



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

510

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9		1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.

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Slope stakes

El Monte Park - El Capitan
road. County Survey # 606

Slope stakes Sta. 301 to 376 Pages 2-46

Slope stakes sta. 175 to 189. 48-53

" " " 153 " 161 55-58

" " " 294 " 300+50 59-60

" " " 242 " 265+50 61-66

" " " 224 " 241+50 67-70

" " " 219 " 223+50 71

" " " 161+50 " 174+50 72-74

" " " 132+50 " 152+50 75-79

" " " 291+00 292+50 - 79

Sta. of curves where Elev's are carried on

inside of curve for super-elevation 80

Xsec. + slope stakes Co. road from
Head prop. to dam.

Sta	L. El.	Grade	+5.4	G. Rod	stake	$\frac{f}{L}$	Louden	8/24/55	2
							Saper	Remmen	stake
303+25	12.8	15.07	18.2	-3.1	$\frac{10.5}{F 7.4}$ 28.1	$\frac{-3.0}{16}$	$\frac{-2.3}{0}$	$\frac{-1.3}{13}$	$\frac{3.1}{Gr.}$ 170
= 475	11.7	14.37	17.1	-2.8	$\frac{7.6}{F 6.8}$ 27.2	$\frac{-6.9}{20}$	$\frac{-3.0}{4}$	$\frac{-2.7}{0}$	$\frac{2.5}{CO. B}$ 18.1
302+25	12.6	14.01	18.0	-4.0	$\frac{11.2}{F 7.2}$ 27.8	$\frac{-7.0}{22}$	$\frac{-1.4}{0}$		$\frac{5.5}{F 1.5}$ 19.2
+75	11.1	13.76	16.6	-2.8	$\frac{18.1}{F 5.3}$ 24.9	$\frac{-5.0}{15}$	$\frac{-2.7}{0}$		$\frac{4.7}{F 1.9}$ 19.8
+50	10.1	13.68	14.9	-1.2	$\frac{7.0}{F 5.8}$ 25.7		$\frac{-3.6}{0}$		$\frac{3.4}{F 2.2}$ 20.3
301	509.8	13.52	15.2	+1.7	$\frac{8.1}{F 6.1}$ 26.6	$\frac{-5.2}{23}$	$\frac{-3.7}{0}$		$\frac{3.7}{F 2.0}$ 20

	± El.	Grade	Grad	Stake	±	Stake					
306	16.5	19.15	+7.3 23.8	-4.7	13.0 F 8.3 29.4	-0.2 23	-5.3 15	-2.6 -1.9 6	+2.8 17	3 2.0 C 2.7 19.3	
+50	16.1	18.29	5.4 21.5	-3.2	9.1 F 5.9 25.8	-5.4 15	-2.2 0	+0.4 9		1.6 C 1.6 18.8	
305	14.9	17.57	5.4 20.3	-2.7	7.7 F 5.0 24.5		-2.7 0	+1.5 8		+0.8 C 3.5 19.7	
+50	15.5	16.85	5.4 20.9	-4.1	9.1 F 5.0 24.5		-3.1 3	-1.3 0		1.8 C 2.3 19.1	
+25	14.5	16.4	+5.4 19.9	+3.5		-7.1 30	-4.6 17	-3.1 5	+1.9 0	+0.5 25	+1.5 30
304	11.2	16.14	+5.4 16.6	-0.5	4.3 F 3.8 20.7		-5.8 11	-4.9 0		2.4 F 1.9 19.8	
+80	13.4	15.8	+5.4 18.8	-3.0		-8.1 33	-4.2 25	-2.4 0	+1.9 5	+2.5 25	
303+50	12.5	15.43	+5.4 17.9	-2.4	10.1 F 7.7 28.6		-3.6 17	-2.9 0	+0.2 12		1.7 C 0.7 18.3

± El	Grade	G. rod.	super	stake
+29 ³⁰ 24.5	25.00	+5.4 29.9	4.9	4.4 30.5 +0.5 -0.5 18.2
308	23.7	+6.0 33.8 24.1 37.5	5.1 33.7 +0.4 -0.4	5.5 30.4 17.6

stake	±	stake
-0.6 3	+12.5 17.5	.80 22.5 29.2 5.4 C.28.3
-0.5 0.0 0 4 15.0	+15.5	32.1

Note- On super-elevated sections intermediate elevs. are referred to center-line grade.

+50	22.5	22.92	+5.4 +13.2 27.9 35.7	4.9 -12.1 -5.0 -12.8 +0.1 -0.1	4.9 18.0	-0.4 0	+2.5 C.15.4 25.7
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307	21.8	21.62	+8.3 +1.0 29.8 30.1	-2.2 -8.5R	2.2 Grade 17.0	+0.6 +0.2 +0.3 16 0 10	1.1 C.7.4 21.7
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3.7

306+50	21.8	20.31	+5.4 27.2	-6.9	16.3 F.9.1 31.1	-1.6 +0.7 +1.5 21 6 0	6.1 C.O.8 18.4
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	±EI.	Grade	G.rod Super				
		2.6	154		137.0	7.3	40.3
+50	33.4	30.77	38.8	8.0	39.6	+0.7	-0.7

Stake
52
62.1
19.0

±

$\frac{+2.6}{0} + \frac{+2.6}{4} + \frac{+25.4}{19.0}$

Stake
65
C 33.8
34.9

		1.7	154	+29.6		6.4	32.0	
310	31.2	29.46	36.6	60.8	7.1	31.3	+0.7	-0.7

56
60.8
18.4

$\frac{+0.9}{16} + \frac{+1.7}{0} + \frac{+1.5}{4} + \frac{+8.0}{13} + \frac{+20.5}{16}$

2.0
C 30.0
33.0

			+5.4	+32.5		5.2	33.7	
+50	28.6	28.15	34.0	61.1	5.9	32.0	+0.7	-0.7

55
F 0.3
17.4

$\frac{+0.5}{14} + \frac{+0.5}{0} + \frac{+0.7}{4} + \frac{+1.7}{12} + \frac{+18.1}{16}$

5.7
C 28.0
32.0

			+5.4	+28.0		4.7	28.7	
309	26.8	26.85	32.2	54.8	5.4	28.0	+0.7	-0.7

22.5
F 17.8
43.7

$\frac{-4.6}{25} - \frac{-1.3}{18} - \frac{-0.3}{16} + \frac{0}{0} + \frac{0}{7} + \frac{+7.1}{12}$

9.4
C 19.3
27.6

			5.4	+28.0		4.6	-28.4	
308+50	25.3	25.54	30.7	53.3	5.2	27.8	+0.6	-0.6

06
F 2.0
2.0.0

$\frac{-0.4}{18} - \frac{-0.4}{5} - \frac{-0.2}{0} + \frac{+10.5}{13}$

8.3
C 20.1
28.1

EEI Grade Grad Super

Stake

±

Stake

+50 40.3 33.76 ^{6.5} ^{+5.4 +22.8} 45.7 83.1 12.0 47.3 ^{14.0} ^{47.3} -2.0 +2.0

^{6.2}
C-7.8
21.9

^{+66+6.6+7.8} ^{+34.1}
0 6 13 23

^{4.9}
C-42.4
39.2

+13¹ B.C. 40.9 33.5 ^{5.9} 46.3 12.8 47.3 ^{14.4} ^{47.7} -1.6 +1.6

^{6.4}
C-8.0
22

^{+7.4+7.4+4.5} ^{+34.9}
0 -4 13 21

^{4.8}
C-42.9
39.5

312 40.9 33.43 -1.47 +1.4

311+50 39.9 32.83 ^{5.4 +45.2} 45.3 85.1 12.5 52.3 ^{12.8} ^{52.0} -3.3 +0.33

^{5.1}
C-7.7
21.8

^{+7.1} ^{+11.6} ^{+33.6}
0 7 12

^{2.6}
C-49.4
42.7

+9¹⁰ E.C. 35.9 31.73 ^{7.5.1} 41.3 9.6 ^{1.1} ^{50.3} +0.5 -0.5

^{5.3}
C-3.8
19.9

^{+3.1} ^{+4.2} ^{+8.0} ^{+28.4}
1 0 7 12

^{6.8}
C-44.0
40.0

+86²² EC 30.4 31.7 +49 67 6.5 40.8
72.3 40.6 +0.2 -0.2

+50 32.4 32.29 6 -0.4 +0.4

+40²⁹ EC 32.4 32.5 5.5 45.1 6.1 45.1
-0.6 +0.6

314 34.4 33.07 116 10.4 10.1
46.0 12.9 -1.5 +1.5

314+30 33.0 32.6

+50 36.9 33.59 42.3 82.1 8.7 48.5 10.7 46.5
-2.0 +2.0

313 38.8 33.82 44.2 10.4 12.4 8.4
-2.0 +2.0

~~C 0.9
5.4 18.5
C -1.1
18.6~~

~~E
-1.3 +1.5 +6.7
0 4 13~~

~~7
C 27.8 2.8
31.9 C -28.6
30.0~~

Note: Use E grade on inside of curve.

57
60.4
18.2

-0.1 0.0 +4.5 +19.5 11.3
0 2 9 15 C -33.8
34.9

11.8
C -2.6
19.3

+1.6 +1.3 +2.2
18 0 17

8.5
C -1.6
18.8

+0.6 -0.2 +0.4 +6.4 +13.0 +31
21 17 0 15 26 34

6.2
C -4.5
20.2

+33 +37 +87 +37.3 7.8
0 15 20 29 C -38.7
37.3

8.2
C -6.2
21.1

+5.0
0

5.3
C 3.1
19.5

?
 ↑
 +50 Balance Pt.
 Vok
 +50 26.9 28.58 32.3 77.7 3.7 49.1 +0.6 -0.6
54 +50.8 3.1 11.7

316 31.0 29.51 32.4 80.0 2.7 50.5 +0.7 -0.7
1.4 +49.0 2.2 51.2

+50 30.9 30.44 36.3 79.0 5.7 48.6 +0.7 -0.7
54 +48.1 5.2 49.2

+30 32.0 30.8

315 30.4 31.36 +0.4 -0.4

Stake

~~F 3.5
 22.3
 0
 F 2.9
 21.4~~

~~-0.5 -1.7 +7.5
 3 0 13~~

~~F 3.8
 22.7
 5.3
 F 3.1
 21.6~~

~~-2.4 +1.5 +40.0
 6 0 30~~

~~F 3.1
 21.7
 6
 F 2.4
 20.6~~

~~-1.8 +0.5 +32.4
 5 0 21~~

~~-2.0 -2.0 +1.2 +13.7 +26.7 +39
 26 4 0 16 21 40~~

~~-1.5 -1.5 -1.5 -1.0 +7.0 +25
 25 20 2 0 19 34~~

(Use & grade on inside of curve)

Stake

~~C 45.9
 40.9
 3.4
 C-46.3
 41.1~~

~~C 47.1
 41.6
 2.5
 C-49.4
 42.2~~

~~C 44.3
 40.2~~

~~4.3
 C-45.1
 40.5~~

#EI	Grade	54	46.7	Grid	Feet
318	25.4	26.40	31.8	72.1	44 45.7

Stroke
 $\frac{54}{18.7}$
 ~~$\frac{F-1.9}{18.5}$~~

Stroke
 $\frac{-1.0}{0}$ $\frac{+0.8}{1.3}$ $\frac{+35.0}{33}$ $\frac{10.2}{C-35.5}$
 35.7

+50	26.0	26.87	31.4	74.5	4.5	47.6	+0.1	-0.1
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~~$\frac{F1.1}{18.7}$~~
 ~~$\frac{54}{18.5}$~~

$\frac{+0.9}{0}$ $\frac{+1.5}{12}$ $\frac{+40.1}{36}$ $\frac{C41.9}{39.0}$
 ~~$\frac{54}{18.5}$~~
 39.0
~~39.0~~
 39.0

317	26.2	27.45	31.6	79.8	4.6	52.2	+0.3	-0.3
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~~$\frac{F2.2}{20.3}$~~
 ~~$\frac{54}{19.8}$~~

$\frac{+1.4}{0}$ $\frac{+51.7}{43.8}$

+71 ⁸⁸	E.C.	26.1	28.2	31.5	33	42.1	+0.5	-0.5
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~~$\frac{F3.1}{21.7}$~~
 ~~$\frac{54}{20.9}$~~

$\frac{-2.1}{0}$ $\frac{+7.4}{11}$ $\frac{+31.5}{25}$ $\frac{C46.8}{41.4}$
 ~~$\frac{54}{20.9}$~~
~~47.3~~
 47.6

(Use E grade on inside of curve)

E El Grade

G.rod Super Stake

E

10

stake

$\begin{array}{r} 14 \quad 32.6 \\ +50 \quad 21.7 \quad 26.64 \quad 31.1 \quad 62.3 \quad 4.5 \quad 35.7 \end{array}$

$\begin{array}{r} 7.4 \\ F-2.9 \\ \hline 21.4 \end{array}$

$\begin{array}{r} -3.2 \quad +3.1 \\ 7 \quad 0 \end{array}$

$\begin{array}{r} +15.8 \quad 4.2 \\ 8 \quad C-31.5 \\ \hline 33.7 \end{array}$

$\begin{array}{r} 54 \quad 39.9 \\ 319 \quad 25.7 \quad 26.36 \quad 31.1 \quad 65.6 \quad 4.7 \quad 39.2 \end{array}$

$\begin{array}{r} 6.8 \\ F-2.1 \\ \hline 20.1 \end{array}$

$\begin{array}{r} -2.5 \quad -0.7 \quad +8.0 \quad +21.8 \quad 11.3 \\ 3 \quad 0 \quad 16 \quad 23 \quad C-21.9 \\ \hline 31.9 \end{array}$

$\begin{array}{r} 54 \quad 36.4 \\ 318+50 \quad 24.7 \quad 26.23 \quad 30.1 \quad 61.1 \quad 3.7 \quad 35.9 \end{array}$

$\begin{array}{r} 5.3 \\ F-1.4 \\ \hline 19.1 \end{array}$

$\begin{array}{r} -1.5 \quad +0.7 \\ 0 \quad 9 \quad 26.2 \quad 4.3 \\ 24 \quad C-31.6 \\ \hline 33.8 \end{array}$

EE Grade

Grad Super

Stake

⊕

11

Stake

L
 + 27⁴¹ BC 23.1 27.7 28.5 49.4 0.8 21.7 -0.5 +0.5

63
 F 5.0
 24.5

-4.6 -4.6 +4.8
 0 4 10

13.0
 C - 8.7
 22.1

321 22.9 27.48 28.3 49.3 0.8 21.8 -0.3 +0.3

55
 F 4.4
 23.6

-4.6 -4.5 -2.4 +11.5 6.0
 0 3 12 12 C - 15.5
 25.7

+50 26.4 27.20 28.6 53.9 1.4 26.7 -0.1 +0.1

53
 F 3.9
 22.9

-3.9 -0.8
 7 0

+15.6 8.8
 C - 17.8
 22 26.9

370 27.2 26.92 28.4 68.7 1.5 41.8

51
 F 3.6
 22.4

-3.9 +0.3
 7 0

+19.4 1.6
 14 C - 40.2
 38.1

E

324 31.1 29.16 36.5⁺⁵⁴ 7.3 8.0 66
-0.7 +0.7

G.C
C-1.4
18.7

+1.1
+1.9
0

3.5
C-3.1
19.6

+50 28.5 28.88 33.5 36.0 4.6 7.1 5.3 6.4
-0.7 +0.7

5.7
F0.4
17.6

-2.9 -1.0 -0.4
22 18 0

2.0
C-4.4
20.2

323 27.6 28.60 35.6 7.0 8.0 7.6 6.3
-0.8 +0.7

11.0
F-3.4
22.1

-4.1 -3.0 -1.0
12 2 0

2.8
C-3.5
19.8

+53¹⁰ EC. 32.9 30.0 54 54 8.8 7.8
 38.3 8.3 -0.5 +0.5

$\frac{2.6}{C-1.2}$
 18.6

$\frac{+1.3}{7}$

$\frac{+2.9}{0}$

14
 $\frac{0.8}{C-7.0}$
 21.5

+50 33.1 30.00 -0.5 +0.5

325 34.5 29.72 54 54 10.9 9.5
 3.9 10.2 -0.7 +0.7

$\frac{9.9}{C-1.0}$
 18.5

$\frac{+5.2}{0}$

$\frac{2.6}{C-6.9}$
 21.5

+50 31.0 29.44 54 7.6 7.7 8.5
 36.4 38.6 7.0 9.2 -0.7 +0.7

$\frac{6.7}{C-1.0}$
 18.5

$\frac{+0.6}{0}$ $\frac{+3.2}{1.5}$

$\frac{3.7}{C-4.8}$
 20.4

327 29.0 30.38 34.4 4.0

6.1
F-2.1
20.1

-1.8 -1.4 -1.5 0.0
11 0 11 12

3.5
C-0.5
18.2

+50 30.2 30.25 35.6 5.4

5.4
4.0
18

-0.6 0.0 +0.2 +2.4
13 0 9 14

2.7
C-2.7
19.4

326 30.8 30.13 36.2 6.1 6.4 5.8
-0.3 +0.3

6.4
Gr.
18.0

+0.7 +0.7 +1.7
0 5 7

0.2
C-1.6
18.8

L
 +60 ⁸⁴ 80 27.0 30.8 +5.4 1.6 -0.9 +0.9

~~F46
 23.9
 L
 F 3.7
 22.5~~

~~£
 -10 -3.8
 15 0~~

~~F5.4 16
 25.1
 3
 F-4.6
 23.9~~

+50 26.9 30.75 -0.8 +0.8

328 26.5 30.63 31.9 1.3 -0.4 +0.4

~~3.8
 F4.1
 23.1~~

~~-4.1 -4.3 -3.8
 0 13 14~~

~~F4.5
 23.2
 5
 F4.1
 23.1~~

Note: Use £ grate on inside of curve

+50 27.5 30.50 32.9 2.4

~~4.2
 F-3.8
 22.7~~

~~-3.2 -3.0 -3.0 -2.6
 11 0 12 13~~

~~2.9
 F-2.0
 20~~

£

+50 Balance Ft.

330	32.1	31.66	+3.8	8.3	9.6	6.9
			37.5	8.7	-1.4	+1.4

F 0.4
17.6
~~F 1.1 (1)~~
18.6

C 3.4
17.7

+0.5	+0.5	+0.6	1.4
0	12	15	27.5
			C 5.0
			20.5

+50	29.7	31.38	5.4	5.0	2.3
			3.7	-1.4	+1.4

F 2.5
20.8
~~F 1.2~~
18.8

-1.8	-1.7	-1.8
14	0	9

F 1.2
18.8
~~2.3~~
18

↑

+20 Balance Ft.

↓

329	28.0	30.97	+5.4	3.7	1.4
			2.5	-1.3	+1.3

F 3.7
22.6
~~F 2.2~~
~~F 3.5 (1)~~
20.7

-3.0	-2.9	-2.5
15	0	12

F 5.5
25.3
~~2.2~~
~~F 2.5~~
23.8

(Use £ grade on inside of curve)

+50	40.2	34.56	5.4 45.6	11.0	N.A -0.4	10.6 +0.4
-----	------	-------	-------------	------	-------------	--------------

$$\begin{array}{r} C 3.8 \\ 19.9 \\ \hline 4.2 \\ \hline 20.5 \end{array}$$

+5.6	+6.6
0	17

$$\begin{array}{r} C 5.8 \\ 20.9 \\ \hline 14 \\ \hline C - 6.2 \\ \hline 21.1 \end{array}$$

+2.178

331	37.2	33.67			-0.8	+0.8
-----	------	-------	--	--	------	------

$$\begin{array}{r} C 2.4 \\ 19.2 \end{array}$$

+87 ¹⁵ EC	36.9	33.5	5.4 88	88	9.7 -0.9	1.9 +0.9
----------------------	------	------	-----------	----	-------------	-------------

$$\begin{array}{r} 4.9 \\ \hline C - 3.2 \\ \hline 19.7 \end{array}$$

+3.4
0

$$\begin{array}{r} C 2.8 \\ 19.4 \\ \hline 2.2 \\ \hline C - 3.1 \\ \hline 19.8 \end{array}$$

EV.C.			5.4		8.6	6.0
+50	34.7	32.78		7.3	-1.3	+1.3

$$\begin{array}{r} C 1.1 \\ 18.6 \\ \hline 2.9 \\ \hline C - 2.4 \\ \hline 18.2 \end{array}$$

+2.6	+1.9	+2.3
2	0	2

$$\begin{array}{r} C 0.2 \\ 18.1 \\ \hline 1.5 \\ \hline C - 1.5 \\ \hline 18.7 \end{array}$$

(Use & grade on inside of curve)

2

19

333 40.2 37.24 54 8.4

$$\begin{array}{r} 6.7 \\ C-1.7 \\ \hline 18.8 \end{array}$$

$$\begin{array}{r} +3.0 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 3.8 \\ C-4.2 \\ \hline 20.1 \end{array}$$

+0.178

+50 41.2 36.34 54 11.3

$$\begin{array}{r} 7.3 \\ C-4.0 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} +5.9 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 3.8 \\ C-8.0 \\ \hline 22 \end{array}$$

332 41.6 35.45 54 11.6

$$\begin{array}{r} 7.1 \\ C-4.5 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} +6.7 \\ \hline 0 \\ +6.3 \\ \hline 0 \end{array}$$

$$\begin{array}{r} +7.6 \\ \hline 19 \end{array}$$

$$\begin{array}{r} 3.0 \\ C-8.6 \\ \hline 22.3 \end{array}$$

+66 43.0 39.6 2.0

+50 40.7 38.9 39.50 5.4 6.6

+30 36.6 39.3 9.9 2.7

334 38.8 38.92 5.4 5.3

+80 35.1 38.6 5.4 1.9

BVC.
+50 36.3 38.13 5.4 3.4

E

$\frac{-70.0}{35}$ $\frac{-110}{26}$ $\frac{-6.0}{12}$ $\frac{+3.4}{0}$ $\frac{+3.6}{24}$

$\frac{14.0}{F-7.4}$ $\frac{+1.2}{0}$ $\frac{+41}{7}$ $\frac{1.8}{C-4.8}$
28.1 20.4

$\frac{-8.0}{30}$ $\frac{-2.7}{0}$ $\frac{-1.3}{7}$ $\frac{+4.7}{14}$ $\frac{+4.9}{25}$

$\frac{11.3}{F6.0}$ $\frac{-5.6}{-2.0}$ $\frac{-0.1}{0}$ $\frac{+1.9}{15}$ $\frac{1.4}{C-3.9}$
26.0 19.9

$\frac{-5.1}{2.5}$ $\frac{-3.5}{0}$ $\frac{-1.6}{1.9}$ $\frac{0.01}{2.3}$

$\frac{5.7}{F2.3}$ $\frac{-2.0}{0}$ $\frac{-1.2}{1.8}$ $\frac{4.3}{F0.9}$
20.4 18.3

+ 30 39.2 39.9 7.5
89

336 42.9 -40.02 11.1 +2.9 5.4 5.4 14.0

+50 44.4 40.05 2.8 11.8 7.2 16.2

335 43.0 39.88 11.6 14.7
85

$\frac{-19}{20}$ $\frac{-15}{3}$ $\frac{-0.7}{0}$ $\frac{+3.7}{8}$ $\frac{+4.1}{25}$

$\frac{5.4}{17.7}$ $\frac{-0.2}{3}$ $\frac{+2.9}{0}$ $\frac{+9.0}{5}$ $\frac{3.4}{23.3}$
 $\frac{10.6}{23.3}$

$\frac{5.4}{18.9}$ $\frac{+1.9}{5}$ $\frac{+4.4}{0}$ $\frac{+11.2}{3}$ $\frac{4.1}{24.0}$
 $\frac{12.3}{24.0}$

$\frac{11.3}{19.7}$ $\frac{+9.4}{15}$ $\frac{+3.1}{0}$ $\frac{+2.9}{6}$ $\frac{+9.4}{15}$ $\frac{3.7}{23.5}$
 $\frac{11.0}{23.5}$

⊕

+70

34.9

38.9

17.9

1.4

$\frac{+15.4}{35}$

$\frac{+7.8}{4}$

$\frac{-4.0}{0}$

$\frac{-4.6}{1}$

$\frac{-4.0}{23}$

$\frac{-6.3}{27}$

$\frac{-7.6}{35}$

+50

34.6

39.09

+5.4 +2.0

0.9

1.55

+1.0

17.5

+2.05

24.5

+2.0

-2.0

~~F 10.5~~

~~32.8~~

~~7.5~~

~~27.7~~

$\frac{-4.1}{22}$

$\frac{-4.5}{0}$

$\frac{-4.5}{2}$

$\frac{+5.2}{7}$

~~C 9.2~~

~~22.6~~

~~5.9~~

~~11.8~~

~~13.8~~

R

+14 BS

35.1

~~35.2~~

39.3

+5.4

1.2

0.3

2.1

+1.0

-1.0

+1.4

-1.4

~~F 9.0~~

~~30.5~~

~~7.3~~

~~27.5~~

$\frac{-4.7}{22}$

$\frac{-4.2}{0}$

~~F 3.1~~

~~21.7~~

~~4.3~~

~~7.0~~

~~0.3~~

~~F 3.1~~

~~21.7~~

~~1.5~~

~~2.1~~

~~2.0~~

337

35.3

39.43

+5.4

1.3

0.2

2.4

+1.2

-1.2

~~F 8.7~~

~~30.1~~

~~7.5~~

~~27.6~~

$\frac{-4.0}{22}$

$\frac{-4.1}{0}$

~~F 3.1~~

~~21.7~~

~~1.5~~

~~2.1~~

~~2.0~~

78000

EVC -

+50

37.5

39.77

+5.4

3.1

2.5

3.7

+0.6

-0.6

~~F 3.9~~

~~22.9~~

~~8.5~~

~~21.9~~

$\frac{-2.7}{2}$

$\frac{-2.3}{0}$

$\frac{-3.1}{10}$

~~F 2.6~~

~~20.9~~

~~5.9~~

~~20.1~~

~~2.0~~

Note: Use E grade on inside of curve

339 32.8 38.06 5.4 23.8 21 18.5 +2.2 20.7 -2.2

$$\frac{F 15.6}{40.4}$$

$$\frac{F 13.0}{36.5}$$

$$\frac{-9.5}{28} \quad \frac{-4.8}{19} \quad \frac{-5.3}{0} \quad \frac{-5.1}{5} \quad \frac{+3.7}{7} \quad \frac{+1.5}{19}$$

$$\frac{C 12.3}{24.2}$$

$$\frac{C 14.7}{25.8}$$

-00686

+50 32.9 38.40 23.4 5.4 17.9 20.1 +2.2 20.1 -2.2

$$\frac{F 12.6}{35.9}$$

$$\frac{F 10.4}{32.6}$$

$$\frac{-8.1}{28} \quad \frac{-4.4}{21} \quad \frac{-5.5}{0} \quad \frac{-5.0}{3} \quad \frac{-1.1}{6} \quad \frac{+8.4}{8} \quad \frac{+13.3}{19} \quad \frac{0-11.6}{26.3}$$

$$\frac{C 14.1}{25.1}$$

$$\frac{C 14.6}{25.3}$$

338 40.3 38.74 3.4 13.2 5.0 14.8 2.9 17.0 +2.2 -2.2

$$\frac{F 12.6}{35.2}$$

$$\frac{F 9.8}{30.9}$$

$$\frac{-4.1}{24} \quad \frac{-5.2}{2} \quad \frac{+1.6}{0} \quad \frac{+9.4}{6} \quad \frac{+12.2}{13}$$

$$\frac{C 14.6}{25.3}$$

$$\frac{C 17.0}{26.5}$$

(Use $\frac{1}{2}$ grade on inside of curve)

+80 31.5 36.8 0.1

+50 31.9 37.03 5.4 9.7 0.3 4.6 +2.2 -2.2

-200686
340 32.5 37.37 5.2 13.2 0.5 8.3 +2.2 -2.2

+50 32.6 37.71 5.4 2.0 0.3 14.9 +2.2 -2.2

13.8
6.9
20.7
13.8
6.9
20.7
-15.2 -12.9 -10.6 -5.1 -5.3 -5.5 -3.9
50 42 29 13 0 11 36

F 19.7
46.6
10.0
F 16.6
41.9
-12.9 -8.7 -5.2 -5.1 -1.2 -5.3
28 26 14 0 15 11

F 0.8
18.2
5.1
C 17
18.8

F 16.2
42.1
10
F 14.9
38.0
5.2
C 20.5

-11.6 -5.1 -4.9 -5.0 0.0
28 17 0 9 11

C 2.9
19.4
5.4
C 5.1
20.5

F 15.9
40.9
10
F 13.9
37.7

-11.0 -5.0 -5.1 -5.0 +2.9 4.2
27 18 0 7 8 17

C 2.9
22.5
5.8
C 11.3
23.6

(Use to grade on inside of curve)

+30 31.3 36.1 54 0.6

$\frac{-8.0}{31} \quad \frac{-5.1}{25} \quad \frac{-4.8}{0} \quad \frac{-3.0}{14} \quad \frac{-1.8}{25}$

342 30.9 36.13 60 0.8 +0.3 -0.3

$\frac{F 7.8}{28.7}$
 ~~$\frac{8.0}{17.5}$~~
~~28.2~~

$\frac{-5.8}{24} \quad \frac{-5.2}{6} \quad \frac{-4.9}{9} \quad \frac{-3.6}{20}$

$\frac{F 2.6}{20.9}$
 ~~$\frac{3.6}{22.5}$~~
~~20.7~~

B.V.C.
 +50 31.0 36.34 54 0.1 +1.0 -1.0

$\frac{F 12.2}{35.3}$

~~$\frac{10.1}{10.9}$~~
~~33.4~~

$\frac{-9.4}{28} \quad \frac{-4.1}{19} \quad \frac{-5.0}{16} \quad \frac{-5.3}{0} \quad \frac{-5.3}{8} \quad \frac{-3.3}{10}$

$\frac{F 2.4}{20.6}$
 ~~$\frac{2.5}{11.5}$~~
~~11.2~~

+25 Balance Ft.

E.C.
 +22^{1/2} 31.1 36.5 54 0.0 +1.5 -1.5

$\frac{F 14.2}{38.3}$

~~$\frac{10.0}{11.8}$~~
~~34.7~~

$\frac{-9.5}{28} \quad \frac{-5.1}{18} \quad \frac{-5.4}{0} \quad \frac{-5.6}{10} \quad \frac{-2.8}{14}$

$\frac{F 3.6}{22.4}$
 ~~$\frac{3.5}{11.5}$~~
~~20.1~~

341 31.3 36.69 0.0 +1.7 -1.8

$\frac{F 17.0}{42.5}$

~~$\frac{17.8}{14.5}$~~
~~38.7~~

$\frac{-10.9}{30} \quad \frac{-5.5}{17} \quad \frac{-5.4}{0} \quad \frac{-5.7}{11}$

$\frac{F 2.5}{20.8}$
 ~~$\frac{2.9}{11.1}$~~
~~18.6~~

(Use E grade on inside of curve)

+50 42.3 36.5 | 23 8.0 8.1 13.8

$$\begin{array}{r} 52 \\ C-2.7 \\ \hline 19.3 \end{array}$$

$$\begin{array}{r} +5.8 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 3.3 \\ C-10.5 \\ \hline 23.2 \end{array}$$

7.0
0
3
4
3

343 39.1 36.34 33 9.4 6.1 12.2

$$\begin{array}{r} 10.7 \\ F4.6 \\ \hline 23.9 \end{array}$$

$$\begin{array}{r} -4.9 + 0.3 + 2.8 \\ \hline 16 \quad 12 \quad 0 \end{array}$$

$$\begin{array}{r} 4.0 \\ C-8.2 \\ \hline 22.1 \end{array}$$

EYC.

+50 34.6 36.17 2.1 9.2 0.6 7.7

$$\begin{array}{r} 52 \\ F4.8 \\ \hline 24.1 \end{array}$$

$$\begin{array}{r} -4.7 - 4.7 - 1.5 + 1.4 \\ \hline 4 \quad 0 \quad 11 \end{array}$$

$$\begin{array}{r} 4.7 \\ C-2.8 \\ \hline 17.4 \end{array}$$

+25 48.2 37.1 7.3 184

$$\begin{array}{r} \cancel{+} \\ -5.6 \\ \hline 40 \end{array} \quad \begin{array}{r} -5.6 \\ \hline 25 \end{array} \quad \begin{array}{r} +6.6 \\ \hline 15 \end{array} \quad \begin{array}{r} +11.1 \\ \hline 0 \end{array} \quad \begin{array}{r} -15.4 \\ \hline 130 \end{array}$$

345 50.7 37.03 4.7 8.5 ^{13.4} 18.4 22.2

$$\begin{array}{r} 6.9 \\ C-6.5 \\ \hline 21.2 \end{array} \quad \begin{array}{r} +9.4 \\ \hline 20 \end{array} \quad \begin{array}{r} +13.7 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 3.2 \\ C-19.0 \\ \hline 27.5 \end{array}$$

+100.343

+50 48.6 36.86 4.0 9.0 15.7 20.7

$$\begin{array}{r} 7.4 \\ C-8.3 \\ \hline 22.2 \end{array} \quad \begin{array}{r} +9.9 \\ \hline 16 \end{array} \quad \begin{array}{r} +11.7 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 4.5 \\ C-16.2 \\ \hline 26.1 \end{array}$$

+15. Balance Ft.

344 46.0 36.69 3.9 8.4 13.2 17.7

$$\begin{array}{r} 7.2 \\ C-0.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} +9.3 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 4.7 \\ C-13.0 \\ \hline 24.5 \end{array}$$

+60 39.4 37.5 54 7.3

$\frac{-5.1}{35} \frac{-0.9}{27} \frac{-0.3}{21} \frac{+2.4}{10} \frac{+1.9}{0} \frac{+6.3}{30}$

+50 38.7 37.54 -1.0 +1.0

L
+41 $\frac{65}{BC}$ 39.0 37.4 3.5 13.0 5.1 14.6 -0.9 +0.9 6.0 13.7

$\frac{F 4.0}{8.8} \frac{23.0}{21.2}$

$\frac{-2.6}{20} \frac{+1.6}{0} \frac{+9.2}{13}$

$\frac{C 11.3}{23.7} \frac{5}{29.1}$

+00343

346 43.7 37.37 15 13.0 7.8 19.3 -0.6 +0.6 8.4 16.7

$\frac{F 6.2}{18.0} \frac{27.3}{25.4}$

$\frac{-5.8}{22} \frac{-2.9}{18} \frac{+6.3}{0} \frac{+13.8}{18}$

$\frac{C 13.9}{25.0} \frac{1.2}{25.2}$

↑ Note: Use A grade on inside of curve

+75 47.6 37.3 0 7.7 10.3 18.0

$\frac{-6.7}{35} \frac{-6.7}{23} \frac{-3.6}{20} \frac{+10.3}{0} \frac{+15.5}{17} \frac{+15.7}{30}$

+50 37.20 -0.1 +0.1

+44 36.9 37.2 5.4 5.1 -0.1 +0.1 10.5 10.2 5.2 10.1

$\frac{11.2}{F 6.1} \frac{26.1}{26.1}$

$\frac{-5.9}{21} \frac{-0.3}{0} \frac{+4.2}{13}$

$\frac{4.0}{C-6.1} \frac{21.0}{21.0}$

348 33.8 38.06 5.4 10.1 11 5.8 2.4 1.4
-1.4 +1.4

~~F 4.5
23.8
5.4
F 3.0
21.8~~

~~-4.3 -4.1
0 8~~

~~F 2.4
20.6~~

~~C 3.9
18.9~~

+100343

+ 50 35.9 37.89 3.0 9.3 1.0 7.3 2.4 5.4
-1.4 +1.4

~~F 4.0
23.0
5.4
F 3.0
21.5~~

~~-4.2 -2.0 -2.6
12 0 8~~

~~Grade
18.0~~

~~C 3.9
18.6~~

347 36.7 37.71 5.4 4.4 5.7 3.0
-1.4 +1.4

~~F 3.4
22.1~~

~~C 2
F 0.5
17.7~~

~~-1.8 -1.0 +1.9
18 0 11~~

~~Grade
18.0~~

~~C 1.5
18.8~~

(Use grade on inside of cone)

⊕

L
+63⁴⁹ PCC

+50 36.9 38.57 8.9 7.2 8.6 5.8
-1.4 +1.4

~~F 2.2
20.3
9.6
F 1.9
18.5~~

~~-22 -17 +31
1 0 7~~

~~C 1.2
18.6
3.2
C 2.6
19.3~~

349 35.6 38.40 5.0 11.5 2.5 8.7 4.0 7.3
-1.4 +1.4

~~F 3.6
22.4
6.4
F 2.4
20.6~~

~~-28 -26
0 8~~

~~C 0.8
18.4
1.8
C 2.5
17.2~~

1.00343

+50 34.4 38.23 5.4 1.6 3.0 0.2
-1.4 +1.4

~~F 5.0
24.5
0.0
F 3.0
21.5~~

~~-5 -3.8 -3.7
0 11~~

~~F 2.9
21.4
2.1
F 1.9
19.8~~

(Use grade on inside of curve)

357 359 3909 54 11.0 2.2 7.8 ^{2.6} ^{7.4} -0.4 +0.4

~~F 3.3
22.0
5.7
F 3.1
21.6~~

~~-3.2 -2.8
0 8~~

~~C 0.8
18.4
6.2
C 2.3
18.6~~

+50 359 3891 50 11.8 2.0 8.8 ^{2.8} ^{8.0} -0.8 +0.8

~~F 3.4
22.1
5.4
F 2.0
20.9~~

~~-3.0
0~~

~~C 4.3
20.2
3.9
C 5.1
20.5~~

350 37.8 3874 4.5 11.3 3.6 10.4 ^{4.8} ^{7.2} -1.2 +1.2

~~F 2.0
20.0
5.6
F 0.8
18.2~~

~~-1.8 -0.9 +2.9
3 0 6~~

~~C 4.6
20.3
3.4
C 5.8
20.9~~

+80 38.3 38.6 5.1

~~-2.2 -1.7 -0.3 +1.2 +1.2
2.2 3 0 4 25~~

(Use 2 grade on inside of curve)

750 36.6 39.68 54 2.4 2.2
2.3 -0.1 +0.1

~~5.5
F 3.1
21.6~~

ϵ
~~-3.5 -3.1 -3.6
17 0 12~~

~~6.1
F 3.9
22.8~~

+17¹⁶ EC 36.3 39.5 54 2.4 2.0
2.2 -0.2 +0.2

~~F 4.7
24.1
6.9
F 4.5
23.7~~

ϵ
~~-3.2
0~~

~~F 3.7
22.5
5.5
F 3.5
22.2~~

EVC
352 36.3 39.43 2.2 +0.2

750 36.0 39.26 54 2.4 1.3
2.1 -0.3 +0.3

~~F 4.5
23.8
0.6
F 4.2/m
23.7~~

ϵ
~~-3.3 -4.1
0 13~~

~~F 3.6
22.4
5.2
F 3.8
21.9~~

(Use ϵ grade on inside of curve)

354 44.1 41.06 5.8 8.8

10.8
F2.0
20.0

$\frac{-22}{14}$ $\frac{+3.0}{0}$ $\frac{+1.6}{3}$

33
5.5
C-3.3
19.6

150 38.7 40.57 5.4 3.5

59
F2.4
20.6

$\frac{-2.7}{8}$ $\frac{-1.9}{0}$ $\frac{-0.5}{7}$

2.8
8-0.7
18.3

+25 Balance Ft.

EVC
353 37.8 40.09 1.9 2.6

54
F2.8
21.2

$\frac{-3.9}{1}$ $\frac{-2.3}{0}$ $\frac{-3.0}{12}$

4.7
F2.1
20.1

¢

L
²⁶
 +74 BC 44.7 42.7 4.3 12.6 6.3 14.6 -1.3 7.6 13.3
 +1.3

~~C 1.1
 5.186
 17.1~~

~~+0.7 +2.0 +7.5
 3 0 4~~

39
~~C 10.8
 23.4
 7.1~~

+50 Balance Pt.
 BVC
 +50 42.9 42.51 12.4 13.8 1.8
 12.8 -1.0 +1.0

~~C 0.6
 18.3
 12.3
 18.7~~

~~0.0 +0.4 +2.6
 3 0 6~~

~~C 3.3
 19.7
 7.4
 20.1~~

10097
 355 40.6 42.03 10.1 8.8 8.0
 8.4 -0.4 +0.4

~~F 1.0
 18.5
 8.6
 18.2~~

~~-1.2 -1.7 +0.2
 3 0 5~~

~~C 4.0
 20.0
 5.4
 19.3~~

Note: Change ϵ Grade to inside of curve for superdeviation.

+50 42.0 41.54 8.0 8.6

~~10.0
 F 1.5
 19.2~~

~~-1.2 +0.5
 12 0~~

~~4.7
 C-3.8
 19.9~~

+26²⁸ EC. 42.8 43.5 5.4 13.0 4.7 12.3 -1.5 +1.5

357 42.7 43.40 5.4 13.3 4.7 12.6 -1.7 +1.7

4004

EVC
+50 43.9 43.20 5.4 13.0 6.1 13.7 -2.0 +2.0

356 45.7 42.92 3.7 11.4 6.5 14.2 -1.7 +1.7

~~F7.3
28.0
2.2
F-6.7~~

~~-7.5 -1.3 -0.7 -0.2 +7.8
23 12 0 15 18~~

~~C4.0
20.0
C-6.8
21.4~~

~~F8.4
13.0 29.6
F-6.6
20.9~~

~~-0.9 -0.7 -0.6 +4.9
12 0 11 17~~

~~Grade
17.0
C-8.1
22.0~~

~~C0.6
18.3~~

~~+0.4 +0.7 +1.0 +6.7
19 0 8 15~~

~~C7.0
21.5
C-5.2
22.6~~

~~C1.2
18.2
C-2.7
11.3~~

~~+1.5 +2.8 +8.0
2 0 3~~

~~C6.4
21.2
C-8.1
22~~

(Use E grade on inside of curve)

BYC.

+50

43.4 44.0 5A 22.4 48 23.8

$$\frac{4.8}{9.1}$$

 18

$$\frac{-0.6}{0}$$

$$\frac{+11.3}{11}$$

$$\frac{3.2}{-20.6}$$

 28.3

+1004

358

43.4 43.80 5A +22.8 5.0 22.4 -0.3 5.3 22.1 +0.3

$$\frac{F 6.8}{27.2}$$

~~18.5~~

~~26.7~~

$$\frac{-0.7}{17}$$

$$\frac{-0.4}{0}$$

$$\frac{-0.5}{9}$$

$$\frac{+9.6}{13}$$

$$\frac{C 15.8}{25.9}$$

~~6.0~~

~~C - 11.1~~

~~26.1~~

+50

42.8 43.60 5A +20.2 4.6 19.4 5.6 18.4 1.0 +1.0

$$\frac{F 7.3}{28.0}$$

~~20.0~~

~~F 6.4~~

~~26.6~~

$$\frac{-7.0}{21}$$

$$\frac{-1.4}{12}$$

$$\frac{-0.8}{0}$$

$$\frac{-0.4}{12}$$

$$\frac{+9.3}{17.0}$$

$$\frac{C 10.7}{23.4}$$

~~6.3~~

~~C - 12.1~~

~~24.0~~

(Use & grade on inside of curve)

R
+05¹¹ BC 42.9 46.2 5.4 8.0 2.1 A7 +0.8 -0.8

$\frac{10.1}{F 8.8}$
30.2

$\frac{-3.7}{20}$ $\frac{-3.3}{0}$ $\frac{+3.5}{13}$

$\frac{5.5}{G.P.}$
18

BVC
360 43.0 46.07 2 +0.7 -0.7

EVC
+50 43.6 45.13 5.4 27.7 3.7 26.2

$\frac{4.9}{F 1.0}$
18.5

$\frac{-7.5}{0}$ $\frac{-1.4}{10}$ $\frac{+4.9}{21}$ $\frac{9.7}{C 16.5}$
26.2

359 44.1 44.38 5.5 20.1 5.2 23.8

$\frac{1.4}{C -0.3}$
18.1

$\frac{-0.3}{0}$ $\frac{+5.7}{14}$ $\frac{+15.8}{17}$ $\frac{5.1}{C -18.7}$
27.4

+50 42.8 47.57 54 286 0.6 228 +2.2 -2.2

+6.5
+1.6 26.0

11.0
F 17.5
43.2

-14.5 -5.1 -4.8 -0.1 +1.4 +11.8 7.2
38 24 0 5 14 19 C -18.8
27.4

+35 Balance Pt.

361 42.6 47.29 54 261 0.7 21.8 +2.2 -2.2

+1.4 236

15.2
F 16.6
41.9

-13.3 -4.9 -4.7 +0.7 +12.1 C -15.7
33 20 0 20 22 25.8

-4.9
9

+50 42.7 46.84 59 232 1.3 19.1 +1.4 -1.4

+0.1 20.5

11.0
F 11.1
33.7

-8.7 -4.1 -4.1 -4.7 +0.1 9.0
24 16 0 11 18 C -11.5
23.7

+85. Balance Ft.

+50	44.7	48.05	0.1	70.0	+32	66.7	+0.4	-0.4	12.4 F16.0 41.0	-14.9	-3.5	-3.3	-3.3	+30.0	+52.7	0.2 C-66.9 51.4
+25	44.2	48.0	0.5	56.1	+3.3	52.3	+0.7	-0.7	-16.6 45	-14.6	-4.3	-3.8	-3.0	+37.5	5.4 C-47.6 41.8	
363	43.7	48.00	0.2	39.9	+4.1	35.6	+1.1	-1.1	11.5 F16.7 42.0	-15.3	5.1	-4.3		-4.3	10.9 C-25.8 30.9	
+76 ⁰⁷	EC 433	48.00	1.3		+3.1	32.3	+1.5	-1.5	13.0 F17.6 43.4	-14.8	-5.2	-4.4		-4.0	+4.6	+2.0 C-35.8 35.9
+50	43.1	47.96	5.4	37.2	0.5	32.3	+1.9	-1.9	18.2 F19.6 46.4	-15.5	-5.0	-4.9	-4.9	+1.1	6.4 C-27.8 31.9	
+25	43.2	47.9	5.4	34.5	0.7	29.8	+2.0	-2.0	31.8 120.46 F17.5 43.2	-15.9	-15.6	-5.3	-4.7	-4.0	+13.8	3.0 C-28.8 32.4 4.2 C-22.6 29.3
362	42.9	47.82	1.9	29.3	+3.0	24.4	+2.2	-2.2								

365 48.0 48.93 32 507 2.3 49.8 -2.0 +2.0

$\frac{78}{F3.6}$
22.4

$\frac{-17}{17}$ $\frac{-09}{0}$ $\frac{-09}{7}$

$\frac{185}{C-29.3}$
32.7

18074

L
766⁴⁶ B.C. 47.2 48.8 0.3 13.0 +1.3 11.4 -1.7 0.4 9.7 +1.7

$\frac{25}{F2.1}$
20.1

$\frac{-23}{17}$ $\frac{-16}{0}$ $\frac{-15}{12}$

$\frac{+33}{C-13.0}$
24.5

+50 46.9 48.56 0.0 13.3 +1.7 11.6 -1.3 10.8 +1.3

$\frac{-176}{41}$ $\frac{-24}{17}$ $\frac{-1.7}{0}$ $\frac{-1.7}{10}$ +

$\frac{+15}{C-11.8}$
23.9

+25 46.4 48.4 0.6 72.9 +1.4 70.9 -0.9 70.0 +0.9

$\frac{-17.8}{45}$ $\frac{-16.6}{36}$ $\frac{-24}{17}$ $\frac{-2.0}{0}$ $\frac{-2.0}{8}$ $\frac{+54.8}{33}$ 9.2

$\frac{C-60.8}{48.4}$

364 45.7 48.24 0.8 68.5 +1.7 66.0 -0.5 +1.2 65.5 +0.5

$\frac{156}{F10.7}$
A2.1

$\frac{-16.3}{36}$ $\frac{-2.5}{18}$ $\frac{-2.5}{0}$ $\frac{-2.5}{5}$ $\frac{+50.6}{38}$

$\frac{0.8}{C61.7}$
50.3

+75 45.3 48.1 0.0 72.3 +2.8 69.5

$\frac{-176}{50}$ $\frac{-17.2}{41}$ $\frac{-34}{19}$ $\frac{-2.8}{0}$ $\frac{-2.8}{4}$ $\frac{+61.5}{42}$

$\frac{4.0}{C-55.5}$
50.7

+50 48.7 50.94

-0.9 +0.9 $\frac{F14.0}{38}$ $\frac{-13.0}{32}$ $\frac{-1.9}{13}$ $\frac{-1.3}{0}$ $\frac{-1.0}{11}$ $\frac{C1.0}{20}$

+25 48.9 49.9

37.9 36.9 -1.4 +1.4 $\frac{35.5}{15}$ $\frac{-14.4}{33}$ $\frac{-1.6}{15}$ $\frac{-1.0}{0}$ $\frac{+0.9}{8}$ $\frac{C-27.8}{31.9}$

+0.074

⁴⁸+07 E.C. 48.9 49.8

282 -1.6 +1.6 $\frac{26.6}{38.3}$ $\frac{F14.2}{31}$ $\frac{-12.2}{16}$ $\frac{-1.5}{0}$ $\frac{-0.9}{8}$ $\frac{+10.0}{15}$ $\frac{10.5}{C-16.1}$ $\frac{26.0}{26.0}$

366 49.0 49.67

-1.6 +1.6

+50 48.9 49.30 30 388.2.6 38.4 -2.3 +2.3

$\frac{3.2}{F14}$ $\frac{36.1}{19.1}$ $\frac{-0.4}{0}$ $\frac{-0.4}{6}$ $\frac{4.9}{C-31.2}$ $\frac{33.6}{33.6}$

368 49.4 51.15 -0.7 +0.7

$\frac{F 1.5}{19.3}$

$\frac{E 8.9}{27.5}$

~~$\frac{F 1.5}{19.3}$~~

-1.8

$\frac{-1.5}{5}$

$\frac{+7.8}{12}$

~~$\frac{E 8.9}{27.5}$~~

+0.074

+50 50.8 50.78 -0.5 +0.5

$\frac{F 1.5}{19.3}$

$\frac{C 11.1}{23.6}$

~~$\frac{F 1.5}{19.3}$~~

-2.0

$\frac{0.0}{6}$

$\frac{+6.1}{5}$

~~$\frac{C 11.1}{23.6}$~~

L
+35⁸⁴_{BC}

367 48.5 50.41 -0.3 +0.3

$\frac{F 10.3}{32.5}$

$\frac{C 10.1}{23.1}$

~~$\frac{F 10.3}{32.5}$~~

-2.5

$\frac{-1.9}{0}$

$\frac{-1.5}{10}$

$\frac{+3.7}{5}$

~~$\frac{C 10.1}{23.1}$~~

Note: Use 2' Grade on inside of curve for super-elevation. Sta 367+35.84 to 369+43.10

+65. Balance Pt.

+50 51.5 52.26

-0.4 +0.4

+43¹⁰/_{ES}

10074

+369 51.4 51.89

-0.7 +0.7

+50 49.9 51.52

-0.7 +0.7

~~F8.3
29.5
29~~

~~-7.2
29~~

~~-1.2
11~~

~~-0.8
0~~

~~F1.1
18.7
18~~

~~F8.0
29.0
29.5~~

~~-7.0
15~~

~~-0.5
0~~

~~-1.5
3~~

~~F1.8
19.7
19~~

~~F8.0
29.0
28.4~~

~~-7.3
21~~

~~-1.7
9~~

~~-1.6
16~~

~~-0.8
16~~

~~F1.0
18.5
18.2~~

(Use 2 grade on inside of curve)

371 53.8 53.95

+0.1 - 0.1

$\frac{0.0}{17}$ -0.2 $\frac{-0.2}{12}$ $\frac{+1.6}{14}$ $\frac{C 3.3}{19.6}$

+50 52.7 53.21

$\frac{F.10}{23}$ $\frac{-3.6}{16}$ $\frac{-0.7}{10}$ $\frac{-0.5}{14}$ $\frac{-0.5}{15}$ $\frac{+1.2}{15}$ $\frac{C 2.2}{19.1}$

370 52.0 52.65

-0.2 +0.2

$\frac{F.8.1}{29.2}$ $\frac{F.0.7}{18.1}$
 ~~$\frac{F.7.8}{28.7}$ $\frac{-0.6}{9}$ $\frac{-0.6}{0}$ $\frac{C.8.0}{25.7}$~~

BVC
+75

+50 57.6 58.56

+0.22-0.22

$\frac{-3.2}{21.8}$ -1.0 $\frac{C.03}{18.1}$

373 60.5 57.63

+0.2-0.2

$\frac{0.0}{17.8}$ $\frac{+2.1}{14}$ $\frac{+2.9}{0}$ $\frac{C.3.1}{19.7}$

58185 +50 60.7 56.71

+0.2-0.2

$\frac{0.0}{20.4}$ $\frac{+3.3}{15}$ $\frac{+1.0}{0}$ $\frac{+1.2}{15}$ $\frac{+6.2}{16}$ $\frac{C.7.1}{21.7}$

+25. Balance Pt

372 58.0 55.78

+0.2-0.2

F. $\frac{0.0}{17}$ $\frac{+1.5}{14}$ $\frac{+2.2}{0}$ $\frac{+2.1}{16}$ $\frac{+1.1}{17}$ $\frac{C.5.0}{20.5}$

R. 89
+53 B.C.

+50 55.5 54.85

+0.1-0.1

F. $\frac{0.17}{24.2}$ $\frac{-0.2}{12}$ $+0.1$ $\frac{+0.2}{11}$ $\frac{+1.6}{12}$ $\frac{C.1.9}{20.6}$

376 66.3 66.33

-0.9 +1.0

$$\begin{array}{r} \text{F8A} \\ 29.6 \end{array} \quad \begin{array}{r} -7.7 \\ 25 \end{array} \quad \begin{array}{r} +0.5 \\ 14 \end{array} \quad \begin{array}{r} 0.0 \\ 8 \end{array} \quad \begin{array}{r} +0.7 \\ 10 \end{array} \quad \begin{array}{r} +4.9 \\ 12 \end{array} \quad \begin{array}{r} \text{C. 7.7} \\ 21.8 \end{array}$$

+50 63.4 64.01

-1.9 +2.0

$$\begin{array}{r} \text{F4A} \\ 23.6 \end{array} \quad \begin{array}{r} -3.7 \\ 20 \end{array} \quad \begin{array}{r} -0.8 \\ 13 \end{array} \quad \begin{array}{r} -0.6 \\ 10 \end{array} \quad \begin{array}{r} -0.6 \\ 12 \end{array} \quad \begin{array}{r} +2.3 \\ 12 \end{array} \quad \begin{array}{r} \text{C. 3.1} \\ 19.6 \end{array}$$

375 61.1 61.78

-1.9 +2.0

$$\begin{array}{r} \text{C. 0.7} \\ 18.1 \end{array} \quad \begin{array}{r} -0.7 \\ 13 \end{array} \quad \begin{array}{r} -0.3 \\ 13 \end{array} \quad \begin{array}{r} \text{F. 0.4} \\ 17.6 \end{array}$$

+50 60.0 60.71

-1.2 +1.3

$$\begin{array}{r} \text{C. 1.0} \\ 18.5 \end{array} \quad \begin{array}{r} -0.4 \\ 0 \end{array} \quad \begin{array}{r} -1.7 \\ 16 \end{array} \quad \begin{array}{r} \text{C. 0.2} \\ 18.1 \end{array}$$

374 58.6 59.48

+0.5 +0.6

$$\begin{array}{r} \text{F. 8.0} \\ 29.0 \end{array} \quad \begin{array}{r} -1.5 \\ 12 \end{array} \quad \begin{array}{r} -0.9 \\ 12 \end{array} \quad \begin{array}{r} \text{F. 0.9} \\ 18.4 \end{array}$$

Sta.	Elev.	Grade
296		571.92
+50		511.26
295		511.60
+50		511.94
294		511.28
+75		511.20
+50		511.12
+25		511.04
293		510.96

L ~~±~~ R

Slope stakes. Co. road.

Hill
Saper
Remmen

9/8/35

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Sta.	Elev.	Grade	Super. El.		$\frac{d}{e}$	
177	570.6	490.70	+0.7-0.7	$\frac{C 7.2}{21.6}$	+20.0	$\frac{C 29.5}{32.5}$
+50	487.9	489.65	+0.7-0.7	$\frac{C 8.1}{22.2}$	+7.8	$\frac{C 20.6}{28.3}$
176	497.3	488.18	+0.7-0.7	$\frac{C 2.8}{19.1}$	+9.1	$\frac{C 8.6}{22.3}$
+50	487.3	486.31	+0.7-0.7	$\frac{F 4.1}{23.6}$	+1.0	$\frac{C 10.0}{23.0}$
175	476.7	484.04	+0.7-0.7	$\frac{F 12.8}{36.2}$	-7.3	$\frac{F 3.2}{21.8}$

Sta.	Elev.	Grade	Super El.			
180	512.5	488.45 ✓	+0.7-0.7	$\frac{C.10.2}{23.1}$	+24.0	$\frac{C.36.2}{36.1}$
+50	514.6	489.81 ✓	+0.7-0.7	$\frac{C.9.7}{22.9}$	+24.3	$\frac{C.12.6}{39.3}$
179	514.1	490.83 ✓	+0.7-0.7	$\frac{C.9.1}{22.5}$	+23.3	$\frac{C.11.0}{40.0}$
+50	510.3	491.41 ✓	+0.7-0.7	$\frac{C.8.0}{22.0}$	+18.9	$\frac{C.32.1}{37.7}$
178	507.0	491.58 ✓	+0.7-0.7	$\frac{C.7.1}{21.5}$	+15.5	$\frac{C.31.6}{32.8}$
177+50	509.0	491.34 ✓	+0.7-0.7	$\frac{C.7.6}{21.8}$	+17.7	$\frac{C.30.0}{33}$

Sta. Elev. Grade

Super. El.

+50 465.8 480.03

F.11.1
38.6

-14.2

F. 5.6
25.4

182 473.8 481.43

+0.2 -0.2

F.16.1
41.6

-7.6

F. 4.9
24.4

181+85 Balance Pt.

181+50 479.8 483.10

+0.1 -0.4

F. 6.6
26.9

-3.3

F. 0.6
17.9

180+96 494.1 489.90

+0.7 -0.7

C. 1.0
20.0

+9.2

C. 8.0
22

181+65⁰⁰ Balance Pt

180+50 496.3 486.70

+0.7 -0.7

C. 10.4
23.2

+9.6

C. 23.4
29.7

Sta	Elev.	Grade				
185+50	490.9	477.22	+2.2 - 2.2	$\frac{C. 7.6}{21.8}$	+13.7	$C. \frac{22.6}{29.3}$
184+96	480.0	477.03	+2.1 - 2.2	$\frac{F. 1.7}{19.6}$	+3.0	$C. \frac{8.8}{22.4}$
+50	476.8	477.09	+1.4 - 1.5	$\frac{F. 3.1}{21.6}$	-0.3	$C. \frac{0.7}{18.4}$
184	474.3	477.13	+0.8 - 0.8	$\frac{F. 11.4}{34.1}$	-3.1	$F. \frac{0.3}{17.5}$
+50	466.4	478.03		$\frac{F. 11.8}{34.7}$	-11.6	$F. \frac{3.6}{22.4}$
183	466.0	478.90		$\frac{F. 12.8}{36.2}$	-12.9	$F. \frac{10.2}{32.3}$

Sta Elev. Grade

Super El.

+50 479.1 479.20

-1.5 +1.5

$\frac{C. 1.2}{18.6}$

-0.1

$C. \frac{2.5}{19.3}$

185 479.6 478.57

$\frac{C. 0.4}{18.2}$

+0.7

$C. \frac{7.6}{21.8}$

+75 Balance Pt

+50 480.2 478.59

+1.3 - 1.3

$\frac{C. 0.3}{18.2}$

+1.7

$C. \frac{16.6}{23.3}$

187 480.3 478.21

+2.2 - 2.2

$\frac{C. 0.6}{18.3}$

+2.1

$C. \frac{21.6}{28.8}$

+50 496.0 477.88

+2.2 - 2.2

$\frac{C. 0.3}{18.2}$

+18.1

$C. \frac{30.3}{33.2}$

186 497.2 477.55

+2.2 - 2.2

$\frac{C. 10.3}{23.2}$

+19.6

$C. \frac{31.2}{33.6}$

Super 3-24-36

Libell
Hemmen

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H

C

H

Sta. Elev. Grade

Super Elev.

+50 479.6 480.79

+2.0, -1.9

$\frac{F 0.7}{18.1}$

-1.2

$\frac{F 2.4}{20.6}$

191 478.0 480.59

+2.0, -1.9

$\frac{F 1.0}{18.5}$

-2.6

$\frac{F 2.5}{20.8}$

+50 477.9 480.10

+2.0, -1.9

$\frac{F 1.1}{18.7}$

-2.5

$\frac{F 2.8}{21.2}$

190 478.4 480.20

+2.0, -1.9

$\frac{F 1.2}{18.8}$

-1.8

$\frac{F 2.2}{20.3}$

189+50 Balance Ft.

+50 479.0 479.87

+2.0, -1.9

$\frac{F 1.3}{19.0}$

-0.9

$\frac{F 2.6}{20.9}$

189 479.1 479.54

-2.0

$\frac{C 0.6}{18.3}$
 $\frac{C 1.1}{18.6}$

-0.1

$\frac{C 1.1}{18.6}$
 ~~$\frac{C 0.9}{18.5}$~~

Sta. Elev. Grade

Super El.

H

C

FL

+50 482.5 481.57

0.2

193. 482.2 481.37

0.2

+50 481.7 481.18

-1.5 16

$\frac{C 0.6}{18.3}$

+0.5

$\frac{Gr.}{17.0}$

192 480.8 480.98

+2.0, -1.9

$\frac{Gr.}{18.0}$

-0.2

$\frac{F 1.8}{18.8}$

Slope stakes Co. road

Sta Elev Grade

53

155 452.3 458.02

$\frac{F. 5.6}{25.9}$

-5.7

$\frac{F. 5.6}{25.9}$

+50 452.1 458.18

$\frac{F. 6.1}{26.2}$

-6.1

$\frac{F. 6.1}{26.2}$

154 451.6 458.35

$\frac{F. 6.8}{27.2}$

-6.8

$\frac{F. 6.8}{27.2}$

+50 451.5 458.51

$\frac{F. 7.0}{27.5}$

-7.0

$\frac{F. 6.8}{27.2}$

153 451.0 458.67

$\frac{F. 7.4}{28.1}$

-7.7

$\frac{F. 7.4}{28.1}$

Sta. Elev. Grade

153 150 453.4 457.40

F. 3.8
227

-4.0

F. 4.0
23.0

157 153.0 457.38

F. 4.4
236

-4.4

F. 4.3
23.5

+ 50 Balance Pt.

150 152.8 457.53

F. 4.6
239

-4.7

F. 4.6
23.9

156 152.6 457.69

F. 5.2
248

-5.1

F. 5.0
24.5

155+50 452.5 457.85

F. 5.8
247

-5.4

F. 5.3
25.0

Sta. Elev. Grade

160 459.8 459.06

$$\frac{F. 1.2}{23.3}$$

-4.3

$$F. \frac{4.2}{23.3}$$

+50 454.4 458.69

$$\frac{F. 3.8}{22.7}$$

-4.3

$$F. \frac{4.2}{23.3}$$

159 454.3 458.32

$$\frac{F. 3.8}{22.7}$$

-4.0

$$F. \frac{4.0}{23.0}$$

+50 454.0 457.94

$$\frac{F. 4.0}{23.0}$$

-3.9

$$F. \frac{4.0}{23.0}$$

158 453.8 457.60

$$\frac{F. 3.9}{22.8}$$

-3.8

$$F. \frac{4.1}{23.1}$$

sta. Elev. Grade

+50 455.7 460.92

-5.2

162 455.8 460.55

-4.9

+50 455.6 460.18

-4.6

161 455.3 459.81

F. 1.0
23.0

-4.5

F. 1.7
24.1

160+50 455.0 459.43

F. 1.0
23.0

-4.4

F. 4.7
23.6

Oct. 15 1935

Super
Elevations

59

Sta.	d Elev	Grade	Grade rod	Super Elev. C. F.	L	R.
296	506.7	511.92	-5.2		$\frac{F 4.4}{23.6}$	$\frac{F 4.1}{23.1}$
+50	506.2	511.76	-5.6		$\frac{F 4.8}{24.2}$	$\frac{F 4.4}{23.6}$
295	506.3	511.60	-5.3	0.7 0.6	$\frac{F 9.2}{29.3}$	$\frac{F 4.4}{23.6}$
+50	505.4	511.44	-6.0	1.3 1.3	$\frac{F 9.7}{31.6}$	$\frac{F 4.0}{23.0}$
+25	505.9	511.36	-5.5	1.7 1.6	$\frac{F 10.6}{32.9}$	$\frac{F 2.2}{20.3}$
294	509.6	511.28	-1.7	2.0 1.9	$\frac{F 10.9}{33.4}$	$\frac{F 2.1}{20.3}$
+75	508.9	511.20	-2.3	2.0 1.9	$\frac{F 4.8}{24.2}$	$\frac{C 15.6 \text{ vert}}{18.0 \text{ cut}}$
+50		511.12				
+35	503.8	511.07	+22.7	2.0 1.9		$\frac{C 30.8 \text{ vert}}{18.0 \text{ cut}}$
+25		511.04				
293	509.2	510.96	-1.8	2.0 1.9	$\frac{F 5.2}{24.8}$	$\frac{C 3.5 \text{ vert}}{18.0 \text{ cut}}$

Note: Use $\frac{1}{2}$ grade on inside of

curve for super-elevating. Vertical cut around Cape Horn - 18' out.

Sta.	Q. El.	Grade	Grade red	L	R.
+30	509.3	513.36	-4.1	$\frac{F 6.8}{27.2}$	$\frac{F 2.3}{20.5}$
300	509.0	513.20	-4.2	$\frac{F 6.1}{26.1}$	$\frac{F 3.7}{21.0}$
+50	508.7	513.09	-4.3	$\frac{F 5.5}{25.3}$	$\frac{F 2.3}{20.5}$
299	508.3	512.88	-4.6	$\frac{F 5.0}{24.5}$	$\frac{F 3.4}{22.1}$
+50	507.9	512.72	-4.8	$\frac{F 4.8}{24.2}$	$\frac{F 3.4}{22.1}$
298	507.9	512.56	-5.2	$\frac{F 4.6}{23.9}$	$\frac{F 3.0}{21.5}$
+50	507.6	512.40	-4.8	$\frac{F 4.6}{23.9}$	$\frac{F 4.0}{23.0}$
297	507.0	512.24	-5.2	$\frac{F 4.8}{24.2}$	$\frac{F 3.7}{22.5}$
296+50	506.9	512.08	-5.2	$\frac{F 5.1}{24.6}$	$\frac{F 3.8}{21.7}$

Oct. 17 1935
Super
Remains

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Sta.	Elev.	Grade	Grade rod	Super cut	elev. Fill	L.	¢	R
245		503.90						
+90	519.2	503.87	+15.3			$\frac{F.2.1}{20.1}$		$\frac{C.30.0}{33.0}$
+50	518.3	503.73	+14.6	0.36	0.33	$\frac{F.2.7}{20.8}$		$\frac{C.27.2}{31.6}$
244	516.9	503.56	+13.3	0.85	0.80	$\frac{F.2.1}{20.1}$		$\frac{C.23.8}{29.9}$
+50	513.6	503.38	+10.2	1.33	1.25	$\frac{F.0.9}{18.4}$		$\frac{C.19.6}{27.8}$
243	500.7	503.21	-2.5	1.11	1.36	$\frac{F.1.2}{18.8}$		$\frac{C.6.2}{21.1}$
+50	499.5	503.03	-3.5	1.44	1.36	$\frac{F.2.8}{21.2}$		$\frac{F.3.0}{21.5}$
242	499.2	502.86	-3.7	1.11	1.36	$\frac{F.3.0}{21.5}$		$\frac{F.3.4}{22.1}$
+50	499.5	502.69	-3.2	1.11	1.36			
241	499.6	502.51	-2.9	1.11	1.36			

Sta.	± Elev.	Grade	Grade Rod	L.	☉	R.
+50	524.9	505.47	+19.4	Grade <u>21.9</u>	20.0 +12.2	C 28.5 <u>32.3</u>
249	525.4	505.30	+20.1	Grade <u>18.5</u>	11.0 +16.0	C 29.2 <u>32.6</u>
+50	514.5	505.12	+9.4	F 0.2 <u>17.3</u>		C 21.1 <u>28.6</u>
248	504.2	504.95	-0.8	F 1.6 <u>19.4</u>		C 3.9 <u>19.9</u>
+50	503.7	504.77	-1.1	F 8.2 <u>29.3</u>		F 0.7 <u>18.0</u>
247	503.6	504.60	-1.0	F 8.3 <u>29.5</u>		F 0.4 <u>17.6</u>
+50	503.3	504.43	-1.1	F 7.4 <u>28.1</u>		C 2.3 <u>19.2</u>
246	503.0	504.26	-1.3	F 1.6 <u>19.4</u>		C 17.0 <u>26.5</u>
245+50	507.6	504.08	+3.5	F 1.4 <u>19.1</u>		C 24.6 <u>30.3</u>

↑
Note - Advisable
to daylight
these sections.

↓

Oct. 18, 1935

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Sta.	ℓ Elev	Grade	Grade Rod.	Super Cut	Elev. Fill	L.	℄	R
254	505.2	505.42	-0.2	1.4	1.3	$\frac{C 0.3}{19.2}$ $\frac{C 1.7}{18.9}$ $\frac{F 0.5}{17.8}$		$\frac{C 6.4}{21.2}$ $\frac{C 8.0}{22.0}$ $\frac{C 10.7}{23.4}$ $\frac{C 12.3}{24.2}$
+50	516.1	505.51	+10.6	1.4	1.3	$\frac{C 0.7}{18.3}$		$\frac{C 9.7}{22.9}$ $\frac{C 11.3}{23.7}$
253	514.7	505.60	+9.1	1.4	1.3	$\frac{Grade}{20.7}$ $\frac{Grade}{22.1}$		$\frac{C 7.4}{21.7}$ $\frac{C 8.4}{22.2}$
+50	510.5	505.70	+4.8	1.0	0.9	$\frac{C 1.3}{19.7}$ $\frac{C 2.2}{19.1}$ $\frac{F 5.1}{24.7}$		$\frac{C 1.0}{18.5}$ $\frac{C 1.5}{18.8}$
252	503.8	505.80	-2.0	0.5	0.4	$\frac{F 4.8}{21.2}$		
(Use ℄ grade on inside of curve)								
+50	511.8	505.90	+5.9			$\frac{F 0.6}{17.9}$		$\frac{C 11.7}{23.8}$
251	511.9	506.00	+5.9			$\frac{F 4.2}{23.3}$		$\frac{C 14.7}{25.4}$
+50	519.1	505.82	+13.3			$\frac{C 4.8}{20.4}$		$\frac{C 22.3}{29.1}$
250	523.3	505.64	+17.7			$\frac{C 9.9}{22.9}$		$\frac{C 25.6}{30.8}$

Sta.	℄ Elev.	Grade	Super	Elev.	L	℄	R
		Rod	Cut	Fill			
+50	500.6	504.61	-4.0			F3.9 22.9	F3.5 22.3
258	500.7	504.70	-4.0			F4.0 23.0 F4.0 23.0	F3.8 22.7 F4.0 23.0
+50	500.7	504.79	-4.1			F4.3 23.5 F4.1 23.2	F4.0 23.0 F3.9 22.9
257	500.9	504.88	-4.0			F4.1 23.2	F3.9 22.9
+50	501.0	504.97	-4.0	0.5	0.4	F3.6 22.4	F4.2 23.3
256	501.4	505.06	-3.7	1.0	0.9	F3.6 22.4 F2.7 21.0	F5.3 25.0 F4.4 23.6
+50	501.8	505.16	-3.4	1.4	1.3	F4.7 24.1 F3.4 22.1	F5.4 25.1 F4.2 23.3
255	500.3	505.24	-4.9	1.4	1.3	F5.2 24.8 F3.6 22.4	F4.0 23.0 F2.8 20.8
254+50	504.9	505.33	-0.4	1.4	1.3	F5.5 25.3 F2.5 20.8	F2.9 21.4 F1.7 19.5

↑
staked on 100ft stations
Moved on new alignment

(Use ℄ grade on inside of curve)

Sta.	± Elev.	Grade	Grade
		±	Red.
263	501.8	503.81	-2.0
+50	501.5	503.89	-2.4
262	501.6	503.98	-2.4
+50	501.5	504.07	-2.6
261	501.3	504.16	-2.9
+50	501.1	504.25	-3.2
260	501.1	504.34	-3.2
+50	500.8	504.43	-3.6
259	500.8	504.52	-3.7

$$\begin{array}{r} L. \\ F2.2 \\ \hline F2.0 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} F2.3 \\ \hline 20.5 \\ F2.4 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} F2.4 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} F2.5 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} F3.0 \\ \hline 21.5 \end{array}$$

$$\begin{array}{r} F2.8 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} F3.2 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} F3.4 \\ \hline 22.1 \end{array}$$

$$\begin{array}{r} F3.4 \\ \hline 22.1 \end{array}$$

$$\begin{array}{r} F3.5 \\ \hline 22.3 \end{array}$$

$$\begin{array}{r} F3.6 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} F3.6 \\ \hline 22.4 \end{array}$$

C

R

$$\begin{array}{r} F2.0 \\ \hline 20.0 \\ F2.0 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} F2.0 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} F2.3 \\ \hline 20.5 \end{array}$$

$$\begin{array}{r} F2.3 \\ \hline 20.5 \end{array}$$

$$\begin{array}{r} F2.8 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} F2.8 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} F2.7 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} F3.0 \\ \hline 21.5 \end{array}$$

$$\begin{array}{r} F3.1 \\ \hline 21.7 \end{array}$$

$$\begin{array}{r} F3.1 \\ \hline 21.7 \end{array}$$

$$\begin{array}{r} F3.4 \\ \hline 22.1 \end{array}$$

$$\begin{array}{r} F3.5 \\ \hline 22.3 \end{array}$$

$$\begin{array}{r} F3.5 \\ \hline 22.3 \end{array}$$

Sta. E Elev. Grade
Rod.

L

C

R

+39.79	501.1	503.20	-2.1	0.1	0.1
266	501.1	503.27	-2.2	0.1	0.1
+50	501.9	503.36	-1.5	0.2	0.2
265	501.7	503.45	-2.4	0.1	0.1
+50	502.8	503.54	-0.7	0.1	0.1
264	501.7	503.63	-1.9		
263+50	501.6	503.72	-2.1		

$$\frac{F1.8}{19.7}$$

$$\frac{F2.1}{20.2}$$

$$\frac{F2.1}{20.2}$$

$$\frac{F2.1}{20.2}$$

$$\frac{F4.9}{24.4}$$

$$\frac{F4.9}{24.4}$$

$$\frac{F1.0}{18.5}$$

$$\frac{F1.4}{19.1}$$

$$\frac{F1.5}{19.3}$$

$$\frac{F2.1}{20.2}$$

$$\frac{F2.2}{20.3}$$

$$\frac{F3.3}{22.0}$$

$$\frac{F1.9}{17.9}$$

$$\frac{F2.5}{20.8}$$

$$\frac{F0.6}{17.9}$$

$$\frac{C0.6}{18.3}$$

$$\frac{F0.9}{18.3}$$

$$\frac{F1.7}{19.5}$$

$$\frac{F2.2}{20.3}$$

$$\frac{F1.8}{18.7}$$

Oct. 21 1935
Super - Remmen

67

Sta.	Elev.	Grade	Grade Rod	Super Cut	Elev Fill	L.	Q	R
228	494.0	492.48	+1.5	1.0	0.9	$\frac{F 6.3}{24.5}$ $\frac{F 5.4}{25.1}$		$\frac{C 1.7}{18.9}$ $\frac{C 2.7}{19.4}$
E.V.C.	+50 493.2	491.89	+1.3	0.5	0.45	$\frac{F 5.8}{25.7}$ $\frac{F 5.1}{24.7}$		$\frac{C 1.1}{18.6}$ $\frac{C 1.6}{18.8}$
								(Note: Use $\frac{1}{2}$ grade on inside of curve)
227	491.7	491.38	+0.3			$\frac{F 4.0}{23.0}$		$\frac{Grade}{18.0}$
	+50 490.5	491.06	-0.6			$\frac{F 3.8}{22.7}$		$\frac{F 0.3}{17.5}$
226	490.2	490.91	-0.7			$\frac{F 3.8}{22.7}$		$\frac{F 0.5}{17.8}$
B.V.C.	+50 489.7	490.95	-1.2			$\frac{F 3.2}{21.8}$		$\frac{F 1.0}{18.5}$
225	489.1	491.07	-2.0			$\frac{F 3.9}{22.9}$		$\frac{F 1.8}{19.7}$
	+50 488.8	491.20	-2.4			$\frac{F 3.8}{22.7}$		$\frac{F 1.7}{19.5}$
224	488.8	491.32	-2.5			$\frac{F 5.2}{24.8}$		$\frac{F 2.2}{20.2}$

Sta.	± Elev.	Grade	Grade Rod	Super Cut	Elev. Fill	L.	Q	R
2	+50 503.7	499.84	+5.9	1.4	1.3	$\frac{C 0.4}{C 1.8 \cancel{18.2}}$ $\frac{17.9}{17.9}$		$\frac{C 21.8}{23.9}$ $\frac{C 23.5}{27.8}$
232	503.6	497.25	+6.4	1.4	1.3	$\frac{F 9.0}{30.5}$ $\frac{F 6.8}{27.2}$		$\frac{C 19.6}{27.8}$ $\frac{C 21.3}{27.1}$
2	+50 503.4	496.65	+6.8	1.4	1.3	$\frac{F 10.1}{32.2}$ $\frac{F 8.6}{29.9}$		$\frac{C 6.5}{21.3}$ $\frac{C 7.9}{27.0}$
231	500.2	496.05	+4.1	1.4	1.3	$\frac{F 9.6}{31.4}$ $\frac{F 8.1}{29.2}$		$\frac{C 6.7}{21.4}$ $\frac{C 8.1}{27.1}$
2	+50 495.9	495.46	+0.4	1.4	1.3	$\frac{F 9.3}{31.0}$ $\frac{F 7.8}{28.7}$		$\frac{C 6.8}{21.1}$ $\frac{C 7.6}{27.8}$
230	493.2	494.86	-1.7	1.4	1.3	$\frac{F 9.6}{31.4}$ $\frac{F 8.0}{29.0}$		$\frac{C 5.0}{20.5}$ $\frac{C 6.4}{27.2}$
2	+50 491.5	494.29	-2.8	1.4	1.3	$\frac{F 9.0}{30.5}$ $\frac{F 7.6}{28.4}$		$\frac{C 3.7}{19.9}$ $\frac{C 5.1}{20.5}$
229	491.3	493.67	-2.4	1.4	1.3	$\frac{F 8.0}{29.0}$ $\frac{F 6.4}{26.6}$		$\frac{C 3.0}{19.5}$ $\frac{C 4.4}{20.2}$
228+50	494.6	493.08	+1.5	1.4	1.3	$\frac{F 6.9}{27.4}$ $\frac{F 5.6}{25.4}$		$\frac{C 2.4}{17.2}$ $\frac{C 3.9}{20.0}$

(Use ± grade on inside of curve)

Oct. 22 1935
Saper - Remmen

Sta.	L. Elev.	Grade	Grade Rod	Super Cut	Elev. Fill	Q	R
237	493.6	501.62	- 8.0		$\frac{F 8.2}{29.3}$		$\frac{F 7.3}{28.0}$
+50	493.2	501.55	- 8.3		$\frac{F 8.9}{30.4}$		$\frac{F 6.9}{27.4}$
236	493.4	501.41	- 8.0		$\frac{F 8.8}{30.2}$		$\frac{F 6.6}{26.9}$
+50	492.8	501.14	- 8.3	0.3	$\frac{F 9.5}{31.3}$ $\frac{F 9.2}{30.8}$	0.3	$\frac{F 3.0}{31.5}$ $\frac{F 2.7}{31.1}$
235	504.2	500.76	+ 3.4	0.9	$\frac{F 10.7}{33.1}$ $\frac{F 9.9}{31.9}$	0.8	$\frac{C 3.3}{29.7}$ $\frac{C 4.2}{30.1}$
+50	504.8	500.22	+ 4.6	1.3	$\frac{C 3.6}{19.8}$ $\frac{C 4.9}{30.5}$	1.2	$\frac{C 22.9}{29.5}$ $\frac{C 24.8}{30.4}$
234	504.4	499.63	+ 4.8	1.4	$\frac{C 3.2}{19.6}$ $\frac{C 4.6}{29.3}$	1.3	$\frac{C 27.5}{31.8}$ $\frac{C 29.4}{32.7}$
+50	503.6	499.03	+ 4.6	1.4	$\frac{C 2.8}{19.4}$ $\frac{C 4.2}{26.1}$	1.3	$\frac{C 27.7}{31.9}$ $\frac{C 29.2}{32.6}$
233	503.4	498.44	+ 5.0	1.4	$\frac{C 2.8}{19.4}$ $\frac{C 4.2}{20.1}$	1.3	$\frac{C 23.5}{29.8}$ $\frac{C 25.8}{30.9}$

(Use $\frac{1}{2}$ grade on inside of curve)

Sta.	± Elev.	Grade	Grade Rod	Super Cut	Elev. Fill	L.	⊕	R
+50	499.5	502.69	-3.2	1.44	1.36	$\frac{F 2.6}{20.9}$		$\frac{F 3.0}{21.5}$
241	499.6	502.51	-2.9	1.44	1.36	$\frac{F 4.1}{23.2}$		$\frac{F 3.3}{22.0}$
+50	499.7	502.35	-2.6	1.44	1.36	$\frac{F 5.4}{25.1}$		$\frac{F 3.0}{21.5}$
240	500.4	502.17	-1.8	1.3	1.2	$\frac{F 5.3}{25.0}$		$\frac{F 2.4}{20.6}$
+50	502.2	502.00	+0.2	0.8	0.7	$\frac{F 5.8}{25.7}$		$\frac{F 0.2}{17.3}$
239	502.2	501.92	+0.3	0.3	0.3	$\frac{F 6.9}{27.4}$		$\frac{C 0.9}{18.5}$
+50	494.0	501.85	-7.8			$\frac{F 7.9}{28.9}$		$\frac{F 1.3}{19.0}$
238	493.6	501.77	-8.2			$\frac{F 8.4}{29.6}$		$\frac{F 7.3}{28.0}$
237+50	493.5	501.70	-8.2			$\frac{F 8.4}{29.6}$		$\frac{F 7.4}{28.1}$

Oct. 24 1935
Soper-Remmen

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Sta	ℒ Elev.	Grade	Grade Rod.	Super Cut	Elev. Fill	L	ℒ	R
+50	488.3	491.45	-3.2			$\frac{F 5.9}{25.9}$		$\frac{F 2.0}{20.0}$
223	488.3	491.57	-3.3	0.1	0.1	$\frac{F 5.6}{25.4}$		$\frac{F 2.1}{20.2}$
+50	488.7	491.70	-3.0	0.2	0.2	$\frac{F 4.7}{24.1}$		$\frac{F 2.2}{20.3}$
222	489.3	491.56	-2.3	0.2	0.2	$\frac{F 2.9}{21.4}$		$\frac{F 1.6}{19.4}$
+50	489.6	491.42	-1.8	0.2	0.2	$\frac{F 2.8}{21.2}$		$\frac{F 2.6}{20.9}$
221	489.9	491.28	-1.4	0.1	0.1	$\frac{F 2.6}{20.9}$		$\frac{F 1.9}{19.9}$
+50	490.2	491.14	-0.9			$\frac{F 2.1}{20.3}$		$\frac{F 1.3}{19.0}$
220	490.2	491.00	-0.8			$\frac{F 2.3}{20.5}$		$\frac{F 0.8}{18.2}$
+50	490.1	490.85	-0.8			$\frac{F 1.6}{19.4}$		$\frac{F 0.8}{18.2}$
219	490.4	490.70	-0.3			$\frac{F 2.7}{21.1}$		$\frac{F 0.5}{17.8}$

Oct 25 1935
Soper - Remmen

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Sta.	L Elev.	Grade	G. Rod	L	Q	R
+50	458.4	463.17	-4.8	$\frac{F4.8}{24.2}$		$\frac{F4.8}{24.2}$
165	457.8	462.80	-5.0	$\frac{F4.2}{23.3}$		$\frac{F4.7}{24.1}$
+50	457.8	462.42	-4.6	$\frac{F4.1}{23.2}$		$\frac{F4.5}{23.8}$
164	458.4	462.05	-3.6	$\frac{F3.7}{22.6}$		$\frac{F4.3}{23.5}$
+50	457.6	461.68	-4.1	$\frac{F5.3}{25.0}$		$\frac{F3.1}{21.7}$
163	455.8	461.30	-5.5	$\frac{F5.5}{25.3}$		$\frac{F6.0}{26.0}$
+50	455.7	460.93	-5.2	$\frac{F4.9}{24.4}$		$\frac{F5.1}{24.7}$
162	455.8	460.56	-4.8	$\frac{F4.4}{23.6}$		$\frac{F4.8}{24.2}$
161+50	455.6	460.18	-4.6	$\frac{F4.4}{23.6}$		$\frac{F4.7}{24.1}$

Sta L Elev. Grade G. Rod

170 466.1 466.53 -0.4

+50 465.9 466.15 -0.3

169 465.6 465.78 -0.2

+50 465.2 465.41 -0.2

168 461.8 465.03 -3.2

+50 460.9 464.66 -3.8

167 460.3 464.29 -4.0

+50 459.2 463.91 -4.7

166 458.8 463.54 -4.7

L

Q

R

$\frac{\text{Grade}}{17.0}$

$\frac{\text{Grade}}{17.0}$

$\frac{\text{Grade}}{17.0}$

$\frac{F 0.9}{18.4}$

$\frac{F 3.7}{22.6}$

$\frac{F 3.7}{22.5}$

$\frac{F 4.1}{23.2}$

$\frac{F 4.7}{24.1}$

$\frac{F 4.5}{23.8}$

$\frac{\text{Grade}}{17.0}$

$\frac{F 0.2}{17.3}$

$\frac{F 0.2}{17.3}$

$\frac{\text{Grade}}{17.0}$

$\frac{F 2.9}{21.4}$

$\frac{F 3.5}{22.3}$

$\frac{F 3.0}{21.5}$

$\frac{F 2.5}{20.8}$

$\frac{F 4.8}{24.2}$

Oct 26 1935
Super - Remmen

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Sta.	Q. Elev.	Grade	G. Rod	Super Elev.		L	Q	R
				Cut	Fill			
+50	470.5	481.50	-11.0	0.3	0.3	$\frac{F12.0}{35.0}$	$\frac{F7.8}{28.7}$	
174	469.4	478.80	-9.4			$\frac{F10.5}{32.8}$	$\frac{F8.1}{29.2}$	
E.V.C.								
+50	468.4	476.10	-7.7			$\frac{F8.0}{29.0}$	$\frac{F7.0}{27.5}$	
173	467.8	473.59	-5.8			$\frac{F5.9}{25.9}$	$\frac{F4.9}{24.4}$	
+50	467.5	471.48	-4.0			$\frac{F4.1}{23.2}$	$\frac{F3.7}{22.6}$	
172	467.1	469.75	-2.7			$\frac{F2.7}{21.1}$	$\frac{F2.4}{20.6}$	
+50	466.9	468.41	-1.5			$\frac{F1.3}{19.0}$	$\frac{F1.2}{18.8}$	
171	466.6	467.46	-0.9			$\frac{F0.8}{18.2}$	$\frac{F1.0}{18.5}$	
B.V.C.								
170+50	466.4	466.90	-0.5			$\frac{F0.3}{17.5}$	$\frac{F0.6}{17.9}$	

Sta.	℄ Elev.	Grade	G. Rod	Super Cut	Elev. Fill	L	℄	R
+50	451.4	453.16	-1.8					
136	457.8	453.04	+4.8					
+50	460.6	452.92	+7.7	0.3	0.3			
135	461.2	452.80	+8.4	0.9	0.9			
+50	453.2	452.68	+0.5	1.6	1.4			
134	453.3	452.56	+0.7	1.9	1.8			
+50	453.1	452.44	+0.7	1.9	1.8			
133	459.2	452.32	+6.9	1.9	1.8			
132+50	462.7	452.20	+10.5	1.2	1.2			

Sta.	C. Elev	Grade	G. Rod.	Super Cut	Elev. Fill	L	C	R
141	453.6	454.24	-0.6	0.5	0.5			
	+50	453.5	454.12	-0.6				
140	453.0	454.00	-1.0					
	+50	451.5	453.88	-2.4				
139	451.0	453.76	-2.8					
	+50	449.1	453.64	-4.5				
138	448.0	453.52	-5.5					
	+50		453.40					
137	452.2	453.28	-1.1					

$\frac{F 0.5}{17.8}$

Sta.	R. Elev.	Grade	G. Rod.	Super Cut	Elev. Fill	L	C	R
+50	457.6	455.99	+1.6			$\frac{\text{Grade}}{17.0}$		$\frac{C 25.1}{30.6}$
145	457.5	455.76	+1.7			$\frac{C 2.0}{19.0}$		$\frac{C 30.2}{33.1}$
+50	457.5	455.53	+2.0					
144	457.4	455.29	+2.1					
+50	456.8	455.06	+1.7	0.5	0.5	$\frac{C 1.0}{18.5}$		
143	456.0	454.83	+1.2	1.0	0.9	$\frac{C 0.3}{18.2}$		
+50	454.9	454.60	+0.3	1.4	1.3	$\frac{F 0.2}{17.3}$		
142	454.1	454.48	-0.4	1.4	1.3	$\frac{F 0.8}{18.2}$		
141 +50	453.6	454.36	-0.8	1.0	0.9	$\frac{F 0.7}{18.1}$		

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Sta	ℓ Elev.	Grade	G. Rod	L	ℓ	R
150	460.5	458.07	+2.4	$\frac{C 2.8}{19.4}$		$\frac{C 19.0}{27.5}$
+50	460.7	457.84	+2.9	$\frac{C 1.6}{18.8}$		$\frac{C 13.6}{24.8}$
149	459.8	457.61	+2.2	$\frac{F 8.1}{29.2}$		$\frac{C 10.8}{23.4}$
+50	459.0	457.38	+1.6	$\frac{F 7.8}{28.7}$		$\frac{C 14.1}{25.1}$
148	458.6	457.15	+1.4	$\frac{F 8.0}{29.0}$		$\frac{C 13.5}{24.8}$
+50	458.1	456.92	+1.2	$\frac{F 7.8}{28.7}$		$\frac{C 1.0}{18.5}$
147	457.8	456.68	+1.1	$\frac{F 7.9}{28.9}$		$\frac{C 1.9}{19.0}$
+50	457.9	456.45	+1.4	$\frac{F 7.8}{28.7}$		$\frac{C 2.0}{19.0}$
146	458.0	456.22	+1.8	$\frac{F 7.8}{28.7}$		$\frac{C 14.2}{25.1}$

cont'd on page 59

Sta.	℄ Elev.	Grade	G. Rod	Superelev.	
				C	F
292+50	509.9	510.80	-0.9	2.0	19
292	510.2	510.64	-0.4	1.6	1.6
+50	510.1	510.48	-0.4	0.9	0.9
291	510.0	510.32	-0.3	0.2	0.2
+50	463.1	458.84	+4.3		
152	460.8	459.00	+1.8		
+50	460.2	458.77	+1.4		
151	459.9	458.54	+1.4		
150+50	459.7	458.30	+1.4		

L	℄	R
$\frac{F 5.0}{24.5}$		$\frac{F 0.8}{18.2}$
$\frac{F 3.5}{22.3}$		$\frac{F 0.3}{17.5}$
$\frac{F 1.9}{19.9}$		$\frac{F 0.3}{17.5}$
$\frac{F 0.2}{17.3}$		$\frac{F 0.2}{17.3}$
	$\frac{F 8.0}{29.0}$	$\frac{C 2.5}{19.3}$
	$\frac{C 3.7}{19.9}$	$\frac{C 25.1}{30.6}$
	$\frac{C 2.2}{19.1}$	$\frac{C 29.3}{32.7}$
	$\frac{C 2.1}{19.0}$	$\frac{C 29.3}{32.7}$
	$\frac{C 1.8}{18.9}$	$\frac{C 23.4}{29.7}$

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Read stations of curves where $\frac{e}{r}$ elevations to be
carried on inside of curve for super-elevating

77+83.50 to 81+69.80

199+71.25 to 204+67.27

227+94.14 to 234+84.24 x

251+54.75 to 255+96.85 x

272+27.74 to $\frac{279+32.19}{279+08.09}$

291+85.27 to 294+41.92 x Cape Horn

314+86.22 to 316+71.88 x

328+60.84 to 330+87.15 x

337+14.44 to 341+22.12 x

346+41.65 to 352+17.16 x

355+74.26 to 357+26.22 x

367+35.84 to 369+43.10 x

x=changed

