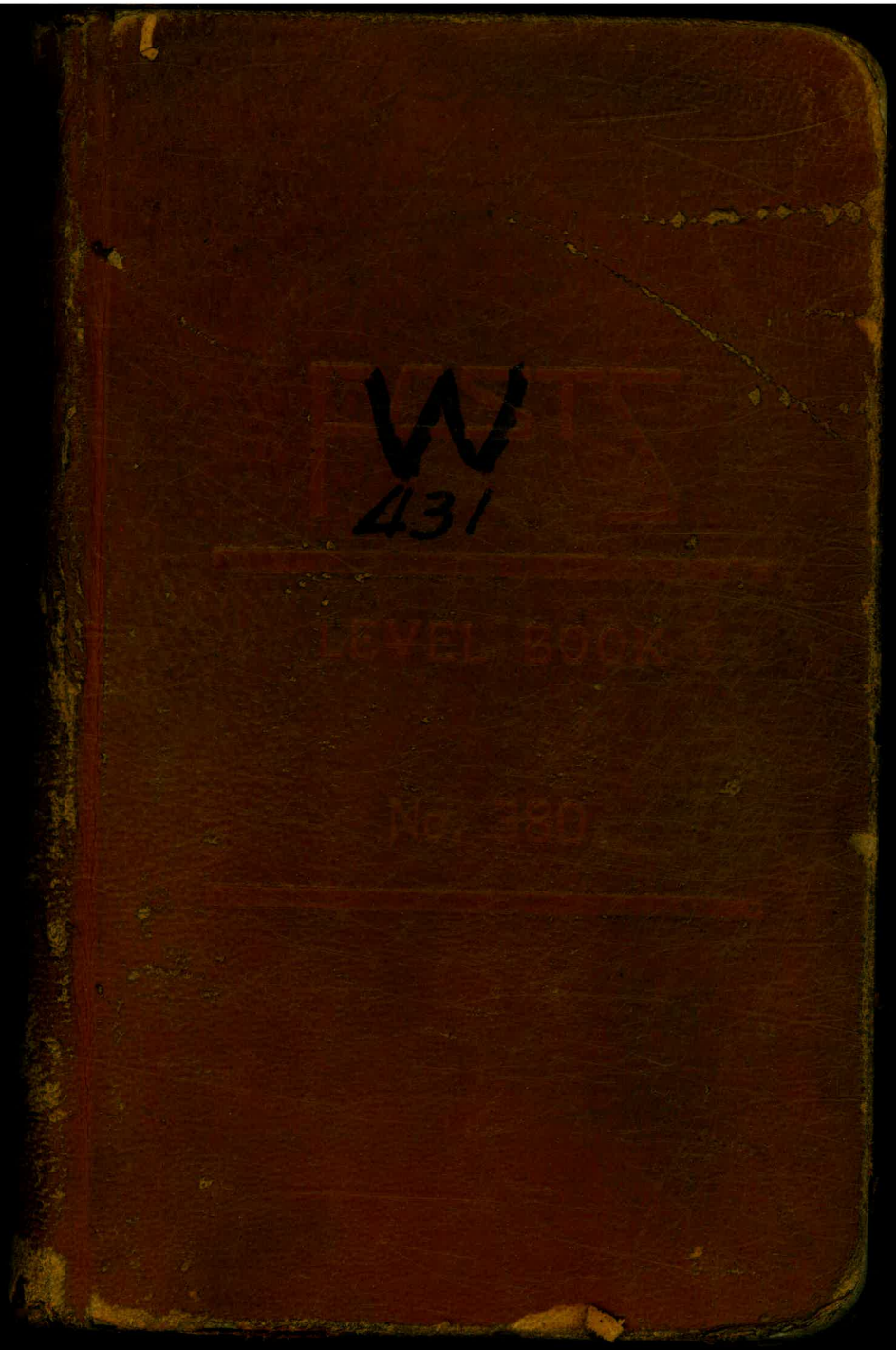
W
431

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ENGINEERING and DRAFTING SUPPLIES

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X sections for Est. #10 of
Spillway Exc. Mar 3-1933

B.M.	12.54	631.54		619.00
	6.85	637.55	0.84	630.70

E4540 (No Exc. on E4520)

N4305			0.G
4295	6.7	30.9	
80	6.9	30.7	
60	6.4	31.2	
40	7.0	30.6	
4220	6.1	31.5	

E4560

4200	5.2	32.4
20	6.2	31.4
40	6.5	31.1
60	5.8	31.8
80	6.5	31.1
4295	6.2	31.4
4305		0.G

Plotted

4320	
4305	
4280	
60	
40	
20	
4200	
4180	
60	
4140	
60	
4180	
4200	
40	
4280	
4315	
25	

Plotted

Elliott Notes
Simpson ↑
Soper-Remmers Ch.

637.55 E4580

		0.G
6.4	31.2	
6.1	31.5	
5.7	31.9	
5.8	31.8	
5.8	31.8	
5.0	32.6	
4.2	33.4	
3.8	33.8	

E4600

2.6	35.0	
2.6	35.0	
3.7	33.9	
4.5	33.1	
5.1	32.5	
5.8	31.8	
5.8	31.8	
		0.G

637.55 E4620

4315			O.G
4310	5.4	32.2	
4280	5.4	32.2	
40	5.1	32.5	
4200	4.4	33.2	
4160	2.3	35.3	
4120	0.8	36.8	
4115			O.G

E4640

4125			O.G
35	1.2	36.4	
60	2.9	34.7	
4200	4.3	33.3	
40	4.9	32.7	
80	5.0	32.6	
4300	2.6	35.0	
4305			O.G

Plotted

E4660

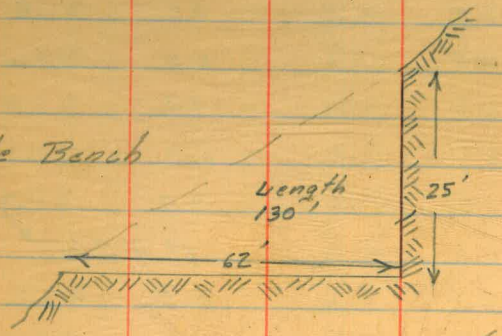
4280			O.G
250	+9.0	46.6	
40	+1.0	38.6	
4200	1.3	36.3	
4160	0.3	37.3	
4140	+3.0	40.6	
4130			O.G

637.55 E4680 (4690 is orig. Ground)

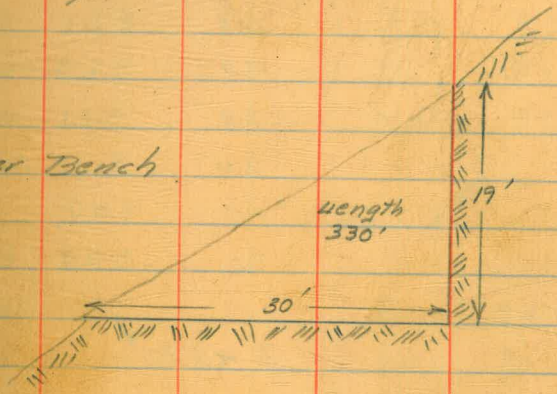
4140			O.G
4160	+12.2	49.8	
4220			O.G
Check	2.8	634.8	Cut Stake M sinks at 10+00

Plotted

Middle Bench



Upper Bench



Elliott - Notes
Simpson - T
Soper - H. Ch.
Temmen - R. Ch.

X Sections of Spillway Est. #11

Mar 29 - 1933

plotted - F. O.

B.M.	6.31	638.95		632.64

No Excavation on E 4520

E. 4540 ✓

N. 4305			O.G
4290	8.4	30.5	
80	8.5	30.4	
60	7.9	31.0	
40	8.2	30.7	
20	7.9	31.0	

E 4560 ✓

4180	6.7	32.2
4200	6.8	32.1
20	7.9	31.0
40	7.8	31.1
60	7.4	31.5
80	8.0	30.9
4290	8.0	30.9
4310		O.G.

E 4580 ✓

4320			O.G.
4300	7.7	31.2	
4280	7.8	31.1	
60	7.3	31.6	
40	7.5	31.4	

638.98

E 4580 ✓

N 4220	7.4	31.5
4200	6.5	32.4
80	5.8	33.1
60	5.4	33.5

E 4600 ✓

4120	3.7	35.2
40	4.1	34.8
60	4.5	34.4
80	5.1	33.8
4200	5.9	33.0
20	6.3	32.6
40	6.7	32.2
60	7.2	31.7
80	7.6	31.3
4310	7.7	31.2
4330		O.G

E 4620 ✓

4330		O.G
4310	4.1	34.8
4280	7.5	31.4
60	7.5	31.4
40	6.6	32.3
20	5.8	33.1
4200	5.4	33.5
4180	4.8	34.1

	638.95		E4620 ✓
4160		3.7	35.2
40		3.4	35.5
30		3.2	35.7
20			O.G.
			E4640 ✓
4120			O.G.
30		2.7	36.2
40		3.4	35.5
60		4.4	34.5
80		4.9	34.0
4200		5.8	33.1
20		6.6	32.3
40		7.0	31.9
60		6.0	32.9
80		+1.2	40.1
4310			O.G
			E4660 ✓
4320			0.G
4310			655.5
280			659.0
230		+0.4	39.3
4210		1.0	37.9
4190		+1.7	40.6
80		+1.2	40.1
60		1.1	37.8

		638.95	E4660 ✓
N4150			1.3 37.6
40			+2.1 41.0
30			O.G
			E4680 ✓
4130			O.G
4140			+13.7 52.6
60			+13.7 52.6
4180			+13.7 52.6
Elev.	12.90	667.05	654.15
4230			1.3 65.7
4270			6.6 60.4
4290			O.G
			E4700 ✓
4175			O.G
4190			+2.8 69.8
4230			+0.4 67.4
B.M.	0.20	696.56	696.36
4240			15.5 81.1
T.P.	0.41	684.54	12.43 684.13
4280			7.6 76.9
4300			9.8 74.7
20			11.4 73.1
40			12.3 72.2

		684.54	E 4700 ✓		
4360			12.4	72.1	
70					0.G
			E 4720 ✓		
4370					0.G
60			10.8	73.7	
40			10.9	73.6	
20			9.6	74.9	
4300			8.3	76.2	
4280			7.0	77.5	
60			4.8	79.7	
40			2.1	82.4	
B.M.	0.20	696.56		696.36	
20			11.1	85.5	
4200			8.1	88.5	
4190			6.6	90.0	
4180					0.G
			E 4740 ✓		
4110					0.G
15			+2.3	98.9	
40			+0.4	97.0	
60			1.9	94.7	
80			5.3	91.3	
4200			8.6	88.0	
20			11.1	85.5	

outside of slope stakes

		696.56	E 4740 ✓		
4240			14.0	82.6	
60			10.9	85.7	
80			14.0	82.6	
		684.54			
4300			6.5	780	
20			5.8	78.7	
40			6.8	77.7	
55			2.9	81.6	
70					0.G
B.M.	0.20	696.56	696.36		
T.P.	12.40	708.58	0.38	696.18	-0.48
			E 4760 ✓		4 11 88
4110					0.G
20			8.1	00.5	
40			9.1	99.5	
60			8.8	99.8	
80			4.8	03.8	
4200			3.1	05.5	
20			1.4	07.2	
40			0.0	08.6	
50					0.G
			E 4780 ✓		
4120					0.G
30			3.6	050	
40			6.1	02.5	

		708.58	4780 ✓		
4160			6.5	02.1	
80			4.9	03.7	
4200			2.6	06.0	
20			1.1	07.5	
40			+0.2	08.8	
	11.88	Transit 719.98	0.48	708.10	
60			10.0	10.0	
80			9.0	11.0	
4300			7.6	12.4	
20			5.6	14.4	
40			3.6	16.4	
50					O.G
T.P.	11.02	Level 730.38	0.62	719.36	
Check on H.I.			4.6	725.8	Slope Stake 6+87.59 725.8
			E 4800 ✓		
4435					O.G
30			3.5	26.9	
20			4.7	25.7	
4400			5.9	24.5	
80			8.0	22.4	
60			10.7	19.7	
40		719.98			
40			2.8	17.2	
20			4.7	15.3	
4300			6.2	13.8	

		719.98	E 4800 ✓	
N 4280			8.2	7.18
60			9.0	11.0
40			9.1	10.9
20			11.2	08.8
4200			11.6	08.4
4180			10.0	10.0
60			8.3	11.7
40			3.1	716.9
20				O.G.
			E 4820 ✓	
B.M.	0.91	759.25		758.34
4135				O.G.
50				735.0
4200			30.9	28.4
↑ Straight				
↓				
4280		719.98	3.5	16.5
4300			3.7	16.3
20			3.5	16.5
40			1.1	18.9
		730.38		
60			8.6	21.8
80			6.4	24.0

		730.38	E 4820 ✓		
N 4400			4.0	26.4	
20			2.6	27.8	
30			1.9	28.5	
40					O.G
		759.25			
			E 4840 ✓		
4145					O.G
4155			6.2	53.1	
4210			11.0	48.3	
↓ Straight →					
		730.38			
4280			+2.3	32.7	
4300			2.7	27.7	
20			8.6	21.8	
40			10.9	19.5	
60			5.2	25.2	
80			0.6	29.8	
T.P.	12.60	Level 742.90	0.08	730.30	
4400			14.0	28.9	
20			12.4	30.5	
40			12.9	30.0	
52					O.G.

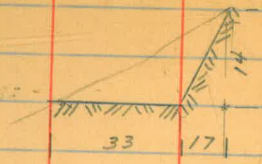
				E 4860 ✓	
B.M.	11.97	770.31		758.34	
T.P	6.79	776.96	0.14	770.17	
4145					O.G.
4160			5.5	71.5	
4180			8.1	68.9	
4200			11.4	65.6	
↑ Straight ↓					
N 4280		Level 742.90	+3.6	46.5	
4300			1.8	41.1	
20			6.0	36.9	
40			8.6	34.3	
60			5.8	37.1	
80			9.1	33.8	
4400			10.8	32.1	
20			10.9	32.0	
40			11.0	31.9	
50			3.8	39.1	
	10.93	Transit 753.65	0.18	742.72	
4461					O.G.
		776.96	E 4880 ✓		
4110					O.G
4120			3.8	73.2	

		776.96	E 4880 ✓		
4140			4.0	73.0	
60			6.5	70.5	
80			7.2	69.8	
4200			11.0	66.0	
↑					
Straight					
↓		753.65			
4280			4.2	49.5	
4300			7.3	46.4	
20			10.1	43.6	
		742.90			
40			2.4	40.5	
60			5.1	37.8	
80			7.3	35.6	
4400			7.9	35.0	
20			8.6	34.3	
40			8.9	34.0	
50			2.6	40.3	
60					O.G
			E 4900 ✓		
4120					O.G.
30				773.2	
Elev.	0.64	808.84		808.2	
4200			23.4	85.4	

		E 4900 ✓		
	753.65			
4280		+1.0	54.7	
4300		3.2	50.5	
20		8.0	45.7	
40		9.1	44.6	
60		10.4	43.3	
80		10.3	43.4	
4400		1.0	52.7	
4470				O.G
	End Mar 30 - 1933			
	Start Mar 31 - 1933			
		E 4920 ✓		
4220	808.8			O.G
4260		18.5	90.3	
4320			764.2	
4380				O.G
		E 4940 ✓		
4280				O.G
4320			782.7	
4360				O.G
E 4950 is original ground				

ROAD ON E. SIDE SPILLWAY
Monthly Est # 11 - April 4 - 1933

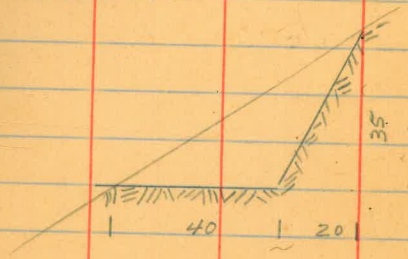
East End



= 231 □'

80'

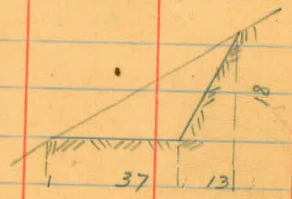
465.5 x 80 = 37,240 ft³



= 700 □'

65'

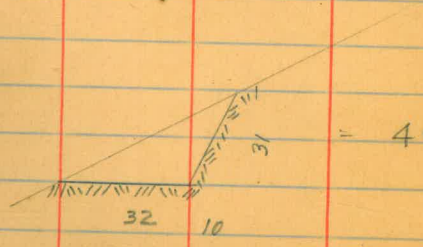
516.5 x 65 = 33,572.5



= 333 □'

50'

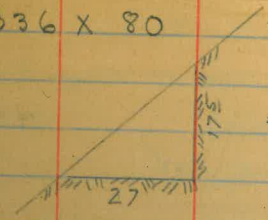
414.5 x 50 = 20,725



= 496 □'

80'

336 x 80 = 26,880



= 236 □'

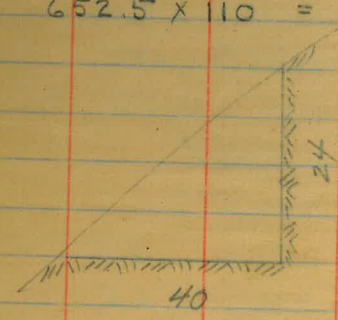
75

530.5 x 75 = 39,787.5

= 825 □'

110

652.5 x 110 = 71,775



= 480 □'

125'

240 x 125 = 30 000

259,980 ft³

0.0 Cu. End about E5000

259,980 ÷ 27 = 9,629 Cubic Yards

X Sections of Spillway
Estimate #12 - May 2 - 1933

E 5520 is Orig. Ground

B.M.	12.51	754.48		741.97	
		E 5500 ✓			
N 4330					O.G
4306			11.2	43.3	
4281			12.5	42.0	
4270			19.0	35.5	Slope to O.G.
		E 5480 ✓			
4270			15.4	39.1	Slope to O.G.
77			11.1	43.4	
4320			8.0	46.5	
4343			+3.3	57.8	
4345					O.G
		E 5460 ✓			
4260					O.G
4270			9.9	44.6	
4320			6.5	48.0	
45			+1.2	55.7	
52					O.G
		E 5440 ✓			
43.55					O.G
40			+3.6	58.1	
43.20			4.7	49.8	
4270			8.5	46.0	
4258					O.G

Plotted 3/4/33 F.O. - R.E.L. 12

		754.48	E 5420 ✓		
4273					O.G
4283			5.0	749.5	
4327			2.2	52.3	
4348			+9.3	63.8	
4360					O.G
			E 5400 ✓		
4280					O.G
4294			2.6	51.9	
4335			0.0	54.5	
4364			+10.0	64.5	
4378					O.G
			E 5380 ✓		
T.P.	13.05	766.83	0.70	753.78	
4276					O.G
4312			13.1	53.7	
4356			9.0	57.8	
4376			0.9	65.9	
4383					O.G
			E 5360 ✓		
4305			24.4	42.4	Slope to O.G.
27			10.6	56.2	
60			7.1	59.7	
80			0.0	766.8	
4393					O.G.

		766.83	E 5340 ✓		
N. 4300					O.G
36			11.2	755.6	
70			6.1	60.7	
4390					O.G
			E5320 ✓		
4310			21.2	45.6	510 pc to O.G
34			5.3	61.5	
50			4.2	62.6	
70			4.2	62.6	
4385					O.G
			E5300 ✓		
4285					O.G
4320			2.6	64.2	
51			3.2	63.6	
72			+8.6	75.4	
4380					O.G
			E5280 ✓		
4303					O.G
4310			0.3	66.5	
43			1.2	65.6	
54			+5.4	72.2	
43 64					O.G
T.P.			0.75	766.08	
	12.05	778.13			

		778.13	E5260 ✓		
4342					O.G
41			5.0	773.1	
29			10.4	67.7	
4304			10.5	67.6	
4280					O.G
			E5240 ✓		
4338					O.G
28			4.4	73.7	
20			8.4	69.7	
4304			8.2	69.9	
4280					O.G
			E5220 ✓		
4335					O.G
20			6.5	71.6	
4298			6.8	71.3	
4294					O.G
			E5200 ✓		
4285					O.G
4295			5.4	72.7	
4330			3.5	74.6	
40			+2.9	81.0	
4345					O.G

		778.13	E5180 ✓		
4372					0.G
60			+16.0	794.1	
4330			1.9	80.0	
4297			3.3	74.8	
4270					0.G.
			E5160 ✓		
4454					0.G
	12.46	808.71		796.05	
4400			0.2	808.5	
4380			-0.2	08.5	
		778.13			
4330			0.1	778.0	
4297			0.9	77.2	
4280					0.G
			E5140 ✓		
4280					0.G
T.P.	11.86	789.60	0.39	777.74	
4298			10.1	79.5	
4328			10.1	79.5	
		808.71			
4373			0.2	808.5	
4405			0.5	08.2	
4425			+13.0	21.7	
4440					0.G

		808.7	E5120 ✓		
4434					0.G
4420			+11.0	819.7	
4400			1.6	07.1	
4360			2.3	06.4	
		789.60			
4322			7.6	782.0	
4294			9.0	80.6	
4273					0.G
			E5100 ✓		
4280					0.G
4293			6.0	83.6	
4316			5.7	83.9	
		808.7			
4348			4.1	804.6	
4393			2.6	06.1	
4411			+7.8	16.5	
4415				835.2	
4428					0.G
			E5080 ✓		
B.M.	10.76	806.81		796.05	
4427					0.G
4409			+15.6	22.4	
4380			1.6	05.2	
4336			3.9	02.9	

		789.60	E5080 ✓		
4308			3.8	85.8	
4280			3.3	86.3	
4270					O.G
		806.81	E5060 ✓		
4444					O.G.
4397			0.9	05.9	
4360			4.3	02.5	
4326			4.8	02.0	
		789.60			
4300			2.8	86.8	
4265			1.8	87.8	
4255					O.G
		806.81	E5040 ✓		
4443					O.G
4395			2.1	04.7	
4340			5.9	00.9	
4310			5.7	01.1	
		789.60			
4290			1.2	88.4	
50			+0.7	90.3	
40					O.G
T.P.	12.53	802.10	0.03	789.57	

		802.10	E5020 ✓		
4230					O.G
34			9.9	92.2	
4280			11.5	90.6	
4290			2.6	99.5	
4320			2.1	00.0	
40			1.5	00.6	
60			0.4	01.7	
4390			+2.9	05.0	
T.P.	10.76	806.81	6.05	796.05	
			End May 2-1933		
			Start May 3-1933		
4481					O.G
			E5000 ✓		
4470					O.G
4440			0.0	06.8	
4380			4.0	02.8	
4360			6.0	00.8	
4320			7.0	99.8	
4285			8.6	98.2	
4274			13.8	93.0	
4230			13.7	93.1	
25					O.G

		806.81	E4980 ✓		
4467					O.G
4450			72.0	08.8	
4400			3.0	03.8	
4360			5.3	01.5	
4320			7.1	99.7	
4280			9.3	97.5	
60			12.1	94.7	
4230			11.8	95.0	
4220					O.G
			E4960 ✓		
	4.5	811.3	0.0	806.8	
4470					O.G
4451			2.5	08.8	
4420			4.1	07.2	
4330			11.0	00.3	
		806.81			
4280			9.8	97.0	
4240			12.2	94.6	
4210			12.7	94.1	
4200					O.G
B.M.	1.55	797.60		796.05	

		797.60	E4940 ✓		
4125					O.G
4130			21.3	76.3	
4150			19.6	78.0	
4190			12.3	85.3	
4250			2.9	94.7	
	5.77	801.82		796.05	
4280			4.5	97.3	
4329			22.7	79.1	
4364			9.7	92.1	
4430			18.7	93.1	
4490					O.G
			E4920 ✓		
4500					O.G
	4.79	800.84		796.05	
	0.0	794.39	6.45	794.39	
4447			25.5	68.9	
4387				755.8	
4362			19.6	74.8	
4315			32.7	61.7	
4270			3.3	91.1	
	4.79	800.84		796.05	
4243			11.3	89.5	

800.84 E4920 ✓

4218			32	97.6
4212			10.3	90.5
	0.0	783.7		783.7
4160			5.9	77.8
4120			8.9	74.8
4110				0.0

West of 4920 Same as last month.

Spillway Cross Sections for Estimate No. 13

B.M.	12.16	615.98		603.82	
			E.4420		
N.4180			6.9	609.1	✓
90			5.6	610.4	✓
4200			4.9	611.1	✓
10			4.0	612.0	✓
20			3.3	612.7	✓
30			1.6	614.4	✓
40			+0.4	616.4	✓
50			+0.6	616.6	✓
60			+1.0	617.0	✓
B.M.	1.84	634.48		632.64	
			E.4430		
N.4280			5.2	629.3	✓
4270			4.7	629.8	✓
63			10.0	624.5	✓
		615.98			
58			+0.4	616.4	✓
50			+0.3	616.3	✓
40			+0.1	616.1	✓
30			+0.5	616.5	✓
20			3.4	612.6	✓
10			4.5	611.5	✓
4200			5.4	610.6	✓
4190			6.4	609.6	✓

May 29. 1933.
Converse - Recording
Simpson - Inst.
Loudon - Chain
Soper - Chain
Carter - Stakes

	E.4430		
4180	615.98	7.0	609.0 ✓
74		7.5	608.5 ✓
	E.4440		
N.4160		8.7	607.3 ✓
70		8.5	07.5 ✓
80		7.7	08.3 ✓
90		6.6	09.4 ✓
4200		5.6	10.4 ✓
10		4.4	11.6 ✓
20		2.4	13.6 ✓
30		0.1	15.9 ✓
40		0.0	616.0 ✓
50		+0.1	616.1 ✓
54		+0.1	16.1 ✓
	634.48		
55		12.4	622.1 ✓
60		9.7	24.8 ✓
70		5.0	29.5 ✓
80		5.3	29.2 ✓
	E.4450		
N.4280		5.3	29.2 ✓
70		5.1	29.4 ✓
60		8.8	25.7 ✓
5.2		12.3	22.2 ✓

	615.98		E. 4450		
N. 4250		+0.8	616.8		
40		+0.5	616.5	✓	
30		0.2	615.8	✓	
20		0.0	616.0	✓	
10		2.6	613.4	✓	
4200		5.2	610.8	✓	
4190		6.8	609.2	✓	
80		8.0	608.0	✓	
70		9.2	606.8	✓	
60		10.1	605.9	✓	
55		9.8	606.2	✓	
50		13.9	602.1	✓	
40		20.1	595.9	✓	
30		22.7	593.3	✓	
20		29.2	586.8	✓	
10		30.2	585.8	✓	
4100		32.8	583.2	✓	
4090		34.5	581.5	✓	
80		33.5	582.5	✓	
75		33.0	583.0	✓	
72		24.7	591.2	✓	
60		24.1	591.9	✓	
			E. 4460		
N. 4060		23.4	592.6	✓	
70		24.2	91.8 ~~93.8~~	✓	
80		24.9	91.1 ~~93.1~~	✓	

	615.98	E. 4460		
N. 4090		24.6	591.4	✓
4100		23.8	92.2	✓
10		22.0	94.0	✓
20		19.6	96.4	✓
30		14.8	601.2	✓
40		13.1	02.9	✓
50		12.1	03.9	✓
60		10.7	05.3	✓
70		9.6	06.4	✓
80		9.3	06.7	✓
90		6.8	09.2	✓
4200		1.9	14.1	✓
05		+0.4	16.4	✓
10		+0.4	16.4	✓
20		0.4	15.6	✓
30		0.2	15.8	✓
40		+0.3	16.3	✓
44		+0.7	16.7	✓
45		+4.6	20.6	✓
50	634.48	9.8	624.7	✓
60		6.5	28.0	✓
70		5.7	29.3	✓
80		5.1	29.4	✓

		634.48	E.4470		
N.4280			4.9	629.6	✓
70			5.0	29.5	✓
60			5.2	29.3	✓
52			5.2	29.3	✓
34		615.98	0.6	615.4	✓
4200			0.5	15.5	✓
4180			8.4	07.6	✓
60			11.2	04.8	✓
40			13.5	02.5	✓
20			15.8	600.2	✓
4100			17.6	598.4	✓
4080			19.7	96.3	✓
60			20.9	95.1	✓
			E.4480		
4060			20.2	595.8	✓
80			19.2	96.8	✓
4100			17.6	98.4	✓
20			15.5	600.5	✓
40			13.6	02.4	✓
65			10.7	05.3	✓
87			1.9	14.1	✓
4200			1.1	14.9	✓
20			0.8	15.2	✓
28			0.7	15.3	✓
30			+1.8	17.8	✓

		634.48	E.4480		
N.4242			6.0	628.5	✓
47			5.1	29.4	✓
60			5.0	29.5	✓
80			4.7	29.8	✓
4300			5.0	29.5	✓
			E.4490		
N.4300			4.8	629.7	✓
4280			4.6	29.9	✓
60			4.6	29.9	✓
40			4.9	29.6	✓
		615.98			
22			1.1	614.9	✓
4200			1.2	614.8	✓
4180			1.5	614.5	✓
43			13.7	02.3	✓
20			15.5	600.5	✓
4100			17.2	598.8	✓
4080			18.8	97.2	✓
60			19.8	96.2	✓
			E.4500		
N.4060			19.7	596.3	✓
80			18.5	97.5	✓
4100			17.0	99.0	✓
20			14.3	601.7	✓
40			8.9	07.1	✓
60			1.3	14.7	✓

		615.98	E. 4500		
N. 4170			1.8	614.2	✓
80			1.7	14.3	✓
4200			1.3	14.7	✓
15			1.2	14.8	✓
32		624.48	9.7	624.8	✓
33			4.8	29.7	✓
40			4.7	29.8	✓
60			4.3	30.2	✓
80			4.7	29.8	✓
90			4.4	30.1	✓
4300			7.2	27.3	✓
			E. 4510		
N. 4300			3.9	630.6	✓
4280			4.6	29.9	✓
60			4.1	30.4	✓
40			4.2	30.3	✓
23			4.7	29.8	✓
21			10.8	23.7	✓
05		615.98	1.1	14.9	✓
4180			1.5	14.5	✓
60			1.7	14.3	✓
50			1.4	14.6	✓
40			3.3	12.7	✓
20			9.4	06.6	✓
4100			13.7	02.3	✓
4090			17.1	598.9	✓

		615.98	E. 4510		
N. 4060			19.5	596.5	✓
			E. 4520		
N. 4090			10.9	605.1	✓
4120			4.9	11.1	✓
30			0.7	15.3	✓
40			1.4	14.6	✓
60			1.3	14.7	✓
80			1.4	14.6	✓
92			0.9	15.1	✓
4215		624.48	8.4	26.1	✓
16			4.4	30.1	✓
20			4.2	30.3	✓
40			3.8	30.7	✓
60			3.9	30.6	✓
80			4.7	29.8	✓
4300			1.5	33.0	✓
			E. 4530		
N. 4310			+4.0	638.5	✓
05			+3.2	37.7	✓
4294			3.2	31.3	✓
90			4.4	30.1	✓
80			4.3	30.2	✓
60			4.1	30.4	✓
40			3.7	30.8	✓
20			3.6	30.9	✓
07			4.1	30.4	✓

		634.48	E.4530		
N.4207			7.4	627.1	✓
4190		615.98	+3.2	19.2	✓
75			1.2	14.8	✓
60			1.1	14.9	✓
40			0.9	15.1	✓
20			1.0	15.0	✓
T.P.	5.14	620.71	0.41	615.57	
05			6.0	14.7	✓
4080			12.0	08.7	✓
			E.4540		
N.4080			5.1	15.6	✓
4100			5.5	15.2	✓
20			5.4	15.3	✓
40			5.5	15.2	✓
60			5.7	15.0	✓
80			+1.0	21.7	✓
93		634.48	8.0	26.5	✓
95			3.9	30.6	✓
4200			3.7	30.8	✓
20			3.2	31.3	✓
40			3.6	30.9	✓
60			3.7	30.8	✓
80			4.0	30.5	✓
92			3.9	30.6	✓
4300			0.4	34.1	✓
05			+5.5	40.0	✓

		634.48	E.4550		
N.4307			+7.2	641.7	✓
4300			+1.2	35.7	✓
4294			3.1	31.4	✓
80			3.7	30.8	✓
60			3.0	31.5	✓
40			3.6	30.9	✓
20			3.0	31.5	✓
4200			2.6	31.9	✓
4180			2.9	31.6	✓
77			6.8	27.7	✓
30		620.71	5.3	16.4	✓
4100			5.1	15.6	✓
4080			5.1	15.6	✓
			E.4560		
N.4080			4.9	15.8	✓
4100			5.0	15.7	✓
20			4.6	16.1	✓
40		634.48	12.1	22.4	✓
60			7.5	27.0	✓
60			2.1	32.4	✓
80			2.2	32.3	✓
4200			2.3	32.2	✓
20			3.2	31.3	✓
40			3.1	31.4	✓
60			2.9	31.6	✓
80			3.4	31.1	✓

		634.48	E 4560		
N. 4296			3.3	631.2	✓
4309			+9.4	43.9	✓
			E 4570		
4312			+12.2	46.7	✓
07			+1.8	36.3	✓
4300			2.9	31.6	✓
4280			3.3	31.2	✓
60			2.6	31.9	✓
40			3.1	31.4	✓
20			3.0	31.5	✓
4200			2.2	32.3	✓
4180			1.7	32.8	✓
60			1.5	33.0	✓
40			1.4	33.1	✓
36			7.1	27.4	✓
20			12.5	22.0	✓
4100		620.71	1.9	18.8	✓
4080			3.7	17.0	✓
			E 4580		
N. 4080			11.3	609.4	✓
4100			8.7	12.0	✓
17			5.6	15.1	✓
22			0.5	20.2	✓
40			0.5	20.2	✓
60			0.9	19.8	✓
80			1.3	19.4	✓

		620.71	E 4580		
N. 4200			1.9	618.8	✓
20			2.6	18.1	✓
40			3.0	17.7	✓
60			2.7	18.0	✓
80			3.3	17.4	✓
B.M.	7.51	640.15		632.64	
	12.90	652.11	0.94	639.21	
4300		640.15	8.9	31.3	✓
11			3.8	36.4	✓
18		652.11	2.9	49.2	✓
			E 4590		
N. 4321			1.0	51.1	✓
16		640.15	3.2	37.0	✓
06			8.8	31.4	✓
4300			9.0	31.2	✓
4280			8.7	31.5	✓
60			8.6	31.6	✓
40			8.4	31.8	✓
20			8.2	32.0	✓
4200			7.5	32.7	✓
4180			6.3	33.9	✓
60			6.1	34.1	✓
40			5.8	34.4	✓
20			5.5	34.7	✓
4100			4.9	35.3	✓

E.4600

N.4100	640.15	4.6	635.6	✓
20		4.9	35.3	✓
40		5.2	35.0	✓
60		5.7	34.5	✓
80		6.3	33.9	✓
4200		7.1	33.1	✓
20		7.5	32.7	✓
40		7.9	32.3	✓
60		8.4	31.8	✓
80		8.7	31.5	✓
4300		9.1	31.1	✓
10		8.7	31.5	✓
19		2.9	37.3	✓
25	652.11	+0.7	52.8	✓

E.4610

N.4326		+4.3	56.4	✓
21		1.9	50.2	✓
19		10.5	41.6	✓
4300	640.15	8.2	32.0	✓
4280		8.4	31.8	✓
60		8.4	31.8	✓
40		7.5	32.7	✓
20		7.0	33.2	✓
4200		6.9	33.3	✓
4180		6.0	34.2	✓

N.4160	640.15	5.4	634.8	✓
40		5.0	35.2	✓
20		4.5	35.7	✓
4100		4.1	36.1	✓

E.4620

N.4100		3.4	36.8	✓
20		3.6	36.6	✓
40		4.5	35.7	✓
60		5.0	35.2	✓
80		5.9	34.3	✓
4200		6.6	33.6	✓
20		6.7	33.5	✓
40		7.7	32.5	✓
60		8.6	31.6	✓
80		8.7	31.5	✓
95		8.5	31.7	✓
4313		0.1	40.1	✓
17		+7.7	47.9	✓
26	652.11	+3.8	55.4	✓
40		+2.6	54.7	✓

E.4630

N.4338		+2.3	54.4	✓
20		+2.5	54.6	✓
13		6.1	46.0	✓
4300		11.9	40.2	✓

			E.4630		
N.4280		640.15	7.0	633.2	✓
70			8.8	31.4	✓
60			9.1	31.1	✓
40			8.4	31.8	✓
20			7.0	33.2	✓
4200			6.5	33.7	✓
4180			6.2	34.0	✓
60			5.1	35.1	✓
40			4.2	36.0	✓
30			3.6	36.6	✓
21		652.11	8.3	43.8	✓
			E.4640		
N.4123			3.1	649.0	✓
30		640.15	1.3	38.9	✓
40			3.4	36.8	✓
60			5.4	34.8	✓
80			6.3	33.9	✓
4200			6.9	33.3	✓
20			7.6	32.6	✓
40			8.1	32.1	✓
60			5.3	34.9	✓
80			0.2	40.0	✓
4300		652.11	4.8	47.3	✓
10			1.0	51.1	✓
	12.83	664.44	0.50	651.61	

		664.44	E.4640		
N.4315			9.9	654.5	✓
35			10.2	54.2	✓
39			+1.1	65.5	✓
50			0.0	64.4	✓
			E.4650		
N.4360			+2.1	66.5	✓
35			+2.4	66.8	✓
29			9.6	54.8	✓
10			9.5	54.9	✓
4294			8.0	56.4	✓
80		652.11	3.1	49.0	✓
60			10.0	42.1	✓
40			15.6	36.5 ~~37.5~~	✓
20			18.5	33.6	✓
4200			18.1	34.0	✓
4180			18.1	34.0	✓
60			16.2	35.9	✓
40			11.4	40.7	✓
32			11.8	40.3	✓
26			0.0	52.1	✓
			E.4660		
N.4178			+6.5	658.6	✓
34			5.7	46.4	✓
40			5.1	47.0	✓
60			11.1	41.0	✓

			E.4660		
N.4170		652.11	13.2	638.9	✓
80			12.3	639.8	✓
90			11.5	40.6	✓
A200			12.8	39.3	✓
20			12.6	39.5	✓
30			11.4	40.7	✓
75		664.44	9.6	54.8	✓
80			5.5	58.9	✓
A300			8.1	56.3	✓
15			8.6	55.8	✓
	9.14	673.41	0.17	664.27	
24			14.5	58.9	✓
29			4.8	68.6	✓
50			5.2	68.2	✓
70			7.0	66.4	✓
			E.4670		
N.4360			4.0	69.4	✓
40			3.7	69.7	✓
17			2.5	70.9	✓
A292		664.44	6.6	57.8	✓
80			6.1	58.3	✓
64			3.8	60.6	✓
52			7.4	57.0	✓
30			9.9	54.5	✓
17			12.9	51.5	✓

N.4210		664.44	19.3	645.1	✓
A200			19.4	45.0	✓
A190			16.2	48.2	✓
70			20.2	44.2	✓
60			16.5	47.9	✓
38			9.8	54.6	✓
35			0.5	63.9	✓
			May 31. 1933		
			Same Party as May 29.		
	3.98	668.25		664.27	
T.P.	12.52	680.56	0.21	668.04	
			E.4680		
N.4130			11.8	668.8	
40		668.25	2.0	66.2	✓
48			11.8	56.4	✓
60			12.8	55.4	✓
70			16.9	51.3	✓
80			16.5	51.7	✓
90			9.7	58.5	✓
A210			8.8	59.4	✓
30			2.6	65.6	✓
50			5.8	62.4	✓
73			11.8	56.4	✓
80		680.56	8.4	72.2	✓
90			5.3	75.3	✓

		680.56		E 4680	
N. 4300			6.9	673.7	✓
20			9.0	671.6	✓
40			9.1	71.5	✓
60			10.6	70.0	✓
70			7.2	73.4	✓
75			+4.6	85.2	✓
			E 4690		
N. 4375			+5.4	86.0	✓
70			6.6	74.0	✓
60			10.1	70.5	✓
40			7.8	72.8	✓
20			7.6	73.0	✓
4300			6.4	74.2	✓
4280			3.7	76.9	✓
	12.42	692.46	0.52	680.04	
65		680.56	1.4	79.2	✓
60			2.7	77.9	✓
50			16.3	64.3	✓
40			16.4	64.2	✓
20			13.6	67.0	✓
4200			11.9	68.7	✓
4190			11.2	69.4	✓
80			8.2	72.4	✓
60			14.5	66.1	✓
50			8.5	72.1	✓

			680.56	E 4690	
N. 4140				4.8	675.8	✓
30				2.1	78.5	✓
				E 4700	
4130			692.46	6.1	86.4	✓
40				8.5	84.0	✓
50				12.0	80.5	✓
60				16.3	76.2	✓
70				13.3	79.2	✓
80			680.56	4.7	75.9	✓
4200				8.9	71.7	✓
20				11.2	69.4	✓
30				11.0	69.6	✓
40				+2.4	83.0	✓
60				3.1	77.5	✓
80				3.7	76.9	✓
4300				5.5	75.1	✓
20				6.1	74.5	✓
40				7.4	73.2	✓
60				7.2	73.4	✓
65				3.8	76.8	✓
70				+7.0	87.6	✓
				E 4710	
N. 4375				+11.1	91.7	✓
70				3.4	77.2	✓

		E 4710		
N. 4360	680.56	7.1	673.5	✓
40		7.5	73.1	✓
20		4.9	75.7	✓
4300		4.4	76.2	✓
4280		2.9	77.7	✓
60		0.9	79.7	✓
40	692.46	10.1	82.4	✓
20		6.7	85.8	✓
4210		5.5	87.0	✓
4198		14.5	78.0	✓
90		10.7	82.3	✓
80		8.7	84.3	✓
70		4.4	88.1	✓
60		5.5	87.0	✓
50		4.5	88.0	✓
40		+0.5	93.0	✓
30		+3.0	95.5	✓
		E. 4720		
N. 4130		+3.8	696.3	✓
40		+5.7	97.7	✓
60		+3.6	96.1	✓
80		0.1	92.4	✓
4200		3.8	88.7	✓
20		7.0	85.5	✓
40		9.7	82.8	✓

		E 4720		
N. 4260	692.46	12.1	680.4	
80	680.56	2.1	78.5	✓
4300		3.2	77.4	✓
20		5.8	74.8	✓
40		6.7	73.9	✓
60		5.9	74.7	✓
74		0.0	80.6	✓
76		+12.2	92.8	✓
		E 4730		
N. 4370		+10.7	691.3	✓
67		1.5	79.1	✓
60		1.9	78.7	✓
50		6.2	74.4	✓
40		6.1	74.5	✓
20		4.9	75.7	✓
4300		4.2	76.4	✓
4280		1.4	79.2	✓
60	692.46	12.0	80.5	✓
40		9.7	82.8	✓
20		7.0	85.5	✓
4200		3.9	88.6 ~~88.7~~	✓
4180		0.5	92.0	✓
60		+3.0	95.5	✓
40		+5.5	98.0	✓
20		+3.2	95.7	✓

			E.4740		
N.4120		692.46	+5.2	697.7	✓
40			+5.7	98.2	✓
60			+2.4	94.9	✓
80			1.2	91.3	✓
4200			4.5	88.0	✓
20			7.0	85.5	✓
40			9.8	82.7	✓
50			10.7	81.8	✓
60			8.1	84.4	✓
70			7.1	85.4	✓
80			10.2	82.3	✓
4300			14.5	78.0	✓
20		680.56	2.1	79.5	✓
40			2.9	77.7	✓
55			+0.9	81.5	✓
63		692.46	+5.1	97.6	✓
			E.4750		
N.4350			+10.0	702.5	✓
40			8.5	684.0	✓
70			9.4	83.1	✓
4300			10.6	81.9	✓
4280			6.1	86.4	✓
60			2.3	90.2	✓
40			4.3	88.2	✓
20			1.1	91.4	✓
4200			0.2	92.3	✓

			E.4750		
N.4180		692.46	0.3	692.2	
	12.87	705.07	0.26	692.20	
	12.69	717.62	0.14	704.93	
60		705.07	9.3	695.8	✓
40			6.1	99.0	✓
20			5.8	99.3	✓
			E.4760		
N.4130			4.2	700.9	✓
40			5.0	700.1	✓
60			6.9	698.2	✓
80			5.0	700.1	✓
4200		717.62	11.9	05.7	✓
20			10.3	07.3	✓
40			8.6	09.0	✓
60			7.8	09.8	✓
Check			7.16	710.46	710.40
N.4280		717.56	6.5	11.1	
4300			5.8	11.8	
20			12.5	05.1	
40			10.8	06.8	
T.P.	12.89	730.25	0.20	717.36	
60		717.56	3.7	13.9	
80			3.8	13.8	
4400		730.25	14.1	16.1	
20			6.1	24.1	

E.4770

N.4420	730.25	4.9	725.3
4400		6.6	23.6
4380		8.7	21.5
60		11.1	19.1
40		13.6	16.6
20	717.56	3.2	14.4
4300		4.5	13.1
4280		6.6	11.0
60		7.9	709.7
40		8.9	08.7
20		10.5	07.1
4200		12.5	05.1
4180		15.6	02.0
60		17.1	700.5
40		16.1	701.5
30		15.4	702.2

E.4780

N.4130	717.56	15.1	702.5
40		14.6	03.0
60		14.9	02.7
80		13.5	04.1
4200		11.6	06.0
20		10.1	07.5
40		8.8	08.8
60		7.6	10.0

N.4280	717.56	6.3	711.3
4300		4.6	13.0
20		3.0	14.6
40		0.9	16.7
60	730.25	11.4	18.8
80		8.3	21.9
4400		6.2	24.0
20		4.1	26.1

E.4790

N.4420		3.2	727.0
4400		4.9	25.3
4380		7.6	22.6
60		10.6	19.6
40		13.2	17.0
20	717.56	2.6	15.0
4300		4.5	13.1
4280		6.0	11.6
60		7.2	10.4
40		8.4	09.2
20		9.5	08.1
4200		10.6	07.0
4180		12.0	05.6
60		13.0	04.6
45		13.4	04.2
30		4.6	13.0

E. 4800

N. 4138	717.56	+2.1	719.7
60		11.8	05.8
80		11.0	06.6
4200		9.8	07.8
20		9.0	08.6
40		8.0	09.6
60		7.0	10.6
80		5.7	11.9
4300		4.0	13.6
20		2.3	15.3
40		0.3	17.3
60	730.25	10.5	19.7
80		7.4	22.8
4400		4.2	26.0
20		2.2	28.0
30		2.0	28.2
37		+7.5	37.7

E. 4810

N. 4436		+9.2	739.4
31		7.1	29.1
20		1.1	29.1
4400		5.9	26.3
4380		7.3	22.9
60		10.1	20.1
40		12.5	17.7

E. 4810

N. 4320	717.56	1.5	716.1
4300		3.5	14.1
4280		5.9	11.7
60		6.9	10.7
40		7.6	10.0
20		4.9	12.7
4200		+0.3	17.9
4180		0.7	16.9
60	730.25	11.5	18.7
50		6.9	23.3
45		6.6	23.6
40		2.4	27.8

E. 4820

N. 4147		+0.8	731.0
60		0.5	29.7
80		4.2	26.0
90		1.3	28.9
4200		3.8	26.4
10		1.3	28.9
20		4.9	25.3
40	717.56	2.9	14.7
50		0.5	17.1
70		4.9	12.7
80		4.7	12.9
4300		2.8	14.8
20		0.9	16.7

E.4820

N. 4340		730.25	12.2	718.0
60			9.8	20.4
80			6.8	23.4
4400			3.6	26.6
20			0.6	29.6
T.P.	13.18	743.41	0.02	730.23
33			13.6	29.8
40			+1.8	45.2

E.4830

N.4445			+7.8	751.2
37			12.9	30.5
20			12.7	30.7
4400		730.25	2.5	27.7
4380			5.6	24.6
60			8.9	21.3
40			11.8	18.4
20			13.5	16.7
4300			13.9	16.3
4280			11.7	18.5
70			11.2	19.0
40			1.7	28.5
30			0.0	30.2
4205		743.41	4.7	38.7
4190			2.6	40.8
80			8.0	35.4
60			2.9	40.5

E.4830

N.4150		743.41	4.3	739.1

E.4840

N.4146				762.0
4158			+4.7	748.1
68			+11.6	755.0
80			+5.9	49.3
4190			+7.1	56.5
4215			+5.9	49.3
30			5.3	38.1
40			7.8	35.6
60			12.9	30.5
80		730.25	4.2	26.0
4300			7.4	22.8
20			11.4	18.8
40			8.9	21.3
60			6.1	24.1
80			2.5	27.7
4400			1.1	29.1
20		743.41	11.6	31.8
30			13.3	30.1
40			12.1	31.3
51			+14.7	58.1
T.P.			7.17	736.24
	7.54	743.78	0.26	743.52
	12.24	755.76		

June 1, 1933.
Same Party as May 31.

E. 4850

	743.78		
N. 4457			766.0
N. 4444		12.2	731.6
30		13.3	30.5
20		10.8	33.0
4400		13.1	30.7
4390		13.1	30.7
80		9.8	34.0
60		11.4	32.4
40		16.4	27.4
20		17.7	26.1
4300		13.6	30.2
4290		8.7	35.1
80		9.4	34.4
70		4.9	38.9
60		5.4	38.4
40	755.76	13.0	42.8
20		+0.2	56.0
10		+1.8	57.6
4200		+0.7	56.5
4180		+4.6	60.4
65		+12.1	67.9
55		+6.8	62.6
40		+15.9	71.7
20		+16.8	72.6
4105		+18.1	73.9

E. 4860

N. 4105	755.76	+18.0	773.8
20		+16.7	72.5
40		+16.3	72.1
60		+16.5	72.3
80		+13.2	69.0
4200		+9.4	65.2
20		+6.3	62.1
30		+4.6	60.4
50		6.8	49.0
65		6.0	49.8
80		11.8	44.0
4300	743.78	5.5	38.3
20		8.6	35.2
40		8.4	35.4
60		7.3	36.5
80		10.2	33.6
4400		11.1	32.7
20		10.3	33.5
30		12.3	31.5
40		12.4	31.4
45		8.4	35.4
4461			769.8

E 4870

N. 4465			772.9
55		+9.1	752.9
50		6.4	37.4

E 4870

N. 4440		743.78	12.3	731.5
30			12.2	31.6
20			9.7	34.1
4400			9.2	34.6
80			9.1	34.7
60			6.8	37.0
40			4.1	39.7
4320			0.6	43.2
4300		755.76	9.0	46.8
4280			5.7	50.1
60			2.2	53.6
T.P.	12.65	768.21	0.20	755.56
40			11.1	57.1
20			6.8	61.4
4200			2.9	65.3
4180			+0.8	69.0
60			+4.0	72.2
40			+5.9	74.1
20			+4.4	72.6
4100			+6.1	74.3

E 4880

N. 4100			+5.8	74.0
20			+5.1	73.3
30			+6.8	75.0
40			+6.0	74.2

E 4880

N. 4160		768.21	+3.2	771.4
80			+0.1	68.3
4200			3.5	64.7
20			6.7	61.5
40			10.9	57.3
60			14.7	53.5
80			18.6	49.6
4300		743.78	+2.7	46.5
20			0.4	43.4
40			3.4	40.4
60			5.8	38.0
80			7.3	36.5
4400			8.1	35.7
10			9.2	34.6
20			11.8	32.0
30			9.3	34.5
40			5.7	38.1
51			2.4	41.4
55			+10.5	54.3
4468				774.0

E 4890

N. 4476				780.2
52		743.78	+9.2	53.0
5.0			+3.8	47.6
40			0.1	43.7

			E. 4890	
N. 4420		743.78	10.3	33.5
10			9.9	33.9
4400			7.4	36.4
4380			6.6	37.2
60			4.7	39.1
40			2.6	41.2
20			+0.2	44.0
4300			+3.1	46.9
280			+6.0	49.8
60			+9.5	53.3
		768.21		
40			11.3	56.9
20			6.7	61.5
4200			3.4	64.8
4180			+0.8	69.0
60			+3.4	71.6
40			+5.8	74.0
20			+7.4	75.6
10			+5.8	74.0
100			+5.6	73.8
			E 4900	
4100			+8.5	76.7
10			+5.5	73.7
20			+7.8	76.0
40			+6.1	74.3

		768.21	E 4900	
4160			+4.3	772.5
80			+5.7	73.9
200			+10.2	78.4
10			+10.6	78.8
		743.78		
T.P.	12.12	755.89	0.01	743.77
		768.21		
20			+15.7	83.9
60			0.6	67.6
		755.89		
80			1.4	54.5
4300			4.7	51.2
20			10.9	45.0
40			11.7	44.2
60			14.0	41.9
80			16.2	39.7
4400			16.5	39.4
20			14.6	41.3
52			0.9	55.0
4481				786.5
			E. 4910	
N. 4488		768.21		697.4
4462			3.7	64.5
45			9.3	58.9
38			13.5	54.7

EA910

N. 4430		768.21	11.8	756.4
05		755.89	8.9	47.0
4380			10.1	45.8
60			6.6	49.3
40			4.3	51.6
20			4.3	51.6
10			2.2	53.7
		768.21		
T.P	10.25	778.27	0.19	768.02
4280			3.2	75.1
60			+3.8	82.1
50			+3.6	81.9
20			+16.3	94.6
10			+7.8	86.1
4200			+6.9	85.2
4180			+1.6	79.9
60			3.5	74.8
40			2.9	75.4
20			2.0	76.3
10			3.4	74.9
4100			0.5	77.8

		778.27		
4110			1.4	76.9
20			2.0	76.3
40			1.4	76.9
60			0.8	77.5
80			+2.3	80.6
4200			+6.4	84.7
10			+12.2	90.5
20			+19.6	97.9
30			+19.2	97.5
45			+11.2	89.5
70			+12.8	91.1
83			0.0	78.3
		768.21		
4315			5.3	62.9
		778.27		
60			7.8	
70			4.8	
T.P	1.84	778.87	1.24	777.03
	12.12	791.23	0.24	779.11 → 778.63
95		778.87	23.8	55.1
4415			15.5	63.4
35			13.7	65.2
45			9.3	769.6
94				807.3

CORRECT FOR MISTAKE

June 2. 1933.
Converse - Notes, Loudon } Chain
Simpson - Inst. Newcomb }
Soper - Chain

E. 4938

44 84			809.3	
N. 44 73		791.23	+5.0	796.2
44 00		778.87	14.8	64.1
43 90			4.2	74.7
75			5.6	73.3
65		791.23	7.3	83.9
50			16.3	74.9
10			19.2	72.0
43 00			16.8	74.4
	11.81	802.62	0.42	790.81
42 70			5.8	96.8
55			4.0	98.6
45			6.3	96.3
25			6.5	96.1
42 00		791.23	5.5	85.7
41 80			9.2	82.0
60			11.9	79.3
40			12.9	78.3
20			14.8	76.4

E 4940

N. 41 30		14.1	77.1
40		13.6	77.6
60		10.6	80.6
80		8.1	83.1
42 00		4.5	86.7

Correct for mistake of 0.5'

E 4940

N. 42 20	802.62	12.3	790.3
40		8.6	94.0
60		6.9	95.7
80		5.1	97.5
43 20	791.23	11.5	79.7
60		5.4	85.8
70		+1.8	93.0
85		7.3	83.9
44 35		2.8	88.4
55	802.62	5.0	797.6
75		+1.2	803.8
88		+24.3	15.5
	12.12	814.35 0.39	802.23

E 4950

N. 44 85		+4.4	818.8
N. 44 75		3.2	811.2
55		7.8	806.6
44 40	802.62	5.0	797.6
43 90		9.2	93.4
70		1.3	801.3
50		10.8	791.8
20		15.5	87.1
43 10		3.3	799.3
42 80		5.5	97.1
60		6.9	95.7
40		8.9	93.7
20		11.7	90.9

Correct for mistake of 0.5'

			E.4950		
N.4200		802.62	15.1	787.5	
4180			18.2	84.4	
60			23.1	79.5	
4140			25.1	77.5	
			E.4960		
N.4150			22.8	779.8	
60			23.0	79.6	
80			12.6	90.0	
90			5.3	97.3	
4200			7.5	95.1	
10			12.0	90.0	
20			10.9	91.7	
40			8.4	94.2	
60			6.5	97.1	
80			5.3	97.3	
4300			3.6	99.0	
20			2.8	799.8	
40			1.4	801.2	
60		814.35	11.2	803.0	
80			6.7	07.7	
4400			9.2	05.2	
20			7.2	07.2	
40			4.4	10.0	
60			+2.3	16.7	
70			+5.8	20.2	
			3.7	800.7	

Correct for mistake of 0.05

B.M.	12.40	771.41		759.01
	13.02	784.08	0.35	771.06
	11.44	794.86	0.66	783.42
			0.64	794.22
Check.		802.12 ~~802.62~~	7.92	794.20 ~~794.70~~
	12.74	806.96		794.22
N.4460				
40				
20				
4400				
4380				
60				
40				
20				
4300				
4280				
60				
40				
30				
4220				
4230				
40				
60				

On Axis.

E.4970

	N.6.
+7.6	809.6
0.7	06.3
3.7	03.3
3.9	03.1
5.6	01.4
6.8	800.2
7.5	799.5
8.3	98.7
9.6	97.4
11.7	95.3
12.9	94.1
13.4	93.6
11.5	95.5

E.4980

12.0	
12.9	
12.5	

		E.4980	
N.4280	806.96	9.5	797.5
4300		8.2	98.8
20		7.3	799.7
40		6.9	800.1
60		5.7	01.3
80		4.7	02.3
4400		3.2	03.8
20		1.1	05.9
40		+2.0	09.0
60		+13.0	19.0
			N.6.
		E4990	
4460		+14.1	21.1
20		0.6	06.4
4400		2.9	04.1
4380		4.8	02.2
60		5.7	01.3
40		6.6	800.4
20		7.2	799.8
4300		8.0	99.0
4280		9.2	97.8
70		9.5	97.5
60		13.5	93.5
40		13.4	93.6
30		12.9	94.1

N.4220			
N.4230			
40			
60			
70			
80			
4300			
20			
40			
60			
80			
4410			
62			
N.4466			
4410			
4380			
60			
40			
20			
4300			

806.96	E4990		
	11.0	796.0	
	E5000		
	13.3	793.7	
	12.2	92.8	
	12.7	92.3	
	12.8	92.2	
	9.3	97.7	
	8.2	98.8	
	7.3	99.7	
	6.6	800.4	
	5.7	01.3	
	4.4	02.6	
	2.0	05.0	
	+20.0	27.0	
		N.6.	
	E.5010		
		N.6.	
	+26.5	833.5	
	1.9	05.1	
	4.2	02.8	
	5.7	01.3	
	6.7	00.3	
	7.4	799.6	
	8.2	98.8	

	806.96	E.5010	
N.4290		8.7	798.3
80		15.2	91.8
60	794.86	3.2	91.7
40		2.9	92.0
30		4.0	90.9
		E.5020	
N.4230		5.9	89.0
40		3.2	91.7
60		4.1	90.8
80		4.6	90.3
90	806.96	7.8	99.2
4300		7.8	99.2
20		7.1	99.9
40		6.6	800.4
60		5.3	01.7
80		3.7	03.3
4410		1.8	05.2
			N.6.
		E.5030	
N.			N.6
4390		2.7	04.3
80		3.7	03.3
60		5.3	01.7
40		6.2	00.8
20		6.6	00.4

		806.96	E.5030
N.4300			6.4 800.6
4285		794.86	6.2
4260			5.2
40			4.0
			E.5040
N.4250			5.0
60			5.5
80			6.4
90			6.7
4310		806.96	6.1 800.9
20			6.1 00.9
40			6.1
60			5.2
80			3.7
90			2.8
			N.6.
			E.5050
N.			N.6.
4385			2.8
80			3.7
60			4.9
40			6.1
30			6.0
20			4.2
4300		794.86	7.6

		E.5050	
N.4280	794.86	7.2	787.7
70		7.0	87.9
60		6.1	88.8
		E5060	
N.4270		7.2	87.6
80		7.9	87.0
4305		8.5	786.4
75	806.96	5.1	801.9
40		5.3	01.7
60		4.5	02.5
80		3.7	03.8
			N.6.
		E.5070	
			N.6.
4380		3.0	
60		4.0	
40		5.0	
30		4.3	
10	794.86	9.0	
4290		9.0	
70		8.3	
		E.5080	
4280		8.8	
4300		10.0	
15		10.0	

N.4335		E.5080	
60	806.96	4.1	07.9
80		3.4	03.6
4420		1.8	05.2
45		+21.5	28.5
		+33.0	40.0
			N.6.
		E.5090	
			N.6.
4420		+23.8	829.8
4380		1.4	05.6
60		3.0	04.0
40		3.9	03.1
33		5.5	01.5
20	794.86	10.6	84.3
4300		10.7	
4290		10.3	
		E.5100	
N.4290		11.5	
4300		11.8	
70		11.5	
50	806.96	7.4	
60		7.5	
80		1.5	
4420		+22.8	
			N.6.

E. 5110

806.96

N. N. 6.

4415 +14.0

4385 0.8

60 7.3

55 1.2

25 794.86 12.5

4300 12.9

4290 12.2

E. 5120

4290 14.4

4300 14.0

26 13.5

58 806.96 1.2

80 0.6

95 +0.3

4420 +12.5

N. 6.

E. 5130

N. 6.

4420 +12.5

4400 +1.0

4380 +0.2

67 0.1

28 794.86 14.3

794.86 E 5130

N. 4310 14.9

4295 14.9

1.46 784.88 783.42

E. 5140

N. 4300 6.0

30 5.5

74 806.96 +1.2

80 +0.8

4400 +1.6

28 +17.0

N. 6.

E. 5150

N. 6.

N. 4428 +21.6

4395 +1.4

74 +1.0

32 784.88 5.7

20 6.9

4300 7.1

Xsections of Spillway

Est. No. 15

Aug. 3, 1933

B.M.	13.21	771.55 ✓		758.34
			1.00	770.55 ✓
	12.13	782.68 ✓		

E 4900 ✓

N 4090	5.2	77.5
4100	8.0	74.7
4140	8.9	73.8
4190	10.1	72.6
4230	6.8	75.9
40	3.4	79.3

North same as last Xsections

E 4920 ✓

North same as last Xsections

N 4270	+1.0	83.7
4260	3.6	79.1
4200	7.7	75.0
4160	9.1	73.6
4130	8.6	74.1
4110	5.2	77.5

E 4940 ✓

4120	5.7	77.0
4130	8.4	74.3
4170	8.7	74.0
4210	7.4	75.3
4250	2.9	79.8
80	1.8	80.9
4290	+5.0	87.7

North same as last Xsections

Plotted Aug. 4, F.O. + R.E.L.

43 ✓

782.68

E 4960 ✓

4135	7.6	75.1
50	9.4	73.3
4230	8.0	74.7
4255	+3.0	85.7
4285	+4.6	87.3

813.1

4300	13.3	99.8
4360	11.6	01.5

North same as last Xsections

Set B.M. 4.53 784.50 ✓ 2.71 779.97 ✓

E 5000 ✓

N 4190	4.8	79.7
4200	6.8	77.7
4350	1.6	72.9

813.1

4350 Too	10.6	02.5
70	11.3	01.8
4420	6.2	06.9
4505	+2.3	15.4

Run to neat line at top of slope

E 5040

Run to neat line at top of slope

4495	+0.9	14.0
4440	2.4	10.7
4370	9.9	03.2

E5040

	11.60	791.57		779.97
4360			5.1	86.5
4320			8.8	82.8
4280			9.9	81.7
4260			10.8	80.8
4200			20.0	71.6 O.G. +-

E5080

		813.1		
	Run to neat line at top of slope			
4480			1.0	12.1
4400			5.8	07.3
		791.6		
4385			5.3	86.3
4360			7.5	84.1
4315			6.8	84.8
B.M.	12.31	749.16		736.85
			0.20	748.96
	9.31	758.27		
4300			1.8	56.5
4250			6.6	51.7
4240			11.9	46.4
Intersect O.G.				
4180			12.7	45.6

or 1 to 1 slope to O.G. from 4180 for deduction

758.3

E5120

4225			11.5	46.8
Intersect O.G. or 1 to 1 to O.G. from 4225				
4300			9.9	48.4
		791.57		
4330			10.1	81.5
4360			9.8	81.8
4400			5.6	86.0
T.P.	11.19	801.60	1.16	790.41
T.P.			0.81	800.79
	12.32	813.11		
4410			3.7	09.4
4460			0.5	12.6
4475			0.7	12.4
	Run to neat line at top of cut			
T.P.	12.08	824.61	0.58	812.53

824.6 E5160 ✓

← Run to next line at toe of cut

4485	12.4	812.2
4440	13.0	11.6
4397	15.5	09.1
791.6		
4370	9.4	782.2
4350	10.4	81.2
758.3		
4325	3.9	54.4
4290	10.0	48.3

Intersect O.G or 1 to 1 slope to O.G from 4235

4235	12.0	46.3

824.6 E5200 ✓

↑ ½ to 1 slope to O.G.

4510	+25.6	850.2
4470	9.7	14.9
4430	10.5	14.1
4415	8.9	15.7
758.3		
4340	5.0	753.3
4300	8.7	49.6

Intersect O.G or 1 to 1 to O.G. from 4250

4250	10.8	47.5

824.6 E5240 ✓

↑ ½ to 1 to O.G.

4505	+18.4	843.0
4460	8.3	16.3
4440	7.5	17.1
4420	6.2	18.4
758.3		
4381	+13.1	771.4
4361	+13.1	71.4
4345	9.1	49.2

Intersect O.G or 1 to 1 to O.G. from 4260

4260	10.8	47.5

824.61 E5280 ✓

↑ ½ to 1 to O.G.

4498	+8.8	833.4
4485	0.0	24.6
4435	2.2	822.4
758.3		
4398	+10.0	768.3
4378	+10.0	768.3
4355	26.0	732.3
4310	26.0	732.3
4305	11.0	747.3

Intersect or

4275	11.6	746.7

E 5320 ✓

		824.6	
↑ ½ to 1 to O.G.			
4503			850.6
4475		+7.2	31.8
4455		+3.7	28.3
		758.27	
4409		+ 7.3	65.6
4389		+ 7.3	65.6
4359		24.1	34.2
4327		24.1	34.2
4316		11.3	47.0
Intersect or			
4300		12.8	45.5
T.P.		10.53	747.74 ✓
	3.0	750.7 ✓	

E 5360 ✓

4300	4.8	45.9
Intersect O.G or 1 to 1 slope from 4300 to O.G.		
4330	3.3	47.4
4335	14.0	36.7
4382	12.3	38.4
4395	+11.8	62.5
4430	+14.8	65.5
4500	+90.8	841.5
↓ ½ To 1 to O.G.		

E 5400 ✓

	4.5	752.2	747.7
4283		5.6	46.6
Intersect OG or 1 to 1 slope from 4283			
4343		4.6	47.6
4350		12.5	39.7
4390		10.8	41.4
4407		+8.7	60.9
4482		+61.8	814.0
↓ ½ to 1 to O.G.			

E 5440 ✓

	5.2	752.9	747.7
↑ ½ to 1 to O.G			
4469		+45.0	97.9
4420		+4.1	57.0
4395		8.2	44.7
4360		8.9	44.0
4355		4.7	48.2
Intersect or slope 1 to 1 to O.G.			
4275		6.0	46.9

E5480

	3.5	751.2		747.7
4278			7.3	43.9
Intersect O.G. or slope 1 to 1 to O.G.				
4335			2.2	49.0
4420			1.2	50.0
4453			+19.4	70.6
4458			+32.8	84.0
4461			+37.4	88.6
↓ 1/2 to 1 to O.G.				

E5500

B.M.	1.83	749.57		747.74
4277			8.0	41.6
Intersect O.G. or slope 1 to 1 to O.G. from 4277				
4340			0.8	48.8
4415			+0.8	50.4
4460			+39.6	89.2
↓ 1/2 to 1 to O.G.				

		749.57		
T.P.			11.40	738.17
	9.1	747.3		
4274			7.4	39.9
Intersect o.g. or 1 to 1 slope				
4313			3.8	43.5
	14.3	762.0		747.7
4448			+26.0	88.0
4466			+36.9	98.9
↓ 1/2 to 1 to O.G.				

E5520

E5560 is O.G.

Sept 5 - 1933

(Stadia)

X sections of Spillway Est. #16

E 5560 is O.G.

E 5520 ✓

Transit Point	H.I.	Direction	Slope Dist.	Vert. Angle	Hor. Dist.	Diff. Elev.	North.	Elev.	
N 4300 E 5520	742.1	So.	—	0.0	28	-2.5	4272	739.6	4272
#2		No.	—	0.0	15	+1.4	4315	743.5	
#3		No.	73	+23°33	61.4	+26.6	4361	768.7	
#4		No.	—	—	110	+20.6	4410	762.7	
#5								791.4	on the ½ to 1 slope then ½ to 1 to O.G.

E 5500 ✓

N 4300 E 5500	744.0					738.0			
#1		So.	—	—	20	-1.9	4280	742.1	
#2		No.	—	—	40	+4.8	4340	752.8	
#3		No.	121	+6°31′	120	+13.6 (-5½)	4420	752.2	
#4		No.	154	+8°45′	150.5	+28.0	4450.5	761.0	Then ½ to 1 to O.G.

E 5480 ✓

N 4300 E 5480	746.1					741.1			
#1		No.	154	+7°40′	150.5	+20.2	4450.5	766.3	½ to 1 to O.G.
#2		No.	—	—	130	+5.0	4430	751.1	
#3		No.	—	—	85	+2.5	4385	748.6	
#4		No.	—	—	33	+2.9	4333	749.0	
#5		So.	—	—	15	-1.8	4285	744.3	

Elliott - Notes
Simpson - π
Soper - Salgado - Ch + Rod

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Plotted Sept. 7, 1933 F.O. + R.E.L.

E5440 ✓

Transit N4300 E5440	H.I.	Direction	Sl. Dist.	Vert. ∠	Hor. Dist	Diff. Elev.	North	Elev.	
	747.7								
#1		So.	—	—	20	-0.9	4280	746.8	
#2		No.	—	—	55	+0.8	4355	748.5	
#3		No.	—	—	55	-8.0	4355	739.7	
#4		No.	—	—	70	-15.0	4370	732.7	
#5		No.	—	—	90	-15.8	4390	731.9	
#6		No.	—	—	100	-10.7	4400	737.0	
#7		No.	—	—	103	-1.1	4403	746.6	
#8		No.	—	—	143	+1.0	4443	748.7	½ to 1 to O.G.

E5400 ✓

N4300 E5400	746.9								
#1		No.	—	—	145	-1.7	4445	745.2	½ to 1 to O.G.
#2		"	—	—	93	-4.6	4393	742.3	
#3		"	—	—	88				
#4		"	—	—	75	-18.1	4375	728.8	
#5		"	—	—	22	-18.1	4322	728.8	
#6		"	—	—	21	+0.9	4321	747.8	
#7		So.	—	—	15	-0.1	4285	746.8	

E 5360 ✓

	H.I.	Direction	Sl. Dist.	Vert. L.	Hor. Dist	Diff. El.	North	Elev.	
N 4300 E 5360	746.0								
#1		—	—	—	0.0	0.0	4300	746.0	
#2		No.	—	—	27	+1.5	4327	747.5	
#3		"	—	—	30		4330	726.2	
#4		"	—	—	70		4370	727.0	
#5		"	—	—	85	-5.2	4385	740.8	
#6		"	—	—	130	-3.3	4430	742.7	
#7		"	—	—	146	+2.2	4446	748.2	½ to 1 to O.G

E 5320 ✓

N 4300 E 5320	746.1								
#1		No.	152	+3°43'		+9.7	4451	755.8	½ to 1 to O.G.
#2		"	—	—	128	-3.9	4428	742.2	
#3		"	—	—	69	-7.8	4369	738.3	
#4		"	—	—	44	—	4340	726.6	
#5		"	—	—	17	—	4317	726.6	
#6		"	—	—	15	+0.9	4315	747.0	
#7		So.	—	—	3	0.0	4297	746.1	

E5280

Transit N 4300 E 5280	H.I	Direction	Sl. Dist.	Vert. ∠	Hor. Dist.	Diff. Elev.	North.	Elev.	
	747.2								
#1		So.	—	—	22	-0.3	4278	746.9	
#2		No.	—	—	2	+0.2	4302	747.4	
#3		No.	—	—	5	—	4305	724.2	
#4		No.	50	-26°22'	41.2	-19.9	4341	727.3	
#5		No.	60	-12°04'	57.4	-12.2	4357	735.0	
#6		No.	85	-8°01'	83.4	-11.7	4383	735.5	
#7		No.	111	-3°28'	110.5	-6.7	4410	740.5	
#8		No.	176	+10°49'	170	+32.3	4470	779.5	½ to 1 to O.G.

E5240

N 4280 E 5240	5.4 747.2								
#1		No.	198	+9°51'	192.2	+33.3	4472	7705	½ to 1 to O.G.
#2		No.	167	+6°45'	164.8	+19.3	4445	766.5	
#3		No.	135	+8°27'	132.1	+19.7	4412	766.9	
#4		No.	78	-11°21'	74.8	-15.0	4355	732.2	
#5		No.	—	—	10		4290	724.4	
#6		No.	—	—	9	+0.8	4289	748.0	
#7		So.	—	—	20	-0.2	4260	747.0	

E5200

Transit. N 4260 E 5200	H.I.	Dir.	Sl. Dist.	Vert. ∠	Hor. Dist	Diff. Elev	North	Elev.	
	747.4					747.4			
#1		So.	—	—	10	-0.3	4250	747.1	
#2		No.	—	—	14	0.0	4274	747.4	
#3		No.	—	—	17	—	4277	721.9	
#4		No.	77	-16°15′	72	747.4 -20.6	4332	726.8	
#5		No.	132	+7°13′	130	+16.4	4390	763.8	
#6		No.	200	+6°32′	197.4	+22.6	4457	770.0	
#7		No.	221	+8°48′	215.8	+33.4	4476	780.8	½ to 1 to O.G.

E5150

N 4300 E 5150	5.1 751.0								
#1		So.	—	—	62	751.0 -4.5	4238	746.5	
#2		No.	—	—	0.0	0.0	4300	751.0	
#3		No.	72	+9°36′	70	751.0 +11.8	4370	762.8	
#4		No.	148	+6°36′	146	+16.9	4446	768.0	1 to 1 to intersection with ½ to 1 slope

E5120 ✓

Transit	H.I.	N. or S.	S/. Dist.	Vert. ∠	Dist.	Diff. Elev.	North	Elev.	
N 4300 E5120	5.3 751.8								
#1		S.	—	—	73	751.8 −5.3	4227	746.5	
#2		N.	—	—	0	0	4300	751.8	
#3		N.	73	+9°30′	71	+11.9	4371	763.7	
#4		N.	145	+9°15′	141	+23.0 (−3°)	4441	771.8	
#5		N.	206	+17°0′	188.5	+52.5	4488.5	804.3	½ to 1 to O.G.
			E 5080 ✓						
N4300 E5080	4.2 758.0								
#1		N.	206	+15°18′	191.5	758.0 +50.0	4491.5	808.0	½ to 1 to O.G.
#2		N.	170	+11°24′	173.4	+33.0	4473.4	791.0	
#3		N.	135	+3°57′	135	+9.3 (−1°)	4435	766.3	
#4		N.	47	+8°15	46	+6.6	4346	764.6	
#5		—	0	0	0	0.	4300	758.0	
#6		S.	—	—	23	−10.1	4277	747.9	
#7		S.	113	−5°38	112	−11.0	4188	747.0	

Sept 6 - 1933

E 5060 ✓

Transit N4300 E5060	H.I. 4.7 763.1	N. or S.	Bl. Dist.	Vert. ∠	Hor. Dist	Diff. Elev 763.1	North	Elev.	
#1		S.	122	−5°42′	120.8	−12.0	4179	751.1	
2		S.	95	−5°49′	94	−9.6 (−7.0)	4206	760.5	
3		S.	—	—	28	763.1 +0.5	4272	763.6	
4		N.	—	—	21	+1.7	4321	764.8	
5		N.	—	—	130	+3.8	4430	766.9	
6.		N.	162	+9°34′	157.5	+26.5	4457.5	787.6	
7.		N.	198	+11°35′	190	+39.0	4490	802.1	½ to 1 to O. G.

E 5020 ✓

N4300 E5020	5.2 763.9								
#1		N.	199	+10°25′	192.6	763.9 +35.1	4492.6	799.0	½ to 1 to O. G.
2.		N.	158	+10°11′	153.1	+27.4	4453	791.3	
3.		N.	—	—	118	763.9 +4.7	4418	768.6	
4.		S.	—	—	24	0.0	4276	763.9	
5.		S.	61	+15°51	56.5	+16.0	4243.5	779.9	Level south to O. G.

E 4980 ✓

Transit N4191.3 E4980	5.1 H.I.	N. or S.	Sl. Dist.	Vert. ∠	Hor. Dist.	Diff Elev. 776.9	North	Elev.	
#1		S.	—	—	36	+1.5	4155	778.4	
2		N.	—	—	11	+0.4	4202	777.3	
3		N.	32	-12°16'	30.6	-6.6 -(5°)	4222	765.3	
4		N.	146	-4°20'	145.2	-11.0	4336	765.9	
5		N.	—	—	187	-4.2	4378	772.7	
6		N.	216	+2°29'	216	+9.3	4407	786.2	
7		N.	250	+3°34'	250	+15.5	4441	792.4	
8		N.	277	+2°53'	277	+13.8 -(4°)	4468	785.7	
9		N.	305	+3°43'	305	+19.0	4496	795.9	½ to 1 to O.G.

E 4960 ✓

N4191.3 E4960	5.2 775.3					775.3			
#1		N.	307	+4°20'	305.2	+23.0	4496	798.3	½ to 1 to O.G.
2		N.	276	+3°21'	275.1	+16.0 -(3°)	4466	788.3	
3		N.	208	+3°55'	207.1	+14.2	4398	789.5	
4		N.	—	—	164	-8.3	4355	767.0	
5		N.	—	—	25	-11.3	4216	764.0	
6		N.	—	—	9	-0.5	4200	774.8	
7		0	—	—	0	0.0	4191	775.3	
8		S.	—	—	5.2	-0.2	4139	775.1	

4940 ✓

Transit N 4171.3 E 4940	H.I. 5.4 774.3	N. or S.	Slope Dist	Vert. ∠	Hor. Dist	Diff. El. 774.3	North	Elev.	
#1		S.	—	—	75	-5.0	4096	769.3	
2		N.	—	—	16	+0.5	4187	774.8	
3		N.	—	—	20	-7.8	4191	766.5	
4		N.	119	-4°27′	118.3	+9.2	4289	783.5	
5		N.	—	—	172	-7.4	4343	766.9	
6.		N.	209	+2°27′	209	+9.0	4380	783.3	
7.		N.	264	+3°18′	264	+15.1	4435	789.4	
8.		N.	322	+4°04′	320.4	+22.8	4491	797.1	½ to 1 to O.G.

E 4920 ✓

N 4151.3 E 4920	H.I. 4.9 774.2								
#1		N.	—	—	133	+0.6	4284	774.8	North same as last Est.
#2		N.	99	-5°19′	98	+9.1	4249	783.3	
3		N.	—	—	41	-7.8	4192	766.4	
4		N	—	—	28	+0.4	4179	774.6	
5		0	0	0	0	0	4151	774.2	
6		S.	—	—	15	-5.3	4136	768.9	
7		S.	—	—	67	-5.5	4084	768.7	

E 4900 Same as last Est.

X Sections on Oct 3. 1933 for monthly Est. of Spillway Excavation and spoil. Elliott, Soper, Remmen

B.M.	3.80	753.80		750.00 ✓
Set B.M.			6.90	746.90 ✓
T.P.			11.10	742.70 ✓
	1.44	744.14		✓

E5600 is O.G.

E5580 ✓

N 4290		O.G
80	7.4	736.7
60	8.8	35.3
45	9.4	34.7
40	7.0	37.1
4208	8.1	36.0
4197	16.2	27.9
4165	29.3	14.8
4090		O.G

E5560 ✓

4087		O.G.
4180	5.7	738.4
4242	5.7	38.4
38	6.3	37.8
4260	6.8	37.3

744.14

E5560 ✓

4283	6.3	737.8
90		O.G

E5520 ✓ S X

↑ on north same as last sections (p. 48)

4260	1.7	742.4
4220	3.8	40.3
4173	4.5	39.6
4024		O.G,

E5500 ✓ S X

4028		O.G.
4176	3.9	740.2
4220	3.6	40.5
4260	1.6	42.5

on north same as last sections (p. 48) ↓

E5480 ✓ S X

↑ on north same as last sections (p. 48)

4250	0.0	744.1
4248	4.2	39.9
4200	3.8	40.3
4173	13.0	31.1
4032		O.G,

		744.14	E5460 ✓ S X	
4105				O.G.
4215			5.8	38.3
4248			5.7	38.4
B.M.	4.48	751.38		746.90
4253			6.2	45.2
Back of So. Line of wier			2.9	48.5
B.M	3.50	752.75		749.25
Toe of O.G. concrete				730.7
4400			3.8	49.0
on toe of ½ to 1 slope			5.3	47.5
		744.14	E5420 ✓ S X	
4132				O.G.
4223			9.4	734.7
4245			9.7	34.4
4255		751.4	5.3	746.1
Back of wier			3.6	47.8
Toe of O.G. conc.		752.8		729.8
4398			16.8	36.0
4402			8.7	44.1
On toe of ½ to 1 slope			5.4	47.4

		744.14	E5380 ✓ S X 58	
T.P.	0.58	731.66 ✓	13.06	731.08 ✓
4140				O.G.
4217			2.8	28.9
4242			2.2	29.5
		751.4		
4259			5.6	45.8
Back of wier			4.3	47.1
Toe of O.G. Conc.		752.8		728.7
4383			19.5	33.3
4388			12.0	40.8
Toe of ½ to 1 slope			9.2	43.6
		731.66	E5340 ✓ S X	
4140				O.G
4205			9.3	22.4
4233			8.7	23.0
4256		751.4	6.5	44.9
Back of wier			4.6	46.8
		752.25		
T.P.	0.70	743.19 ✓	10.26	742.49 ✓
Toe of O.G. Conc.				727.2
4372			9.7	33.5
4383			2.7	40.5
Toe of ½ to 1 slope			0.9	742.3

		731.66	E5300	S ✓ X
T.P.	0.25	718.77	13.14	718.52 ✓
4097				O.G.
4190			3.2	15.6
4222			1.6	17.2
4246		751.4	6.0	45.4
Back of wier			5.0	46.4
Toe of O.G. Conc.		743.2		726.1
4367			6.0	37.2
4400			3.7	39.5
Toe of ½ to 1 slope			1.3	41.9

		718.77	E5260	S ✓ X
4101				O.G
4200			7.1	711.7
4158			9.7	709.1
4256		751.4	4.5	46.9
Back of wier			4.8	46.6
Toe of O.G. conc.		743.2		725.1
4345			11.1	32.1
4380			8.8	34.4
4387			3.2	40.0
Toe of ½ to 1 slope			1.4	41.8

		718.77	E5220	59 S ✓ X
T.P.	0.78	707.01	12.5 ✓	706.23 ✓
4100				O.G.
4146			2.5	04.5
4180			1.4	05.6
4235		751.4	4.2	47.2 2+16
Back of wier			3.7	47.5
Toe of O.G. conc.		743.2		723.2
4320			15.7	27.5
4365			12.2	31.0
4375			4.6	38.6
Toe of ½ to 1 slope			5.0	38.2 S ✓ X

		751.38	E5180	
4177				O.G Toe of sch lope?
T.P.	4.54	752.20 ✓	3.72	747.66 ✓
4225			5.4	46.8
Back of wier			4.9	47.3
		743.19		
T.P.	0.68	731.68	12.19	731.00
Back of wier			19.5	12.2
6' North of back of wier			19.5	12.2
" " " "			12.7	19.0
4300			11.7	21.0
4315			5.7	26.0
		743.2		
4360			6.8	36.4
Toe of ½ to 1 Slope			4.6	38.6

752.20 E5140 1/x

4200				0.6
4228			5.7	46.5
Back of wier			5.2	47.0
B.M.	9.74	740.74 (31.7) ✓		731.00 ✓

Back of wier	23.0	717.7
6' No. of back of wier	23.0	17.7
1' " " "	19.7	21.0
4300	18.7	22.0
4310	11.9	28.8
4330	5.4	35.3
4385	4.0	36.7
On toe of ½ to 1 slope	+13.0	753.7

752.2 E5100 69/x

4205	5.6	46.6
Back of wier	6.2	46.0
740.7		
Back of wier	20.6	720.1
4295	16.5	24.2
4315	6.5	34.2
4360	6.3	34.4
4400	6.0	34.7
On toe of ½ to 1 slope	+13.0	753.7

E5060 ✓R

		752.2			
4170 Back of Wier			5.1	747.1	O.G. ±
			5.3	46.9	
B.M.	6.33	737.33		731.00	
Back of Wier			14.0	23.3	
4280			11.6	25.7	
4290			16.1	21.2	
4315			3.4	33.9	
4360			3.5	33.8	
Toe of ½ to 1 slope			2.7	34.6	

E5040 61 ✓

	752.2			
4160		1.2	51.0	O.G. ±
4190		1.2	51.0	
4220		5.4	46.8	
	737.33			
4230		7.7	29.6	
4265		11.0	26.3	
4300		11.8	25.5	
4315		3.8	33.5	
4360		4.6	32.7	
Toe of ½ to slope		3.2	34.1	Complete

E5000 ✓K

T.P.	11.45	748.70	✓ 0.08	737.25	✓
T.P.	5.98	753.17	✓ 1.51	747.19	✓
	10.10	763.08	0.19	752.98	
	11.31	774.13	0.26	762.82	
A167			4.1	70.0	O.G.
A216			4.1	70.0	
		753.17			
A225			0.5	52.7	
		737.33			
A250			4.2	33.1	
4360			5.9	31.4	
Toe of ½:1 slope			5.4	31.9	

E4980 ✓ x

	737.33			
Toe of ½ to 1 schlope		5.4	31.9	
4360		6.0	31.3	
4250		5.5	31.8	
	753.17			
4240		6.2	47.0	
4220		3.1	50.1	
	774.13			
4208		3.8	70.3	
4140		4.7	69.4	O.G.

E4940 ✓ x

	774.13			
4092		5.9	68.2	O.G.
4193		3.8	70.3	
	753.17			
4205		3.1	750.1	
4214		5.3	47.1	
4255		5.1	48.1	
	737.33			
4270		5.0	32.3	
4360		6.1	31.2	
Toe of ½ to 1 slope		5.1	32.2	

E4900 ✓ x

	737.33			
Toe of ½ to 1 slope		3.6	33.7	
4360		6.4	30.9	
4280		5.8	31.5	
	753.17			
4263		5.7	47.5	
4225		5.5	47.7	
4205		4.2	49.0	
	774.13			
4176		4.3	69.8	
4074		7.1	67.0	O.G.

E4860 ✓ x

	774.13			
4090		4.5	69.6	O.G.
4165		4.4	69.7	
4190	753.17	0.3	52.9	
4212		4.3	48.9	
4260		6.2	47.0	
4280	737.33	6.4	30.9	
4360		6.2	31.1	
Toe of ½ to 1 slope		3.2	34.1	

West of E4860 Same as previous Estimates

Xsections of Spillway Exc. and Spoil Oct 31 – 1933
Elliott-Soper-McHugh

B.M.	1.46	751.33	749.87
		10.34	740.99
	3.79	744.78	

E 5600 is O.G.

E 5580

N4290			O.G.
4280		8.4	36.4
4244		9.9	34.9
4240		8.0	36.8
4210		8.5	36.3
4197		16.4	28.4
4140		42.5	02.3
4082			O.G Toe

E 5560

4075			O.G Toe
4150		23.2	21.6
4165		17.7	27.1
4178		18.0	26.8
4193		6.9	37.9
4220		6.9	37.9
4245		6.2	38.6
50		7.2	37.6
83		6.9	37.9
4290			O.G.

744.78 E5520

↑ on north same as previous

4260	2.4	42.4
4190	4.3	40.5
4165	22.2	22.6
4152	16.0	28.8
4025		O.G. Toe

E 5500

4026		O.G. Toe
4172	4.0	40.8
4220	4.3	40.5
4260	2.3	42.5

↓ on north same as previous

E 5480

4032			O.G. Toe
4180		6.0	38.8
4200		5.2	39.6
4220		5.1	39.7
4250		4.9	39.9
4252		0.3	44.5
B.M.	2.33	752.20	749.87
4350		4.0	48.2
on ½ to 1 to O.G.		3.9	48.3

752.20 E 5460

Back of wier			3.6	48.6
4290			5.4	46.8
4253			7.1	45.1
B.M.	2.91	752.78		749.87
	1.20	741.00	12.98	739.80
4247			2.4	38.6
4216			2.6	38.4
4200			14.4	26.6
4168			21.1	19.9
4064				O.G. Toc

752.2 E 5420

Back of wier			4.0	48.2
4255			6.3	45.9
		741.00		
4245			6.8	34.2
4223			6.7	34.3
4139				O.G. Toc
T.P.			11.61	729.39
	0.33	729.72		

752.2 E 5380

Back of wier	4.5	47.7
4258	6.4	45.8
729.7		
4242	0.9	28.8
4218	1.4	28.3
4139		O.G Toc

752.2 E 5340

Back of wier	5.1	47.1
4256	7.3	44.9
729.7		
4232	7.1	22.6
4205	7.4	22.3
4137		O.G. Toc

E5300

		752.2			
Back of wier			5.2	47.0	
4253			6.8	45.4	
		729.72			
4222			13.0	16.7	
4190			14.1	15.6	
T.P.			12.82	716.90	
	0.22	717.12			
4118				O.G.	Toe

Plotted for bottom of Puddle core spoil Dec. 14-34 E.B.H.

E5260

		752.2			
Back of wier			5.5	46.7	
4245			5.6	46.6	
		717.1			
4200			6.1	11.0	
4158			8.2	08.9	
4105				O.G.	Toe

E5220

B.M.	2.3	752.3		750.0	
Back of wier			4.2	48.1	
4235			4.9	47.4	
		717.1			
4181			11.4	05.7	
4148			12.1	05.0	
4102				O.G.	Toe

E5180

		752.3			
Back of wier			4.8	47.5	
4226			5.3	47.0	
4177				O.G.	Toe

752.3

Back of wier

4126

4198

4165

4200

4220
4241.4

Back of wier

4173

4180

Back of wier 4228

E5140 ✓

5.1 47.2

5.9 46.4

O.G.

E5100 ✓

O.G

4.3 48.0

6.3 46.0

6.2 46.1

E5060

O.G

5.8 46.5

5.5 46.8

Continued Nov 1-1933

B.M. 5.53 726.47 720.94

E5000

↑ ½ to 1 to Elev. 770 then level to O.G.

4245 6.7 19.8

4400 7.7 18.8

4417 +2.4 28.9

on ½ to 1 to O.G. +3.0 29.5

726.5

on ½ to 1 to O.G.

4416

4400

4260

4255

4230

4218 Back of wier ±

B.M 9.50 759.5

4215 3.1 56.4

4184 +4.5 64.0

4155 2.1 57.4

4153 12.8 46.7

4130 12.5 47.0 O.G. ±

4145

4190

4217

726.5

4219 Back of wier ± 15.0 11.5

4255 10.0 16.5

4265 5.7 20.8

4400 6.8 19.7

4414 +4.8 31.3

on ½ to 1 to O.G. +5.0 31.5

E5020

+3.8 30.3

+3.5 30.0

7.0 19.5

5.7 20.8

12.0 14.5

13.2 13.3

9.4 17.1

750.0

E5040

12.4 47.1 O.G ±

9.3 50.2

12.5 47.0

		726.5	E5060	
on ½ to 1 to O.G.			+6.4	32.9
4412			+6.0	36.5
4400			5.1	21.4
at toe of Ogee Concrete			5.2	23.3
			E5100	
at toe of Ogee Concrete			4.5	22.0
4398			4.1	22.4
		743.0		
4410			6.3	36.7
On ½ to 1 slope to O.G.			6.8	36.2
			E5140	
On ½ to 1 slope to O.G.			4.9	38.1
4416			5.3	37.7
		726.47		
T.P.	7.99	731.36	3.10	723.37
4403			7.9	23.5
at toe of Ogee conc.			9.6	21.8
T.P.	12.93	742.98	1.31	730.05

		731.4	E5180	
at toe of Ogee conc.			8.5	22.9
4400			7.5	23.9
		743.0		
4413			4.8	38.2
On ½ to 1 slope to O.G.			4.0	39.0
			E5220	
		743.0		
On ½ to 1 slope to O.G.			4.4	38.6
4410			3.4	39.6
		731.4		
4400			5.6	25.8
at toe of Ogee conc.			7.6	23.8

E 5260

Subgrade finished from toe of Ogee to N 4398

743.0

4410	2.7	40.3
On ½ to 1 slope to O.G.	1.9	41.1

E 5300

Subgrade finished from toe of Ogee to N. 4395

742.98

4407	2.5	40.5
On ½ to 1 slope to O.G.	1.3	41.7
T. P. 7.80 750.60	0.18	742.80

E 5340

Subgrade finished from toe of Ogee to N. 4395

750.6

4410	8.7	41.9
On ½ to 1 slope to O.G.	8.4	42.2

E 5380

Subgrade finished from toe of Ogee to 4402

750.6

4412	8.3	42.3
On ½ to 1 to O.G.	7.3	43.3

E 5420

Subgrade finished from toe of Ogee to 4395

750.6

4406	6.0	44.6
On ½ to 1 to O.G.	4.4	46.2

E 5460

Subgrade finished from toe of Ogee to 4393

750.6

4400	2.0	48.6
On ½ to 1 to O.G.	3.2	47.4

Nov. 3, 1933
Simpson
Salgado
Remmen:

E 4960

B.M. 4.70 728.85 724.15

½ To 1 To Elev. 770, Then Level to O.G.

4228	9.3	19.5	Toe Slope
4310	9.8	19.0	
4390	8.3	20.5	
4425	2.1	26.7	
4453	1.1	27.7	Toe Slope

½:1 To O.G.

E 4920

½:1 To Elev. 770, Then Level to O.G.

4214	8.6	20.2	Toe Slope
4295	9.1	19.7	
4410	4.4	24.4	
4450	3.5	25.3	

½:1 To O.G.

E 4880

½:1 To Elev. 770, Then Level to O.G.

4202	9.4	19.4
4310	11.2	17.6
4380	9.8	19.0
4403	4.2	24.6
4444	4.0	24.8

½:1 To O.G.

728.85 E 4840

South of Here Same as Last Est.

4218	12.1	16.7
4310	12.0	16.8
4404	5.5	23.3
4434	5.5	23.3

½:1 To O.G.

E 4800 is Same as Last Est.

Addition Sections for original ground under material wasted from puddle core beach.

Jan 19-1934

E5320

N 4127					O.G. - Toc
B.M.	9.84	713.67		703.83	
T.P.			0.12	713.55	
	11.94	725.49			
4198			6.3	19.2	
4205			6.6	18.9	
4215			6.2	19.3	
4225			4.5	21.0	

E5360

N4142					O.G. Toc
4213			+0.6	26.1	
4217			-0.3	25.2	
4236			+0.6	26.1	

Ck for Plotting Sept 1-28-34 EBH

E5180

B.M.	2.42	706.25		703.83	
4170			3.9	02.3	✓
4150			5.1	01.1	✓
4144			4.2	02.0	✓
4128			14.0	92.2	✓
T.P.	+0.00	693.26	12.99	693.26	
4110			2.2	91.1	✓
4100			4.4	88.9	✓
4080			5.2	88.1	✓

E5200

B.M.	7.02	710.85		703.83	
4174			7.2	03.6	✓
4146			7.8	03.0	✓
4140			11.6	99.2	✓
		693.26			
4120			8.0	85.3	✓
4110			13.0	80.3	✓
4080			14.9	78.4	✓
T.P.	0.69	681.00	12.95	680.31	

Ck for Plotting 1-28-34 EBH

E5220

		710.85			
4177			5.2	05.6	✓
4148			6.0	04.8	✓

681.00 E5220

4110	3.9	677.1	✓
4100	9.3	671.7	✓
4080	11.1	669.9	✓
4060	10.4	670.6	✓

E5240

710.85

4186	2.9	707.9	✓
4160	4.0	06.8	✓
4152	3.9	06.9	✓

681.00

4110	5.0	676.0	✓
4100	8.9	72.1	✓
4090	8.9	72.1	✓
4075	18.2	62.8	✓

Stripping
Final X Sections So. Abutement
April 23-1934

Elliott
Simpson
Soper
Remmen

N3090

Staff		714.2			
E5020			8.8	705.4	✓
30			7.3	06.9	✓
40			7.9	06.3	✓
50	Plotted		9.8	04.4	✓
60			12.6	01.6	✓
↑ Taken previously ↓					
5130			14.9	699.3	✓
40			14.8	99.4	✓
50			14.4	99.8	✓
60			13.3	700.9	✓

N3080

5160			13.0	01.2	✓
50			13.6	00.6	✓
40			14.1	00.1	✓
30			14.2	00.0	✓
20			13.8	00.4	✓
10			12.3	01.9	✓
5100			10.8	03.4	✓
5090			9.6	04.6	✓
80			8.0	06.2	✓

✓ Plotting 9-27-34 EBR

N3080

5070		714.2	6.3	707.9	✓
60			4.8	09.4	✓
50			3.5	10.7	✓
40			2.3	11.9	✓
30			2.0	12.2	✓
20			2.2	12.0	✓

N3070

5020			2.0	12.2	✓
30			1.9	12.3	✓
40			2.5	11.7	✓
50			3.7	10.5	✓
60	Plotted		4.6	09.6	✓
70			6.4	07.8	✓
80			8.4	05.8	✓
90			9.6	04.6	✓
5100			9.9	04.3	✓
10			10.9	03.3	✓
15			11.8	02.4	✓
20			10.7	03.5	✓
30			9.4	04.8	✓
42			2.5	11.7 O.G.	✓

X Sections for top of ~~puddle~~ core
waste and bottom of spillway spoil
Apr. 1 24-1934. Elliott-Simpson. Soper-Remmers

N 4180

B.M.	4.50	709.77		705.27	
5220			2.5	07.3	
30			1.5	08.3	
40			0.5	09.3	
50			+0.6	10.4	
60			+1.8	11.6	
70			+2.2	12.0	
80			+2.0	11.8	
90			+2.6	12.4	
5300			+0.4	10.2	
10			-2.8	07.0	
20			-4.0	05.8	

N 4170

5220			2.3	07.5	
30			1.2	08.6	
40			0.2	09.6	
50			2.2	07.6	
60			6.5	03.3	
70			8.2	01.6	
80			4.0	05.8	
90			p+1.6	11.4	
5300			4.2	05.6	
10			9.6	00.2	
20			12.1	97.7	

C.K. for Plotting 9-28-34 EBH

T.P.				709.77	
			12.53	697.24	
	0.55	Level 697.79			

N 4160

5320			6.8	91.0	
10			4.0	93.8	
5300			+2.7	00.5	
5290			+5.9	03.7	
80			+0.5	98.3	
70			3.8	94.0	
60			1.9	95.9	
		709.8			
50			8.4	01.4	
40			2.4	07.4	
30			3.5	06.3	
20			1.8	08.0	

N 4150

5220			4.9	04.9	
30			4.0	05.8	
40			6.4	03.4	
50			10.8	99.0	
		Level 697.8			
60			9.2	88.6	
70			10.6	87.2	
80			7.0	90.8	
90			0.7	97.1	

N4150

level
697.8

5300	4.1	93.7	
10	9.3	88.5	
20	14.1	83.7	

N4140

5320	20.1	77.7
10	15.4	82.4
5300	9.7	88.1
5290	6.3	91.5
80	15.2	82.6
70	15.9	81.9
60	14.8	83.0
50	7.0	90.8
40	0.8	97.0

709.8

30	10.7	98.9
20	8.6	01.2

N4130

697.79

5220	4.8	93.0
30	6.7	91.1
40	8.0	89.8
50	11.9	85.9
T.P.	12.87	684.92

π
685.14

0.22

T.P.

0.91

π
685.14

level
673.38

12.67 672.47

N4130

685.1

5260	5.1	80.0
70	6.7	78.4
80	9.4	75.7
90	1.9	83.2
5300	3.9	81.2
10	8.9	76.2
20	12.2	72.9

N4120

5320	19.8	65.3
10	12.3	72.8
5300	11.2	73.9
5290	8.2	76.9
80	13.5	71.6
70	10.1	75.0
60	10.4	74.7
50	3.2	81.9
40	2.9	82.2
30	1.3	83.8
20	+1.0	86.1

N4110

		685.1			
5220			5.1	80.0	✓
30			8.4	76.7	✓
40			9.1	76.0	✓
50			9.9	75.2	✓
60			12.4	72.7	✓
70			11.9	73.2	✓
		673.38			
80			2.3	71.1	✓
90			6.9	66.5	✓
5300			3.0	70.4	✓
10			9.4	64.0	✓
20			14.2	59.2	✓
T.P.		✓	13.00	660.38	
	0.37	660.75			

N4100

5350			11.4	49.4	✓
40			9.9	50.9	✓
30			6.6	54.2	✓
20			5.3	55.5	✓
10			6.3	54.5	✓
5300			0.7	60.1	✓
		673.4			
5290			13.9	59.5	✓
80			5.4	68.0	✓

N4100

5270	673.4	2.4	71.0	✓
60		1.1	72.3	✓
50		0.7	72.7	✓
40		0.0	73.4	✓
30		+1.6	75.0	✓
20		+3.8	77.2	✓

N4090

5220		+0.9	74.3	✓
30		0.3	73.1	✓
40		1.5	71.9	✓
50		2.7	70.7	✓
60		4.4	69.0	✓
70		9.1	64.3	✓
80		10.3	63.1	✓
90		19.9	53.5	✓
	660.8			
5300		9.1	51.7	✓
10		12.6	48.2	✓
20		9.2	51.6	✓
30		8.6	52.2	✓
40		10.7	50.1	✓
50		12.8	48.0	✓

Ck. for Plotting 9-28-34 CBH

N4080

660.8

5350	14.5	46.3	✓
40	12.7	48.1	✓
30	11.5	49.3	✓
20	11.6	49.2	✓
10	14.0	46.8	✓
5300	13.9	46.9	✓
5290	12.3	48.5	✓
80	8.8	52.0	✓
70	2.2	58.6	✓

673.38

60	11.3	62.1	✓
50	9.6	63.8	✓
40	6.6	66.8	✓

N4070

B.M. Check	8.77	664.61	664.63

660.8

5280	11.0	49.8	✓
90	13.4	47.4	✓
5300	14.3	45.5	✓
10	15.4	45.4	✓
20	13.8	47.0	✓
30	14.1	46.7	✓
40	14.8	46.0	✓
50	16.2	44.6	✓

5350			
40			
30			
20			
10			
5300			
5290			
80			

N4060

660.8

	16.8	44.0	✓
	16.1	44.7	✓
	16.0	44.8	✓
	15.6	45.2	✓
	16.1	44.7	✓
	15.8	45.0	✓
	13.1	47.7	✓
	11.1	49.7	✓

Ck for Closing 9.28-34 CBM

Sept 5 – 1933

B.M.	12.53	742.89		730.36
T.P.			0.16	742.73
	10.08	752.81		
E5520			~~5.5~~	~~747.3~~
			10.7	742.1
E5500			8.8	744.0
E6480			6.7	746.1
E5440			5.1	747.7
E5400			5.9	746.9
E5360			6.8	746.0
5320			6.7	746.1
5280			5.6	747.2
5240			5.6	747.2
5200			5.4	747.4
T.P.			9.37	752.44
	3.67	756.11		
T.P.			3.06	753.05
	10.98	764.03		
5120			12.2	751.8
5080			6.0	758.0

Sept 6 – 1933

T.P.	12.06	765.11		753.05	
5060			2.0	763.1	
T.P.			0.70	764.41	
5020			1.2	763.9	
T.P.				764.41	
	11.64	776.05			
			0.81	775.24	
	6.72	781.96			
Check on Sl. Stk.			2.5	779.5	
				64.2	
				715.3	715.4
4980			5.1	776.9	
4960			6.7	775.3	
4940			7.7	774.3	
4920			7.8	774.2	

IMPROVED TABLES

AND

INFORMATION

5,3
2,8

4,4
2,9

50,4