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Spillway - Slope stakes

Oct. 26-1934.

B.M. 11.33 744.92 733.59

4+00 + 3.02 747.94 721.04

B.M. 10.51 744.10 733.59

4+25 0.00 744.10 720.35

4+50 2.63 741.47 719.67

B.M. 1.87 728.86
22.04
- 6.83 726.99

4+25 7.51 721.35

Oct. 31-1934.

B.M. 6.17 756.06 749.89

T.P. 3.02 753.04

8.87 761.91

4+71²¹ 1.03 760.88 Set Point

T.P. 12.71 749.20 X

4+87²⁹ 5.86 756.05^{subgrade} 718.65

B.M. 8.25 735.24 726.99

T.P. 10.46 743.74 1.96 733.28

5+00 + 2.2 745.9 Set Point

11⁹⁵ out from toe of slope (should be 13.85)

1⁹⁰ right

13.0

43.25
5.85
37.40
18.70
15.63
3.07

cut 26² out 13⁴⁵

cut 23²⁵ out 11²⁰

Set Point 13³⁸ out - 1⁵ Back of Subgrade

cut 21⁸⁰ out 10²⁰

23⁵¹ out from toe of slope

2⁶² off set to Subgrade at top of wall

cut 37²⁰ out 18²⁰

Grades Around Bottom of cone at East
end of Spillway

See Page 76

Oct. 26-1934

B.M.	1.20	751.09 ✓	749.89	
Finish Grade at Face of Wier (A)	6.09	745.00 ✓	744.20	Finish Grade
8' So. of Face of Wier (B) on toe of cone	9.56	741.53 ✓	743.60	F. 2 ⁶⁷
14' So. of Face of Wier (C) on toe of cone	9.21	741.88 ✓	743.00	F. 1 ⁷²
20' So. of Face of Wier (D) on toe of cone	9.24	741.85 ✓	742.60	F. 1 ¹⁵
24' So. of Face of Wier (E) on toe of cone	9.45	741.64 ✓	742.45	F. 0 ²⁶
25' So. of Face of Wier (F) on toe of cone (East end of cone)	9.67	741.42 ✓	742.45	F. 1 ⁰³
East edge of 10 Section	8.79	742.30 ✓	742.45	F. 0 ¹⁵

Oct. 27-1934

B.M.	5.24	755.13 ✓	749.89
"F"	12.68	742.45 ✓	
"E"	12.53	742.60 ✓	
"D"	12.13	743.00 ✓	
"C"	11.53	743.60 ✓	
"B"	10.93	744.20 ✓	

Simpson
Soper
Isbell

Grades For 20' Apron Along Face of Weir.

Oct. 29. 1934.

B.M.	4.47	754.36	749.89
At Face of Weir		9.36	745.00 ✓
21' South of Face of Weir		11.46	742.90 ✓
1' offset to edge of concrete			

Nov. 2-1934.

B.M.	2.79	752.68	749.89
T.P.		12.40	740.28
	1.50	741.78	
60' out from Face of Weir		2.78	739.00
38' " " " " "		0.58	741.20
28' " " " " "		+0.4	742.2
26' " " " " "		+0.6	742.4

Nov. 3-1934

B.M.	0.84	750.73	749.89
On Face of Weir (Finish Grade)		5.73	745.00
21' South of Face of Weir		7.83	742.90

Nov. 16-1934

B.M.	1.60	751.49	749.89
on Face of Weir (Finish Grade)		6.49	745.00
21' South of Face of Weir		8.59	742.90

Finish Floor Grades.

5.

Oct. 31-1934.

B.M. 3.37 730.36 ✓ 726.99

3+25 6.27 724.09 ✓

3+50 6.95 723.41 ✓

3+75 7.64 722.72 ✓

Nov. -1-1934.

B.M. 4.07 731.06 726.99

4+55 10.53 720.53 vertical cut 2.55

Set Point 188 out from Subgrade

4+71²¹ Slope stake 6.36 724.70 subgrade, 719.09Cut 5⁶ out 2⁸

4+25 9.71 721.35 vertical cut 7.00

Nov. 3-1934

B.M. 1.07 728.06 726.99

3+40 4.38 723.68

2+20 3.83 724.23

Nov. 7-1934.

B.M. 5.68 732.67 726.99

T.P. 11.57 721.10

6.94 728.04

4+87²⁹ 8.39 719.65 vertical cut 2.00

5+00 8.84 719.20 "

Top of Wall Points.

Nov. 7-1934.

B.M.	6.36	756.25	749.89	
T.P.		3.88	752.37	
	9.84	762.21		
A+40		0.71	761.50	set Point
A+10		0.13	762.08	" "

Nov. 8-1934

T.P.	10.46	762.83	752.37	
3+80		0.18	762.65	set Point
T.P.	2.80	755.17	752.37	
5+00		8.77	746.40	718.20

Nov. 9-1934

T.P.	2.74	755.11	752.37	
------	------	--------	--------	--

~~5+20~~

~~5+40~~

~~717.61~~

~~715.25~~

B.M.	7.30	731.89	724.59	
------	------	--------	--------	--

5+40		+ 1.22	733.11	set Point
------	--	--------	--------	-----------

5+20		+ 1.3	733.2	717.0
------	--	-------	-------	-------

Back of Subgrade at Elev. of Top of wall.
 Tight. to " " " " " "

22⁰⁵ out

19⁶⁹ out

for Elev. of top of wall only

cut 28² out 14¹

(should be 8⁹³ out)

6²² out. - 2²¹ tight

cut 16³ out 8¹

Vertical cuts And Finish Floor Grades

7

Nov. 7-1934.

B.M. 8.26 711.79 703.53

5+80		0.80	710.99	Vertical cut 2°05'
6+00		4.28	707.51	"
+20		8.34	703.45	"

Nov. 8-1934.

B.M. 1.83 728.82 726.99

4+10 7.05 721.77

Nov. 9-1934.

B.M. 1.87 728.86 726.99

4+30 7.65 721.21

4+50 8.19 720.67

B.M. 2.70 729.69 726.99

Set B.M. 5.10 724.59 Spike set

in Lead Plug in Side wall
Sta. 4+00 - Side wall stationing.

B.M. 11.95 745.54 733.59

4+71² slope stake 3.38 742.16 719.09Set Point 0²⁵ Back of Subgrade
cut 23°7' 1228 outNov. 12-1934.

B.M. 0.82 725.41 724.59

4+50 4.74 720.67

Top of Wall Points.

Nov. 12-1934.

B.M.	5.95	755.84		749.89	
T.P.			3.48	752.36	
	10.45	762.81			
3+80			0.16	762.65	Set Point for Elev. of top of wall only.

T.P.	10.46	762.82		752.36	
4+05		$\frac{61.50}{1.32}$	0.65	762.17	

Nov. 21-1934

B.M.	11.79	745.38		733.59	
5+80			2.58	742.80	Set Point 24^{57} out 8 ¹⁷ Back of Subgrade at Elev. of Top of Wall

B.M.	12.22	745.81		733.59	
5+58 ⁷¹			+ 2.06	747.87	Set Point 18^{17} out 1 ¹⁷ Back of Subgrade at Elev. of Top of Wall

B.M.	5.87	755.26		749.89	
			+ 4.74	760.00	

Nov. 22-1934.

B.M.	5.21	755.10		749.89	
5+13 ⁸⁵			+ 4.90	760.00	Set Point 29^{91} out 8 ⁶³ BACK of Subgrade at Elev. of Top of Wall Grade Break in top of Wall
			+ 5.20	760.30	

B.M.	5.35	755.24		749.89	
5+00			+ 5.06	760.30	Set Top of Wall Point at Subgrade.

B.M.	8.84	732.16		724.12	
			+ 2.92	735.08	

Nov. 12-1934.

B.M.	7.50	731.70		724.20	
5+58 ⁷⁰			5.42	726.28	713.08 cut 13 ³ out 65

B.M.	0.48	725.07		724.59	
5+00			5.87	719.20	
+20			7.06	718.01	

Nov. 14-1934

B.M.	0.59	725.18		724.59	
5+20			7.17	718.01	vertical cut 2 ⁰⁰
+40			8.93	716.25	"
+40	slope stake		+4.6	729.78	subgrade 715.25
+58 ⁷			11.10	714.08	cut 14 ⁵ out 72 ⁵

4+60			4.78	720.40	
------	--	--	------	--------	--

B.M.	0.55	725.14		724.59	
5+58 ²			11.06	714.08	
+20			7.13	718.01	

B.M.	7.83	732.03		724.20	
5+58 ²			5.71	726.32	713.08 cut 13 ² out 66 ⁰
			7.36	725.67	= B.M. Elev. 724.59

Finish Floor Grades,

Nov. 15-1934

B.M. 0.85 725.44 724.59

4+87²⁹ 5.79 719.65

B.M. 0.40 724.99 724.59

5+20 6.98 718.01

B.M. 4.38 749.38 745.00

6.48 742.90

Nov. 21-1934.

B.M. 12.95 737.54 724.59

5+40 slope stake 0.00 737.54 Subgrade 715.25

Nov. 23-1934.

B.M. 13.03 746.62 733.59

5+40 slope stake 3.37 743.25 715.25

Nov. 24-1934

B.M. 8.91 733.03 724.12

6+00 $\frac{7.17}{16.03}$ 6.52 726.51 706.51

724.59
2.02
726.61
725.65
0.96

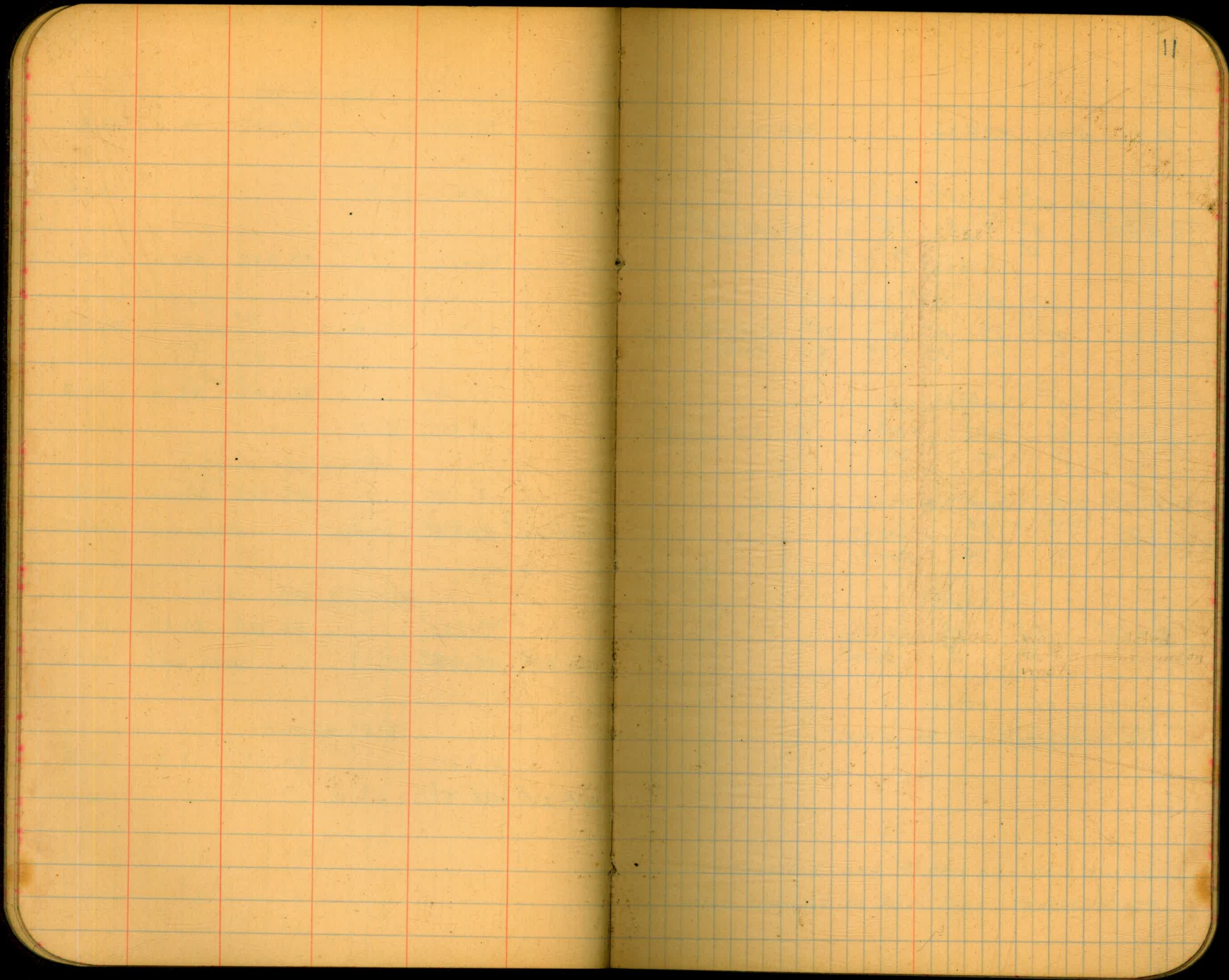
26.6
25.2
1.4

cut 22³ out 11¹⁵

6+12

cut 28⁰ out 14⁰⁰

cut 20⁰ out 10⁰



B.M. 4.22 728.34 724.12

6+40 $\begin{matrix} 724.3 \\ 4.9 \\ 0 \end{matrix}$ $\begin{matrix} 722.5 \\ 5.8 \\ 1 \end{matrix}$ $\begin{matrix} 722.8 \\ 5.5 \\ 19 \end{matrix}$ $\begin{matrix} 728.2 \\ 0.1 \\ 23 \end{matrix}$ $\begin{matrix} 727.7 \\ 0.6 \\ 40 \end{matrix}$ at toe of Bank.

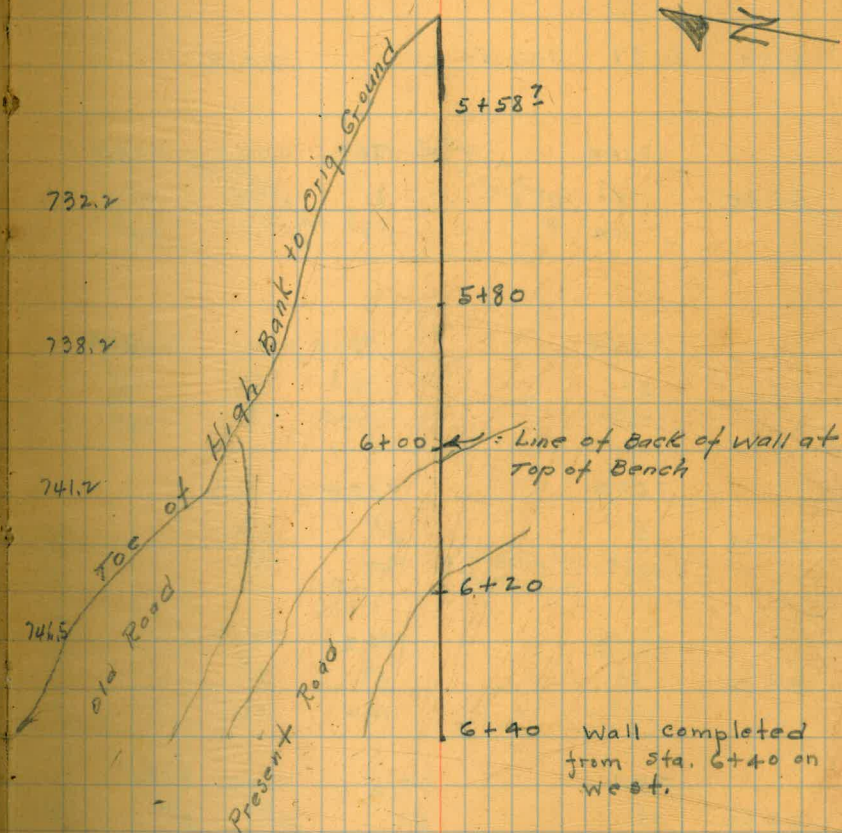
6+20 $\begin{matrix} 724.3 \\ 4.0 \\ 0 \end{matrix}$ $\begin{matrix} 723.1 \\ 5.2 \\ 1 \end{matrix}$ $\begin{matrix} 723.8 \\ 4.5 \\ 13 \end{matrix}$ $\begin{matrix} 728.3 \\ 0.0 \\ 19 \end{matrix}$ $\begin{matrix} 728.3 \\ 0.0 \\ 27 \end{matrix}$ at toe of Bank.

6+00 $\begin{matrix} 724.4 \\ 3.9 \\ 0 \end{matrix}$ $\begin{matrix} 731.1 \\ +2.8 \\ 19 \end{matrix}$ $\begin{matrix} 739.1 \\ +10.8 \\ 23 \end{matrix}$ Wall 8' Lower

5+80 $\begin{matrix} 726.5 \\ 1.8 \\ 0 \end{matrix}$ $\begin{matrix} 726.4 \\ 1.9 \\ 14 \end{matrix}$ at toe of Bank.

5+58? $\begin{matrix} 726.2 \\ 2.1 \\ 0 \end{matrix}$ $\begin{matrix} 726.3 \\ 2.0 \\ 5 \end{matrix}$ at toe of Bank.

No over-break at Sta. 5+45.



6+40 Wall completed from Sta. 6+40 on west.

X Sections are taken on wall stations and normal to the line shown above

X Sections Above North Spillway
 Slope to Determine amount of Material
 to be Put in for Ramp Down onto Spillway
 Floor.

X sections are taken Normal to \perp of
 Spillway and Distances are North From \perp .

B.M.	3.39	727.51		724.12
6+40	7244 3 ¹ 114 ²	= Top of Finished Wall, at inside edge	7244 3 ¹ 115 ³	7234 4 ¹ 115 ⁶
6+50	7214 6 ¹ 113 ⁴	"	7214 6 ¹ 114 ⁶	7228 4 ⁷ 115 ⁵
6+60	7224 5 ¹ 115 ⁶	Subgrade at Top of Bank	7224 5 ¹ 120	7223 5 ² 130
6+70	7222 5 ³ 116 ⁰	"	7223 5 ² 120	7222 5 ³ 130
6+80	719.7 7 ⁸ 116	"	721.5 6 ⁰ 118 ⁵	722.2 5 ³ 125
6+90	721.4 6 ¹ 119	"	721.7 5 ⁸ 130	722.1 5 ⁴ 130
7+00	721.2 6 ³ 118 ²	"	721.2 6 ³ 130	

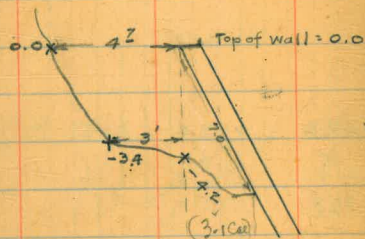
Nov. 23-1934.
 Simpson
 Paper
 Isbell.

Reduced Sec. 8-24 68H

X Sections Back of North Side Wall,
Sta. 7+52 to Sta. 7+90 to determine
Amount of Material required to
Back-Fill.

Nov. 27-1934

7+51 = 0.0.

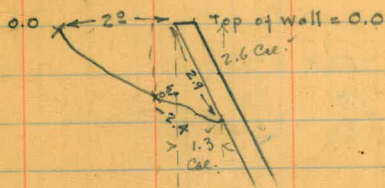


7+60

$$\text{Area} = \left(\frac{1.7 \times 3.4}{2} \right) + \left(\frac{3.4 + 4.2}{2} \times 3 \right) + \frac{4.2 \times 3.1}{2} = 20.80$$

$$\text{Vol.} = \frac{20.80 + 0}{2} \times 9$$

93.60

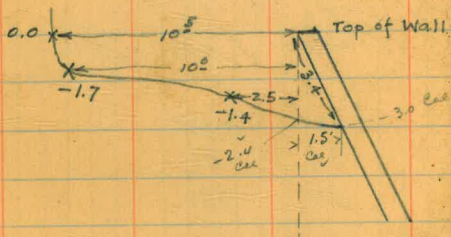


7+73

$$\text{Area} = \left(\frac{2.4 \times 1.5}{2} \right) + (2.4 \times 1.5) + \left(\frac{2.4}{2} \times 1.3 \right) = 4.56$$

$$\text{Vol.} = \frac{4.56 + 18.60}{2} \times 12 = 138.96$$

7+85



$$\text{Area} = \left(\frac{1.7 \times 1.5}{2} \right) + \left(\frac{1.7 + 1.4}{2} \times 1.5 \right) + \left(\frac{1.4 + 2.4}{2} \times 2.5 \right) + \left(\frac{2.4}{2} \times 1.5 \right) = 18.60$$

$$\text{Vol.} = \frac{18.60 + 0}{2} \times 5 = 46.50$$

7+90 = 0.0.

Total Cuft. = 443.90
" " Cufts. = 16.4

Simpson
Soper
Isbell
Remmen.

14

11/28/34
Cal by xxx.
checked " "

Area
Sgt. ✓
0.0

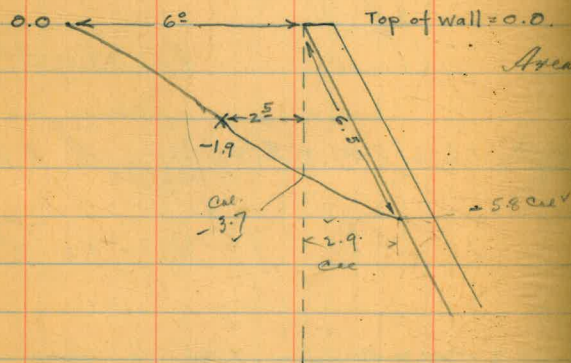
Vol. Cuft. ✓

X Sections Back of South Side Wall,
Sta. 10+90 to Sta. 11+23, to Determine
Amount of Material Required to
Back-Fill

Nov. 27-1934.

10+90 = 0.0.

11+08



11+23 = 0.0.

Simpson
Saper
Isbell
Remmen

15

11/28/34
Curtchley

Area
sq ft
0.0

cu ft

$$Vol. = \frac{0 + 15.69 \times 18}{2} = 141.21$$

$$Area = \left(\frac{1.9}{2} \times 3.5 \right) + \left(\frac{1.9 + 3.7}{2} \times 2.5 \right) + \left(3.7 \times \frac{2.9}{2} \right) = 15.69$$

$$Vol. = \frac{15.69 + 0}{2} \times 15 = 117.67$$

0.0

$$Total\ Cu\ ft = 258.88$$

$$" Cu\ yds = 9.6$$

Elevations of Pipes Set in Top of Dam
to Measure Movement.

Nov. 26-1934.

Simpson
Saper
Remmen
Isbell

20

B.M.	8.39	777.93	769.54	Plug at	North end of Dam - E4165.0
T.P.			3.78	774.15	
	4.80	778.95			
T.P.			7.35	771.60	
	4.55	776.15			
B.M.			6.48	769.67	Set in South end of Core Wall - E2998.0 Use this Elev. for checking Monuments.
	7.58	777.25			
N 3110			5.85	571.40	Top of 1 1/2" Pipe - East edge
"			5.87	571.38	" " " "
N 3220			4.90	572.35	Top of 1 1/2" Pipe - East Side
"			4.91	572.34	" " " "
N 3340			4.34	572.91	Top of 1 1/2" Pipe - East Side
"			4.34	572.91	" " " "
T.P.			4.33	772.92	
	6.47	779.39			
N 3460			5.58	773.81	Top of 1 1/2" Pipe - East Side
"			5.59	773.80	" " " "
N 3560			5.38	774.01	Top of 1 1/2" Pipe North edge
"			5.38	774.01	" " East edge

Elevs. of Pipe in Top of Dam cont'd.

Nov, 26-1934

21

779.39

N 3660

5.23 774.16 = Top of 1/2" Pipe - East Edge

"

5.24 774.15 " " 3" " " "

N 3760

5.77 773.62 Top of 1/2" Pipe - East Edge.

"

5.75 773.61 " " 3" " " "

T.P.

5.64 773.75

3.63 777.38

N 3860

4.48 772.90 Top of 1/2" Pipe - East edge.

"

4.48 772.90 " " 3" " " "

N 3960

5.15 772.23 Top of 1/2" Pipe - East edge

"

5.15 772.23 " " 3" " " "

N 4060

5.99 771.39 Top of 1/2" Pipe East edge

"

6.01 771.37 " " 3" " " "

B.M.

7.855 769.525 - check on B.M. Elev. 769.54.

Final X Sections of Spoil Material Left
in Spillway for Roadway.

These X sections are taken normal to Face Line
of the Ogee, and Distances are North from
The face of the Ogee. Sta. 0+00 to 5+00.

B.M. 1.24 751.13 749.89

	✓ 748.7	✓ 748.0	✓ 747.2	✓ 747.1
0-07	2 ⁴ 23	3 ¹ 30	3 ⁹ 40	4 ⁰ 50

	✓ 750.7	✓ 750.6	✓ 749.1	✓ 747.9
0+00	0 ⁴ 0	0 ⁵ 10	2 ⁰ 20	3 ² 30

	✓ 750.6	✓ 750.3	✓ 749.0	✓ 747.8
0+10	0 ⁵ 0	0 ⁸ 10	2 ¹ 20	3 ⁸ 30

	✓ 750.6	✓ 749.9	✓ 748.5	✓ 746.9
0+20	0 ⁵ 0	1 ² 10	2 ⁶ 20	4 ² 30

	✓ 750.3	✓ 749.6	✓ 747.4	✓ 745.9
0+30	0 ⁸ 0	1 ⁵ 10	3 ⁷ 20	5 ⁴ 30

Dec. 6-1934.

Simpson
Seper
Isbell
Remmen
Salgado,

23

	✓ 747.1	
	4 ⁰	intersection with side wall
	60	

	✓ 747.0	✓ 746.9	✓ 746.6
	4 ¹	4 ²	4 ⁵ intersection with side wall
	40	50	61 62

	✓ 746.1	✓ 745.6	✓ 744.9	✓ 744.7
	5 ⁰	5 ⁵	6 ²	6 ⁴
	40	50	60	65

	✓ 745.6	✓ 744.4	✓ 743.8	✓ 743.4
	5 ⁵	6 ⁷	7 ³	7 ²
	40	50	60	68

	✓ 744.5	✓ 743.6	✓ 742.8	✓ 742.4
	6 ⁶	7 ⁵	8 ³	8 ²
	40	50	60	72

Reduced Dec. 8. 34 G.B.H.
Checked By. 9.0 Dec. 14, 1934
Plotted

Plotted m. 20

751.13

	✓	✓	✓	✓	✓	✓	✓	✓	✓
	747.5	746.0	744.3	743.3	742.3	741.9	741.4	741.6	
0 + 40	3 ⁶ / ₁₁ on edge concrete	5 ¹ / ₂₀	6 ⁸ / ₃₀	7 ⁸ / ₄₀	8 ⁸ / ₅₀	9 ² / ₆₀	9 ⁷ / ₇₀	9 ⁵ / ₇₆	intersection with side wall
	✓	✓	✓	✓	✓	✓	✓	✓	
	740.5	742.8	742.0	741.2	740.7	740.3	740.3		
+ 50	10 ⁶ / ₂₀ on edge concrete	8 ³ / ₃₀	9 ¹ / ₄₀	9 ⁹ / ₅₀	10 ⁴ / ₆₀	10 ⁸ / ₇₀	10 ⁸ / ₇₉		"
	✓	✓	✓	✓	✓	✓	✓	✓	
	734.3	736.3	740.5	740.5	740.2	739.6	739.3	739.2	
+ 60	16 ⁸ / ₂₄ on edge concrete	14 ⁸ / ₃₀	10 ⁶ / ₃₇	10 ⁶ / ₄₀	10 ⁸ / ₅₀	11 ⁵ / ₆₀	11 ⁸ / ₇₀	11 ⁹ / ₈₂	"
changed to match sections	24								
T.P.	0.93	739.33	12.73	738.40					
	✓	✓	✓	✓	✓	✓	✓	✓	
	731.1	732.9	739.5	739.1	738.5	738.3	738.3	738.4	
0 + 70	8 ² / ₂₆ on concrete floor	6 ⁴ / ₃₀	10 ² / ₄₀	0 ² / ₅₀	6 ⁸ / ₆₀	1 ⁰ / ₇₀	1 ⁰ / ₈₀	0 ⁹ / ₈₆	"
	✓	✓	✓	✓	✓	✓	✓	✓	
Grade = 30.8	730.9	737.5	738.0	737.6	737.2	737.2	737.4		
0 + 80	8 ⁴ / ₃₀ on concrete Floor	1 ⁸ / ₄₁	1 ³ / ₅₀	1 ⁷ / ₆₀	2 ¹ / ₇₀	2 ¹ / ₈₀	1 ⁹ / ₈₉		"

Plotted
M.

	739.33													
30.5	7364	733.1	736.9	737.0	736.8	7364	736.4	7366						
0+90	8 ² 36	on Concrete Floor	6 ² 40	2 ⁴ 46	2 ³ 50	2 ⁵ 60	2 ² 70	2 ⁹ 80	2 ⁷ 93	= intersection with side wall				
	7303	731.9	736.6	736.5	7344	7361	735.7	735.8	736.0					
1+00	9 ² 38	"	7 ⁴ 40	2 ⁷ 47	2 ⁸ 50	2 ⁹ 60	3 ² 70	3 ⁶ 80	3 ⁵ 90	3 ³ 97				
	730.0	732.7	7361	735.8	735.8	735.6	735.4	735.5						
+10	9 ² 38	"	6 ⁶ 40	3 ² 44	3 ⁵ 50	3 ⁵ 60	3 ⁵ 70	3 ⁷ 80	3 ⁹ 90	3 ⁸ 100				
	729.7	732.2	734.7	734.8	734.7	735.6	735.5	735.6	735.3	735.4	735.5			
+20	9 ⁶ 38	"	7 ¹ 40	4 ⁶ 43	4 ⁵ 50	4 ⁶ 60	3 ⁷ 63	3 ⁸ 70	3 ⁷ 80	4 ⁰ 90	3 ⁹ 100	3 ⁸ 104		
	729.4	732.9	733.1	733.2	735.5	735.5	735.4	735.2	735.3	735.2				
+30	9 ¹ 38	"	6 ⁴ 42	6 ² 50	6 ¹ 60	3 ⁸ 62	3 ⁸ 70	3 ⁹ 80	4 ¹ 90	4 ⁰ 100	4 ¹ 109	108	Plotted.	
	729.2	731.1	731.6	731.7	734.9	735.3	735.2	734.9	734.8	734.8				
1+40	10 ² 38	"	8 ² 40	7 ² 50	7 ⁶ 60	4 ⁴ 64	4 ⁰ 70	4 ¹ 80	4 ⁴ 90	4 ⁵ 100	4 ⁵ 112			

739.33

	28.9	728.9	739.1	730.2	730.2	734.9
1+50	10 ⁵ 38	on Concrete Floor 40	9 ² 50	9 ¹ 62	9 ¹ 62	4 ⁴ 69

	728.6	729.1	729.0	729.0	734.7	
+60	10 ⁷ 38	"	10 ² 40	10 ³ 50	10 ³ 63	4 ⁶ 71

	728.3	734.1	734.5	734.2	734.1	
+70	11 ² 65	"	5 ² 74	4 ⁸ 80	5 ¹ 90	5 ² 100

	728.1	734.0	733.9	733.7	733.7	
+80	11 ² 70	"	5 ³ 78	5 ⁴ 90	5 ⁶ 100	5 ⁶ 110

	727.5	733.1	733.3	733.1	
2+00	11 ² 77	"	6 ² 85	6 ² 90	6 ² 100

	734.7	734.6	734.7	734.6	734.6	
	4 ⁶ 80	4 ⁷ 90	4 ⁶ 100	4 ⁷ 110	4 ⁷ 116	= intersection with side wall

	734.7	734.3	734.3	734.4	734.5
	4 ⁶ 80	5 ² 90	5 ² 100	4 ⁹ 110	4 ⁸ 120

	734.2	734.1	734.2	
	5 ¹ 110	5 ² 120	5 ¹ 124	"

	733.7	733.7	
	5 ⁶ 120	5 ⁶ 128	"

	733.0	732.9	733.1	733.2
	6 ³ 110	6 ⁴ 120	6 ² 130	6 ⁴ 135

739.33

	27.0	726.9	732.5	732.7	732.6	732.6	732.7	732.8	732.8	
Z+20	12 ⁴ 85	on concrete Floor	6 ⁸ 94	6 ⁶ 100	6 ⁷ 110	6 ⁷ 120	6 ⁶ 130	6 ⁵ 140	6 ⁵ 143	= intersection with Side wall

		726.4	731.9	732.3	732.0	731.9	732.3	732.3	
+40	12 ² 92	"	7 ⁴ 101	7 ⁵ 110	7 ³ 120	7 ⁴ 130	7 ² 140	7 ² 151	"

	25.9	725.8	731.8	731.9	731.5		731.6	731.8	731.7	
+60	13 ⁵ 101	"	7 ⁵ 110	7 ⁴ 120	7 ² 130		7 ² 140	7 ⁵ 150	7 ⁶ 157	"

T.P. 9.13 730.20

0.58 730.78

Check on B.M. 6.69 724.09 Rec. Elev. 724.12

730.78

	25.3	725.7	731.4	731.3	731.2		731.2	731.3	731.3	
Z+80	5 ⁴ 109	on concrete Floor	6 ⁶ 118	6 ⁵ 130	6 ⁴ 140		6 ⁴ 150	6 ⁵ 160	6 ⁵ 167	"

Dec. 6-1934.

28

730.78

	✓ 724.8	✓ 730.8	✓ 730.8	✓ 730.5	✓ 730.5	✓ 730.5	✓ 730.3	✓ 730.3	
3+00	6 ⁰ 116	on Concrete Floor	0 ⁰ 127	0 ⁰ 130	0 ³ 140	0 ³ 150	0 ³ 160	0 ⁵ 170	0 ⁵ 174 = intersection with Side Wall
	24.2 ✓ 724.3	✓ 730.6	✓ 730.3	✓ 730.1	✓ 730.1	✓ 730.0	✓ 729.6		
3+20	6 ⁵ 126	"	0 ² 134	0 ⁵ 140	0 ⁷ 150	0 ⁷ 160	0 ⁸ 170	1 ² 182	"
	✓ 723.7	✓ 729.4	✓ 729.4	✓ 729.7	✓ 729.6	✓ 729.3	✓ 729.1		
+40	7 ¹ 134	"	1 ⁴ 143	1 ⁴ 150	1 ¹ 160	1 ² 170	1 ⁵ 180	1 ⁷ 190	"
	✓ 723.1	✓ 728.7	✓ 729.4	✓ 729.3	✓ 728.3	✓ 728.7	✓ 728.6		
+60	7 ⁷ 140	"	2 ¹ 150	1 ⁴ 160	1 ⁵ 170	2 ⁰ 180	2 ¹ 190	2 ² 197	"
	✓ 722.6	✓ 728.9	✓ 729.2	✓ 728.8	✓ 728.5	✓ 728.3	✓ 728.2	✓ 728.1	
3+80	8 ² 146	"	1 ⁹ 155	1 ⁶ 160	2 ⁰ 170	2 ³ 180	2 ⁵ 190	2 ⁶ 200	2 ⁷ 205

730.78

	22.0	(722)	729.2	729.0	728.3	728.1	728.0	728.0		
A+00	8 ⁷ 151	on concrete Floor	16 ⁶ 161	18 ⁸ 170	25 ⁵ 180	27 ⁷ 190	28 ⁸ 200	28 ⁸ 213	= intersection with Side Wall	
	X									
	721.5		728.7	728.3	727.9		727.8	727.7	727.5	
+20	9 ³ 158	"	2 ¹ 168	2 ⁵ 180	2 ⁹ 190		3 ⁰ 200	3 ¹ 210	3 ³ 221	"
	20.9	(7210)	728.2	727.9	727.4		727.3	727.4	726.9	726.7
+40	9 ⁸ 165	"	2 ⁶ 174	2 ⁹ 180	3 ⁴ 190		3 ⁵ 200	3 ⁴ 210	3 ⁹ 220	4 ¹ 228
	720.4		727.4	727.1	726.5		726.4	726.3	726.2	726.2
+60	10 ⁴ 170	"	3 ⁴ 179	3 ⁷ 190	4 ³ 200		4 ⁴ 210	4 ⁵ 220	4 ⁶ 230	4 ⁶ 236
	19.8	(719.9)	726.3	726.6	726.0		725.8	725.7	725.6	725.7
+80	10 ⁹ 177	"	4 ⁵ 184	4 ³ 190	4 ⁸ 200		5 ⁰ 210	5 ¹ 220	5 ² 230	5 ¹ 240
	19.7	(7190)	725.9	726.2	725.9		725.6	725.4	725.3	725.6
+87 ²⁹	11 ² 179	"	4 ⁹ 187	4 ⁶ 190	4 ⁹ 200		5 ² 210	5 ⁴ 220	5 ⁵ 230	5 ² 240
	719.2		725.8	725.9	725.4		725.1	725.1	725.2	725.1
5+00	11 ⁶ 183	"	5 ⁰ 191	4 ⁹ 200	5 ⁴ 210		5 ⁷ 220	5 ⁷ 230	5 ⁶ 240	5 ⁷ 249

X Sections west of Sta. 5+10 and at Sta. 5+10
are Normal to ϕ of Spillway and Distances
are North from ϕ .

		730.78				
	X		X	✓	✓	✓
18.7	718.8		719.4	719.6	720.2	725.4
5+10	12 ⁸ 15	on concrete Floor	11 ⁴ 19	11 ³ 30	10 ⁶ 42	5 ⁴ 49
	✓		✓	✓	✓	
	718.0		720.0	720.7	721.8	724.2
5+20	12 ⁸ 25	"	10 ⁸ 28	10 ¹ 40	9 ⁰ 50	8 ⁶ 52
	✓		✓	✓	✓	
17.2	717.4		721.2	722.1	722.9	724.2
+30	13 ⁴ 32	"	9 ⁶ 40	8 ⁷ 50	7 ⁹ 60	6 ⁶ 62
T.P.			10.50		720.28	
	3.92	724.20				
	✓		✓	✓	✓	
	716.3	722.5	722.8	723.3		
+40	7 ⁹ 38	1 ⁷ 49	1 ⁴ 60	0 ⁸ 70		

Note: See Detail Plan of Finish
Floor Grades. Sta. 4+87²
to Sta 5+58²,

	✓	✓	✓	✓	✓	
	725.4	725.0	724.7	725.0	725.2	724.9
	5 ⁴ 60	5 ⁸ 70	6 ¹ 80	5 ⁸ 90	5 ⁶ 100	5 ⁹ 107
						intersection with side wall
	✓	✓	✓	✓	✓	
	725.1	724.8	724.4	724.5	724.8	724.5
	5 ⁷ 60	6 ⁰ 70	6 ⁴ 80	6 ³ 90	6 ⁰ 100	6 ³ 109
						"
	✓	✓	✓	✓	✓	
	724.3	724.2	724.3	724.6	724.4	
	6 ⁵ 70	6 ⁶ 80	8 ⁵ 90	6 ² 100	6 ⁴ 110	"
						✓
	✓	✓	✓	✓	✓	
	723.7	724.1	724.3	724.4		
	0 ⁵ 80	0 ¹ 90	+0 ¹ 100	+0 ² 111		"
						✓

724.20

	15.2	715	718.1	722.8	723.5	723.7
5+50	9 ¹ 44	on Concrete Floor	6 ¹ 50	1 ³ 60	0 ⁷ 70	0 ⁵ 80

	724.0	724.2	724.2
	0 ² 90	0 ⁰ 100	0 ⁰ 111

intersection with
Side Wall

	13.9	714.0	718.3	723.5	723.5	723.7
+60	10 ² 50	"	5 ² 60	0 ⁷ 68	0 ⁷ 80	0 ⁵ 90

	723.9	724.2
	0 ² 100	0 ⁰ 112

"

	12.5	712.6	716.5	723.4	723.4	723.4
+70	11 ² 52	"	7 ⁷ 60	0 ⁸ 70	0 ⁸ 80	0 ⁸ 90

	723.6	723.8
	0 ⁶ 100	0 ⁴ 112

"

	711.0	714.6	721.4	723.2	723.1	
+80	13 ² 55	"	9 ⁶ 60	2 ⁸ 70	1 ¹ 73	1 ¹ 80

	723.1	723.5	723.7
	1 ¹ 90	0 ⁷ 100	0 ⁵ 112

"

	709.3	712.6	722.0	723.1	
5+90	14 ⁹ 57	"	4 ⁶ 70	2 ² 72	1 ¹ 80

	723.2	723.3	723.8
	1 ⁰ 90	0 ⁹ 100	0 ⁴ 112

"

724.20

	✓		✓	✓	✓
	707.5		710.0	715.8	723.1
6+00	16 ⁷ 56	on concrete Floor	14 ² 60	8 ⁴ 70	1 ¹ 78

	✓		✓	✓	✓
	05.6	705.4	711.8	723.0	723.1
+10	18 ⁸ 60	"	12 ⁴ 70	12 ¹ 83	1 ¹ 90

	✓		✓	✓	✓
	03.5	703.4	708.7	717.0	722.9
+20	20 ² 62	"	15 ⁵ 70	7 ² 80	1 ² 87

	✓		✓	✓	✓
	01.2	700.9	705.9	714.5	722.4
+30	23 ³ 62	"	18 ³ 70	9 ⁷ 80	1 ⁸ 89

	✓		✓	✓	✓
	98.8	698.9	702.3	711.3	722.2
+40	25 ³ 64	"	21 ⁹ 70	12 ⁹ 80	2 ² 93

	✓	✓	✓	
	723.1	723.7	723.5	
	1 ¹ 90	1 ² 100	0 ⁷ 112	= intersection with side wall

	✓	✓		
	723.1	723.4		
	1 ¹ 100	0 ⁸ 112	"	

	✓	✓	✓	
	722.8	723.0	723.2	
	1 ⁴ 90	1 ² 100	1 ² 112	"

	✓	✓		
	723.0	723.4		
	1 ³ 100	0 ⁸ 112	"	

	✓	✓		
	723.0	723.5		
	1 ² 100	0 ⁷ 113	"	

724.20

	96.2	696.7	699.9	708.8	715.9
6+50	27 ⁵ 66	on Concrete Floor	24 ³ 70	15 ⁴ 80	8 ² 90

	93.6	693.5	698.7	706.4	712.7
+60	30 ⁷ 65		25 ⁵ 70	17 ⁸ 80	11 ⁵ 90

T.P.	0.29	711.51	12.98	711.22
------	------	--------	-------	--------

	90.8	690.9	694.7	701.3	707.6
+70	20 ⁶ 64	on Concrete Floor	16 ⁸ 70	10 ² 80	3 ⁹ 90

	87.8	687.9	690.1	695.0	701.3
+80	23 ⁶ 65	"	21 ⁴ 70	16 ⁵ 80	10 ² 90

	85.6	685.9	687.5	690.7	696.9
+87 ²⁹	25 ⁶ 65	"	24 ² 73	20 ⁸ 80	14 ⁶ 90

	722.6	723.0	723.1
	1 ⁶ 98	1 ² 110	1 ¹ O.G. 120

	717.9	722.4	722.7
	6 ³ 100	1 ⁸ 108	1 ⁵ O.G. 120

	711.9	716.1
+0 ⁴	100	112 ⁵

Subgrade slope

	705.8	707.6
	5 ² 100	3 ⁹ 108 ⁵

intersection with
side wall

	700.1	701.0
	11 ⁴ 100	10 ⁵ 106

Note: See original
Xsections on Page 13
of this Book (Sta. 6+40
to Sta. 7+00)

Reduced Dec. 8-24 1934
Checked F.O. Dec. 14, 1934

711.51
 T.P. 12.44 699.07
 0.10 699.17

	↓	✓	✓	✓	✓
81.6	6821	6834	6874	6903	6904
7+00	17 ¹ 75 on conc. Floor	15 ⁸ 80	11 ⁸ 90	8 ⁹ 100	8 ⁸ 1017

intersection with
side wall ✓

	↓	✓	✓	
78.4	6825	6807	6830	
7+10	20 ² 83 "	18 ⁵ 90	16 ² 99	=

" ✓

7+20 = 0.0.

check on B.M.

2.86 696.31 Rec. Elev. 696.36

40

46

47

Final X Sections - Spillway Floor And
Footing Subgrade.

Nov. 2-1934

B.M.	3.67	730.66		726.99
		720.5	719.8	719.9
4+16		10.3 182	10.9 183	10.9 186.2
		720.3	719.4	719.2
4+26		10.4 185.5	11.3 186	11.5 189.3
		721.2		721.2
4+36		10.8 189.6	11.6 191	11.8 193.6
		719.9	719.1	718.9
				721.1

B.M.	3.99	730.98		726.99
		719.1	718.4	718.3
4+46		11.2 192.4	12.6 193.4	12.7 199
		720.5		720.5
+56		11.3 196	11.8 196.5	12.5 201.2
		720.7		720.7
+64		11.7 199.2	12.5 199.7	12.5 204.7
		720.5		720.5

Reduced & Plotted C.B.A.
Ch for 11-27-34

10.90 720.08 on vertical cut sta. 4+71.2

Elev. 720.09

J.S. ✓

Final X Sections - Spillway Footing
Trench at toe of North Wall.

Nov. 8-1934.

B.M. 2.74 729.73 726.99
T.P. 8.85 720.88
3.77 724.65

4+75	719.2 5.4 202.4	718.1 6.5 204.0	718.1 6.5 206.2	720.0 4.6 208.1
+85	718.9 5.7 206.7	717.8 6.8 207.8	717.8 6.8 209.8	719.6 5.0 210.7
4+95	718.5 6.1 209.2	717.4 7.2 209.4	717.4 7.2 212.6	719.3 5.3 213.2

Plotted C.P.A.
Reduced vol.

J.S. ✓

5.44 719.21 on Vertical Cut at Sta. 5+00
Elev. 719.20.

Final X Sections - Spillway Floor
Subgrade - Nov. 14-1934.

52

0.59 725.18 724.59

	720.5 ←	720.4 ←	720.5 ←
4 + 26	47	48	47
	150	170	182

	720.1 ←	720.0 ←	
4 + 36	51	52	
	160	180	

	719.9 ←	719.5 ←	719.7 ←
4 + 46	53	52	55
	160	180	190

	719.5 ←	719.3 ←	719.2 ←
4 + 56	52	59	60
	160	180	194

Plotted & Reduced G.A.H. for

Nov. 15-1934

B.M. 0.45 725.04 724.59

	719.0 ←	719.1 ←	719.4 ←
4 + 64	60	59	56
	165	180	195

	718.6 ←	718.8 ←	719.2 ←
+ 75	64	62	58
	170	185	200

	718.5 ←	718.5 ←	718.9 ←
+ 85	65	65	61
	170	185	200

J.S. ←

725.04

4+95

717.8	718.4	718.2	718.1	718.4
7 ²	6 ⁵	6 ⁸	6 ⁹	6 ⁵
145	160	170	185	200

5+05

717.6	717.6	717.7	718.0	718.3	717.0
7 ⁴	7 ⁴	7 ³	7 ²	6 ³	8 ²
145	160	180	200	212	212 ³

J.S.V.

5.83 719.21 on Finish

Grade Pin - sta. 5+00
Elev. 719.20Plotted & checked
2/24/34
11-27-34

717.0	718.4
8 ²	6 ²
215	215 ⁵

$$\begin{array}{r} 744.50 \\ .150 \\ \hline 743.00 \end{array}$$
$$\begin{array}{r} 749.89 \\ 5.36 \\ \hline 755.25 \\ 11.7 \\ \hline 743.55 \end{array}$$

Final X Sections of Apron Subgrade
Along South Side of Weir.

Jimpson
Soper
Isbell

68

Oct. 30 - 1934.

Distances Are South From Face of Weir, and
Stations are Crest Stationing.

B.M. 1.60[✓] 751.49[✓] 749.89

connect to curve around Bottom of Cone.

	7440	7436	7428	7414	7414	7428
0 + 10	7 ⁵	7 ²	8 ⁷	10 ¹	10 ¹	8 ⁷
	0	10	18 ⁷	18 ²	19 ²	20

	7444	7438	7427	7414	7414	7425
0 + 25	7 ¹	7 ⁸	8 ⁸	10 ¹	10 ¹	9 ²
	0	10	18 ³	18 ⁵	19 ²	20

	7444	7434	7428	7423	7414	7414	7425
+ 28	7 ¹	8 ¹	9 ¹	9 ²	10 ¹	10 ¹	9 ²
	0	12	14	18	19	19 ²	20

	7446	7436	7426	7413	7413	7425
+ 30	6 ⁹	7 ⁹	8 ⁹	10 ²	10 ²	9 ²
	0	10	18 ⁵	18 ⁵	19 ²	20

	7445	7434	7427	7413	7413	7427
0 + 50	7 ⁰	8 ¹	8 ⁸	10 ²	10 ²	8 ⁸
	0	10	18 ⁸	18 ⁹	19 ²	20

Nov. - 5 - 1934

B.M. 1.72 751.61[✓] 749.89

	7443	7436	7427	7417	7418	7430
0 + 70	7 ³	8 ⁰	8 ⁹	9 ⁹	9 ⁸	8 ⁶
	0	10	18 ⁵	18 ⁸	20	20

Reduced Dec 8 - 34 B.S.M.

Final X sections of Apron Subgrade. Nov. 3-1934
Cont'd.

Simpson
Soper
Isbell

69

751.61

	7444	743.5	742.6	741.5	741.5	743.0
0 + 90	7 ² 0	8 ¹ 10	9 ⁰ 18	10 ¹ 18 ²	10 ¹ 19 ⁴	8 ⁶ 19 ⁵

	7444	743.3	742.6	741.4	741.4	743.0
1 + 10	7 ² 0	8 ³ 10	9 ⁰ 18	10 ² 18 ²	10 ² 19 ⁶	8 ⁶ 19 ⁵

	7442	743.5	742.8	741.6	741.6	742.9
1 + 30	7 ² 0	8 ¹ 10	8 ⁸ 18 ²	10 ⁰ 18 ⁴	10 ⁰ 19 ²	8 ⁷ 19 ²

1.72 ✓
749.89 B.M.
Elev. 749.89

Nov. 17-1934.

B.M.	4.38	749.38		745.00
------	------	--------	--	--------

	7445	743.5	742.7	741.7	741.7	742.6
1 + 50	4 ⁹ 0	5 ⁹ 10	6 ⁷ 18 ⁵	7 ⁷ 18 ⁶	7 ⁷ 20	6 ⁸ 20

	7446	743.5	742.8	741.8	741.8	742.6
1 + 70	4 ⁸ 0	5 ⁹ 10	6 ⁶ 18 ³	7 ⁶ 18 ⁴	7 ⁶ 20	6 ⁸ 20

	7445	743.5	742.6	741.8	741.8	742.5
+ 90	4 ⁹ 0	5 ⁹ 10	6 ⁸ 18 ⁴	7 ⁶ 18 ⁵	7 ⁶ 20	6 ⁹ 20

	7446	743.5	742.6	741.6	741.6	742.5
2 + 10	4 ⁸ 0	5 ⁹ 10	6 ⁸ 18 ⁵	7 ⁸ 18 ⁶	7 ⁸ 19 ⁹	6 ⁹ 20

Final Xsections of Apron Subgrade Cont'd.
Nov. - 17 - 1934.

Simpson
Soper
Isbell.

70

749.38

	7445	7435	7426	7417	7417	7424
2+30	4 ⁹ 0	5 ⁹ 10	6 ⁸ 18 ²	7 ⁷ 18 ⁵	7 ⁷ 19 ⁷	7 ⁰ 19 ¹

	7445	7435	7426	7416	7416	7424
+50	4 ⁹ 0	5 ⁹ 10	6 ⁸ 18 ⁴	7 ⁸ 18 ⁵	7 ⁸ 19 ⁸	7 ⁰ 19 ⁸

	7445	7435	7425	7414	7413	7423
+70	4 ⁹ 0	5 ⁹ 10	6 ⁹ 18 ⁴	8 ⁰ 18 ⁵	8 ¹ 19 ⁹	7 ¹ 20

	7444	7433	7425	7414	7414	7423
+90	5 ⁰ 0	6 ¹ 10	6 ⁸ 18 ⁴	8 ⁰ 18 ⁵	8 ⁰ 20	7 ¹ 20

	744.5	7435	7426	7415	7415	7424
3+10	4 ⁹ 0	5 ⁹ 10	6 ⁸ 18 ⁵	7 ⁹ 18 ⁶	7 ⁹ 20	7 ⁰ 20

	7445	7435	7428	7417	7417	7428
+30	4 ⁹ 0	5 ⁹ 10	6 ⁶ 18 ³	7 ⁷ 18 ⁴	7 ⁷ 19 ⁹	6 ⁶ 19 ⁹

	744.5	743.6	742.7	741.6	741.5	7424
+50	4 ⁹ 0	5 ⁸ 10	6 ⁷ 18 ⁵	7 ⁸ 18 ⁶	7 ⁹ 19 ⁹	7 ⁰ 20

+70	5¹ 0	5⁸ 10	6⁷ 18³	7⁷ 18⁴	7⁷ 19⁹	6⁹ 19⁸
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Reduced Dec. 8 - 34

See next page

Final xsections of Apron Subgrade Cont'd.

Nov. 17-1934.

Simpson
Soper
Isbell

71

749.38

3+90	4⁹	5⁷	6⁷	7⁸	7⁸	6⁹
	0	10	18 ⁴	18 ⁶	19 ⁷	19 ⁹

4.38 745.00 = Finish

Grade at Face of Weir

Nov. 19-1934

Finish Gr.
at Face of Weir

3.87 748.87 745.00

744A 743.6 742.8 741.7 741.7 742.6

3+70	4 ⁵	5 ³	6 ¹	7 ²	7 ²	6 ³
	0	10	18 ³	18 ⁴	19 ⁶	19 ⁸

744.6 743.6 742.8 741.7 741.7 742.6

+90	4 ³	5 ³	6 ¹	7 ²	7 ²	6 ³
	0	10	18 ⁵	18 ⁶	19 ⁷	19 ⁸

744.6 748.5 742.4 741.6 741.4 742.8

4+10	4 ³	5 ⁴	6 ⁵	7 ³	7 ⁵	6 ¹
	0	10	18 ⁶	18 ⁷	20	20

744.5 743.4 742.6 741.6 741.6 742.6

+30	4 ⁴	5 ⁵	6 ³	7 ³	7 ³	6 ³
	0	10	18 ⁶	18 ⁷	20	20

744.5 743.5 742.7 741.6 741.6 742.7

+50	4 ⁴	5 ⁴	6 ²	7 ³	7 ³	6 ²
	0	10	18 ⁴	18 ⁵	20	20

Final X sections of Apron Subgrade
cont'd. - Nov. 19-1934

Simpson
Soper
Isbell

72

748.87

	744.3	743.5	743.0	742.0	741.9	743.1
4+70	4 ⁶	5 ⁴	5 ²	6 ²	7 ⁰	5 ⁸
	0	0	18 ⁰	18 ³	19 ²	20

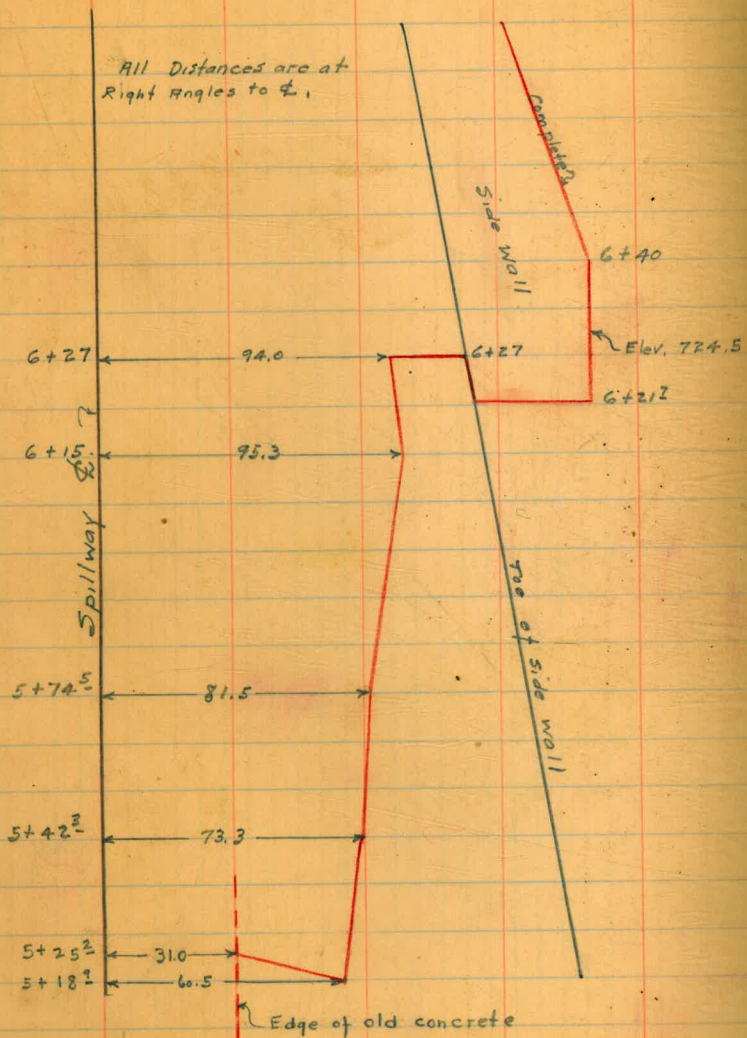
	744.4	743.5	742.7	741.9	741.9	742.9
+90	4 ⁵	5 ⁴	6 ²	7 ⁰	7 ⁰	5 ⁹
	0	10	18 ⁰	18 ⁵	20	20

	744.3	743.6	742.6	741.8	741.8	743.1
5+05	4 ⁶	5 ³	6 ³	7 ¹	7 ¹	5 ⁸
	0	10	18 ³	18 ⁵	20	20

3.86 745.01 = Elev. 745.00

Out Line of Concrete in Place in Spillway
Floor And Side Wall - Oct. 30-1934.

78



Concrete Floor Completed in upper
Spillway East of Sta. 3+03. 10/30/34.

Red Lines indicate Limits of concrete Paured to Date.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope from side or vertical
table for any width roadway, slope 1 to 1
If ground is nearly level, the cut or fill at any
table is located by the number given in the
left column and top row. The number in the
of table is same row and column as distance
from side to slope table. It should be not

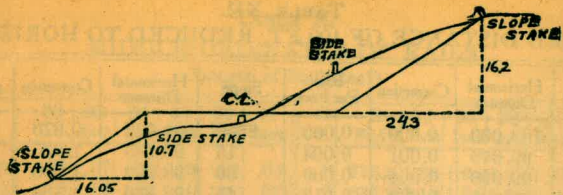
IMPROVED TABLES

AND

INFORMATION

TABLE No. 2.

To find Top and External for curve of
any other degree divide by degree of curve and
add constant found in column of constant
General curve with a given I and R
by dividing I by R and finding the result in
the column for constant.
The distance from a point on the roadway to
the curve is not given by the table.
It should be found by the table.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

X Sections
 N 33 00 From Elev.
 3560 650 to 650
 3700

8.567
 20.49
 77103
 51402
 17134
 17725.123

120
 20.57
 20.46
 5043' = 5+20
 2.59
 8042' = 5+00

Sta 3+80

26.81
 80.43
 5.36
 8577

26.81
 5.36
 32.17
 2=46

7+40.00
 5+58.70
 181.30
 6642
 3626
 7252
 10878
 10878
 120419.26
 9550
 10750
 100.62
 6.92

8.567
 20.91
 8567
 77103
 17134
 17913597
 120
 59
 99724
 100.9
 897516
 99724
 100.621516

8.567
 1935
 42835
 25701
 77103
 8567
 16577.145
 120

~~0-112 = 175.3~~

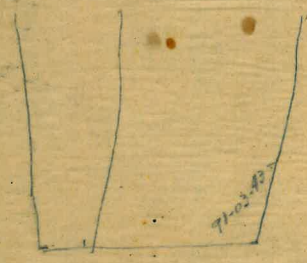
61
 1018
 488
 51
 1098

25.7
 18
 31
 74.7

564.25 = East end
 565.00 = West end

15.8
 0+006
 11.2

18W



712862
 90
 1775960
 1612843
 183115

7234.29
 712846
 1-03-43

895960
 183115
 712845
 895960
 723229
 172731
 712845

885616
 712840
 1800000

