δ 12°-38 L

EC. 6°-19' D 16°

228+13.95 25°-16' 12°-38 L

+50 6-04 T 39.77

+25 4-04 L 78.96

228+00 2-04 R 35.9.26

227+74.18 BC.

228+13.95 6' 24'

BC 4' 26'

145.48

165.92

S 39-30 W S 39-17 W

226+84.79 EC.

EC. 22°-52' R 226+56.22

+80 21-11 Δ 45°-11 L

+70 17-11 D 70°

226+56.22 91°-28' 45°-11 L

+60 14-11 T 36.76

+50 10-11 L 65.33

+40 7-11 R 87.17

+30 3-11

EC 5' 26'

226+56.22 11' 17'

BC 15' 25'

Read

226+19.46 BC.

Sta. Angle Mag. B. Calc. B

514°W 513-43W

231+43.68 EC.

P.I. 231+124

Δ 10°04' R

D 16°

T 31.64

L 62.91

R 359.26

231+12.41 20°08' 10°04' R

230+80.77 BC.

127.79

155.84

231+12.41 25' - 21' -

Road

EC 5' - 21' -

230+16.46 EC.

P.I. 229+88

EC 11-45 Δ 23°30'

230+00 10°06' D 20°

+757°36' T 59.89

+805°06' L 117.50

229+25 2°36' R 287.94

229+58.85 47°00' 23°30' L

228+98.96 BC.

229+58.85 11' - 20' -

229+00 24' 10" W of Road

BC 15' - 29' -

Sta. Angle Mag B. Calc. B

S. 49-30W S50-03W

2 235+42.54 EC.

P1. 235+06.30

A 23°52L

D 32°

L 74.58

T 38.34

R 181.90

2 235+06.30 17°44'
23°52L

2 234+67.96 BC.

S. 73-30W S73-55W

EC. 30.06

+70 25-44'

+60 22-56

2 232+85.60 EC.

+50 20-08 P1. 232+39.83

+40 17-20 A 60°12R

+30 14-32 D 56°

+20 11-44 T 61.73

+10 8-56 L 107.50

232+06-08 R 106.58

2 232+39.83 120°-24'
60°12R

2 231+78.10 BC.

+90 3°-20'

547.16

EC. | 3' - 23' |

235+06.30 | 8.5' - 17' |

Road

BC. | 3' - 20' |

282.43

EC. | 3' - 22' |

3" IRON WATER PIPE
232+77

232+39.83 - 8' | 22' |

BC | 5' - 20' |

Sta. Angle Mag. B. Calc. B.

9/22/3

Converse-clear hat
Hill
Mattoon
Rammen

58

pow.
pole
10' - 249+11

pow.
pole
7.5' - 247+93.

pow.
pole
2.2' } 13' - 23' }

pow.
pole
0' 6" - 244+95

pow.
pole
1.8' } 9' - 24' }

242+90 16' Cones culv.
Rubble hd. walls

EC. 3' - 24' }

Road 240+68

240+51.36

240+04
iron water pipe

BC. 4' - 24' }

Road

576-10W

246+43.50 1°-20'
0°40' R

575-30W 575-30W

242+95.32 4°06'
2°03' R

573-30W 573-27W

241+08.73 EC.

EC. 11°42' PI. 240+51.36

241+00 10-50 Δ 23°24' R

+76 8-20 D 20°

+50 5-50 T 59.63

+25 3-20 L 117.00

240+00 0-50 R 287.94

240+51.36 16-17-30
23°24' R

239+91.73 BF.

537.95

348.18

x

246.22

Sta Angle Mag. B. Calc. B.
569°W 569-44W

EC 33°-19'

+20 27-34

+10 29-04 P.I. 254+99.65

255+00 20-34 Δ 67°-38L

+90 17-04 D 70°

+80 13-34 T 58.39

+70 10-04 L 96.62

+60 6-34 R 87.17

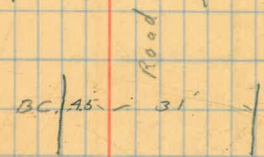
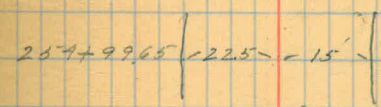
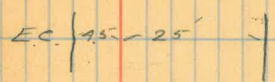
+50 3°-04'

2 253+37.88 EC.

135°-16'
254+99.65 67°38L

2 254+41.26 BC.

170.30



N41-30°W N42-38W

EC 30°-36'

+50 29-34 P.I. 251+81.45

+25 25-04 Δ 61°12R

252+00 20-34 D 36°

+75 16-04 T 95.69

+50 11-34 L 170.0

+25 7-04 R 161.80

251+00 2°-34'

252+55.76 EC.

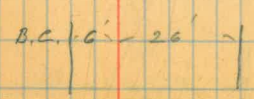
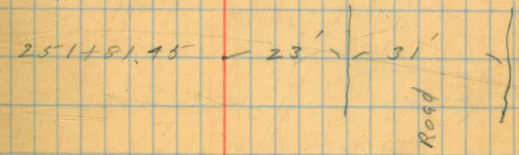
122°24'
251+81.45 61°12R

250+85.76 BC.

339.58



Table
P.O. 72 - 251+83 (on curve)



Sta. Angle Mag. B. Calc. B.

\downarrow
 S 66-30W S 58°00W
 8°40'
 257+24.83 4°20' L

x

257+24.83 | 45 - 19.5 |

75.23

\downarrow
 S 62°W S 62-30W

256+80.53 EC.

R 1 256+49.79

EC. | 55 - 24' |

14-18-30"

256+49.79 7°24' L

Δ 7°24' L

D 12°

T 30.93

x

256+49.79 | 65 - 24' |

L 61.67

R 478.34

256+18.86 BC.

BC. | 55 - 29' |

Road

Sta Angle Mag. B. Calc. B.
S73-30W S74-02W

260+72.52 EC.

260+54.74 $23^{\circ}08'$
 $11^{\circ}34'R$

260+36.37 BC.

259+03.22 $9^{\circ}40'$
 $4^{\circ}50'L$

S61°30'W S62-28'W

258+17.93 EC.

257+89.02 $18^{\circ}35'-30''$
 $9^{\circ}18'R$

257+59.80 BC.

Pl. 260+54.74

A $11^{\circ}34'R$

D 32°

T 18.37

L 36.15

R 181.90

260+54.74 | 5' - 20' |

259+03.22 | 45' - 21' |

Pl. 257+89.02

A $9^{\circ}18'R$

D 16°

T 29.22

L 58.13

R 359.26

EC. | 6' - 19' |

257+89.02 | 5.5' - 20' |

BC. | 5' - 16' |

9/23/30

Converse
Hill
Mattoon
Remmen

clear + warm

63

Sta. Angle Mag. B. Calc. B

S 65° W S 64-44 W

270+76.76 E.C.

P1 270+56.50

Δ 11° 30' L

D 28°

T 20.51

L 41.07

R 206.68

23° 00'
270+56.50 11° 30' L

270+56.50 | 155' 21' }

270+35.69 B.C.

S 76° W S 76-14 W

269+66.80 E.C.

P1

E.C. | 2' 23' }

150 12-05' Δ 28° 10' R

+50 12-04 D 24°

+25 9-01 T 60.33

269+00 6-07 L 117.36

+75 3-01 R 240.49

56° 20'
269+09.77 28° 10' R

269+09.77 | 6' 29' }

268+49.44 B.C.

B.C. | 2' 26' }

Sta Angle Mag. B. Calc. B.

273+87.25 6°-36'
3°18' L

↓
S48-13W

273+87.25 | 1' - 25' |

272+99.75 3°50'
1°55' L

↓
S57-31W

272+99.75 | 1' - 24' |

271+98.23 E.C.

↓
S54°W S53-26W

Pl. 271+63.15

E.C. | 1' - 22' |

D 11°-18' L

D 16°

271+63.15 22-36
11°-18' L

T 35.51

271+63.15 | 6' - 19' |

L 70.62

R 359.26

271+27.61 B.C.

B.C. | 1' - 23' |

271+04 [4' - 26'] 12" gal. scale

Sta. Angle Mag. B Calc. B.

S49-30W S49-69W

278+08.53 E.C.

P.I. 277+67.78

E.C. 16.59 Δ 33.58 R

67° 56'

277+57.78 33° 58' R

278+00 15-37 D 32°

+75 11-37 T 55.40

+50 7-37 L 106.15

+25 3-37 R 181.40

277+02.38 B.C.

278+63. }
3.5' } 16" Concr. Culvert }
23' }

E.C. 5' - 32' }

277+57.78 11' - 34' }

B.C. 6' - 32' }

S17-30W S16-01W

276+13.69 E.C.

E.C. 16.06'

276+00 14-11 P.I. 275+35.80

+75 12-14 Δ 32° 12' L

+50 9-11 D 20°

61° 24'

275+35.80 32° 12' L

+25 7-14 T 83.11

275+00 4-11 L 161.00

+75 2-14 R 287.94

274+52.69 B.C.

E.C. 4' - 29.5' }

275+35.80 17' - 13' }

B.C. 4.5' - 25' }

Sta. Angle Mag. Calc. B

S 68-30 W S 69-12 W

285+18.09 E.C.

P.I. 287+86.85

E.C. | 3' - 25' |

E.C. 13-50' Δ 27-40' R

+25 11-18 D 22°

287+86.85 55° 20' 27-40' R

288+00 8-33 T 64.52

287+86.85 Δ | 33' |

+75 6-48 L 125.76

+50 3-03 R 202.04

287+22.33 B.C.

B.C. | 4' - 25' |

621.57

S 41° W S 41-32 W

282+07.66 E.C.

P.I. 281+65.54

Δ 8-27 L

D 10°

281+65.54 16° 54' 8-27 L

T 42.38

281+65.54 | 6' - 18' |

L 84.50

R 573.69

281+23.16 B.C.

Sta. Angle Mag. Calc. B

S 84-30 W S 85-38 W

294+75.48 E.C.

P.I. 294+37.92

Δ 9° 03' R

D 12°

T 37.86

L 75.42

R 478.34

294+37.92 18° 06'
9° 03' R

294+37.92 } 2' - 24' }

294+00.06 B.C.

S 76-35 W

292+16.23 9° 40'
1° 30' L

292+16.23 } 1' - 19' }

S 81° W S 81-25 W

291+14.81 E.C.

P.I. 290+76.90

Δ 12° 13' R

D 16°

T 38.44

L 76.35

R 359.26

290+76.90 24° 26'
12° 13' R

E.C. } 1' - 22' }

290+76.90 } 25' }

20" riveted steel pipe (from Oyama at Home)
290+68

290+38.46 B.C.

B.C. } 1' - 23' }

Sta. Angle Mag. B. Calc. B.

2

303+62.55
8°-30'
4°-15' L

S81°W S86-06W

2

303+62.55 | 4' - 20' - |

2

302+45.09 EC.

S88-30W N29-39W

Pi. 301+85.31

EC. | 4' - 21' - |

A 14°-27R

D 12°

T 60.64

L 120.12

R 478.34

301+85.31 | 31' - |

2

301+85.31
28°-54'
14°-27' R

BC. | 5' - 26' - |

301+22 ^{pool}/_{pool} 6'

301+24.67 BC.

2

299+46.96
9°-53'-30"
4°-57' L

S75°W S75-54W

299+46.96 | 5' - 21' - |

2

298+12.05
9°-34'
4°-47' L

S80-51W

298+12.05 | 5' - 20' - |

Sta. Angle Mag. B. Calc. B.

9/21/30

Converse clear hot
Hill
Mottaan
Remmen

69

S 97-30 W S 76-48 W

307+73.88 E.C.

E.C. 13.59 P. 307+05.75

E.C. 21

+50 11-36 Δ 27.50

+25 9-06 D 20

307+05.75 55° 56'; 27° 38' L

307+00 6-36 T 71.20

307+05.75 13' 14'

+75 4-06 L 152.25

+50 1-36 R 287.94

306+34.05 B.C.

B.C. 22

305+37.98 E.C.

P. 305+02.30

S 76° W S 74-46 W

Δ 11° 20' L

305+02.30 22° 40'; 11° 20' L

D 16'

305+02.30 5' 20'

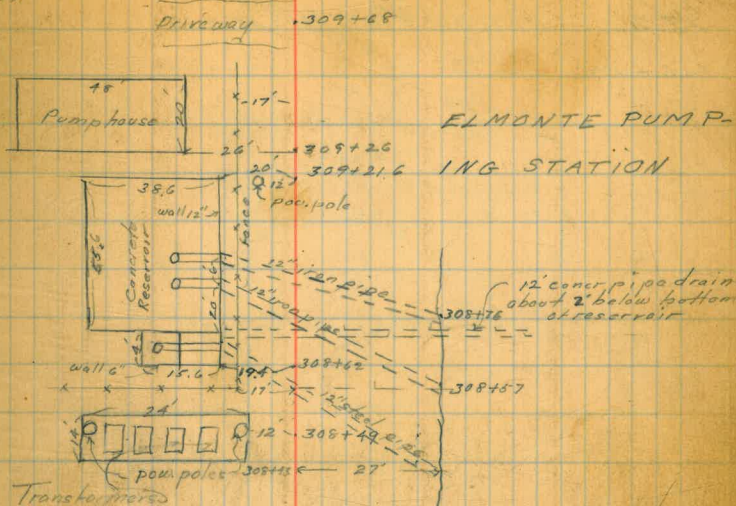
T 35.66

Road

304+66.65 B.C.

L 70.83

R 359.26



Sta. Angle Mag. B Cale. B
P.O.T.

326+15.92

9/21/30

Converse
Mill
Mottson
Remman

clear & warm

70

Road 327+46

12" galv. pipe 326+36.3

pow. pole 325+65
8' - 5' 28' 12'

2" steel water pipe 325+49.0

Road 325+65

325+35.2 2" steel water pipe

324+86.0 10' 5'

Road 324+42.15

30' 12" Galv. Iron pipe

pow. pole 323+17

pow. pole 320+16

Abandoned Wind Mill 317+72 2" Pipe (Not in use)
25' 317+65

317+23

pow. pole 317+18

Road 315+73

pow. pole 314+16

314+05.55 36' 6' Fence

1492.9

S 47-26W

311+23.00 0°38'R

Sta. Angle Mag. B. Calc. B.
 S 30-30 W S 28-35 W

338+22.80 EC.
 18°44'
 337+89.32 S 22 R
 337+55.72 BC.

Abandoned
 Sec Book #327
 Page 37

P.I. 339+89.31
 Δ 5°22' R
 D 8°
 T 33.60
 L 67.08
 R 716.78

10°41'30"
 332+75.05 S 24-30 W S 23°13 W
 25' R

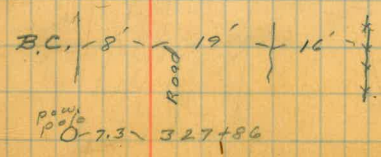
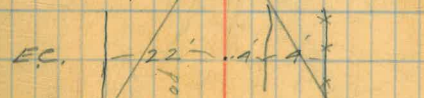
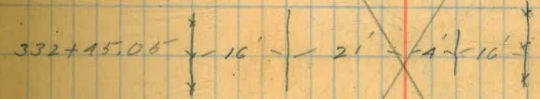
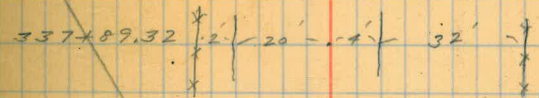
S 23-30 W S 22°22 W
 329+87.02 EC -

50°08'
 329+10.22 25°04 L

328+30.35 BC.

EC. 12-32 P.I. 329+10.22
 +75 11-34 Δ 25°04 L
 +50 9-34 D 16°
 +25 7-34 T 79.87
 329+10 5-34 L 156.67
 +75 3-34 R 359.26
 +50 1-34

429.94
 544.27
 337.00
 294.3



Sta. Angle Mag. B. Calc. B.

348+50.22 P.O.T.

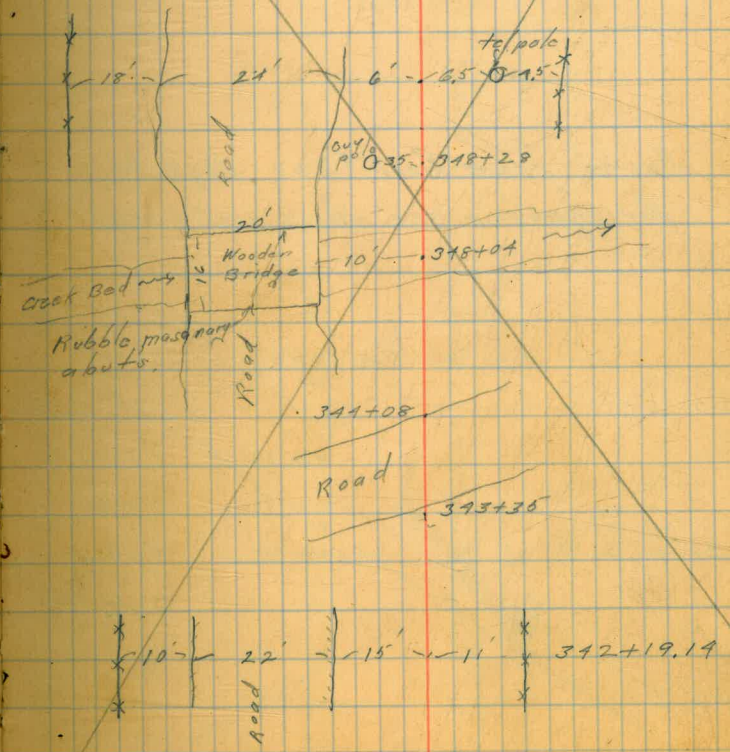
Abandoned.

1174.17

S27°30'W S25-27W

342+19.14 6-16-30" 3°08'L

Nota Row of pepper, eucalyptus & cypress trees 34' to left of line from sta. 348+50 to sta. 354



Sta Angle Mag. B. Cal. B.

S80-45W S80-22W

368+96.34 1°27' L

1414.4

X

Begin. of eucalyptus trees on both sides of road

435.88

X

S82°W S81-19W

3°12' 364+60.16 1°36' R

364+60.16

364+76

364+20

363+41

end of row of trees

Contd. From Book #327, Page 36.
For equasion see above book + page.

S81°W S80-13W

354+46.08 EC

R.I. 353+93.31

EC 27°22' D 54°46' R

+25 22-32 D 46°

109°52' 353+93.31 54°46' R

354+00 16-47 T 66.29

+75 11-02 L 119.99

+50 8°17' R 122.97

Abandoned.

353+27.92 BC

Begin. of row of eucalyptus trees

EC 10'

29'

22'

353+93.31

12'

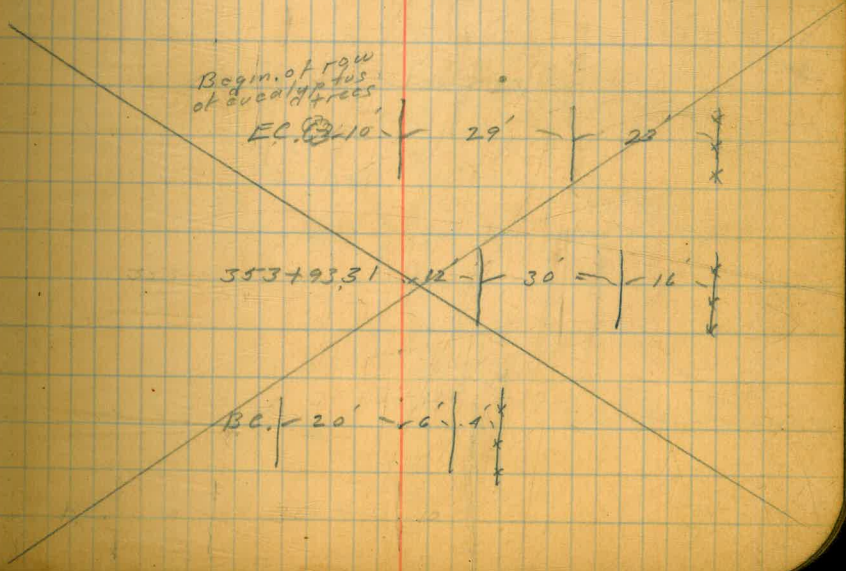
30'

16'

BC 20'

10'

11'

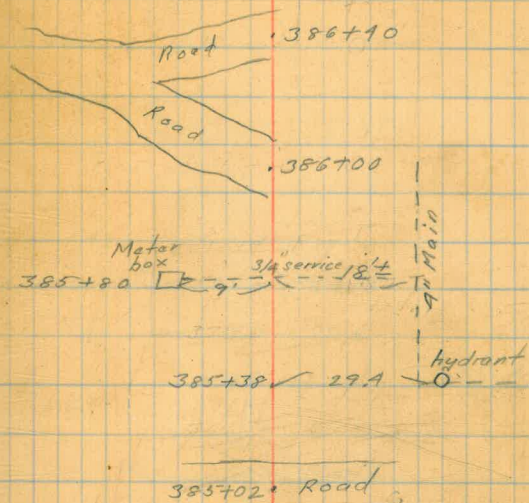


Sta. Angle Mag. B. Calc. B.

9/25/26

Converse part cloudy - warm
Hill
Mottson
Remmen

74

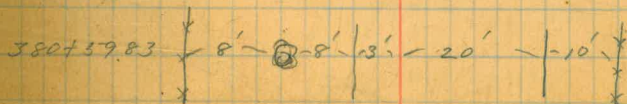
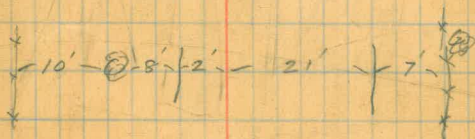


power pole
13' 384+83

384+24 [18" Cor. iron culv. 5' 25']

804.25

x



383+10.74 0°22'
0°11' L

S 81° W S 80-11 W

380+59.83 P.O.T.

Sta. Angle Mag. B. Calc. B.

9/26/30

Converse clear + warm
Hill
Mutton
Remmon

75

S 81° 15' W S 80° 11' W

391+1997 P.O.T.

537.45

Water Meter
394+83 9' 3/4" SERVICE
18"

power pole O 9.1 - 394+98

Road 394+90

power pole O 10' - 392+98

392+15 30'

End of row of
eucalyptus
trees on right

End of row of eucalyptus trees
on left

Meter box
390+59
3/4" SERVICE

Road 390+39

Road 389+80

Road 388+79

Meter box
10' - 388+58
18"
3/4" SERVICE

Sta. Angle Mag. B. Calc. B.

396+57.92 $0^{\circ}10'$
 $0^{\circ}05' R$

S 80-45 W S 80-16 W

1108.46

x

396+57.92 $0^{\circ}09'$ 21' x 11' x

Road 396+19

Water
pole $0^{\circ}09'$ 395+94
 $3/4$ service

Cement work 3' 395+82

76

Road 406+21

406+16 $3/4$ service

405+59 $3/4$ service

Road 405+21

Road 404+85

power
pole $0^{\circ}09'$ 404+64

403+17

403+09 $3/4$ service

Road 402+75

power
pole $0^{\circ}09'$ 402+14

401+12 $3/4$ service

Road 400+62

power
pole $0^{\circ}09'$ 399+54

Sta. Angle Mag. B. Calc. B.

N 84-30W N 85-53W

411+75.15	EC.	EC. 16-27 1/2	PI. 411+08.98
		+50 13-27	
		+25 10-27	Δ 32° 57' L
411+08.98	32° 57' L	411+00 7-27	D 24°
		+75 4-27	T 71.12
410+37.86	BC.	+50 1° 27'	L 137.29
			R 240.99

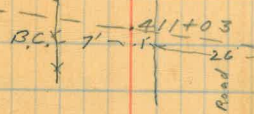
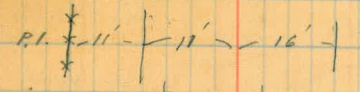
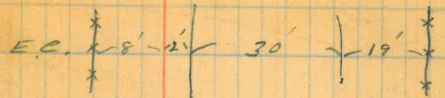
N 52-30W N 52-56W

409+74.03	EC.	PI. 409+25.39
		Δ 91° 46' L
409+25.39	41° 46' L	D 40
		T 55.78
408+69.61		L 104.42
409+74.03	BC.	R 146.19

N 10°-30W N 11-10W

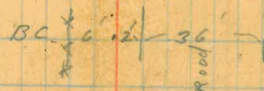
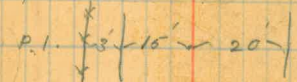
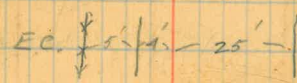
407+96.33	EC.	PI. 407+65.88
		Δ 88° 34' R
		D 90°
407+65.88	88° 34' R	T 68.96
		L 98.41
406+96.92	BC.	R 70.71

406.51



Proposed 24" pipe line from Los Cochas creek to Lake Lindo To be placed about 1' below road.

190.73.



199.02



Note Property line Files not exact.

on S. Tangent

Sta. Angle Mag. B Calc. B.

N27°30'W N27-19W

418+87.26 E.C.

P.I. 418+17.89

EC 10°47' Δ 21°34' R

+75 10-03 D 16°

+50 8-03 T 68.72

+25 6-03 L 137.79

418+00 1-03 R 352.26

+75 2°03

417+49.47 BC.

N49°W N48-53W

EC 18°30'

+50 17-58 P.I. 415+10.54

416 18-58 Δ 37° R

+50 11-58 D 12°

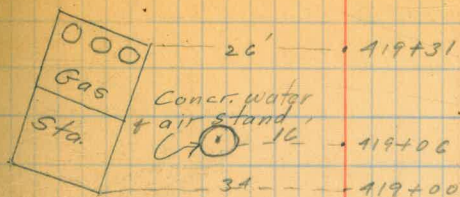
415 8-58 T 160.05

+50 5-58 L 308.33

414+00 2-58 R 478.34

413+50.49 BC.

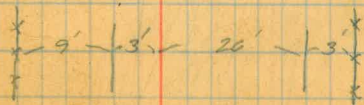
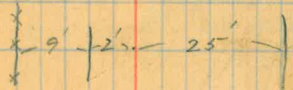
78



185.42



317.12



X

Sta. Angle Mag. B Calc. B

423+56.5 Tie to end of El Capitan Pipe Line

423+2780 P.O.T.

420+29.93 E.C.

420+01.26 $111^{\circ}31'$
 $72^{\circ}17' L$

419+19.62 B.C.

$S 80^{\circ}24' W$

P.I. 420+01.26

$\Delta 72^{\circ}17' L$

D 90°

T 51.61

L 80.31

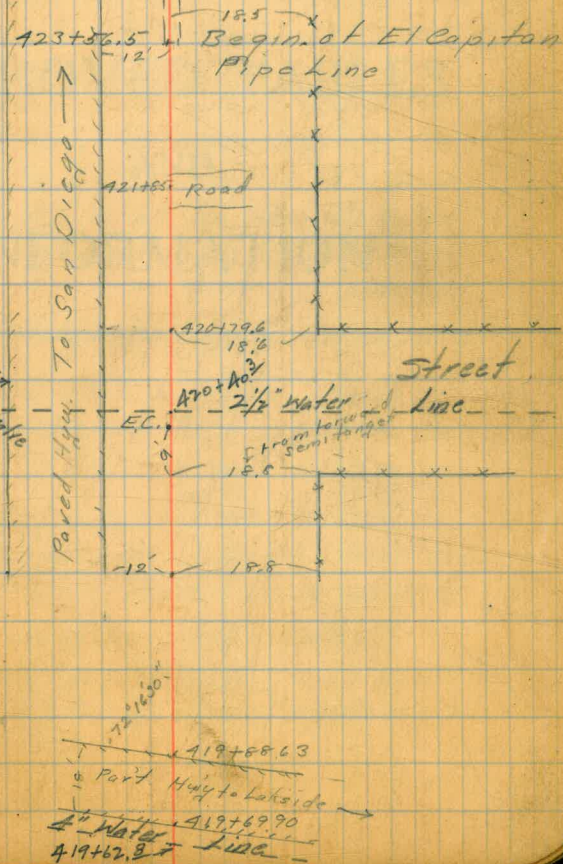
R 70.71

378.21

$\pm 7^{\circ}$

Water Line

Paved Hwy. To San Diego



DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double-entry method in left column and top row. The number in body

from side stake to slope stake. If ground is not

IMPROVED TABLES
AND
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

$$391 + 19.97$$

$$\frac{9}{10} \frac{124}{25}$$

$$10 \cdot 11$$

$$828$$

1.43' into old

line from apt 20 + 29.28

$$9 + 33.8$$

$$1.177$$

$$10 + 41.5$$

1.43' L off line from apt

$$2396$$

$$41 + 67.46$$

$$2396$$

$$2391.42$$

$$71 \frac{78.79}{75.91}$$

$$72 + 54.20$$

$$96.15$$

$$231 + 43.68$$

$$232 + 39.83$$

$$308 + 62$$

$$309 + 25.6$$

$$309 + 25.6$$

$$308 + 62$$

$$309 + 21.6$$

$$70 + 97.47$$

$$26.29$$

$$71 + 23.75$$

$$123 + 56.50$$

$$120 + 29.93$$

$$326.57$$

$$51.64$$

$$378.21$$

$$51.64$$

$$100$$

$$78.25$$

$$414 + 21.75$$

$$378.21$$

$$417 + 99.96$$

Page 51 sta 211 + 96

$$10 + 85.78$$

$$35.23$$

$$10 + 50.55$$

6/24/61