

W
505

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

505⁷⁰ 2524 ft

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

F03 316

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1 1/2 see inside of back cover.

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Made in U. S. A.

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to b
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exam
30.6

Index

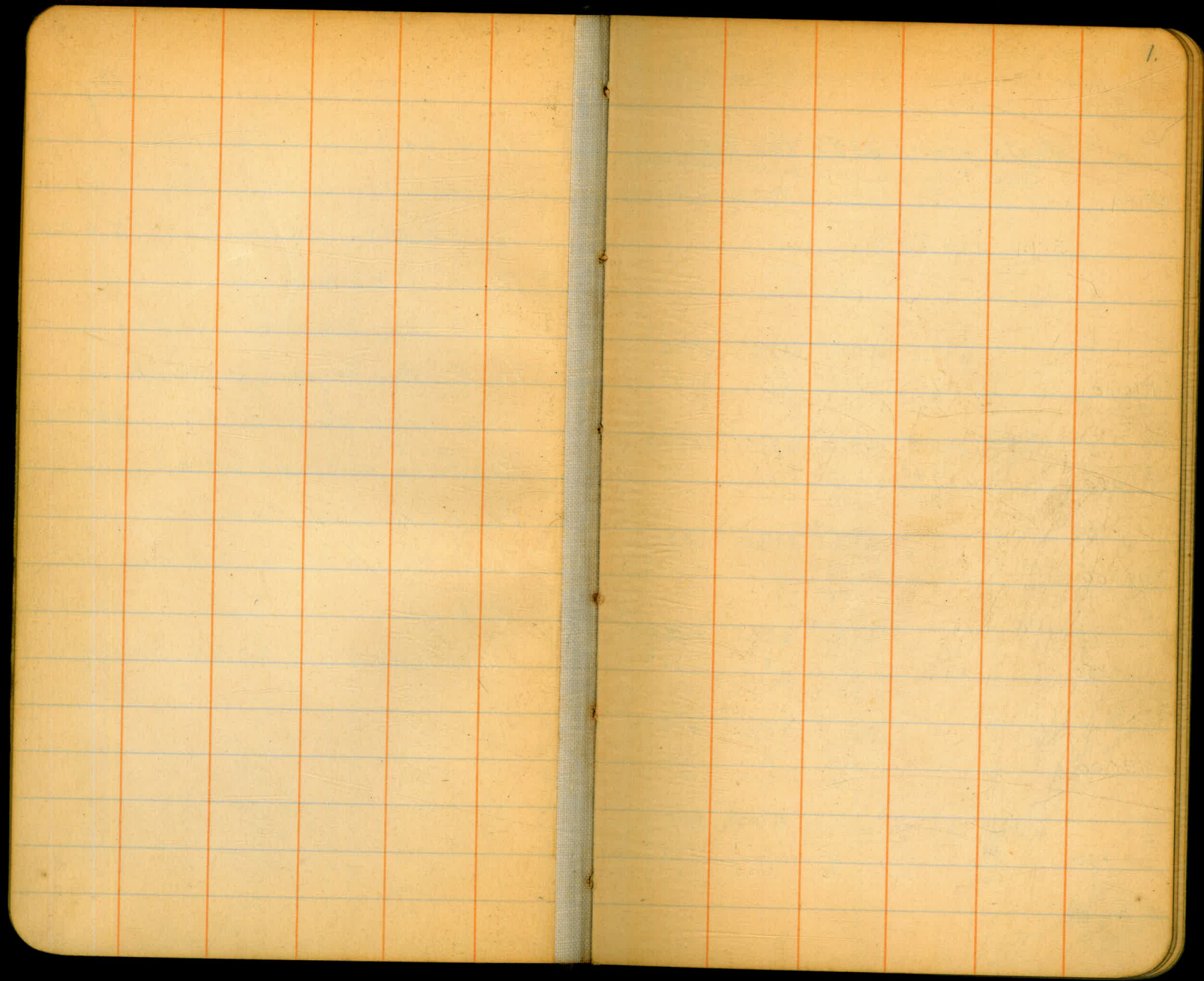
Pages

Profile & x'secs of Co.
road loc. from sta.
97 to sta. 100+15 2-25

Profile & x'secs of Co.
road loc. from Lakeside
to El Monte pump station
sta. 0+00 to sta. 97 26-55

Profile & x'secs of al-
ternate line, Co. road
loc. from sta. 99 to
sta. 127. 56-63

Bench levels El Capitan Dam to Pump Plant 64-79



Profile And Cross-sections of Co. Road
 Survey #512, From El-Monte Pumping Plant
 To El-Monte Park.

March-30-1935
 Hill-Simpson
 Soper-Remmen.

2.

Contd. from page 55, this book.
 See Page 56, this Book, For Alter. note Lines.

B.M. 438.93 U.S.G.S. Gauging Sta. At El-Monte Pumping Plant.

5.74 444.67

	L.			Φ	R.	
97+00	437.1 7 ⁸ 25	437.2 7 ⁵ 20	437.5 7 ² 13	437.8 6 ⁹	437.3 7 ¹ 13	438.5 6 ² 30
+50	437.3 7 ⁴ 24	437.1 7 ⁶ 19	437.3 7 ³ 13	437.7 7 ²	437.6 7 ¹ 20	437.8 6 ⁹ 30
98+00		437.0 7 ⁷ 24	437.5 7 ² 13	438.1 6 ⁶	438.1 6 ⁶ 15	438.2 6 ⁵ 30
+50		438.1 6 ⁶ 23	438.1 6 ⁶ 13	438.5 6 ²	438.5 6 ² 15	438.6 6 ¹ 30
99+00		438.5 6 ² 21	438.7 6 ⁹ 13	438.9 5 ⁸	438.4 6 ³ 15	438.9 5 ⁸ 29
+50	436.1 8 ⁶ 30	436.8 7 ⁹ 21	439.4 5 ³ 16	439.3 5 ⁴ 13	439.1 5 ⁶	438.4 6 ³ 13
					441.4 3 ³ 29	

1/5/35 - ab
 plotted
 2/12/35

+ Sec - Plotted
 G.W.G.
 4/2/35

444.67

	434.3 ✓	434.3 ✓	440.0 ✓	439.9 ✓	439.5 ✓
100+00	10 [±]	10 [±]	4 [±]	4 [±]	5 [±]
	38	28	16	13	

+50	434.3 ✓	434.7 ✓	440.1 ✓	440.0 ✓	439.7 ✓
	10 [±]	10 [±]	4 [±]	4 [±]	5 [±]
	40	30	21	13	

101+00	434.5 ✓	435.0 ✓	440.5 ✓	440.0 ✓	439.4 ✓
	10 [±]	9 [±]	4 [±]	4 [±]	5 [±]
	35	29	21	13	

+50	434.7 ✓	434.8 ✓	439.9 ✓	439.6 ✓	439.3 ✓
	10 [±]	9 [±]	4 [±]	5 [±]	5 [±]
	40	30	20	13	

T.P.

4.85 439.82

4.32 444.14

102+00	434.6 ✓	436.1 ✓	440.0 ✓	439.5 ✓	439.1 ✓
	9 [±]	8 [±]	4 [±]	4 [±]	5 [±]
	32	24	18	13	

+50	434.9 ✓	435.6 ✓	439.8 ✓	439.4 ✓	439.0 ✓
	9 [±]	8 [±]	4 [±]	4 [±]	5 [±]
	34	24	18	13	

	438.5 ✓	444.0 ✓	449.0 ✓
	6 [±]	0 [±]	+4 [±]
	11	14	26

	438.8 ✓	448.8 ✓	453.8 ✓
	5 [±]	+4 [±]	+9 [±]
	8	12	27

	438.9 ✓	451.9 ✓	456.9 ✓
	5 [±]	+7 [±]	+12 [±]
	8	13	22

	439.0 ✓	445.0 ✓	453.0 ✓	458.0 ✓
	5 [±]	+0 [±]	+8 [±]	+13 [±]
	10	12	20	30

Cut is Shale and Shattered Rock, Formation

Plotted
G.W.C.
1/14/35

	444.14	L.	4	R.	
103+00	435.0 9 ¹ 27	435.3 8 ⁸ 19	439.7 4 ⁷ 13	438.9 5 ²	438.4 5 ⁷ 14
+50	435.3 8 ⁸ 20	435.8 8 ³ 13	436.1 8 ⁰ 10	439.3 4 ⁸ Edge Rd. 5 Rd.	438.9 5 ²
+81	435.3 8 ⁸ 28	435.8 8 ³ 13	436.0 8 ¹ 6	439.4 4 ⁷ Edge Rd. Rd.	438.8 5 ² 7
104+00	435.6 8 ⁵ 24	435.5 8 ⁶ 13	435.6 8 ⁵ 6	437.4 6 ²	439.5 4 ⁶ outside Edge Rd. 4 Rd.
+50	435.6 8 ⁵ 22	435.5 8 ⁶ 13	435.6 8 ⁵ 9	436.7 7 ⁴	439.1 5 ⁰ outside Edge Rd. 13
105+00		435.5 8 ⁶ 25	436.7 7 ⁴ 13	436.6 7 ⁵	437.9 6 ² 20
+50		435.9 8 ² 25	435.9 8 ² 13	437.6 6 ⁵	438.1 6 ⁰ 25
106+00		436.1 8 ⁰ 25	436.5 7 ⁶ 13	437.7 6 ⁴	438.1 6 ⁰ 25

Plotted
G.W.G.S.
A.A.-35

	444.14 ✓	L.	¢	R.				
106+50		436.1 ✓ 8 ⁰ 25	436.7 ✓ 7 ² 13	437.1 ✓ 7 ⁰	438.3 ✓ 5 ⁸ 25			
107+00		438.5 ✓ 5 ⁶ 25	438.1 ✓ 6 ⁰ 13	436.3 ✓ 7 ⁸	437.7 ✓ 6 ⁹ 16	438.6 ✓ 5 ⁵ 35	441.1 ✓ 3 ⁰ 45	outside Edge Rd.
T.P.	9.40	7.58	436.56 ✓					
	445.96 ✓							
+50		439.1 ✓ 6 ³ 25	438.9 ✓ 7 ¹ 13	437.7 ✓ 8 ⁸	436.8 ✓ 9 ² 17	438.7 ✓ 7 ² 20	438.7 ✓ 7 ³ 25	
108+00	440.6 ✓ 5 ⁴ 30	440.6 ✓ 5 ⁴ 25	438.9 ✓ 7 ¹ 13	438.3 ✓ 7 ² 10	438.5 ✓ 7 ⁵	436.7 ✓ 9 ³ 27	438.6 ✓ 7 ⁴ 30	439.4 ✓ 6 ⁶ 40
+50		439.7 ✓ 6 ⁸ 25	438.1 ✓ 7 ² 13	438.1 ✓ 7 ²	436.9 ✓ 9 ¹ 26			
109+00		438.3 ✓ 7 ⁷ 25	438.6 ✓ 7 ⁴ 13	438.4 ✓ 7 ⁶	437.6 ✓ 8 ⁴ 18	439.4 ✓ 6 ⁶ 28	442.7 ✓ 3 ³ 55	outside Edge Rd.

Plotted
6.A.G.
A-A-35

	445.96 ✓	L.	£.	R.	
		440.0 ✓	440.0 ✓	440.0 ✓	440.0 ✓
109+50		60 25	58 13	58	60 25
		439.8 ✓	439.8 ✓	439.7 ✓	440.1 ✓
110+00		60 25	60 13	60	50 25
		440.4 ✓	440.5 ✓	440.5 ✓	440.7 ✓
+50		50 25	55 13	55	50 25
		440.5 ✓	440.8 ✓	440.6 ✓	441.0 ✓
111+00		55 25	50 13	50	50 25
		441.5 ✓	441.7 ✓	441.7 ✓	442.4 ✓
+50		45 25	48 13	48	30 80 [±]
		440.4 ✓	440.5 ✓	440.6 ✓	441.1 ✓
112+00		50 25	55 13	50	40 25
		440.4 ✓	440.6 ✓	440.7 ✓	440.8 ✓
+50		50 25	50 13	50	50 25
		440.5 ✓	440.5 ✓	440.4 ✓	440.3 ✓
113+00		55 25	55 13	50	50 25

outside
Edge Rd.

21[±] outside
Edge Rd.
115[±]

Plotted
G.W.G.
A-5-35

Cont'd. From Page 6.

March-30-1935.

7.

	445.96 [✓]	L.	£.	R.
113+50		AA1.5 [✓] 4 ⁵ 25	AA0.9 [✓] 5 ¹ 13	AA1.0 [✓] 5 ⁰ 25
114+00		AA2.2 [✓] 3 ⁸ 25	AA2.4 [✓] 3 ⁶ 13	AA2.4 [✓] 4 ³ 25
+50		AA2.3 [✓] 3 ⁷ 25	AA2.5 [✓] 3 ⁵ 13	AA2.8 [✓] 3 ² 25
115+00		AA2.6 [✓] 3 ⁴ 25	AA2.7 [✓] 3 ³ 13	AA2.8 [✓] 3 ² 25
T.P.		3.15	442.81 [✓]	
	5.48	448.29 [✓]		
+50		AA2.0 [✓] 5 ³ 25	AA2.9 [✓] 5 ⁴ 13	AA2.8 [✓] 5 ⁵ 25
116+00		AA2.9 [✓] 5 ⁴ 25	AA2.9 [✓] 5 ⁴ 13	AA2.1 [✓] 6 ³ 25
				AAA.8 [✓] 1 ² outside 112 ² Edge Rd.

Plotted
C.W.C.
4/6/35

	448.29	L.	¢
116+50	441.9 ✓ 6 ⁴ 25	441.6 ✓ 6 ⁷ 13	441.9 ✓ 6 ⁴
117+00	442.5 ✓ 5 ⁸ 25	442.5 ✓ 5 ⁸ 13	442.5 ✓ 5 ⁸
+50	442.8 ✓ 5 ⁵ 25	443.0 ✓ 5 ³ 13	443.1 ✓ 5 ²
118+00	443.0 ✓ 5 ³ 25	443.1 ✓ 5 ² 13	443.1 ✓ 5 ²
+50	443.4 ✓ 4 ⁹ 25	443.3 ✓ 5 ⁰ 13	443.0 ✓ 5 ³
119+00	443.7 ✓ 5 ¹ 25	443.7 ✓ 5 ¹ 13	443.4 ✓ 4 ⁹
+50	443.8 ✓ 4 ⁵ 25	444.1 ✓ 4 ² 13	444.7 ✓ 4 ¹
120+00	443.8 ✓ 4 ⁵ 25	443.9 ✓ 4 ⁴ 13	444.0 ✓ 4 ³

	R.
	441.8 ✓ 6 ⁵ 25
	442.9 ✓ 5 ⁴ 25
	446.8 ✓ 1 ⁵ = outside 125 [±] Edge Rd.
	443.7 ✓ 5 ¹ 25
	442.9 ✓ 5 ⁴ 25
	443.7 ✓ 5 ¹ 25
	443.9 ✓ 4 ⁴ 25
	448.5 ✓ +0 ² = outside 100 [±] Edge Rd.
	444.6 ✓ 3 ⁷ 25
	444.4 ✓ 3 ⁹ 25

Plotted
6 mi. G.
A-35.

448.29 ✓

L.

£.

R.

120+50

443.8 ✓

4⁵

25

443.9 ✓

4⁴

13

444.1 ✓

4²

444.5 ✓

3⁸

25

T.P.

3.90

444.39 ✓

8.52

452.91 ✓

121+00

444. ✓

8⁷

25

444.3 ✓

8⁶

13

444.3 ✓

8⁶

445.3 ✓

7⁶

27

447. ✓

5⁷

34

outside
Edge Rd.

+50

444.4 ✓

8⁵

25

444.7 ✓

8²

13

445.1 ✓

7²

446.0 ✓

6²

13

446.9 ✓

6²

18

outside
Edge Rd.

447.6 ✓

5²

48

inside
Edge Rd.

122+00

444.8 ✓

8¹

25

445.1 ✓

7⁸

13

445.4 ✓

7⁵

447. ✓

5⁷

5

outside
Edge Rd.

447.7 ✓

5²

33

"

+50

446.7 ✓

6²

25

447.3 ✓

5⁶

13

448.0 ✓

4⁹

448.0 ✓

4⁹

22

inside
Edge Rd.

123+00

446.4 ✓

6⁵

30

447.8 ✓

5¹

13

448.3 ✓

4⁶

448.1 ✓

4⁸

14

449.0 ✓

3²

16

449.3 ✓

13⁶

25

Plotted
G.W.C.
A/6/35

Cont'd. From Page 9.

March-30-1935.

10

	452.91	L.	Φ	R.					
123+50	445.9 [✓] 7 ⁰ 33	446.5 [✓] 6 ⁴ 25	447.8 [✓] 5 ¹ 21	448.0 [✓] 4 ⁹ 13	448.3 [✓] 4 ⁶	448.2 [✓] 4 ⁷ 8	452.1 [✓] 0 ⁸ 16	456.1 [✓] +3 ² 31	
124+00	445.4 [✓] 7 ⁵ 37	445.7 [✓] 7 ² 29	448.1 [✓] 4 ⁸ 24	448.5 [✓] 4 ⁴ 13	448.6 [✓] 4 ³	448.6 [✓] 4 ³ 4	449.7 [✓] 3 ² 5	452.4 [✓] 0 ⁵ 10	457.4 [✓] +4 ⁵ 25
+50	445.3 [✓] 7 ⁶ 40	445.9 [✓] 7 ⁰ 32	448.8 [✓] 4 ¹ 24	449.4 [✓] 3 ⁵ 13	449.3 [✓] 3 ⁶ 3	449.3 [✓] 3 ⁶ 3	452.7 [✓] 0 ² 6	458.7 [✓] +5 ⁸ 29	
125+00	445.3 [✓] 7 ⁶ 40	447.3 [✓] 5 ⁶ 28	450.2 [✓] 2 ⁷ 23	450.5 [✓] 2 ⁴ 13	450.1 [✓] 2 ⁸	450.2 [✓] 2 ⁷ 5	452.5 [✓] 0 ⁴ 7	458.5 [✓] +5 ⁶ 28	
+50	445.3 [✓] 7 ⁶ 35	448.7 [✓] 4 ² 21	451.6 [✓] 1 ³ 16	451.5 [✓] 1 ⁴ 13	451.4 [✓] 1 ⁵	451.1 [✓] 1 ⁸ 9	456.5 [✓] +3 ⁶ 13	459.9 [✓] +7 ⁰ 27	
126+00	445.6 [✓] 7 ³ 25	446.5 [✓] 6 ⁴ 15	451.9 [✓] 1 ⁰ outside 10 Edge Rd.	452.4 [✓] 0 ⁵		452.5 [✓] 0 ⁴ inside 18 Edge Rd.			
T.P.		0.82	452.09 [✓]						
	6.53	458.62 [✓]							

Plotted
G.W.G.
A-6-35

Cont'd. From Page 10

April-2, 1935.
Hill-Simpson
Seper-Remmen.

11.

458.62

	L.	℄	R.
126+50	443.1 ✓ 13 ^E 35	445.4 ✓ 13 ^E 23	447.5 ✓ 11 ^L 13
	448.8 ✓ 9 ^E 7	453.4 ✓ 5 ^L outside Edge Rd.	453.5 ✓ 5 ^L inside Edge Rd. 26
127+00	444.7 ✓ 13 ^E 30	445.8 ✓ 12 ^E 13	449.0 ✓ 9 ^E
	445.0 ✓ 13 ^E 35	445.5 ✓ 13 ^L 13	447.9 ✓ 11 ^E
+50	445.6 ✓ 13 ^E 35	445.7 ✓ 12 ^E 13	445.8 ✓ 12 ^E
128+00	446.3 ✓ 12 ^E 30	446.4 ✓ 12 ^E 13	446.9 ✓ 11 ^L
+50	446.8 ✓ 11 ^E 30	447.4 ✓ 11 ^E 13	448.1 ✓ 10 ^E
129+00	446.5 ✓ 12 ^L 30	447.1 ✓ 11 ^E 13	447.4 ✓ 11 ^E
+50	445.8 ✓ 12 ^E 25	445.9 ✓ 12 ^L 13	447.0 ✓ 11 ^E
130+00	448.9 ✓ 9 ^L 9	455.5 ✓ 3 ^L outside Edge Rd. 21	457.1 ✓ 1 ^E inside Edge Rd. 53
B.M. #27	0.61	458.01 - check on	B.M. #27 - Rec. Elev. = 458.04

Plotted
G.W.G.
4-6-35

	✓ 458.62	✓ 458.8	✓ 449.0	L. ✓ 450.1	£ ✓ 455.4	R. ✓ 455.4		
130+46	12 ⁸ 30	12 ⁸ 22	9 ⁶ 13	8 ⁵ 8	3 ⁴ = out. side Edge Rd.	3 ⁴ = inside Edge Rd.		
131+00	✓ 445.7	✓ 446.3	✓ 455.0	✓ 454.8	✓ 454.2	✓ 453.5	✓ 464.5	✓ 468.5
	12 ⁹ 50	12 ⁸ 36	36. outside Edge Rd. 23	3 ⁸ 13	4 ⁴	5 ¹ = inside Edge Rd. 7	+ 5 ⁹ ± 15	+ 9 ⁹ ± 31

T.F. 3.40 455.22 ✓
3.68 458.90

+ 30	✓ 445.6	✓ 445.7	✓ 455.0	✓ 454.4	✓ 453.4	✓ 463.4	✓ 466.4
	13 ⁸ 50	13 ⁸ 42	3 ⁹ = outside Edge Rd. 29	4 ⁷ 13	5 ⁷ = inside Edge Rd.	+ 4 ⁸ 5	+ 7 ⁸ ± 17

131+50	✓ 445.9	✓ 445.9	✓ 454.6	✓ 453.7	✓ 453.4	✓ 459.1	✓ 465.7
	13 ⁸ 63	13 ⁸ 44	4 ⁸ = outside Edge Rd. 33	5 ⁸ 13	5 ⁸ = inside Edge Rd. 4	+ 0 ⁸	+ 6 ⁸ ± 21

132+00 =	✓ 445.6	✓ 446.4	✓ 454.4	✓ 453.4	✓ 457.8	✓ 462.7	✓ 469.7
132+50 =	13 ⁸ 60	12 ⁷ 45	4 ⁵ = outside Edge Rd. 35	5 ⁷ = outside Edge Rd. 6	1 ² 5	+ 3 ⁸	+ 10 ⁸ ± 23

133+00	✓ 445.0	✓ 446.5	✓ 454.4	✓ 453.7	✓ 453.2	✓ 459.2	✓ 464.6	✓ 469.6
	13 ⁸ 54	12 ⁸ 41	4 ⁷ = outside Edge Rd. 32	5 ⁸ 13	5 ⁷ = outside Edge Rd. 3	+ 0 ⁸	+ 5 ² ± 5	+ 10 ² ± 20

+ 50	✓ 444.8	✓ 445.3	✓ 454.4	✓ 453.9	✓ 453.1	✓ 458.0	✓ 466.1	✓ 471.1
	14 ² 50	13 ⁶ 38	4 ⁷ = outside Edge Rd. 29	5 ⁸ 13	5 ⁸ = outside Edge Rd.	0 ⁹ 1	+ 7 ⁸ ± 9	+ 12 ⁸ ± 26

Equation - Error in chaining. ✓

Plotted
G.W.O.
4-6-35

458.90 ✓

L.

£.

R.

134+00 442.9 ✓ 16° River Channel. 50
 445.6 ✓ 13° 38
 454.1 ✓ 4° Rd. 27
 453.9 ✓ 5° 13
 453.3 ✓ 5° 56

453.0 ✓ 5° Rd. 2
 466.0 ✓ +7.2 ± 8
 470.0 ✓ +11.2 ± 24

+50 443.3 ✓ 15° 50
 443.3 ✓ 15° 41
 453.9 ✓ 5° Rd. 28
 453.8 ✓ 5° 13
 453.2 ✓ 5° Rd. 52

463.2 ✓ +4.2 ± 3
 467.2 ✓ +8.2 ± 19

135+00 443.7 ✓ 15° 43
 453.7 ✓ 5° Rd. 30
 453.4 ✓ 5° 13
 452.6 ✓ 6° Rd. 3
 461.2 ✓ +2.2 ±

462.7 ✓ +3.2 ± 1
 467.7 ✓ +8.2 ± 21

+50 443.6 ✓ 15° 48
 447.0 ✓ 11° 39
 452.3 ✓ 5° 33
 452.6 ✓ 6° 13
 452.3 ✓ 6° Rd. 7
 459.6 ✓ +0.7 4
 460.6 ✓ +1.7

465.6 ✓ +6.7 ± 22

136+00 443.7 ✓ 15° River 42
 453.1 ✓ 5° Rd. 32
 452.1 ✓ 6° 13
 451.8 ✓ 7° Rd. 5
 457.8 ✓ 1°

462.8 ✓ +3.2 ± 20

+50 444.1 ✓ 14° River 37
 452.6 ✓ 6° Rd. 46
 452.2 ✓ 6° 13
 451.4 ✓ 7° 52

456.6 ✓ 2.2 Rd. 4
 460.6 ✓ +1.7 ± 20

T.P. 7.32 451.58 ✓

6.53 458.11 ✓

137+00 444.2 ✓ 13° River 33
 446.4 ✓ 11° 22
 452.5 ✓ 5° Rd. 15
 452.4 ✓ 5° 13
 452.2 ✓ 5° 52

451.7 ✓ 6.4 Rd. 12
 455.5 ✓ 2.6 15
 460.5 ✓ +2.2 ± 28

Cut is Shale Formation. ✓

Plotted
G.W.G.
A-6-35

458.11 ✓

	L.	Φ	R.
137+52	444.5 ✓ 13 ⁶ / ₃₂ River.	447.1 ✓ 11 ⁰ / ₁₃	451.6 ✓ 6 ⁵ / ₂₉ outside Edge Rd.
+62	445.8 ✓ 12 ³ / ₂₇	448.0 ✓ 10 ¹ / ₄	452.9 ✓ 5 ² / ₂₉ inside Edge Rd.
	444.5 ✓ 13 ⁶ / ₃₄ River	448.6 ✓ 9 ² / ₃₄	451.5 ✓ 6 ⁶ / ₃ outside Edge Rd.
138+00	444.5 ✓ 13 ⁶ / ₃₄ River	447.1 ✓ 11 ⁰ / ₁₃	453.4 ✓ 4 ⁷ / ₃₀ inside Edge Rd.
+50	443.8 ✓ 14 ³ / ₃₄ River	448.0 ✓ 10 ¹ / ₁₃	451.6 ✓ 6 ⁵ / ₇ "
	447.5 ✓ 10 ⁶ / ₁₃	449.1 ✓ 9 ⁰ / ₁₃	452.7 ✓ 5 ⁴ / ₁₁ "
139+00	445.0 ✓ 13 ¹ / ₂₆ River	448.5 ✓ 9 ⁶ / ₁₃	454.5 ✓ 3 ⁵ / ₄₀ "
+50	443.8 ✓ 14 ³ / ₃₄ River	449.1 ✓ 9 ⁰ / ₁₃	452.7 ✓ 5 ⁴ / ₁₁ "
	445.0 ✓ 13 ¹ / ₂₆ River	448.5 ✓ 9 ⁶ / ₁₃	454.3 ✓ 3 ⁸ / ₄₁ "
	444.9 ✓ 13 ² / ₃₁ River	449.1 ✓ 10 ⁰ / ₁₃	453.7 ✓ 4 ² / ₈ "
140+00	445.8 ✓ 12 ³ / ₃₇ River	450.0 ✓ 8 ¹ / ₈	453.9 ✓ 4 ² / ₃₆ "
+50	449.7 ✓ 8 ⁹ / ₁₃	451.5 ✓ 6 ⁶ / ₁₃	453.0 ✓ 5 ¹ / ₂ "
	445.8 ✓ 12 ³ / ₃₇ River	450.0 ✓ 8 ¹ / ₈	453.7 ✓ 4 ² / ₃₁ "
	445.8 ✓ 12 ³ / ₃₇ River	450.0 ✓ 8 ¹ / ₈	453.0 ✓ 4 ⁹ / ₂₄ Rd.
	445.4 ✓ 12 ⁷ / ₅₀ River	453.4 ✓ 4 ⁷ / ₁₃ Rd.	453.7 ✓ 4 ² / ₁₅ Rd.
	446.4 ✓ 11 ⁷ / ₂₃	453.5 ✓ 4 ⁶ / ₁₃	456.3 ✓ 1 ⁸ / ₃₀

Plotted
G.W.G.
A-6-35

458.11 ✓

141+00	AA54 ✓ 12 ⁷ River 50	AA6.1 ✓ 12 ² 38	AS4. ✓ 3 ² Rd. 26	AS4.0 ✓ 4 ¹ 13	AS3.6 ✓ 4 ⁵	AS3.4 ✓ 4 ⁷ Rd. 5	AS9.9 ✓ + 1 ² 13	AS3.6 ✓ + 5 ⁵ 23
--------	---------------------------------------	----------------------------------	------------------------------------	---------------------------------	---------------------------	------------------------------------	-----------------------------------	-----------------------------------

+50	AA6.2 ✓ 11 ⁹ River 50	AA6.5 ✓ 11 ⁶ 40	AS5.0 ✓ 3 ¹ Rd. 30	AS4.3 ✓ 3 ⁸ 13	AS3.6 ✓ 4 ⁵ Rd.	AS3.1 ✓ + 5 ⁰ ± 4	AS7.1 ✓ + 9 ⁰ ± 20	
-----	--	----------------------------------	-------------------------------------	---------------------------------	-------------------------------	------------------------------------	-------------------------------------	--

142+00	AA6.5 ✓ 11 ⁶ River 50	AA6.5 ✓ 11 ⁶ 37	AS5.4 ✓ 2 ⁷ Rd. 26	AS4.8 ✓ 3 ³ 13	AS4.1 ✓ 4 ⁰ Rd.	AS6.1 ✓ + 8 ⁰ ± 5	AS7.1 ✓ + 13 ⁰ ± 25	
--------	--	----------------------------------	-------------------------------------	---------------------------------	-------------------------------	------------------------------------	--------------------------------------	--

T.P. 2.64 455.47 ✓

7.09 462.56 ✓

+50	AA6.8 ✓ 15 ⁸ River 50	AA7.1 ✓ 15 ⁵ 34	AS5.8 ✓ 6 ⁸ 23	AS5.5 ✓ 7 ¹ 13	AS4.9 ✓ 7 ²	AS4.7 ✓ 7 ² 3	AS7.7 ✓ + 5 ¹ ± 9	AS2.6 ✓ + 10 ⁰ ± 29
-----	--	----------------------------------	---------------------------------	---------------------------------	---------------------------	--------------------------------	------------------------------------	--------------------------------------

143+00	AA6.9 ✓ 15 ⁷ 50	AA7.2 ✓ 15 ⁴ 33	AS6.1 ✓ 6 ⁵ 21	AS6.0 ✓ 6 ⁶ 13	AS6.0 ✓ 6 ⁶	AS5.8 ✓ 6 ⁸ 4	AS6.8 ✓ + 3 ² ± 8	AS7.8 ✓ + 13 ² ± 28
--------	----------------------------------	----------------------------------	---------------------------------	---------------------------------	---------------------------	--------------------------------	------------------------------------	--------------------------------------

+50	AA7.0 ✓ 15 ⁶ 50	AA7.3 ✓ 15 ³ 32	AS6.3 ✓ 6 ³ 21	AS6.7 ✓ 5 ² 13	AS6.8 ✓ 5 ⁸	AS6.6 ✓ 6 ² 5	AS9.6 ✓ + 6 ⁰ ± 11	AS3.6 ✓ + 11 ⁰ ± 26
-----	----------------------------------	----------------------------------	---------------------------------	---------------------------------	---------------------------	--------------------------------	-------------------------------------	--------------------------------------

Shale Formation

✓

?

Plotted
A-8-35
G.M.G.

462.56 ✓

	L.				℄	R.		
144+00	447.4 ✓ 15 [±] 36	447.0 ✓ 5 [±] 21	457.4 ✓ 5 [±] 13	457.4 ✓ 5 [±]	457.0 ✓ 5 [±] 5	470.0 ✓ +7 [±] 12	478.0 ✓ +15 [±] 32	
+50	447.5 ✓ 15 [±] 38	457.3 ✓ 5 [±] 24	457.7 ✓ 4 [±] 13	457.5 ✓ 5 [±]	457.7 ✓ 4 [±] 9	471.7 ✓ +9 [±] 14	481.7 ✓ +19 [±] 34	
145+00	447.8 ✓ 14 [±] 35	457.8 ✓ 4 [±] 25	457.7 ✓ 4 [±] 13	457.5 ✓ 5 [±]	457.4 ✓ 5 [±] 6	471.4 ✓ +8 [±] 12	476.4 ✓ +13 [±] 27	
+50	448.4 ✓ 14 [±] 26	457.4 ✓ 5 [±] 15	457.5 ✓ 5 [±] 13	457.6 ✓ 5 [±]	457.3 ✓ 5 [±] 9	469.3 ✓ +6 [±] 13	474.3 ✓ +11 [±] 28	
146+00	448.4 ✓ 14 [±] 20	457.7 ✓ 4 [±] 13	458.0 ✓ 4 [±] 10	458.0 ✓ 4 [±]	457.8 ✓ 4 [±] 14	467.8 ✓ +5 [±] 19	472.8 ✓ +10 [±] 34	
+50	448.5 ✓ 14 [±] 30	448.8 ✓ 13 [±] 15	457.7 ✓ 4 [±] 4	457.9 ✓ 4 [±]	458.0 ✓ 4 [±] 24			
147+00	448.8 ✓ 13 [±] 30	448.9 ✓ 13 [±] 16	457.7 ✓ 4 [±] 3	457.8 ✓ 4 [±]	458.1 ✓ 4 [±] 25			
+50	449.1 ✓ 13 [±] 30	449.3 ✓ 13 [±] 17	458.1 ✓ 4 [±] 9	458.1 ✓ 4 [±]	457.9 ✓ 4 [±] 20			

Shale Formation

9.3
-7.7
1/4 8.9
1/4 17.8
1/4 50.

Plotted
G.W.G.
A-8-35

		L.		£.	R.			
148+00	← Level	449.4 ✓ 13 ⁴ 30	449.3 ✓ 13 ³ 20	458.5 ✓ 4 ² 10	458.6 ✓ 4 ⁰	458.1 ✓ 7 ⁵ 15	466.1 ✓ +5 ⁵ ± 20	473.1 ✓ +10 ⁵ ± 35
+50	"		449.6 ✓ 12 ⁰ 28	459.0 ✓ 3 ⁶ 13	459.0 ✓ 3 ⁶	458.7 ✓ 3 ⁷ 14	465.7 ✓ +3 ¹ ± 18	475.7 ✓ +13 ¹ ± 38
T.P.			3.05	459.51 ✓				
		5.84	465.35 ✓					

149+00	← Level	449.6 ✓ 15 ⁷ 29	459.4 ✓ 5 ² 15	459.3 ✓ 6 ⁰ 13	459.8 ✓ 5 ⁵	459.9 ✓ 5 ⁴ 17	467.3 ✓ +2 ⁰ 21	472.3 ✓ +7 ⁰ ± 33
+50	"	449.8 ✓ 15 ⁵ 31	460.6 ✓ 7 ⁷ 17	460.5 ✓ 4 ⁸ 13	460.1 ✓ 4 ⁶	460.5 ✓ 4 ⁸ 15	470.3 ✓ +5 ⁰ 20	472.7 ✓ +7 ⁴ ± 30
150+00	"	450.0 ✓ 15 ³ 35	460.7 ✓ 7 ⁶ 20	460.5 ✓ 7 ⁸ 13	460.5 ✓ 7 ⁸	460.3 ✓ 5 ⁰ 7	473.0 ✓ +7 ² ± 14	478.0 ✓ +12 ⁷ ± 22
+50	"	451.3 ✓ 14 ⁰ 33	460.4 ✓ 7 ⁹ 26	460.4 ✓ 5 ¹ 13	459.7 ✓ 5 ⁶	459.4 ✓ 5 ⁹ 4	472.3 ✓ +7 ⁰ ± 10	474.3 ✓ +9 ⁰ ± 25

Shale Formation

Plotted
G.W.G.
A-8-35

465.35 ✓

		L.		R.
151+00	← Level	450.3 ✓ 15° 38	460.6 ✓ 47 30	460.5 ✓ 48 13
+50	"	450.6 ✓ 147 39	461.0 ✓ 43 28	460.7 ✓ 46 13
152+00	"	450.8 ✓ 145 37	462.9 ✓ 24 21	460.8 ✓ 45 13
+25	"	450.4 ✓ 142 34	463.3 ✓ 20 18	461.9 ✓ 24 13
+50	"		450.9 ✓ 144 25	463.4 ✓ 17 11
+65	← Level		450.0 ✓ 153 20	462.2 ✓ 31

		R.		R.
		459.7 ✓ 56 3	465.7 ✓ 40± 4	475.9 ✓ +106± 12
		460.0 ✓ 53 4	475.3 ✓ +10± 12	480.9 ✓ +156± 25
		459.9 ✓ 54 10	476.9 ✓ +116± 16	481.9 ✓ +166± 31
		460.0 ✓ 53 20	475.0 ✓ +92± 25	
		460.2 ✓ 51 50		
		463.6 ✓ 17 8	461.6 ✓ 32 30	

B.M. #25 - Rec. Elev. = 463.70

B.M. #25 1.69 463.66 = check on
463.70 ✓

1.69 465.39 ✓

T.P. 12.94 452.45 ✓

4.92 457.37 ✓

Plotted
G.W.G.
4-8-35

Cont'd. From Page 18.

April-2-1935.

19

457.37 ✓

	L.		£.
152+75	450.7 ✓ 6 ² 25	450.9 ✓ 6 ⁵ 13	451.1 ✓ 6 ³

153+00	451.1 ✓ 6 ² 25	451.1 ✓ 6 ³ 13.	451.0 ✓ 6 ⁴
--------	---------------------------------	----------------------------------	---------------------------

+50	Level	451.5 ✓ 5 ²
-----	-------	---------------------------

154+00	"	451.6 ✓ 5 ²
--------	---	---------------------------

+50	"	452.1 ✓ 5 ³
-----	---	---------------------------

155+00	"	452.3 ✓ 5 ¹
--------	---	---------------------------

+50	"	452.5 ✓ 4 ²
-----	---	---------------------------

156+00	"	452.6 ✓ 4.8
--------	---	----------------

R.

451.7 ✓ 5 ² 10	464. ✓ +6 ² = outside 20 = Edge Rd.	463.7 ✓ +6 ² 30
---------------------------------	--	----------------------------------

451.1 ✓ 6 ² 25

Level

"

"

"

"

"

Plotted
G.W.C. 5
1-8-35

Cont'd. From Page 19.

457.37 ✓

L.

£.

R.

156+50

Level

452.8 ✓
4[±]

Level

157+00

"

453.0 ✓
4[±]

"

+50

"

453.4 ✓
4[±]

"

158+00

"

453.8 ✓
3[±]

"

T.P.

3.42

453.95 ✓

.6.22

460.17 ✓

454.0 ✓
6[±]

+50

"

"

159+00

"

454.3 ✓
5[±]

"

+50

"

454.4 ✓
5[±]

"

160+00

"

454.8 ✓
5[±]

"

+50

"

455.0 ✓
5[±]

"

161+00

"

455.3 ✓
4[±]

"

+50

"

455.6 ✓
4[±]

"

Plotted
S.W.G.
A-8-35

	460.17 ✓	L.	458.8 ✓ 4 4	R.
162+00		Level	455.7 ✓ 4 5	Level
+50		"	458.8 ✓ 4 4	"
163+00		"	457.6 ✓ 2 6	"
+50		"		"
T.P.		2.93	457.24 ✓	
	6.53	463.77 ✓		
164+00		"	458.4 ✓ 5 4	"
+50		"	457.8 ✓ 6 0	"
165+00		"	457.8 ✓ 6 0	"
+50		"	458.4 ✓ 5 4	"
166+00		"	458.8 ✓ 5 0	"
+50		"	459.2 ✓ 4 6	"
167+00		"	460.3 ✓ 3 5	"
+50		"	460.9 ✓ 2 9	"
168+00		"	461.8 ✓ 2 0	"
+40		"	462.9 ✓ 0 9	"
T.P.		0.61	463.16 ✓	

Plotted
G.M.G.
4-8-35

Cont'd. From Page 21.

April-2-1935.

22.

	L.	£.	R.
T.P.	463.16 ✓		
8.45	471.61 ✓		
168 +50	Level	465.2 ✓ 64	Level
169 +00	"	465.6 ✓ 60	"
+50	"	465.9 ✓ 57	"
170 +00	"	466.1 ✓ 55	"
+50	"	466.4 ✓ 52	"
171 +00	"	466.6 ✓ 50	"
+50	"	466.9 ✓ 47	"
172 +00	"	467.1 ✓ 45	"
+50	"	467.5 ✓ 42	"
173 +00	"	467.8 ✓ 38	"
+50	"	468.4 ✓ 32	"
174 +00	"	469.4 ✓ 22	"
T.P.	1.42 470.19 ✓		
12.00	482.19 ✓		

Plotted
G.W.G.
A-8-35

482.19 ✓ L. E. R.

174+50 469.8 ✓ 470. ✓ 470.5 ✓ 473.5 ✓
 12⁺ 12⁺ 11⁺ 8⁺
 25 13 25

175+00 474.7 ✓ 476.4 ✓ 476.7 ✓ 483.8 ✓
 7⁺ 5⁺ 5⁺ +16
 25 13 25

T.P. 0.98 481.21 ✓

12.51 493.72 ✓

+50 481.8 ✓ 484.4 ✓ 487.3 ✓ 489.0 ✓ 495.8 ✓ 493.9 ✓
 11⁺ 9⁺ 6⁺ 4⁺ +2⁺ outside +0⁺ inside
 25 13 10 23 Edge Rd. 57 Edge Rd.

T.P. 2.38 491.34 ✓

11.82 503.16 ✓

+90 A.88.4 ✓ A91.6 ✓ A91.9 ✓ A97.3 ✓ A95.1 ✓
 14⁺ 11⁺ 11⁺ 5⁺ 8⁺
 30 13 8 5⁺ outside 34 inside
 Edge Rd. Edge Rd.

176+00 489.6 ✓ A92.3 ✓ A97.7 ✓ A97.3 ✓ 495.3 ✓
 13⁺ 10⁺ 5⁺ 5⁺ 7⁺
 30 16 6 outside 29
 Edge Rd.

Plotted
 G.W.G.
 A-8-35

	503.16 ✓	L.	£.	R.			
176+50	499.9 ✓ 3 ³ - outside 35 Edge Rd.	498.3 ✓ 4 ⁹ 13	497.4 ✓ 5 ² inside Edge Rd.	505.6 ✓ +2 ⁴ 3	509.3 ✓ +6 ² 20	512.4 ✓ +9 ² 30	
T.P.		0.35	502.81 ✓				
	12.05	514.86 ✓					
+58	500.0 ✓ 14 ⁹ outside 38 Edge Rd.	498.0 ✓ 16 ⁷ 13	497.1 ✓ 17 ² inside 5 Edge Rd.	506.3 ✓ -8 ⁶	509.4 ✓ 5 ⁵ 15	513.8 ✓ 1 ¹ 30	
177+00	500.4 ✓ 14 ⁵ outside 47 Edge Rd.	498.3 ✓ 16 ⁶ inside 18 Edge Rd.	507.0 ✓ 7 ⁷ 14	510.6 ✓ 4 ³	515.5 ✓ +0 ⁶ 20	518.8 ✓ +3 ⁹ 32	
+50	499.5 ✓ 15 ⁴ 39	498.6 ✓ 16 ³ 13	498.4 ✓ 16 ⁵ " 10	506.7 ✓ 8 ² 7	509.0 ✓ 5 ⁹	518.4 ✓ +3 ⁵ 27	
178+00	499.1 ✓ 15 ² " 33	499.6 ✓ 15 ³ " 13	499.0 ✓ 15 ⁹ " 5	506.3 ✓ 8 ⁶ 2	507.0 ✓ 7 ⁹	513.7 ✓ 1 ² 15	520.0 ✓ +5 ³ 30
T.P.		2.14	512.72 ✓				
	6.60	519.32 ✓					

Plotted
G.W.G.
A-8-35

Cont'd. From Page 24.

April-2-1935.

25.

519.32 ✓

L.

A.

R.

178+50
500.7 ✓
18⁶ outside
33 Edge Rd.
50 0.2 ✓
19¹ 499.7 ✓
13 7 inside
Edge Rd.
507.6 ✓
11⁷ 510.3 ✓
4 9⁰

517.8 ✓
1⁵
15
527.3 ✓
+8⁰
30

179+00
500.7 ✓
18⁶ "
34
500.5 ✓
18⁸ "
13
500.5 ✓
18⁸ "
10
511.2 ✓
8¹
6
514.1 ✓
5²

521.8 ✓
+2⁵
15
529.6 ✓
+10³
30

+50
500.9 ✓
18⁴ "
38
499.9 ✓
19⁴ "
13
510.9 ✓
8⁴
9
514.6 ✓
4⁷

517. ✓
2¹
4
521.4 ✓
+2¹
15
528.6 ✓
+9³
30

180+00
500.6 ✓
18⁷ "
42
498.5 ✓
20⁸ "
14
509.9 ✓
9⁴
8
512.5 ✓
6⁸

517.7 ✓
1⁶
15
522.6 ✓
+3³
30

+15
500.0 ✓
19³ "
38
497.9 ✓
21⁴
13
497.8 ✓
21⁵
10
510.5 ✓
8⁸

512.3 ✓
7⁰
9
518. ✓
1¹
30

T.P.
7.82 511.50 ✓

0.85 512.35 ✓

B.M. #22 9.49 502.86 check on

B.M. #23 Rec. Elev. 502.88

Cont'd. in Book #506-Page 1.

*Entire file plotted
7/22*

*Plotted
G.M.B.
A-8-35*

Profile And Cross-sections of Co. Road Survey
 #606 - From Lakeside to El-Monta Pumping Plant.

April-9-1935.
 Hill-Simpson
 Soper-Remmen

B.M.

400.13 Co. B.M.

#21 City's Elev. - 1931 Pipe Line Survey.

6.41

406.54

L.

R.

R.

-6+67

✓
A01.5
50
21

✓
A02.1
4²

4² Pavement Opposite End
of Existing 36" pipe Line to S.D.

-6+50

✓
A01.6
4²
21

✓
A02.2
4²

4² Pavement

-6+00

✓
A01.7
4²
21

✓
A02.4
4²

-5+50

✓
A02.1
4²
21

✓
A02.6
3²

-5+00

✓
A02.9
3²
21

✓
A03.3
3²

-4+50

✓
A04.1
2²
21

✓
A04.5
2⁰

-4+00

✓
A06.1
0²
21

✓
A06.3
0²

Profile plotted 4/11/35

Plotted
G.W.C.
4-11-35

	406.54	L.	406.47	R.
T.P.		0.07		
	11.16	417.63		
-3+50		✓ A08.3 9 ³ 21	✓ A08.0 9 ⁶ = 4	Pavement
-3+00		✓ A09.6 8 ⁰ 21	✓ A09.6 8 ⁰	"
-2+50		✓ A10.9 6 ⁷ 21	✓ A11.1 6 ⁵	"
-2+00		✓ A12.3 5 ³ 21	✓ A12.5 5 ¹	"
-1+50		✓ A13.6 4 ⁰ 21	✓ A13.9 3 ²	"
-1+00		✓ A14.3 3 ³ 21	✓ A15.1 2 ⁵	"
-0+50		✓ A15.0 2 ⁶ 21	✓ A15.9 1 ⁷	edge of Pavement at Curve

Plotted
G.W.G.
A-10-35

	✓ 417.63	L.	✓ 415.1	✓ 415.1	✓ 415.1	R.	✓ 415.6
0 + 00			2 ⁵ 25	2 ⁵ 21	2 ⁵		2 ⁵ 25
T.P.		2.84	✓ 414.79				
	1.87	✓ 416.66					
+ 50		✓ 414.7	✓ 414.8	✓ 414.6	✓ 415.7		1 ⁵ 25
		2 ⁰ 25	1 ² 21	2 ¹			
1 + 00		✓ 414.4	✓ 414.6	✓ 414.1	✓ 414.7		2 ⁰ 25
		2 ³ 25	2 ¹ 21	2 ⁶			
+ 50		✓ 414.1	✓ 414.7	✓ 413.8	✓ 414.7		2 ⁰ 25
		2 ⁰ 25	2 ⁵ 21	2 ²			
2 + 00		✓ 413.6	✓ 413.6	✓ 413.7	✓ 413.6		3 ¹ 25
		3 ¹ 25	3 ¹ 21	3 ⁵			
+ 50		✓ 411.3	✓ 411.4	✓ 411.9	✓ 411.7		3 ⁰ 25
		5 ⁴ 25	5 ³ 21	4 ⁸			
3 + 00		✓ 408.4	✓ 408.5	✓ 408.3	✓ 409.5		7 ² 25
		8 ³ 25	8 ² 21	7 ²			

Plotted
G.W.G.
A-10-35

Contd. From Page 28

April-9-1935.

29

	416.66	L.	£.	R.
3+50	✓ A05.4 11 ³ 25	✓ A05.6 11 ¹ 21	✓ A05.5 11 ² 5	✓ A06.6 10 ¹ 25
4+00		✓ A0A.6 12 ¹ 25	✓ A0A.7 12 ⁰ 21	✓ A0A.9 11 ² 25
T.P.		11.93	✓ A04.73	
	8.85	✓ 413.58		
+50		✓ A0A.6 9 ⁰ 25	✓ A05.0 8 ⁶ 21	✓ A05.A 8 ² 25
5+00		✓ A08.3 5 ² 25	✓ A08.A 5 ² 21	✓ A08.1 5 ⁵ 25
+40		✓ A09.8 3 ⁸ 25	✓ A09.8 3 ⁸ 21	✓ A10.7 3 ⁶ 25
+75		✓ A09.0 4 ⁶ 25	✓ A09.1 4 ⁵ 21	✓ A09.A 4 ² 25

Plotted
G.W.G.
A-10-35

	413.58	L.	£.	R.
6+00	✓ 406.9 67 25	✓ 406.9 67 21	✓ 406.9 67	✓ 407.8 58 25
T.P.	1.11	✓ 12.84	✓ 400.74	
	✓ 401.85			
+50	✓ 400.9 12 25	✓ 400.8 12 21	✓ 401.2 07	✓ 402.4 +05 25
7+00	✓ 395.8 62 25	✓ 396.2 57 21	✓ 397.1 48	✓ 396.8 52 8
	✓ 398.7 32 18	✓ 398.8 32 25		
+20	✓ 392.4 95 25	✓ 392.9 90 Edge 21 Lake	✓ 394.6 73	✓ 395.7 62 25

7+32

392.9

90 = water surface at West shore of Arm of Lake.

Park Care-taker says water is about 2.5' deep
at crossing of this line.

T.P.

1.11 400.74

1.03 401.77

Plotted
G.W.C.
4-10-35

	401.77	L.	392.8 [✓]	R.	
8+52			9°		Water Surface at East Shore of Lake.
+50		392.8 [✓]	392.9 [✓]	393.9 [✓]	394.4 [✓]
		9° water 4 sur.	8°	7°	7°
				6	25
9+00	393.6 [✓]	393.6 [✓]	394.5 [✓]	396.7 [✓]	
	8°	8°	7°	5°	
	25	21		25	
+50	396.2 [✓]	396.3 [✓]	396.5 [✓]	397.1 [✓]	
	5°	5°	5°	4°	
	25	21		25	
T.P.		1.20	400.57 [✓]		
	9.53	410.10 [✓]			
10+00	401.0 [✓]	401.0 [✓]	401.1 [✓]	401.1 [✓]	
	9°	9°	9°	9°	
	25	21		25	
+50	406.0 [✓]	406.0 [✓]	405.7 [✓]	405.5 [✓]	
	4°	4°	4°	4°	
	25	21		25	
11+00	405.6 [✓]	405.7 [✓]	405.8 [✓]	406.3 [✓]	
	4°	4°	4°	3°	
	25	21		25	

Plotted
6.11.16.
A-10-35

	410.10	L.	£.	R.
11+50	399.7 10 ⁴ 25	400.1 10 ² 21	402.2 7 ⁹	402.8 7 ⁷ 19
12+00	395.4 14 ² 25	395.8 14 ³ 21	398.2 11 ⁹	400.8 9 ³ 25
T.P.	12.73	413.14	9.69 400.41	
+50	399.0 14 ¹ 25	399.5 13 ⁶ 21	400.4 12 ⁷	400.5 12 ⁶ 22
13+00	401.0 9 ¹ 25	403.6 9 ⁵ 21	402.7 10 ⁴ 15	404.2 8 ⁹ 13
+50	408.6 4 ⁵ 25	408.4 4 ⁷ 21	408.2 4 ⁹ 19	410.0 3 ¹ 17
14+00	408.6 4 ⁵ 25	408.4 4 ⁷ 21	408.2 4 ⁹ 19	410.0 3 ¹ 17
				407.8 5 ² 25
				405.3 7 ⁸ 25
				407.9 5 ² 25
				402.1 11 ² 25
				400.5 12 ⁶ 22
				407.8 5 ² 25
				407.9 5 ² 25
				410.9 2 ² 25

Plotted
G.M.G.
4-10-35

	413.14	L,	✓	✓	✓
		103.1	103.8	108.8	
14+50		10 ²	9 ³	4 ³	
		25	21		

T.P.

12.58 400.56

2.36

402.92

15+00

393.6	394.1	397.4
9 ³	8 ³	5 ⁵
25	21	

+30

392.4

10⁵Water Surface at West Shore of Lake
Upper Crossing.

Note: water about 2.5' Deep at this Crossing.

T.P.

2.09 400.83

4.49

405.32

T.P.

3.62 401.70

2.51

404.21

22+75

392.4

11⁸ - water surface at East Shore of Lake.

R,	✓	✓
	409.1	411.1
	4 ⁰	2 ⁰
	23	25

396.4

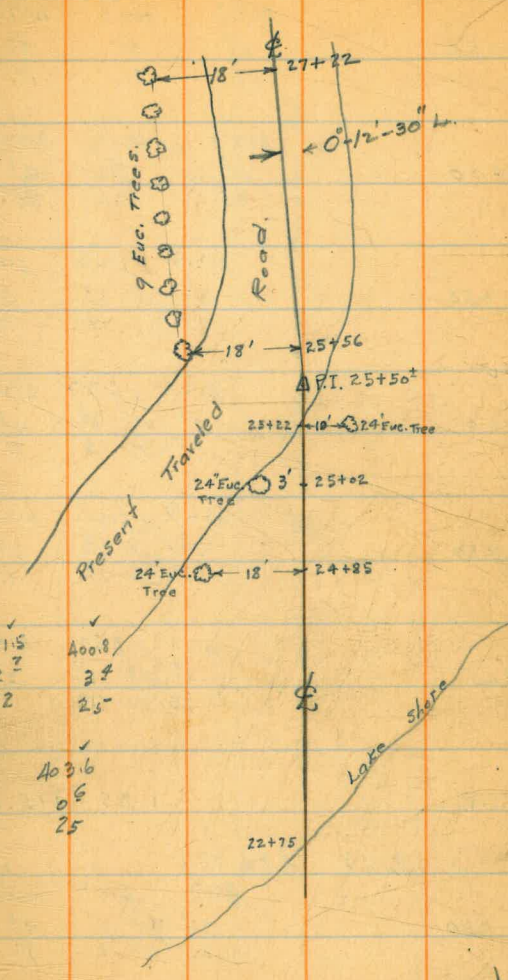
6⁵

25

Plotted
G.M.G.
4-10-35

	A04.21	L.	4.
23+00	393.2	393.2	392.9
	11 ²	11 ²	11 ³
	25	21	
+50	395.0	395.0	394.7
	9 ²	9 ²	9 ⁵
	25	21	
24+00	397.7	397.6	396.5
	6 ⁵	6 ⁶	7 ⁷
	25	21	
+50	399.9	399.7	398.8
	4 ²	4 ⁵	5 ⁴
	25	21	
25+00	401.6	401.7	400.9
	2 ⁶	2 ⁵	3 ²
	25	21	17
+50	402.7	402.7	402.0
	1 ⁵	1 ⁵	2 ² Edge
	25	21	16 Rd.
26+00	405.7	406.1	404.0
	+1 ⁵	+1 ⁹	0 ² Edge
	25	21	11 Rd.
T.P.		0.23	403.98
12.73	416.71		
Set B.M.		6.67	410.04 Spike in

	R.
	392.4
	11 ²
	25
	393.7
	10 ⁵
	25
	395.5
	8 ⁷
	25
	397.4
	6 ⁸
	25
	399.7
	4 ⁵
	25
	402.8
	1 ⁴ Edge
	9 Rd.
	12
	403.6
	0 ⁶
	25
	404.5
	+0 ³ Edge
	13 Rd.



Plotted
G.W.G.
A-10-35

26+50
 416.71 ✓ L ✓
 109.9 ✓ 109.5 ✓ 107.1 ✓
 6⁸ 7² 9⁶
 25 21 10

R,
 107.5 ✓
 9²
 25

27+00
 412.6 ✓ 411.1 ✓ 110.1 ✓
 4² 5⁶ 6⁶
 25 21 10

109.9 ✓ 110.0 ✓ 110.7 ✓
 6⁸ 5² 6⁰
 15 17 25

+50
 413.5 ✓ 412.8 ✓ 111.7 ✓
 3² 3² 5⁰
 25 21 11

111.9 ✓
 4⁸
 25

28+00
 413.8 ✓ 413.7 ✓ 112.7 ✓
 2² 3² 4⁸
 25 21 11

112.8 ✓
 3²
 25

+50
 412.5 ✓ 414.1 ✓ 113.0 ✓
 2² 2⁶ 3²
 25 21 11

113.4 ✓
 3²
 25

29+00
 416.1 ✓ 415.7 ✓ 113.8 ✓
 6² 1⁵ 2²
 25 21 11

114.0 ✓
 2²
 25

T.P. 1.25 415.46 ✓

+50
 8.73 424.19 ✓
 416.7 ✓ 416.1 ✓ 114.8 ✓
 7⁵ 8¹ 9⁴
 25 21 10

115.1 ✓
 9²
 25

30+00
 417.8 ✓ 417.3 ✓ 115.7 ✓
 6⁴ 6⁹ 8⁵
 25 21 10

116.1 ✓
 8²
 25

is about on G. Traveled Rd.

Plotted
 G.W.G.
 1-10-35

	424.19	L.	£	R.
30+50	✓ 19.0 5 ² 25	✓ 18.7 6 ² 12	✓ 16.8 7 ² 10	✓ 17.3 6 ² 25
31+00	✓ 19.3 4 ² 25	✓ 19.2 5 ² 12	✓ 18.0 6 ² 10	✓ 17.4 5 ² 25
+50	✓ 20.5 3 ² 25	✓ 20.0 4 ² 12	✓ 18.7 5 ² 10	✓ 18.9 5 ² 25
32+00	✓ 20.2 4 ² 25	✓ 19.6 4 ² 12	✓ 18.8 5 ² 10	✓ 19.1 5 ² 25
+50	✓ 20.3 3 ² 25	✓ 19.8 4 ² 12	✓ 18.9 5 ² 10	✓ 19.3 4 ² 25
33+00	✓ 20.9 3 ² 25	✓ 20.1 4 ² 12	✓ 19.1 5 ² 11	✓ 19.6 4 ² 25
+50	✓ 21.4 2 ² 25	✓ 20.9 3 ² 12	✓ 19.1 4 ² 10	✓ 20.2 4 ² 25
34+00	✓ 22.9 1 ² 25	✓ 22.1 2 ² 13	✓ 20.2 4 ² 11	✓ 20.7 3 ² 25

Plotted
G.W.G.
A-11-35

424.19 L. E. R.

34+50	✓ 422.3 19 25	✓ 421.7 25 12	✓ 419.8 44 11	✓ 420.7 35	✓ 420.7 35 25	
35+00	✓ 422.3 19 25	✓ 421.6 26 13	✓ 419.9 43 12	✓ 420.5 37	✓ 420.4 38 25	
+50		✓ 419.6 46 25	✓ 419.6 46 12	✓ 420.3 39	✓ 420.4 38 16	✓ 418.7 55 25
36+00	✓ 420.1 41 25	✓ 420.1 41 12	✓ 420.7 35	✓ 420.3 39 25		
+50	✓ 422.0 22 25	✓ 421.1 34 13	✓ 421.5 27	✓ 421.2 32 21	✓ 422.2 22 25	

T.P.

2.35 421.84

11.56 433.40

37+00	✓ 423.3 10 25	✓ 423.2 10 14	✓ 422.2 11 13	✓ 422.7 10 7	✓ 423.3 11 20	✓ 423.7 9 22	✓ 424.1 9 25
+50	✓ 424.8 8 25	✓ 424.4 9 14	✓ 423.2 10 13	✓ 423.9 9	✓ 423.3 10 20	✓ 424.8 8 22	✓ 425.1 8 25

Plotted
G.W.G.
A-11-35

433.40

L.

£.

R.

38+00

✓ 426.0	✓ 425.8	✓ 424.8	✓ 425.2
7 ⁸	7 ⁶	8 ⁶	8 ²
25	14	13	

✓ 424.6	✓ 425.2	✓ 425.9
8 ⁸	8 ²	7 ⁵
20	22	25

+50

✓ 426.6	✓ 427.3	✓ 425.9	✓ 426.5
6 ⁸	6 ¹	7 ⁵	6 ²
25	14	12	

✓ 425.7	✓ 426.9	✓ 426.7
7 ⁷	6 ⁵	6 ⁷
20	22	25

39+00

✓ 428.0	✓ 427.3	✓ 427.8
5 ⁴	6 ¹	5 ⁶
25	13	

✓ 426.9	✓ 428.3	✓ 428.1
6 ⁵	5 ¹	5 ²
20	21	25

+50

✓ 428.4	✓ 428.7	✓ 429.1
5 ⁰	4 ²	4 ²
25	18	

✓ 427.8	✓ 428.5	✓ 428.6
5 ⁶	4 ²	4 ⁸
20	21	25

40+00

✓ 429.2	✓ 429.0	✓ 429.9
4 ²	4 ⁷	3 ⁵
25	20	

✓ 428.9	✓ 429.9	✓ 430.1
4 ⁵	3 ⁵	3 ³
20	22	25

+50

✓ 430.2	✓ 430.8
3 ²	2 ⁶
25	

✓ 430.5
2 ²
25

41+00

✓ 431.4	✓ 431.5
2 ⁰	1 ²
25	

✓ 430.3
3 ¹
25

+50

✓ 431.9	✓ 432.3
1 ⁵	1 ¹
25	

✓ 430.9
2 ⁵
25

Plotted
S.W.C.
4-11-35

433.40

L.

S.

R.

42+00

432.4

10

25

432.5

0.5

25

431.7

12

25

T.P.

1.51

431.89

2.78

434.67

+50

432.6

2

25

432.7

1

25

433.5

12

25

432.6

2

25

43+00

432.0

07

26

432.4

23

23

432.5

10

25

433.7

10

25

432.8

19

25

+50

Top of 3' Bank

432.7

20

24

432.9

07

25

432.0

07

25

433.0

17

25

44+00

433.3

14

22

433.3

05

25

432.4

05

25

433.3

14

25

+50

432.5

22

21

433.8

09

25

432.6

21

25

45+00

430.8

39

20

432.4

23

25

431.4

33

25

Plotted
G.M.G.
4-11-35

	434.67	L.	℄.	R.
45+50	✓ 128.6 6 ¹ 25	✓ 429.0 21	✓ 430.9 3 ⁸	✓ 430.1 4 ⁶ 25
46+00	✓ 128.9 5 ⁸ 25	✓ 429.0 21	✓ 429.8 4 ⁷	✓ 429.3 5 ²
+50	✓ 128.4 6 ³ 25	✓ 428.6 21	✓ 429.7 5 ⁰	✓ 428.8 5 ⁷ 25
47+00	✓ 125.5 Bottom of 9 ² Quail Creek 29	✓ 128.7 6 ⁰ 25	✓ 430.3 4 ⁴	✓ 429.5 5 ² 25
+50	✓ 430.9 3 ⁸ 25	✓ 431.0 24	✓ 431.3 3 ⁴	✓ 430.4 4 ³ 25
48+00	✓ 128.0 6 ⁷ 26	✓ 431.6 3 ¹ 24	✓ 432.3 2 ⁴	✓ 431.3 3 ⁴ 23
+50	✓ 430.4 4 ³ 25	✓ 433.5 1 ² 24	✓ 433.4 1 ³	✓ 432.9 1 ⁸ 25
B.M.	2.58	432.09	Spike in	Power Pole # 78762 24' Lf. of sta. 47+85

Plotted
G.W.G.
4-11-35

B.M.

432.09 ✓

12.39 444.48 ✓

L.

£.

R.

49+00

431.2 ✓
13³/₄ Bottom
26 Quail Creek.

434.0 ✓
10⁵/₂₂ ~~434.0~~
22

434.8 ✓
9⁷

434.0 ✓
10⁵/₂₅

+50

435.8 ✓
8⁷/₂₅ ~~436.0~~
25

437.0 ✓
7⁵

436.1 ✓
8⁹/₁₈

436.7 ✓
7⁸/₂₂

50+00

438.5 ✓
6⁹/₂₅ ~~438.9~~
25

439.4 ✓
5¹

440.1 ✓
4⁹/₂₅

+50

434.4 ✓
10¹/₅₂ Bottom
Quail Creek.

437.4 ✓
7¹/₄₂ ~~440.1~~
19

440.4 ✓
4¹

440.6 ✓
3⁹/₂₅

+90

435.5 ✓
9° - Flow Line of Quail
Creek at Bridge

441.1 ✓
3⁹

= Floor of Wooden Bridge
over Quail Creek

51+00

436.3 ✓
8²/₂₅

439.8 ✓
4⁷/₂₂ ~~439.9~~
22

441.1 ✓
3⁹

440.9 ✓
3⁵/₁₀

437.4 ✓
7¹/₂₅

+50

438.0 ✓
6⁵/₂₅

440.1 ✓
4⁴/₂₂ ~~440.1~~
22

441.1 ✓
3⁹

441.0 ✓
3⁵/₁₀

439.6 ✓
4⁹/₂₅

Plotted
G.W.G.
4-13-35

444.48 ✓ L. £. R.

52+00

439.9 ✓
 $\frac{440.6}{21}$
 25
 26
 14
 441.9 ✓
 26
 14
 441.8 ✓
 27

441.8 ✓
 27
 10
 440.8 ✓
 27
 25

+50

440.7 ✓
 $\frac{441.2}{21}$
 38
 24
 442.4 ✓
 21
 14
 442.5 ✓
 20

442.5 ✓
 20
 11
 441.3 ✓
 30
 25

T.P.

1.81 442.67 ✓

8.86 451.53 ✓

53+00

441.5 ✓
 $\frac{442.0}{21}$
 10
 25
 443.0 ✓
 85
 14
 443.2 ✓
 80

443.3 ✓
 80
 11
 441.6 ✓
 99
 24

+50

442.1 ✓
 $\frac{442.4}{21}$
 9
 23
 443.5 ✓
 80
 14
 443.9 ✓
 75

444.0 ✓
 75
 11
 442.4 ✓
 91
 24

54+00

444.2 ✓
 70
 25
 444.2 ✓
 70
 23
 442.7 ✓
 80
 21
 444.1 ✓
 70
 14
 444.6 ✓
 60

444.8 ✓
 60
 11
 443.0 ✓
 85
 24

+50

444.3 ✓
 70
 25
 444.5 ✓
 70
 23
 442.5 ✓
 $\frac{443.0}{21}$
 80
 22
 444.8 ✓
 60
 15
 445.2 ✓
 60

445.4 ✓
 60
 11
 443.1 ✓
 70
 24

Plotted
 G.M.C.
 4-13-35

Cont'd. From Page 42.

April-12-1935

43

	451.53 ✓	L.	4.	
55+00	445.7 ✓ 5 ⁸ 25	445.6 ✓ 5 ⁹ 23	444.3 ✓ 7 ² 22	445.3 ✓ 6 ² 15
+50	446.2 ✓ 5 ³ 25	446.2 ✓ 5 ³ 22	445.1 ✓ 6 ² 21	446.0 ✓ 5 ⁵ 15
56+00		446.4 ✓ 5 ¹ 25	446.0 ✓ 5 ⁵ 21	446.9 ✓ 4 ⁶ 15
+50			447.1 ✓ 4 ⁴ 25	448.2 ✓ 3 ³
57+00			448.5 ✓ 3 ⁰ 25	449.3 ✓ 2 ²
+50			449.7 ✓ 1 ⁸ 25	450.8 ✓ 0 ⁷
T.P.		0.83	450.70 ✓	
	12.43	463.13		
58+00	451.9 ✓ 11 ² 25	452.1 ✓ 11 ⁰ 22	451.1 ✓ 12 ⁰ 21	452.0 ✓ 11 ¹ 16

	R.
446.0 ✓	444.5 ✓
5 ⁵	7 ⁰
11	24
446.7 ✓	445.4 ✓
4 ⁸	6 ¹
11	25
447.5 ✓	446.7 ✓
4 ⁰	5 ³
11	25
448.4 ✓	447.3 ✓
3 ¹	4 ²
11	25
449.6 ✓	448.4 ✓
1 ⁹	3 ¹
11	25
451.2 ✓	449.9 ✓
0 ³	1 ⁶
11	25

Plotted
6 m. 6
4-13-35

Cont'd. From Page 43

April-12-1935.

44.

463.13

L.

L.

R.

58+50 454.9 454.8 453.2 454.2 454.9
 8² 8³ 9² 8² 8²
 25 22 21 16

454.9 453.2
 8² 9²
 11 24

59+00 457.5 457.2 455.9 457.0
 5² 5² 7² 6¹
 25 23 22

457.0 455.0
 6¹ 8¹
 11 24

+50 459.8 459.5 457.8 458.7 459.2
 3² 3² 5² 4² 3²
 25 23 22 15

459.1 457.3
 4² 5²
 11 25

60+00 460.0 461.8 460.2 461.0 461.3
 1¹ 1³ 2² 2¹ 1²
 25 22 21 16

461.0 459.1
 2¹ 4²
 11 25

T.P.

0.21 462.92

13.01 475.93

+50 465.5 465.1 462.0 463.3 463.7
 10² 10² 13² 12² 12²
 25 20 19 13

463.4 461.2
 12² 14²
 13 25

61+00 467.6 467.6 464.0 465.7 465.8
 8³ 8³ 11² 10² Edge 10²
 25 16 14 8 Rd.

465.7 464.4
 10² Edge 11²
 19 Rd. 25

on Traveled Rd. to Here

Plotted
 G.M.G.
 A-13-35

475.93 L. 4.

61+50 469.8 ✓ 469.5 ✓ 468.9 ✓ 467.2 ✓
 6² 6⁴ 10⁰ 8² = N. Edge
 25 9 8 1 Rd.

+87 471.5 ✓ 470.2 ✓ 467.1 ✓
 4⁴ 5² 8⁸
 25 2 Rd.

62+00 472.2 ✓ 471.7 ✓ 470.5 ✓
 3² 4² 5⁴
 25 10 Rd.

+50 473.9 ✓ 472.3 ✓
 2⁰ 4² 3⁶
 25 21 Rd.

63+00 475.4 ✓ 473.1 ✓
 0⁵ 4² 2⁸
 25 21 Rd.

+50 476.7 ✓ 474.5 ✓
 1⁰ 1⁴
 25 21 Rd.

T.P. 1.61 474.32 ✓

64+00 477.4 ✓ 474.3 ✓
 3⁴ 4² 6⁵
 25 21 Rd.

R.

467.7 ✓ 8² = S. Edge
 27 Rd.

468.1 ✓ 468.5 ✓
 7⁸ = N. Edge 7⁴ = S. Edge
 6 Rd. 37 Rd.

470.5 ✓ 467.5 ✓ 468.4 ✓ 468.6 ✓
 5⁴ 8⁴ 7⁵ = N. Edge 7³ = S. Edge
 1 2 9 Rd. 40 Rd.

470.9 ✓ 467.9 ✓ 468.8 ✓ 468.7 ✓
 5⁰ 8⁰ 7¹ = N. Edge 7² = S. Edge
 14 15 22 Rd. 51 Rd.

471.1 ✓ 4⁸
 25

471.9 ✓ 4⁰
 25

472.4 ✓ 8⁴
 25

Plotted
 G.M.G.
 4-13-35

480.80 ✓

L.

£.

R.

64+50

✓
A77.2
3³
25

✓
A76.8
21

✓
A76.5
6³

65+00

✓
A76.6
4²
25

✓
A76.2
21

✓
A76.4
6²

+50

✓
A76.0
4⁸
25

✓
A75.6
21

✓
A75.5
7³

66+00

✓
A75.3
5⁵
25

✓
A74.6
21

✓
A74.0
7⁸

+50

✓
A74.3
6⁵
25

✓
A74.1
21

✓
A73.4
7⁶

67+00

✓
A74.2
6⁶
25

✓
A74.1
21

✓
A73.4
7⁷

+50

✓
A75.6
5²
25

✓
A75.5
21

✓
A75.1
5²

68+00

✓
A77.5
3³
25

✓
A77.3
21

✓
A76.4
4⁴
5

✓
A75.6
5²
4

✓
N. Edge Rd.

✓
A75.8
5²

✓
A72.0
8⁸
25

✓
A64.3
16⁵
107

= N. Edge At Junction of 2 Rds.
Rd.

✓
A71.5
9³
25

✓
A70.7
10²
25

✓
A70.8
10²
25

✓
A67.8
13²
47

= N. Edge Rd.

✓
A71.0
9⁸
27

✓
A69.4
11⁴
28

✓
A69.6
11²
33

= N. Edge Rd.

✓
A73.1
7⁷
14

✓
A71.7
9²
15

= N. edge Rd.

✓
A74.0
8⁸
25

✓
A74.4
5²
4

✓
A73.6
7²
5

✓
A73.5
7³
40

= S. Edge Rd.

✓
A75.5
5²
31

= S. Edge Rd.

Plotted
G.M.G.
A-13-35

Cont'd. From Page 46.

April-12-1935.

47.

	480.80	L.	£.	R.
Set B.M.		4.57	476.23	Spike in Power Pole #78772 33' Rt. of sta. 68+00
	7.72	483.75		
68+50	180.7 3 ³ 25	480.1 5.5 11	177.4 6 ⁶ 10	177.8 6 ⁷ 30
			N. edge Rd.	S. Edge Rd.
69+00	183.0 1 ⁰ 25	181.1 2 ⁹ 13	178.6 5 ⁸ 12	179.0 5 ⁰ 25
+50	181.4 +0 ⁴ 25	182.6 1 ⁴ 14	179.0 5 ⁰ 11	179.7 4 ⁸ 25
70+00	184.7 +0 ⁷ 25	183.3 0 ⁷ 15	178.7 5 ⁸ 12	178.9 5 ¹ 25
+50	182.7 +0 ² 25	182.8 1 ² 15	176.4 7 ⁴ 12	177.1 6 ⁹ 25
71+00	182.1 1 ⁹ 25	180.7 3 ³ 16	174.1 9 ⁹ 13	174.7 9 ³ 25
+50	180.0 4 ⁰ 25	178.5 5 ⁵ 17	171.8 12 ² 14	172.4 11 ⁶ 24

Plotted
G.W.C.
A-15-35

483.95

L.

£

R.

72+00	477.2 68 25	✓ 475.8 8 19	469.3 14 15	✓ 470.0 14 25		
-------	-------------------	-----------------------	-------------------	------------------------	--	--

(476.3)
21

= N. Edge Rd.

T.P.

12.73 471.22

0.76 471.98

+50	475.7 +3 25	✓ 474.4 +2 20	467.2 4 17	467.9 4 25	467.3 4 25	
		(474.3) 21	Toe Bank			
73+00	472.7 +0 25	471.6 0 21	465.3 6 17	465.9 6 25	465.1 6 25	
+50	470.3 1 25	469.4 2 21	467.9 9 17	463.5 8 16	462.7 9 16	463.5 8 25
74+00	469.2 2 30	466.7 5 23	460.6 11 19	461.2 10 25	460.7 11 15	461.3 10 22
		(463.7) 21			S. Edge Rd.	
+50	465.9 6 30	463.9 8 23	459.6 12 20	459.3 12 25	458.8 13 25	459.4 12 25
		(461.0) 21				

T.P.

12.82 459.16

Plotted
G.W.G.
4-15-35

T.P. 459.16

0.05 ✓ 459.21 ✓
 466.8 ✓ 462.6 ✓
 75+00 +75± +5±
 35 25
 465.6 ✓ 458.9 ✓
 +50 +6± +3±
 35 26
 457.8 ✓ 451.7 ✓
 76+00 1± 8°
 27 24
 454.8 ✓ 448.7 ✓ 449.4 ✓ 449.1 ✓
 +50 4.8 10.5 9.8 10.1
 28 26
 446.3 ✓ 447.3 ✓ 446.7 ✓
 77+00 12.9 11.9 12.5
 29 22

456.8
2±. Top
22 Bank.
AS6.8
AS6.8
21

453.9
5.3
22
AS3.9
AS3.9
21

451.7
8°
24
AS1.7
AS1.7
21

448.9
10.5
26
AS8.9
AS8.9
21

447.3
11.9
22
AS7.3
AS7.3
21

R. 456.6 ✓ 456.6 ✓
 26 - S. Edge 26
 13 Rd. 25
 454.7 ✓ 455.2 ✓
 5° " 4°
 11 25
 451.4 ✓ 452.8 ✓
 7.8 " 6.4
 10 25
 448.9 ✓ 450.8 ✓ 450.9 ✓
 10.3 " 8.4 8.3
 8 10 25
 446.5 ✓ 448.6 ✓ 449.4 ✓
 12.7 " 10.6 9.8
 7 10 25

T.P. 12.69 446.52

1.01 447.53

+50 445.0 ✓ 445.5 ✓ 445.1 ✓
 2±. Edge 2° 2±
 31 Rd. 20

444.7 ✓ 446.7 ✓ 448.7 ✓
 2.8 - Edge 0.8 +1±
 6 Rd. 7 25

Plotted
 G.M.W.G.
 A-15-35

	447.53	L.	£.	R.			
78+00		443.4 3 ¹ Edge - 28 Rd.	443.5 4 ⁰	443.7 4 ² Edge 6 Rd.	444.9 2 ⁶ 7	445.7 1 ⁸ 21	446.9 0 ⁶ 25
+50		443.4 4 ¹ " 32	442.7 4 ⁸ Edge Rd.	443.0 4 ⁵ 6	443.9 3 ⁶ 15	446.6 0 ³ 25	
79+00		442.4 5 ¹ " 30	442.7 5 ³ Edge Rd.	442.7 4 ⁸ 10	446.1 1 ⁴ 25		
+50		441.4 6 ¹ " 35	441.4 6 ¹ "	443.5 5 ⁰ 10	444.9 2 ⁶ 25		
80+00		441.3 6 ² 30	441.9 5 ⁶ 20	441.3 6 ² "	442.5 5 ⁰ 3	442.8 4 ⁷ 10	445.2 2 ³ 25
+50		442.7 5 ³ " 27	441.7 5 ⁸	441.5 6 ⁰ Edge 6 Rd.	443.3 4 ² 7	445.8 1 ⁷ 25	
81+00		442.7 5 ³ " 25	442.1 5 ⁴	441.9 5 ⁶ " 10	444.7 2 ⁸ 11	447.1 0 ⁴ 25	
+50		441.6 5 ² 30	442.1 5 ⁴	442.0 5 ⁵ " 12	444.3 3 ² 13	445.6 1 ⁹ 25	

Plotted
G.W.G.
4-15-35

Cont'd. From Page 50.

April-12-1935.

51

	447.53	L.	£.	R.
82+00	✓ 110.2 7 ³ 25	✓ 440.4 41	✓ 441.3 6 ²	✓ 441.8 5 ⁷ 13
				✓ 443.1 4 ¹ 25
Set B.M.	2.20	443.20	6.53	441.00
			Spike in	Tel. Pole 29' W. of Sta. 82+04. # D282547.
+ 50	✓ 139.1 4 ¹ 25	✓ 439.2 41	✓ 439.8 3 ⁴	✓ 440.1 3 ¹ 20
83+00	✓ 437.7 5 ⁵ 25	✓ 438.7 4 ⁵ 20	✓ 439.3 3 ⁹	✓ 440.9 2 ³ 28
+ 50	✓ 436.5 6 ⁷ 25	✓ 438.5 4 ² 21	✓ 439.1 4 ¹	✓ 440.1 3 ¹ 27
84+00	✓ 436.9 6 ³ 25	✓ 438.2 5 ⁰ 21	✓ 439.0 4 ²	✓ 439.7 3 ⁵ 25
+ 50	✓ 437.1 6 ¹ 25	✓ 438.3 4 ⁹ 21	✓ 438.8 4 ⁴	✓ 438.7 4 ⁵ 20
				✓ 440.5 2 ⁷ 25

£ is about on & Traveled Rd.

Plotted
G.W.G.
4-15-35

	443.20	L.	€	R.
85+00		136.1 7 ¹ 25	137.4 5 ² 20	138.0 5 ²
+50		135.4 7 ⁸ 25	136.7 7 ⁰ 20	136.7 6 ⁵
86+00		135.2 8 ⁰ 25	135.0 8 ² 22	136.0 7 ²
+50		135.1 8 ¹ 25	135.0 8 ² 22	135.7 7 ⁵
87+00			134.8 8 ⁴ 25	135.5 7 ⁷
+50			134.5 8 ⁷ 25	135.5 7 ⁷
T.P.		8.17	435.03	
	5.70	440.73		

Plotted
G.W.G.
A-15-35

Cont'd. From Page 52.

April-12-1935

53

440.73

L.

R.

R.

88+00

✓
434.9
5⁸
25

✓
435.0
21

✓
435.4
5²

✓
435.7
5⁰
25

+50

✓
435.1
5⁶
25

✓
435.2
21

✓
435.5
5²

✓
435.7
5⁵
25

89+00

✓
435.1
5⁶
25

✓
435.2
21

✓
435.5
5²

✓
435.1
5⁶
25

+50

✓
434.9
5⁸
25

✓
435.0
21

✓
435.4
5³

✓
435.3
5⁴
25

90+00

✓
435.1
5⁶
25

✓
435.2
21

✓
435.5
5²

✓
435.6
5¹
25

+50

✓
435.4
5³
25

✓
435.4
21

✓
435.7
5⁰

✓
435.3
5⁴
25

91+00

✓
435.4
5³
25

✓
435.5
21

✓
435.9
4⁸

✓
435.6
5¹
25

+50

✓
435.3
5⁴
25

✓
435.4
21

✓
435.9
4⁸

✓
435.7
5⁰
25

Plotted
G.W.G.
4-15-35

440.73

L.

L.

R.

92+00

435.6
5'
25

435.7
21

436.2
4'

436.2
4'
25

+50

435.5
5'
25

435.6
21

436.2
4'

436.6
4'
25

93+00

435.6
5'
25

435.7
21

436.1
4'

436.6
4'
25

+50

435.6
5'
25

435.8
21

436.6
4'

436.6
4'
25

T.P.

4.62 436.11

6.07 442.18

94+00

436.1
6'
25

436.2
21

436.8
5'

436.6
5'
25

+50

436.3
5'
25

436.4
21

437.0
5'

437.0
5'
25

Plotted
G.W.G.
4-15-35

442.18 ✓

L.

±

R.

95+00

436.6 ✓
56
25

436.7
21

437.7 ✓
50

437.1 ✓
51
25

+50

436.7 ✓
55
25

436.8
21

437.4 ✓
48

436.9 ✓
53
25

96+00

436.9 ✓
53
25

437.0
21

437.5 ✓
47

437.7 ✓
45
25

+50

437.1 ✓
51
25

437.2
21

437.8 ✓
49

437.5 ✓
47
25

B.M.

3.32 438.86 ✓ = check on

U. S. G. S. Gauging sta. #1 El-Mente Pumping Plant.
Rec. Elev. 438.93.

Profile plotted of m
Computed and checked
G.M.G. 4-13-35
Plotted
G.M.G. 4-15-35

Contd. on Page 2 of this Book.

Profile And XSections of Alternate Lines For Road
Location From El Monte Pumping Plant
East.

B.M.

438.93 = U.S.G.S.

6.17 445.10

E.

Start of Alternate Line #2.

99+45.7 B.C.

436.7	439.3	439.2	439.0
8 ²	5 ⁸ Edge	5 ²	6 ¹
22	16	13	

100+00

434.4	439.8	440.0	439.5
10 ⁷	5 ³ "	5 ¹	5 ⁵
26	15	13	

+50

434.3	434.3	440.2	440.2	439.3
10 ⁸	10 ⁸	4 ¹ "	4 ⁹	5 ⁸
40	28	19	13	

101+00

434.5	434.9	440.2	440.1	439.4
10 ⁶	10 ²	4 ⁹ "	5 ⁰	5 ⁷
40	28	20	13	

+50

434.5	434.8	439.8	439.6	439.2
10 ⁶	10 ³	5 ³ "	5 ⁵	5 ⁹
40	30	20	13	

102+00

434.6	435.7	440.0	439.4	439.0
10 ⁵	9 ⁴	5 ¹ "	5 ⁷	6 ¹
40	27	20	13	

+50

436.0	439.7	439.2	438.7
9 ¹	5 ⁴	5 ⁹	6 ⁴
30	25	13	

May-8-1935
Hill - Simpson
Soper - Remmen

56

Gauging Sta. At El Monte Pumping Plant.

438.3	440.1
6 ³ Edge	5 ⁰
14 Rd.	25

438.4	443.5	446.9
6 ⁷ "	1 ⁶	+1 ⁸
12	15	23

438.6	447.8	452.8
6 ⁵ "	+2 ⁷	+7 ² ±
8	13	25

438.7	451.4	456.4
6 ⁴ "	+6 ³	+11 ³
8	13	23

438.8	445.1	455.3	460.3
6 ³ "	0 ⁰	+10 ²	+15 ² ±
10	11	21	30

438.5	445.4	455.6	460.6
6 ⁶ "	+0 ²	+10 ⁵	+15 ⁵ ±
8	11	24	34

438.6	448.5	455.0	465.0
6 ⁵ "	+3 ⁴	+9 ²	+19 ² ±
1	5	15	30

Computed + checked
5/12/35
G.W.G.
Plotted 5/15/35

	445.10				¢
T.P.		5.15	439.75		
	6.04	445.99			
103+00	✓ 435.4 10 ⁶ 31	✓ 439.4 6 ⁶ Edge 26 Ed.	✓ 439.0 7 ⁹ 13	✓ 438.4 7 ⁶	
+50	✓ 436.1 9 ² 29	✓ 439.1 6 ⁹ " 24	✓ 439.0 7 ⁹ 13	✓ 438.7 7 ³	
104+00	✓ 435.9 10 ¹ 30	✓ 439.3 6 ⁷ " 20	✓ 439.7 6 ⁸ 13	✓ 439.3 6 ⁷	
+50	✓ 436.6 9 ⁹ 30	✓ 437.3 8 ⁷ 20	✓ 439.3 6 ⁷ " 16	✓ 439.5 6 ⁵ 13	✓ 439.9 6 ¹
105+00	✓ 437.4 8 ⁶ 25	✓ 438.1 7 ⁹ 15	✓ 439.5 6 ⁵ 13	✓ 440.1 5 ⁹	
+50	✓ 437.4 8 ⁶ 25	✓ 438.3 7 ⁷ 13	✓ 440.3 5 ² 9	✓ 440.6 5 [±]	
106+00	✓ 437.9 8 ¹ 25	✓ 438.1 7 ⁹ 13	✓ 441.3 4 ⁷ 7	✓ 441.2 4 [±]	

✓ 438.5 7 ⁵ - Top Bank 1 at edge Rd.	✓ 445.6 0 [±] 4	✓ 451.1 +5 [±] 8	✓ 456.1 +10 [±] 19	✓ 462.1 +16 [±] 30
✓ 438.3 7 ⁷ 4	✓ 447.9 3 ¹ 7	✓ 450.7 +4 ⁷ 22		
✓ 439.0 7 ⁹ 9	✓ 441.9 4 ¹ 11	✓ 444.4 1 ⁶ 25		
✓ 439.7 6 ³ 15	✓ 443.1 2 ⁹ 29			
✓ 440.4 5 ⁶ 22	✓ 440.3 5 ⁷ 30			
✓ 441.3 4 ⁷ 22	✓ 441.1 4 ⁹ 30			
✓ 442.0 4 ⁹ 25				

Computed & checked
5/14-35.
G.W.G.
Plotted
5/15/35

Cont'd. From Page 57.

May-8-1935

58.

445.99

106+50
 438.0 8⁰ 25
 439.1 6² 13
 440.8 5² Edge 9 Rd.
 441.1 4⁹

107+00
 438.6 7⁴ 25
 440.7 5⁸ 13
 441.3 4⁷ 12
 441.6 4⁴

+50
 438.9 7¹ 25
 439.5 6⁵ 19
 442.1 3¹ Edge 15 Rd.
 442.1 3⁹ 13
 442.1 3⁹

108+00
 439.8 6² 25
 442.7 3⁸ 20
 442.3 3⁷ 13
 442.7 3⁸

+50
 440.1 5⁹ 27
 442.5 3⁵ 23
 442.7 3³ 13
 442.7 3⁸

109+00
 442.7 3³ 25
 442.7 3³ 13
 442.7 3⁸

T.P.

5.48

448.05

3.42 442.57

441.5 7⁵ 25

441.5 4⁵ 20
 444.4 1⁶ 22
 450.4 +4⁴ 32

441.9 4¹ Toe Bank 14 And Edge Rd.
 448.4 +2⁴ 18
 451.4 +8⁴ 28

441.8 4² 7
 445.2 0⁵ 10
 460.7 +14⁷ 31

442.0 4⁰ 4
 446.5 +0⁵ 6
 460.7 +14⁷ 29

442.1 3⁹ 2
 448.7 +2² 5
 461.7 +15² 25
 466.7 +20² 35

Computed and checked.
 5/14/35.
 G.M.G.
 Plotted
 5/15/35

448.05

109+50

✓	✓	✓	✓
447.7	447.9	441.9	
5 ³	5 ¹	6 ¹	
25	13		

✓	✓	✓
441.9	444.9	461.3
6 ¹ - Top Bank	3 ¹	+ 13 ³
1 - Mud Edge Rd.	2	27

110+00

✓	✓	✓	✓
440.6	447.8	447.9	447.3
7 ⁴	5 ³	5 ¹	5 ⁷
28	24	13	

✓	✓	✓
447.1	445.6	461.3
5 ⁹	2 ⁴	+ 13 ³
4	5	27

+ 50

✓	✓	✓	✓
441.0	447.6	443.0	447.3
7 ⁰	5 ⁴	5 ⁰	5 ⁷
30	23	13	

✓	✓	✓
447.0	444.1	461.3
6 ⁰	3 ⁹	+ 13 ³
7	8	32

111+00

✓	✓	✓	✓
440.6	447.3	447.5	447.5
7 ⁴	5 ⁷	5 ⁵	5 ⁵
30	19	13	

✓	✓	✓
447.1	445.7	455.0
5 ⁹	2 ⁸	+ 7 ⁰
10	12	30

+ 50

✓	✓	✓	✓
440.7	447.7	447.5	447.8
7 ³	5 ⁸	5 ⁵	5 ²
26	18	13	

✓	✓	✓
447.3	443.0	447.4
5 ⁷	5 ⁰	6 ⁶
13	14	25

112+00

✓	✓	✓	✓	✓
441.1	441.4	447.9	443.1	443.7
6 ⁹	6 ⁶	5 ¹	4 ⁹	4 ⁸
25	19	16	13	

✓	✓	✓
447.9	444.7	446.7
5 ¹	3 ³	1 ⁸
14	16	25

+ 50

✓	✓	✓	✓
441.5	447.3	443.7	443.4
6 ⁵	5 ⁷	4 ⁸	4 ⁶
25	13	11	

✓	✓	✓
443.1	444.1	444.8
4 ⁹	3 ⁹	3 ²
16	18	25

113+00

✓	✓	✓
441.8	443.0	443.9
6 ²	5 ⁰	4 ¹
25	13	

5 ²	✓	✓
443.9	445.7	
4 ¹	2 ³	
18	25	

Computed and checked.
5/14/35
G.W.G.
Plotted
5/15/35

✓
448.05

113+50
 ✓ 442.9 5¹ 25
 ✓ 443.7 4³ 13
 ✓ 444.5 3⁵ 11
 ✓ 444.8 3²

114+00
 ✓ 442.8 5² 25
 ✓ 443.4 4⁴ 15
 ✓ 445.0 3² 12
 ✓ 445.2 2⁸

+50
 ✓ 441.9 6¹ 30
 ✓ 443.7 4⁸ 21
 ✓ 444.4 3⁶ 18
 ✓ 444.6 3⁴ 13
 ✓ 444.9 3¹

Start of Alternate Line #3
 114+84⁹⁷ B.C.

✓
445.0
3¹⁰

115+00
 ✓ 444.9 3¹ 25
 ✓ 445.4 2⁶ 13
 ✓ 445.0 3²
 T.P. 2.93 445.12

7.24 452.36

+50
 ✓ 445.8 6⁶ 25
 ✓ 445.9 6⁵ 13
 ✓ 445.3 7¹ - Bank

116+00
 ✓ 446.0 6⁴ 25
 ✓ 446.7 6² 13
 ✓ 446.0 6⁴

✓ 445.1 2⁹ 19
 ✓ 447.7 0³ 25

✓ 445.0 3² 16
 ✓ 446.7 1⁸ -17
 ✓ 447.6 0⁴ 25

5.3 ✓ 444.4 3⁶ 8
 ✓ 450.9 + 2⁹ 13
 ✓ 457.7 + 9² 27

✓ 444.7 3³ 3
 ✓ 455.7 + 7² 9
 ✓ 463.6 + 15⁶ 26

✓ 457.1 + 4⁷ 6
 ✓ 462.6 + 10² 19
 ✓ 467.6 + 15² 30

✓ 445.8 6⁶ 3
 ✓ 455.3 + 2⁹ 9
 ✓ 464.0 + 11⁶ 27

Computed & checked.
 5/12/35
 G.W.G.
 Plotted
 5/15/35

452.36

116+50	✓ AA3.8 8 ⁶ 25	✓ AA6.0 6 ² 20	✓ AA6.2 6 ² 13	✓ AA6.5 5 ⁹	✓ AA6.4 6 ⁰ 9	✓ AA7.5 4 ⁹ 10	✓ A53.5 + 1 ¹ 28
117+00	✓ AA4.6 7 ⁸ 27	✓ AA6.4 6 ⁰ 19	✓ AA6.8 5 ⁶ 13	✓ 447.4 5 ⁰	✓ AA7.4 5 ⁰ 14	✓ AA8.4 4 ⁰ 15	✓ AA9.4 3 ⁰ 25
+50	✓ AA4.1 8 ³ 25	✓ AA5.4 7 ⁰ 17	✓ AA6.6 5 ⁸ 15	✓ AA6.6 5 ⁸ 13	✓ AA7.5 4 ⁹ 15	✓ AA7.5 4 ⁹ 15	✓ A51.0 1 ² 18
118+00	✓ AA3.6 8 ⁸ 25	✓ AA5.5 6 ⁷ 13	✓ AA6.8 5 ⁶ 11	✓ AA7.5 4 ⁹	✓ AA7.5 4 ⁹ 17		
+50	✓ AA4.4 8 ⁰ 25	✓ AA5.1 7 ² 13	✓ AA5.3 7 ¹ 11	✓ AA6.9 5 ⁵ 7	✓ AA7.4 5 ⁰	✓ AA7.7 4 ⁷ 23	
119+00	✓ AA5.2 7 ² 25	✓ AA5.4 7 ⁰ 13	✓ AA6.4 6 ⁰ 5	✓ A52.4 0 ⁰ 3	✓ AA8.1 4 ³	✓ AA9.1 3 ³ 28	
+50	✓ AA5.5 6 ⁹ 25	✓ AA5.7 6 ⁷ 13	✓ AA6.8 5 ⁶ 3	✓ AA8.5 3 ⁹	✓ AA9.5 2 ⁹ 16	✓ A50.3 2 ¹ 32	
120+00	✓ AA5.8 6 ⁶ 25	✓ AA6.4 6 ⁰ 13	✓ AA7.0 5 ⁴ 4	✓ AA8.3 7 ¹	✓ AA9.7 2 ⁷ 15	✓ A50.2 2 ² 32	

Computed + checked.
5/14/35.
B.W.G.
Plotted
5/15/35

120+50	✓ 452.36 ✓ AA6.1 2 ³ 25	✓ AA7.1 5 ³ 13	✓ AA7.5 4 ⁹ 10	✓ AA8.6 3 ⁸ 5	✓ AA8.8 3 ⁵	✓ AA9.4 3 ⁰ 12	✓ AA9.6 2 ⁸ 26	✓
121+00		✓ AA6.6 7 ⁸ 25	✓ AA6.1 6 ³ 13	✓ AA7.8 4 ⁶ 11	✓ AA8.4 4 ⁰ 19			
T.P.	4.39		3.61	448.75				
	✓ 453.14							
+50	✓ AA5.0 8 ¹ 25	✓ AA5.5 7 ⁶ 20	✓ AA7.7 5 ⁹ 16	✓ AA7.3 5 ⁸ 13	✓ AA7.9 5 ²	✓ AA7.9 5 ² 13	✓ AA5.3 0 ⁸ 17	✓ AA5.1 +1 ² 24
122+00			✓ AA5.8 7 ³ 25	✓ AA6.7 6 ⁴ 13	✓ AA7.7 5 ²	✓ AA7.5 5 ⁶ 11	✓ AA5.6 0 ⁵ 15	✓ AA5.6 +4 ⁵ 25
+50	✓ AA5.7 7 ⁹ 27	✓ AA5.3 7 ⁸ 22	✓ AA7.0 6 ¹ 18	✓ AA7.7 5 ⁹ 13	✓ AA7.4 5 ²	✓ AA7.6 5 ⁵ 10	✓ AA5.1 2 ⁰ 12	✓ AA5.1 +2 ⁰ 25
123+00	✓ AA6.0 7 ¹ 25	✓ AA7.7 5 ⁹ 21	✓ AA7.8 5 ³ 13	✓ AA7.9 5 ²	✓ AA7.7 5 ⁴ 10	✓ AA7.7 5 ⁴ 10	✓ AA8.8 4 ³ 11	✓ AA5.1 1 ⁰ 25
+50		✓ AA6.5 6 ⁶ 25	✓ AA7.9 5 ² 13	✓ AA8.7 4 ⁹	✓ AA8.1 5 ⁰ 10	✓ AA8.1 5 ⁰ 10	✓ AA8.9 4 ² 11	✓ AA9.1 4 ⁰ 25

Computed + Checked
5/14/35.
b.n.o.
Plotted
5/18/35

453.14

	✓ AA5.6	✓ AA7.1	✓ AA7.6	✓ AA8.2	
124+00	7 ⁵ 25	6 ⁰ 20	5 ⁵ 13	4 ⁹	

+50	✓ AA5.5	✓ AA5.7	✓ AA7.8	✓ AA8.2	✓ AA8.4
	7 ⁶ 25	7 ⁷ 22	5 ³ 19	4 ⁹ 13	4 ⁷

125+00	✓ AA5.7	✓ AA8.8	✓ AA9.0	✓ AA9.3	
	7 ⁷ 25	4 ³ 18	4 ¹ 13	3 ⁸	

+50	✓ AA7.4	✓ AA7.8	✓ A50.2	✓ A50.3	✓ A50.2
	5 ⁷ 25	5 ³ 22	2 ⁹ 18	2 ⁸ 13	2 ⁹

126+00	✓ AA7.3	✓ AA8.5	✓ A51.5	✓ A51.6	✓ A51.4
	5 ⁸ 25	4 ⁶ 18	1 ⁶ 14	1 ⁵ 13	1 ⁷

+50	✓ AA5.5	✓ AA6.0	✓ AA6.8	✓ A52.0	✓ A52.3
	7 ⁶ 25	7 ¹ 17	6 ³ 13	1 ¹ 8	0 ⁸

127+00 use Orig. XSection at Sta. 126+50

A53.1
0⁰

127+03.50 P.I.
126+50⁺ P.O.T = Intersection with Co. Survey

A53.2
+0¹

0.7 452.4 = check on Sta. 126+00 of Co. Survey - Rec. Elev. 452.4
See Page 10, this Book.

✓ AA8.0	✓ AA8.8	✓ A53.9
5 ¹ 10	4 ³ 11	+0 ² 25

✓ AA8.5	✓ AA9.8	✓ A57.1
4 ⁶ 10	3 ³ 11	+4 ⁰ 27

✓ AA9.3	✓ A52.6	✓ A57.1
3 ⁸ 9	0 ⁵ 12	+4 ⁰ 25

✓ A50.2	✓ A51.1	✓ A58.1
2 ⁹ 9	2 ⁰ 11	+5 ⁰ 29

✓ A50.7	✓ A56.6	✓ A61.1
2 ⁴ 12	+3 ⁵ 15	+8 ⁰ 30

✓ A52.3	✓ A59.1	✓ A63.1
0 ⁸ 18	+6 ⁰ 23	+10 ⁰ 23

Computed & checked.
 5/14/35.
 G. W. G.
 Plotted
 5/15/35

Bench levels from El Capitan Dam to El Monte Park.

Soper
Remmen
Oct. 11, 1935

64

(Corrected Elev) (See note on page 65)

B.M. 563.65

B.M. #1 Point on rock 40' Rt. 12+70

11.44 575.09

TP. 3.65 571.44

2.11 573.55

3.05 570.50 570.57

(Book 316)
Check on old B.M. #2 (Nail in sycamore tree) Recorded El. 570.56
New B.M. #2 - 14' right of 16+82

TP. 5.52 568.03

6.35 574.38

TP. 4.97 569.41 569.48

Set new B.M. #3 Nail in triple oak - 25' Rt. Sta 19+80

1.45 570.86

TP. 5.88 564.98

3.32 568.30

TP. 4.60 563.70

9.61 573.31

0.67 572.64 572.71

Point on rock
✓ on old B.M. El. 572.71 (Book 316) - New B.M. #4. 23' Rt. 26+15

TP. 5.28 568.03

6.77 574.80

TP. 0.25 574.55

574.55 (Corrected Elev)

11.73 586.28

TP 6.62 579.66 579.73

Set new B.M. #5. Nail in crotch of 30" oak. 100' E of end of 6.4% road.

0.52 580.18

TP 11.58 568.60

0.44 569.04

TP 7.76 561.28

8.66 569.94

1.13 568.81 568.88

← on B.M. #4 El. 568.88 (Book 316) Use for new B.M. #6
Nail in S. side 24" oak. 50' Lt. Sta. 38+25

Note: Difference in two sets of levels = 0.07 (see book # 308 page 56). Use B.M. #1 to station 12+50. Use B.M. #2 from Sta. 12+50.

B.M. #6 568.88

0.98 569.86

TP 12.13 557.73

0.51 558.24

TP 6.55 551.69

2.83 554.52

554.52

TP 5.83 548.69

3.27 551.96

TP 8.32 543.64

3.90 547.54

8.05 539.49

Set new B.M. #7 Paint on rock 35' Rt. Sta. 51+50

TP 2.55 544.99

3.10 548.09

TP 6.52 541.57

1.48 543.05

TP 3.37 539.68

on old B.M. Elev. 539.69 (to close to pipe line)

0.92 540.60

TP 4.96 535.64

set new B.M. #8 13' Rt. Sta. 59+50 Nail in 24" oak.

4.47 540.11

TP 7.77 532.34

4.02 536.36

TP 3.96 532.40

5.35 537.75

537.75

TP. 0.52 537.23

Oct. 16 1935 - Saper - Remmen

B.M. 537.23

0.85 538.08

TP 6.74 531.34

6.52 537.86

TP 2.83 535.03

7.32 542.35

TP 0.30 542.05

7.44 549.49

10.40 539.09

TP 5.28 544.21

4.86 549.07

0.63 548.44

Check on old B.M. #10. Nail in oak stump. 25' Rt. Sta. 75+15

TP 9.22 539.85

0.72 540.57

New B.M. #9 Nail in 24" oak. 40' Lt. Sta. 68+85
Old Rec. El. 537.23 (Book 317 page 68)

Set new B.M. #10. Nail in oak stump. 25' Rt. Sta. 75+15

New B.M. #11. Nail in oak tree 75' Lt. Sta. 78+75

	540.57		
TP		12.48	528.09
	6.15	534.24	
TP		4.44	529.80
	1.32	531.12	
TP		6.02	525.10
	2.94	528.04	
TP		4.00	524.04
	6.85	530.89	
TP		3.18	527.71
	8.79	536.50	
TP		0.56	535.94
	9.81	545.75	
TP		11.60	534.15
	0.91	535.06	
TP		8.38	526.68
	1.17	527.85	
	2.74	525.11	

check on old B.M. #1. 525.00. New B.M. #12, nail in 30" oak 8' Rt. Sta. 88+70

Set new B.M. #13 Nail in 4"x4" fence post. 8' Rt. Sta. 97+10

Set new B.M. #14. Nail in 18" oak tree. 12' Rt. Sta. 102+95

527.85

TP. 5.99 521.26

9.56 531.42

TP. 8.02 523.40 ←

0.86 524.26

5.43 518.83

523.40 ←

0.58 523.98

TP. 7.04 516.94

4.56 521.50

TP. 7.89 513.61

2.38 515.99

TP. 4.64 511.35

3.83 515.18

TP. 5.62 509.56

5.33 514.89

0.46 514.43 Check on

old B.M. #1514.43. Nail in S.W. fork of 40" oak tree. 1' Rt. Sta 120+05
 (Book 216 page 30) New B.M. #17

Set new B.M. #15. Nail in 12" Sycamore 12' Lt. Sta. 107+30
 (Northern Limb of a group of 5)

Set new B.M. #16 Nail in W. side of 24" Willow tree. 25' Lt. Sta 116+50

Bench levels from El Monte Park to Lakeside

Oct 24 1935
Soper
Remmen

70

B.M. #17 514.43

0.00 514.43

TP 4.92 509.51

3.43 512.94

TP 4.76 508.18

3.02 511.20

TP 3.75 507.45

2.77 510.22

Set new B.M. #18. Nail in 6"x6" post. West end post of El Monte Park Entrance
35' Lt Sta 129+25

TP 4.89 505.33

4.08 509.41

TP 5.36 504.05

4.65 508.70

TP 5.08 503.62

Set new B.M. #19. Nail in 36" oak 5' Rt Sta 139+95

2.82 506.44

TP 5.20 501.24

4.97 506.21

TP 2.69 503.52

Set new B.M. #20. Nail in 36" oak. 20' Rt. Sta 146+40

2.78 506.30

	506.30		
TP		5.07	501.23
	7.82	509.05	
TP		2.56	506.49
	2.32	508.81	
TP		4.37	504.44
	2.75	507.19	
TP		6.07	501.12
	7.73	508.85	
TP		5.85	503.00
	3.90	506.90	
TP		6.40	500.50
	5.67	506.17	
TP		3.57	502.60
	3.94	506.54	
TP		8.58	497.96
	11.87	509.83	
TP		5.92	503.91

✓ on old B.M. El. 501.09. (Book 316) New B.M. #21. Nail in Sycamore 25' Rt. Sta. 122+95

Set new B.M. #22. Nail in power pole #75551. 35' Lt. Sta. 170+10

Ctd from page 11

		503.91	
	2.75	506.66	
TP		11.49	495.17
	2.63	497.80	
TP		4.13	493.69
	0.20	493.87	
		2.48	491.39
TP		4.32	489.55
	4.67	494.22	
TP		2.35	491.87
	5.21	497.08	
TP		2.40	494.68
	0.28	494.96	
TP		6.37	488.59
	2.54	491.13	
TP		3.65	487.48
	2.82	490.30	
TP		2.47	487.83

Nov. 16 1935
Soper
Remmon

12

Set new B.M. #23. Nail in power pole #173435. 30' Lt. Sta. 184+80

✓ on old B.M. #22 (El. 491.37) El. 491.75 by Simpson Book 316 page 39

Set new B.M. #24 Nail in power pole #173430. 35' Lt. Sta. 196+05

Set new B.M. #25 Nail in power pole #173427 30' Lt. Sta. 205+95

			487.83
	2.70	490.53	
TP		2.95	487.58
	3.50	491.08	
TP		6.80	484.28
	2.86	487.14	
TP		3.87	483.27
	3.68	486.95	
TP		3.37	489.58
	2.36	485.94	
TP		6.30	479.64
	6.52	486.16	
TP		9.82	476.34
	8.46	484.80	
		4.56	480.24
TP		0.13	484.67
	10.24	494.91	
TP		0.07	494.84

^{#25A}
 ← to B.M. Elev. 487.58. (this pole will be outside of R/W of road relocation)

Set new B.M. #26 Nail in power pole #173422 30' Lt. Sta. 218+45

Set new B.M. #27 Nail in 24" oak tree 50' Lt. Sta. 226+50.
 Elev. 480.23 (page 76 - check levels)

Ctd from page 73

Nov. 18 1935
Soper
Remmen

74

494.84

9.31 504.15

TP

1.33 502.82

✓ on old

B.M. # 22 Elev. 502.88 New B.M. # 28. Nail in 30" oak 20' Rt Sta. 231+50
Elev 502.84 - page 76 (check levels)

1.40 504.22

TP

12.62 491.60

0.04 491.64

TP

12.94 478.70

0.15 478.85

TP

8.26 470.59

1.44 472.03

TP

6.04 465.99

4.22 470.21

8.39 461.82

TP

9.19 461.02

Set new B.M. # 29. Nail in 8" Sycamore 60' Rt. Sta. 243+15
Elev. 461.86 - (page 77 - check levels)

2.29 463.30

TP

5.52 457.78

2.58 460.36

TP

4.93 455.43

Cont'd from page 74

455.43

3.49 458.92

T.P.

4.86 ~~454.06~~

Set new B.M. # 30. Nail in 1"x2" marker. On fence line - 70' Rt. Sta. 252+80
Elev 454.11 (page 77 - check levels)

3.63 457.69

T.P.

5.91 451.88

4.69 456.57

T.P.

0.20 456.37

8.66 465.03

~~463.61~~
1.42 ~~463.81~~

Too old B.M. # 25 Rec. Elev. 463.70 Book 316 page 49
Elev. 463.66 (page 77 - check levels)
New B.M. # 30A.

Cont'd on page 78

75

Friday Dec. 13 1935

Super
Remmen

76

Check levels from B.M. #25H to old B.M. #25

B.M. 3.11 490.69 487.58

TP 7.27 483.42

4.40 487.82

TP 4.24 483.58

2.34 485.92

TP 6.78 479.14

7.22 486.36

TP 6.13 480.23

5.39 485.62

TP 0.09 485.53

9.83 495.36

TP 0.32 495.04

9.68 ^{504.72}
404.72

TP 1.88 502.84

1.29 504.13

TP 12.82 491.31

0.11 491.42

check on B.M. #26 Elev. 483.58

check on B.M. #27 Elev. 480.24

check on B.M. Elev. 502.88. Book 316.

Cont'd from page 76

77

491.42

TP 12.75 478.67

1.21 479.88

TP 10.09 469.79

1.30 471.09

TP 9.46 461.63

4.77 466.40

4.54 461.86

check on B.M. 29 Elev 461.82 Changed to 461.86

1.70 463.33 461.63

TP 5.74 457.59

2.11 459.70

TP 5.65 454.05

3.06 457.11

3.00 454.11

B.M. 30 changed to Elev. 454.11

TP 0.40 456.71

10.82 467.53

3.87 463.66

B.M. 30A.

Bench levels - continued from page 75

B. M. #30A 1.41 465.07 463.66

TP 5.45 459.62

3.40 463.02

TP 2.12 460.90

0.92 461.82

TP 7.02 454.80

3.61 458.41

TP 0.76 457.69

0.15 ~~458.84~~
457.84

TP 3.88 ~~454.96~~
53.96

5.80 ~~460.76~~
59.76

TP 1.76 ~~459.00~~
458.00

1.66 459.66

TP 6.77 452.89

0.48 453.37

TP 5.25 448.12

Set new B.M. #31 spike in rock 40' Lt Sta. 264+00

Set new B.M. #32 spike in south side of 18" Sycamore. North limb of a clump of sycamores. 55' Lt Sta 272+50

check on old B.M. #458.00 (page 11 1/2 book) Use for New B.M. #33
Nail in 24" oak 35' Lt 280+90

Cont'd from page 78

448.12

7.03 455.15

TP 6.96 448.19

2.24 450.43

TP 6.82 443.61

3.89 447.50

TP 4.71 442.79

3.59 446.38

TP 6.84 439.54

5.65 445.19

6.26 438.93

Bench levels continued in
Book # 506 page 52

79

Set new B.M. #34 Nail in 36" Sycamore 30' Rt 297+00

U.S.G.S. Gauging station at El Monte Pumping Plant
New B.M. # 35

CALCULATION OF EARTHWORK.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
Roadway 16 feet wide, Side Slopes 1 on 1 1/2
For Single Track Embankment.

6000
12
360 A
12 X
48

Width	HEIGHT														
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.56	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w = 16.2$ and $h = 5.3$, cu. yds. $= 1.48 + .028 + .089 = 1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) $= h$, and $\frac{1}{2}$ the roadbed $= w$, add the triangles formed by taking the distance out to each break in turn ($= w$'s) by the difference between the cuts (or fills) on each side of it ($= h$'s) always subtracting the outer from the inner.

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 $= 43.9$. For slopes of 1 on 1 see inside of front cover.