W[illegible]

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[illegible]

449

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

CHICAGO, ILL.

MICROFILMED

JAN 12 1965

D 662

U 650

Tile to Δ = 144'

Left 48'

Curve 32'

MICROFILMED

Profile of core wall for Est. #15 page 1

X Sections of Rock Emb. Est #15 p 1-4

" " " " " 27 " 43-46

Typical Hy Fill Sec Est 15 Page 5

17 " 14

27 " 43-46

30 " 47-48

X Section Down Stream Spoil Est 15 " 6-7

" 16 " 10-11½

" 17 " 12-14

" 18 " 18-21

" 19 " 22-25

" 20 " 27-30

" 21 " 31-32

" 22 " 33-35

" 23 " 38-39

" " " " After Nov. 16, 34 " 57+69

" " " " Finals 70-73

X Section Upstream Spoil Est 16 7-10

" 18 15-18

" 23 36-37

" 24 39-41

" 25 45

X Section of Plaza N end Dam to West Prior to Placing D.G. 50-53

Fence location around Plaz 54

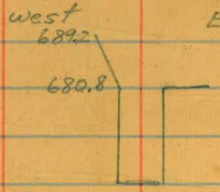
Estimate of Down stream Rock Emb N 4040 to Eyler. 770 Plaza 55

Profile of core wall
for Monthly Est. #15
Aug 1 - 1933

698.99

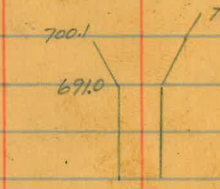
12.73 686.26

4.38 690.64

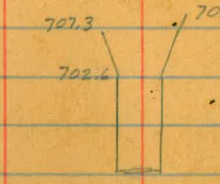


N3120 13.8 676.8

3110 13.3 677.3

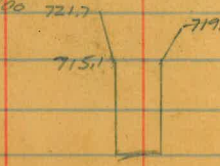


3100 11.0 679.6



3080 3.3 87.3

3075 3.4 87.2

3075 Too 

0.2 90.4

3070 +2.1 92.7

3060 +3.2 93.8

Upstream Rock Emb.
for No. Estimate #15 Aug 1 - 1933

1

N3160 is O.G.

666.2

N3180

5177 3.4 62.8

5230 4.4 61.8

5255 9.0 57.2

N3200

5265 14.3 51.9

40 4.8 61.4

5220 4.2 62.0

5177 3.3 62.9

N3220

5177 3.3 62.9

5235 4.4 61.8

5270 15.1 51.1

N3240

5280 ± 650.0

5270 ± 650.0

5255 9.8 56.4

5240 5.1 61.1

5220 3.7 60.5

5177 3.5 62.7

N3280

5177 3.9 62.3

5215 4.3 61.9

5225 2.6 63.6

Plotted Aug 3, - R.F.L. & F.O.

	666.2	N 3280 ✓
5255	9.7	56.5
5270 ?		650.0
5280 ?		650.0 ✓
		N 3320 ✓
5280 ?		650.0
5270	17.1	49.1
5255	10.2	56.6
5230	3.4	62.8
5220	4.9	61.3
5177	4.5	61.7
		N 3360 ✓
5177	4.5	61.7
5225	5.3	60.9
5240	4.6	61.6
5253	9.1	57.1
5265	18.5	47.7
5280 ?		650.0 ✓
		N 3400 ✓
5280 ?		650.0
5270	16.3	49.9
5255	12.6	53.6
5230	5.2	61.0
5210	4.5	61.7
5177	4.3	61.9

	666.2	✓
		N 3440
5177	4.3	61.9
5220	5.1	61.1
5235	3.5	62.7
5251	9.0	57.2
5265	18.6	47.6
5280 ?		650.0 End Angle
	0.0	663.1 ✓
		N 3480 Start Angle
5177	1.5	61.6
5220	2.0	61.1
5264	8.3	54.8
5271	13.2	49.9
5280 ?		650.0
		N 3520 ✓
5280 ?		650.0
70	15.0	48.1
60	8.4	54.7
30	2.8	60.3
5210	1.7	61.4
5177	1.5	61.6

663.1

5177
5220
35
62
70
5280?

5280?
67
60
40
20
5177

5177
5220
60
67
5280?

5280?
65
55
5230
5177

N3560

1.2	61.9
2.3	60.8
2.7	60.4
8.0	55.1
14.2	48.9
	650.0

N3600

	650.0
14.0	49.1
7.7	55.4
3.3	59.8
2.4	60.7
1.1	62.0

N3640

0.8	62.3
1.9	61.2
8.4	54.7
14.7	48.4
	650.0

N3680

	650.0
15.2	47.9
6.6	56.5
2.3	60.8
1.5	61.6

663.1

5177
5220
50
62
5280?

5280?
5265
52
40
5220
5177

5177
5220
51
60
75
5280?

5280?
75
60
50
5220
5177

N3720

2.4	60.7
2.8	60.3
5.6	57.5
15.0	48.1
	650.0

N3760

	650.0
15.0	48.1
7.5	55.6
5.3	57.8
4.8	58.3
3.8	59.3

N3800

4.0	59.1
4.1	59.0
5.4	57.7
16.2	46.9
16.2	46.9
	650.0

N3840

	650.0
16.2	46.9
16.2	46.9
5.9	57.2
4.1	59.0
3.5	59.6

663.1

N3880 ✓

5177	
5220	
55	
67	
5280?	
	668.1
5280?	
77	
67	
56	
5220	
5177	
5177	
5220	
43	
67	
5280?	

2.6	60.5
3.4	59.7
5.4	57.7
15.2	47.9
	650.0

N3920 ✓

	650.0
20.2	47.9
20.4	47.7
9.2	58 9
7.6	60.5
7.0	61.1

N3960 ✓

6.6	61.5
7.1	61.0
6.4	61.7
21.2	46.9
	650.0

5295	← → Finished to toe
5280?	
60	
43	
5220	
5177	
5177	
5220	
35	
67	
5295	← → Finished to toe
5220	
5235	
5220	
5177	
5177	
5233	

No reckon N4070

668.1

N4000 ✓

21.7	46.4
21.7	46.4
7.3	60.9
6.3	61.8
6.0	62.1 ✓

N4040

3.2	64.9
4.0	64.1
4.4	63.7
	644.9

N4060

644.9 Toe

2.5	65.6
2.0	66.1
1.2	66.9

New H.T 673.1

N4080 ✓

4.4	68.7
3.2	69.9 Toe

Typical Section of Hyd. Fill
For Mo. Estimate Aug 2. 1933

Taken on N3620

	0.0	663.8	663.8
5172		1.9	61.9
5165		11.1	52.7
5120		13.7	50.1
5077			648.4 Water Surf.
4927			648.4 Water Surf
4835		11.0	52.8
4817		1.8	52.0
4800		1.8	62.0

Plotted Aug. 3

F.O. & REL.

Xsections of Downstream Spoil for Est. #15 Aug 4 - 1933
Elliott-Simpson-Soper Remmen

B.M.	10.91	707.27		696.36

N4430 is O.G.

✓N4440

4625				O.G
4600			15.8	691.5
4470				O.G

✓N4460

4655				O.G
4600			0.0	707.3
T.P.	12.52	719.49	0.30	706.97
T.P.	2.82	721.10	1.21	718.28
4435				O.G.

✓N4480

4650		721.10		O.G
4620			0.9	20.1
4595			3.6	17.5
4540			14.4	06.7
4480			27.7	93.4
		679.2		
4430			4.9	74.3
4415			11.9	67.3 O.G

679.2

✓N4500

4406	6.2	73.0	O.G.
4450	+16.8	96.0	
721.10			
4480	14.7	06.4	
4525	5.3	15.8	
4605		O.G	

✓N4520

4580		O.G.	
4460	8.9	12.2	
4450	12.6	08.5	
679.2			
4390	2.2	77.0	O.G

✓N4530

4398	0.8	678.4	O.G.
4450	721.10 8.9	712.2	
4570		O.G	

✓N4550

4530		O.G	
4440	9.3	11.8	
B.M.	11.88	679.16	667.28
4400	+2.8	82.0	O.G.

		721.10	N4570.	
4500				O.G
4440			10.5	710.6
T.P.	0.21	709.04	12.27	708.83
4407			20.2	688.8 O.G
		N4590 is O.G.		
T.P.			12.74	696.30

X Sections of Upstream Spoil for Est. #16 – Aug. 31, 1933.

7.

B.M.	12.97	708.57	695.60
		N 3940 is O.G.	
		N 3920	
6162		16.2	692.4 O.G
6175		7.2	701.4
6225		3.8	4.1
6255			O.G.
		N 3900	
6283			O.G.
6255		1.4	707.2
6195		4.7	3.9
6152			O.G.
		N 3880	
6150			O.G.
6220		2.8	705.8
6260		1.5	7.1
6283		0.5	8.1
6318			O.G
		N 3860	
6351			O.G
6310		0.2	8.4
6280		1.1	7.5
6250		1.7	6.9
6225		10.5	698.1
6152			O.G.

		708.57	N3840	
6161			O.G.	✓
6210		29.3	679.3	✓
6278		1.8	706.8	✓
6320		1.3	707.3	✓
6345		1.3	707.3	✓
6380			O.G.	✓
			N3820	
6400			O.G	✓
6386		16.5	692.1	
6362		0.3	708.3	✓
6345		0.4	8.2	✓
6280		13.6	695.0	✓
6168			O.G.	✓
B.M.	2.69	695.99		693.30
			N3800	
6425			O.G.	✓
6400		5.6	690.4	✓
6380		3.2	93.8	✓
6360		+3.4	699.4	✓
6320		9.2	86.8	✓
6280		15.1	80.9	✓
6250		25.6	70.4	✓
6172			O.G.	✓

		695.99	N3780	
6163			O.G	✓
6260		34.5	661.5	✓
6280		29.7	66.3	✓
6320		23.0	73.0	✓
6350		4.3	91.7	✓
6400		5.2	90.8	✓
6435		4.7	91.3	✓
6440			O.G.	✓
			N3760	
6460			O.G.	✓
6448		4.4	91.6	✓
6420		5.6	90.4	✓
6380		5.2	90.8	✓
6355		4.8	91.2	✓
6300		41.5	54.5	✓
6265		48.1	47.9	✓
6215			O.G.	✓
			N3740	
6250			O.G	✓
6280		57.8	638.2	✓
6370		4.9	91.1	✓
6400		5.1	90.9	✓
6440		4.7	691.3	✓
6462		3.3	92.7	✓
6480			O.G.	

N3720

B.M.	2.60	695.90	693.30	
6495			O.G.	✓
6476		1.6	694.3	✓
6440		4.0	91.9	✓
6407		4.2	91.7	✓
6355		24.3	71.6	✓
6270			O.G.	✓

N3700

6275		O.G	✓
6335	47.8	48.1	✓
6440	3.5	92.4	✓
6460	3.1	92.8	✓
6493	1.5	94.4	✓
6514		O.G.	✓

N3680

6538		O.G.	✓
6512	1.2	94.7	✓
6457	2.6	93.3	✓
6420	25.0	70.9	✓
6338	59.4	36.5	✓
6283		O.G.	✓

695.90

N3660

6356		O.G.	✓
6380	53.1	42.8	✓
6410	41.9	54.0	✓
6469	1.9	94.0	✓
6527	0.5	95.4	✓
6558		O.G.	✓

N3640

6580		O.G.	✓
6545	0.0	695.9	✓
6490	1.6	94.3	✓
6465	12.3	83.6	✓
6380		O.G.	✓

B.M.	6.23	699.53	693.30

N3620

6390		O.G.	✓
6470	26.0	73.5	✓
6514	4.5	95.0	✓
6560	3.2	96.3	✓
6591		O.G.	✓

N3600

6598		O.G	✓
6555	4.3	95.2	✓
6540	4.2	5.3	✓
6520	11.4	88.1	✓
6400		O.G.	✓

Cross-sections of Downstream Spoil for Est. #16 Sept. 1, 1933

699.53 N3580

6420		O.G.	✓
6510	28.1	71.4	✓
6535	20.4	79.1	✓
6555	18.4	81.1	✓
6600		O.G.	✓

671.7 N3560

6450		O.G.	✓
6505	15.5	56.2	✓
6545	7.4	64.3	✓
6560	7.6	64.1	✓
6594		O.G	✓

N3540

6585		O.G.	✓
6560	22.8	48.9	✓
6520	26.5	45.2	✓
6475		O.G.	✓

N3520 is O.G.

B.M.	12.46	680.88		668.42	
T.P.	11.81	692.52	0.17	680.71	
T.P.	12.55	704.52	0.55	691.97	
Set B.M.			2.82	701.70	Spike in Bank

N4730 is O.G. ✓

N4710 ✓

4335	3.8	700.7	O.G.	✓
4305	3.0	701.5		✓
4275			O.G.	✓

N4690 ✓

4350	2.7	701.8	O.G.	✓
4320	2.8	701.7		✓
4271			O.G.	✓

N4670 ✓

4272			O.G.	✓
4330	5.7	698.8		✓
4345	1.8	702.7		✓
4360			O.G.	✓

T.P.	12.81	716.87	0.46	704.06
Set B.M.			3.17	713.70

716.87

4380			
4357	1.1	715.8	✓
4340	0.6	716.3	✓
4265			O.G. ✓

Sept 2 – 1933

N4630 ✓

B.M.	5.36	719.06	
4233		713.70	O.G ✓
4325	2.6	716.5	✓
4380	4.3	714.8	✓
4405			O.G ✓

N4610 ✓

4425			O.G ✓
4405	4.7	714.4	✓
4360	4.6	14.5	✓
4330	3.0	16.1	✓
4217			O.G ✓

N4590 ✓

4212			O.G ✓
4313	4.1	715.0	✓
4360	5.3	13.8	✓
4435	6.9	12.2	✓
4445			O.G ✓

719.06

N4570 ✓

4500			O.G. ✓
4450	9.1	710.0	✓
4350	5.6	13.5	✓
4318	4.0	15.1	✓
4214			O.G. ✓

N4550 ✓

4213			O.G ✓
4330	4.4	714.7	✓
4350	5.8	13.3	✓
4450	8.1	11.0	✓
4520			O.G ✓

N4530 ✓

4560			O.G ✓
4500	7.3	711.8	✓
4450	7.5	11.6	✓
4350	5.2	13.9	✓
4325	14.6	045	✓
4220			O.G ✓

B.M. 4.43 718.13 713.70

N4520 ✓

4585			O.G. ✓
4550	4.8	713.3	✓
4420	6.8	11.3	✓
4365	4.6	13.5	✓
4325	19.8	698.3	✓
4220			O.G ✓

718.13

N4500 ✓

4630			O.G. ✓
4560	2.3	715.8	✓
4470	5.2	712.9	✓
4370	16.9	701.2	✓
4320	33.7	684.4	✓
4220			O.G. ✓

N4480 ✓

4650			O.G. ✓
4590	0.9	717.2	✓
4515	11.6	706.5	✓
4370	32.0	686.1	✓
4315	47.0	671.1	✓
4235			O.G. ✓

Sept 5 - 1933

B.M.	11.38	707.74	696.36

N4460 ✓

4650			O.G. ✓
4600	1.8	705.9	✓
4535	15.4	692.3	✓
B.M.	0.94	697.30	696.36
4500	7.2	690.1	✓
4440	17.6	679.7	✓
4350	28.6	68.7	✓
4300	46.5	50.8	✓
4250			O.G. ✓

697.30

N4440 ✓

4287			O.G. ✓
4360	41.8	655.5	✓
4480	26.3	71.0	✓
4550	16.6	80.7	✓
4600	6.1	91.2	✓
4625			O.G. ✓

N4430 is O.G. ✓

Simpson
Sagado
McHugh

Cross-Sections of Down Stream Spoil, For Est. #17 — Oct. 2-1933

B.M. 7.35 721.05 713.70

N 4730 is O.G.

N 4720

E 4200 Toe
4270
4290
4309

O.G.
22.8 698.3
18.0 703.1 ✓
20.4 700.7 O.G.

N 4700

4160 Toe
4270
4295
4329 Toe

O.G.
10.5 710.6
5.5 715.6 ✓
O.G.

N 4680

4353 Toe
4315
4263
4120 Toe

O.G.
4.2 716.9 ✓
5.5 715.6
O.G.

N 4660

4100 Toe
4257
4342
4370

O.G.
6.5 714.6 ✓
4.0 717.1
O.G.

721.05

N 4640

4392
4365
4317
4240
4095 Toe

O.G.
5.5 715.6
5.3 15.8 ✓
7.1 14.0
O.G.

N 4620

4090 Toe
4230
4320
4390
4412 Toe

O.G.
8.9 712.2
6.0 15.1 ✓
5.7 15.4
O.G.

N 4600

4446
4430
4380
4330
4230
4095 Toe

O.G.
7.9 713.2
6.7 14.4 ✓
6.8 14.3
9.3 11.8
O.G.

N 4580

4093 Toe
4235
4330
4400
4460
4480

O.G.
9.7 711.4
7.4 13.7 ✓
8.2 12.9
12.1 09.0
O.G.

721.05

N4560

4095	Toe	O.G.	
4240		10.0	711.1
4350		7.8	13.3 ✓
4410		8.9	12.2
4470		11.6	09.5
4520		10.7	10.4 O.G.

N4540

4095	Toe	O.G.	
4257		10.1	711.0
4340		8.3	12.8 ✓
4470		10.4	10.7
4550		8.2	12.9 O.G.

N4520

4105	Toe	O.G.	
4225		33.2	687.9
4277		9.4	711.7
4350		8.5	12.6 ✓
4380		8.4	12.7
4435		9.8	11.3
4550		6.3	14.8

East of Here is Same as last est.

B.M.	3.99	717.69	713.70

N4500

4110	Toe		O.G.
4225		39.3	678.4
4277		19.7	698.0
4305		18.0	699.7 ✓
4370		16.6	701.1
4480		4.9	712.8

East of here is Same as last est.

T.P.	0.34	706.35	11.68	706.01
T.P.	0.78	695.24	11.89	694.46

N4480

East of here is Same as last est.

4470		+4.0	699.2
4390		7.2	688.0
4290		12.7	682.5 ✓
4250		19.0	676.2
4122	Toe		O.G.
T.P.		11.23	684.01
	0.78	684.79	
		11.82	672.97
	1.27	674.24	

	674.24	N4460	
4131	Toe		O.G.
4245		14.7	659.5
4280		6.6	67.6
4385		1.5	72.7
4410		0.0	74.2
4470		+8.8	83.0

East of here same as last est.

N4440

East of here same as last est.

4470		5.2	69.0
4410		14.0	60.2
4290		21.9	52.3
4260		25.0	49.2
4215		37.0	37.2
4145	Toe		O.G.

N4420

4210	Toe		O.G.
4270		38.1	36.1
4350			O.G.

N4410 is O.G.

Elliot Simpson

Typical section of hydraulic fill for Est #17. Oct 2, 1933 14

B.M.	00	685.2	685.2
E 5140		+2.8	88.0
5130		4.7	80.5
5100		6.7	78.5
5062 W.S.		8.7	76.5
5000			63.5
	685.5		
4926 W.S.		9.0	76.5
4875		6.2	79.3
4854		4.3	81.2
4843		+2.5	88.0

Rock embankment complete to Elev. 687.5 on both faces.

Oct 30, 1933.

Simpson
Salgado
Remmen.

15

Cross-Sections of Upstream Spoil Bank For Monthly Est. #18.

B.M. 12.72 708.32 ✓ 695.60

N3940 is O.G.

N3920 ✓

6159	Toe	O.G.	~~707.7~~
73		7.4	00.9
6200		5.5	02.8
26		3.3	05.0
55		O.G.	

N3900 ✓

6285		O.G.	
55		1.1	07.2
30		2.4	05.9
6195		4.6	03.7
6152	Toe	O.G.	

N3880 ✓

6149	Toe	O.G.	
6220		3.2	05.1
50		1.9	06.4
83		0.7	07.6
6315		O.G.	

708.32

N3860 ✓

6351		O.G.	
6311		0.1	708.2
6280		0.9	07.4
6249		1.7	06.6
6223		11.2	97.1
6153	Toe	O.G.	

N3840 ✓

6162	Toe	O.G.	
6226		22.2	86.1

T.P. 3.84 711.82 ✓

6278		0.34	707.98
6325		5.6	06.2
44		4.4	07.4
79		4.4	07.4
		O.G.	

696.71

N3820 ✓

6407		6.5	90.2
6387		4.1	92.6
6362		3.7	08.1
49		2.7	09.1
25		9.9	01.9
6284		15.3	96.5
6169		O.G.	

711.82

B.M.	3.41	696.71	
			693.30

N3800

6425	7.8	88.9	O.G.
6400	6.3	90.4	
6380	3.7	93.0	
6360	+2.2	98.9	
6318	10.1	86.6	
6280	16.3	80.4	
6246	27.5	69.2	
6171			O.G.

N3780

6162	O.G.		TOC
6270	32.9	63.8	
90	29.4	67.3	
6320	23.5	73.2	
50	5.4	91.3	
77	5.3	91.4	
6420	6.6	90.1	
35	6.4	90.3	
40	9.1	97.6	O.G.

696.71

N3760

6461	10.7	86.0	O.G.
47	5.4	91.3	
20	6.3	90.4	
6390	5.6	91.1	
80	6.1	90.6	
57	5.7	91.0	
33	19.2	77.5	
6300	41.9	54.8	
6272	47.0	49.7	
6217	TOC		O.G.

N3740

6237	TOC		O.G.
6280	60.0	36.7	
6350	17.1	79.6	
69	7.2	89.5	
80	6.2	90.5	
6400	6.0	90.7	
20	5.8	90.9	
40	5.4	91.3	
62	3.7	93.0	
80			O.G.

696.71

N3720 ✓

6496			O.G.
76		2.7	94.0
60		3.4	93.3
20		5.4	91.3
6407		5.4	91.3
6383		19.4	77.3
6363		23.5	73.2
6335		36.3	60.4
6272	TOE		O.G.

Oct. 31, 1933.

B.M. 3.82 697.12 693.30

N3700 ✓

6270	TOE		O.G.
6350		41.6	55.5
6370		37.5	59.6
6400		22.1	75.0
40		4.8	92.3
70		3.9	93.2
94		3.3	93.8
6517			O.G.

697.12

N3680 ✓

6538			O.G.
6513		2.8	94.3
6490		3.1	94.0
6458		4.1	93.0
6420		26.4	70.7
6395		36.6	60.5
6357		55.4	41.7
6320		67.6	29.5
6284	TOE		O.G.

N3660 ✓

6360	TOE		O.G.
6380		54.6	42.5
6410		43.1	54.0
6455		11.2	85.9
6471		3.2	93.9
6500		2.6	94.5
6527		1.7	95.4
6559			O.G.

N3640 ✓

6581			O.G.
6545		1.3	95.8
6510		2.1	95.0
6489		2.9	94.2
6462		16.0	81.1
6385	TOE		O.G.

		697.12	N3620 ✓	
6592				O.G.
6563			1.4	95.7
6535			1.3	95.8
6515			2.5	94.6
6468			24.0	73.1
6398	TOE			O.G.
			N3600 ✓	
6400	TOE			O.G.
6460			40.2	56.9
6520			10.0	87.1
6540			2.4	94.7
6555			0.6	96.5
6572			9.3	87.8
6596				O.G.
T.P.	1.04	685.82 ✓	12.34	684.78
			N3580 ✓	
6598				O.G.
6577			11.9	73.9
6552			5.4	80.4
6515			12.2	73.6
6422				O.G.
T.P.			12.77	673.05
	1.11	674.16		

		674.16	N3560 ✓	
6440	TOE			O.G.
6506			17.5	56.7
37			10.2	64.0
67			11.2	63.0
93				O.G.
			N3540 ✓	
6585				O.G.
6563			25.3	48.9
6539			25.2	49.0
6500			33.0	41.2
6476				O.G.
B.M.		5.44	668.72	Rec. Elev. 668.74

N3510 is O.G.

Simpson
Salgado
Remmen.

Cross-Sections of Downstream Spoil Bank, For Monthly Est. #18 Nov. 1, 1933.

B.M.	2.89	704.59		701.70

N4740 is O.G.

N4720

4310		4.0	00.6 O.G.
4286		3.0	01.6
4260		10.7	93.9
4210		14.7	89.9
4180		36.7	67.9
4091	Toe		O.G.

N4700

B.M.	6.53	720.23	713.70
4329			O.G.
4295		4.5	15.7
4280		5.2	15.0
4267		10.0	10.2
4246		10.8	09.4
4222		18.2	02.0
4167		48.1	72.1
4075			O.G.

720.23

N4680

4028	Toe		O.G.
4160		44.0	76.2
4200		18.9	01.3
25		6.9	13.3
60		5.3	14.9
90		4.3	15.9
4314		3.7	16.5
4353			O.G.

N4660

4369			O.G.
4344		3.1	17.1
4310		4.4	15.8
4280		5.3	14.9
4240		6.8	13.4
4207		7.6	12.6
4175		24.7	95.5
4018	Toe		O.G.

N4640

4015	Toe		O.G.
4190		7.4	12.8
4250		7.1	13.1
4280		5.9	14.3
4320		4.4	15.8
4366		4.7	15.5
4389			O.G.

720.23

4411			
4390			
4335			
4280			
4220			
4187			
4010	Toe		

N4620 ✓

		O.G.
4.9	15.3	
5.3	14.9	
6.3	13.9	
8.3	11.9	
8.8	11.4	

N4600 ✓

4011	Toe	
4190		
4210		
4250		
4280		
4330		
4387		
4418		
4436		
4456		

	O.G.
8.5	11.7
9.4	10.8
7.7	12.5
7.1	13.1
5.9	14.3
5.9	14.3
7.0	13.2
12.9	07.3
12.9	07.3

N4580 ✓

4480		
4449		
4403		
4343		
4280		
4240		

11.6	08.6	O.G.
11.1	09.1	
7.6	12.6	
6.6	13.6	
7.7	12.5	
8.6	11.6	

720.23

4188	
4013	Toe
4016	Toe
4187	
4195	
4205	
25	
60	
4330	
71	
4440	
80	
4520	
B.M.	
	3.25
4022	Toe
4179	
4206	
30	
80	
4350	
4430	
4480	
4550	

N4580 ✓

10.9	09.3

O.G.

N4560 ✓

O.G.

14.4	05.8	
12.1	08.1	
9.9	10.3	
10.2	10.0	
8.4	11.8	
7.1	13.1	
7.3	12.9	
9.3	10.9	
10.6	09.6	
9.8	10.4	
6.52	713.71	Rec. Elev. 713.70

716.95

N4540 ✓

O.G.

22.9	94.0	
8.2	08.7	
7.7	09.2	
5.7	11.2	
4.3	12.6	
5.5	11.4	
5.9	11.0	
4.0	12.9	O.G.

716.95

N4520

4025	Toe			O.G.
4159		44.7	72.2	
4200		19.8	97.1	
30		7.2	09.7	
60		6.9	10.0	
4315		5.5	11.4	
70		4.3	12.6	
4440		5.9	11.0	
80		5.2	11.7	
4550		2.8	14.1	
4590		1.9	15.0	O.G.

N4510

4025	Toe			O.G.
4160		47.4	69.5	
4216		18.6	98.3	
55		7.6	09.3	
80		6.0	10.9	
4303		9.6	07.3	
70		8.2	08.7	
4410		4.6	12.3	
50		5.6	11.3	
4520		3.5	13.4	
80		1.6	15.3	
4610		1.3	15.6	O.G.

716.95

N4490

4635	0.3	16.6	O.G.
4600	0.0	16.9	
4550	0.4	16.5	
4500	4.8	12.1	
4465	11.0	05.9	
4405	19.8	97.1	
4340	23.6	93.3	
4300	23.6	93.3	
4280	20.5	96.4	
4250	22.6	94.3	
4200	37.4	79.5	
4149	63.8	53.1	
4033	Toe		O.G.

Nov. 2, 1933

		Level		
B.M.	2.91	716.61		713.70
T.P.	0.34	704.07	12.88	703.73
T.P.	0.55	691.61	13.01	691.06

N4470

716.61

4655	1.2	15.4	O.G.
4613	1.0	15.6	
4536	16.7	99.9	
4500	19.1	97.5	

		691.61	N4470	
4409			9.4	82.2
4307			15.2	76.4
4280			11.2	80.4
4243			14.1	77.5
T.P.			12.95	678.66
	0.78	679.44		
4180			25.4	54.0
4118			58.0	21.4
4043	Toe			O.G
			N4450	
4100	Toe			O.G.
4160			47.5	31.9
4210			27.4	52.0
4240			18.6	60.8
4290			15.6	63.8
4315			18.3	61.1
4410			12.4	67.0
4500			+3.4	82.8
4540			+6.9	86.3
		716.61		
4610			16.9	99.7
4645			14.8	01.8 O.G.

O.G. East		679.44	N4430	
4410				O.G
4370			30.2	49.2
4280			31.6	47.8
4240			34.2	45.2
4190			48.4	31.0
4118	Toe			O.G.

N4400 is O.G.

Simpson
Salgado
Remen

Cross-sections of Downstream Spoil Bank For Monthly Est. #19. Nov. 29, 1933.

N 4740 is O.G.

B.M. 7.36 721.06 713.70

N4720

E 4310 700.6 O.G.
4286 701.6
4260 693.9
4210 689.9
4180 667.9
4079 Toe O.G.

N4700

4329 O.G.
4300 6.7 14.4
4280 6.2 14.9
4260 12.0 09.1
4240 13.1 08.0
4210 22.1 99.0
4160 48.2 72.9
4070 Toe O.G.

721.06 N4680

4353 O.G.
4315 4.9 16.2
4290 5.0 16.1
4260 6.2 14.9
4215 8.0 13.1
4180 28.3 92.8
4145 50.5 70.6
4020 Toe O.G.

N4660

4369 O.G.
4344 3.5 17.6
4305 5.6 15.5
4260 7.1 14.0
4230 7.9 13.2
4202 8.4 12.7
4190 14.2 06.9
4155 36.5 84.6
4020 Toe O.G.

721.06

E 4389

4366

4330

4310

4290

4260

4230

4192

4170

4017 Toe

T.P.

3.39 715.33

4007 Toe

4180

4220

4260

4310

4370

East of Here same as last Est.

N 4640 ✓

		O.G.
5.5	15.6	
5.2	15.9	
5.8	15.3	
6.3	14.8	
7.7	13.4	
8.4	12.7	
8.9	12.2	
21.3	99.8	
		O.G.
9.12	711.94	

N 4620 ✓

		O.G.
4.8	10.5	
3.6	11.7	
2.3	13.0	
0.6	14.7	
1.0	14.3	

East of Here same as last Est.

715.38

N 4600 ✓

East of Here same as last Est.

4370	1.3	14.0
4320	1.2	14.1
4290	1.7	13.6
4260	2.5	12.8
4200	4.0	11.3
4178	5.8	09.5
4007 Toe		O.G.

N 4580 ✓

4006 Toe		O.G.
4181	4.1	11.2
4230	4.2	11.1
4260	3.0	12.3
4300	2.3	13.0
4340	1.8	13.5
4370	1.6	13.7

East of Here same as last Est.

Note: All sections south are same as last estimate East of E 4370

715.33

N4560

4370		2.4	12.9
4320		2.5	12.8
4260		3.7	11.6
4220		4.6	10.7
4190		4.1	11.2
4010	Toe		O.G.

N4540

4370		3.0	12.3
4340		2.9	12.4
4310		3.7	11.6
4260		4.6	10.7
4235		4.7	10.6
4197		4.1	11.2
4012	Toe		O.G.

N4520

4370		2.7	12.6
4320		3.7	11.6
4260		4.3	11.0
4220		4.8	10.5
4180		27.4	87.9
4015	Toe		O.G.

715.33

N4510

4017	Toe		O.G.
4164		42.5	72.8
4200		20.2	95.1
4232		6.6	08.7
4260		4.7	10.6
4300		8.6	06.7
4340		6.4	08.9
4370		6.3	09.0
T.P.		12.61	702.72
	0.54	703.26	

N4490

4370		9.4	93.9
4332		10.6	92.7
4290		8.3	95.0
4250		6.0	97.3
4220		15.2	88.1
T.P.		12.77	610.49
	0.78	691.27	
4200		10.5	80.8
T.P.	2.40	680.74	12.93 678.34
4160			20.0 60.7
4027	Toe		O.G.

680.74

N4470

4032	Toe			O.G.
4160			31.4	49.3
4205			12.1	68.6
4240			1.2	79.5
4290			1.0	79.7
4325			3.6	77.1
4370			2.4	78.3
T.P.			12.57	668.17
	0.41	668.58		

N4450

4370			5.3	63.3
4310			7.5	61.1
4290			4.5	64.1
4250			3.4	65.2
4220			8.9	59.7
T.P.			12.93	655.65
	0.48	656.13		
4190			6.3	49.8
4130			33.5	22.6
4045	Toe			O.G.

656.13

N4430

4070	Toe			O.G.
4125			46.0	10.1
4180			23.1	33.0
4240			7.4	48.7
4270			6.9	49.2
4310			9.5	46.6
4370			7.2	48.9

N4410

4310				O.G.
4260			20.0	36.1
4235			22.2	33.9
4185			34.2	21.9
4126	Toe			O.G.
T.P.			12.87	643.26
	0.63	643.89		
B.M.			14.06	629.83

Rec. Elev. 629.89

N 4390 is O.G.

Additional Loose Rock in Abutments above Elev. 700 Est. #20 Elliott Delaney
Jan 2 - 1934

Upstream

N3500 to 4040 = 20' wide 3' high

N3120 to 3500 = 10' wide 3' high

Downstream

N3160 to 3830 = 15' wide 2½' high

Elliott
Simpson
Soper
Remmen

Jan 3-1934
Xsections of Dnstr. Spoil

N4750 is O.G.

B.M.	2.82	704.52	701.70

N4740

E 4260			O.G.
4180		40.4	664.1
4102			O.G.

N4720

4085			O.G
4170		33.0	71.5
4200		19.6	84.9
4280		4.5	700.0
4310			O.G.

N4700

B.M.	7.21	720.91	713.70
4328			O.G.
4300		5.7	715.2
4280		6.3	14.6
4210		18.5	02.4
4170		30.1	690.8
4073			O.G.

720.91 N4680

E 4355		O.G.
4315	4.5	716.4
4210	7.9	13.0
4135	54.4	666.5
4023		O.G.
T.P.	4.78	716.13

End Jan 3

Start Jan 4

N4660

T.P.	3.52	719.65	716.13
4017			O.G.
4147			682.0
4195		6.5	713.1
4260		5.9	13.7
4345		2.5	17.1
4370			O.G.

N4640

4015		O.G.
4185	7.1	712.5
4260	6.4	13.2
4365	4.1	15.5
4394		O.G.

719.65 N4620

4009		0.G,
4133		678.5
4180	8.0	711.6
4260	6.6	13.0
4330	4.7	14.9
4390	4.5	15.1
4410		0.G

N4600

3980		0.G
4010		585.0
4175	9.0	10.6
4260	7.0	12.6
4310	5.7	13.9
4420	6.5	13.1
4435		0.G

N4580

3990		0.G
4012		587.5
4130		683.0
4175	8.7	10.9
4230	8.8	10.8
4260	7.4	12.2
4340	6.1	13.5
4410	7.3	12.3
4480		0.G,

719.65 N4560

3990		0.G
4010		585.0
4132		676.0
4180	10.0	709.6
4230	9.1	10.5
4260	8.1	11.5
4360	6.6	13.0
4460	9.6	10.0
4530		0.G,

N4540

4010		0.G.
4144		676.1
4195	11.9	707.7
4215	9.4	10.2
4260	9.1	10.5
4350	7.1	12.5
4460	8.4	11.2
4560		0.G.
	0.51 716.64	716.13

N4520

4015		0.G
4200	13.6	03.0
4215	7.6	09.0
4260	5.9	10.7
4350	4.5	12.1

716.64 level N4520 ✓

E4460		5.4	11.2
4600			O.G.
		N4510	
3990			O.G.
4020			583.0
4192		23.8	692.8
4215		12.8	703.8
4260		6.0	10.6
4310		9.4	07.2
4410		4.8	11.8
4460		5.0	11.6
4570		1.4	15.2
4620			O.G.
T.P.		12.41	704.23
	0.37	704.60 π	

N4490 ✓

716.6 ±

4660			O.G
4570		+0.3	16.9
4550		0.2	16.4
4485		7.1	09.5
	704.6 π		
4370		10.9	6937
4310		10.0	94.6
4250		8.8	95.8

704.60 π N4490 ✓

4215		15.3	689.3
T.P.	0.36	692.16 π 12.80	691.80
4185		13.5	78.1
4029			O.G
		N4470 ✓	
4037			O.G
4165		36.7	55.5
4210		19.0	73.2
4250		11.6	80.6
4370		14.0	78.2
4500	716.64 π	19.1	97.5
4540		16.4	700.2
4610		1.3	15.3
4660			O.G.
		N 4450 ✓	
4645			O.G
4600		18.0	698.6
	692.16 ±		
4535		7.3	84.9
4500		9.8	82.4
T.P.	0.56	680.31 12.41	679.75
4410		12.7	67.6
T.P.	0.32	668.25 12.38	667.93
4310		7.5	60.7

		668.25	N4450 ✓		
4260			2.2	666.0	
4200			11.0	57.2	
		634.1			
4145			2.4	31.7	
4113			2.9	31.2	
4035				O.G.	
			N4430 ✓		
4035				O.G.	
4103			4.3	29.8	
4165			3.3	30.8	
4200			+8.4	42.5	
		668.25			
4260			18.4	49.8	
4310			21.7	46.5	
4370			19.4	48.8	
4410			14.6	53.6	
4530				O.G.	
T.P.	1.93	656.89	13.29	654.96	
	1.41	645.47	12.83	644.06	

		645.47	N4410 ✓		
4310				O.G.	
4260			9.6	35.9	
T.P.	1.44	634.06	12.85	632.62	
B.M.			4.20	629.86	629.89
	4.20	634.09			
4210			4.4	29.7	
4102			4.4	29.7	
4032				O.G.	
			N4390 ✓		
4270				O.G.	
4200			4.6	29.5	
4105			3.6	30.5	
4030				O.G.	
			N4370 ✓		
4280				O.G.	
4190			4.1	30.0	
4120			3.6	30.5	
4090			20.9	13.2	
4035				O.G.	

N4325 is O.G.

End Jan 4 - 1934

X Sections of Downstream Spoil
For Est. #21 - Feb 1 - 1934
Elliott - Soper - Remmen

B.M.	0.53	604.35 ✓		603.82

N4320 (Average this section on the So. with 0.0 on N 4310)

E 4100				O.G.
4080			16.7	587.6
4040				O.G.
T.P.			1.22	603.13
	12.57	615.70		

N4340 (Average this section on the South with 0.0 on N4325 between E. 4215 & 4100)

E 4250				O.G.
4215			9.2	06.5
4200			7.0	08.7
4120			5.3	10.4
4090			10.4	05.3
4060			23.8	591.9
4025				O.G.
T.P.	12.30	627.21	0.79	614.91

N4360

4265				O.G.
4245			4.8	22.4
4215			5.9	21.3
4190			2.4	24.8

627.21 N4360

4120			2.6	24.6
4100			5.0	22.2
4076			15.2	12.0
4015				O.G
T.P.	8.16	634.58	0.79	626.42

N4370

4300				O.G.
4255			7.8	26.8
4200			5.0	29.6
4105			4.5	30.1
4090			9.4	25.2
4070			21.1	13.5
4010				O.G.

N4390

4300				O.G.
4250			7.4	27.2
4200			5.0	29.6
4100			5.0	29.6
4085			4.7	29.9
4007				O.G.

N4410

4005				O.G.
4077			5.0	29.6
4085 ✓			5.6	29.0

	634.58	N4410	
4195		4.8	29.8
on East same as Est. 20			
↓			
		N4430	
↑ on East same as Est. 20			
4165		3.6	31.0
4085		5.6	29.0
4075		4.7	29.9
4010			O.G.
		N4450	
4014			O.G.
4078		5.1	29.5
4145		2.8	31.8
↓ on East same as Est. 20			
		N4470	
↑ on East same as Est. 20			
4125		3.2	31.4
4090		3.6	31.0
B.M.	0.61	585.6	584.99
4023		3.3	82.3
4000			O.G.

Spoil N. of N4470 is same as Est. 20

X Sections of Downstr. Spoil

For Est #22 - Feb. 28 - 1934
Elliott - Soper - Remmen

B.M.	0.70	604.52		603.82
		N4320	(Average this section on the Sp. with 0.0 on N4300)	
4100				O.G.
4065			16.6	87.9
4022				O.G.
		N4340	(Average this section on the sp. with 0.0 on N. 4325 between E4215 & 4100)	
T.P.			0.18	604.34
	11.19	615.53		
4009				O.G.
4065			12.7	02.8
4090			7.8	07.7
4120			5.6	09.9
4160			6.6	08.9
4190			6.6	08.9
4250				O.G.
T.P.			0.03	615.50

End Feb 28 - 1934
Start Mar 1 - 1934

	12.78	628.28		615.50
		628.28	N4360	
4270				O.G.
4215			7.4	20.9
4185			3.7	24.6
4120			4.5	23.8
4080			7.9	20.4
4050			20.5	07.8
4002				O.G.
			N4370	
4000				O.G.
4070			4.3	24.0
T.P.	6.05	634.19	0.14	628.14
4100			4.8	29.4
4120			4.5	29.7
4200			4.9	29.3
4300				O.G.
B.M.			4.42	629.77 629.89
	4.42	634.31		

N4390 ✓

634.31

4300			O.G.
4185	4.5	29.8	
4120	4.7	29.6	
4068	4.5	29.8	
3998			O.G.

N4410 ✓

634.31

3997			O.G.
4068	4.2	30.1	
4120	4.6	29.7	
4220	4.7	29.6	
4260	+1.5	38.8	
4310			O.G.

N4430 ✓

634.31

4170	3.5	30.8	
4120	4.5	29.8	
4074	3.4	30.9	
3999			O.G.

N4450 ✓

634.3

4003			O.G.
4080	3.5	30.8	
4120	3.8	30.5	
4145	3.0	31.3	

N4470

4125	634.3	2.9	31.4
4095		2.8	31.5
4010			O.G.

X Sections of Spoil for Est. 23
April 2 - 1934

E 5600 is O.G.

B.M.	9.00	734.73 ✓		725.73

E 5580

4220		+1.5	736.2
4210		+1.5	36.2
4195		6.0	28.7
4144		28.8	05.9
4081			O.G.

E 5560

T.P.	6.72	741.15 ✓	0.30	734.43 ✓
4220			3.2	38.0
4200			3.1	38.1
4190			6.8	34.4
80			8.2	33.0
60			15.4	25.8
45			23.2	18.0
4062				O.G.

Plotted

E 5540

T.P.	11.54	745.97 ✓	6.72	734.43 ✓
4230			6.3	39.7
20			5.2	40.8
4200			4.5	41.5
4169			4.2	41.8
4020				O.G.

E 5520

745.97 ✓

4240	4.8	41.2
20	4.9	41.1
4200	4.4	41.6
4163	4.5	41.5
4025		O.G.

E 5500

4240	5.0	41.0
30	5.4	40.6
10	4.8	41.2
4180	4.7	41.3
4165	6.3	39.7
4027		O.G.

Plotted

E 5480

4240	6.4	39.6
30	6.0	40.0
10	5.2	40.8
4180	5.2	40.8
4170	5.8	40.2
4034		O.G.

E5460

745.97'

4240	7.8	738.2
20	7.5	38.5
4200	7.6	38.4
4170	16.0	30.0
4142	31.2	14.8
4060		O.G.

E5440

4230	9.7	36.3
4220	9.8	36.2
4202	22.0	24.0
4160	32.1	13.9
4061		O.G

Posted.

E5420

4230	11.9	34.1
23	11.4	34.6
4184	40.1	05.9
4147	52.8	693.2
4102		O.G

All other Eastings remain as previously shown in notes for other estimates.

X Sections of downstr. Spoil Est. #23
April 3 - 1934
Elliott - Soper - Remmen.

N 4470

B.M.	1.90	634.54	632.64
E 4120		3.1	31.4
4100		3.0	31.5
4094		2.2	32.3
4012			O.G.

N4450

4005		O.G.
4078	2.3	32.2
4085	3.7	30.8
4120	3.9	30.6

Plotted

N4430

4120	4.6	29.9
4075	4.4	30.1
4071	2.2	32.3
3997		O.G

N4410

3994		O.G
4064	3.2	31.3
4070	4.4	30.1
4120	4.6	29.9

N4390

634.54

4120	4.8	29.7
4067	4.5	30.0
4064	3.5	31.0
3996		O.G.

N 4370

4120	4.9	29.6
4085	5.2	29.3
4070	10.5	24.0
4050	20.1	14.4
3998		O.G.

Plotted

N4360

4000		O.G.
4050	25.8	08.7
4070	17.9	16.6
4085	11.5	23.0
4097	10.6	23.9
4120	10.5	24.0
T.P	12.49	6 X22.05
0.73	6 X22.78	

N 4340

(Average this section on the So. with 0.0 on N. 4325 between E 4215 & E 4100)

4120	12.7	10.1
T.P.	12.59	6 X10.19
0.26	6 X10.45	

N4340

6
710.45 ✓

4080		4.0	06.5 ✓
4060		11.8	598.7 ✓
4009			O.G.
	Plotted N4320		(Average this section on the Sol with 00 on N4300)
4024			O.G.
4070		21.8	588.7 ✓
4100			O.G.

April-27.1934

Simpson
Soper
Remmen.

X Sections of East end of Spillway Excavation and Spoil bank for Estimate #24.

B.M.	0.25	750.14		749.89
T.P.			12.66	737.48
	1.15	738.63		

E 5610 is O.G.

E 5600

North of 4160 is O.G.

N4160	37.4	01.2	O.G.
4104	O.G.		Toe

E 5580

4081	O.G		Toe
4140	35.0	03.6	
4190	13.8	24.8	
4210	2.5	36.1	
40	2.1	36.5	
43	3.6	35.0	
70	+1.6	40.2	
77	+5.3	43.9	
90	+7.7	46.3	

North of N4290 is finished to Neat Lines

	738.63		

E 5560

4063	O.G.		Toe
4150	17.3	21.3	
70	7.8	30.8	
4200	0.7	37.9	
T.P.	1.15	737.48	
	12.88	750.36	
40	12.0	38.4	
70	8.0	42.4	
4300	7.8	42.6	
20	7.2	43.2	
33	1.3	49.1	
T.P	0.47	749.89	
	12.84	762.73	
47	+11.2	73.9	
62	+26.3	89.0	
80	+36.6	99.3	
90	+40.1	802.8	Toe of Finished slope

Neat Line Slope to O.G.

E 5540

Neat Line Slope to O.G.

4403	+30.0	92.7	Toe of Finished slope
4385	+20.6	83.3	
60	+4.2	66.9	
40	-11.8	50.9	
4320	-14.1	48.6	

E 5540

750.36

4280	7.6	42.8
60	9.9	40.5
40	10.3	40.1
20	9.5	40.9
4200	8.9	41.5
4180	8.7	41.7
4168	9.0	41.4
4028	O.G.	Toe

E 5520

4026	O.G.	Toe
4163	9.3	41.1
80	9.1	41.3
4240	9.3	41.1
90	5.2	45.2
4320	3.6	46.8
4340	2.6	47.8

762.73

60	3.6	59.1
78	0.0	62.7
4400	+12.6	75.3
08	-1.4	61.3 Finished Slope

Neat line slope to O.G.

E 5500

750.36

Finished slope to O.G.

4443	+2.4	52.8 Toe of finished slope
4409	16.6	33.8
4401	16.6	33.8 about toe of Ogee Conc.

762.73

4375	10.9	51.8 about back of weir conc.
4342	12.0	50.7

750.36

4320	3.8	46.6
4240	9.4	41.0
4210	9.3	41.1
4180	9.4	41.0
4165	11.1	39.3
4027	O.G.	Toe

April-28-1934

B.M. 0.71 750.60 749.89

E 5480

4032	O.G.	Toe
4168	10.3	40.3
4210	9.8	40.8
46	10.6	40.0
53	6.4	44.2
4320	3.2	47.4

E5480

750.60

4368	2.2	48.4	Back of weir
4395	17.7	32.9	Toe of Ogee
4420	17.7	32.9	
4440	7.7	42.9	Toe of finished slope

Finished Slope to O.G.

E5460

Finished Slope to O.G.

4441	7.3	43.3	Toe of finished slope
4425	16.3	34.3	
4389	18.5	32.1	Toe of Ogee

↑ Same as last Est. ↓

4220	12.4	38.2	
18	10.2	40.4	
4181	10.7	39.9	
4140	38.0	12.6	
4035			Toe

E5440

750.60

4064	0.6.		Toe
4186	11.0	39.6	
4210	10.6	40.0	
20	14.4	36.2	

↑ Same as last Est. ↓

4382	14.2	36.4	Toe of Ogee
4400	17.8	32.8	
4430	17.1	33.5	
4438	12.7	37.9	Toe of finished slope

Finished Slope to O.G.

E5420

Finished Slope to O.G.

4440	11.1	39.5	
30	15.0	35.6	
4407	14.5	36.1	
4400	13.9	36.7	
4390	12.8	37.8	

↑ Same as last Est. ↓

4221	16.5	34.1	
13	11.3	39.3	
4188	13.4	37.2	
4067	0.G.		Toe

	750.60		
T.P.		9.98	740.62
	0.72	741.34	

E5410

	O.G.	Toe
A068		
4180	12.1	29.2
4203	2.9	38.4
10	2.8	38.5
4220	8.4	32.9

on North same as last Est.

E5390

on North same as last Est.

4219	11.5	29.8
11	17.2	24.1
4190	20.2	21.1
70	29.3	12.0
50	41.1	00.2
4088	O.G.	Toe

E5370

	O.G.	Toe
4103		
4170	44.6	96.7
4196	34.5	06.8

on North same as last Est.

E.5350 is Same as last Est.

May 29-1934

Added X Sections of spillway spoil for Est. #25

B.M.	1.43	751.32	749.89
T.P.		9.30	742.02
	0.91	742.93	

E. of E. 5460 same as previous

E 5460

N. 4220	4.6	38.3
4215	2.3	40.6
4178	3.4	39.5
4037		O.G.

E 5440

4220	6.9	36.0
4215	3.3	39.6
4185	3.6	39.3
4065		O.G.

E 5420

4220	8.7	34.2
4214	4.3	38.6
4190	4.0	38.9
4069		O.G.

E 5400

4219	11.5	31.4
4209	4.4	38.5
4193	3.8	39.1
4067		O.G.

742.93

T.P.	12.49	730.44
	0.37	730.81

E 5380

4215	3.0	27.8
4205	1.4	29.4
4180	9.0	21.8
4090		O.G.

E 5360

4197	16.8	14.0
4172	25.9	04.9
4155	33.3	97.5
4092		O.G.

E 5340

4158	42.5	88.3
4140	49.0	81.8
4100		O.G.

W. of 5340 same as previous

Monthly Estimate #27 July 1934.
Hydraulic fill & rock embank.

	712.0	N. 3900			8/1/34 Reduced & ck. [illegible]
E. 4837		10.0	702.0	✓	
61		5.5	706.5	✓	
96		+1.4	13.4	✓	
4906		+1.7	13.7	✓	713.0
45		00	12.0	✓	
50		0.5	11.5	✓	
60		1.0	11.0	✓	
70		3.0	09.0	✓	
80		4.0	08.0	✓	
90		4.0	08.0	✓	
5000		4.0	08.0	✓	709.2
10		6.0	06.0	✓	
20		5.0	07.0	✓	
30		5.5	06.5	✓	
40		3.0	09.0	✓	
50		0.5	11.5	✓	
58		00	12.0	✓	
90		+1.0	13.0	✓	
5103		+2.9	14.9	✓	713.6
17		+2.6	14.6	✓	
30		4.0	708.0	✓	

Plotted By J.W. Williams

Use this section from N. 3900 to north abutment.

W.S. 712.0

Converse
Salgado
Isbell
Delgney
} Aug. 1, 1934. 43

N. 3800.

	712.0				
E4837		11.0	701.0	✓	
53		11.3	00.7	✓	
63		5.0	07.0	✓	
78		4.0	08.0	✓	
97		+2.0	14.0	✓	
4918		+2.2	14.2	✓	713.4
50		0.0	12.0	✓	
60		0.5	11.5	✓	
70		2.5	09.5	✓	
80		4.5	07.5	✓	
90		4.0	08.0	✓	
5000		4.5	07.5	✓	
10		6.0	06.0	✓	709.2
20		5.5	06.5	✓	
30		4.0	08.0	✓	
40		2.5	09.5	✓	
50		0.5	11.5	✓	
58		0.0	12.0	✓	
5105		+3.4	15.4	✓	714.4
19		+3.7	15.7	✓	
30		1.3	10.7	✓	

Plotted By J.W. Williams

N. 3700

713.0

E 4836	10.5	701.5 ✓	
50	9.9	02.1 ✓	
65	3.0	09.0 ✓	
80	2.8	09.2 ✓	
98	+2.8	14.8 ✓	
A913	+2.3	14.3 ✓	713.7
50	0.0	12.0 ✓	
60	0.5	11.5 ✓	
70	1.0	11.0 ✓	
80	3.0	09.0 ✓	
90	7.5	04.5 ✓	
5000	7.5	04.5 ✓	708.7
10	5.5	06.5 ✓	
20	7.0	05.0 ✓	
30	4.5	07.5 ✓	
40	3.0	09.0 ✓	
50	0.5	11.5 ✓	
55	0.0	12.0 ✓	
94	+2.5	14.5 ✓	714.0
5101	+3.3	15.3 ✓	
17	+4.2	16.2 ✓	
30	1.3	10.7 ✓	

Plotted by J.M.

N. 3600

713.0

E 4836	12.0	700.0 ✓	
51	10.5	01.5 ✓	
64	3.7	08.8 ✓	
80	2.5	09.5 ✓	
98	+2.0	14.0 ✓	
A915	+2.0	14.0 ✓	713.3
50	0.0	12.0 ✓	
60	0.5	11.5 ✓	
70	3.0	09.0 ✓	
80	6.0	06.0 ✓	
90	6.5	05.5 ✓	
5000	7.0	05.0 ✓	708.7
10	5.5	06.5 ✓	
20	4.5	07.5 ✓	
30	3.0	09.0 ✓	
40	1.0	11.0 ✓	
50	0.0	12.0 ✓	
97	+1.7	13.7 ✓	713.9
5102	+3.9	15.9 ✓	
19	+4.5	16.5 ✓	
31	1.2	10.8 ✓	

Plotted by J.M.

N. 3500

	717.0		
E A836	17.0	700.0 ✓	
52	11.0	01.0 ✓	
64	1.4	10.6 ✓	
80	1.8	10.2 ✓	
94	+3.0	15.0 ✓	
A91A	+7.5	14.5 ✓	714.0
50	0.0	12.0 ✓	
60	0.5	11.5 ✓	
70	3.0	09.0 ✓	
80	5.5	06.5 ✓	
90	6.5	05.5 ✓	
5000	5.5	06.5 ✓	708.7
10	5.5	06.5 ✓	
20	5.0	07.0 ✓	
30	5.5	06.5 ✓	
40	7.5	09.5 ✓	
50	0.5	11.5 ✓	
55	0.0	12.0 ✓	
5107	+3.3	15.3 ✓	714.7
19	+3.3	15.3 ✓	
30	1.0	711.0 ✓	

Plotted by J.W.

N. 3400

	717.0		
E.A836	11.8	700.2 ✓	
52	10.5	01.5 ✓	
69	1.5	10.5 ✓	
80	1.7	10.3 ✓	
95	+3.0	15.0 ✓	
A913	+7.8	14.8 ✓	714.0
60	0.0	12.0 ✓	
70	3.5	08.5 ✓	
80	7.0	05.0 ✓	
90	7.5	04.5 ✓	
5000	6.0	06.0 ✓	707.3
10	5.5	06.5 ✓	
20	6.0	06.0 ✓	
30	6.0	06.0 ✓	
40	5.5	06.5 ✓	
50	0.0	12.0 ✓	
97	+2.7	14.7 ✓	714.0
5118	+3.0	15.0 ✓	
30	3.0	09.0 ✓	

Plotted by J.W.

N. 3300

	712.0			
E. 4836		12.0	700.0 ✓	
53		10.5	01.5 ✓	
68		2.0	10.0 ✓	
90		2.0	10.0 ✓	
4902		+3.0	15.0 ✓	
18		+2.5	14.5 ✓	714.0
60		0.0	12.0 ✓	
70		3.0	09.0 ✓	
80		6.0	06.0 ✓	
90		8.0	04.0 ✓	
5000		6.5	05.5 ✓	
10		6.0	06.0 ✓	707.5
20		5.5	06.5 ✓	
30		7.0	05.0 ✓	
40		6.0	06.0 ✓	
50		2.0	10.0 ✓	
55		0.0	12.0 ✓	
80		+2.0	14.0 ✓	713.5
5118		+2.6	14.6 ✓	
30		2.2	09.8 ✓	

Use this section for N. 3250 also.

N. 3200

	712.0			
E. 4836		12.0	700.0 ✓	
55		9.3	702.7 ✓	
67		3.3	08.7 ✓	
80		1.8	10.2 ✓	
4900		+3.0	15.0 ✓	Av. 714.0
20		+3.0	15.0 ✓	
60		0.0	12.0 ✓	
70		5.0	07.0 ✓	
80		8.0	04.0 ✓	
90		6.5	05.5 ✓	54
5000		7.0	05.0 ✓	Av 706.6
10		6.0	06.0 ✓	
20		7.0	05.0 ✓	
30		8.5	03.5 ✓	
40		6.0	06.0 ✓	
50		0.0	12.0 ✓	
97		+3.0	15.0 ✓	Av. 711.2
5107		5.5	706.5 ✓	
25		5.0	07.0 ✓	8/2/34.
31		3.5	08.5 ✓	Reduced & ck. [illegible]

Use this section including N 3240 to south abutment

Cross Section of Top of Dam
For Est. # 30

Nov. 1, 1934
Osborne
Remmen
Adams

B.M.	7.52	771.97	764.45

N 3100

4976	Finish Rock	7.6	764.4
80		8.0	764.0
87		3.1	768.9
5005		3.2	768.8
16		8.9	763.1
26	Finish Rock	8.3	763.7

N 3200

4977		6.6	765.4
80		6.6	765.4
83		4.8	767.2
5009		5.2	766.8
16		8.0	764.0
25		7.0	765.0

N 3300

4975		7.0	765.0
78		7.2	764.8
80		5.8	766.2
5011		5.4	766.6
17		6.7	765.3
25		6.6	765.4

4973			
75			
80			
5012			
18			
27			
T.P.			

N 3400

771.97

	7.5	764.5
	7.8	764.2
	4.9	767.1
	5.7	766.3
	8.0	764.0
	6.5	765.5
6.42	6.88	765.09
	771.51	

N 3500

4971		7.2	764.3
74		8.2	763.3
80		5.2	766.3
5016		4.8	766.7
26		5.3	766.2

N 3600

4972		7.5	764.0
75		8.1	763.4
80		5.2	766.3
5014		4.4	767.1
26		5.0	765

N 3700

771.51

4971	7.9	763.6 ✓	
74	8.4	763.1 ✓	
80	4.9	766.6 ✓	
5014	4.2	767.3 ✓	
21	9.5	762.0 ✓	✓
32	8.4	763.1 ✓	

N 3800

4974	7.5	764.0 ✓	
77	7.9	763.6 ✓	
80	4.5	767.0 ✓	
5013	4.3	767.2 ✓	✓
40	7.9	763.6 ✓	
32	8.8	762.7 ✓	

N 3900

T.P.	7.68	763.83 ✓	
7.76	771.59 ✓		
4976	6.8	764.8 ✓	
78	7.5	764.1 ✓	
83	4.4	767.2 ✓	✓
5011	3.7	767.9 ✓	
16	8.2	763.4 ✓	
28	8.0	763.6 ✓	

N 4000

771.59 ✓

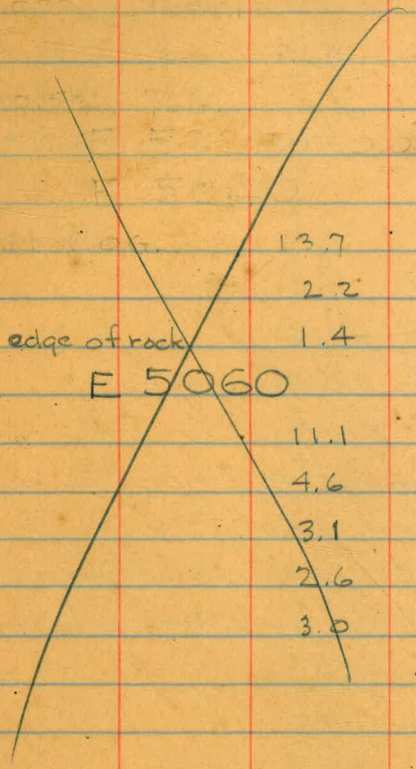
4976	7.0	764.6 ✓	
79	7.8	763.8 ✓	
83	5.0	766.6 ✓	
5011	4.9	766.7 ✓	✓
18	9.1	762.5 ✓	
27	7.7	763.9 ✓	

Note - Use section on N 3100 to South abutment.

Use section on N 4000 to north abutment except for warped section on upstream from N. 4110 to N. 4180, and downstream rock embankment which extends only to N. 4050.

Cross Section of Spoil South of Dam
For Est. #30

B.M.



N 4		13.7
4200		2.2
4170	edge of rock	1.4
	E 5060	
4232		11.1
23		4.6
4189		3.1
4160		2.6
40		3.0

Final Cross Section of Plaza N.W. of Dam
Prior to Placeing of D. G. for finishing.

Nov. 7, 1934

B.M.	3.73	773.27		769.54	
		N 4213 = 0.0		N. Edge	
		N 4210			
5004	on Core wall		3.6	769.7	
5000			2.9	770.4	
4990			3.0	770.3	
80	edge		3.0	770.3	
		N 4200			
5005	conc.		3.6	769.7	
5000			2.6	770.7	
4990			2.7	770.6	
80			2.8	770.5	
70			2.8	770.5	
60			3.0	770.3	
		N 4190			
5000	conc.		3.7	769.6	
4990			2.0	771.3	
80			3.3	770.0	
70			3.2	770.1	
60			2.8	770.5	
50			2.6	770.7	
40			3.2	770.1	
30	edge		3.1	770.2	

12/3/34 Plotted on X Sec. Drawing

Reduced By C.B.H.
Plotted By C.B.H.
Checked " A.V.M.
} From Page 50 to 53

Osborne
Remmen
Adams

N 4180 spillway.

		773.27			
4910			3.4	769.9	
20			3.1	770.2	
30			3.1	770.2	
40			3.3	770.0	
50			2.6	770.7	
60			2.7	770.6	
70			3.6	769.7	
80			3.9	769.4	
90			2.5	770.8	
5000	conc.		3.9	769.4	
		N 4170			
4993	edge		3.2	770.1	
90			3.1	770.2	
80			3.7	769.6	
70			3.7	769.6	
60			2.8	770.5	
50			3.2	770.1	
40			3.4	769.9	
30			3.5	769.8	
20			3.5	769.8	
10			3.4	769.9	
4900			3.5	769.8	
4890			3.7	769.6	
83	edge		3.9	769.4	

Plotted on Dam Sec. 3/9/35

N 4160

773.27

4860		3.8	769.5
70		3.8	769.5
80		3.8	769.5
90		3.6	769.7
4900		3.8	769.5
10		3.7	769.6
20		3.8	769.5
30		4.0	769.3
40		3.6	769.7
50		3.5	769.8
60		3.7	769.6
70		3.7	769.6
80		2.3	771.0
85		2.3	771.0

Rested on pavement

N 4150

4980		2.5	770.8
70		3.7	769.6
60		3.9	769.4
50		4.0	769.3
40		3.7	769.6
30		3.7	769.6
20		3.4	769.9
10		4.2	769.1
4900		3.8	769.5

N 4150

773.27

4890		3.7	769.6
80		4.1	769.2
70		3.7	769.6
60		3.7	769.6
57	edge	3.7	769.6

N 4140

4845		3.6	769.7
50		2.6	770.7
60		3.8	769.5
70		3.7	769.6
80		4.0	769.3
90		2.9	770.4
4900		3.6	769.7
10		4.2	769.1
20		4.3	769.0
30		3.9	769.4
40		4.0	769.3
50		3.9	769.4
60		3.5	769.8
70		3.0	770.3
75	edge	2.7	770.6
80	on fill	8.1	765.2

Rested on pavement

N 4130

773.27

4980	on fill	8.1	765.2 ✓
70	" "	7.6	765.7 ✓
60	edge	2.6	770.7 ✓
50		3.8	769.5 ✓
40		4.0	769.3 ✓
30		4.0	769.3 ✓
20		4.6	768.7 ✓
10		4.7	768.6 ✓
4900		5.1	768.2 ✓
4890		3.2	770.1 ✓
80		4.1	769.2 ✓
70		4.0	769.3 ✓
60		3.9	769.4 ✓
50		3.5	769.8 ✓
40	edge	4.1	769.2 ✓

N 4120

4840	edge	1.7	771.6 ✓
50		3.9	769.4 ✓
60		4.0	769.3 ✓
70		4.5	768.8 ✓
80		4.1	769.2 ✓
90		4.7	768.6 ✓
4900		5.1	768.2 ✓
10		4.6	768.7 ✓
20		5.1	768.2 ✓

N 4120

773.27

4930		4.3	769.0 ✓
40		3.8	769.5 ✓
50		3.7	769.6 ✓
60	edge of fill	6.5	766.8 ✓
70	fill	7.5	765.8 ✓
80	"	8.1	765.2 ✓

N 4110

4980	fill	7.9	765.4 ✓
70	"	7.3	~~768.0~~ 766.0
60	"	6.2	767.1 ✓
50		3.7	769.6 ✓
40		3.9	769.4 ✓
30		4.7	768.6 ✓
20		5.2	768.1 ✓
10		5.1	768.2 ✓
4900		4.7	768.6 ✓
4890		4.7	768.6 ✓
80		4.4	768.9 ✓
70		4.3	769.0 ✓
60		4.0	769.3 ✓
50		3.8	769.5 ✓
40		3.8	769.5 ✓

12/3/54 Plotted on Dam Lee [illegible]

N 4100

773.27

4845	edge	3.8	769.5
50		4.2	769.1
60		3.9	769.4
70		4.2	769.1
80		3.0	770.3
90		5.0	768.3
4900		5.3	768.0
10		5.0	768.3
20		5.2	768.1
30		4.5	768.8
40	edge	4.2	769.1
50	on fill	5.2	768.1
60	" "	6.2	767.1
80	" "	7.6	765.7

B.M. 354 773.08 769.54

N 4090

4933		4.5	768.6
20		5.0	768.1
10		5.0	768.1
4900		5.1	768.0
4890		5.0	768.1
80		1.2	771.9
70		2.3	770.8
60		2.5	770.6

N 4090

773.08

4850	edge	4.6	768.5

N 4080

4870	edge	2.7	770.4
80		3.5	769.6
90		4.6	768.5
4900		5.7	767.4
10		4.5	768.6
20		4.4	768.7

N 4070

4895	South edge	6.3	766.8

Location of Fence line Around Plaza

Osborne
Remmen
Adams

Nov. 9, 1934

0+00 = ℄ West tile set in curb = N. 4212.72 E. 4997.00

Set Nail + Stake every 8'

1+44 = South 66° 30' West - 144'.

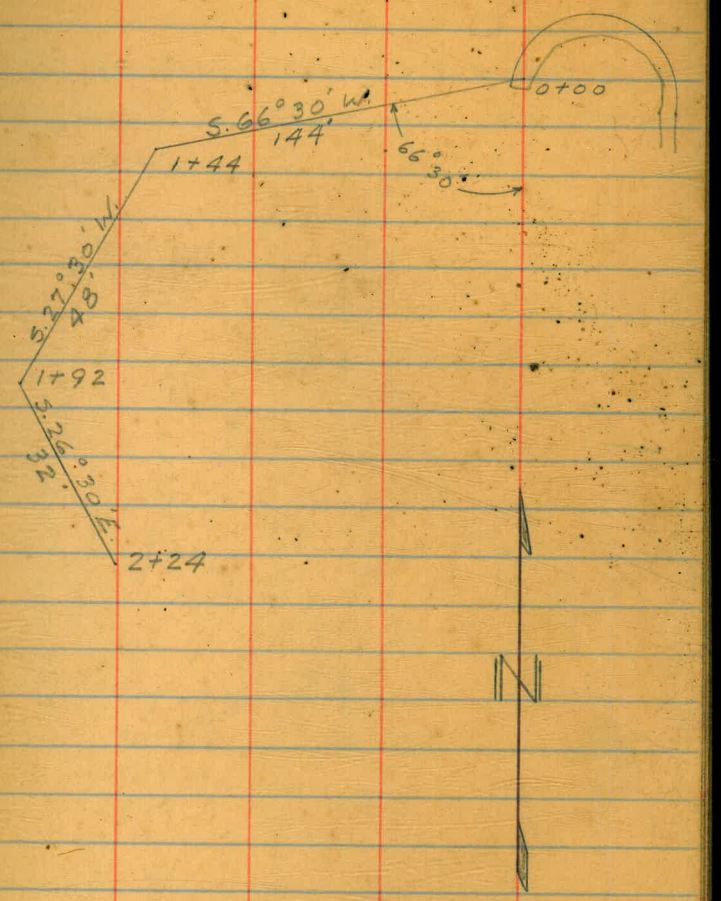
Set Nail + Stake every 8'

1+92 = South 27° 30' West - 48'

Set Nail + Stake every 8'

2+24 = South 26° 30' East - 32'

Cross Chiseled in Large Boulder

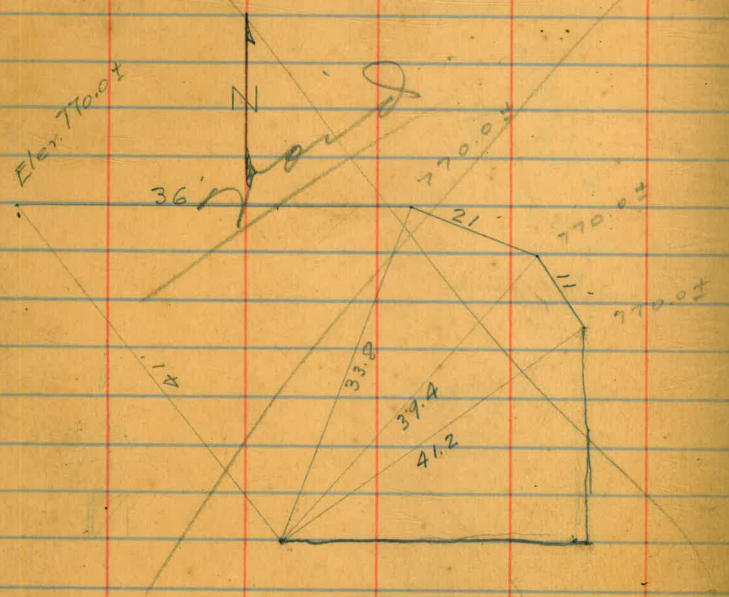


Estimate of Rock Cap on fill Adjacent to Plaza

Osborne
Remmen
Adams

Nov. 10, 1934

Note: Owing to lack of X-Sections the Surface area of the rock fill was measured and Est. to be 3' thick - See sketch

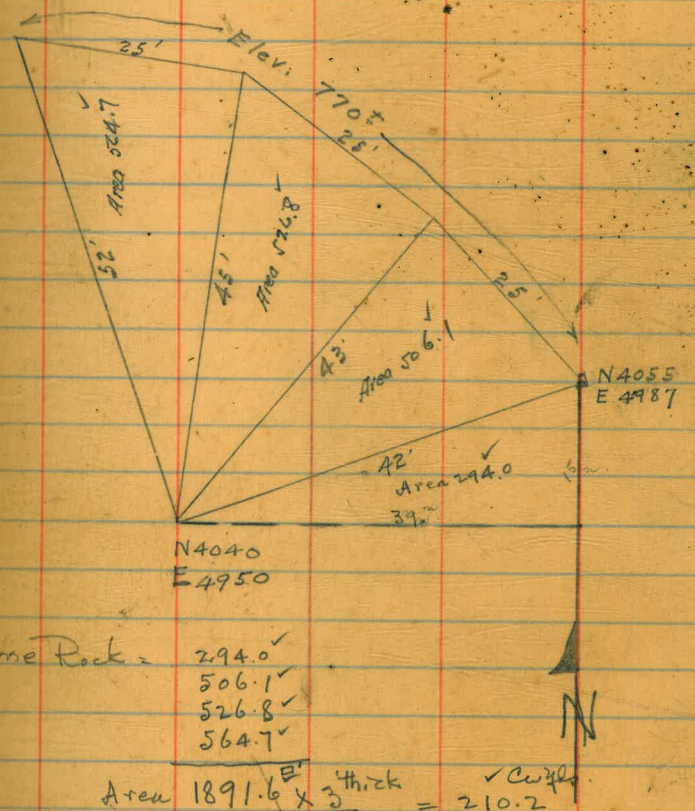


Estimate of Rock Cap on Fill Adjacent to Plaza.

Simpson
Soper
Isbell

Dec. 17-1934

Sketch of Surface Area of Rock Cap on Fill Adjacent to Plaza, as Layed by the Contractors.



Volume Rock = 294.0 ✓
506.1 ✓
526.8 ✓
564.7 ✓

Area 1891.6 sq ft × 3' thick / 27 = 210.2 ✓ Cu Yds.

X Sections of Spoil Area For Material Moved From Spillway, on and After Nov. 13-1934.

These x sections are over the portion of the original Spoil Bank that has been excavated to be put in the Dam. (See Page 70 For Finals)

Simpson - Notes, Super - Rod, Meyer - Level, Salgado - " , Isbell - Tape, Remmen - "

Nov. 13-1934.

		Transit.			
B.M.	3.78	717.48		713.70	
T.P.			13.03	704.45	
		Level			
	0.71	705.16			
			N 4480		
		717.48			
E 4527			11.0	706.5	0.G.
		705.16			
4515			5.3	699.9	
4496			2.3	702.9	0.G.
4485			3.1	702.1	0.G.

Plotted

Notes Reduced from Page 57 to 69 By C.B.H. Plotted. Checked — A.V.M.

4480				
4500				
15				
20				
30				
		717.48		
4542				
			N 4490	
		705.16		
			3.8	701.4
			9.4	695.8
			9.3	695.9
			9.5	695.7
			1.3	703.9
		717.48		
			2.1	715.4 0.G.
			N 4500	
4543			2.4	715.1 0.G.
		705.16		
4518			9.5	695.7
10			9.4	695.8
4500			9.7	695.5
4490			9.4	695.8
80			9.5	695.7
70			7.2	698.0

Plotted

Plotted

Spoil Bank Xsections contd. - Nov. 13-1934.

Meyer

N4510

705.16

4462	9.8	695.4
70	10.1	695.1
80	9.6	695.6
90	9.6	695.6
4500	9.6	695.6
10	9.2	696.0
18	9.1	696.1

Plotted

717.48

4545	2.9	714.6	0.6

N4520

4543	3.5	714.0

705.16

18	9.3	695.9
10	9.3	695.9
4500	10.0	695.2
4490	9.5	695.7
80	9.2	696.0
70	9.5	695.7
60	9.5	695.7
4445	9.6	695.6

Plotted

4426		
40		
50		
60		
70		
80		
90		
4500		
14		

717.48

38	3.9	713.6	0.6

N4525

4525		
24		
14		

N4530

705.16

4500	9.3	695.9
4490	9.3	695.9
80	9.4	695.8
70	9.3	695.9
60	9.3	695.9
50	9.5	695.7
40	9.7	695.5
4428	9.8	695.4

Plotted

717.48

	3.9	713.6	0.6

N4540

	5.6	711.9	O.G. on East
	9.9	707.6	
	13.2	704.3	

705.16

4500	9.0	696.2
4490	9.8	695.4
80	9.9	695.3
70	10.0	695.2
60	9.6	695.6
50	9.3	695.9
40	9.3	695.9
4428	9.0	696.2

Plotted

Spoil Bank X Sections Cont'd. - Nov. 13 - 1934.

	705.16	N4550		
4424		9.0	696.2'	
30		8.8	696.4'	
40		9.2	696.0'	
50		9.0	696.2'	
60		9.3	695.9'	
70		9.4	695.8'	
80		9.5	695.7'	
85		9.5	695.7'	
4500		3.0	702.2'	
	717.48			
08		13.1	704.4'	
4509		6.7	710.8'	O.G. on East.
		N4560.		
4494		7.6	709.9'	O.G. on East.
	705.16			
91		2.0	703.2'	
80		3.4	701.8'	
70		3.3	701.9'	
60		8.6	696.6'	
50		8.8	696.4'	
40		9.0	696.2'	
30		9.0	696.2'	
20		8.8	696.4'	
4408		8.8	696.4'	

Plotted

Plotted

	705.16	N4570		
4405		8.4	696.8'	
20		8.7	696.5'	
30		8.8	696.4'	
40		8.7	696.5'	
50		8.9	696.3'	
	717.48			
65		12.5	705.0'	
4470		8.3	709.2'	O.G. on East.
		N4580		
4454		8.7	708.8'	O.G. on East.
	705.16			
50		4.0	701.2'	
40		4.0	701.2'	
30		1.7	703.5'	
20		5.4	699.8'	
10		8.0	697.2'	
4400		8.0	697.2'	

Plotted

Spoil Bank Xsections Cont'd. – Nov. 13-1934.

	717.48	N4590	
4430		6.0	711.5 ✓ O.G. on East.
29		9.0	708.5 ✓
	705.16		
20		2.5	702.7 ✓
10		7.2	698.0 ✓
4400		8.0	697.2 ✓
4395		8.0	697.2 ✓
			Plotted
T.P.		6.52	698.64 ✓ End of Nov. 12-1934.

Nov. 16-1934.

Simpson – Notes Soper-Rod
Meyer – Level Isbell-Tape
Salgado – Level Remmen- "

		698.64
	1.04	699.68 ✓
T.P.		11.55 688.13 ✓
	0.73	688.86 ✓

N4470

E 4410	5.1	683.8 ✓ O.G.
20	4.7	684.2 ✓
30	7.4	681.5 ✓
40	7.3	681.6 ✓
55	6.0	682.9 ✓
		Plotted
	699.68	
66	8.7	691.0 ✓ O.G. on East.

Note: South of N4470 is original Spoil bank, Not disturbed.

Continued from Page 57 - this Book.

688.86	N4480	
4450	10.6	678.3 ✓
40	10.2	678.7 ✓
30	9.7	679.2 ✓
20	8.8	680.1 ✓
10	8.2	680.7 ✓
4400	7.4	681.5 ✓
4390	6.0	682.9 ✓
80	4.9	684.0 ✓
70	5.1	683.8 ✓
4360	3.4	685.5 ✓ O.G.
	N4490	
699.68		
4320	8.1	691.6 ✓ O.G.
30	11.6	688.1 ✓
688.86		
40	3.1	685.8 ✓
50	4.1	684.8 ✓
60	6.2	682.7 ✓
70	6.7	682.2 ✓
80	6.5	682.4 ✓
90	6.9	682.0 ✓
4400	7.4	681.5 ✓
10	8.0	680.9 ✓
20	8.7	680.2 ✓
30	8.9	680.0 ✓

Plotted

Plotted

688.86

4440		
4453		
	N4490	
4464	9.7	679.2
50	10.3	678.6
	N4500	
40	2.8	686.1
30	10.3	678.6
20	10.1	678.8
10	9.0	679.9
4400	8.4	680.5
4390	7.8	681.1
80	7.3	681.6
70	6.9	682.0
60	6.6	682.3
50	4.9	684.0
40	3.2	685.7
30	4.5	684.4
	5.9	683.0
	6.7	682.2

699.68

20	14.5	685.2

688.86

10	0.7	688.2
4300	1.5	687.4

Plotted

Plotted

688.86

4300	6.2	682.7
10	5.7	683.2
20	5.0	683.9
30	3.4	685.5
40	3.8	685.1
50	6.5	682.4
60	5.1	683.8
70	6.6	682.3
80	6.8	682.1
90	5.8	683.1
4400	6.4	682.5
10	7.5	681.4
20	8.3	680.6
30	7.6	681.3
40	8.0	680.9
50	5.7	683.2
44 59	2.3	686.6
	N4520	
44 36	1.3	687.6
30	1.5	687.4
20	3.0	685.9
10	3.2	685.7
4400	4.9	684.0
4390	5.7	683.2
80	7.5	681.4

Plotted

Plotted

688.86 N4520

4370	6.8	682.1
60	6.4	682.5
50	6.4	682.5
40	6.0	682.9
30	6.2	682.7
20	5.8	683.1
10	5.8	683.1
4300	6.5	682.4

Plotted

N 4530.

4300	6.3	682.6
10	5.7	683.2
20	5.7	683.2
30	5.7	683.2
40	5.8	683.1
50	6.2	682.7
60	6.4	682.5
70	7.2	681.7
80	7.4	~~682.5~~ 681.5
90	8.1	680.8
4400	7.7	681.2
10	7.3	681.6
23	0.0	688.9

Plotted

688.86 N4540

4425	0.0	688.9
12	6.9	682.0
4400	7.9	681.0
90	7.9	681.0
80	8.3	680.6
70	7.4	681.5
60	6.6	682.3
50	5.8	683.1
40	5.4	683.5
30	5.4	683.5
20	5.7	683.2
10	5.9	683.0
4300	6.3	682.6

Plotted

699.68 N4550

4421	10.0	689.7
688.86 10	1.3	687.6
4400	3.3	685.6
4395	7.8	681.1
80	8.1	680.8
70	7.7	681.2
60	6.6	682.3
50	5.8	683.1
40	5.4	683.5
30	5.3	683.6

Plotted

Spoil Bank X Sections cont'd.

	688.86	N 4550		
4320		5.5	683.4	
10		5.6	683.3	
4300		5.8	683.1	
		N 4560		
4300		5.0	683.9	
10		5.3	683.6	
20		5.1	683.8	
30		5.4	683.5	
40		5.7	683.2	
50		6.2	682.7	
60		7.2	681.7	
70		7.6	681.3	
80		7.6	681.3	
90		6.6	682.3	
4405	699.68	10.0	689.7	
		N 4570		
4402		9.1	6906	
	688.86			
4385		6.8	~~683.1~~ 682.1	
70		7.0	681.9	
60		6.8	682.1	
50		6.4	~~683.5~~ 682.5	
40		5.4	683.5	
30		5.6	683.3	
20		5.4	683.5	

Plotted

Plotted

Plotted

Nov. 16-1934.

63

	688.86	N 4570	
4310		5.1	683.8
4300		4.7	684.2
4290		4.2	684.7
80		1.9	687.0
70		4.6	684.3
60		4.3	684.6
50		3.2	685.7
		N 4580	
4210		2.6	6863
20		2.6	6863
30		3.0	685.9
40		2.7	6862
50		3.1	685.8
60		3.6	6853
70		2.5	6864
80		4.0	684.9
90		4.0	684.9
4300		4.5	684.4
10		4.8	684.1
20		5.4	683.5
30		5.3	683.6
40		5.7	683.2
50		6.2	682.7
60		4.1	684.8
70		4.7	684.2

Plotted

Plotted

Spoil Bank Xsections cont'd,

	688.86	N4580	
4380		3.4	685.5
	699.68		
4390		9.1	690.6
		N4590	
4383		10.0	689.7
75		10.3	689.4
	688.86		
65		2.7	686.2
50		5.6	683.3
40		5.6	683.3
30		5.2	683.7
20		5.0	683.9
10		4.6	684.3
4300		4.0	684.9
4290		3.8	685.1
80		3.7	685.2
70		3.5	685.4
60		2.7	686.2
50		2.7	686.2
40		2.7	686.2
30		2.4	686.5
20		2.1	686.8
10		2.0	686.9

Plotted

Plotted

Nov. 16-1934.

64

	688.86	N4600	
4210		1.3	687.6
20		1.7	687.2
30		2.2	686.7
40		2.3	686.6
50		2.3	686.6
60		2.7	686.2
70		3.2	685.7
80		3.4	685.5
90		3.8	685.1
4300		3.8	685.1
10		3.9	685.0
20		4.0	684.9
30		4.8	684.1
40		4.1	684.8
50		1.4	687.5
	699.68		
60		10.1	689.6
75		9.1	690.6
90		2.6	697.1
4402		2.4	697.3
T.P.	12.52	711.16	698.64
15		8.4	702.8
25		0.7	710.5 O.G.
44 35		4.3	706.9 "

Plotted

711.16 N4610

4425	5.2	706.0	O.G.
18	2.8	708.4	O.G.
10	6.8	704.4	
4400	10.0	701.2	
4390	12.6	698.6	
82	10.8	700.4	

699.68

65	9.4	690.3
50	10.2	689.5
40	10.2	689.5
30	7.1	692.6
20	10.2	689.5
10	12.2	687.5
4300	14.3	685.4
4290	14.5	685.2
80	14.0	685.7
70	13.7	686.0
60	13.3	686.4
50	13.0	686.7
40	11.2	688.5
30	12.4	687.3
20	11.9	687.8
10	11.9	687.8
4200	11.4	688.3

Plotted

699.68 N4620

4200	10.7	689.0
10	11.5	688.2
20	11.8	687.9
30	10.4	689.3
40	12.2	687.5
50	12.8	686.9
60	13.0	686.7
70	12.9	686.8
80	13.4	686.3
90	13.4	686.3
4300	11.2	688.5
10	10.0	689.7
20	3.0	696.7
30	8.4	691.3
40	9.7	690.0
50	9.1	690.6
60	9.1	690.6
70	5.7	694.0
80	0.0	699.7

711.16

90	6.4	704.8
4402	1.5	709.7 O.G.
10	4.6	706.6 O.G.

Plotted

Spoil Bank Xsections cont'd.

Nov. 16-1934.

66

711.16 N4630

4410	5.7	705.5	O.G.
4395	1.2	710.0	O.G.
85	6.4	704.8	
75	13.0	698.2	
699.68			
70	1.7	698.0	
60	8.1	691.6	
50	8.0	691.7	
40	8.1	691.6	
30	8.1	691.6	
17	1.6	698.1	
10	7.3	692.4	
4300	10.7	689.0	
4290	11.5	688.2	
80	10.3	689.4	
70	12.6	687.1	
60	12.7	687.0	
50	12.6	687.1	
40	12.5	687.2	
35	12.4	687.3	
25	8.6	691.1	
20	11.0	688.7	
10	10.9	688.8	
4200	11.0	688.7	

699.68 N4640

4200	10.4	689.3	
10	9.8	689.9	
20	8.9	690.8	
30	11.1	688.6	
40	11.9	687.8	
50	11.9	687.8	
60	11.7	688.0	
70	9.2	690.5	
80	1.3	698.4	
90	2.0	697.7	
4300	1.3	698.4	
10	0.9	698.8	
20	4.3	695.4	
30	6.5	693.2	
40	7.2	692.5	
50	7.0	692.7	
60	6.6	693.1	
711.16			
70	11.4	699.8	
78	10.5	700.7	
85	3.8	707.4	O.G.
95	5.9	705.3	O.G.

711.16 N 4650

4390		7.0	704.2 O.G
77		5.8	705.4 O.G
70		9.5	701.7
	699.68		
60		2.3	697.4
50		6.3	693.4
40		6.0	693.7
30		5.6	694.1
20		5.1	694.6
10		0.9	698.8
4300		1.0	698.7
4290		1.8	697.9
80		1.3	698.4
75		1.1	698.6
70		5.3	694.4
60		9.8	689.9
50		10.8	688.9
40		10.9	688.8
30		10.0	689.7
20		9.2	690.5
10		9.1	690.6
4200		10.0	689.7

699.68 N 4660

4200		9.6	690.1
10		9.2	690.5
20		8.6	691.1
30		8.8	690.9
40		9.1	690.6
50		9.0	690.7
60		8.3	691.4
70		1.5	698.2
80		1.4	698.3
	711.16		
90		12.6	698.6
4300		12.2	699.0
	699.68		
10		2.7	697.0
20		3.8	695.9
30		4.5	695.2
40		4.6	695.1
50		4.0	695.7
	711.16		
60		10.5	700.7
67		6.1	705.1 O.G.
4370		7.6	703.6 O.G.

		N4670	
	711.16		
4370		8.5	702.7 O.G.
60		8.0	703.2 O.G.
50		10.8	700.4
	699.68		
40		2.3	697.4
30		3.2	696.5
20		2.7	697.0
10		2.4	697.3
4300		1.0	698.7
4290		0.9	698.8
	711.16		
80		12.8	698.4
70		13.0	698.2
	699.68		
60		3.0	696.7
50		5.9	693.8
40		6.5	693.2
30		7.5	692.2
20		8.0	691.7
10		8.7	691.0
4200		8.9	690.8

		N4680	
	699.68		
4200		8.5	691.2
10		8.4	691.3
20		7.5	692.2
30		6.6	693.1
40		5.2	694.5
50		2.0	697.7
	711.16		
60		13.6	697.6
70		13.1	698.1
80		12.4	698.8
90		11.8	699.4
4300		12.0	699.2
10		12.9	698.3
20		13.1	698.1
30		13.1	698.1
40		9.4	701.8
50		7.8	703.4
55		9.2	702.0 O.G.

711.16 **N4690**

4345		9.7	701.5 O.G.
35		5.9	705.3
25		11.0	700.2
10		11.7	699.5
4300		11.9	699.3
4290		12.1	699.1
80		12.2	699.0
70		12.8	698.4
60		13.3	697.9
50		14.8	696.4
40		16.4	694.8
30		17.4	693.8
	699.68		
20		7.1	692.6
10		8.1	691.6
4200		8.6	691.1

Plotted

N4700

4200		8.6	691.1
10		8.0	691.7
20		7.0	692.7
	711.16		
30		16.9	694.3
40		15.6	695.6
50		14.7	696.5
60		13.7	697.5

Plotted

711.16 **N4700**

4270		12.6	698.6
80		12.4	698.8
90		12.1	699.1
4300		11.6	699.6
10		11.2	700.0
20		10.3	700.9
30		10.1	701.1
40		10.2	701.0
T.P.		2.77	708.39
	5.52	713.91	
		0.24	713.67 = check on B.M. Elev. 713.70

Plotted Reduced by Grant

Final X Sections of Downstream Spoil Bank, For Material From Spillway Road.

(See Pages 57-69 - For original X sections)

Dec. 7-1934
Simpson
Soper
Sobell
Remmen
Salgado,

B.M. 1.80 "A" 715.50 713.70

T.P. 12.92 702.58

0.32 "B" 702.90

N 4470 is Original Ground.

N4480

"A" 715.50

E 4540	7.2	708.3
30	7.1	708.4
20	8.6	706.9
10	10.4	705.1
4500	12.6	702.9
4496	12.8	702.7 O.G.
	"B" 702.90	
70	11.0	691.9 O.G.
60	17.2	685.7
4447	24.5	678.4 O.G.

N4490

4442	23.8	679.1 O.G.
50	19.0	683.9
60	13.2	689.7
70	6.7	696.2

Plotted & Reduced. Dec. 24 C.B.K.

"A" 715.50

N4490

4480	13.6	701.9
90	9.2	706.3
4500	6.1	709.4
10	3.1	712.4
20	2.2	713.3
30	1.8	713.7
45 40	1.3	714.2 O.G.

N4500

4550	0.5	715.0 O.G.
4540	1.0	714.5
30	1.3	714.2
20	1.5	714.0
10	1.7	713.8
4500	2.2	713.3
4490	2.9	712.6
80	7.8	707.7
	"B" 702.90	
70	2.7	700.2
60	9.2	693.7
50	16.3	686.6
4439	23.7	679.2 O.G.

Reduced & Plotted by C.B.K.

N4510

"B"
702.90

4438	21.8	681.1 O.G.
50	14.0	688.9
60	6.2	696.7

"A"
715.50

70	11.3	704.2
80	3.7	711.8
90	2.6	712.9
4500	2.1	713.4
10	2.0	713.5
20	1.9	713.6
30	1.6	713.9
40	1.2	714.3
50	0.5	715.0

N4520

4550	1.3	714.2 O.G.
40	1.4	714.1
30	1.9	713.6
20	2.2	713.3
10	2.4	713.1
4500	2.5	713.0
4490	2.8	712.7
78	3.7	711.8
4470	8.5	707.0

Dec. 7-1934

"B"
702.90

N4520

4460	3.5	699.4
4454	7.3	695.6 O.G.

N4530

4452	7.2	695.7 O.G.
60	1.2	701.7

"A"
715.50

70	6.6	708.9
74	4.1	711.4
80	3.4	712.1
90	3.1	712.4
4500	3.0	712.5
10	2.9	712.6
20	2.8	712.7
30	2.4	713.1
4540	1.9	713.6

N4540

4530	3.0	712.5 O.G.
20	3.3	712.2
10	3.6	711.9
4500	3.6	711.9
4490	3.5	712.0
80	3.9	711.6

Reduced & Plotted by E.B.H.

N4540

"A"
715.50

4470	4.2	711.3
60	10.1	705.4

"B"
702.90

4447	7.0	695.9 O.G.

N4550

4445	6.7	696.2 O.G.
50	2.7	700.2

"A"
715.50

60	5.9	709.6
70	5.2	710.3
80	4.7	710.8
90	4.5	711.0
4500	4.1	711.4
10	4.3	711.2
20	4.0	711.5
4530	3.8	711.7 O.G.

N4560

4530	4.4	711.1 O.G.
20	4.6	710.9
10	4.7	710.8
4500	4.8	710.7
4490	5.0	710.5

Dec. 7-1934

N4560

"A"
715.50

4480	5.2	710.3
70	5.6	709.9
63	5.8	709.7
60	8.2	707.3

"B"
702.90

50	2.9	700.0
4444	6.5	696.4 O.G.

N4570

4433	6.2	696.7 O.G.
40	3.4	699.5

"A"
715.50

50	11.4	704.1
59	6.6	708.9
70	6.1	709.4
80	5.9	709.6
90	5.5	710.0
4500	5.5	710.0
4510	5.5	710.0 O.G.

N4580

4500	6.2	709.3 O.G.
4490	6.6	708.9
80	6.7	708.8

Plotted & Reduced by C.B.H.

N4580

"A" 715.50

4470	6.7	708.8	
60	6.7	708.8	
50	7.0	708.5	
40	10.1	705.4	
4430	11.5	704.0	O.G.

N4590

4470	7.5	708.0	O.G.
60	7.5	708.0	
50	7.5	708.0	
40	8.0	707.5	
30	7.6	707.9	
26	7.4	708.1	
20	11.0	704.5	
	"B" 702.90		
4410	4.9	698.0	O.G.

N4600

4401	5.6	697.3	O.G.
10	0.6	702.3	

Dec. 7-1934

N4600

"A" 715.50

4420	8.7	706.8	
30	8.3	707.2	
40	8.5	707.0	
4430	8.4	707.1	O.G.

N4610

4440	8.9	706.6	O.G.
30	9.1	706.4	
20	9.0	706.5	
10	8.9	706.6	
	"B" 702.90		
4400	0.9	702.0	
4387	4.0	698.9	O.G.

N4620

4380	2.6	700.3	O.G.
	"A" 715.50		
90	10.0	705.5	
4400	8.8	706.7	
10	9.2	706.3	
4420	9.4	706.1	
4430	9.4	706.1	O.G.

N 4630 is Original Ground.

Plotted & Reduced Dec. 34 [illegible]

B.M.	9.87	712.46		702.59	Grade
4028	F-1.00		+0.54	713.00	714.00
4036	F-1.00		+4.54	717.00	718.00
4044	F-1.50		+8.04	720.50	722.00
4052	F 1.00		+8.54	721.00	722.00
4060	F 1.00		+12.54	725.00	726.00
4068	F 1.00		+12.54	725.00	726.00
4076	F 1.00		+16.54	729.00	730.00

712.46
17
712.29

720.50
712.29
8.21

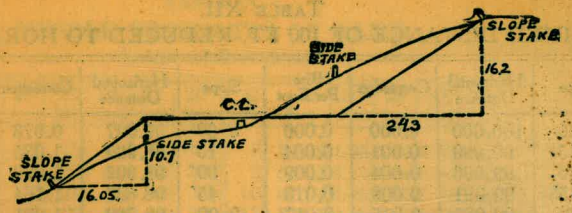
712.46
4.54
717.00

712.46
8.07
720.50
712.39
8.61

IMPROVED TABLES

AND

INFORMATION



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4.65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13.65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18.15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29 40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37 20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45 90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50 70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51 90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55 95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57 00	57.15	57 30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58 95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66 30	66.45	66.60	66 75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67 95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69 75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

Corewall
Elev. 740 – 4160 to 0+15

62.9
37.1
47.1

3203.5

N 4643.68
E 4514.42

7.52

2.68

2.4

63
67
130