

W
448

ENGINEERING
LEVEL
NO. 448

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \times 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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448

N3760 between 6150 + 6320

MICROFILMED

JAN 12 1965

Index

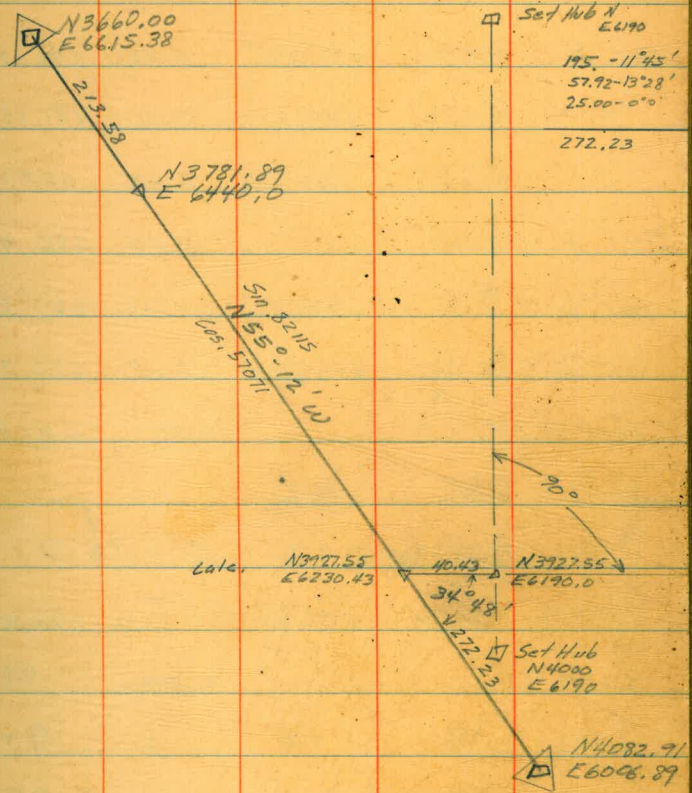
Page

Control Points on Upstream Spoil Area	1
Original X sections on Upstream Spoil Area	2-20
" " " " Downstream " "	21-42
Levelson Points spanning Crack	
N ^o of Spillway	43-52
X Sec of Spoil Area Hog Pen Mottle	66-79

MICROFILMED

JAN 12 1968

Calculations of Control Lines
on Upstream Spoil Area



Original X sections of Spoil Area
upstream July 26-1933

very warm

Elliott - Notes = Simpson T - Seper - Remmen Ch

B.M. 0.94

694.24

693.30

2

N3840

Cont. from
Book 357
28

B.M.	7.92	703.52 ✓	695.60	6330	9.0	85.2
Set B.M.	0.24	693.54 ✓	10.22 693.30 ✓	40	3.0	91.2
T.P.	0.24	681.37 ✓	12.41 681.13 ✓	50	2.6	91.6
	0.59	669.33 ✓	12.63 668.74 ✓	60	1.6	92.6
Set B.M.	0.22	656.71 ✓	12.84 656.49 ✓	70	2.2	92.0
Set B.M.	0.98	645.43 ✓	12.26 644.45 ✓	80	2.5	91.7
Set B.M.	2.04	634.83 ✓	12.64 632.79 ✓	6390	2.8	91.4
Check B.M.		3.39	631.44 631.46			

N3830

Cont. in FD. 357 Page 251

N3860

B.M.	1.14	694.44 ✓	693.30 ✓	T.P.	0.46	681.90	13.00	681.44
6330		0.0	94.4			694.24		
6340		0.7	93.7	80			4.7	89.5
50		1.0	93.4	70			6.7	87.5
				60			9.7	84.5
6360		1.6	92.8	50			12.1	82.1
50		0.9	93.5			681.9		
40		0.1	94.3	40			3.0	78.9
30		2.6	91.8	6330			5.3	76.6

Notes of Plotting

9/6/33
CP Plotting

Cont. from
Book 357
35

↓

621.9 N3820

6330	10.8	71.1	Cont. from Book 351 35	6320
40	8.8	73.1		70
50	7.3	74.6		60
60	3.3	78.6		50
	694.24			40
70	14.4	79.8		30
80	11.3	82.9		
90	4.9	89.3		6330
6400	3.7	90.5		40
10	4.1	90.1		50
20	4.5	89.7		60
		N3810		70
6440	5.7	88.5		80
30	5.1	89.1		90
20	4.8	89.4		
10	4.3	89.9		6400
6400	6.3	87.9		10
6390	11.3	82.9		20
				30

9/6/24
Ed. S. Parker

↓

681.9 N3810

	1.6	80.3		6320
	8.4	73.5		70
	7.5	74.4		60
	13.1	68.8		50
	13.9	68.0		40
	12.8	69.1	Cont. from Book 357 37	30
		N3800		
	19.9	62.0	Cont. from Book 352 37	6330
	19.1	62.8		40
	15.1	66.8		50
	14.6	67.3		60
	10.5	71.4		70
	7.9	74.0		80
	4.3	77.6		90
	694.24			
	10.2	84.0		6400
	8.2	86.0		10
	4.8	89.4		20
	5.6	88.6		30

9/6/24
Ed. S. Parker

694.24 N 3790 ✓

6440	6.3	87.9 ✓
30	5.4	88.8 ✓
20	8.6	85.6 ✓
10	15.7	78.5 ✓

681.90

6400	8.8	73.1 ✓
6390	10.1	71.8 ✓
80	12.0	69.9 ✓
70	14.3	67.6 ✓

T.P. 1.39 ✓ 670.70 12.59 669.31 ✓

60	6.1	64.6 ✓
50	9.6	61.1 ✓
40	12.2	58.5 ✓
30	12.2	58.5 ✓

N 3780

6330	16.9	53.8 ✓
40	17.1	53.6 ✓
50	10.8	59.9 ✓
60	10.0	60.7 ✓

670.7

N 3780 ✓

6370	6.9	63.8 ✓
80	4.8	65.9 ✓
90	11.7	69.0 ✓

681.90

6400	14.6	67.3 ✓
10	11.5	70.4 ✓
20	5.1	76.8 ✓
30	+3.1	85.0 ✓
40	+6.0	87.9 ✓

6450
6440

N 3770
+5.4 687.3
+3.2 85.1

30	+0.3	82.2 ✓
20	7.7	74.2 ✓
10	16.9	65.0 ✓

670.70

6400	3.9	67.0 ✓
6390	8.0	62.7 ✓
80	9.8	60.9 ✓

aluminum
flotation

aluminum
flotation

670.70

N3770

6370

11.8 58.9 ✓

60

14.5 56.2 ✓

50

15.1 55.6 ✓

40

19.8 50.9 ✓

30

19.2 51.5 ✓

Check B.M.

14.2 656.5 656.49

End July 26

5.78 662.27 ✓

B.M.

12.79 645.58 ✓

632.79 ✓

Start July 27

G.W. Converse
Elliott
Simpson
Soper
Remmen

688.3

N3760

60

1.9 86.4 ✓

50

3.2 85.1 ✓

6440

8.6 79.7 ✓

30

11.0 77.3 ✓

675.3

20

8.0 67.3 ✓

10

12.6 62.7 ✓

662.3

6400

3.2 59.1 ✓

6390

6.7 55.6 ✓

80

6.9 55.4 ✓

Plotting Check

	662.3 ^L	N3760 [↓]	
6370		8.6	53.7 ✓
60		11.5	50.8 ✓
50		13.2	49.1 ✓
40		16.5	45.8 ✓
30		17.7	44.6 ✓
	645.6 [↑]	N3750 [↓]	
6190		21.0	24.6 ✓
6200		17.6	28.0 ✓
10		16.7	28.9 ✓
20		15.3	30.3 ✓
30		15.0	30.6 ✓
40		14.4	31.2 ✓
50		13.9	31.7 ✓
60		12.3	33.3 ✓
70		11.0	34.6 ✓
80		10.7	34.9 ✓
90		8.5	37.1 ✓
6300		7.9	37.7 ✓
10		6.5	39.1 ✓

9/14/54
Plotting Checked
N

	645.6 [↑]	N3750 [↓]	
6320		5.3	40.3 ✓
30		2.0	43.6 ✓
	662.3 ^L		
40		17.1	45.2 ✓
50		16.3	46.0 ✓
60		14.0	48.3 ✓
70		10.2	52.1 ✓
80		12.0	50.3 ✓
90		9.9	52.4 ✓
6400		2.8	59.5 ✓
	675.3 [↑]		
10		13.5	61.8 ✓
20		9.3	66.0 ✓
30		4.3	71.0 ✓
40		1.0	76.3 ✓
	Continued on page 13		N3740 [↓]
6440		5.3	70.0 ✓
30		9.1	66.2 ✓
20		13.1	62.2 ✓

9/14/54
Plotting Checked
N

	662.3	N3740	
6410	0.8	61.5	
6400	5.0	57.3	
6390	10.0	52.3	
80	12.9	49.4	
70	18.3	44.0	
	645.6		
60	2.7	42.9	
50	3.4	42.2	
40	3.1	42.5	
30	1.5	44.1	
20	7.0	38.6	
10	9.8	35.8	
6300	9.6	36.0	
6290	13.2	32.4	
80	14.5	31.1	
70	15.2	30.4	
60	16.1	29.5	
50	17.5	28.1	
40	18.0	27.6	

9/10/54
Plotting in

	645.6	N3740	
6230	18.8	26.8	
20	19.0	26.6	
		N3730	
6230	22.5	23.1	
40	20.6	25.0	
50	21.0	24.6	
60	18.6	27.0	
70	19.2	26.4	
80	18.0	27.6	
90	17.2	28.4	
6300	14.8	30.8	
10	13.6	32.0	
20	9.5	36.1	
30	5.6	40.0	
40	5.6	40.0	
50	6.9	38.7	
60	4.0	41.6	
	662.3		
70	17.4	44.9	

9/10/54
Plotting in

X

662.3

N3730

6380	14.3	48.0
90	8.4	53.9
6400	7.1	55.2
10	3.0	59.3
20	1.7	60.6
30	+1.7	64.0
40	+3.4	65.7

Continued on N3720
Page 13

6440	+1.5	60.8 63.8
30	1.0	61.3
20	2.1	60.2
10	5.2	57.1
6400	8.3	54.0
6390	9.2	53.1
80	16.2	46.1
70	19.0	43.3
	645.6	
60	5.0	40.6
50	10.3	35.3

94/32
et.
at
20

8

645.6

N3720

6340	9.1	36.5
30	11.6	34.0
20	14.6	31.0
10	16.6	29.0
6300	18.1	27.5
6290	22.2	23.4
80	22.5	23.1
70	22.4	23.2
6260	24.2	21.4

N3710

B.M.	12.83	645.62	632.79
6280		26.0	19.6
90		24.1	21.5
6300		21.2	24.4
10		16.6	29.0
20		17.5	28.1
30		14.8	30.8
40		11.4	34.2
50		9.0	36.6

at
of
20

645.6

N3710

6360 6.1 39.5 ✓

70 3.5 42.1 ✓

80 ^W 662.3 → 17.0 45.3 ✓

90 13.6 48.7 ✓

6400 9.6 52.7 ✓

10 7.0 55.3 ✓

20 5.1 57.2 ✓

30 2.7 59.6 ✓

40 0.6 61.7 ✓

675.2

50 11.2 64.0 ✓

60 8.1 67.1 ✓

70 5.2 70.0 ✓

80 1.6 73.6 ✓

687.7

90 8.5 79.2 ✓

6500 4.1 83.6 ✓

10 4.8 82.9 ✓

687.7

N3700

4.9 82.8 ✓

9.0 78.7 ✓

675.2

3.5 71.7 ✓

6.8 68.4 ✓

8.3 66.9 ✓

10.7 64.5 ✓

13.3 61.9 ✓

^W
662.3

40 2.6 59.7 ✓

30 5.0 57.3 ✓

20 7.4 54.9 ✓

10 9.5 52.8 ✓

6400 10.0 52.3 ✓

6390 14.5 47.8 ✓

80 17.8 44.5 ✓

6456

70 4.6 41.0 ✓

60 7.3 38.3 ✓

9/4/34
Ch. Plotting9/4/34
Ch. Plotting

645.6

N3700

6350 9.8 35.8 ✓

40 12.5 32.1 ✓

30 17.0 28.6 ✓

20 18.6 27.0 ✓

10 21.1 24.5 ✓

6300 22.0 23.6 ✓

N3690

6300 27.3 18.3 ✓

10 23.4 22.2 ✓

20 22.4 23.2 ✓

30 18.3 27.3 ✓

40 14.9 30.7 ✓

50 11.8 33.8 ✓

60 8.6 37.0 ✓

70 6.3 39.3 ✓

80 2.9 42.7 ✓

90 0.0 45.6 ✓

662.3

6400 14.3 48.0 ✓

10

662.3

N3690

6410 11.9 50.4 ✓

20 10.1 52.2 ✓

30 7.6 54.7 ✓

40 4.6 57.7 ✓

675.2

50 15.0 60.2 ✓

60 13.3 61.9 ✓

70 11.2 64.0 ✓

80 8.6 66.6 ✓

90 6.6 68.6 ✓

6500 2.0 73.2 ✓

10 +4.4 79.6 ✓

20 +8.3 83.5 ✓

N3680

6530 +8.3 83.5 ✓

20 +2.9 78.1 ✓

10 1.4 73.8 ✓

6500 6.5 68.7 ✓

6490 9.1 66.1 ✓

9/1/54
9/1/54
Ob.
20

9/1/54
9/1/54
Ob.
20

675.2

N3680

6480

10.7 64.5 ✓

70

12.6 62.6 ✓

60

15.0 60.2 ✓

662.3

50

4.2 58.1 ✓

40

6.5 55.8 ✓

30

10.5 51.8 ✓

20

12.8 49.5 ✓

10

15.0 47.3 ✓

6400

16.9 45.4 ✓

645.6

6390

2.4 43.2 ✓

80

4.2 41.4 ✓

70

7.8 37.8 ✓

60

10.2 35.4 ✓

50

13.1 32.5 ✓

40

15.7 29.9 ✓

30

18.4 27.2 ✓

20

21.0 24.6 ✓

63 10

22.9 22.7 ✓

645.6

N3670

6310

21.8 23.8 ✓

20

20.1 25.5 ✓

30

18.5 27.1 ✓

40

16.9 28.7 ✓

50

14.0 31.6 ✓

60

11.2 34.4 ✓

70

8.9 36.7 ✓

80

6.6 39.0 ✓

90

5.1 40.5 ✓

6400

3.0 42.6 ✓

10

1.7 43.9 ✓

662.3

20

16.0 46.3 ✓

30

13.4 48.9 ✓

40

9.8 52.5 ✓

50

6.6 55.7 ✓

60

4.2 58.1 ✓

70

1.8 60.5 ✓

80

0.7 61.6 ✓

675.3

✓ N3670

6490 11.6 63.7 ✓

6500 10.2 65.1 ✓

10 3.2 72.1 ✓

20 2.8 72.5 ✓

30 +5.3 80.6 ✓

40 +5.0 80.3 ✓

✓ N3660

6540 +5.0 80.3 ✓

30 +5.9 81.2 ✓

20 4.3 74.0 ✓

10 8.6 66.7 ✓

6500 12.1 63.2 ✓

6490 13.8 61.5 ✓

80 662.3 2.8 59.5 ✓

70 4.2 58.1 ✓

60 5.5 56.8 ✓

50 7.7 54.6 ✓

40 9.0 53.3 ✓

30 15.9 46.4 ✓

9/14/54 Plotting Checked

645.6

✓ N3660

6420 5.1 40.5 ✓

10 7.1 38.5 ✓

6400 7.1 38.5 ✓

6390 8.1 37.5 ✓

80 8.3 37.3 ✓

70 10.6 35.0 ✓

60 12.5 33.1 ✓

50 15.4 30.2 ✓

40 17.7 27.9 ✓

30 19.6 26.0 ✓

20 20.8 24.8 ✓

10 23.0 22.6 ✓

N3650 is on page 14

9/14/54 Plotting Checked
5/27/54

12

N3720

B.M.	0.0	681.1 ✓	681.1
6450			14.6 66.5 ✓
60			11.1 70.0 ✓
70			5.2 75.9 ✓
	7.8	688.9 ✓	681.1
80			7.2 81.7 ✓
90			5.5 83.4 ✓
6500			5.6 83.3 ✓

N3730

6480			4.8 84.1 ✓
70			7.6 81.3 ✓
		681.1	
60			6.2 74.9 ✓
50			10.3 70.8 ✓

N3740

6450			6.7 74.4 ✓
60			1.3 79.8 ✓
	7.0	688.1	681.1
70			2.8 85.3 ✓
80			3.1 85.0 ✓

688.1

N3750

6470			2.4 85.7 ✓
60			2.5 85.6 ✓
50			7.5 80.6 ✓

965
965
965

965
965
965

F.M. July 27-1943

✓ N3650

B.M.	4.05	660.54 ^L	656.49	
		675.3 ^T		
6550			73.8	79.1 ✓
40			14.3	79.6 ✓
30			1.1	74.2 ✓
20			6.8	68.5 ✓
10			10.2	65.1 ✓
6500			13.4	61.9 ✓
6490			15.9	59.4 ✓
		660.5 ^L		
80			2.8	57.7 ✓
70			4.3	56.2 ✓
60			5.5	55.0 ✓
50			7.1	53.4 ✓
40			10.9	49.6 ✓
30			14.7	45.8 ✓
		645.6 ^T		
20			3.5	42.1 ✓

9/6/20 Plotting checked

14

645.6^T

✓ N3650

6410	9.0	36.6 ✓
6400	11.6	34.0 ✓
6390	11.6	34.0 ✓
80	10.7	34.9 ✓
70	13.8	31.8 ✓
60	14.3	31.3 ✓
50	16.4	29.2 ✓
40	19.0	26.6 ✓
30	21.3	24.3 ✓
		✓ N3640
6330	23.0	22.6 ✓
40	21.3	24.3 ✓
50	19.4	26.2 ✓
60	18.6	27.0 ✓
70	16.6	29.0 ✓
80	17.6	28.0 ✓
90	16.5	29.1 ✓
6400	14.5	31.1 ✓

9/6/20 Plotting checked

	645.6	N3640	
6410		7.5	38.1 ✓
20		4.8	40.8 ✓
30		0.9	45.7 ✓
B.M.	0.68	645.13	644.45
		L	660.5
40		14.3	46.2 ✓
50		10.9	49.6 ✓
60		8.0	52.5 ✓
70		6.5	54.0 ✓
80		5.7	54.8 ✓
90		3.1	57.4 ✓
6500		0.9	59.6 ✓
	675.3		
10		12.5	62.8 ✓
20		10.2	65.1 ✓
30		7.0	68.3 ✓
40		2.8	72.5 ✓
50		+2.4	77.7 ✓
60		+2.7	78.0 ✓

9/4/34
Electing Checked No.

	675.3	N3630	
6580		+1.5	76.8 ✓
70		+1.5	76.8 ✓
60		0.2	75.1 ✓
50		3.6	71.7 ✓
40		8.0	67.3 ✓
30		10.0	65.3 ✓
20		12.3	63.0 ✓
10		14.0	61.3 ✓
	660.5		
6500		1.7	58.8 ✓
6490		4.6	55.9 ✓
80		6.9	53.6 ✓
70		9.9	50.6 ✓
60		11.6	48.9 ✓
50		13.8	46.7 ✓
	645.7		
40		1.3	43.8 ✓
30		2.0	43.1 ✓
20		7.8	37.3 ✓

9/10/34
Reading Ch.

6451

✓ 3630

6410	10.4	34.7
6400	14.2	30.9
6390	19.0	26.1
80	23.5	21.6
70	20.0	25.1
60	20.8	24.3
6350	19.8	25.3

✓ N 3620

6350	24.6	20.5
60	23.8	21.3
70	25.6	19.5
80	23.1	22.0
90	16.1	29.0
6400	15.0	30.1
10	13.0	32.1
20	7.8	35.3
30	6.1	39.0
40	3.5	41.6

7/4/34
Plotted Ch. 20

6451

✓ N 3620

6450	1.3	43.8
60	14.0	46.5
70	12.0	48.5
80	9.5	51.0
90	7.0	53.5
6500	3.5	57.0
10	2.0	58.5
20	0.3	60.2

673.5

30	12.0	61.5
40	10.1	63.4
50	8.2	65.3
60	5.5	68.0
70	3.5	70.0
80	1.3	72.2
90	+1.1	74.6

9/13/34
Plotted Checked 20

	673.5	N3610 ✓	
6600		0.0	73.5 ✓
6590		4.1	69.4 ✓
80		7.9	65.6 ✓
70		9.8	63.7 ✓
60		11.6	61.9 ✓
50		12.7	60.8 ✓
	660.5		
40		0.7	59.8 ✓
30		1.3	59.2 ✓
20		2.8	57.7 ✓
10		4.3	56.2 ✓
6500		5.8	54.7 ✓
6490		9.0	51.5 ✓
80		10.4	50.1 ✓
70		13.8	46.7 ✓
	645.1		
60		0.4	44.7 ✓
50		4.0	41.1 ✓
40		6.6	38.5 ✓

9/4/24
Plotting Checked

	645.1	N3610	
6430		6.1	39.0 ✓
20		12.8	32.3 ✓
10		16.2	28.9 ✓
6400		19.8	25.3 ✓
6390		21.9	23.2 ✓
80		23.3	21.8 ✓
70		30.0	15.1 ✓
		✓N3600	
6390		25.8	619.3 ✓
6400		22.4	22.7 ✓
10		19.1	26.0 ✓
20		15.4	29.7 ✓
30		12.9	32.2 ✓
40		9.7	35.4 ✓
50		6.8	38.3 ✓
60		3.3	41.8 ✓
70		1.0	44.1 ✓
	660.5		
80		14.0	46.5 ✓

9/4/24
Plotting Checked

660.5 ✓ N3600

6490	11.5	49.0 ✓
6500	9.0	51.5 ✓
10	6.6	53.9 ✓
20	5.4	55.1 ✓
30	4.0	56.5 ✓
40	3.0	57.5 ✓
50	2.7	57.8 ✓
60	2.6	57.9 ✓
70	3.4	57.1 ✓
80	1.7	58.8 ✓

9/15/54
Flooding Checked 20

673.5

90	8.2	65.3 ✓
6600	0.8	72.7 ✓
10	1.0	72.5 ✓

✓ N3590

6610	1.7	71.8 ✓
6600	4.9	68.6 ✓
6590	12.5	61.0 ✓

660.5 ✓ N3590

6580	6.2	54.3 ✓
70	7.1	53.4 ✓
60	5.4	55.1 ✓
50	5.1	55.4 ✓
40	5.3	55.2 ✓
30	6.3	54.2 ✓
20	8.0	52.5 ✓
10	9.7	50.8 ✓
6500	10.9	49.6 ✓
6490	14.2	46.3 ✓
80	16.0	44.5 ✓

9/15/54
Flooding Checked 20

645.1

70	4.0	41.1 ✓
60	6.5	38.6 ✓
50	10.0	35.1 ✓
40	13.5	31.6 ✓
30	14.7	30.4 ✓
20	17.0	28.1 ✓
10	21.9	23.2 ✓
6400	26.2	18.9 ✓

19

	[↑] 645.1		✓ N3580
6410		23.3	21.8 ✓
6420		20.0	25.1 ✓
30		17.6	27.5 ✓
40		15.9	29.2 ✓
50		12.6	32.5 ✓
60		10.6	34.5 ✓
70		7.5	37.6 ✓
80		5.1	40.0 ✓
90		1.1	44.0 ✓
	[↓] 660.5		
6500		15.1	45.4 ✓
10		12.2	48.3 ✓
20		11.0	49.5 ✓
30		9.5	51.0 ✓
40		7.8	52.7 ✓
50		7.8	52.7 ✓
60		8.6	51.7 ✓
70		11.1	49.4 ✓
80		9.3	51.2 ✓

9/4/54 Plotting Check 11/2

	[↓] 660.5		✓ N3580
6590		3.2	657.3 ✓
6600		9.3	664.2 ✓
10		2.3	71.2 ✓
20		2.3	71.2 ✓
			✓ N3570
6620		3.3	70.2 ✓
10		6.6	66.9 ✓
6600		12.5	61.0 ✓
	[↓] 660.5		
6590		6.1	54.4 ✓
80		12.9	47.6 ✓
70		17.0	43.5 ✓
60		11.7	48.8 ✓
50		10.4	50.1 ✓
40		10.4	50.1 ✓
30		12.2	48.3 ✓
20		14.0	46.5 ✓
10		15.0	45.5 ✓

9/4/54 Plotting Check 11/2

645.1

✓ N3570

6500	3.3	41.8
6490	5.4	39.7
80	8.2	36.9
70	10.3	34.8
60	12.5	32.6
50	15.1	30.0
40	18.5	26.6
30	21.5	23.6
20	24.0	21.1
10	27.0	18.1

9/13/34
Plotting checked in

✓ N3560

N3560

6420	28.5	616.6
30	24.5	20.6
40	21.2	23.9
50	17.7	27.4
60	15.1	30.0
70	12.4	32.7
80	10.3	34.8
90	7.8	37.3

9/14/34
Plotting checked in

645.1

✓ N3560

6500	5.5	639.6
10	3.2	41.9
20	1.1	44.0
660.5		
30	14.5	646.0
40	13.2	47.3
50	13.6	46.9
60	15.7	44.8
70	17.8	42.7
80	15.9	44.6
90	9.2	51.3

Plotting checked in

6600

673.5

10	11.0	662.5
20	4.8	68.7
30	4.5	69.0

End July 27 - 1933

Continued from Book 357

page 110

Aug 16 - 1933

644.34

N4510 ✓

Level
644.34

N4520 ✓

Cont. on
Page 37

4250

9.4

34.9

4200

22.0

22.3 ✓

40

10.4

33.9

11

22.0

22.3 ✓

30

11.9

32.4

13

13.5

30.8 ✓

20

13.6

30.7

20

12.3

32.0 ✓

17

21.8

22.5

30

10.3

34.0 ✓

4200

21.8

22.5

Cont. from
Page 37

40

7.8

36.5 ✓

N4500 ✓

Cont. from
Book 357-59

50

3.5

40.8 ✓

4200

21.5

22.8

60

4.3

40.0 ✓

4223

21.7

22.6

70

4.8

39.5 ✓

T.P.

3.01

Level
635.16 ✓

12.19

632.15 ✓

80

3.6

40.7 ✓

0.18

634.98 ✓

90

3.3

41.0 ✓

11.15

X
646.13 ✓

4300

+2.3

46.6 ✓

Cont. in
Book 357
59

26

635.2

5.9

29.3

N4510 ✓

4300

+2.8

47.1 ✓

Cont. in
Book 357
59

40

5.5

29.7

4290

3.5

40.8 ✓

50

5.4

29.8

80

7.6

36.7 ✓

60

4.0

31.2

70

9.3

35.0 ✓

70

646.1

3.4

31.8

60

8.5

35.8 ✓

80

9.1

37.0

90

3.8

42.3

4300

0.1

46.0

Cont. on
Page 37

Plotting sh. as shown by C.P.M.

T
646.1

N4490 ✓

U.
635.2

N4480 ✓

22

4300 0.8 45.3

4250 5.8 29.4

4290 3.8 42.3

60 2.6 32.6

80 7.4 38.7

70 10.4 35.7

70 11.8 34.3

80 7.6 38.5

635.2

90 5.5 40.6

60 4.8 30.4

4300 2.5 43.6

50 7.9 27.3

N4470 ✓

40 5.1 30.1

4300 4.2 41.9

30 12.1 23.1

4290 7.0 39.1

20 12.2 23.0

80 9.0 37.1

10 12.0 23.2

70 10.6 35.5

4200 11.9 23.3

60 12.3 33.8

Cont. from
Page 37

N4480 ✓

U.
635.2

4200 11.6 23.6

50 4.8 30.4

10 11.6 23.6

45 6.2 29.5

20 11.6 23.6

43 11.3 23.9

30 11.8 23.4

30 11.3 23.9

37 11.8 23.4

20 11.3 23.9

40 10.0 25.2

10 11.4 23.8

4200 11.6 23.6

Cont. from
Page 38

Plotting as shown by
E.H.H.

635.2

N4460 ✓

Cont. from
Page 38

4200	11.5	23.7
10	11.1	24.1
20	11.2	24.0
30	11.0	24.2
40	11.2	24.0
47	11.0	24.2
49	5.2	30.0
60	2.7	32.5

↑
646.1

70	12.4	33.7
80	10.3	35.8
90	8.8	37.3
4300	5.9	40.2

N4450 ✓

4300	7.1	39.0
4290	10.2	35.9
80	12.6	33.5
70	3.1	32.1
60	5.1	30.1

4.
635.2Plotting closed 9-12-34
as shown by

23

635.2

N4450 ✓

4256	10.8	24.4
50	10.8	24.4
40	10.7	24.5
30	10.6	24.6
20	10.7	24.5
10	11.4	23.8
05	11.3	23.9
4200	13.0	22.2

Cont. from
Page 38

N4440 ✓

Cont. from
p. 39

4200	13.5	21.7
4205	11.4	23.8
10	10.1	25.1
20	10.7	24.5
30	10.4	24.8
40	10.3	24.9
50	10.3	24.9
60	10.5	24.7
65	10.3	24.9
66	4.8	30.4

635.2

N4440 ✓

4270 4.7 30.5 ✓
80 3.3 31.9 ✓

646.1

90 12.1 34.0
4300 8.7 37.4 ^{35.7}/_{6'}

N4430 ✓

4300 11.1 35.0 ✓
4290 14.0 32.1 ✓

635.16

4277 4.9 30.3 ✓
74 9.6 25.6 ✓

60 9.9 25.3 ✓

50 9.9 25.3 ✓

40 10.0 25.2 ✓

30 10.1 25.1 ✓

20 10.3 24.9 ✓

10 9.7 25.5 ✓

4200 15.6 19.6 ✓

T.P. 0.0 632.92 ✓ 2.24 632.92 ✓

635.16

N4420 ✓

0.25 634.91 ✓

12.35

level
647.26 ✓

cont. in Book
357-58

4410

+3.7 51.0 ✓

4400

0.0 47.3 ✓

4390

3.3 44.0 ✓

80

5.7 41.6 ✓

70

5.4 41.9 ✓

60

4.5 42.8 ✓

50

5.2 42.1 ✓

40

6.8 40.5 ✓

30

8.3 39.0 ✓

20

10.2 37.1 ✓

10

12.3 35.0 ✓

4300

14.7 32.6 ✓

632.92

4288

2.7 30.2 ✓

86

7.3 25.6 ✓

70

7.2 25.7 ✓

60

7.2 25.7 ✓

as shown by
Plotting sheet 7-12-34 Book

632.92

N4420 ✓

4250

7.3 25.6

Cont on

40

7.5 25.4

Page 39

N4410 ✓

4250

7.1 25.8

60

6.9 26.0

70

6.8 26.1

80

6.6 26.3

90

6.7 26.2

98

6.7 26.2

4300

1.8 31.1

647.26

10

14.6 32.7

20

12.7 34.6

30

10.9 36.4

40

9.0 38.3

50

8.1 39.2

60

8.2 39.1

70

7.8 39.5

80

7.8 39.5

647.3

N4410 ✓

4390

5.1 42.2

4400

2.4 44.9

10

+0.1 47.4

N4400 ✓

4410

3.0 44.3

4400

4.5 42.8

4390

7.1 40.2

80

8.6 38.7

70

10.7 36.6

60

10.9 36.4

50

11.4 35.9

40

11.9 35.4

30

12.8 34.5

20

15.2 32.1

632.92

14

11.4 31.5

12

6.3 26.6

4300

6.3 26.6

4290

6.2 26.7

632.92

N4400 ✓

4280 6.4 26.5 ✓

70 6.7 26.2 ✓

60 6.6 26.3 ✓

Cont. on Page 40

N4390 ✓

Cont. from Page 41

4270 6.5 26.4 ✓

80 6.3 26.6 ✓

90 6.0 26.9 ✓

4300 5.8 27.1 ✓

10 5.7 27.2 ✓

20 5.7 27.2 ✓

27 5.5 27.4 ✓

29 1.0 31.9 ✓

40 +0.4 33.3 ✓

50 +1.3 34.2 ✓

60 +2.6 35.5 ✓

70 +2.3 35.2 ✓

80 +2.9 35.8 ✓

90 +1.3 34.2 ✓

4400 +2.0 34.9 ✓

4410 +3.6 36.5 ✓

632.92

N4380 ✓

4410 +3.0 35.9 ✓

4400 +2.0 34.9 ✓

4390 +0.8 33.7 ✓

80 0.3 32.6 ✓

70 1.4 31.5 ✓

60 2.5 30.4 ✓

50 3.2 29.7 ✓

40 4.3 28.6 ✓

30 5.0 27.9 ✓

20 5.3 27.6 ✓

10 5.5 27.4 ✓

4300 5.6 27.3 ✓

4290 5.9 27.0 ✓

80 6.1 26.8 ✓

Cont. on Page 41

N4370 ✓

4290 5.8 27.1 - Cont. on P. 41

4300 5.5 27.4 ✓

10 5.3 27.6 ✓

20 5.1 27.8 ✓

Platting ok. as shown by CDA

632.92

N4370 ✓

4330 4.7 28.2 ✓

40 4.3 28.6 ✓

50 3.7 29.2 ✓

60 2.9 30.0 ✓

70 1.9 31.0 ✓

80 0.7 32.2 ✓

90 +0.3 33.2 ✓

4400 +1.4 34.3 ✓

10 +2.4 35.3 ✓

end of
sec

N4360 ✓

4410 +0.7 33.6 ✓

end of
sec

4400 0.1 32.8 ✓

4390 0.8 32.1 ✓

80 1.6 31.3 ✓

70 2.4 30.5 ✓

60 3.1 29.8 ✓

50 3.8 29.1 ✓

40 4.4 28.5 ✓

30 4.9 28.0 ✓

632.92

N4360 ✓

27

4320

5.0 27.9 ✓

10

5.5 27.4 ✓

4300

5.2 27.7 ✓

Cont Pa = 42

B.M. check

301 629.91 629.89

Plotting ok as shown
by
S.B.H.

Aug. 26, 1933 Simpson
Soper
Rammen

7
671.98

N4920 ✓

28

B.M. 11.16 ^{Level} 679.58 ✓ 668.42

4150

5.7 86.1

T.P. 13.03 ^{Transit} 691.78 ✓ 0.83 678.75 ✓

40

11.6 80.2

N4950 ✓

N4910 ✓

E 4140 3.1 88.7

4140

16.8 75.0

50 3.2 88.6

50

11.4 80.4

60 2.9 88.9

60

7.7 84.1

N4940 ✓

67

0.4 91.4

4160 2.8 89.0

70

0.3 91.5

50 2.5 89.3

80

1.1 90.7

40 1.9 89.9

90

0.8 91.0

N4930 ✓

N4900 ✓

4140 7.2 84.6

4190

0.2 91.6

50 1.2 90.6

80

+0.6 92.4

60 2.2 89.6

75

+0.9 92.7

70 2.2 89.6

60

9.1 82.7

N4920 ✓

50

15.2 76.6

4180 1.5 90.3

679.58

70 2.0 89.8

40

9.4 70.2

60 1.1 90.7

679.58

N4890 ✓

4140	13.4	66.2
50	8.2	71.4
60	1.3	78.3

691.78

70	6.5	85.3
80	+1.4	93.2
90	+0.4	92.2
4200	+0.4	92.2

N4880 ✓

4210	+0.8	92.6
4200	+0.8	92.6
4185	+0.5	92.3
80	4.4	87.4
70	9.8	82.0

679.58

60	3.9	75.7
50	8.0	71.6
40	14.1	65.5

679.58

N4870 ✓

29

4140	14.4	65.2
50	10.0	69.6
60	3.4	76.2

691.78

70	12.9	78.9
80	8.5	83.3
90	+1.6	93.4
4200	+0.9	92.7
10	+0.8	92.6

Aug. 28, 1933

B.M.	0.20	^{transit} 668.62 ✓	668.42
B.M.	12.46	^{level} 680.88 ✓	668.42

N4860 ✓

4190	+6.7	87.6
80	+0.4	81.3
70	3.6	77.3
60	8.3	72.6
50	12.9	68.0
40	16.5	64.4

680.88

N4850 ✓

4140	17.7	63.2
50	14.7	66.2
60	10.7	70.2
70	7.0	73.9
80	1.9	79.0
90	+3.9	84.8

N4840 ✓

4190	0.8	80.1
80	4.4	76.5
70	9.7	71.2
60	13.2	67.7
50	3.8	64.8
40	5.0	63.6
30	9.2	59.4
20	14.2	54.4
10	17.7	50.9
4100	22.9	45.7
4090	29.3	39.3

transit
668.62

3181 668.62

N4830 ✓

30

4108	19.4	49.2
20	14.6	54.0
30	11.1	57.5
40	7.2	61.4
50	5.6	63.0
60	2.5	66.1

Level
680.88

70	10.1	70.8
80	8.0	72.9
90	5.9	75.0

N4820 ✓

4190	11.2	69.7
80	14.3	66.6
70	2.1	66.5
60	4.3	64.3
50	6.6	62.0
40	11.2	57.4
30	13.4	55.2
22	15.7	52.9

transit
668.62

Transit
668.62

N4810 ✓

4127	17.1	51.5
40	13.0	55.6
50	10.1	58.5
60	5.3	63.3
70	9.3	59.3
80	5.8	62.8
90	1.9	66.7

N4800 ✓

4190	1.9	66.7
80	7.3	61.3
70	11.2	57.4
T.P.	0.51	Level ✓ 656.00
60	1.5	54.5
50	0.5	55.5
40	2.7	53.3
31	4.7	51.3
27	12.8	43.2

1184 656.00

N4790 ✓

31

4133	11.3	44.7
35	5.7	50.3
40	5.2	50.8
50	8.1	47.9
60	5.4	50.6
70	12.5	56.1

668.62

80	7.1	61.5
90	1.8	66.8

N4780 ✓

4190	3.8	64.8
80	7.8	60.8
70	13.4	55.2
60	5.2	51.2
50	8.9	47.1
45	13.8	42.2
40	13.7	42.3
33	10.2	45.8

656.00

656.00

N4770 ✓

4127	16.6	39.4
40	15.3	40.7
50	13.1	42.9
60	6.4	47.6
70	1.2	54.8

668.62

80	7.6	61.0
90	6.1	62.5

N4760 ✓

4190	8.5	60.1
80	11.1	57.5

Level
656.00

70	1.5	54.5
60	7.6	48.4
50	13.6	42.4

T.R. 0.72 ^{Transit} 643.75 ✓

40 5.5 38.2

30 10.1 33.6

21 8.3 35.4

from Book 450

843.75

N4750 ✓

32

4117	13.8	29.9
20	13.2	30.5
30	10.8	32.9
40	5.7	38.0
50	1.1	42.6

656.00

60	8.3	47.7
70	3.0	53.0
80	0.0	56.0
90	+2.3	58.3

N4740 ✓

4190	+0.9	56.9
80	2.5	53.5
70	5.9	50.1
60	9.3	46.7
50	13.4	42.6

643.75

40 5.3 38.4

30 9.4 34.3

4119 13.8 29.9

Cont. from Book 450-11

Cont. from Book 450-11

Cont. in Book 357-64

Cont. in Book 357-64

643.75

N4730 ✓

Cont. from

B. 450-11

4120

12.0

317.8

4129

10.8

329.0

30

8.9

348.0

40

7.0

367.0

40

5.2

38.5

50

3.8

39.9

50

0.9

428.0

656.00

656.00

60

10.7

453.0

60

12.7

43.3

70

7.1

489.0

70

9.6

46.4

80

4.2

518.0

80

6.3

49.7

90

0.9

55.1

90

2.0

54.0

N4720 ✓

Cont. in
Book 357-64

4190

1.7

54.3

4190

4.2

51.8

80

4.8

51.2

80

8.0

48.0

70

8.4

47.6

70

11.0

45.0

60

11.8

44.2

60

2.2

41.5

643.75

643.75

50

2.2

41.5

50

5.3

38.4

40

5.6

38.1

40

8.6

35.1

30

9.1

34.6

32

10.3

33.4

24

11.4

32.3

33

643.75

N4710 ✓

Book 450
12

4129

10.8

329.0

40

7.0

367.0

50

3.8

39.9

656.00

60

12.7

43.3

70

9.6

46.4

80

6.3

49.7

90

2.0

54.0

N4700 ✓

4190

4.2

51.8

80

8.0

48.0

70

11.0

45.0

60

2.2

41.5

50

5.3

38.4

40

8.6

35.1

32

10.3

33.4

Book 450
12

Plotting checked 9-12-34 G.W.

643.75

N4690 ✓

4138

11.2

32.5 ✓

 $\frac{450}{12}$

50

6.5

37.2 ✓

60

3.5

40.2 ✓

656.00

70

12.9

43.1 ✓

80

8.8

47.2 ✓

90

6.2

49.8 ✓

 $\frac{357}{65}$

N4680 ✓

4190

8.5

47.5 ✓

 $\frac{357}{66}$

80

11.5

44.5 ✓

70

14.5

41.5 ✓

643.75

60

5.1

38.6 ✓

50

8.7

35.0 ✓

42

11.0

32.7 ✓

632.15

4138

13.3

18.9 ✓

 $\frac{450}{12}$

14.7

17.4 ✓

N4670 ✓

4140

13.6

18.5 ✓

 $\frac{450}{12}$

43

13.6

18.5 ✓

632.15

N4670 ✓

34

4144

8.7

23.4 ✓

643.75

4155

8.2

35.5 ✓

60

5.7

38.0 ✓

70

3.2

40.5 ✓

656.00

80

12.8

43.2 ✓

90

10.3

45.7 ✓

 $\frac{357}{66}$

4190

11.9

44.1 ✓

 $\frac{357}{67}$

643.75

80

2.1

41.6 ✓

67

5.6

38.1 ✓

632.15

51

9.3

22.8 ✓

50

13.0

19.1 ✓

40

13.1

19.0 ✓

 $\frac{450}{12}$

Plotting of points

Plotting checked 9-12-34 BSH

632.15

N4650 ✓

4140

12.9

19.2 ✓

450-12

54

12.9

19.2 ✓

58

8.0

24.1 ✓

643.75

4167

12.5

31.2 ✓

70

6.0

37.7 ✓

80

3.3

40.4 ✓

90

13.5

42.5 ✓

357/67

656.00

N4640 ✓

4190

15.1

40.9 ✓

357/67

643.75

75

6.3

37.4 ✓

632.15

62

7.5

24.6 ✓

60

12.6

19.5 ✓

50

12.6

19.5 ✓

40

12.5

19.6 ✓

450/13

N4630 ✓

4140

12.2

19.9 ✓

450/13

35.

632.15

N4630 ✓

4165

12.4

19.7 ✓

66

8.4

23.7 ✓

643.75

4175

7.9

35.8 ✓

90

4.5

39.2 ✓

357-68

N4620 ✓

4190

8.3

35.4 ✓

357-68

80

10.3

33.4 ✓

72

12.2

31.5 ✓

T.P 0.74

632.15 ✓

12.34

631.41 ✓

69

12.2

19.9 ✓

60

11.9

20.2 ✓

40

12.0

20.1 ✓

450-13

N4610 ✓

4140

11.6

20.5 ✓

60

11.6

20.5 ✓

73

11.9

20.2 ✓

75

3.9

28.2 ✓

80

3.4

28.7 ✓

90

1.0

31.1 ✓

Book

357

69

632.15

N4600 ✓

Book
357
69

4190	3.8	28.3
80	6.3	25.8
77	8.2	23.9
76	11.7	20.4
60	11.1	21.0
40	11.6	20.5

N4590 ✓

Cont. from
Book 450
13

4140	12.5	19.6
42	11.0	21.1
60	11.0	21.1
80	11.2	20.9
81	5.5	26.6
90	2.6	29.5

N4580 ✓

4187	2.4	29.7
85	11.1	21.0
60	10.9	21.2
49	10.5	21.6
40	16.2	15.9

632.15

N4570 ✓

Cont. from
Book 450-14

36

4140	18.1	14.0
52	10.5	21.6
70	10.6	21.5
89	10.9	21.2
92	0.4	31.7

N4560 ✓

Cont. in Book 450
14

4197	0.3	31.8
T.P.	5.65	626.93
93	10.87	621.28
80	5.3	21.6
55	5.2	21.7
40	5.0	21.9
	11.0	15.9

N4550 ✓

Cont. from
Book 450-14

4140	10.6	16.3
60	5.2	21.7
80	5.0	21.9
97	5.0	21.9

Cont. in
Book 357-70

626.93

N4540 ✓

Cont. in
557-70

4180

4.6 22.3 ✓

68

4.1 22.8 ✓

60

5.8 21.1 ✓

50

9.0 17.9 ✓

40

11.6 15.3 ✓ ⁴⁵⁰/₁₄

N4530 ✓

4140

12.3 14.6 ✓

50

10.4 16.5 ✓

60

7.5 19.4 ✓

70

4.7 22.2 ✓

80

4.5 22.4 ✓

90

4.5 22.4 ✓

N4520 ✓

4190

4.3 22.6 ✓ ^{Cont. on}/_{Page 21}

80

4.2 22.7 ✓

70

4.5 22.4 ✓

60

8.0 18.9 ✓

50

10.8 16.1 ✓

40

13.2 13.7 ✓ ^{See FB 450}/_{Page 14 & 40}/₄₁₃₉

626.93

N4510 ✓

Cont. from
Book 450-15

37

4140

13.7 13.2 ✓

50

11.5 15.4 ✓

60

8.6 18.3 ✓

70

6.1 20.8 ✓

80

4.1 22.8 ✓

90

4.1 22.8 ✓

N4500 ✓

Cont. from
Page 21

4190

3.8 23.1 ✓

80

4.4 22.5 ✓

70

7.6 19.3 ✓

60

10.0 16.9 ✓

50

12.2 14.7 ✓

43

13.9 13.0 ✓

T.P. 0.27

Transit
614.36 ✓12.84 614.09 ✓ ^{Cont. in Book}/₄₅₀₋₁₅

4140

11.0 03.4 ✓ ^{Cont. from}/_{B-150-15}

42

14.3 12.6 ✓

50

13.2 13.7 ✓

Level
626.93

626.93

N4490 ✓

4160	11.3	15.6
70	8.7	18.2
80	3.9	23.0
85	0.7	26.2
90	3.3	23.6

N4480 ✓

Cont. Page 23

4190	3.7	23.2
80	7.5	19.4
70	9.7	17.2
60	12.2	14.7
50	14.5	12.4

614.36

46	1.7	12.7
42	11.2	03.2
40	11.4	03.0

Cont. from Book 4470 N

N4470 ✓

Cont. from Book 4470 N

4140	11.8	02.6
45	11.5	02.9
48	2.5	11.9

614.36

N4470 ✓

38

4160	0.7	13.2
	626.93	
70	11.0	15.9
80	9.4	17.5
90	6.0	20.9
95	3.7	23.2

N4460 ✓

4190	9.2	17.7
80	12.8	14.1
	614.36	
70	1.1	13.3
60	3.0	11.4
53	3.6	10.8
48	11.9	02.5
40	12.1	02.3

Plotting of 9-12-34 - 684

Cont. from Book 4470 N

N4450 ✓

4140	12.4	02.0
50	12.4	02.0
53	6.1	08.3

614.36

N4450 ✓

4160	5.5	08.9✓
70	4.6	09.8✓
80	3.6	10.8✓

626.93

Cont on 23

90	11.4	15.5✓
----	------	-------

N4440 ✓

Cont. P. 23

4190	12.0	14.9✓
------	------	-------

614.36

80	6.6	07.8✓
----	-----	-------

70	7.9	06.5✓
----	-----	-------

60	9.0	05.4✓
----	-----	-------

54	8.6	05.8✓
----	-----	-------

51	12.9	01.5✓
----	------	-------

40	12.7	01.7✓
----	------	-------

Cont. from Book 250/15

N4430 ✓

Cont. from Book 450/15

4140	12.9	01.5✓
------	------	-------

53	13.2	01.2✓
----	------	-------

60	13.1	01.3✓
----	------	-------

70	10.4	04.0✓
----	------	-------

614.36

N4430 ✓

4180	8.0	06.4✓
------	-----	-------

90	1.1	13.3✓
----	-----	-------

Cont on Page 24

626.93

N4420 ✓

Cont from P. 25

4230	1.5	25.4✓
------	-----	-------

20	1.9	25.0✓
----	-----	-------

10	1.5	25.4✓
----	-----	-------

4200	8.6	18.3✓
------	-----	-------

4190	14.8	12.1✓
------	------	-------

614.36

80	5.8	08.6✓
----	-----	-------

70	9.6	04.8✓
----	-----	-------

60	12.9	01.5✓
----	------	-------

50	13.5	00.9✓
----	------	-------

4140	13.2	01.2✓
------	------	-------

Cont. Book 450-16

626.93

T.P.	4.86	631.16	0.63	626.30✓
------	------	--------	------	---------

B.M.			1.27	629.89✓ = check on
------	--	--	------	--------------------

B.M. elev. 629.89

614.36

T.P.	11.62	602.74✓
------	-------	---------

N4410 ✓

	13.05	615.79 ✓	602.74	
4140			14.9	00.9 ✓
50			15.2	00.6 ✓
60			14.7	01.1 ✓
70			8.6	07.2 ✓
75			4.3	11.5 ✓
80			5.3	10.5 ✓
90			3.3	12.5 ✓
4200			40.7	16.5 ✓

631.16

10			10.8	20.4 ✓
20			6.1	25.1 ✓
30			5.2	26.0 ✓
40			5.4	25.8 ✓

N4400 ✓

4250			5.2	26.0 ✓
40			5.5	25.7 ✓
32			3.7	27.5 ✓
20			9.7	21.5 ✓

Conti from
Page 26

631.16

N4400 ✓

40

4210			15.6	15.6 ✓
		615.79		
4200			2.3	13.5 ✓
4188			4.9	10.9 ✓
80			2.1	13.7 ✓
71			7.5	08.3 ✓
62			15.2	00.6 ✓
50			15.5	00.3 ✓
40			15.3	00.5 ✓

N4390 ✓

4140			15.5	00.3 ✓
50			15.8	00.0 ✓
62			15.8	00.0 ✓
74			6.1	09.7 ✓
80			6.6	09.2 ✓
90			6.0	09.8 ✓
4200			3.1	12.7 ✓
10			2.4	13.4 ✓

631.16

N4390 ✓

4220	14.0	17.2 ✓
30	7.8	23.4 ✓
37	32	28.0 ✓
40	4.9	26.3 ✓
50	4.9	26.3 ✓
60	4.5	26.7 ✓

N4380 ✓

4270	4.4	26.8 ✓
60	3.5	27.7 ✓
50	3.3	27.9 ✓
40	6.6	24.6 ✓
35	8.8	22.4 ✓

615.79

25	6.3	09.5 ✓
10	12.0	03.8 ✓
4200	11.3	04.5 ✓
4190	11.2	04.6 ✓
80	14.0	01.8 ✓
70	11.7	04.1 ✓

0324 615.79

N4380 ✓

41

4160	16.1	599.7 ✓
50	15.9	99.9 ✓
4140	15.8	600.0 ✓

N4370 ✓

4140	16.1	599.7 ✓
50	16.0	99.8 ✓
60	16.1	99.7 ✓
70	15.1	600.7 ✓
80	13.7	02.1 ✓
90	13.4	02.4 ✓
4200	13.3	02.5 ✓
10	13.6	02.2 ✓
20	12.6	03.2 ✓
35	4.2	11.6 ✓

631.16

40	12.1	19.1 ✓
50	6.8	24.4 ✓
55	4.5	26.7 ✓
70	4.0	27.2 ✓
80	4.1	27.1 ✓

631.16

N4360 ✓

Conti Srom

Page 27

4290

3.6

27.6 ✓

80

1.7

29.5 ✓

70

3.5

27.7 ✓

60

5.6

25.6 ✓

47

10.5

20.7 ✓

615.79

40

7.0

08.8 ✓

30

10.5

05.3 ✓

20

13.6

02.2 ✓

10

13.8

02.0 ✓

4200

13.9

01.9 ✓

4190

14.0

01.8 ✓

80

14.6

01.2 ✓

70

15.6

00.2 ✓

60

16.2

599.6 ✓

50

16.6

99.2 ✓

40

16.5

99.3 ✓

Williams Sept. 19. 33

Osborn

43

Levels on points spanning Cracks above Spillway North Slope

St.	+	x	-	Elev	851.34		
	6.37	857.71	1.17	856.54			
	12.00	868.54					
# 1			7.30	861.24	South	Spk	o
"			7.33	861.21	North	Spk	o
			0.22		868.32	T.P.	
	11.19	879.51					
# 2			4.18	875.33	South	o Spk.	
"			4.11	875.40	North	x on rock.	
			0.54		878.97		
	11.52	890.49					
			0.20		890.29		
	10.73	901.02	0.28		900.74		
	10.11	910.85	0.15		910.70		
	11.77	922.47					
# 3			3.45	919.02	Spk North		
"			3.34	919.13	+ on Rock South		
T.P.			0.08		922.37		
	10.66	933.05	0.33		932.72		
	11.38	944.10					

Levels on points spanning Cracks

44

	+	-	El.	T.P.	
	944.10				
11.06	955.04	0.12		943.98	
		0.225		954.815	
11.49	966.30				
		0.37		965.93	
11.01	976.94				
# 4		4.08	972.86		South side
"		3.95	972.99		North side
		0.89		976.05	T.P.
9.12	985.17				
		0.79	984.38		B.M. on Top of Ridge 984.40
	985.19				(used corrected B.M. going East.)
11.1	974.91	11.39	973.80		
		11.68		963.23	
1.67	964.90				
		12.22		952.68	
0.99	953.67				
		13.04	940.63		✓
1.18	941.81				
		12.64		929.19	✓
0.35	929.54				

Levels on Points Spanning Cracks

	+	x	-	El.	T.P.		
		929.54					
# 6			11.09	918.45		North Spk.	
			11.17	918.37		South Crosson Rock	
T.P.			12.77		916.77		
	0.58	917.35					
			12.47	904.88			
	0.69	905.57					
# 7			11.94	893.63		North Spk	940.63
"			12.06	893.51		Cross on Rock South	5.65
							946.28
N4580 ground			5.9		899.7	Check on Board.	6.32
E 5340							#5 939.96 N Spk
							946.28
							" 6.34 939.94 S Cross Rock

Oct. 19, 1933

Simpson
Salgado
Reimann

46

Check Levels on Points Spanning Cracks above Spillway North Slope

B.M.	12.99	864.33	851.34		
# 1			3.18	861.15	North Spk.
"			3.23	861.10	South Spk.
T.P.			0.41	863.92	
	12.24	876.16			
# 2			0.96	875.20	South Spk. @
"			0.76	875.40	North X on Rock
T.P.			0.96	875.20	
	12.79	887.99			
T.P.			0.31	887.68	
	12.42	900.10			
T.P.			0.74	899.36	
	12.43	911.79			
T.P.			1.09	910.70	
	12.76	923.46			
# 3			4.32	919.14	South X on Rock
"			4.41	919.05	North Spk. @
Set B.M.			1.64	921.82	Point of Rock 50' N.W. of Points #3

Oct. 19, 1933.

47

Check Levels on Points Spanning cracks

B.M.	12.32	934.14		921.82	
T.P.			0.86	933.28	
	12.40	945.68			
T.P.			0.63	945.05	
	12.46	957.51			
T.P.			0.60	956.91	
	12.66	969.57			
T.P.			0.44	969.13	
	11.96	981.09			
#4			8.23	972.86	South Spk. ⊙
"			8.11	972.98	North Spk. ⊙
T.P.			1.94	979.15	
	7.65	986.80			
B.M.			2.40	984.40 = B.M.	on top of Ridge Rec. elev. 984.40
T.P.			12.72	974.08	
	1.25	975.33			
T.P.			13.14	962.19	
	0.59	962.78			
T.P.			13.05	949.73	

Oct. 19, 1933.

Check Levels on Points Spanning Cracks

T.P.	0.37	950.10	949.73
#5			10.17 939.93
"			10.16 939.94
T.P.			13.13 936.97
	1.17	938.14	
B.M.			1.84 936.30 on
T.P.			13.09 925.05
	0.64	925.69	
#6			7.32 918.37
"			7.26 918.43
T.P.			12.87 912.82
	0.97	913.79	
T.P.			12.66 901.13
	3.02	904.15	
#7			10.63 893.52
"			10.51 893.64
Set B.M.			2.54 901.61 on

48

South X on Rock

North Spk. ⊙

Boulder 60[±] N.E. of Point #5. Rec. Elev. 936.29

South X on Rock

North Spk. ⊙

South X on Rock.

North Spk. ⊙

Boulder 80[±] N.E. of Point #7.

Nov. 14, 1933.

Simpson
Remmen.

49

Check Levels on Points Spanning Cracks

Above spillway North Slope.

B.M.	11.70	863.04	851.34		
# 1			1.90	861.14	No. spk.
"			1.96	861.08	So. spk. in Moun.
T.P.	12.82	875.65	0.21	862.83	
# 2			0.24	875.41?	No. X on Rock
"			0.47	875.18	So. spk. in Moun.
B.M.	3.36	925.18		921.82	
# 3			6.13	919.05	No. spk. in Moun
"			6.04	919.14	So. X on Rock
B.M.	0.32	984.72		984.40	
# 4			11.73	972.99?	No. spk. in Moun.
"			11.86	972.86-	So. spk. in Moun.

Nov. 14, 1933

50

Check Levels on Points Spanning Cracks.

B.M.	9.10	945.40	-	936.30
------	------	--------	---	--------

5

5.46 939.94

No. Spk. in Moun.

"

5.47 939.93

So. X on Rock.

B.M.	0.645	936.945		936.300
------	-------	---------	--	---------

T.P.

10.150 926.793

0.815 927.610

6

9.19 918.42

No. spk. in Moun.

"

9.26 918.35

So. X on Rock.

B.M.	1.55	903.16		901.61
------	------	--------	--	--------

7

9.64 893.52

So. X on Rock.

"

9.53 893.63

No. Spk. in Moun.

Check Levels on Points Spanning Cracks above
Spillway North Slope.

B.M.	10.98	862.32	851.34	
#1		1.20	61.12	N.
"		1.28	61.04	S.
T.P.		1.28	861.04	
	10.08	871.12		
T.P.		0.79	870.33	
	10.61	880.94		
#2		5.82	875.12	S.
"		5.57	875.37	N.
B.M.	2.87	924.69	921.82	
#3		5.64	19.05	N.
"		5.57	19.12	S.
B.M.	0.55	984.95	984.40	
#4		11.94	73.01	N.
"		12.08	72.87	S.

Jan. 15, 1934
Simpson
Osborne.

57

B.M.			936.30	
	2.49	944.79		
#5		4.86	939.93	N.
"		4.88	39.91	S.
T.P.		0.85	943.94	
	11.66	955.60		
T.P.		2.53	953.07	
	8.695	961.765		
Point "A"		8.910	952.855	
B.M.	0.78	937.08	936.30	
T.P.		11.83	925.25	
	2.47	927.72		
#6		9.37	918.35	S.
"		9.29	18.43	N.
B.M.	1.59	903.20	901.61	
#7		9.68	93.52	S.
"		9.56	893.645	N.

Elev. of Point "A" in center of P
mass above spillway cut. Feb 26, 1934

52

Elliot
Soper
Remmen.

B.M.	10.615	946.915		936.30
	9.565	954.625	1.855	945.06
	8.50	963.025	0.100	954.525
Monument "A"		10.190		952.835

Total outward movement = 0.21'

Oct. 29-1934

Simpson
Soper
Jebell

B.M.	12.35	948.65 ✓		936.30
			0.37	948.28 ✓
	10.81	⁹ 959.09 ✓		
Monument "A"		6.29	⁹	952.80 ✓

~~10.81~~
Total outward movement = 0.31'

55

57

X Sections of Upstream Spoil Area.
continued from page 20, this book.

B.M.	0.03	693.32 ✓		693.30
T.P.	0.48	680.93 ✓	12.88	680.45 ✓
Set B.M.	1.19	^{Level} 669.93 ✓	12.19	668.74 ✓
T.P.	0.44	^π 657.80 ✓	12.57	657.36 ✓

^{Level}
669.93

N 3550

6670		1.4	68.5
60		1.5	68.4
50		1.6	68.3
40		1.7	68.2
30		1.5	68.4
25		1.4	68.5
20		3.6	66.3
10		10.6	59.3
	^π 657.80		
6600		3.6	54.2
90		8.6	49.2
6580		15.8	42.0

↓ interpolate for section west.

Aug. 25, 1933

Simpson
Super
Remmen.

^π
657.80

N 3540

60

6434		38.8	619.0 ✓
40		36.6	21.2 ✓
50		33.0	24.8 ✓
60		30.2	27.6 ✓
70		27.9	27.9 ✓
80		25.8	32.0 ✓
90		22.9	34.9 ✓
6500		20.7	37.1 ✓
10		20.0	37.8 ✓
20		19.0	38.8 ✓
30		17.0	40.8 ✓
40		16.4	41.4 ✓
50		17.3	40.5 ✓
60		19.4	38.4 ✓
70		22.4	35.4 ✓
80		17.1	40.7 ✓
90		11.2	46.6 ✓
6600		6.8	51.0 ✓
10		1.8	56.0 ✓

Level
669.93

N 3540

6620	7.5	62.4 ✓
25	1.8	68.1 ✓
40	2.0	67.9 ✓
50	2.4	67.5 ✓
60	2.5	67.4 ✓
70	2.3	67.6 ✓

N 3530

6680	3.0	66.9
70	3.3	66.6
60	3.2	66.7
50	2.7	67.2
40	3.0	66.9
35	3.0	66.9
30	5.8	64.1
20	11.2	58.7
10	3.2	54.6
6600	8.7	49.1
90	13.3	44.5

π
657.80

657.80

N 3530

T.P.	0.34	Level 645.06 ✓	13.08	644.72 ✓
6580			5.3	39.8
70			9.7	35.4
60			10.1	35.0
50			7.6	37.5
40			7.7	37.4
30			8.0	37.1
20			9.1	36.0
10			10.9	34.2
6500			11.5	33.6
90			12.3	32.8
80			14.5	30.6
70			16.6	28.5
60			18.9	26.2
50			21.3	23.8
6443			23.5	21.6

Level
645.06

N3520

6450	31.2	13.9
58	20.8	24.3
70	18.8	26.3
80	16.7	28.4
90	15.4	29.7
6500	15.0	30.1
10	13.9	31.2
20	13.1	32.0
30	12.7	32.4
40	12.5	32.6
50	13.0	32.1
60	14.8	30.3
65	9.4	35.7
70	8.8	36.3
80	7.6	37.5
90	14.5	43.3
6600	10.7	47.1
10	5.5	52.3

*
657.80

T

657.80

N3520

6620	3.5	54.3
30	+1.9	59.7
40	+6.4	64.2
45	+8.4	66.2
50	+8.8	66.6
60	+8.4	66.2
70	+8.3	66.1
80	+8.2	66.0

N3510

6690	+7.5	65.3
80	+7.6	65.4
70	+7.7	65.5
60	+6.1	63.9
50	+3.0	60.8
40	0.7	57.1
30	4.7	53.1
20	5.5	52.3
10	7.7	50.1
6600	13.8	44.0

Level
645.06

N 3510

6590	5.2	39.9
80	9.4	35.7
70	13.4	31.7
60	19.0	26.1
50	20.5	24.6
40	17.9	27.2
30	17.2	27.9
20	17.2	27.9
10	17.5	27.6
6500	18.0	27.1
90	18.6	26.5
6480	32.6	12.5

N 3500

6530	29.6	15.5
40	28.3	16.8
50	23.2	21.9
60	21.3	23.8
70	16.6	28.5
80	11.6	33.5

Level
645.06

N 3500

6590	7.1	38.0
	π 657.80	
6600	16.0	41.8
10	13.6	44.2
20	10.6	47.2
30	8.7	49.1
40	6.5	51.3
50	3.7	54.1
60	1.7	56.1
70	+0.8	58.6

N 3490

6670	6.2	51.6
60	9.0	48.8
50	9.3	48.5
40	11.4	46.4
30	12.8	45.0
20	11.7	46.1
	Level 645.06	
10	2.4	42.7

Level
645.06

N 3490

6600	1.8	43.3
6590	9.0	36.1
80	13.0	32.1
70	25.5	19.6
60	26.3	18.8

N 3480

6570	26.1	19.0
80	25.2	19.9
85	24.7	20.4
90	10.4	34.7
6600	5.4	39.7
10	4.5	40.6
20	5.0	40.1
30	3.3	41.8
40	2.7	42.4
50	3.0	42.1
60	2.8	42.3
70	+1.8	46.9

Level
645.06

N 3470

6670	4.3	40.8
60	6.2	38.9
48	8.2	36.9
40	12.5	32.6
30	13.6	31.5
20	13.6	31.5
10	12.0	33.1
07	10.8	34.3
6600	18.6	26.5
6590	23.6	21.5

N 3460

6630	19.3	25.8
40	18.3	26.8
45	11.7	33.4
50	12.3	32.8
60	10.4	34.7
70	7.1	38.0

645.06

N 3450

6670

11.0

34.1

60

16.8

28.3

50

19.2

25.9

40

19.6

25.5

65

Feb. 8 1934
Simpson
Soper
Remmen

Sections of Spoil Area For
Material Wasted from "Hog Box"

B.M.	4.50	754.47	749.97	Sta. 4+76 Crest Sta.
T.P.		7.43	747.04	
	0.71	747.75		
T.P.		12.58	735.17	
	0.49	735.66		
Set B.M.		9.93	725.93	Spike in Bank 30' East of Powder House
	0.93	726.66		

E 5880

NA100	5.7
4090	6.1
85	4.2
80	7.0
70	8.3
60	7.6
52	8.5

66

RUCE YOUNG

Automotive Electrician

Phone Fr. 4104

SAN DIEGO, CALIFORNIA

"Friendly Service"

9/14/34

Not Necessary

Reduce or flat

these notes at present

↑

G.W.C.

W.W.

Pages 66-79

Feb. 8 1934

Simpson
Soper
Remmen

66

Sections of Spoil Area For
Material Wasted from "Hog Box"

					726.66	E 5870
				4055		8.7
B.M.	4.50	754.47	749.97	Sta. 4+76 Crest Sta.	65	9.2
T.P.		7.43	747.04		80	9.7
	0.71	747.75			94	4.1
T.P.		12.58	735.17		97	5.7
	0.49	735.66			4110	5.4
Set B.M.		9.93	725.93	Spike in Bank 30' East of Powder House		
	0.93	726.66				E 5860
				4110		5.2
		E 5880		03		5.4
N 4100		5.7		4100		5.0
4090		6.1		4090		11.1
85		4.2		70		10.9
80		7.0		59		9.2
70		8.3				
60		7.6				
52		8.5				

	726.66	E5850	
4061		11.2	
70		12.4	
90		13.4	
4100		7.2	
03		5.3	
10		5.0	
20		4.7	
B.M.		0.93	725.73

Feb. 9, 1934

B.M.	1.29	727.02	725.73
		E5840	
4120		5.0	
10		4.5	
03		5.7	
T.P.	0.46	^{Transit} 714.43	13.05 713.97
4093		2.0	
85		2.9	
4063		0.9	

	714.43	E5830
4065		2.8
80		4.0
91		4.4
	727.02	
4100		10.8
05		5.2
15		4.9
25		4.7

E5820

4125		4.6
15		5.0
07		5.0
4100		12.8
	714.43	
4093		5.9
85		6.0
67		4.7

714.43 E5810
4061 6.9
67 5.6
75 6.9
93 7.9

727.02
4102 8.0
10 3.9
15 4.8
30 4.3

E5800
4135 4.1
25 4.4
20 4.1
11 3.2
05 5.3

714.43
4096 9.6
85 9.3
75 8.6
4058 8.7

68
714.43 E5790
4060 9.1
70 9.5
85 10.9
98 11.3
4101 7.6

727.02
07 6.4
15 3.5
20 4.2
30 4.0

E5780
4140 3.7
25 3.9
15 4.4
10 9.6

714.43
05 8.5
4100 13.0

714.43

E5780

4085

12.7

70

11.4

62

10.6

58

12.5

E5770

4060

12.7

65

11.6

80

14.1

4102

15.0

07

11.7

727.02

14

12.1

24

4.7

30

3.5

40

3.5

E5760

4150

3.1

35

3.3

27

4.0

714.43

E5760

4110

13.6

05

16.6

4090

16.4

75

15.7

64

12.7

E5750

4066

16.9

80

17.7

4100

18.3

10

17.1

17

9.1

727.02

25

15.0

31

4.2

36

2.7

30

2.8

727.02

E 5740

4150

2.5

37

2.2

714.43

21

8.5

18

14.3

08

19.9

4090

19.5

4073

19.4

E 5730

4075

20.9

85

21.1

4100

21.5

10

21.4

20

14.1

24

8.3

727.02

44

2.0

60

1.9

727.02

E 5720

4160

1.4

4148

2.0

714.43

4125

10.6

4112

21.3

10

23.2

4095

23.1

4079

22.7

E 5710

4078

23.1

85

24.4

4100

24.7

10

24.8

21

18.4

29

8.3

727.02

51

1.3

70

0.8

	727.02	E 5700
4170		0.3
155		0.6
148		4.8
	714.43	
138		3.3
128		11.9
	701.75	
112		13.6
4100		13.6
4085		13.1

	727.02	E 5690
T.P.	4.64	731.35
		0.31
		726.71
4175	Rd.	4.0
59		4.9
47		12.3
	714.43	
4130		11.2

	689.08	E 5690
4127		+5.2
13		2.7
4100		2.5
4085		2.0
	731.35	E 5680
4180	Rd.	3.3
66		3.8
50		14.3
	714.43	
33		11.5

	689.08
4126	+0.6
19	3.4
15	4.1
4100	3.8
4085	3.5
4079	3.7

		731.35	E 5670
4185	Rd.		2.6
71			2.8
		714.43	
50			1.9
32			15.1
		689.08	
26			2.2
20			5.2
4105			5.4
4090			5.0
81			5.4
		731.35	E 5660
4190	Rd.		1.8
78			2.5
74			1.4
65			9.0
		714.43	
50			4.0
30			18.9

72

		689.08	E 5660
4126			1.7
20			6.7
4100			6.6
4082			7.7
		731.35	E 5650
4195	Rd.		1.1
80			2.0
65			11.1
		714.43	
50			4.6
30			18.3
		689.08	
26			4.0
20			7.8
4100			7.9
4083			8.9

	731.35	E 5640	
4200 Rd		0.4	
4185		1.4	
70		11.7	
	714.43		
50		7.7	
34		15.4	
	689.08		
34		2.4	
22		9.5	
4105		9.3	
4085		9.7	
	731.35	E 5630	
4200 Rd		+0.2	731.6
4190		0.7	730.7
75		10.9	720.5
	714.43		
60		4.0	710.4
50		9.4	705.0
38		14.6	699.8

	689.08	E 5630	
4135		5.0	684.1
26		9.5	679.6
20		10.7	678.4
4005		10.7	678.4
4086		10.8	678.3
	731.35	E 5620	
4200		+0.7	732.1
4195		+0.5	731.9
75		14.8	716.6
	714.43		
62		6.6	707.8
50		9.6	704.8
40		13.4	701.0
	689.98		
37		6.9	683.9
30		9.1	680.9
20		11.9	678.1
4100		12.9	677.1
4087		13.1	676.9

Dec. 9-1934 C.B.H.

Dec. 13-1934 F.O.

Reduced & Checked

Checked

731.35

E 5610

4210

+ 2.1

733.5 ✓

0.05

701.75

701.70

4198

+ 1.5

732.9 ✓

T.P.

13.00

688.75

80

12.8

718.6 ✓

0.33

689.08

714.43

60

9.9

704.5 ✓

T.P.

0.33

688.75

45

14.4

700.0 ✓

1.23

689.98

689.98

E 5600

43

3.3

686.7 ✓

A 130

3.2

20

11.8

678.2 ✓

A 110

12.4

4105

13.4

676.6 ✓

A 096

14.6

4091

14.2

675.8 ✓

T.P.

12.34

677.64

Set stab

N 4090 - E 5630

731.35

E 5600

4210

+ 2.8

02

+ 2.2

4185

11.4

714.43

70

7.2

50

18.2

T.P.

12.73

701.70

Feb. 14, 1934

Simpson
Super
Remmen:

7.5

670.52 E 5870

B.M.	1.10	726.83	725.73
T.P.			12.97 713.86
	0.12	^{Level} 713.98	
T.P.			12.99 700.99
	0.49	701.48	
		713.98	E 5880
N 4050		+1.1	
40		6.1	
30		13.8	
		701.48	
20		8.5	
10		15.5	
4000	See Pg. 79-682.86	2.9	
3990		7.1	
80		12.3	
	See Pg. 79-670.52		
70		3.3	
60		11.1	
50		16.2	

3948	18.6
60	11.0
70	7.6
80	1.9
90	9.8
4000	5.0
4010	17.8
20	10.7
30	3.7
	713.98
40	8.5
50	0.6
	E 5860
4050	1.9
40	10.1
	701.48
30	5.1
20	12.8

682.86

E5860

713.98

E5850

4010

2.2

4050

5.5

4000

7.8

E5840

3990

10.5

4060

2.2

670.52

50

9.3

80

3.8

701.48

70

7.8

40

3.8

60

14.1

30

9.8

3948

21.4

20

15.2

E5850

682.86

3953

19.2

10

40.9

60

16.1

4000

7.4

70

11.9

3990

670.52

3.6

80

5.1

80

9.3

682.86

90

13.3

70

14.0

4000

7.5

3965

16.6

10

4.3

E5830

4020

701.48

14.8

3965

20.2

30

7.8

72

13.8

40

0.4

80

11.0

90

4.6

682.86

E5830

4000

9.4

10

0.8

701.48

4020

17.9

30

13.5

40

6.9

713.98

50

12.4

E5820

4060

9.0

701.48

50

3.3

40

10.2

T.P.

12.49

688.99

0.76

Level
689.75

30

4.7

20

7.5

10

14.8

689.75

E5820

4000

23.5

3990

24.8

82

28.9

E5810

3987

30.7

90

27.8

4000

23.9

10

20.2

20

11.2

30

6.0

40

0.2

701.48

50

4.8

60

+4.4

E5800

4055

+2.9

50

2.1

40

11.0

	689.75	E5800
4030		6.5
20		14.0
10		18.9
4000		24.2
3992		27.1

E5790

3994		26.3
4000		23.4
10		14.4
20		11.0
30		5.9

701.48

40		11.4
50		4.4

E5780

4050		5.6
40		12.3
	689.75	
30		6.0

	689.75	E5780
4020		11.2
10		16.8
4000		23.6
3997		24.9

E5770

4000		23.4
10		17.0
20		8.8
30		6.1
40		3.0

701.48

50		7.7
----	--	-----

E5760

4060		3.6
50		10.3
	689.75	
40		5.5
30		8.5
20		11.4

	689.75	E 5760
4010	17.5	
4002	23.4	
		E 5750
4007	23.7	
10	22.5	
20	17.3	
30	12.7	
40	7.9	
	701.48	
50	13.9	
60	7.5	

	689.75	
Set T.P. on Boulder	9.20	680.55
T.P.	5.95	682.86
		12.84
		676.91
T.P.		12.37
		670.49
	0.03	670.52

Feb. 15, 1934

Simpson
Japer
Bommer

79

T.P.	8.98	Transit 689.53	680.55	N4020 E 5760
T.P.			12.56	676.97
	0.46	Level 677.43		
		689.53		E 5740
A060			0.7	
50			5.4	
40			10.1	
		677.43		
30			2.6	
20			6.3	
4013			9.4	
				E 5730
4017			9.7	
20			8.8	
30			5.4	
40			1.5	
		689.53		
50			10.0	
60			6.5	
70			0.7	

continued in Book #458-Pg. 1

Note from N 4840
on south section
Run west to top of
bank on quarry Rd.

