

W  
500

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.

For Single Track Embankment.

509

MICROFILMED

H	0	1	2	3	4	5	6	7	8	9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

Copyright, 1914, by Eugene Dietzgen Co.

Made in U. S. A.

DIST

H

0  
1  
2  
3  
4  
5  
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7  
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9  
10  
11  
12  
13  
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36  
37  
38  
39  
40

Ex  
to be a  
of road  
exampl  
30.6 =

## Index

Pages

Pipe line profile levels	1-58
Profile levels on revised line on Julian Ave. Sept. 1935.	59-71
Notes from sheet paper-Linda lake.	72
Check levels.	73-74
Levels line change El Monte pump plant.	75-76
Reprofile 42+50 - 43+00	77
Reprofile sta. 85+50 - 89+50	78

Profile levels El Capitan Pipe Line  
 Cont. from Book #508

8-13-35

H. H.  
 Landon  
 Super.  
 Remmer.

B.M.	3.75	491.33	487.58	Grade	
207		5.9	85.4	78.30	7.1
+50		6.8	84.5	78.15	6.3
208		7.9	83.4	472.98 478.00	5.4
+50		8.3	83.0	73 77.45	5.3
209		9.4	81.9	49 77.50	4.4
+50		9.5	81.8	24 77.25	4.6
+85		9.8	81.5	77.1	4.4
210		7.8	83.5	76.99 477.00	6.5

On pole # P 173426

-0.30%

-0.50%

✓  
491.33

210 +50 5.7 485.6<sup>✓</sup> 76.67<sup>66</sup> 8.9

211 5.3 86.0<sup>✓</sup> 76.33<sup>✓</sup> 9.7

+50 5.2 86.1<sup>✓</sup> 76.00<sup>✓</sup> 10.1

212 6.1 85.2<sup>✓</sup> 75.67<sup>66</sup> 9.5

+50 7.2 84.1<sup>✓</sup> 75.33<sup>✓</sup> 8.8

213 8.1 83.2<sup>✓</sup> 75.00<sup>✓</sup> 8.2

+50 8.5 82.8<sup>✓</sup> 74.67<sup>66</sup> 8.1

214 8.9 82.4<sup>✓</sup> 74.33<sup>✓</sup> 8.1

J.P. 5.00 87.82<sup>✓</sup> 8.51 82.82<sup>✓</sup>

-0.667%

487.82

2

214+50 ✓ 5.7 ✓ 482.1 ✓ 474.00<sup>83</sup> 8.1

215 6.0 ✓ 81.8 ✓ 73.91<sup>74</sup> 7.9

+50 5.5 ✓ 82.3 ✓ 73.83<sup>85</sup> 8.4

216 5.3 ✓ 82.5 ✓ 73.74<sup>76</sup> 8.7

+50 5.0 ✓ 82.8 ✓ 73.66<sup>77</sup> 9.1

217 5.7 ✓ 82.1 ✓ 73.57<sup>78</sup> 8.5

+50 5.8 ✓ 82.0 ✓ 73.49<sup>48</sup> 8.5

218 X 6.0 ✓ 81.8 ✓ 473.70<sup>79</sup> 8.4

+50 6.5 ✓ 81.3 ✓ 73.22<sup>23</sup> 8.1

-0.17%

487.82

219

7.4 480.1 73.05

see FB 424-22

For Class I x Use Levels <sup>524</sup>

+25 are widening road on curve prior to class 7.7 80.1 73.0

+50

9.7 78.1 72.87

88

220

10.0 77.8 72.70

71

+50

10.5 77.3 72.52

52

221

10.7 77.1 72.35

37

+50

10.0 77.8 72.17

20

222

9.4 78.4 72.00

02

T.P.

7.86 86.12 9.56 78.26

-0.35%

-0.50%

✓  
486.12

516  
7  
Grade's

4

222+50 7.4 478.7 471.7 6.9

223 6.7 79.4 71.3 8.1

+50 6.1 80.0 71.29

224 5.6 80.5

+37 5.5 80.6

+50 +3.0 89.1

+53 +4.1 90.2

+90 +9.0 95.1

225 +8.8 94.9

FB 524 } for these 3  
See page 23 }  
at head sec. 524  
54

See 524  
54 } for panels

-0.502



486.12 ✓

225+37

+6.0 492.1 ✓

+50

+33 89.4 ✓ 7033

+88

-0.508

3.3 87.8 ✓

+92

8.5 77.6 ✓

226

Y

8.5 77.6 ✓ 470.<sup>08</sup><sub>00</sub>

+50

9.0 77.1 ✓ 7033

+60

9.2 76.9 ✓

+87

11.6 74.5 ✓

+90

18.7 67.4 ✓

✓  
486.12

Grade

227 X

19.6 ✓  
466.5

470.66  
466.00

T.P.

5.45

78.62 ✓

12.95

73.17 ✓

+50

12.2

66.4 ✓

71.00

228

12.4

66.7 ✓

71.90

+50

12.5

66.1 ✓

72.93

229

13.3

65.3 ✓

74.42

+29

13.0

65.6 ✓

+33

4.5

74.1 ✓

+40 X

465.82

+50

2.3

76.3 ✓

475.91

286.31  
+19.31

478.62 ✓  
TP 12.59 90.81 0.40 78.22 ✓  
Grade

230 x 4.4 486.4 ✓ 477.40 ✓

TP 12.92 502.39 ✓ 1.34 89.47 ✓

+32 6.4 96.0 ✓

+50 5.4 97.0 ✓ 79.15 ✓

+75 97.8 ✓ 80.02 ✓

231 x 4.1 98.3 ✓ 480.90 ✓

+25 504.3 ✓ 81.35 ✓

+50 2.7 99.7 ✓ 81.80 ✓

+75 2.3 500.1 ✓ 82.70 ✓

232 2.3 500.1 ✓ 82.70 ✓

+25 4.40 04.47 ✓

T.P. 2.32 500.07 ✓

For Class 2 Excavation - Book 503

00 = present road grade  
13' bench

Sta 230+67

		0.0		
		13.0		0.0
+12.8	C 10.2	0.0		
22.0	15.6	10.0		0.0

+15.0	C 14.0	11.3	0.0	
21.0	16.5	7.0	1.0	0.0

46.3	C 15.6	11.1		0.0
19.6	16.9	1.5	4.7	3.0

+17.7	C 17.1	12.9	12.4	
21.0	17.3	8.0	3.5	0.0

+18.6	C 17.5	11.0	0.0	
20.5	17.4	5.0	2.0	0.0

20.5	C 17.2	10.5	0.0	
25.0	17.3	6.0	3.0	0.0

19.2	C 15.2	12.8	0.0	
25.0	16.8	8.0	4.0	0.0

504.47

Grade

B.M.

1.64 502.83 502.88

Cor. ✓  
504.52

232 +54

4.3 500.7 483.60

+75

233

5.0 499.5 83.70

+25

+50

+0.20  
+0.20

6.7 97.8 83.80

+78

6.1 498.4

+78

234 Y

+3.1 507.6 483.90

+27

+1.3 505.8

+38

-2.60

6.5 498.0

+50

6.5 98.0 82.60

+57

17.9 C13.5 8.8 0.0  
24.0 16.4 8.0 6.0 0.0

13.3 C10.2 7.8 0.0  
21.0 15.5 10.0 7.0 0.0

11.6 C9.2 6.0 0.0  
21.0 15.3 10.0 8.0 0.0

11.0 C8.5 6.4 0.0  
20.0 15.1 10.0 8.0 0.0

11.9 C10.7 7.8 0.0  
20.0 15.7 8.0 5.0 0.0

14.5 C12.4 8.5  
21.0 16.1 7.0 0.0

15.2 C13.2 8.9 0.0 0.0  
23.0 16.3 4.0 5.0

15.0 C12.5 7.5 0.0 0.0  
25.0 16.1 7.7 1.0 5.0 10.0

13.1 C11.3 8.2  
23.0 15.8 3.0 0.0

11.3 C9.2 8.0 0.0  
25.0 15.3 9.0 5.0 0.0

10.3 C9.2 0.0  
25.0 15.0 9.0 0.0

504.52

235

6.4 ✓ 498.1 81.30

20  
+50

12.3 ✓ 492.2

(+34)

490.1

T.P. 0.45 91.98 12.99 91.53

+50x

4.4 ✓ 87.6 480.00

from 524/63

236

13.1 ✓ 78.9 73.00

T.P. 0.84 79.79 13.03 78.95

+50x

8.3 ✓ 71.5 466.00

+55

9.2 ✓ 70.6

237

10.5 ✓ 69.3

234+63

0.0  
13.0 0.0

9

479.79

237+50

11.6 468.2

238

12.0 67.8

+50

12.4 67.4

239

12.7 67.1

+50

12.9 66.9

T.P.

3.22

70.15

12.86

66.93

240 X

3.4

66.8

459.80

-7.0

+50

-0.75%

3.6

66.6

59.42

+7.2

241

4.0

66.2

59.05

+7.2

4

2

RH

10

	✓ 170.15			
241+50		4.1	466.1	458.67
242		4.5	65.7	58.30
+50		4.7	65.5	57.92
+64		5.1	65.1	57.81
+74	-0.75%	8.2	62.0	57.74
243		8.2	62.0	57.55
+50		9.1	61.1	57.17
244		9.4	60.8	56.80
+50		10.8	59.4	56.42

H	Q	RH	11
		+7.4	
		+7.4	
		+7.6	
		+7.3	To F.B. 524-1/2
		+4.3	
		+4.5	
		+3.9	
		+4.0	
		+3.0	

✓  
470.15  
245 10.9 459.3 456.05

T.P. 3.41 62.05 11.51 58.64

+50 3.5 58.5 55.67 +2.8

246 3.7 58.3 55.30 +3.0

+50 3.9 58.1 54.92 +3.2

247 3.3 58.7 54.55 +4.2

+50 3.8 58.2 54.17 +4.0

248 5.9 56.1 453.80 +2.3

+50 6.2 55.8 53.50 +2.3

-0.75%

X  
-0.60%

4 1 77

+3.3

+2.8

+3.0

+3.2

+4.2

+4.0

+2.3

+2.3

12



✓  
462.05

249	6.3	✓ 55.7	453.20
-----	-----	-----------	--------

H Q Rt

+2.5

+50	5.7	✓ 56.3	52.90
-----	-----	-----------	-------

+3.4

250	6.3	✓ 55.7	52.60
-----	-----	-----------	-------

+3.1

+50	6.6	✓ 55.4	52.30
-----	-----	-----------	-------

+3.1

-0.60%

251	7.0	✓ 55.0	52.00
-----	-----	-----------	-------

+3.0

T.P.	3.48	✓ 58.23	7.30	✓ 54.75
------	------	------------	------	------------

+50	3.7	✓ 54.5	51.70
-----	-----	-----------	-------

+2.8

252	3.8	✓ 54.4	51.40
-----	-----	-----------	-------

+3.0

+50	4.1	✓ 54.1	51.10
-----	-----	-----------	-------

+3.0

13

458.23 ✓

253	4.1	✓ 454.1	450.80
+50	4.6	✓ 53.6	50.50
254	4.8	✓ 53.4	50.20
+50	5.3	✓ 52.9	49.90
255	5.5	✓ 52.7	449.60
+50	5.8	✓ 52.4	49.00 49.55
256	5.9	✓ 52.3	48.40 49.50
+50	6.3	✓ 51.9	47.80 49.45
257	6.4	✓ 51.8	47.20 49.40

-0.60%

-1.80%

H C RT 14

+3.3  
+3.1  
+3.2  
+3.0  
+3.1  
+3.4  
+3.9  
+4.1  
+4.6

Cross-section  
 Soper Remmen Jan 3 1936  
 Additional cross-section  
 Jan 25, 1936  
 Soper Remmen

257+50	-1.20%	458.23	6.6	451.6	444.35	46.60
258	X		7.1	51.1	49.30	446.00
+50			7.2	51.0	49.25	46.80
+60				59.4		46.96
T.P.	7.73	65.19	0.77	57.46		
B.M.		1.56	463.63		463.70	
+65		Cor. 2 65.26		61.7	47.04	
+70			1.1	62.5		
+80				63.8	47.28	
259	+1.60%		2.7	62.6	47.20	47.60
+50			4.3	61.0	47.15	48.40
260			4.6	60.7	449.10	49.20

to 60.524/57

104	4.2	4.2	4.2
120	10.0		20.0
134	16.9	14.5	10.7
25.0	10.0	2.9	12.4
			2.9
			7.0
			8.0
			28.0

16.0	14.7	12.6	8.2	4.4	4.0
15.0	2.8	14.7	2.8	8.0	7.0
					30.0

9.5	16.2	16.5	2.4	3.4
15.0	2.8		28	18.0
				35.0

13.5	15.0	15.5	2.4	3.0
15.0		7.0	23.0	30.0

12.6	12.6	13.4
70.0		11.0

+11.5

257+50  
 258+50  
 259+50  
 260+50  
 261+50  
 262+50  
 263+50  
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 294+50  
 295+50  
 296+50  
 297+50  
 298+50  
 299+50  
 300+50

H C RT

✓  
465.26

260+50 ✓  
49 460.4 450.00  
~~449.00~~

+104

261 ✓  
4.8 60.5 49.78  
~~48.90~~

✓  
 $\frac{10.7}{10.0} \quad \frac{10.7}{10.0} \quad \frac{+0.6}{19.0} \quad \frac{+0.6}{25.0}$

+50 ✓  
4.4 60.9 49.57  
~~48.80~~

✓  
 $\frac{11.3}{10.0} \quad \frac{11.3}{11.3} \quad \frac{+11.3}{30} \quad \frac{+0.4}{19.0} \quad \frac{+0.4}{25.0}$

262 ✓  
5.6 59.7 49.35  
~~48.70~~

✓  
 $\frac{10.4+0.8}{10.4} \quad \frac{+0.8}{15.0} \quad \frac{+0.8}{25.0}$

+50 -0.43% ✓  
6.0 59.3 49.14  
~~48.60~~

✓  
 $\frac{7.8+0.4}{10.2} \quad \frac{+0.4}{13.0} \quad \frac{+0.4}{25.0}$

263 ✓  
7.0 58.6 48.92  
~~58.3 48.50~~

✓  
 $\frac{4.3+0.8}{9.4} \quad \frac{+0.8}{9.0} \quad \frac{+0.8}{25.0}$

+50 ✓  
9.0 56.3 48.71  
~~48.40~~

from FB 524/57 -

✓  
 $\frac{9.8}{15.0} \quad \frac{9.8}{2.8} \quad \frac{9.8}{1.0} \quad \frac{7.6}{2.8} \quad \frac{2.7+0.6+0.6}{6.0} \quad \frac{0.6}{25.0}$

264 ✓  
13.0 57.3 48.50  
~~48.30~~

✓  
 $\frac{9.6}{15.0} \quad \frac{5.5}{2.8} \quad \frac{3.8}{3.8} \quad \frac{2.0}{2.8} \quad \frac{1.3+1.3}{6.0} \quad \frac{1.3}{25.0}$

+50 -0.25% ✓  
14.6 50.7 48.37  
~~48.20~~

✓  
 $\frac{10.0}{25.0} \quad \frac{10.0}{10.0} \quad \frac{4.0}{2.8} \quad \frac{2.3}{2.3} \quad \frac{1.6}{2.8} \quad \frac{1.1}{6.0} \quad \frac{+1.1}{25.0}$

465.26 ✓  
 265 10.8 454.5 ✓ 48.25  
 448.70

+28 7.8 57.5 ✓ 48.17

T.P. 2.53 60.14 ✓ 7.65 57.61 ✓

+50 2.6 57.5 ✓ 48.12  
 48.00

266 -0.25% 2.5 57.6 ✓ 48.00  
 47.90

+50 2.4 57.7 ✓ 47.87  
 47.80

267 2.6 57.5 ✓ 47.75  
 47.70

+50 3.1 57.0 ✓ 47.62  
 47.60

268 4.0 56.1 ✓ 47.50  
 47.50

14 17  
 97 97 8.2 ✓  
 15.0 5.0 2.8 6.3 4.3 +0.3 +0.3  
 2.8 9.0 25.0

93 ✓  
 15.0 9.3 2.3 +0.3 +0.3  
 2.8 11.0 25.0

94 ✓  
 15.0 9.4 2.4 8.1 +1.4 +1.4  
 1.5 2.8 10.0 25.0

96 ✓  
 15.0 9.6 2.0 0.0 0.0  
 1.0 17.0 25.0

98 ✓  
 15.0 9.8 2.8  
 11.0

✓  
 9.8

✓  
 9.4

✓  
 8.6

	460.14		Grade
268+50	4.4	✓ 455.7	47.37 <del>447.40</del>
269	5.0	✓ 55.1	47.25 47.30
+50	5.6	✓ 54.5	47.12 47.20
270	6.0	✓ 54.1	447.00 <del>447.10</del>
+50	6.3	✓ 53.8	46.62 46.70
+70	6.8	✓ 53.3	46.47
271	11.1	✓ 49.0	46.25 <del>445.10</del>
+50	11.6	✓ 48.5	45.87 44.90
272	12.4	✓ 47.7	445.50 <del>44.70</del>

-0.25%

-0.75%

H C RT

18

54.1	54.1	54.1
7.1	7.1	7.1
15.0	15.0	15.0

See Reading + -  
with reference to  
corrected grade

53.8	53.8	53.8	46.0	45.0
7.2	7.2	7.2	-0.6	-0.8
15.0	7.2	4.0	17.0	25.0

53.4	53.3	46.3	46.1
46.2	46.2	-0.2	-0.1
15.0	6.8	10.0	25.0

53.2	53.3	49.0	46.6	46.0
7.1	7.0	+0.4	-0.2	
15.0	7.0	2.8	8.0	25.0

52.9	52.9	50.5	48.5	45.7	45.7
7.0	7.0	4.6	-0.7	-0.7	
15.0	13.5	7.5	2.6	17.0	25.0

53.4	53.4	47.7	45.3	45.7
7.9	7.9	✓	-0.2	-0.3
25.0	20.0	2.2	15.0	25.0

272+50

+60

T.P.

273

+50

+87

274

+06

+50

460.14

✓  
10.4 ✓ 449.7 ✓ 444.50 ✓ 45.37

12.7 ✓ 47.4 ✓ 45.34

6.30 ✓ 58.08 ✓ 8.36 ✓ 51.78

10.8 ✓ 47.3 ✓ 45.24  
44.3010.7 ✓ 47.4 ✓ 45.12  
44.10

11.1 ✓ 47.0 ✓ 45.02

8.5 ✓ 49.6 ✓ 44.99  
443.90

5.8 ✓ 52.3 ✓ 44.97

5.7 ✓ 52.4 ✓ 44.86  
43.85

L R RT

53.3 53.3 49.7 44.6 44.4  
7.9 7.9 -0.8 -1.0  
30.0 23.0 4.3 17.0 30.052.6 49.3 47.4 44.5 44.2  
7.3 4.0 -0.8 -1.1  
23.0 17.0 2.1 15.0 30.052.4 48.2 47.3 45.3 45.3  
7.2 3.0 +0.1 +0.1  
23.0 15.0 2.1 17.0 25.051.1 50.8 48.7 47.4 44.8 44.8  
6.0 5.7 3.6 -0.3 -0.3  
25.0 16.0 12.0 2.3 20 25.052.4 52.3 47.0 44.9 44.8  
7.4 7.3 -0.1 -0.2  
15.0 7.0 20 16.0 25.0

49.6

4.6

52.3 52.3 46.5 44.5 44.5  
7.3 7.3 +1.5 -0.5 -0.5  
15.0 7.3 2.0 20.0 30.052.4 52.4 52.4  
7.5 7.5  
15.0 7.5 11.0

19

	458.08			
275	6.0	452.1	44.73 443.80	
+50	5.6	52.5	44.60 43.75	
276	4.9	53.7	44.48 43.70	
+18		53.4	44.43	
+50	4.3	53.8	44.35 43.65	
277	4.2	53.9	44.22 43.60	
+50	4.2	53.9	44.09 43.55	
278	4.3	53.8	43.96 43.50	
+50	4.6	53.5	43.84 43.45	
279	4.5	53.6	43.71 43.40	
+40		54.5	43.60	

-0.2568

Slopestake + from present road grade 20  
13' front of ditch  
1/4 total slope

H	Q	RT	
19.4	14.1	7.0	7.6
30.0	15.0	12.0	7.4
			15.0

See Book 503 page 9

19.5	19.0	14.2	7.5	7.9	7.9
21.0	15.2	7.5	6.0	7.9	15.0
				+8.7	

23.6	18.3	8.8	7.0	7.0
26.0	13.0	10.0	7.0	15.0
				+9.5

				+9.7
				+9.8

				+9.5	+9.8
				10.5	

22.7	11.3	18.7	8.5	8.0	+9.7
19.0	15.8	10.5	8.0		

23.0	17.9	17.6	7.6		+9.9
22.0	15.0	12.0	8.0		

	10.9	10.9
	73.0	



✓ 458.08  
 ✓ 279+50 3.6 ✓ 454.5 43.58  
 443.35  
 ✓ +70 55.1 43.53  
 TP 4.95 ✓ 60.11 292 55.16  
 ✓ +95 4.8 ✓ 55.3 43.46  
 ✓ 280 -0.25% 6.2 ✓ 53.9 43.45  
 43.30  
 B.M. #27 2.08 ✓ 58.03 458.00  
 ✓ +50 14.1 ✓ 46.0 43.32  
 43.25  
 ✓ 281 -0.35% 13.5 ✓ 46.6 443.20  
 ✓ +50 12.6 ✓ 47.5 43.02  
 ✓ 282 13.4 ✓ 46.7 42.85

Lt Q Rt 5.6 21

+10.9 ✓  
 54.83 ✓ 55.13 55.13 483 480  
 11.3 11.6 11.6 4.8 4.5 ✓  
 15.0 11.6 10.0 22.0 30.0

✓ 64.9 ✓ 55.26 ✓ 46.5 ✓ 46.0  
 11.4 3.0 2.5  
 15.0 11.8 18.0 23.0

53.9 ✓  
 +10.5

55.4 ✓ 49.6 ✓ 46.0 45.3  
 12.1 6.3 2.0  
 25.0 14.0 2.7 15.0

47.4 ✓ 46.6 45.9  
 4.2 2.7  
 15.0 3.4 15.0

47.5  
 +4.5

46.7  
 +3.9

Additional cross-sections  
Jan 27, 1936 22  
Super  
Remmen

460.11

282+50	14.2	45.9	442.67
283	14.6	45.5	42.50
+50	14.7	45.4	42.32
284	12.8	47.3	42.15
+50	13.2	46.9	41.94
+60	12.8	47.3	41.94
285	8.6	51.5	41.80
+50	9.3	50.8	41.62
286	10.4	49.7	41.45

-0.35%

4	♀	RT
45.9	45.9	45.9
$\frac{3.2}{15.0}$	3.2	$\frac{3.2}{15.0}$
49.7	45.5	45.5
$\frac{7.2}{25.0}$	$\frac{3.0}{8.0}$	$\frac{3.0}{15.0}$
50.7	45.4	45.3
$\frac{8.4}{19.0}$	3.1	$\frac{3.0}{15.0}$
53.4	53.4	49.6
$\frac{11.3}{20.0}$	$\frac{11.3}{15.0}$	$\frac{7.5}{10.0}$
47.3	45.6	45.6
$\frac{3.5}{7.0}$	$\frac{3.5}{15.0}$	
53.0	52.0	46.7
$\frac{11.0}{15.0}$	$\frac{10.6}{2.0}$	$\frac{4.7}{2.0}$
46.9	44.9	44.9
$\frac{3.9}{20.0}$		
52.9	52.6	47.3
$\frac{11.0}{15.0}$	$\frac{10.7}{5.0}$	$\frac{3.6}{5.4}$
45.5	45.0	45.0
$\frac{9.9}{15.0}$	$\frac{9.7}{5.0}$	$\frac{6.3}{20.0}$
50.8	50.8	50.8
$\frac{9.2}{15.0}$	9.2	$\frac{9.2}{10.0}$

	✓ 460.11			
T.P.	3.07	52.32	10.86	49.25
286+50	-0.35%	3.5	✓ 48.8	441.27
287	X	4.0	✓ 48.3	41.10
+50		4.2	✓ 48.1	40.82 40.92
288	-0.55%	4.0	✓ 48.3	40.55 40.75
+50		4.7	✓ 47.6	40.27 40.57
287	X	5.1	✓ 47.2	440.00 40.40
+50	-0.40%	4.8	✓ 47.5	39.80 40.22
290		4.3	✓ 48.0	39.60 40.05

48.0	48.0	48.0
84	84	84
150	84	100

452.32 ✓

290+50

4.2 ✓ 448.1 39.40  
439.87

48.4 48.1 46.1 46.1  
9.0 6.7 6.7  
15.0 8.7 10.0 15.0

291

-0.40%

4.6 ✓ 47.7 39.70  
39.90

49.5 48.7 47.2 46.6  
10.3 9.5 7.4  
15.0 4.0 8.5 15.0

+50x

5.5 ✓ 46.8 439.00  
39.56

49.0 48.2 46.8 45.1  
10.0 9.3 6.7  
15.0 4.0 7.8 15.0

292

6.4 ✓ 45.9 38.96  
39.35

48.2 48.2 45.2 44.6  
8.7 9.7 5.6  
15.0 8.0 6.9 15.0

TP 168

49.53 ✓ 4.47 ✓ 47.85

+50

-0.08%

4.2 ✓ 45.3 38.91  
39.17

47.8 47.6 45.0 44.8  
8.9 8.7 5.9  
15.0 7.0 6.4 15.0

293

2.6 ✓ 46.9 38.87  
39.00

47.4 46.2 44.0 43.1  
8.2 8.0 5.1 4.8  
15.0 8.0 7.0 15.0

+50x

2.7 ✓ 46.8 38.83  
38.82

47.8 46.8 46.2 44.4 44.0  
9.0 8.0 8.0 5.8 5.2  
15.0 8.0 8.0 8.0 15.0

294

-0.3%

2.6 ✓ 46.9 38.65

47.6 46.2 46.2 44.4  
9.2 8.3 8.1 5.6  
15.0 8.3 5.0 15.0

449.53

294+50	3.2	446.3	438.48
295	3.5	46.0	38.30
+50	3.7	45.8	38.13
296	4.0	45.5	37.95
+50	4.7	44.8	37.78
297	4.7	44.8	37.60
+10	4.6	44.9	37.57
+40	6.0	43.5	37.46
+50	5.8	43.7	37.43

-0.35%

Lt 2 Rt

25

46 <sup>B</sup>	46 <sup>B</sup>	46 <sup>B</sup>	46 <sup>B</sup>
8.5	7.8	7.8	5.3
15.0	7.0	7.0	15.0

45 <sup>B</sup>	44 <sup>B</sup>	44 <sup>B</sup>
7.2	7.0	7.0
15.0	7.0	10.0

45 <sup>B</sup>	44 <sup>B</sup>	44 <sup>B</sup>	42 <sup>B</sup>
7.4	7.2	7.2	4.4
15.0	7.2	2.0	15.0

45 <sup>B</sup>	44.9	42.5	41.9
7.4	7.3	4.9	4.3
15.0	7.0	8.0	15.0

45 <sup>B</sup>	43 <sup>B</sup>	5	42.7
7.6	2.5	4.0	3.2
15.0	2.0	6.0	15.0

✓  
449.53

298. 6.6 ✓ 42.9 437.25

H Q RT  
AAH  
7.2 44<sup>2</sup>  
15.0 5.0 5.7 5.0  
5.0 15.0

+50 7.2 ✓ 42.3 37.08

AS<sup>5</sup>  
6.4 43<sup>2</sup>  
15.0 2.0 5.2 4.5  
15.0

299 6.6 ✓ 42.9 36.90

A3H  
6.5 42<sup>2</sup> 41<sup>8</sup> 41<sup>2</sup>  
15.0 6.0 5.0 5.0  
4.9 4.4  
5.0 15.0

+50 7.0 ✓ 42.5 36.73

A3<sup>0</sup>  
6.3 42<sup>5</sup> 42<sup>5</sup> 41<sup>0</sup> 41<sup>0</sup>  
15.0 5.8 3.0 8.0 15.0  
5.8 4.3 4.3

300 -0.35% 7.1 ✓ 42.4 36.55

A2<sup>2</sup>  
6.2 42<sup>4</sup> 42<sup>4</sup> 40<sup>8</sup> 40<sup>5</sup>  
15.0 5.9 5.0 13.0 20.0  
4.4 4.0

+50 6.7 ✓ 42.8 36.38

A3<sup>0</sup>  
6.6 42<sup>8</sup> 42<sup>8</sup>  
15.0 6.4 6.4  
10.0

T.P. 4.19 ✓ 46.77 6.73 ✓ 42.80

301 4.2 ✓ 42.8 436.20

+50 4.1 ✓ 42.9 36.03  
35.85

✓  
496.99

302

4.3 ✓ 442.7 35.85  
35.50

+50

4.4 ✓ 42.6 35.67  
35.15

303

4.6 ✓ 42.4 35.50  
34.80

+50

5.0 ✓ 42.0 35.33  
34.45

304

6.0 ✓ 41.0 35.15  
34.10

+50

7.2 ✓ 39.8 34.98  
33.75

305

8.3 ✓ 38.7 434.80  
33.40

+50

8.7 ✓ 38.3 34.35  
33.05

306

8.3 ✓ 38.7 33.90  
32.70

-0.35%

-0.90%

H Q RH

27

42<sup>6</sup> 42<sup>6</sup> 42<sup>6</sup>  
6.9 6.9 6.9  
15.0 10.0 10.0

42<sup>6</sup> 42<sup>3</sup> 40<sup>5</sup>  
7.1 6.8 5.0  
15.0 8.0 15.0

42<sup>7</sup> 42<sup>8</sup> 42<sup>8</sup> 39<sup>8</sup> 39<sup>8</sup>  
6.9 6.7 6.7 3.5 3.7  
15.0 3.0 7.0 15.0

41<sup>8</sup> 41<sup>1</sup> 41<sup>2</sup> 39<sup>9</sup> 38<sup>2</sup>  
6.7 6.6 5.9 3.9 3.6  
15.0 7.5 6.0 15.0

41<sup>2</sup> 41<sup>2</sup> 39<sup>8</sup> 38<sup>2</sup> 38<sup>4</sup>  
6.2 6.0 4.8 3.9 3.4  
15.0 4.0 4.0 15.0

41<sup>4</sup> 41<sup>2</sup> 38<sup>1</sup> 38<sup>2</sup>  
6.6 6.4 3.9 3.4  
15.0 6.0 15.0

41<sup>0</sup> 40<sup>9</sup> 38<sup>3</sup> 38<sup>2</sup> 37<sup>2</sup>  
6.7 6.6 4.0 4.0 2.9  
15.0 5.0 7.0 15.0

40<sup>5</sup> 40<sup>0</sup> 38<sup>2</sup> 38<sup>2</sup> 37<sup>5</sup>  
6.6 6.1 4.8 4.3 3.7  
15.0 2.0 1.0 15.0

446.99 ✓

306+25		7.4	✓ 439.6	33.67
+50	-0.90%	7.5	✓ 39.5	33.45 32.55
307		7.9	✓ 39.1	433.00 432.00
+50		8.2	✓ 38.8	32.90 31.99
308		8.1	✓ 38.9	32.80 31.95
T.P	5.24	45.11	✓ 7.12	✓ 39.87
+50	-0.20%	6.0	✓ 39.1	32.70 31.92
309		5.8	✓ 39.3	32.60 31.90
+50		5.8	39.6 ✓	32.5 32.50 31.87
+95			40.2	32.41

40 <sup>2</sup>	39 <sup>6</sup>	38 <sup>2</sup>	37 <sup>4</sup>
$\frac{6.5}{15.0}$	5.9	$\frac{4.5}{2.0}$	$\frac{3.7}{15.0}$
40 <sup>1</sup>	39 <sup>5</sup>	39 <sup>5</sup>	37 <sup>2</sup> 37 <sup>2</sup>
$\frac{6.7}{15.0}$	6.1	$\frac{6.1}{2.0}$	$\frac{4.3}{5.0}$ $\frac{3.8}{15.0}$
39 <sup>5</sup>	39 <sup>1</sup>	39 <sup>6</sup>	37 <sup>1</sup> 36 <sup>2</sup>
$\frac{6.5}{15.0}$	6.1	$\frac{6.6}{6.0}$	$\frac{4.1}{10.0}$ $\frac{3.7}{15.0}$
39 <sup>0</sup>	38 <sup>2</sup>	39 <sup>1</sup>	
$\frac{6.1}{15.0}$	5.9	$\frac{6.2}{10.0}$	
39 <sup>2</sup>	39 <sup>2</sup>	39 <sup>2</sup>	
$\frac{6.6}{15.0}$	6.7	$\frac{7.0}{10.0}$	
39 <sup>2</sup>	39 <sup>2</sup>	40 <sup>2</sup>	37 <sup>1</sup> 34 <sup>6</sup>
$\frac{6.9}{15.0}$	7.1	$\frac{7.7}{4.0}$	$\frac{4.6}{9.0}$ $\frac{2.1}{20.0}$
39 <sup>2</sup>	40 <sup>2</sup>	37 <sup>2</sup>	35 <sup>4</sup> 34 <sup>2</sup>
$\frac{7.3}{15.0}$	7.8	$\frac{5.2}{2.8}$	$\frac{3.0}{6.0}$ $\frac{2.3}{15.0}$

Seepage 45



See page 75

(Elevs for line change)  
Page 75

145.11

~~310~~

5.3 ~~40.0~~ ✓ 32.40  
~~439.8~~ 31.85

+50

5.0 39.5 ✓ 32.30  
40.1 31.82

311

5.2 36.8 ✓ 32.20  
39.9 31.80

+50

5.6 36.6 ✓ 32.10  
39.5 31.77

312

-0.20%

6.3 36.3 ✓ 32.00  
38.8 31.75

+12

38.7 ✓ 31.98

+50

6.8 38.3 ✓ 31.90  
38.3 31.72

B.M

6.20 38.91 ✓ (438.93)

313

7.5 37.8 ✓ 31.80  
37.6 31.70

+50

7.8 37.2 ✓ 31.70  
37.3 31.55

4 4 81

29

39<sup>5</sup> 40<sup>6</sup> 39<sup>5</sup> 36<sup>7</sup> 34<sup>2</sup> 34<sup>2</sup>  
7.2 8.3 4.4 2.0 2.0  
15.0 2.8 7.2 2.8 8.0 20.0

39<sup>8</sup> 40<sup>2</sup> 39<sup>2</sup> 36<sup>8</sup> 35<sup>0</sup> 34<sup>2</sup> 34<sup>2</sup>  
7.6 8.0 6.8 2.8 2.0 2.0  
15.0 6.0 2.8 4.0 2.8 6.0 15.0

39<sup>8</sup> 39<sup>2</sup> 37<sup>0</sup> 36<sup>6</sup> 36<sup>6</sup> 34<sup>4</sup> 34<sup>2</sup>  
7.7 7.8 5.0 4.5 2.3 2.1  
15.0 7.0 4.0 4.5 2.0 8.0 15.0

23 7.3 5.0 4.3 4.3  
15.0 7.0 5.0 4.3 15.0  
38<sup>2</sup> 38<sup>2</sup> 36<sup>5</sup>  
6.7 6.7 6.5  
15.0 6.7 15.0

U.S.G.S. El Monte pump plant.

cor. 1  
445.13

30

~~314~~

~~7.8~~

~~437.3~~

~~31.60~~

~~31.40~~

~~+50~~

~~7.7~~

~~36.9~~

~~31.50~~

~~31.25~~

~~315~~

~~8.1~~

~~37.0~~

~~431.40~~

~~31.10~~

~~T.P.~~

~~393~~

~~41.43~~

~~7.63~~

~~37.50~~

~~+50~~

~~4.4~~

~~37.0~~

~~31.30~~

~~30.95~~

~~316~~

~~4.5~~

~~36.9~~

~~31.20~~

~~30.80~~

~~316 + 05.13~~

~~316 + 00~~

~~31.19~~

~~+50~~

~~4.7~~

~~36.7~~

~~31.09~~

~~30.65~~

~~317~~

~~5.0~~

~~36.4~~

~~30.99~~

~~30.50~~

~~+50~~

~~5.0~~

~~36.4~~

~~30.89~~

~~30.35~~

~~0.22%~~

~~-0.198%~~

	✓ 441.43			
318		5.2	✓ 436.2	30.80 <del>30.80</del>
		L		
+50		5.3	✓ 36.1	30.70 <del>30.05</del>
319		5.4	✓ 36.0	30.60 <del>29.90</del>
+50		5.3	✓ 36.1	30.50 <del>29.75</del>
320	-0.198%	5.6	✓ 35.8	30.40 <del>29.80</del>
+50		5.6	✓ 35.8	30.30 <del>29.45</del>
321		5.8	✓ 35.6	30.20 <del>29.30</del>
+50		6.1	✓ 35.3	30.10 <del>29.15</del>
322		6.2	✓ 35.2	430.00 <del>29.00</del>

320+50 - 343+50 Changed by County Road Dist.

Book  $\frac{524}{58-61}$

441.43

322750 5.9 435.5 30.05  
~~27.85~~

T.P 5.30 41.04 5.69 35.74

323 5.6 35.4 30.10  
~~28.70~~

+50 6.0 35.0 30.15  
~~28.55~~

324 5.8 35.2 30.20  
~~428.40~~

+50 5.7 35.3 30.25  
~~28.90~~

325 5.4 35.6 30.30  
~~29.40~~

+50 5.1 35.9 430.35  
~~29.90~~

326 4.0 37.0 30.80  
~~30.10~~

+0.10%

+0.70%

441.04				
326+50	2.8	438.2	31.25	<del>30.90</del>
327	2.5	38.8	31.70	31.40
+50	2.3	38.7	32.15	<del>31.90</del>
328	2.0	38.8	32.60	<del>32.40</del>
+50	2.0	39.0	33.05	<del>32.90</del>
329	0.9	40.1	33.50	<del>33.40</del>
T.P. +50	5.90	46.71	0.23	40.81
+50	5.2	41.5	33.95	<del>33.90</del>
330	4.5	42.2	434.40	<del>434.40</del>

+0.90%

446.71 ✓

330+50	4.5	442.2 ✓	34.5
331	4.8	41.9 ✓	34.90
+50	5.0	41.7 ✓	35.15
332	5.0	41.7 ✓	35.40
+50	4.3	42.4 ✓	35.65
333 x	3.4	43.3 ✓	35.90
+50	2.1	44.6 ✓	37.64 38.10
334	0.6	46.1 ✓	39.89 40.30
T.P.	12.64	58.80 ✓	0.55 46.16 ✓

✓  
458.80

334+50	107	✓ 448.1	42.13 <del>42.50</del>
335	8.5	✓ 50.3	44.37 <del>44.70</del>
+50	6.0	✓ 57.8	46.62 <del>46.90</del>
336	2.9	✓ 55.9	48.86 <del>49.10</del>
+50	0.6	✓ 58.7	51.10 <del>51.90</del>
T.P.	10.72	✓ 69.10	0.22 58.38
337	9.2	✓ 59.9	53.35 <del>53.50</del>
+50	7.3	✓ 61.8	55.59 <del>55.70</del>
338	5.1	✓ 64.0	57.83 <del>57.90</del>

+4.4878

4 2 RT

35

	469.10			
338+50	2.9	466.2	60.68	
+15			461.20	
339	1.0	68.1	62.07	
T.P.	12.02	80.5	0.47	68.63
+50	10.3	70.3	63.82	
340	7.9	74.7	65.57	
+50	5.2	75.4	67.32	
+15			468.20	
341	1.5	79.1	68.65	
			68.45	
+50	11.3	81.9	69.55	
+15			68.95	
342	0.5	80.1	69.89	
			69.45	
+20		81.1		

44.487%  
3.05%  
1.00%  
-0.44%

See Book 503 page 18-20  
for x-sections class 2 Exc.

6.0	6.0	2.8	4.1	2.8	5.0	8.0
6.5	6.5	2.4	2.8	5.0	8.0	
11.8	13.8	2.8	4.0	7.0	14.9	
8.1	14.4	2.8	7.0	15.0		
9.1	9.1	2.8	0.8	10.7	14.7	15.4
2.8	9.8	7.5	13.0	1.0	14.3	15.0
2.9	9.5	0.7	10.7	0.8	12.5	13.6
2.8	9.2	1.5	11.5	2.9	12.7	13.0



(Plans for line change)  
Book 479 page 59

180.65

342+50

2.2

78.5  
~~80.9~~  
478.4

69.67  
~~69.75~~

+75

79.4

69.56

343

(Coincident on page 59)

4.0

78.4

76.6

69.45  
~~70.05~~

Lindo Lake Route - Void

~~28~~  
+50

4.3

76.3

+50

4.0

75.7

76.6

69.23

~~69.75~~

B.M.

3.31 79.57  
Pole # 78772

4.39

76.26

(76.23)

book 505 P 47

344

-44%

5.0

74.4

74.0

69.01

69.45

+50

7.1

73.6

72.5

68.79

69.15

345

7.2

74.5

72.4

68.57

68.85

+50

7.5

74.7

72.1

68.35

68.55

IT C RT

37

Void - see page 59

~~74 84 108 115 120~~  
~~29 16 25 110 28 60~~

~~74 85 92 97 99~~  
~~30 29 28 60~~

84

(Elev. for line change)  
Back 479 - 57

✓  
479.57

346	6.8	75.4 ✓ 72.8	68.13 68.25
+50	6.4	75.8 ✓ 73.2	67.91 67.95
+75			467.80
347	6.1	76.1 ✓ 73.5	67.45
+50	5.7	75.5 ✓ 73.9	66.75
348	6.5	74.8 ✓ 73.1	66.05
+50	7.1	73.5 ✓ 72.5	65.35
+75			465.00
349	7.9	72.2 ✓ 71.7	63.97
+30	9.0	✓ 70.6	
+34	12.0	✓ 67.6	

-0.44%

-1.40%

-4.11%

LT      ♀      RT

(Elevs for line change)  
Book 479 - 57

479.57

349+50

12.2 70.8 ✓  
467.2 61.91

+75

69.8 ✓  
60.78

+87

12.3 67.3

+95

68.9 ✓  
64.7 60.06

350

12.8 66.8 59.85

+18

64.2 ✓  
59.11

T.P.

0.04

66.86 12.75 66.82

+50

-4.16%

7 63.8 ✓  
65.2 57.80

351

4.3 61.9 ✓  
62.6 55.74

$\frac{351+41.80}{351+58.00} = \text{Equation}$

+56

6.5 60.0 ✓  
60.2

352

8.8 58.1 ✓  
52.29

+59

11.0 55.9 ✓  
50.23

W Q R

8.9

$\frac{52}{60} \frac{5.1}{4.0} \frac{13.7}{2.8} 9.0$

$\frac{4.0}{60} \frac{5.0}{2.8} \frac{5.0}{1.0} 8.8$

4.9

$\frac{6.4}{6.0} \frac{6.0}{2.8} 5.1 \frac{5.0}{2.8} \frac{8.6}{3.0} \frac{8.6}{6.0}$

$\frac{6.6}{6.0} \frac{6.5}{2.8} \frac{6.5}{1.0} 6.0 \frac{5.3}{2.8} \frac{5.3}{6.0}$

6.2

	✓			
	466.86			
353	13.3	✓ 453.6	48.17	
T.P.	0.04	✓ 53.98	12.92	✓ 53.94
+50	2.5	✓ 51.5	46.12	
354	4.3	✓ 49.7	44.06	
+50	5.5	✓ 48.5	442.00	
355	6.6	✓ 47.4	41.40	
+50	7.3	✓ 46.7	40.80	
356	8.3	✓ 45.7	40.20	
+50	9.0	✓ 45.0	39.60	

-4.1168  
 -1.208

4 0 11

70

45398 ✓

<del>357</del>		9.5	44.5 ✓	39.00
+50		10.1	43.9 ✓	38.40
358		10.7	43.3 ✓	37.80
+50		11.3	42.7 ✓	37.20
359		11.8	42.2 ✓	36.60
T.P.	1.06	43.32 ✓	11.72 ✓	42.26 ✓ 37.26
+50		1.8	41.5 ✓	436.00
360		2.5	40.8 ✓	33.5 <del>37.8</del>
40 <del>+50</del>		2.3	41.0 ✓	

-1.20%

-5.0%

360	+43	6.9	436.4	✓
+50		7.9	35.4	✓
+57		7.0	36.3	✓
+59		2.5	40.8	✓
361		3.4	39.9	✓
+50		5.3	38.0	✓
362		7.9	35.4	✓
+50		9.7	33.6	✓
363		11.0	32.3	✓

443.32 ✓  
 431.00 ✓  
 431.60 ✓

500.5  
 -500.8

443.32 ✓

43 ✓

~~363 +50~~

~~12.0 431.3 ✓~~

~~B.M.~~

~~11.23 32.09 (32.09) ✓~~

~~book 505 40 ✓~~

~~364~~

~~12.9 30.4 ✓~~

~~+50~~

~~13.9 29.4 ✓~~

~~T.P.~~

~~8.45~~

~~38.74 ✓~~

~~13.03 ✓~~

~~30.29 ✓~~

~~365~~

~~9.9 28.8 ✓~~

~~+50~~

~~9.6 29.1 ✓~~

~~366~~

~~8.2 30.5 ✓~~

~~+50~~

~~6.5 32.2 ✓~~

✓  
438.74

367

5.2 433.5 ✓

+50

5.0 33.7 ✓

368

5.3 33.4 ✓

+50

5.7 33.0 ✓

369

6.2 32.5 ✓

+50

6.5 32.2 ✓

370

7.0 31.7 ✓

+50

7.8 30.9 ✓

T.P.

0.35 31.61 7.48 31.26 ✓



✓  
431.61

371 1.8 429.8 ✓

+50 2.5 29.1 ✓

372 2.8 28.8 ✓

+50 4.8 26.8 ✓

373 5.7 25.9 ✓

+50 7.3 24.3 ✓

374 8.7 22.9 ✓

+50 9.8 21.8 ✓

375 10.3 21.3 ✓

45

✓  
13161

~~375~~+50

11.3 470.3 ✓

~~376~~

11.8 19.8 ✓

~~+50~~

10.9 20.7 ✓

~~377~~

10.8 20.8 ✓

~~+50~~

11.0 20.6 ✓

~~378~~

12.0 19.6 ✓

T.P. 1.35 21.49 ✓ 11.47 ✓ 20.14 ✓

~~+50~~

2.7 18.8 ✓

~~379~~

2.0 19.5 ✓

16

(Profile on line change)  
Book 508 page 77

47

✓  
421.49

~~379+50~~

~~2.3 419.7 ✓~~

~~380~~

~~2.7 18.8 ✓~~

~~+50~~

~~3.7 17.8 ✓~~

~~381~~

~~4.5 17.0 ✓~~

~~+50~~

~~5.0 15.9 ✓  
16.5 ✓~~

~~382~~

~~6.8 14.6 ✓  
14.7 ✓~~

~~+50~~

~~7.7 13.7 ✓  
13.8 ✓~~

~~383~~

~~8.6 13.2 ✓  
12.9 ✓~~

~~+50~~

~~9.3 12.6 ✓  
12.7 ✓~~

(Profile on line change)  
Book 508 page 77

48

✓  
121.49

~~384~~

8.8

11.5 ✓

~~12.7~~

+50

11.0

09.4 ✓

~~10.5~~

T.P.

1.15

✓  
10.04

12.60

✓  
08.89

B.M.

0.91

✓  
10.03

410.04

Sta 385 + 25 +  
Exc Stump book 505 P 34

385

3.2

06.3 ✓

~~06.8~~

+50

6.4

03.4 ✓

~~03.6~~

+75

7.9

✓  
02.1

386

8.2

02.7 ✓

~~01.8~~

+16

02.0 ✓

~~+33~~

~~8.2~~

~~01.8~~

+22

00.8

(Profile on line change)  
book 508 page 77

79

✓  
410.04

~~386~~ ✓

9.3 400.7 ✓

+50

9.5 <sup>00.2</sup> ✓  
00.5

387

11.2 <sup>98.6</sup> ✓  
398.8

T.P.

0.65

399.55

11.14

398.90 ✓

+50

2.8

96.5 ✓  
96.8

388

4.9

94.4 ✓  
94.7

+50

6.7

92.8 ✓  
92.9

+60.18

389

8.3

92.1 ✓  
91.3

+50

8.6

✓  
91.0

399.55 ✓

~~390~~

88 390.8 ✓

~~+50~~

9.0 90.6 ✓

~~391~~

9.0 90.6 ✓

~~T.P.~~

~~4.56~~

~~95.19~~

~~892~~

~~90.63~~ ✓

~~+50~~

~~4.7~~

~~90.5~~ ✓

~~392~~

~~4.7~~

~~90.5~~ ✓

~~+50~~

~~4.6~~

~~90.6~~ ✓

~~393~~

~~4.7~~

~~90.5~~ ✓

~~+50~~

~~4.8~~

~~90.4~~ ✓

50

✓  
395.19

~~394~~

4.8

✓  
390.4

+50

4.7

✓  
90.5

395

4.7

✓  
90.5

+50

4.7

✓  
90.5

396

4.4

✓  
90.8

T.P.

12.43

✓  
403.36

4.26

✓  
90.93

+50

6.9

✓  
396.5

T.P.

8.48

✓  
11.71

0.13

✓  
03.23

397

3.8

✓  
07.9

51

	✓ 411.71	
397+02	3.2	✓ 408.5
+35	3.5	✓ 08.7
+37	2.0	✓ 09.7
+50	2.0	✓ 09.7
398	5.0	✓ 06.7
+18	6.3	✓ 05.4
+19	8.0	✓ 03.7
+50	9.0	✓ 407.7
399	13.8	✓ 397.9



✓  
411.71

~~399~~+50

15.3 396.4 ✓

400

9.4 402.7 ✓

+22

9.0 02.7 ✓

+24

7.1 04.6 ✓

T.P.

5.31

07.96

9.06

02.65 ✓

+50

2.1

05.9  
06.9 ✓

401

3.3 04.7 ✓

+22

5.0 03.0 ✓

+24

6.8 01.2 ✓

53

✓  
407.96

401+50

8.2 399.8 ✓

402

12.9 95.1 ✓

TP

11.72

✓  
06.79

12.89

95.07 ✓

+50

13.3

393.5 ✓

403

16.7

90.1 ✓

+50

16.7

90.1 ✓

404

15.8

91.0 ✓

+50

9.8

397.0 ✓

405

3.8

403.0 ✓

34

	✓ 406.79		
T.P	8.34	✓ 14.36	0.77 06.02 ✓
405+40		6.2	08.7 ✓
+50		5.6	08.8 ✓
+80		4.5	09.9 ✓
406		4.6	09.8 ✓
+50		7.5	06.9 ✓
407		9.8	04.6 ✓
+50		9.5	04.9 ✓
408		8.0	06.4 ✓

414.36

~~408+50~~~~5.0 09.12~~~~409~~~~2.0 12.14~~~~+50~~~~0.6 13.8~~~~TP.~~~~6.23~~~~80.02~~~~0.57~~~~13.79~~~~410~~~~5.8~~~~14.2~~~~+50~~~~5.4~~~~14.6~~~~411~~~~5.1~~~~14.9~~~~+50~~~~4.5~~~~15.5~~~~+58~~~~Pav.~~~~4.08~~~~15.94~~

470.02 ✓

411+93 Par. 5.42 14.60 ✓

412 5.6 14.4 ✓

+50 6.0 14.0 ✓

413 6.8 13.7 ✓

+50 7.9 12.1 ✓

414 9.6 10.4 ✓

T.P. 0.49 11.17 9.34 10.68 ✓

+50 2.1 09.1 ✓

415 3.4 07.8 ✓

✓  
411.17

<del>415+50</del>			<del>6.0</del>	<del>405.2</del>	✓
<del>416</del>			<del>7.8</del>	<del>03.4</del>	✓
<del>+50</del>			<del>9.0</del>	<del>02.2</del>	✓
<del>417</del>			<del>9.5</del>	<del>01.7</del>	✓
<del>+50</del>			<del>9.5</del>	<del>01.7</del>	✓
<del>418</del>			<del>9.7</del>	<del>01.5</del>	✓
T.P.	2.71	04.70	9.18	01.99	✓
B.M.			4.62	400.08 (400.13)	✓

Co. B.M. book 505 P. 26

Reduced & checked  
G.W.G. Aug. 15, 1935.

Profile levels, El Capitan Pipe line location  
on Julian Ave.

B.M.				
File # 78772	0.74	476.97	476.23	
<del>342+98.23</del>		0.3	476.7	✓
<del>343</del>			76.6	
<del>343+50</del>		2.3	474.7	✓
<del>344</del>		4.2	472.8	✓
<del>+50</del>		6.0	471.0	✓
<del>345</del>		7.9	469.1	✓
<del>+50</del>		9.7	467.3	✓
<del>346</del>		11.1	465.9	✓
<del>TP.</del>	0.93	466.75	11.15	465.82
<del>346+50</del>		2.3	464.4	✓
<del>347</del>		2.5	464.2	✓
<del>+50</del>		2.8	463.9	✓
<del>348</del>		3.7	463.0	✓
<del>+50</del>		4.1	462.6	✓
<del>349</del>		5.2	461.5	✓
<del>+50</del>		6.3	460.4	✓
<del>350</del>		6.9	459.8	✓

Sept. 30-34  
H. H.  
Soper - level left.  
Remmen - rod

F.B. 524 H.F.S.  
58-61

Q	R	59
476.8	478.0	478.1
02	+10	+12
30	10	60
21 476.9	03 476.7	04 476.6
30	20	13 475.7
40 473.0	20 475.0	40
30	30	30 474.0
58 471.2	42 471.8	70
30	10	40 473.0
79 469.1	50 472.0	49 471.1
30	20	30
96 467.2	81 468.9	50 472.0
30	10	30
109 466.1	98 467.2	69 470.1
30	10	30
		85 468.5
		30
		96 467.2
		70
464.7	465.9	466.7
20	08	00
30	10	50

Level

Book 503 page for Class 2 Excavation

Book 524 Changed by County  
65-66

Reduced 4  
H.V.N.

350+50		7.4	459.3 ✓
351		7.7	459.0 ✓
351+40		7.1	459.6 ✓
+50		8.5	458.2 ✓
+65		11.9	454.8 ✓
+70		11.8	454.9 ✓
+80		8.8	457.9 ✓
352		8.3	458.4 ✓
TP.	5.37	464.42	7.70 459.05 ✓
Van B.M. #33		4.33	460.09 (460.15) ✓
B.M. #33	4.33	464.48	460.15 ✓
352+50		5.9	458.6 ✓
353		5.5	459.0 ✓
+50		5.3	459.2 ✓
354		4.7	459.8 ✓
+50		4.1	460.4 ✓
355		3.4	461.1 ✓

466.75 ✓



Left

Q

Right

60

524/65

459.6 ✓

459.3 ✓

$$\frac{72}{30} 459.6$$

$$\frac{74}{30} 459.3$$

$$\frac{72}{40} 459.5$$

$$\frac{86}{30} 458.7$$

Level

Flow line of

$$\frac{72}{30} 459.0$$

$$\frac{98}{30}$$
456.9 ✓  
Quail Creek

Level

524/65

Rock # 316

Used old elev.

Reduced & ✓  
N.Y.N.



464.48 ✓

<del>355</del>			2.8	461.7	✓
356			2.1	462.4	✓
+50			1.9	462.6	✓
357			2.9	461.6	✓
T.P.	0.69	464.64 ✓	0.53	463.95	✓
+50			3.2	461.4	✓
358			4.3	460.3	✓
+50			5.3	459.3	✓
359			6.1	458.5	✓
+50			6.9	457.7	✓
360			7.7	456.9	✓
+50			8.6	456.0	✓
361			9.4	455.2	✓
+50			10.2	454.4	✓
362			11.0	453.6	✓
T.P.	0.80	454.45 ✓	10.99	453.65	✓
+50			1.5	453.0	✓

Reduced +  
H.V.N. ✓

454.45 ✓

363		2.2	452.3 ✓
+50		2.8	451.7 ✓
364		3.4	451.1 ✓
+50		4.0	450.5 ✓
365		4.4	450.1 ✓
+50		4.8	449.7 ✓
366		5.0	449.5 ✓
+50		5.4	449.1 ✓
		7.6 →	446.9 ✓
367		5.4	449.1 ✓
+50		4.1	450.4 ✓
+90		3.3	451.2 ✓
368		0.8	453.7 ✓
+50		2.0	452.5 ✓
+60		5.2	449.3 ✓
369		7.1	447.4 ✓
77	0.79	444.42	10.82 443.63 ✓
+50		1.1	443.3 ✓

Flyline-Covert  
(on right)To FB 524-67  
at 366+74

Left

E

Right

62

Line relocated see Book 506-69

449.7 ✓	448.9 ✓	450.0 ✓	450.5 ✓
$\frac{53}{30}$	$\frac{55}{20}$	$\frac{45}{22}$	$\frac{40}{60}$
444.50.1 ✓	35 451.0 ✓	31 451.4 ✓	
$\frac{36}{30}$	$\frac{08}{20}$	$\frac{+22}{60}$	456.7 ✓
35 451.0 ✓	32 451.3 ✓	+0.6 455.1 ✓	+2.7 457.7 ✓
$\frac{50}{30}$	$\frac{50}{70}$	$\frac{+15}{40}$	$\frac{+62}{90}$
449.7 ✓	449.5 ✓	456.7 ✓	460.7 ✓
$\frac{53}{30}$	$\frac{30}{02}$	$\frac{+10}{60}$	455.5 ✓
69 447.6 ✓	74 447.1 ✓	46 449.9 ✓	30 450.9 ✓
$\frac{30}{30}$	$\frac{20}{20}$	$\frac{30}{30}$	$\frac{60}{60}$

Level

Reduced to  
H.V.N.

444.42

370		3.9	440.5	✓
+50		5.4	439.0	✓
371		6.4	438.0	✓
+50		6.5	437.9	✓
372		6.0	438.4	✓
+50		6.6	437.8	✓
373		8.6	435.8	✓
+50		10.8	433.6	✓
374		12.5	431.9	✓
TP.	1.76	433.19	12.99	431.43
r.B.M. #35		0.01	433.18	(433.07)
B.M. #35	0.01	433.08		433.07
374+50		2.5	430.6	✓
375		3.8	429.3	✓
+50		7.0	426.1	✓
376		10.0	423.1	✓
+50		12.7	420.4	✓

Book # 316

used old elev.

Reduced + ✓  
H.V.N.

		433.08 <sup>✓</sup>		
TP.	0.28	420.42 <sup>✓</sup>	12.94	420.14 <sup>✓</sup>
377			2.0	418.4 <sup>✓</sup>
+50			3.6	416.8 <sup>✓</sup>
378			5.0	415.4 <sup>✓</sup>
+50			5.8	414.6 <sup>✓</sup>
379			6.5	413.9 <sup>✓</sup>
+50			7.2	413.2 <sup>✓</sup>
380			7.8	412.6 <sup>✓</sup>
+50			8.5	411.9 <sup>✓</sup>
381			9.3	411.1 <sup>✓</sup>
+50			9.9	410.5 <sup>✓</sup>
TP.	1.90	412.31 <sup>✓</sup>	10.01	410.41 <sup>✓</sup>
382			2.6	409.7 <sup>✓</sup>
+50			3.1	409.2 <sup>✓</sup>
383			3.3	409.0 <sup>✓</sup>
+50			3.6	408.7 <sup>✓</sup>
384			3.9	408.4 <sup>✓</sup>

Reduced & v  
H.V.N.

412.31<sup>✓</sup>

<del>384+50</del>			3.8	408.5 <sup>✓</sup>	
<del>385</del>			3.8	408.5 <sup>✓</sup>	
<del>+50</del>			5.0	407.3 <sup>✓</sup>	
<del>386</del>			6.6	405.7 <sup>✓</sup>	
<del>+50</del>			7.7	404.6 <sup>✓</sup>	
<del>387.</del>			8.3	404.0 <sup>✓</sup>	
<del>+50</del>			8.4	403.9 <sup>✓</sup>	
<del>387+72</del>			11.5	400.8 <sup>✓</sup>	Flow line
<del>387+72</del>			10.8	401.5 <sup>✓</sup>	" " " "
<del>388</del>			8.6	403.7 <sup>✓</sup>	C.I. Culvert 17 <sup>5</sup> right
<del>+50</del>			8.9	403.4 <sup>✓</sup>	" " " "
<del>389</del>			8.1	404.2 <sup>✓</sup>	C.I. Culvert 12 <sup>5</sup> left.
TP and Check on B.M. #36	12.81	416.66 <sup>✓</sup>	8.46	403.85 (403.86) <sup>✓</sup>	Book # 316
+50			10.7	406.0 <sup>✓</sup>	
390			7.4	409.3 <sup>✓</sup>	
+50			4.0	412.7 <sup>✓</sup>	
391			1.0	415.7 <sup>✓</sup>	

Reduced +<sup>✓</sup>  
H.V.N.

		416.66			
TP	11.33	427. <sup>70</sup> <del>50</del>	0.29	416.37	✓
391+50			9.8	417.9	✓
392			8.0	19.7	✓
+39			10.7	17.0	✓ Flowline of 14' C.I. Culvert 19' Right
+49			8.4	19.3	✓ " " " " 12' Left.
+50			6.2	21.5	✓
393			5.0	22.7	✓
+50			4.0	23.7	✓
394			2.7	25.0	✓
+50			1.1	26.6	✓
TP	9.17	436. <sup>39</sup> <del>79</del>	0.48	427. <sup>22</sup> <del>82</del>	✓
395			8.4	428.0	✓
+50			7.5	28.9	✓
396			6.9	29.5	✓
+50			6.2	30.2	✓
397			5.5	30.9	✓
+50			5.0	31.4	✓

Reduced +  
G.W.G.

39 ✓  
436.79

398		4.5	431.9	✓
+50		4.3	32.1	✓
399		4.2	32.2	✓
+50		3.9	32.5	✓
400		4.6	31.8	✓
+50		5.5	30.9	✓
401		6.4	30.0	✓
+50		7.3	29.1	✓
402		8.1	28.3	✓
TP	0.59	<sup>93</sup> 427.73	<sup>34</sup> 9.05 427.74	✓
+50		0.8	427.1	✓
403		2.3	25.6	✓
+50		4.1	23.8	✓
404		5.7	22.2	✓
+50		7.3	20.6	✓
405		8.5	19.4	✓
+50		9.6	18.3	✓

Reduced + ✓  
G.W.G.

93  
427.73

406		10.4	417.5	✓
+50		10.9	17.0	✓
TP	7.27	<del>423.91</del>	11.09	416.64 <sup>84</sup>
407		7.3	416.8	✓
+50		7.3	16.8	✓
+87		10.0	14.1	Flow ✓
+99		9.3	14.8	✓
408		7.2	16.9	✓
+50		6.4	17.7	✓
409		4.8	19.3	✓
+50		4.0	20.1	✓
410		4.1	20.0	✓
+50		6.2	17.9	✓
L.B.M. #38		7.13	416.78 (416.89) <sup>98</sup>	✓
B.M. #38	1.24	418.13 <sup>✓</sup>	<del>416.89</del>	
411		1.3	416.9	✓

line of 14" C.I. Culvert 16' Right

" " " 17' Left

Line change see  $\frac{516}{65}$

Bank = 3/6

used old elev.

68  
Reduced + ✓  
G.W.C.



22  
418.73

411+50		1.9	416.3	✓	
412		3.6	14.6	✓	
+50		5.5	17.7	✓	
413		6.9	11.3	✓	
+50		8.0	10.2	✓	
414		8.8	09.4	✓	
+50		9.1	09.1	✓	
415		9.4	08.8	✓	
TP.	3.61	<del>413.05</del> 412.99	8.81	41 409.32	✓
+50		4.5	408.5	✓	
416		4.7	08.3	✓	
+50		5.0	08.0	✓	
417		5.3	07.7	✓	
+44		8.0	05.0	✓	
+47		5.1	07.9	✓	
+50		5.5	07.5	✓	
418		5.5	07.5	✓	

Flow line of 14" C.I. Culvert 13<sup>E</sup> Right

23 Left

Reduced + ✓  
G.W.G.

413.02  
412.93

418+50		5.4	407.6	✓
419		5.4	07.6	✓
+50		5.4	07.6	✓
420		5.9	07.1	✓
TP.	4.56	412. <sup>24</sup> 75	534	407. <sup>68</sup> 59 ✓
+50		5.4	406.8	✓
421		5.5	06.7	✓
+50		5.3	06.9	✓
422		4.1	08.1	✓
+50		3.3	08.9	✓
+88'		2.3	09.9	✓
423+08 <sup>2</sup>		2.5	09.7	✓
423+22 <sup>19</sup> Δ		2.6	09.6	✓
+50		3.5	08.7	✓
TP.	0.79	409. <sup>50</sup> 71	353	408. <sup>71</sup> 62 ✓
424		2.4	407.1	✓
+50		4.8	04.7	✓

Edge of concrete Highway

Reduced + ✓  
S.W.G.

.50 ✓  
409.41

425			6.2	403.3	✓
+50			7.2	07.3	✓
426			7.6	01.9	✓
+50			7.7	01.8	✓
426+90 <sup>18</sup>			8.0	01.51	✓
418+00 <sup>90</sup>				90	
T.P.	3.07	404.97	7.60	401.80	
			4.80	400.97	17

County B.M. # 21 - El. 400.22

422+80.5 - 4" steel water main. 407.7

423+72.5 - 2 1/2" " " " 406.3

Reduced + ✓  
S.W.G.

Notes Copied from Street paper apparently sent into office

Profile of Portions of Co Road Survey 606

Crossing Linda Lake at Lakeside 6/6/35

Sta	+	x	-	Elev.	Assumed
7+00				100.0	"
	2.00			102.00	
7+40	<sup>Water</sup> Edge West Bank		7.1	94.9	Water Surface
	+50		8.2	93.8	
8+00			8.8	93.2	
	+50		8.4	93.6	

Contd in Orig Profile Notes

15+00	4.0			104.0	100.0 Assumed Elev
15+45	Edge Water West Bank		9.9	94.1	Water Surface
	+50		10.4	93.6	
16			10.9	93.1	
17			11.1	92.9	
18			11.0	93.0	
19			11.1	92.9	
20			11.0	93.0	
21			10.9	93.1	
22			10.5	93.5	

Contd in Orig Profile Notes.

Check levels near El Monte  
Pump plant.

Saper  
Rimmon

Nov. 29, 1935

75

U.S.G.S.

B.M.

~~439.83~~

~~5.85 445.68~~

Check Levels B.M. #27 to U.S.G.S.

B.M. #27 1.83 459.87 458.04

TP 6.03 453.84

2.56 456.40

TP 9.01 447.39

7.72 455.11

TP 7.57 447.54

1.93 ~~448.77~~  
49.47

TP 6.71 444.76  
442.76

4.48 447.24  
446.24

TP 5.41 441.83  
440.83

2.10 443.93  
442.93

TP 4.61 439.32  
438.92

5.38 444.70  
~~443.70~~  
33.70

438.92

5.78 439.92

1.83	6.03	458.04
2.56	9.01	437.92
7.72	7.57	26.12
1.93	6.71	58.04
4.48	5.41	38.92
2.10	4.61	19.12
5.38	5.78	
26.00	45.12	
	26.00	
	19.12	

Elev. 438.95. Pipe line levels - 1931.  
U.S.G.S. marked Elev. 439.83

Check Levels - U.S.G.S to B.M. in pde. 78772

U.S.G.S.B.M. 3.03 442.86 439.83

TP. 5.40 437.46

4.04 441.50

TP. 5.13 436.37

4.64 441.01

TP 2.45 438.56

Discontinued -

Use elev. 438.93 at gauging station B.M.

Profile of line change at El Monte

Pumping station. Elevs changed on page 29

B.M.	5.89	444.82	438.93
309+33.09 B.C.	5.2	439.6	✓
+50	5.2	39.6	✓
+95	4.6	40.2	✓
310	4.8	40.0	✓
+50	5.3	39.5	✓
311	8.0	36.8	✓
+50	8.2	36.6	✓
312	8.5	36.3	✓
+07	8.5	36.3	✓
+12	6.1	38.7	✓
50	6.5	38.3	✓
313	7.0	37.8	✓
T.P.	5.89	438.93	✓
3.30	442.23		
+50	5.0	37.2	✓
314+04.76 P.I.	5.2	37.0	✓

Book 524  
69

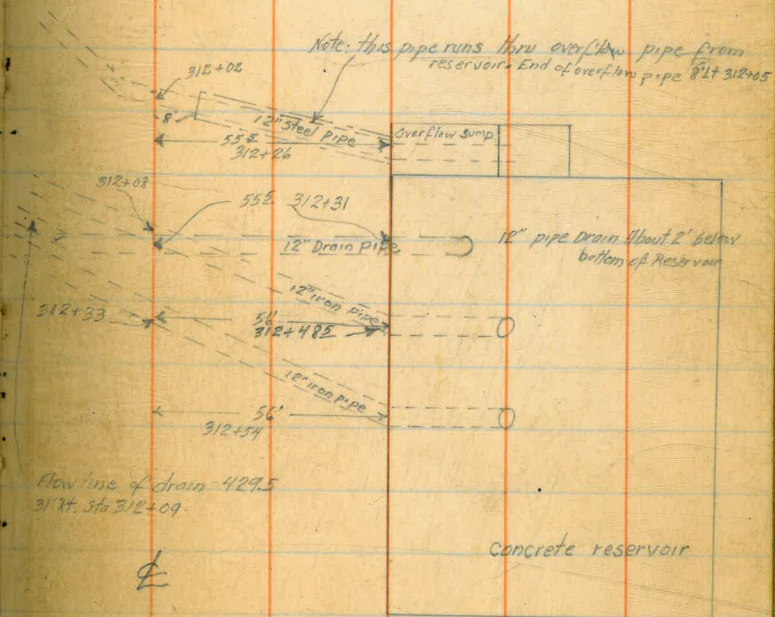
Book 524  
64

Book  $\frac{524}{64}$ 

442.23 ✓

<del>314+50</del>	<del>5.3</del>	<del>36.9</del> ✓	
<del>315</del>	<del>5.2</del>	<del>37.0</del> ✓	
<del>+50</del>	<del>5.2</del>	<del>37.0</del> ✓	
<del>316+0513</del>	<del>5.3</del>	<del>36.9</del> ✓	gr. elev. pr. levls, page 30, 436.9
<del>316+00</del>			

312+02	434.0	Flow line 12" steel pipe at $\phi$ of Pipeline
312+08	434.8	" " 12" iron pipe at $\phi$ "
312+26	435.4	" " 12" steel pipe 55' H $\phi$
312+33	433.0	" " 12" iron pipe at $\phi$ of Pipeline
312+48.5	435.6	" " 12" iron pipe 56' H $\phi$
312+54	435.6	" " 12" iron pipe 56' H $\phi$
	432.4	Elev. Bottom of Reservoir





Jan 2 1936  
Soil  
Removal

Profile Sta. 42+50 - 43+00

B.M.	2.37	571.25	568.88
P.		12.80	558.45
	2.10	560.85	
42+50		10.9	49.9
43+00		10.9	49.9

534 / 48

Jan 3 1936

Sepher  
Remmen

76

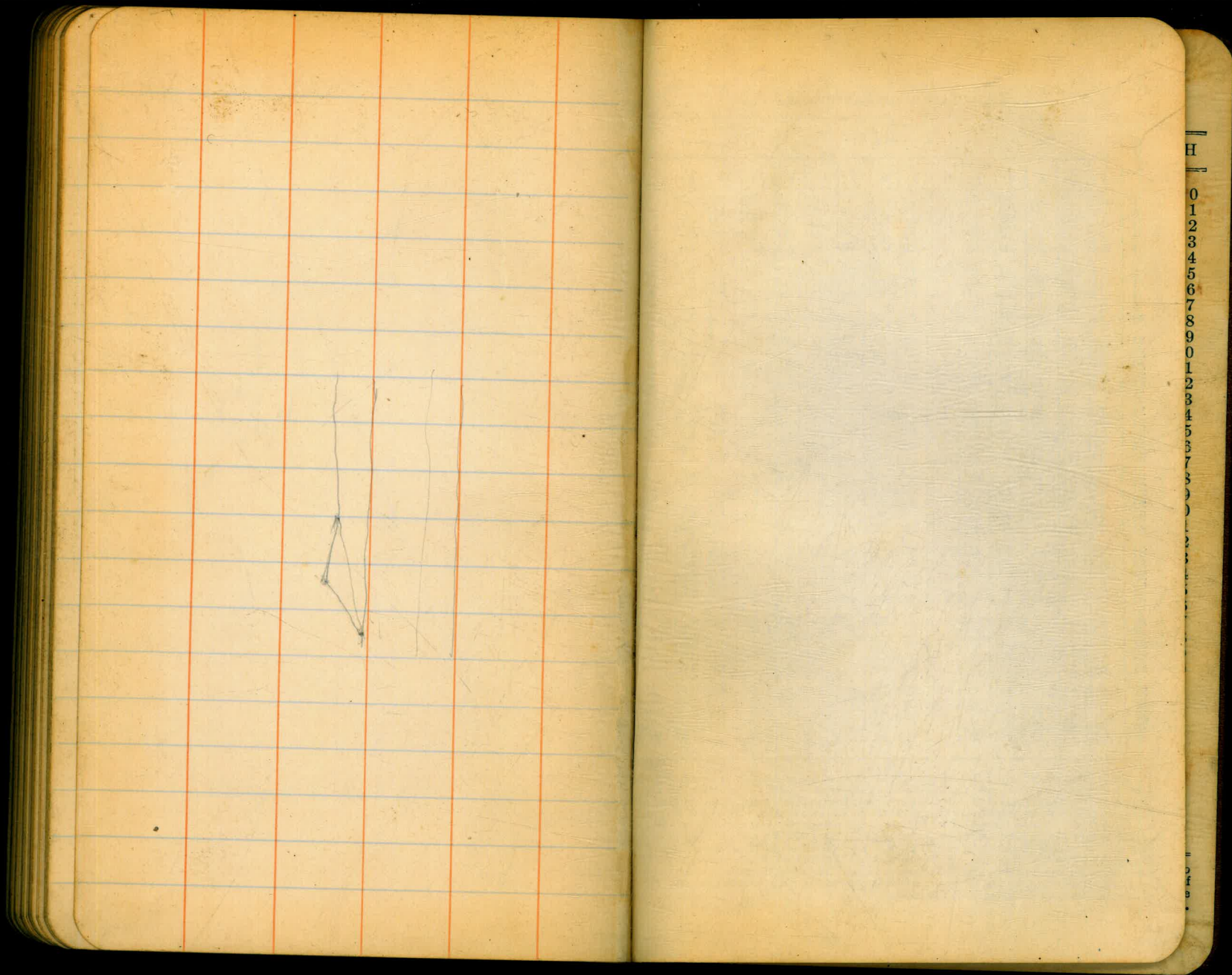
Re-profile Sta. 85+50 - 89+48.34

B.M	7.92	533.02	525.10
85+50		2.4	30.6
+83		1.3	31.7
86+00		2.0	31.0
+50		3.1	29.9
87+00		3.7	29.3
+50		7.2	25.8
+65		8.2	24.8
88+00		9.0	24.0
+50		10.2	22.8
89+00		10.4	22.6
+48.34 EC		10.4	22.6

See  
5<sup>th</sup>/<sub>13</sub><sup>th</sup>

Same elev's on rest of line change

Changed in Book 508 page 41



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