

W
SOS

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

506

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

180+15

B.M. #22 = 502.88

491.35-47.

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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Made in U. S. A.

506.

Index

Profile + Cross Section of County Road

Survey of 1935 El Monte Pumping

Plant to El Monte Park Sta 180⁺ to 288⁺ 79-1-34

Profile of revised line from

sta 239+66.92 to sta 279+00 35-47

Profile levels of revised Pipe line from

sta 131+73.24 to sta 155+00 48-51

Bench levels Pumping Plant to Lakeside 52-56

Profile on line change 131 - 160 57-65

Bench levels via Julian Ave 66-68

H

0
1
2
3
4
5
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39
40

Exam
to be a sl
of roadbed
example a
30.6 = 32.6

Profile And Cross-sections of Co.
Road Survey #512, From El-Monte Pumping
Plant To El-Monte Park.

Cont'd. From Book #505-Page 25.

B.M. 502.88

0.24 503.12

L.

Φ.

R.

180+41

499.4

37[±] outside
35 Edge Rd.

497.7

54[±]
13

496.7

64[±] inside
Edge Rd.

506.2

+ 3[±]
5

511.2

+ 8[±]
25

+50

498.7

44[±] "
30

497.6

55[±]
13

496.3

68[±]

496.0

7[±] inside
5 Edge Rd.

505.0

+ 12[±]
10

509.0

+ 59[±]
30

180+96

487.3

158[±]
35

490.2

129[±]
13

490.4

127[±]
9

494.1

90[±] outside
Edge Rd.

492.0

11[±] inside
36 Edge Rd.

T.P.

12.87

490.25

0.77 491.02

181+27

479.8

11E
30

482.9

8[±]
13

484.2

68[±]

488.2

28[±]
16

491.1

+ 0[±] outside
22 Edge Rd.

489.3

17[±] inside
58 Edge Rd.

+50

476.1

149[±]
30

477.6

134[±]
13

479.8

11E

484.1

69[±]
24

489.0

20[±] "
36

4/6/35
Plotted
G.M.C.
A-8-35

April-3-1935.
Hill-Simpson
Soper-Remmen.

1.

Cont'd. From Page 1.

April-3-1935.

2.

	491.02 ✓	L.	£	R.			
T.P.		12.85	478.17 ✓				
	0.51	478.68 ✓					
181+76		472.9 ✓ 58 30	474.2 ✓ 45 13	475.9 ✓ 28	479.0 ✓ +02 25		
+85	465.0 ✓ 137 30	465.9 ✓ 128 14	474.3 ✓ 44 6	475.0 ✓ 37	478.2 ✓ 05 30		
182+00	465.5 ✓ 132 25	465.5 ✓ 132 13	465.6 ✓ 131 9	473.8 ✓ 49	477.7 ✓ 10 35		
+15		465.8 ✓ 129 25	465.8 ✓ 129 13	466.0 ✓ 127	474.2 ✓ 45 8	475.1 ✓ 36 25	
+50		465.7 ✓ 130 25	465.7 ✓ 130 13	465.8 ✓ 129	465.6 ✓ 131 10	474.0 ✓ 47 17	474.4 ✓ 43 30
183+00		465.8 ✓ 129 25	465.9 ✓ 128 13	466.0 ✓ 127	466.0 ✓ 127 27	474.0 ✓ 47 33	476.5 ✓ 22 outside 57 Edge Rd.
T.P.		2.96	475.72 ✓				
	5.58	481.30 ✓					

Plotted
G.W.G.
4-8-35

481.30 ✓

L.

£.

R.

183+50	466.1 15 ² 25	466.3 15 ⁰ 13	466.4 14 ⁹	466.5 14 ⁸ 11	474.3 7 ⁰ 16	475.9 5 ⁴ outside 35 Edge Rd.
+85	466.6 15 ⁰ 25	467.0 14 ³ 13	468.0 13 ³	468.6 12 ⁷ 4	474.1 7 ² 5	475.8 5 ⁵ outside 19 Edge Rd.
184+00	466.6 15 ¹ 25	466.6 14 ⁷ 13	469.6 11 ⁷ 2	474.3 7 ⁰	475.7 5 ⁶ outside 13 Edge Rd.	476.1 5 ² inside 50 Edge Rd.
+25	466.5 14 ⁸ 25	466.8 14 ⁵ 16	474.5 6 ⁸ 13	475.8 5 ⁵	476.4 4 ⁹ 2	475.8 5 ⁵ 39
+50	467.1 14 ² 36	474.7 6 ⁶ 34	477.1 4 ² outside 13 Edge Rd.	476.8 4 ⁵	476.1 5 ² inside 28 Edge Rd.	
+93	478.8 2 ⁵ outside 38 Edge Rd.	477.8 3 ⁵ 13	476.9 4 ² inside Edge Rd.	479.5 1 ⁸ 2	481.8 +0 ⁵ 16	485.0 +3 ² 30
+96	479.1 2 ² outside 40 Edge Rd.	477.8 3 ⁵ 13	477.0 4 ³ inside 2 Edge Rd.	480.0 1 ³	481.8 +0 ⁵ 15	485.3 +4 ⁰ 30
T.P.	0.40	480.90				

12.44 493.34 ✓

Plotted
G.W.G.
4-8-35

Cont'd. From Page 3

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4.

	493.34 ✓	L.	£.	R.
185+25	480.3 ✓ 13° outside 52 Edge Rd.	478.4 ✓ 14° inside 20 Edge Rd.	483.4 ✓ 9° 14	486.4 ✓ 6° 16
+50	479.7 ✓ 14° inside 29 Edge Rd.	485.6 ✓ 7° 26	488.7 ✓ 5° 13	490.9 ✓ 2° 15
T.P.	9.93	502.23 ✓	1.04	492.30 ✓
+75	479.9 ✓ 22° inside 34 Edge Rd.	488.7 ✓ 14° 30	492.4 ✓ 9° 13	499.8 ✓ 2° 13
186+00	480.5 ✓ 21° " 33	488.4 ✓ 13° 28	494.5 ✓ 7° 13	497.7 ✓ 5° 12
+35	480.9 ✓ 21° 30	480.6 ✓ 21° " 23	488.9 ✓ 13° 20	492.9 ✓ 9° 13
+55	480.6 ✓ 21° 30	488.9 ✓ 13° 20	492.9 ✓ 9° 13	498.7 ✓ 4° 10
	480.6 ✓ 21° 30	480.3 ✓ 21° 17	490.6 ✓ 11° 12	495.0 ✓ 7° 15
				498.4 ✓ 3° 13
				500.1 ✓ 2° 12
				500.7 ✓ 2° 10
				500.7 ✓ 2° 15
				503.5 ✓ +1° 30
				503.8 ✓ +1° 17
				506.4 ✓ +4° 30
				506.4 ✓ +3° 30

Plotted
G.W.C.
4-8-35

Cont'd. From Page 4.

April-3-1935.

5

	502.23 ✓	L.	Φ.	R.
186+85	489.5 ✓ 21 ⁷ outside 45 Edge Rd.	480.6 ✓ 21 ⁶ 13	480.5 ✓ 21 ⁷ inside 5 Edge Rd.	490.5 ✓ 11 ⁷
T.P.		12.18	490.05 ✓	496.4 ✓ 5 ⁸ 15
	3.27	493.32		500.7 ✓ 1 ⁵ 30
T.P.		12.21	481.11 ✓	
	3.43	484.54		
187+00	480.3 ✓ 4 ² Edge 42 Rd.	480.6 ✓ 3 ⁹ Edge 13 Rd.	480.3 ✓ 4 ²	489.7 ✓ +5 ² 2
+50	479.6 ✓ 4 ² 35	480.1 ✓ 4 ² 13	480.2 ✓ 4 ²	495.1 ✓ +10 ⁶ 16
188+00	478.8 ✓ 5 ⁷ 30	479.4 ✓ 5 ¹ 13	479.6 ✓ 4 ²	499.6 ✓ +15 ¹ ± 30
+50	476.8 ✓ 7 ⁷ 28	478.5 ✓ 6 ⁰ 22	478.8 ✓ 5 ⁷ 13	489.7 ✓ +5 ² 14
	476.3 ✓ 8 ² 34	478.2 ✓ 6 ³ 20	479.1 ✓ 5 ⁴	494.7 ✓ +10 ² ± 30
189+00				478.9 ✓ 5 ⁶ 15
				484.2 ✓ 0 ³ 13
				491.2 ✓ +6 ⁷ ± 30
				478.5 ✓ 6 ⁰ 13
				482.4 ✓ 2 ¹ 15
				486.5 ✓ +2 ⁰ ± 30
				478.9 ✓ 5 ⁶ 15
				482.4 ✓ 2 ¹ 17
				486.5 ✓ +2 ⁰ ± 30

Plotted
G.W.G.
4-8-35

484.54 ✓

L.

E.

R.

	476.7 ✓	477.7 ✓	478.3 ✓	479.0 ✓	479.2 ✓	482.6 ✓	485.5 ✓
189+50	7 ⁸	6 ⁸	6 ² Edge	5 ⁵	5 ³ Edge	1 ⁹	+ 1 ⁰ ±
	30	13	11 Rd.		22 Rd.	25	35

	477.0 ✓	477.1 ✓	478.4 ✓	481.0 ✓
190+00	7 ⁵	7 ⁹	6 ¹ Edge	3 ⁵ Edge
	30	13	Rd.	33 Rd.

T.P.

4.62 479.92 ✓

6.77 486.69 ✓

	477.0 ✓	477.4 ✓	477.9 ✓	478.6 ✓	481.7 ✓
+50	9 ⁷	9 ³	8 ⁸	8 ¹ Edge	5 ⁰ Edge Rd.
	30	13		12 Rd.	43

	477.7 ✓	477.8 ✓	478.0 ✓	478.9 ✓	480.8 ✓
191+00	9 ⁰	8 ²	8 ²	7 ⁸ "	5 ⁹ "
	25	13		10	35

	478.0 ✓	478.2 ✓	479.1 ✓	479.6 ✓	480.5 ✓
+50	8 ⁷	8 ⁵	7 ⁶	7 ¹ Edge	6 ² Edge
	25	13	7	Rd.	26 Rd.

	478.1 ✓	478.3 ✓	480.4 ✓	480.8 ✓	480.9 ✓	482.5 ✓
192+00	8 ⁶	8 ⁴	6 ³	5 ²	5 ⁸ "	4 ²
	25	20	15		18	27

Plotted
G.W.G.
4-8-35

	486.69 ✓	L.		Φ.		R.		
192+50	478.9 ✓ 7 ⁸ 30	478.8 ✓ 7 ⁹ 23	480.9 ✓ 5 ⁸ 17	481.3 ✓ 5 ⁴ 13	481.7 ✓ 5 ⁰	481.6 ✓ 5 ¹ 15	483.7 ✓ 3 ⁰ 25	
193+00			480.8 ✓ 5 ⁹ 25	481.8 ✓ 4 ⁹ 13	482.2 ✓ 4 ⁵	482.2 ✓ 4 ⁵ 14	484.1 ✓ 2 ⁵ 25	
+50		480.7 ✓ 6 ⁰ 25	481.5 ✓ 5 ² 18	482.1 ✓ 4 ⁶ 13	482.5 ✓ 4 ²	482.7 ✓ 4 ⁰ 15	483.8 ✓ 2 ⁹ 25	
194+00	480.9 ✓ 5 ⁸ 25	480.5 ✓ 6 ² 19	481.9 ✓ 4 ⁸ 16	482.2 ✓ 4 ⁵ 13	482.8 ✓ 3 ⁹	483.0 ✓ 3 ⁷ 15	483.9 ✓ 2 ⁸ 25	
+50		481.1 ✓ 5 ⁶ 25	482.3 ✓ 4 ⁴ 21	482.7 ✓ 4 ⁰ 13	483.1 ✓ 3 ⁶	483.0 ✓ 3 ⁷ 14	485.2 ✓ 1 ⁵ 16	486.1 ✓ 0 ⁶ 25
195+00		480.3 ✓ 6 ⁴ 25	482.8 ✓ 3 ⁹ 16	482.8 ✓ 3 ⁹ 13	483.4 ✓ 3 ³	483.1 ✓ 3 ⁶ 15	487.0 ✓ 10 ³ 18	486.4 ✓ 0 ³ 25
+50		479.2 ✓ 7 ⁵ 25	482.3 ✓ 4 ⁴ 17	482.4 ✓ 4 ³ 13	483.1 ✓ 3 ⁶	482.9 ✓ 3 ⁸ 17	484.6 ✓ 2 ¹ 20	485.3 ✓ 1 ⁴ 25
T.P.		4.78	481.91					
	9.02	490.93						

Plotted
G.M.G.
A-8-35

	490.93 ✓	L.	Φ.	R.			
196+00	478.7 ✓ 12 ² 25	481.7 ✓ 9 ² 16	481.9 ✓ 9 ⁰ 13	482.9 ✓ 8 ⁰ 18	485.0 ✓ 5 ² 21	486.7 ✓ 4 ² 25	
+50	479.7 ✓ 11 ² 25	481.5 ✓ 9 ² 17	482.0 ✓ 8 ² 13	482.8 ✓ 8 ¹	483.0 ✓ 7 ² 18	485.8 ✓ 5 ¹ 21	486.7 ✓ 4 ² 25
197+00	480.0 ✓ 10 ⁹ 25	482.1 ✓ 8 ² 18	482.4 ✓ 8 ⁵ 13	483.0 ✓ 7 ²	482.7 ✓ 8 ² 17	486.6 ✓ 4 ³ 23	
+50	480.5 ✓ 10 ² 25	483.2 ✓ 7 ² 18	483.0 ✓ 7 ² 13	483.3 ✓ 7 ⁶	482.9 ✓ 8 ⁰ 18	488.7 ✓ 2 ² 25	
198+00	480.1 ✓ 10 ⁸ 25	483.0 ✓ 7 ² 17	483.2 ✓ 7 ² 13	483.6 ✓ 7 ³	483.3 ✓ 7 ⁶ 19	487.9 ✓ 3 ⁰ 25	
+50	480.5 ✓ 10 ² 25	483.5 ✓ 7 ² 19	483.9 ✓ 7 ⁰ 13	484.4 ✓ 6 ⁵	484.2 ✓ 6 ⁷ 18	487.4 ✓ 3 ⁵ 21	489.0 ✓ 1 ² 25
199+00	482.9 ✓ 8 ⁰ 25	484.6 ✓ 6 ³ 20	485.0 ✓ 5 ² 13	485.3 ✓ 5 ⁶	485.4 ✓ 5 ⁵ 15	487.0 ✓ 3 ² 25	
+50	485.9 ✓ 5 ⁰ 25	485.5 ✓ 5 ² 21	486.0 ✓ 4 ² 13	486.3 ✓ 4 ⁶	486.1 ✓ 4 ⁸ 15	492.7 ✓ +1 ² 20	493.5 ✓ +2 ⁶ 25

Plotted
G.W.C.
4-8-35

Contd. From Page 9.

April-3-1935.

10

490.57 ✓ L.

£.

R.

203+50
 483.8 ✓ 483.8 ✓ 485.0 ✓ 485.0 ✓
 6⁸ 6⁸ 5⁶ 5⁶
 25 13 7

485.1 ✓
 4⁹
 25

204+00
 483.6 ✓ 484.1 ✓ 485.8 ✓ 485.8 ✓
 7⁰ 6⁵ 4⁸ 4⁸
 25 20 13

485.8 ✓ 487.5 ✓
 4⁸ 3¹
 18 25

+50
 484.9 ✓ 485.8 ✓ 486.0 ✓
 5⁷ 4⁸ 4⁶
 25 13

486.0 ✓ 488.0 ✓ 488.0 ✓
 4⁶ 2⁶ 2⁶
 15 20 25

205+00
 486.1 ✓ 485.8 ✓ 486.1 ✓
 4⁵ 4⁸ 4⁵
 25 13

486.0 ✓ 488.4 ✓ 488.4 ✓
 4⁶ 2² 2²
 15 19 25

+50
 486.0 ✓ 485.9 ✓ 486.0 ✓
 4⁶ 4⁷ 4⁴
 25 13

486.0 ✓ 488.6 ✓ 488.6 ✓
 4⁴ 2⁰ 2⁰
 15 20 25

206+00
 485.3 ✓ 485.5 ✓ 486.0 ✓
 5³ 5¹ 4⁶
 25 13

486.1 ✓ 487.7 ✓ 487.7 ✓
 4⁵ 2⁹ 2⁹
 17 20 25

+50
 485.2 ✓ 485.6 ✓ 486.3 ✓
 5⁴ 5⁰ 4³
 25 13

485.9 ✓ 488.0 ✓ 488.0 ✓
 4⁷ 2⁶ 2⁶
 16 20 25

207+00
 484.7 ✓ 486.0 ✓ 486.7 ✓
 5⁷ 4⁶ 3⁹
 25 13

486.4 ✓ 488.3 ✓ 488.3 ✓
 4² 2³ 2³
 16 20 25

Plotted
 G.W.G.
 4-8-35

Cont'd. From Page 10.

April-3-1935

11.

490.57 ✓ W. \$.

R.

207+50

485.4 ✓ 486.4 ✓ 487. ✓
 $5\frac{2}{25}$ $4\frac{2}{13}$ $3\frac{4}{13}$

486.6 ✓ 488.9 ✓ 488.9 ✓
 $4\frac{2}{17}$ $1\frac{2}{20}$ $1\frac{2}{25}$

208+00

488.1 ✓ 486.9 ✓ 487.3 ✓ 487.5 ✓
 $2\frac{3}{25}$ $3\frac{2}{19}$ $3\frac{3}{13}$ $3\frac{1}{13}$

487.1 ✓ 490.0 ✓ 490.6 ✓
 $3\frac{5}{16}$ $0\frac{6}{17}$ $0\frac{0}{25}$

+50

488.6 ✓ 487.4 ✓ 487.5 ✓ 487.8 ✓
 $2\frac{0}{25}$ $3\frac{2}{20}$ $3\frac{1}{13}$ $2\frac{8}{13}$

487.4 ✓ 492.3 ✓ 493.4 ✓
 $3\frac{2}{16}$ $+1\frac{2}{17}$ $+2\frac{8}{25}$

209+00

486.9 ✓ 487.0 ✓ 487.6 ✓
 $3\frac{2}{25}$ $3\frac{6}{13}$ $3\frac{0}{13}$

487.0 ✓ 492.1 ✓ 493.1 ✓
 $3\frac{6}{16}$ $+1\frac{5}{18}$ $+2\frac{5}{25}$

T.P.

2.80 487.77 ✓

6.96 494.73 ✓

+50

484.6 ✓ 486.5 ✓ 486.5 ✓ 487.3 ✓
 $10\frac{1}{25}$ $8\frac{2}{17}$ $8\frac{2}{13}$ $7\frac{4}{13}$

486.7 ✓ 488.6 ✓ 490.2 ✓
 $8\frac{0}{16}$ $6\frac{1}{18}$ $4\frac{5}{25}$

210+00

483.4 ✓ 483.3 ✓ 486.3 ✓ 487.0 ✓
 $11\frac{3}{25}$ $11\frac{4}{20}$ $8\frac{4}{13}$ $7\frac{2}{13}$

486.9 ✓ 487.5 ✓
 $7\frac{8}{20}$ $7\frac{2}{25}$

+50

483.3 ✓ 483.5 ✓ 486.3 ✓ 486.5 ✓ 487.0 ✓
 $11\frac{4}{25}$ $11\frac{2}{20}$ $8\frac{4}{15}$ $8\frac{2}{13}$ $7\frac{2}{13}$

486.5 ✓ 486.6 ✓
 $8\frac{2}{15}$ $8\frac{1}{25}$

Plotted
 G.W.G.
 A. 8-35

Cont'd. From Page 11.

494.73

L.

♀

211+00	483.5 11 ² 25	483.8 10 ⁹ 21	486.3 8 ⁴ 15	486.6 8 ¹ 13	487.2 7 ⁵
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+50	483.7 11 ⁰ 25	484.3 10 ⁴ 21	487.1 7 ⁶ 15	487.2 7 ⁵ 13	487.7 7 ⁰
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212+00	485.5 9 ² 25	485.6 9 ¹ 21	487.8 6 ⁹ 16	487.8 6 ⁹ 13	488.3 6 ⁴
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+50	486.9 7 ⁸ 25	487.2 7 ⁵ 21	488.3 6 ⁴ 18	488.5 6 ² 13	489.0 5 ⁷
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213+00	488.1 6 ⁶ 25	488.4 6 ³ 21	489.4 5 ³ 18	489.4 5 ³ 13	489.9 4 ⁸
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+50		489.8 4 ⁹ 25	490.1 4 ⁶ 13	490.5 4 ²	
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214+00		491.0 3 ⁷ 25	490.7 4 ⁰ 13	491.1 3 ⁶	
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+50		491.6 3 ¹ 25	491.0 3 ⁷ 13	491.5 3 ²	
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April-4-1935

Hill - Simpson

Soper - Remmen,

R.

12.

487.1 7 ⁶ 15	487.2 7 ⁵ 25
-------------------------------	-------------------------------

487.6 7 ¹ 15	487.6 7 ¹ 25
-------------------------------	-------------------------------

488.0 6 ⁷ 15	488.9 5 ⁸ 25
-------------------------------	-------------------------------

488.8 5 ⁹ 17	490.9 3 ⁸ 25
-------------------------------	-------------------------------

489.6 5 ¹ 18	491.2 3 ⁵ 20	492.3 2 ⁴ 25
-------------------------------	-------------------------------	-------------------------------

490.0 4 ⁷ 18	492.3 2 ⁴ 19	493.3 1 ⁴ 25
-------------------------------	-------------------------------	-------------------------------

490.8 3 ⁹ 18	493.2 1 ⁵ 19	494.3 0 ⁴ 25
-------------------------------	-------------------------------	-------------------------------

491.5 3 ² 18	494.4 0 ² 20	495.2 1 ⁰ 25
-------------------------------	-------------------------------	-------------------------------

Plotted
G.W.C.
4-8-35

494.73 ✓ L. £.

	490.8 ✓ 37 25	491.3 ✓ 34 13	491.9 ✓ 28
215+00			
+50	491.0 ✓ 37 25	491.4 ✓ 33 13	492.2 ✓ 25
216+00	491.2 ✓ 35 25	491.8 ✓ 29 13	492.6 ✓ 21
+50	492.1 ✓ 26 25	492.2 ✓ 25 13	492.8 ✓ 19

T.P. 2.56 492.17 ✓

2.77 494.94 ✓

217+00	492.5 ✓ 24 25	493.3 ✓ 16 17	492.1 ✓ 28 15	492.2 ✓ 27 13	492.9 ✓ 20
+50	492.1 ✓ 28 25	493.2 ✓ 17 17	491.8 ✓ 31 15	492.0 ✓ 29 13	492.9 ✓ 22
218+00	491.4 ✓ 35 25	492.8 ✓ 21 16	491.5 ✓ 34 13	492.2 ✓ 27	

R.

491.9 ✓ 28 20	494.4 ✓ 03 21	495.9 ✓ +12 25
492.1 ✓ 26 20	494.6 ✓ 01 21	495.8 ✓ +12 25
492.5 ✓ 22 20	494.6 ✓ 01 21	495.8 ✓ +12 25
492.7 ✓ 20 20	495.3 ✓ +08 21	496.1 ✓ +14 25

492.4 ✓ 25 20	495.6 ✓ +02 22	496.7 ✓ +18 25
492.3 ✓ 26 20	495.7 ✓ +08 22	496.3 ✓ +14 25
492.2 ✓ 27 19	495.2 ✓ +03 22	495.7 ✓ +08 25

Plotted
G.M.G.
A-8-35

Cont'd. From Page 13.

April-4-1935
Rain.

14.

	494.94	L.		Q.		R.		
218+50	489.1 58 25	489.2 56 19	491.3 36 15	490.7 42 13	491.2 37	491.1 38 20	493.5 14 22	494.0 09 25
219+00		487.7 72 25	488.1 68 19	490.4 45 13	490.4 45	490.0 49 20	490.9 40 25	
+50		489.0 59 25	489.5 54 14	490.3 46 13	490.1 48	490.1 48 21	491.0 39 25	
220+00		488.5 64 25	488.4 65 14	489.6 53 13	490.2 47	490.0 49 21	490.6 43 22	491.0 39 25
+50			488.7 62 25	489.5 54 13	490.2 47	489.9 50 20	490.5 44 25	
221+00		488.4 65 25	489.2 57 13	489.9 50	489.4 55 20	490.7 42 25		
+50		487.6 73 25	489.3 56 13	489.6 53	489.3 56 19	491.5 34 25		
222+00		487.9 70 25	489.5 54 13	488.8 61 12	489.3 56	489.1 58 19	490.2 47 20	491.4 35 25

Plotted
G.W.C.
4-9-35

Contd. From Page 14.

April-4-1935.

15.

494.94

L.

Φ.

R.

222+50

486.1 ✓ 8 ⁸ 25	488.7 ✓ 6 ³ 13	488.2 ✓ 6 ⁷ 11	488.7 ✓ 6 ³
---------------------------------	---------------------------------	---------------------------------	---------------------------

488.8 ✓ 6 ¹ 19	490.2 ✓ 7 ⁷ 20	490.9 ✓ 4 ⁰ 25
---------------------------------	---------------------------------	---------------------------------

223+00

485.8 ✓ 7 ¹ 25	487.2 ✓ 7 ⁷ 13	488.0 ✓ 6 ⁹ 11	488.3 ✓ 6 ⁵
---------------------------------	---------------------------------	---------------------------------	---------------------------

488.5 ✓ 6 ² 19	490.0 ✓ 4 ⁹ 20	491.1 ✓ 3 ⁸ 25
---------------------------------	---------------------------------	---------------------------------

+50

485.6 ✓ 7 ³ 25	486.9 ✓ 8 ⁰ 13	487.8 ✓ 7 ¹ 10	488.3 ✓ 6 ⁵
---------------------------------	---------------------------------	---------------------------------	---------------------------

488.5 ✓ 6 ² 20	490.6 ✓ 4 ³ 21	491.7 ✓ 3 ³ 25
---------------------------------	---------------------------------	---------------------------------

B.M. #18

3.49 491.45 = check

on B.M. #18 Rec. Elev. 491.47

224+00

485.9 ✓ 9 ⁰ 25	487.1 ✓ 7 ⁸ 13	488.1 ✓ 6 ⁸ 10	488.8 ✓ 6 ¹
---------------------------------	---------------------------------	---------------------------------	---------------------------

488.9 ✓ 6 ⁰ 21	490.8 ✓ 7 ⁴ 23	492.1 ✓ 2 ⁸ 25
---------------------------------	---------------------------------	---------------------------------

T.P.

3.49 491.45

6.47 497.92

+50

487.3 ✓ 10 ⁶ 25	487.6 ✓ 10 ³ 13	488.8 ✓ 9 ¹
----------------------------------	----------------------------------	---------------------------

489.4 ✓ 8 ⁵ 22	490.4 ✓ 7 ⁵ 25
---------------------------------	---------------------------------

Plotted
6.W.G.
4-9-35

	49792	L.	£.	R.
225+00		✓ A86.9 11 ⁰ 25	✓ A88.7 9 ⁷ 13	✓ A89.1 8 ⁸
+50		✓ A87.5 10 ⁴ 25	✓ A89.5 8 ⁴ 15	✓ A89.6 8 ³ 13
226+00		✓ A87.0 10 ⁹ 25	✓ A87.1 10 ⁸ 18	✓ A89.7 8 ² 13
+50		✓ A87.4 10 ⁷ 25	✓ A87.4 10 ⁵ 18	✓ A90.2 7 ⁷ 10
227+00		✓ A87.1 10 ⁸ 25	✓ A89.1 8 ⁸ 13	✓ A90.5 7 ⁴ 10
+50		✓ A87.7 10 ⁷ 25	✓ A89.5 8 ⁴ 13	✓ A91.7 6 ² 13
228+00		✓ A87.4 10 ⁵ 25	✓ A88.9 9 ⁰ 13	✓ A91.3 6 ⁶ 19
+50		✓ A88.3 9 ² 25	✓ A89.1 8 ⁸ 13	✓ A93.2 5 ¹ outside 6 Edge Rd. 4 ⁷
		✓ A87.4 10 ⁵ 25	✓ A88.9 9 ⁰ 13	✓ A93.2 5 ¹ inside + 3 ² 19 Edge Rd. 26
		✓ A88.3 9 ² 25	✓ A89.1 8 ⁸ 13	✓ A93.6 4 ³ inside + 2 ⁰ 22 Edge Rd. 23
		✓ A87.4 10 ⁵ 25	✓ A88.9 9 ⁰ 13	✓ A94.0 3 ⁷ outside 3 Edge Rd. 3 ⁹
		✓ A88.3 9 ² 25	✓ A89.1 8 ⁸ 13	✓ A94.6 3 ³ out: Edge Rd.
		✓ A87.4 10 ⁵ 25	✓ A88.9 9 ⁰ 13	✓ A94.8 3 ¹ inside 29 Edge Rd.

Plotted
S.W.C.
A-9-35

Cont'd. From Page 16.

497.92 ✓

229+00

488.6 ✓

7³

25

489.4 ✓

8⁵

13

491.3 ✓

6⁶

488.0 ✓

9⁷

25

488.4 ✓

9⁵

13

491.5 ✓

6⁷

+50

T.P.

0.05 497.87 ✓

10.18 508.05

230+00

487.9 ✓

20¹

25

488.5 ✓

19⁵

13

488.9 ✓

19¹

8

493.2 ✓

14⁸

+50

489.2 ✓

18⁸

25

489.9 ✓

18¹

11

495.9 ✓

12¹

231+00

489.4 ✓

18⁶

25

492.1 ✓

15⁹

13

494.0 ✓

14⁰

7

500.2 ✓

7⁸

+50

489.3 ✓

18⁷

35

489.9 ✓

18¹

25

495.0 ✓

13⁰

13

503.4 ✓

4⁶ outside

3 Edge Rd.

503.4 ✓

4⁶

April-4-1935

17.

496.7 ✓

17¹ outside

7 Edge Rd.

496.7 ✓

17¹ inside

35 Edge Rd.

497.8 ✓

0²

9

497.7 ✓

0²

36

499.6 ✓

8⁴

8 outside

8 Edge Rd.

499.7 ✓

8⁸

8 inside

35 Edge Rd.

501.2 ✓

6⁸

7

501.0 ✓

7⁰

33

502.3 ✓

5⁷

3

502.0 ✓

6⁰

31

502.6 ✓

5⁴

5 inside

26 Edge Rd.

Plotted
G.W.G.
4-9-35

Cont'd. From Page 17.

April-4-1935

18

	508.05 ✓	L.	£.	
232+00	A88.9 ✓ 19 [°] 50	A90.0 ✓ 18 [°] 35	A93.8 ✓ 14 [°] 22	500.3 ✓ 7 [°] 13
			503.5 ✓ 4 [°] outside 9 Edge Rd.	503.6 ✓ 4 [°]
+50	A89.7 ✓ 18 [°] 50	A90.5 ✓ 17 [°] 40	A93.5 ✓ 14 [°] 28	503.8 ✓ 4 [°] " 15
			503.8 ✓ 4 [°] " 13	503.7 ✓ 4 [°] " 4 [°]
233+00			503.7 ✓ 4 [°] " 23	503.7 ✓ 4 [°] " 13
			504.5 ✓ 3 [°] " 27	503.4 ✓ 4 [°] " 4 [°]
+50			504.5 ✓ 3 [°] " 27	504.4 ✓ 3 [°] " 13
			505.8 ✓ 2 [°] " 28	504.4 ✓ 2 [°] " 13
234+00			505.8 ✓ 2 [°] " 28	504.4 ✓ 3 [°] " 17 side Edge Rd.
T.P.			1.99	506.06 ✓
	1.05	507.11 ✓		
+50	A91.1 ✓ 16 [°] 45	506.3 ✓ 0 [°] outside 21 Edge Rd.	505.7 ✓ 1 [°] 13	504.8 ✓ 2 [°]

	R.		
503.4 ✓	515.9 ✓		
4 [°] inside 19 Edge Rd.	+7 [°] Top 25 Bank		
503.0 ✓	514.0 ✓	517.0 ✓	
5 [°] " 12	+6 [°] " 17	+9 [°] " 26	
503.0 ✓	514.0 ✓	518.0 ✓	
5 [°] " 7	+6 [°] " 12	+10 [°] " 24	
503.6 ✓	515.6 ✓	520.6 ✓	
4 [°] " 2	+7 [°] " 6	+12 [°] " 21	
516.9 ✓	521.9 ✓		
+8 [°] Top 5 Bank	+13 [°] " 20		
504.4 ✓	517.4 ✓	521.4 ✓	
27 inside 8 Edge Rd.	+10 [°] " 13	+14 [°] " 25	

Plotted
G.W.C.
A-9-35

Cont'd. From Page 18.

April 4-1935.

19.

234+95.24
234+88.32 Equation

507.11

L.

♀.

R.

235+00
491.5
15⁶
40

491.6
15⁵
20

494.7
12⁴
13

504.2
2⁹ - outside
Edge Rd.

503.5
3⁶
32 inside Edge
Rd.

+30

491.9
15²
30

492.4
14⁷
13

493.1
14⁰

501.9
5² - outside
Edge Rd.
15

502.6
4⁵ - inside
Edge Rd.
42

+50

492.3
14⁸
30

492.3
14⁸
13

492.8
14³

493.1
14⁰
10

500.9
6² - outside
Edge Rd.
24

501.2
5⁹ - inside
Edge Rd.
50

236+00

492.5
14⁶
30

492.8
14³
13

493.4
13⁷

494.5
12⁶
33

+50

492.7
14⁴
30

493.1
14⁰
13

493.2
13⁹

494.5
12⁶
25

T.P.

9.39 497.72

9.68 507.40

237+00

493.2
14²
30

493.5
13⁹
13

493.6
13⁸

493.9
13⁵
30

+50

493.1
14³
30

493.3
14¹
13

493.5
13²

494.0
13⁴
30

497.0
10⁴ - ♀ Traveled
73 Rd.

Plotted
G.M.C.
A-9-35

507.40 ✓ L, £.

238+00

493.3 ✓ 493.6 ✓ 493.6 ✓
14¹ 13⁸ 13⁸
30 13

+40

493.6 ✓ 493.8 ✓ 494.7 ✓
13⁸ 13⁵ 12⁷
30 13

+66

493.4 ✓ 494.0 ✓ 494.9 ✓
14⁰ 13⁴ 12⁵
25 13

239+00

493.6 ✓ 494.8 ✓ 502.2 ✓
13⁸ 12⁶ 5².outside
35 13 Edge Rd.

+50

494.4 ✓ 495.3 ✓ 498.2 ✓ 501.7 ✓ 502.2 ✓
13⁰ 12¹ 9³ 5⁷.outside 5²
40 18 13 7 Edge Rd.

Cont'd. on page 35, this book

240+00

496.7 ✓ 500.4 ✓
12¹ 10⁷ 7³ " 7⁰
30 15 10

+50

499.3 ✓ 499.6 ✓
12⁴ 11¹ 8¹ " 7⁸
30 18 8

241+00

497.0 ✓ 499.4 ✓
10⁷ 10⁴ 8⁷ " 8⁰
30 13 8

R.

494.7 ✓ 497.5 ✓
12⁷ 9⁷ outside
29 35 Edge Rd.

495.6 ✓ 499.9 ✓ 500.2 ✓
11⁸ 7⁵ " 7².inside
7 20 53 Edge Rd.

501.2 ✓ 501.7 ✓
6² " 5⁷ "
10 46

502.5 ✓ 4².inside
37 Edge Rd.

502.4 ✓ 5⁰ "
25

6⁵ " 5¹
23 30

7² " 5³
24 30

6⁹ "
25

Plotted to here.
G.W.G.
A-9-35

See page 35.

Cont'd. From Page 20.

April-4-1935.

21.

507.40 ✓ L.

£...

R.

241+50

9¹
25

498.7 ✓
8²
13

499.3 ✓
8¹-outside
Edge Rd.

6⁶ = inside
25 Edge Rd.

242+00

9⁰
25

498.6 ✓
8⁸
13

499.1 ✓
8³ "

6⁷ "
25

+50

9⁰
25

498.7 ✓
8⁷
13

498.8 ✓
8⁶ "

6⁶ "
25

T.P.

7.33 500.07 ✓

7.43 507.50 ✓

243+00

10⁴
35

10⁵
26

7¹-outside
20 Edge Rd. 7¹
13

500.4 ✓ 500.8 ✓

6⁷

6⁷
8

+3⁵
21

+8⁵ ±
36

+27

6⁴ "
28

501.3 ✓
6²
13

500.8 ✓
6⁷-inside
Edge Rd.

0⁷
4

+7⁸
15

+12⁸ ±
30

+38

6²-outside
30 Edge Rd.

501.3 ✓
6²
13

6⁶-inside
3 Edge Rd.

507.1 ✓
0⁴

+0⁷
5

+8²
12

+13² ±
27

	507.50	W.		E.		R.			
243+50	6 ⁰ outside 31 Edge Rd.	6 ¹ 13	6 ⁵ inside 7 Edge Rd.	0 ⁴ 2	501.3 0 ²	+1 ⁰ 5	+9 ⁵ 11	+14 ⁵ ± 26	
244+00	6 ⁰ "	6 ⁸ 13	7 ⁰ "	10 ⁰ 5	501.6 +0 ¹	+7 ⁵ 4	+14 ⁵ ± 26		
+50	6 ⁰ "	6 ⁵ 13	6 ⁷ inside 7 Edge Rd.	+2 [±]	509.9 +2 [±]	+3 [±] 4	+9 ⁰ 8	+16 ⁰ ± 29	
245+00	5 ¹ outside 28 Edge Rd.	5 ³ 13	5 ³ inside Edge Rd.	3 ⁴ 5	502.4 5 ³ inside Edge Rd.	3 ⁴ 5	+10 ³ ± 17	+15 ³ ± 32	
+50	11 ³ 30	10 ⁹ 26	4 ⁸ outside 18 Edge Rd.	4 ⁸ 13	502.7 4 ⁸	4 ⁹ inside 8 Edge Rd.	+2 ⁵ 19	+13 ⁰ ± 26	+18 ⁰ ± 41
246+00	11 ⁴ 25	10 ⁵ 14	5 ⁰ outside 7 Edge Rd.	4 ⁷	502.8 4 ⁷	4 ³ " 21			
+36	11 ⁵ 30	10 ⁴ 13	9 ⁸ 8	5 ² out- Edge Rd.	502.3 5 ² out- Edge Rd.	4 ³ " 31			
247+00	11 ⁵ 25	11 ⁵ 13	10 ⁸ 13	10 ⁸	496.7 10 ⁸	4 ² outside 10 Edge Rd.	3 ⁴ inside 40 Edge Rd.		

	507.50	L.	£.	R.			
247+50		11 ⁶ 25	496.0 11 ⁵ 13	496.9 10 ⁶	9 ² 6	4 ⁸ = outside 13 Edge Rd.	3 ¹ = inside 35 Edge Rd.
248+00		11 ⁶ 25	496.5 11 ⁶ 13	499.5 8 ⁰	4 ⁰ = outside 6 Edge Rd.	3 ² = inside 30 Edge Rd.	
+15		10 ⁹ 25	497.2 10 ³ 13	503.6 10 ⁰ 8	3 ² = outside Edge Rd.	3 ² = inside 30 Edge Rd.	
+50		10 ⁷ 25	502.2 5 ³ 13	504.9 2 ⁹ = outside 8 Edge Rd.	2 ⁹ 20	+9 ⁶ ± 26	+13 ⁶ ± 42
T.P.		2.90	504.60				
	3.11	507.71					
B.M.		6.61	501.10 = check on				B.M. #16 - Rec. Elev. 501.09.
249+00	11 ⁰ 35	10 ¹ 26	505.2 2 ⁷ = outside 17 Edge Rd.	505.5 2 ⁵ 13	2 ⁷ = inside 11 Edge Rd.	+12 ³ ± 17	+16 ³ ± 33
+50	11 ⁰ 35	10 ¹ 26	504.3 3 ⁷ " 20	504.3 3 ⁴ 13	4 ⁰ " 8	+8 ⁰ ± 11	+12 ⁰ ± 27

Cont'd. From Page 23.

April-4-1935

24.

	507.71			L.	£.	R.		
250+00	10 [±] 40	10 [±] 30	4 [±] -outside 21 Edge Rd.	503.6 4 [±] 13	503.4 4 [±]	4 [±] -inside 6 Edge Rd.	+6 [±] 9	+10 [±] 25
+50	10 [±] 35	9 [±] 26	5 [±] "	502.3 5 [±] 13	502.1 5 [±]	6 [±] "	0 [±] 9	+6 [±] 25
251+00	10 [±] 30	9 [±] 22	7 [±] "	500.4 7 [±] 13	500.9 6 [±]	6 [±] "	3 [±] 20	+1 [±] 30
+50	9 [±] 30	9 [±] 21	7 [±] "	500.3 7 [±] 13	500.6 7 [±]	7 [±] "	3 [±] 19	+1 [±] 30
252+00	9 [±] 25	9 [±] 18	6 [±] "	501.0 6 [±] 13	501.4 6 [±]	6 [±] "	7 [±] 25	
+50	9 [±] 30	9 [±] 26	5 [±] "	502.5 5 [±] 13	503.0 4 [±]	5 [±] "	1 [±] 19	0 [±] 25
253+00	9 [±] 30	9 [±] 22	3 [±] -outside 13 Edge Rd.	504.5 3 [±]	504.5 3 [±]	3 [±] "	+4 [±] 23	+4 [±] 25
T.P.				2.25	505.46			

Cont'd. From Page 24.

April-5-1935.
Hill-Simpson
Saper-Remmen.

25

		L.	Φ.	R.
T.P.	2.37	507.83	505.46	
253+50	9 [±] 25	498.8 [✓] 9 [°] 13	7 ⁶ 5	505.0 [✓] 2 ⁸ = outside Edge Rd.
+65	9 [±] 25	498.6 [✓] 9 [°] 13	9 [°] 8	500.0 [✓] 7 [±] 2 ⁸ = outside Edge Rd.
254+00		8 ⁸ 25	498.8 [✓] 9 [°] 13	499.1 [✓] 8 ⁷ 2 ⁷ = outside Edge Rd.
+50		8 ⁵ 25	499.5 [✓] 8 [±] 13	499.6 [✓] 8 [±] 6 [±] 25
255+00		8 ³ 25	499.6 [✓] 8 [±] 13	499.8 [✓] 8 [±] 7 [±] 18
+50		8 [±] 25	499.8 [✓] 8 [°] 13	500.3 [✓] 7 [±] 7 [±] 15
256+00		6 ⁹ 25	500.9 [✓] 6 ⁹ 13	500.8 [✓] 7 [°] 6 [±] 30

Cont'd. From Page 25.

April-5-1935.

26

	507.83 ✓	L.	4	R.
256+50		Level	500.6 ✓ 7 ²	Level
257+00		"	500.6 ✓ 7 ²	"
+50		"	500.5 ✓ 7 ²	"
258+00		"	500.6 ✓ 7 ²	"
+50		"	500.2 ✓ 7 ⁴	"
T.P.		7.28	500.55 ✓	
	5.93	506.48 ✓		
259+00		Level	500.8 ✓ 5 ⁷	Level
+50		"	500.8 ✓ 5 ⁷	"
260+00		"	501.0 ✓ 5 ⁵	"
+50		"	501.2 ✓ 5 ³	"
261+00		"	501.4 ✓ 5 ¹	"
+50		"	501.5 ✓ 5 ⁰	"
262+00		"	501.5 ✓ 5 ²	"
+50		"	501.8 ✓ 4 ⁷	"
263+00		"	501.5 ✓ 5 ⁰	"
+50		502.1 ✓ 4 ⁴ 25	502.1 ✓ 4 ⁴ 13	501.4 ✓ 5 ¹ 25

Cultivated Grain Field.

506.48

L.

£.

R.

264+00

502.3

4²

25

502.1

4⁴

13

502.3

4²

502.1

4⁴

25

+50

502.6

3¹

25

502.7

3⁸

13

502.8

2¹

502.1

2⁴

25

T.P.

3.56

502.92

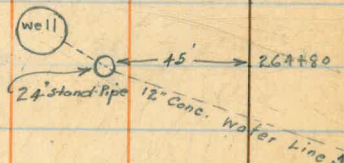
3.73

506.65

264+80

6.4 500 \checkmark Flow Line

in Bottom of Stand-Pipe
45' Left of £.



264+00

265+00

496.3

10³

25

497.0

9⁵

13

498.3

8³

502.1

4⁵

13

501.9

4⁷

33

outside
Edge Rd.

+40

501.2

5⁴

25

501.6

5²

13

501.9

4¹

501.6

5²

10

outside
Edge Rd.

500.7

5¹

34

inside
Edge Rd.

+65

501.1

5⁵

25

501.5

5¹

13

501.4

5²

outside
Edge Rd.

499.9

6⁷

28

inside
Edge Rd.

	506.65 ✓	L.	Φ.	R.
266+00	5 ² 25	501.6 ✓ 5 ⁰ 13	5 ¹ -outside 8 Edge Rd.	501.2 ✓ 5 ⁴
				6 ⁵ inside 19 Edge Rd.
				5 ³ 21
				5 ³ 24
+50		5 ² 25	501.4 ✓ 5 ² "	501.3 ✓ 5 ³
				5 ² "
				5 ³
				5 ⁶ 20
267+00	5 ² 20	5 ² 16	501.4 ✓ 5 ² 13	501.3 ✓ 5 ³
				5 ⁴ "
				4 ⁶ 16
				5 ³ 20
+50	5 ⁰ 20	4 ⁷ 17	501.4 ✓ 5 ² 13	501.5 ✓ 5 ¹
				5 ³
				6 ⁰ 14
				4 ⁶ 15
				5 ³ 20
268+00		4 ⁹ 20	501.4 ✓ 5 ⁴ 13	501.5 ✓ 5 ¹
				5 ⁵
				4 ⁶ 16
				5 ¹ 20
+50		5 ⁷ 20	500.9 ✓ 5 ⁷ 13	501.3 ✓ 5 ³
				5 ²
				4 ⁵ 15
				4 ⁸ 20
T.P.		4.27	502.38 ✓	
	5.95	508.33 ✓		

	508.33 ✓	L.		£.		R.
269+00		6 ⁷ 25	501.6 ✓ 6 ⁷ 13	501.6 ✓ 6 ⁷	6 ⁷ 14	6 ⁷ 20
+50		5 ⁹ 25	502.1 ✓ 6 ² 13	501.9 ✓ 6 ⁷	6 ⁸ 13	6 ³ 20
270+00		5 ⁹ 25	502.3 ✓ 6 ⁰ 13	502.2 ✓ 6 ¹	6 ⁵ 12	5 ⁹ 20
+50		5 ⁷ 25	502.4 ✓ 5 ⁷ 13	502.5 ✓ 5 ⁸	6 ¹ 12	5 ⁶ 20
271+00		5 ¹ 25	502.9 ✓ 5 ⁴ 13	502.9 ✓ 5 ⁴	5 ⁹ 11	5 ¹ 20
+50	4 ⁹ 25	4 ² 15	503.1 ✓ 5 ² 13	503.2 ✓ 5 ¹	5 ⁵ 12	4 ⁵ 20
272+00	4 ⁸ 25	504.5 ✓ 3 ⁸ 13	4 ⁶ 12	503.5 ✓ 4 ²	5 ⁴ 14	4 ⁴ 23
+50	4 ⁹ 25	503.6 ✓ 4 ⁷ 13	4 ⁵ 7	503.8 ✓ 4 ⁵	5 ⁰ 20	4 ³ 28

	508.33 ✓	L.		R.	
273+00	4 ³ 25	503.1 ✓ 4 ⁶ 13	503.6 ✓ 4 ⁷ - outside Edge Rd.	4 ⁹ = inside 26 Edge Rd.	3 ² 34
+50	4 ¹ 25	50A.0 ✓ 4 ³ 13	50A.2 ✓ 4 ¹	4 ⁵ = outside 4 Edge Rd.	4 ² inside 4 ¹ 29 Edge Rd. 38
274+00	3 ⁹ 25	50A.2 ✓ 4 ¹ 13	50A.3 ✓ 4 ⁰	4 ⁴ "	4 ⁷ " 4 ⁰ 30 39
+50	4 ⁰ 25	50A.4 ✓ 3 ⁹ 13	505.0 ✓ 3 ³	4 ¹ "	4 ⁵ " 3 ⁷ 30 36
275+00	4 ⁴ 25	50A.7 ✓ 3 ⁶ 13	50A.4 ✓ 3 ⁹ - out- Edge Rd.	4 ⁴ = inside 27 Edge Rd.	3 ⁵ 32
T.P.		1.52	506.81 ✓		
	3.39	510.20 ✓			
+50	6 ⁷ 25	50A.8 ✓ 5 ⁴ 13	50A.5 ✓ 5 ⁶ outside 3 Edge Rd.	6 ⁶ = inside 22 Edge Rd.	5 ² 27

Cont'd. From Page 30

April-5-1935.

31

	510.20	L.	£.	R.
2.76+00	8° 35	8° 25	5 ¹ 13	4 ⁴ 8
			5 ⁶ -outside 6 Edge Rd.	5 ⁶
+50	7 ⁸ 35	7 ⁸ 25	4 ³ 13	4 ¹ 9
			5 ³ "	5 ³
2.77+00			6 ⁴ 25	4 ⁴ 13
			3 ² 10	5 ⁰ "
+50	5 ⁵ 25	4 ² 13	3 ² 10	5 ⁰ "
				5 ²
2.78+00	6 ⁸ 25	4 ⁴ 13	3 ² 10	5 ⁰ "
				5 ⁰
+50	6 ² 25	5 ⁶ 13	3 ² 9	4 ¹ "
				4 ¹
2.79+00	12 ² 30	7 ⁶ 25	6 ³ 13	3 ² 8
				4 ² "
+50	7 ⁹ 25	6 ⁵ 13	4 ¹ 7	4 ⁶ "
				4 ⁶
				5 ³ "
				18
				4 ²
				25
				5 ¹ "
				18
				5 ⁰
				25

6² = inside
19 Edge Rd. 5²
25

5⁹ " 4⁹ 5⁰
17 " 19 26.

5⁶ " 4⁹
16 " 26

5⁶ " 4⁷
16 " 25

5⁵ " 4⁵ 4⁴
16 " 17 23

5⁴ " 4²
18 " 24

5³ " 4²
18 " 25

5¹ " 3⁹
18 " 25

see page 47

Cont'd. from Page 47, this book.

Plotted
G.M.C.
4-16-35

	510.20	L.		£	
280+00	✓ A97.9 12 ^{3±} 35	✓ 504.9 7 ³ 25	✓ 504.2 6 ⁰ 13	✓ 505.6 4 ⁶ 10	✓ 505.9 4 ³
+50		✓ 504.3 7 ⁴ 30	✓ 504.1 6 ¹ 13	✓ 505.7 4 ⁵ 9	✓ 506.0 4 ³
T.P.			4.05	506.15	
281+00	6.79	✓ 512.94	✓ 507.1 5 ⁸ 6	✓ 506.0 6 ² 4	✓ 506.0 5 ³ 6 ²
+50		✓ 503.6 9 ³ 25	✓ 505.9 503.7 7 ⁰ 13	✓ 506.3 503.6 6 ⁶ 4	✓ 506.3 503.6 6 ⁶
282+00		✓ 503.6 9 ³ 25	✓ 505.5 503.8 7 ⁴ 13	✓ 506.4 503.7 6 ⁵	✓ 506.4 503.7 6 ⁵
+50		✓ 504.0 8 ⁹ 25	✓ 506.0 503.5 6 ⁹ 13	✓ 506.7 504.0 6 ³	✓ 506.7 504.0 6 ³
283+00		✓ 504.6 8 ³ 25	✓ 506.3 503.6 6 ⁶ 13	✓ 507.0 504.3 5 ⁹	✓ 507.0 504.3 5 ⁹

	R.
✓ 505.6 4 ⁶ 18	✓ 506.8 3 ⁴ 25
✓ 505.8 4 ⁴ 18	✓ 506.6 3 ⁶ 25
✓ 505.9 7 ⁰ 18	✓ 507.0 5 ⁹ 25
✓ 506.1 6 ⁸ 21	✓ 507.0 5 ⁹ 25
✓ 506.5 6 ⁴ 20	✓ 506.5 6 ⁴ 25
✓ 506.4 6 ⁵ 20	✓ A06.7 6 ² 25
✓ 506.5 6 ⁴ 19	✓ 507.5 5 ⁴ 25

Plotted
G.W.C.
4-16-35

512.94 ✓

L.

L.

R.

283+50

✓
505.4 ✓
7⁵ ✓
25 ✓
506.8 ✓
6¹ ✓
13 ✓
507.2 ✓
5⁷ ✓

✓
506.8 ✓
6¹ ✓
17 ✓
508.0 ✓
4⁹ ✓
23 ✓
Fence

284+00

✓
506.7 ✓
6⁷ ✓
25 ✓
507.1 ✓
5⁸ ✓
13 ✓
507.7 ✓
5² ✓

✓
507.1 ✓
5⁸ ✓
17 ✓
508.1 ✓
4⁸ ✓
23 ✓

+50

✓
506.8 ✓
6¹ ✓
25 ✓
508.0 ✓
4² ✓
13 ✓
508.1 ✓
4⁸ ✓

✓
507.5 ✓
5⁴ ✓
18 ✓
508.3 ✓
4⁶ ✓
23 ✓

285+00

✓
508.5 ✓
4⁴ ✓
25 ✓
508.5 ✓
4⁴ ✓
13 ✓
508.9 ✓
4⁰ ✓
9 ✓
507.8 ✓
5¹ ✓
7 ✓
508.0 ✓
4⁹ ✓

✓
507.7 ✓
5² ✓
20 ✓
508.2 ✓
4⁵ ✓
24 ✓

+50

✓
508.7 ✓
4² ✓
25 ✓
508.9 ✓
4⁰ ✓
13 ✓
509.1 ✓
3⁸ ✓
9 ✓
508.1 ✓
4⁸ ✓
7 ✓
508.7 ✓
4⁷ ✓

✓
507.7 ✓
5² ✓
20 ✓
508.4 ✓
4⁵ ✓
26 ✓

286+00

✓
508.8 ✓
4¹ ✓
25 ✓
508.6 ✓
4³ ✓
13 ✓
509.0 ✓
3⁹ ✓
10 ✓
508.3 ✓
4⁶ ✓
9 ✓
508.3 ✓
4⁶ ✓

✓
507.8 ✓
5¹ ✓
21 ✓
508.5 ✓
4⁴ ✓
26 ✓

+50

✓
508.9 ✓
4⁰ ✓
25 ✓
508.9 ✓
4⁰ ✓
13 ✓
509.7 ✓
3⁷ ✓
11 ✓
508.4 ✓
4⁵ ✓
10 ✓
508.5 ✓
4⁴ ✓

✓
508.10 ✓
4⁹ ✓
22 ✓
508.6 ✓
4³ ✓
26 ✓

287+00

✓
509.0 ✓
3⁹ ✓
25 ✓
508.9 ✓
4⁰ ✓
13 ✓
508.3 ✓
4⁶ ✓
10 ✓
508.5 ✓
4⁴ ✓

✓
507.9 ✓
5⁰ ✓
21 ✓
508.6 ✓
4³ ✓
26 ✓

Plotted
G.W.G.
4-16-35

Cont'd. From Page 33.

April-5-1935

34.

	512.94	L.	£.	R.
287+50	509.1 3 ⁸ 25	509.3 3 ⁶ 13	508.6 4 ³ 11	508.8 4 ¹
288+00	509.3 3 ⁶ 25	509.1 3 ² 13	508.9 4 ⁰ 12	509.2 3 ⁷
+50	509.7 3 ² 25	510.0 2 ⁹ 13	509.7 3 ⁷ 11	509.5 3 ⁴

508.7 4 ⁷ 19	509.1 3 ⁸ 25	Fence.
508.5 4 ⁷ 19	509.3 3 ⁶ 24	
508.7 4 ² 19	509.6 3 ³ 24	

T.P.

3.94 509.00

5.54 514.54

B.M.

0.14 514.40 = check

on B.M. 12 Rec. Elev. 514.43

Plotted
S.W.G.
A-16-35

Cont'd. in Book #317-Pg 56
~~#308-Pg. 47.~~

Profile And Cross-sections of Co. Road Survey
#606 - Alternate Line from sta. 239+66.92 To

Sta. 279+32.19 =

279+08.09 =

Contd. from page 20, this book.

L.

£.

R.

B.M.

501.09 B.M. #16

7.92 509.01

T.P.

6.36 502.65

1.63 504.28

239+66.92	495.0 9 ³ 25	495.1 9 ² 18	498.4 5 ² 13	501.3 3 ⁰ W. Edge 8 Rd.	501.6 2 ⁷	501.8 2 ⁵ 19	E. Edge Rd.	502.7 1 ⁶ 25
240+00	495.7 8 ⁶ 25	495.4 8 ² 20	498.4 5 ² 13	500.0 4 ³ "	500.4 3 ²	500.8 3 ⁵ 21	"	501.9 2 ⁴ 25
+50	495.8 8 ⁵ 25	496.0 8 ² 21	498.4 5 ² 13	499.2 5 ¹ "	499.7 4 ⁶	500.2 4 ¹ 21	"	501.5 2 ⁸ 25
241+00	496.4 7 ⁹ 25	496.9 7 ⁴ 16	498.2 6 ¹ 13	498.6 5 ² "	499.6 4 ⁷	500.3 4 ⁰ 22	"	501.3 3 ⁰ 25
+50	498.5 5 ⁸ 25	498.7 5 ⁶ 13	499.2 5 ¹ "	499.5 4 ⁸	499.5 3 ⁸ 20	500.5 3 ⁸ 20	"	501.5 2 ⁸ 25

Computed & checked
S.W.G. 4-16-35

Plotted
S.W.G.
4-16-35

April-15-1935.
Hill - Simpson
Soper - Remmen.

35.

	504.28	L.	£.	R.	
242+00	✓ 198.4 5 ² 25	✓ 199.1 5 ² 13	✓ 199.2 5 ¹ W. Edge Rd.	✓ 500.7 3 ⁶ 20 E. Edge Rd.	✓ 501.3 3 ⁰ 25
+50	✓ 198.6 5 ² 25	✓ 199.1 5 ² 13	✓ 199.1 5 ² W. Edge Rd.	✓ 199.5 4 ⁸	✓ 500.7 3 ⁶ 16
243+00	✓ 500.6 3 ⁷ W. Edge Rd.	✓ 500.6 3 ⁷ 13	✓ 500.7 3 ⁶ E. Edge Rd.	✓ 500.8 3 ⁵ 3	✓ 510.0 +5 ² 15
T.P.		✓ 1.63	✓ 502.65		
	✓ 10.94	✓ 513.59			
T.P.		✓ 2.90	✓ 510.69		
	✓ 11.50	✓ 522.19			
+50	✓ 501.5 20 ⁷ W. Edge Rd.	✓ 501.1 21 ¹ E. Edge Rd.	✓ 507.0 15 ² 11	✓ 508.6 13 ⁶ 3	✓ 513.6 8 ⁶
244+00	✓ 501.5 20 ⁷ W. Edge Rd.	✓ 500.5 21 ⁷ E. Edge Rd.	✓ 506.2 16 ⁰ 14	✓ 507.8 14 ⁴ 9	✓ 515.1 7 ¹ 4
			✓ 516.9 5 ³	✓ 517.0 5 ² 3	✓ 521.8 +2 ⁶ 30
			✓ 518.3 3 ⁹ 6	✓ 528.0 +5 ⁸ 30	

Plotted
G.W.G.
4-16-35

	522.19	L.	Q.	R.			
244 + 50	501.6 20 ⁶ W. Edge 44 Rd.	500.6 21 ⁶ E. Edge 18 Rd.	510.0 12 ² 11	516.6 11 ⁷ 7	518.3 5 ⁶ 4	518.3 3 ⁷	530.5 +8 ³ 30
+90	502.5 19 ⁷ W. Edge 42 Rd.	501.6 20 ⁶ E. Edge 16 Rd.	506.8 15 ⁴ 12	512.1 10 ¹ 2	519.7 3 ⁹	532.8 +10 ⁶ 30	
245 + 10	502.1 20 ¹ W. Edge 40 Rd.	502.1 20 ¹ E. Edge 13 Rd.	503.5 18 ⁷ 12	502.0 18 ² 6	507.3 14 ⁹	521.6 0 ⁶ 5	533.0 +10 ⁸ 30
T.P.		11.50	510.69				
	2.90	513.59					
T.P.		10.94	502.65				
	5.44	508.09					
+50		507.7 5 ⁴ W. Edge 35 Rd.	507.6 5 ⁵ E. Edge 7 Rd.	507.6 0 ⁵	520.3 +12 ² 10	528.1 +20 ³ 30	
246 + 00		502.5 5 ⁶ W. Edge 25 Rd.	503.0 5 ¹ 13	503.0 5 ¹ E. Edge Rd.	512.7 +4 ¹ 8	516.1 +8 ⁰ 14	523.5 +15 ⁴ 30

Plotted
G.M.C.
4-16-35

	508.09	L.	♀.	R.				
246+50	✓ 11 ⁴ 30	✓ 197.4 10 ⁷ 25	✓ 502.4 5 ⁷ W. Edge 17 Rd.	✓ 502.5 5 ⁶ 13	✓ 503.3 4 ⁸ & Rd.	✓ 503.1 5 ⁰ E. Edge 14 Rd.	✓ 514.3 +6 ² 30	✓
247+00		✓ 196.1 12 ⁰ 30	✓ 196.9 11 ² 20	✓ 503.3 4 ⁸ W. Edge 11 Rd.	✓ 503.6 4 ⁵	✓ 504.1 4 ⁰ 19	✓ 511.6 +3 ⁵ 23	✓ 519.6 +11 ⁵ ± 33
+50	✓ 11 ⁷ 30	✓ 196.4 11 ⁷ 30	✓ 198.6 9 ⁶ 13	✓ 502.7 5 ⁴ " 10	✓ 503.7 4 ⁴	✓ 504.0 4 ¹ " 20	✓ 522.2 +14 ¹ ± 30	
248+00		✓ 10 ⁷ 30	✓ 197.4 10 ⁷ 30	✓ 503.3 4 ⁸ " 19	✓ 504.2 3 ⁹	✓ 504.2 3 ⁹ " 10	✓ 512.4 +4 ³ 25	✓ 517.4 +9 ³ ± 35
+34		✓ 3 ⁸ W. Edge 32 Rd.	✓ 504.3 3 ⁸ W. Edge 32 Rd.	✓ 504.7 3 ⁴ 13	✓ 504.6 3 ⁵ E. Edge Rd.	✓ 510.9 +2 ⁸ 7	✓ 519.0 +10 ⁹ 25	✓ 521.0 +15 ⁹ ± 34
T.P.		0.14	✓ 507.95					
	12.57	✓ 520.52						
+50		✓ 15 ⁶ W. Edge 34 Rd.	✓ 504.4 16 ¹ E. Edge 5 Rd.	✓ 514.5 6 ⁰	✓ 527.6 +7 ¹ 30			
T.P.		1.35	✓ 519.17					

Plotted
G.W.G.
4-16-35

		L.	¢	R.
	9.64	528.81 ✓	519.17	
248+70	505.7 ✓ 23 ⁶ = W. Edge Rd. 40	504.9 ✓ 23 ⁷ = E. Edge Rd. 11	521.7 ✓ 7 ⁶ 6	523.8 ✓ 5 ⁶ 30
249+00	505.0 ✓ 23 ⁸ " 50	504.6 ✓ 24 ² " 18	522.1 ✓ 6 ⁷ 11	525.4 ✓ 3 ⁴ 30
+50	504.0 ✓ 24 ⁸ " 50	503.9 ✓ 24 ⁹ " 24	517.8 ✓ 11 ⁵ 21	521.9 ✓ 3 ⁹ 30
250+00	503.5 ✓ 25 ³ = W. Edge Rd. 55	503.0 ✓ 25 ⁸ = E. Edge Rd. 28	514.9 ✓ 13 ⁹ 25	517.6 ✓ 11 ² 19
			523.3 ✓ 5 ⁵ 30	531.0 ✓ + 2 ² 30
T.P.		8.59	520.22 ✓	
	2.32	522.54 ✓		
+50	507.7 ✓ 20 ³ = W. Edge Rd. 55	501.6 ✓ 20 ⁹ = E. Edge Rd. 29	508.0 ✓ 14 ⁵ 25	519.1 ✓ 3 ⁴ 30
251+00	500.5 ✓ 22 ² = W. Edge Rd. 57	500.9 ✓ 21 ⁶ = E. Edge Rd. 25	511.9 ✓ 10 ⁶ 18	518.9 ✓ 3 ⁶ 18
				522.0 ✓ 0 ⁵ 30

Plotted
G.W.G.
A-16-35

522.54 ✓

L.

L.

R.

251+50	500.6 ✓ 21 ⁹ 58	=W.Edge Rd.	500.3 ✓ 22 ² 26	=E.Edge Rd.	504.0 ✓ 18 ⁵ 21	511.8 ✓ 10 ⁷
--------	----------------------------------	-------------	----------------------------------	-------------	----------------------------------	----------------------------

516.6 ✓ 5 ² 18	518.6 ✓ 3 ² 30
---------------------------------	---------------------------------

T.P.

12.67 ✓ 509.87

7.14 ✓ 517.01

252+00	500.9 ✓ 16 ¹ 57	=W.Edge Rd.	501.0 ✓ 16 ⁰ 26	=E.Edge Rd.	501.2 ✓ 15 ⁸ 10	503.8 ✓ 13 ²
--------	----------------------------------	-------------	----------------------------------	-------------	----------------------------------	----------------------------

510.6 ✓ 6 ⁴ 30

+50	502.4 ✓ 14 ⁸ 57	"	502.4 ✓ 14 ⁸ 26	"	505.6 ✓ 11 ⁴ 22	510.5 ✓ 6 ⁵
-----	----------------------------------	---	----------------------------------	---	----------------------------------	---------------------------

516.3 ✓ 0 ⁷ 30

253+00	504.0 ✓ 13 ⁰ 55	"	503.9 ✓ 13 ¹ 23	=E.Edge Rd.	511.9 ✓ 5 ¹ 19	514.7 ✓ 2 ³
--------	----------------------------------	---	----------------------------------	-------------	---------------------------------	---------------------------

518.8 ✓ +1 ⁸ 30

+50	504.9 ✓ 12 ¹ 45	"	504.7 ✓ 12 ³ 13	"	514.9 ✓ 2 ¹ 9	516.1 ✓ 0 ⁹
-----	----------------------------------	---	----------------------------------	---	--------------------------------	---------------------------

519.3 ✓ +2 ³ 30

+80	505.3 ✓ 11 ⁷ 35	=W.Edge Rd.	504.8 ✓ 12 ² 4	=E.Edge Rd.	514.7 ✓ 2 ⁸	
-----	----------------------------------	-------------	---------------------------------	-------------	---------------------------	--

517.0 ✓ 0 ⁰ 30

Plotted
G.W.G.
4-16-35

	517.01	L.	£.	R.
253+90	504.9 12 ¹ - W. Edge 31 Rd.	505.5 11 ⁵ 13	504.8 12 ² - E. Edge Rd.	513.4 3 ⁶ 4
T.P.	3.81	509.27	11.55	505.46
254+32	499.6 9 ⁷ 30	501.6 7 ⁷ 19	504.8 4 ⁵ - W. Edge 13 Rd.	505.3 4 ²
+64	499.5 9 ⁸ 30	499.8 9 ⁵ 20	501.7 7 ⁶ 15	502.5 6 ⁸ 5
255+00		499.9 9 ⁴ 30	500.2 9 ¹ 13	500.3 9 ²
+50		500.4 8 ⁹ 30	500.6 8 ⁷ 13	501.8 7 ⁵
256+00		Level	501.4 7 ⁹	Level
+50			501.0 8 ³	

↑ Cultivated
↓ Grain Field

Plotted
G.W.G.
A-16-35

Cont'd. From Page 41.

April-15-1935.

42.

	509.27 ✓	L.	£
257+00		Level	500.9 ✓ 8 1/2
T.P.		8.54	500.73 ✓
	5.15 ✓	505.88 ✓	
+50		Level	500.7 ✓ 5 3/4
258+00		"	500.7 ✓ 5 3/4
+50		"	500.6 ✓ 5 3/4
259+00		"	500.8 ✓ 5 1/2
+50		"	500.8 ✓ 5 1/2
260+00		"	501.7 ✓ 4 8/8
+50		"	501.1 ✓ 4 8/8
261+00		"	501.3 ✓ 4 6/8
+50		"	501.5 ✓ 4 4/8
262+00		"	501.6 ✓ 4 3/8
+50		"	501.5 ✓ 4 4/8
T.P.		4.59	501.29 ✓
	6.40 ✓	507.69 ✓	

R.

Level

"

"

"

"

"

"

"

"

"

"

"

Cultivated Grain Field

Plotted
G.M.G.
4-16-35

Cont'd. From Page 42.

April-15-1935.

43.

	507.69	L.	501.8	R.	
263+00		Level	59	Level	
+50		"	501.6	"	
264+00		"	61	"	
+50		"	501.7	"	
		"	60	"	
		"	502.8	"	
		"	49	"	
	502.6	503.9	504.3	504.5	
+70	51	38	34	32	
	25	13		25	
265+00	497.9	499.2	501.1	504.0	501.9
	98	85	66	37	58 = W. Edge Rd.
	25	13		18	30
+15	496.9	497.2	500.6	502.6	501.9
	108	105	74	51	58 " 65 = E. Edge Rd.
	25	13		15	21
+50	501.6	501.7	501.9	500.9	
	61	60	58 = W. Edge Rd.	68 = E. Edge Rd.	
	25	13		34	
266+00	501.6	501.6	500.9	499.9	501.3
	61	61 = W. Edge Rd.	68	78 " 64	62 = Pca.
	25	13		15	17
+50	501.7	501.5	501.6	500.3	501.3
	60	62 " 61	67	74 " 64	501.2
	25	19	13	9	10
					14

Level →

Plotted
G.W.G.
A-16-35

	507.69							
T.P.		6.66	501.03					
	6.04	507.07						
267+00		501.7	501.1	501.3	501.3			
		5 ⁴	5 ⁷	5 ⁸	5 ⁸ - Fee.	Level →		
		25	13		15			
+50		501.6	501.5	501.5	500.9	501.9	501.4	
		5 ⁵ Fee.	5 ⁶	5 ⁶	6 ²	5 ²	5 ⁷ Fee.	Level →
		22	13		10	12	17	
268+00		501.6	501.4	501.6	501.3	502.1	501.6	
		5 ⁵ "	5 ⁷	5 ⁵	5 ⁸	5 ⁹	5 ⁵ "	"
		19	13		13	14	18	
+50		501.5	501.1	501.4	501.4	502.5	501.9	
		5 ⁶ "	6 ⁰	5 ⁷	5 ⁷	4 ⁶	5 ² "	"
		17	13		14	16	20	
269+00		500.9	501.4	501.6	501.4	502.1	501.6	
		6 ²	5 ⁷	5 ⁵	5 ⁷	5 ⁰	5 ⁵ "	"
		25	13		15	16	22	
+50		502.5	502.0	501.9	501.5	502.1	501.7	
		4 ⁶	5 ¹	5 ²	5 ⁶	5 ⁰	5 ⁴ "	"
		25	13		17	18	24	
270+00	502.5	502.7	502.1	502.1	501.8	502.1	502.3	
	4 ⁶	4 ⁴	5 ⁰	5 ⁰	5 ³	4 ⁷	4 ⁸ "	"
	25	13	11		18	19	25	

Plotted
G.W.G.
4-16-35

	507.07	L.	£	R.		
270+50	502.4 4 ⁷ 25	502.4 4 ⁷ 13	502.5 4 ⁶ 9	502.4 4 ⁷	502.1 5 ⁰ 19	502.6 4 ⁵ Fce. 27
271+00		503.0 4 ¹ 25	502.9 4 ² 13	502.8 4 ²	502.3 4 ⁸ 19	503.0 4 ¹ " 28
+50		503.5 3 ⁶ 25	503.4 3 ⁷ 13	503.1 4 ⁰	502.8 4 ² 21	503.6 3 ⁵ " 30
272+00		503.6 3 ⁵ 25	503.4 3 ⁷ w. Edge Rd.	502.8 4 ² F. Edge Rd. 25	503.8 3 ² Fce. 33	✓
+50		503.5 3 ⁶ 25	503.9 3 ²	503.1 4 ⁰ F. Edge Rd. 31	504.1 3 ⁰ Fce. 39	
273+00		504.0 3 ¹ 25	503.4 3 ²	503.7 3 ⁴ 10	503.6 3 ⁵ 36	504.4 2 ⁹ Fce. 44
T.P.		3.20	503.87			
6.01	509.88					
+50		504.2 5 ⁷ 25	503.9 6 ⁰	503.9 6 ⁰ w. Edge Rd. 13	503.7 6 ² 38	504.3 5 ⁶ Fce. 47

Plotted
6.11.6.
4-16-35

509.88

L.

¢

R.

274+00

✓
50A.1
5⁵
25

✓
50A.2
5⁷

✓
50A.0
5⁹
15

✓
50B.7
6²
40

✓
50A.5
5⁴ Fce.
48

+50

✓
50A.1
5⁸
25

✓
50A.5
5⁴

✓
50A.1
5⁸
12

✓
50B.8
6¹
38

✓
50A.6
5³ "
45

275+00

✓
50A.0
5⁹
25

✓
50A.3
4⁶

✓
50A.5
5⁴
7

✓
50A.1
5⁸
34

✓
50A.7
5³ "
40

+50

✓
50B.2
6⁷
25

✓
50A.4
4⁵

✓
50A.5
5⁴
2

✓
50A.1
5⁹
30

✓
50A.9
5⁰ "
34

276+00

✓
50A.2
7⁷
25

✓
50A.6
7²
18

✓
50A.0
4²
11

✓
50A.5
4⁴
3

✓
50A.5
5⁴

✓
50B.9
6⁰
25

✓
50A.9
5⁰ Fce.
29

+50

✓
50A.2
7⁷
25

✓
50A.5
7⁴
19

✓
50A.1
3⁸
6

✓
50A.8
5¹
4

✓
50A.8
5¹

✓
50A.2
5⁷
21

✓
50A.1
4⁸ "
28

277+00

✓
50A.7
7²
25

✓
50A.4
3⁵
7

✓
50A.1
4⁸
6

✓
50A.1
4⁸

✓
50A.7
5²
19

✓
50A.2
4⁷ "
28

+50

✓
50A.3
5⁶
25

✓
50A.4
3⁵
8

✓
50A.3
4⁶
7

✓
50A.1
4⁸

✓
50A.7
5²
18

✓
50A.1
4⁸ "
27

Plotted
G.W.G.
4-16-35

Cont'd. From Page 48.

April-15-1935.

47.

	509.88	L.		¢		R.	
278+00	503.4 6 ⁷ 25	505.7 4 ² 19	506.5 3 ⁴ 9	505.4 4 ⁷ 8	505.1 4 ⁸	504.7 5 ² 17	505.6 4 ³ Fee. 24
+50	503.8 6 ¹ 25	504.1 5 ⁸ 16	506.4 3 ⁵ 8	505.4 4 ⁵ 7	505.4 4 ⁷	504.7 5 ² 17	505.6 4 ³ " 23
279+00	502.5 7 ⁴ 25	503.6 6 ³ 14	506.3 3 ⁶ 7	505.4 4 ⁵ 6	505.4 4 ⁷	504.7 5 ² 18	505.8 4 ¹ 25

4.6 505.3 = check

on Sta. 279+00 of Original C.
Rec. Elev. 505.3 - See Page 31 - this Book.

Cont'd. on Page 31 - This Book.

Profile levels over relocated Pipe line to
at El Monte Park

Void see page 57

B.N.	2.64	510.09	507.45	
B.C. 131+73.24		6.3	03.8	
132		6.3	03.8	
+50		4.7	05.4	
133		4.0	06.1	
+50		4.2	05.9	
134		4.0	06.1	
+50		4.6	05.5	
P	3.49	508.37	5.21	504.88
135		3.4	05.0	
+50		3.4	05.0	
136		3.5	04.9	
+50		3.6	04.8	
137		4.1	04.3	
+50		4.3	04.1	
138		4.6	03.8	
+33.54 EC		4.8	03.6	

Soper
Remmen

Dec. 6 1935

48.

Cont'd from page 48

49.

508.37

138 +50			4.5	503.9
139			4.8	03.6
+50			5.3	03.1
140			5.6	02.8
+50			4.75	503.62 check on B.M. " 19 Elev. 503.62
141			5.9	02.5
TP	4.10	506.35	6.12	502.25
+50			4.2	02.2
142			4.8	01.6
+50			5.3	01.1
143			5.1	01.3
+50			4.9	01.5
144			4.9	01.5
+50			4.9	01.5
+73.09			4.7	01.7
145			4.7	01.7

506.35

145	50	4.8	501.6	
	+67	4.8	01.6	
	+90	9.3	497.1	
146		9.7	498.7	
	+16.39 E.C.	6.4	500.0	
	+30	2.9	03.5	
		2.83	503.52	check on B.M. #20, El. 503.52
	+50	3.6	02.8	
147		4.2	02.2	
	+50	4.5	01.9	
TR	3.55	506.12	3.78	502.57
148		4.6	01.5	
	+50	4.3	01.8	
149		4.7	01.4	
	+50	4.5	01.6	
150		4.9	01.2	
	+50	4.8	01.3	

Cont'd from page 50

51

506.12

151	5.2	500.9
+50	5.2	500.9
152	5.4	500.7
+50	5.5	0.6
153	5.4	0.7
+50	5.4	0.7
154	5.4	0.7
+50	5.3	0.8
155	4.9	1.2

~~4.9~~

2.61 503.51 check on B.M. #20 (1) 503.52.

Bench levels from Pumping Plant to Lakeside

	3.01	441.94	438.93
TP			5.56 436.38
	4.30	440.68	
TP			4.98 435.70
	4.35	440.05	
TP			2.18 437.87
	6.03	443.90	
TP			2.84 441.06
	5.50	446.56	
TP			3.34 443.22
	12.71	455.93	
TP			4.09 451.84
	11.33	463.17	
TP			0.05 463.12
	9.77	472.89	
			8.59 484.30
TP			0.13 472.76

Dec. 14 1935
Soper
Remmen

52

check on old B.M. Elev 441.00. (Book 505 page 5) New B.M. # 36
Spike in pole # D28854T 15 ft 329+20

Set new B.M. # 37 spike in power pole # 18774 30 ft sta. 337+70

472.76

11.32 484.08

TP 7.77 476.31

4.47 480.78

TP 11.66 469.12

3.63 472.75

TP 9.40 463.35

0.23 463.58

TP 7.09 456.49

0.19 456.68

TP 9.49 447.19

1.65 448.84

TP 6.54 442.30

1.14 443.44

TP 11.31 432.13

2.97 435.10

TP 2.10 433.00

3.52 436.52

check on old B.M. Elev. 476.23 (Book 505 page 47) New B.M. # 38
Spike in power pole # 78772 40' Rt Sta. 343+40

Line thru Linda Lake, from here

↓
set new B.M. # 39 Spike in power pole # 78767 10' Rt Sta 351+10

check on B.M. Elev. 432.09 (Book 505 page 40) New B.M. # 40 Spike in
power pole # 78762 10' Rt 363+50

Cont'd from page 53

	436.52		
TP		6.47	430.05
	0.99	431.04	
TP		9.09	421.95
	3.26	425.21	
TP		6.46	418.75
	2.80	421.55	
TP		7.42	414.13
	2.71	416.84	
TP		6.79	410.05
	0.34	410.39	
TP		9.13	401.26
	0.26	401.52	
TP		10.02	391.50
	4.07	395.57	
TP		4.99	390.58
	4.43	395.01	
TP		4.53	390.48

Dec. 16 1935

Soper
Remmen

54

set new B.M. #41 Spike in power pole #78758 10' Rt 375+25

Check on old B.M. Elev. 410.04 (Book 50.5 page 34) New B.M. #42 Spike in
Eucalyptus stump 18' Lt 384+75

			390.48
	4.74	395.22	
TP		0.50	394.72
	12.71	407.43	
TP		0.72	406.71
	3.82	410.53	
		1.84	408.69
TP		7.01	403.52
	3.46	406.98	
TP		6.35	400.63
	4.88	405.51	
TP		0.25	405.26
	5.48	410.74	
TP		0.13	410.61
	8.21	418.82	
TP		3.41	415.41
	1.70	417.11	

Set new B.M. #43 Spike in Pepper tree 70' H Sta 398+10

Set new B.M. #44 Spike in power pole #78205 S.E. Cor. Vine & Woodside

417.11

TP.

8.16 408.95

set new B.M. #45 Spike in power pole #72615
N.W. Cor. River & Woodside

0.65 409.60

TP.

7.19 402.41

2.98 405.39

5.26 400.13

check on County B.M. #21 Elev. 400.13 (Book 505 page 86)

Final Profile Levels

Profile over line change at El Monte Park

B.M	2.59	510.04 ✓	507.45
131+74.40 BC		6.3	503.7 ✓
132		6.3	03.7 ✓
+50		4.6	05.4 ✓
133		4.0	06.0 ✓
+50		4.1	05.9 ✓
134		4.2	05.8 ✓
+50		4.4	05.6 ✓
135		4.5	05.5 ✓
TP		5.60	504.44 ✓

Jan 10 1936
Soper
Remmen

57

from 508-54

This ξ profile is original ground and
supercedes all ξ profiles sta 131+74.40-159+54.35
H.F.S

Final Profile Levels

58

	4.07	508.51 ✓	504.44	
135+50		3.5	05.0 ✓	
136		3.3	05.2 ✓	
+50		3.7	04.8 ✓	
137		4.3	04.2 ✓	
+50		4.5	04.0 ✓	
138		4.6	03.9 ✓	
+50		4.7	03.8 ✓	
139		5.1	03.4 ✓	
+50		5.3	03.2 ✓	

Final Profile Levels

508.51

140

5.6

502.9 ✓

+50

6.2

02.3 ✓

141

6.3

02.2 ✓

+50

6.5

02.0 ✓

TP.

5.31

503.20 ✓

3.40 506.60 ✓

142

5.0

01.6 ✓

+50

5.3

01.3 ✓

143

5.1

01.5 ✓

Final Profile Levels.

60

506.60

143+50.

5.0 501.6 ✓

144.

5.1 01.5 ✓

+50

5.1 01.5 ✓

145

5.0 01.6 ✓

+50

4.8 01.8 ✓

+65

5.0 01.6 ✓

See F.B. 524, Page 62

~~+85~~

~~9.5 497.1 ✓~~

~~144~~

~~10.4 96.2 ✓~~

145

Sections crossed out are original ground before
bench fill put in. H.F.S.

+75.

3.3 503.3 ✓

506.60

146+50

4.0 502.6 ✓

3.10 503.50 ✓ check on B.M. 20.6m 503.52

147

4.5 02.1 ✓

+50

4.8 01.8 ✓

148

5.0 01.6 ✓

+50

4.9 01.7 ✓

149

5.3 01.3 ✓

TP

3.73 505.82 ✓ 4.51 502.09 ✓

+50

4.3 01.5 ✓

505.82

150	4.6	501.2 ✓
+50	4.6	01.2 ✓
151	4.9	00.9 ✓
+50	5.0	00.8 ✓
152	5.1	00.7 ✓
+50	5.3	00.5 ✓
153	5.1	00.7 ✓
+50	5.1	00.7 ✓
154	5.2	00.6 ✓

505.82

154+50 4.9 500.9 ✓

155 4.7 01.1 ✓

+50 4.6 01.2 ✓

+60 5.5 00.3 ✓

156 5.7 00.1 ✓

+37 6.0 499.8 ✓

45 4.0 501.8 ✓

TP 4.61 509.34 1.09 504.73 ✓

+50 7.9 01.4 ✓

	509.34		
156+67		7.8	501.5 ✓
+78		4.7	04.6 ✓
157		3.8	05.5 ✓
+50		4.6	04.7 ✓
+62		4.8	04.5 ✓
+79	for Class 1 use bottom of class 2 Bx	+4.4	13.7 ✓
158		+4.0	13.3 ✓
+40		+0.4	09.7 ✓
+50		1.0	08.3 ✓

Sections crossed out are original profile before
class 2 excavation. H.F.S.

509.34

159+90	8.2	01.1 ✓
159	8.5	00.8 ✓
+10	8.4	00.9 ✓
+35	3.9	05.4 ✓
+50	2.5	06.8 ✓
+54.35 Bk 62.76 and	2.5	06.8 ✓
	4.3	505.0 ✓ check on

sections crossed out are original profile before class 2 excavation HFS.

Sta 160+00 (505.0 Bk 508-62)

Original ground profile cont'd F.B. $\frac{508}{62}$ HFS.

Check levels-page 71

Bench levels 342-427 via Julian Ave.

B.M. #38	0.80	477.11	476.31
TP		12.75	464.36
	0.77	465.13	
TP		5.21	459.92
	5.31	465.23	
TP		6.97	458.26
	0.17	458.43	
TP		5.41	453.02
	0.56	453.68	
TP		10.15	443.53
	0.67	444.20	
TP		12.30	431.90
	2.78	434.68	
		1.48	433.20
TP		3.45	431.23

Feb 24-36
Soper
Remmen

66

set new B.M. #39. Nail in poupe #74390 25' H sta. 351+80

set new B.M. #40. Nail in 16" Eucalyptus 40' H sta. 364+65

on old B.M. Rec. Elev. 433.07 Book 316

set new B.M. #41. Nail in Eucalyptus stump 28' H. 375+30

431.23

	0.86	432.09		
TP			11.83	420.26
	0.55	420.81		
TP			7.68	413.13
	0.78	413.91		
TP			5.39	408.53
	1.17	409.70		
TP			5.25	404.45
	12.37	416.02		
TP			1.12	415.70
	12.53	428.23		
TP			0.57	427.72
	9.93	437.65		
TP			4.88	432.77
	4.20	436.97		
			3.82	433.15
			1.64	435.33

set new B.M. #42. Nail in power pole #78751. 25' H 388+30

on old B.M. Rec. Elev. 432.95 Box 316 -

set new B.M. #43. Nail in power pole #78756 20' H 564+00+05

	436.97		
TP		9.65	427.32
	0.25	427.57	
TP		8.86	418.71
	2.90	421.01	
TP		1.02	419.99
	1.33	421. ³² 34	
		4.26	417. ⁰⁶ 98
TP		10.40	410. ⁹² 94
	2.21	413. ¹⁸ 20	
TP		5.80	408. ^{07.98} 00
	5.28	413. ²⁶ 28	
		5.48	407. ⁷⁸ 80
		4.23	409. ⁰³ 05

run old B.M. Rec. Elev. 416.89, New B.M. #44. Small R.R. spike in guy pole S.W. corner - Julian's Chestnut.

set new B.M. #45. Nail in guy pole 15' H 420+50

run B.M. Elev. 408.95 Book 516 - page 79 (New B.M. #46)

See check levels - page 71

Profile levels, x section, sta. 366+50 to sta. 370+50

	B.M. 40	777	460.79	453.02	Grade
366+50			12.1	48.7	43.08
367+00			12.0	48.8	42.73
+30			9.2	51.6	42.84
+50			10.1	50.7	42.78
+72			9.6	51.2	42.71
368+00			5.7	55.1	42.63
+36.8			4.7	56.1	42.52

March 3 - 36
Soper
Remman

69

Lt

¢

Rt

Slope stakes + from present road
grade 13' from E ditch + 1/4 tol

Book 503 page 7 for Class 2 Excavation

¢ cut						
5.6			5.6			
5.8			5.8	$\frac{5.8}{1.8}$	$\frac{7.2}{1.0}$	$\frac{7.8}{13.0}$
8.8			8.8	$\frac{6.8}{5.0}$	$\frac{6.8}{0.5}$	$\frac{9.7}{8.0}$ $\frac{8.6}{13.0}$
7.9			7.9	$\frac{7.4}{5.0}$	$\frac{7.4}{3.0}$	$\frac{8.8}{13.0}$
8.5			8.5	$\frac{7.9}{7.0}$	$\frac{10.9}{8.5}$	$\frac{12.9}{10.0}$ $\frac{12.9}{13.0}$ $\frac{14.3}{14.3}$ $\frac{14.6}{23.0}$
13.5			13.5	$\frac{9.7}{5.0}$	$\frac{9.8}{2.8}$	$\frac{15.5}{5.0}$ $\frac{15.3}{10.0}$ $\frac{17.1}{14.5}$ $\frac{17.1}{20.0}$
13.6			13.6	$\frac{7.5}{5.0}$	$\frac{7.5}{2.5}$	$\frac{16.7}{13.6}$ $\frac{16.0}{11.0}$ $\frac{12.0}{16.0}$ $\frac{19.3}{22.0}$

460.79

Grade

cut

368+50

7.5

53.3

42.48

10.8

70 7.1 18.3
5.0 2.5 10.8 9.0

(0.137) 21.9
14.5 22.0

TP

4.84

452.25

12.88

447.71

369+00

5.2

47.1

40.72

6.4

7.0 7.0 8.9 12.9
5.0 3.0 6.4 7.5 8.0

(0.66) 14.6

14.7
20.0

+50

9.0

43.3

37.36

5.9

5.9 5.1 8.8
7.5 11.0

(0.27) 13.7

8.9
20.0

370

11.7

40.6

34.00

6.6

6.6 6.4 7.4 8.5
7.0 9.5 15.0

(No slope data)

+50

13.3

39.0

33.18

5.8

11.9

40.4

Check on
13' offset
Sta 370+00

Elev. 40.3 back 516-45

LT

C

RT

70

March 3-31
Soper
Remmen

71

Check levels - via Julian Ave.

B.M.^{#38} 0.59 476.90 476.31

TP. 9.795 467.105

1.605 468.71

TP. 7.47 461.24

2.52 463.76

3.84 459.92

✓ on B.M.^{#39} Elev. 459.92

TP. 3.01 460.75

2.14 468.89

TP. 11.87 457.02

0.895 457.915

TP. 4.895 453.02

✓ on B.M.^{#40} Elev. 453.02

1.625 454.645

TP. 13.05 441.595

1.105 442.700

9.50 433.20

✓ on old B.M. Rec. Elev. 433.20 (Book 316)

TP. 11.475 431.225

✓ on B.M.^{#41} Elev. 431.23

431.225

0.50 431.725

TP 12.36 419.365

0.185 419.55

TP 8.82 410.73

3.01 413.74

TP 9.29 404.45

v on B.M. #42 Elev 404.45

12.87 417.32

TP 0.33 416.99

12.53 429.52

TP 0.65 428.⁸⁷~~77~~

7.66 436.53

TP 1.20 435.33

v on B.M. #43 Elev. 435.33

0.105 435.435

TP 12.015 423.42

0.1 423.53

TP 6.91 416.62

416.62

5.05 421.67

4.60 417.07

r on B.M. 44 Elev. 417.06

T

12.76 408.91

4.45 413.36

TP

5.94 407.42

6.27 413.69

5.93 407.76

r on B.M. 45

T

4.68 409.01

r on B.M. 46

0.29 409.30

T

6.91 402.37

3.56 405.95

5.84 400.11

r on B.M. Elev 400.13. Erased account of wrong rod reading.

March 5 1936
Soper
Remmon
Isbell

RT

74

Slopeside
(+ from present road grade)
10' " & ditch = 1/2 total

x section and slope stakes sta 335+50 - 347+00

Book 503 Page 18 for Class 2 Excavation

	℄ Elev.	Grade	℄ cut
335+50	52.8	446.55	6.3
336	55.9	48.80	7.1
+50	58.2	51.05	7.2
337	59.9	53.30	6.6
+50	61.8	55.55	6.3
338	64.0	57.80	6.2
+50	66.2	60.05	6.2
339	68.1	62.30	5.8

6.3	$\frac{+6.1}{12.0}$		
7.1	$\frac{+6.6}{8.6}$	$\frac{C.6.2}{11.5}$	$\frac{+15.8}{12.5}$ $\frac{+17.5}{20.0}$
7.2	$\frac{6.5}{7.2}$	$\frac{12.0}{11.2}$	$\frac{C.5.3}{11.3}$ $\frac{+15.1}{20.0}$
6.6	$\frac{6.6}{8.2}$	$\frac{12.0}{10.7}$	$\frac{C.6.0}{11.5}$ $\frac{+15.0}{20.0}$
6.3	$\frac{6.0}{6.1}$	$\frac{12.6}{9.4}$	$\frac{C.7.3}{11.8}$ $\frac{+15.5}{20.0}$
6.2	$\frac{6.2}{4.9}$	$\frac{12.6}{8.0}$	$\frac{C.6.4}{11.0}$ $\frac{+15.4}{20.0}$
6.7	$\frac{6.2}{4.2}$	$\frac{12.7}{7.0}$	$\frac{C.7.8}{11.9}$ $\frac{+16.6}{20.0}$
5.8	$\frac{5.8}{3.0}$	$\frac{12.8}{6.0}$	$\frac{C.8.7}{12.2}$ $\frac{+17.0}{20.0}$

	± Elev.	Grade	± cut
338+50	70.3	64.00	6.3
340	72.7	65.70	7.0
+50	75.4	67.40	8.0
341	79.1	68.70	10.4
+50	81.9	69.60	12.3
342	80.1	69.87	10.2
+50	78.5	69.52	9.0
343	76.6	69.17	7.4
+50	74.7	68.15	6.6

Lt.	±	RT
6.3	$\frac{6.3}{2.4}$ $\frac{12.5}{5.1}$	$\frac{C 8.3}{12.1}$ $\frac{17.2}{20.0}$
7.0	$\frac{7.0}{0.4}$ $\frac{13.9}{3.9}$	$\frac{C 8.5}{12.1}$ $\frac{16.2}{15.0}$
$\frac{8.0}{5.0}$ 8.0	$\frac{14.3}{3.0}$	$\frac{C 7.8}{11.9}$ $\frac{16.4}{15.0}$
$\frac{8.8}{5.0}$ $\frac{8.8}{0.7}$ 10.4	$\frac{14.3}{1.9}$	$\frac{C 6.6}{11.6}$ $\frac{16.1}{15.0}$
$\frac{9.2}{5.0}$ $\frac{9.2}{1.6}$ 12.3	$\frac{13.7}{0.9}$	$\frac{C 5.6}{11.4}$ $\frac{15.2}{15.0}$
$\frac{8.9}{5.0}$ $\frac{8.9}{0.6}$ 10.2	$\frac{11.7}{0.8}$	$\frac{C 4.3}{11.1}$ $\frac{13.6}{15.0}$
$\frac{9.0}{5.0}$ 9.0	$\frac{11.2}{7.0}$	$\frac{C 3.4}{10.9}$ $\frac{12.9}{15.0}$
7.4	$\frac{8.8}{1.0}$	$\frac{9.6}{15.0}$ (no slope stake)
6.6	$\frac{8.0}{0.6}$	$\frac{7.4}{15.0}$

Book 503

	℄ Elev.	Grade	℄ cut
344	72.8	66.45	6.4

+50	71.0	64.75	6.3
-----	------	-------	-----

345	69.1	63.05	6.1
-----	------	-------	-----

+50	67.3	61.35	6.0
-----	------	-------	-----

346	65.9	59.65	6.3
-----	------	-------	-----

+50	64.4	58.45	6.0
-----	------	-------	-----

347	64.2	57.75	6.5
-----	------	-------	-----

Lt	℄.	Rt
----	----	----

64	$\frac{7.8}{0.8}$	$\frac{7.8}{15.0}$
----	-------------------	--------------------

63	$\frac{8.0}{0.8}$	$\frac{7.4}{15.0}$
----	-------------------	--------------------

61	$\frac{9.0}{2.8}$	$\frac{7.8}{6.0}$	$\frac{8.2}{15.0}$
----	-------------------	-------------------	--------------------

60	$\frac{7.7}{1.0}$	$\frac{8.8}{4.0}$	$\frac{7.4}{8.0}$	$\frac{8.3}{15.0}$
----	-------------------	-------------------	-------------------	--------------------

63	$\frac{7.6}{1.0}$	$\frac{8.9}{4.0}$	$\frac{7.9}{7.0}$	$\frac{7.9}{12.0}$
----	-------------------	-------------------	-------------------	--------------------

60	$\frac{7.5}{1.0}$	$\frac{8.1}{4.0}$	$\frac{7.5}{12.0}$
----	-------------------	-------------------	--------------------

65	$\frac{6.5}{12.0}$
----	--------------------

Book 503
for Class 2 Exc.

8) 3400.
37.5

~~18~~ 25.
3

12 75

34 00

4676.

