

W
5/2

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

512

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1 1/2 see inside of back cover.

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Level Notes - Mussey Grave - Jamison Prop. 1 - 3 (c)

Level Notes - Mussey Grove to Brooks prop. 4 - 8

Stadia around 775 Contour - Brooks prop. 10 - 14

Levels from Mussey Grove to 610 Contour
on Jamison property.

B.M. # 43 536.60

3.84 540.44

TP 2.05 538.39

4.66 543.05

TP 10.98 532.07

5.54 537.61

TP 2.33 535.28

3.18 538.46

TP 5.82 532.64

6.03 538.67

TP 2.64 536.03

5.36 541.39

TP = B.M. 1.65 539.74

4.43 544.17

TP 3.20 540.97

5.66 546.63

TP 3.05 543.58

Oct. 30 1935

Converse

Soper

Remmen

R.R. spike in live oak 18' H. 621+02 - (400' West of Mussey Grove)

Set B.M. Point on protruding boulder 18" above stream bed. East bank.

543.58

5.31 548.89

T.P. 2.96 545.93

6.27 552.20

T.P. 2.72 549.48

5.40 554.88

T.P. 3.32 551.56

9.28 560.84

T.P. 2.63 558.21

12.31 570.52

T.P. 0.05 570.47

12.01 582.48

T.P. 0.23 582.20

12.14 594.34

T.P. 0.16 594.18

12.19 606.37

T.P. 0.71 605.66

10.98 616.64

616.64

TP

6.64 610.00

← on old 610' contour stake

12.90 622.90

TP

11.37 611.53

5.79 617.32

TP

7.37 609.95

on old 610' stake

8.73 618.69

TP

9.65 609.03

5.49 614.52

TP

4.51 610.01

7.15 617.16

TP

7.15 610.01

5.00 615.01

Nov. 4 1935
Converse
Soper
Remmen

4

B.M.^d 43 536.60

4.61 541.21

T.P. 3.35 537.86

12.89 550.75

T.P. 0.31 550.44

9.12 559.56

T.P. 0.32 559.24

12.88 572.12

T.P. 2.77 569.35

9.45 578.80

T.P. 0.13 578.67

12.12 590.⁷⁹89

T.P. 0.17 590.⁶¹72

12.97 603.⁵⁹67

T.P. 0.18 603.⁴¹71

11.79 615.⁷⁰90
614.90

T.P. 0.17 615.⁰³03
614.33

85.85

7.40

614.33 85.85
536.60 7.40
77.73 78.45

TP
 8.46 $\begin{matrix} 623.49 \\ 622.79 \end{matrix}$

615.03
 614.33

13.75 609.74

check on old 610 contour stake

TP
 0.07 $\begin{matrix} 613.47 \\ 614.96 \end{matrix}$

$\begin{matrix} 623.49 \\ 614.96 \\ \hline 8.46 \end{matrix}$

12.72 627.63

↑

$\begin{matrix} 775 \\ 8.46 \\ \hline 766.54 \end{matrix}$

TP
 0.06 627.62

12.75 640.37

TP
 0.09 640.29

12.83 653.12

TP
 0.10 653.02

12.60 665.62

TP
 0.14 665.48

12.59 678.07

TP
 0.07 678.00

12.83 690.83

TP
 0.11 690.72

12.32 703.04

TP
 0.20 702.84

97.10

.83

These elevations all 8.46 too low

$\begin{matrix} 702.84 \\ 615.03 \\ \hline 87.81 \end{matrix}$
 $\begin{matrix} 97.10 \\ .83 \\ \hline 96.27 \\ 87.81 \\ \hline 8.46 \end{matrix}$

Nov. 5 1935

6.

			702.84
	11.90	714.74	
TP			0.25 714.49
	10.11	724.60	
TP			0.38 724.22
	12.28	736.50	
TP			0.04 736.46
	12.48	748.94	
TP			0.20 748.74
	12.57	761.31	
TP			0.19 761.12
	12.59	773.71	
TP			0.35 773.36
	12.70	786.06	
TP			10.56 775.50
	12.45	787.95	
	97.08		12.90 775.05
	12.76	787.81	

These elevations all 8.46 too low

775.05
 702.84
 72.21
 97.08
 24.87
 72.21

787.81

787.81

TP 12.79 775.02

5.40 780.42

TP 0.51 779.91

7.30 787.21

TP 12.18 775.03

8.09 783.12

TP 4.49 778.63

1.41 780.04

TP 3.18 776.86

6.03 782.89

TP 6.85 776.04

10.41 786.44

TP 8.12 778.32

2.01 780.33

TP 3.76 776.57

7.28 783.85

TP 9.09 774.76

60.69

60.97

These elevations all 8.46 too low

775.05	60.97
776.76	60.69
.29	.28

TP 774.76

11.98 786.74

TP 11.36 775.38

5.20 780.58

TP 12.88 767.70

12.49 780.19

TP 5.15 775.04

12.42 787.46

TP 12.48 774.98

47.09

↓
36.87

These elevations 8.46 low

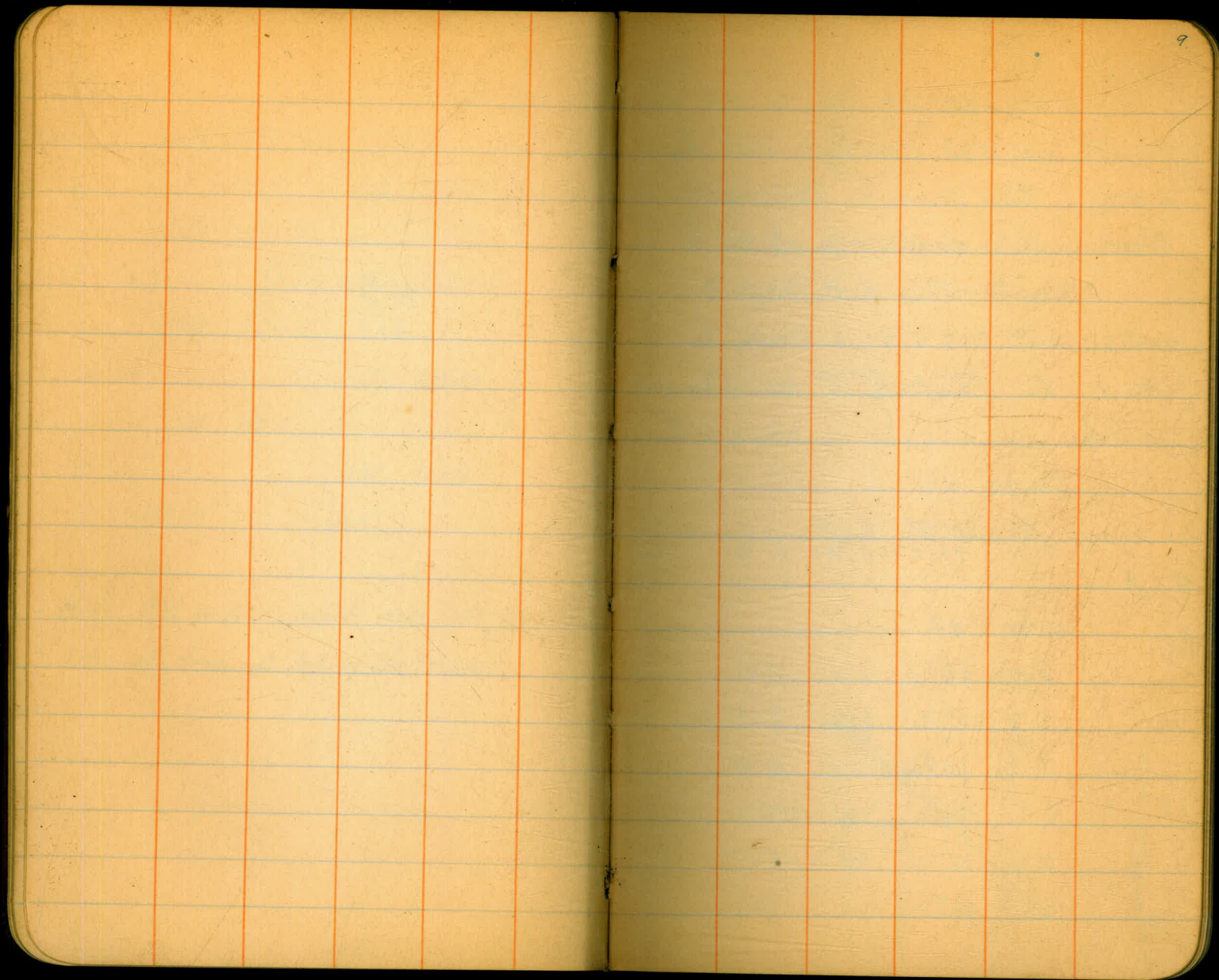
47.09
46.87

0.22

774.98
774.76

.22

Note: 775 Contour points were set up
8.46 at time of taking stadia shots



Location by Stadia of
 points on 775 contour set by
 Level, San Vicente Reservoir
 Basin, S. 1/2 and N.W. 1/4 of S.E. 1/4
 Sec. 20, T. 14 S. R. 1 E.

From To Hor. Angle. Stadia Dist. Vert. Δ. Hor. Dist.
 π 1/4 Cor.

Sec. Cor. 00

π A
 A 117°33' 602 00 602.0
 5-1 90°0' 118 5°30' 117.0

1/4 Cor. 00

~~5-2 351°0' 476' -1°0'
 5-3 0°57' 375' -5°09'
 5-4 343°40' 154' -10°40'
 5-5 270°07' 76' -13°44'
 5-6 147°11' 94' -19°42'
 5-7 198°43' 165' -9°13'~~

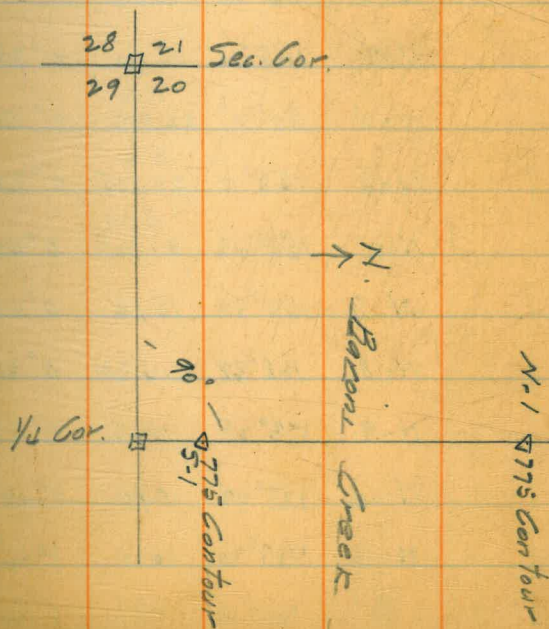
Nov. 7, 1935.
 Converse
 Soper.
 Remmen.

Note - Hor. Angles always read
 to right from back tangent.

"N" points on North side Baroni Creek.

"S" " " South " " "

Back sight on Sec. Cor.



From To Hor. Δ. Stadia Vert. Δ. Hor. Dist.

π 1/4 Cor.

Sec. Cor. 00

VII 89°01' 1570' -5°10' 1557

N-1 90°0' 2x1005 0°50' 2010

π A

1/4 Cor 00

N-1 141°55' 1505 0°39' 1505

N-2 144°20' 1540 0°37' 1540

N-3 148°11' 1610 0°36' 1610

N-4 150°11' ¹⁷⁵⁰ 2x875 0°33' 1750

N-5 153°11' ¹⁶¹⁰ 2x805 0°36' 1610

N-6 158°43' ¹⁵³⁰ 2x765 0°40' 1530

N-7 162°57' 1515 0°40' 1515

N-8 168°37' 1430 0°30' 1430

N-9 173°28' 1745 0°43' 1745

N-10 188°47' 1040 1°07' 1040

N-11 207°30' 1010 1°16' 1010

B 207°08' 987 1°57' 987

Point on Stadia survey of Reservoir

Basis is 1927, by Converse.

Mag. to N-1 = N. 1°30' W. Plate Set for
variation of 14³⁰

From	To	Hor. Δ	Stadia Dist	Vert. Δ	Hor. Dist.
πA					
S-2		351°0'	490	1°0'	490
S-3		358°37'	305	3°21'	304
S-4		338°06'	152	8°02'	149
S-5		69°24'	52	27°22'	41
S-6		135°25'	72	16°38'	66
S-7		206°05'	138	6°0'	136
πB					
A	00		987	2°10'	981
S-8		354°42'	830	1°10'	830
S-9		345°55'	842	1°13'	842
S-10		341°17'	706	1°11'	706
S-11		338°43'	683	1°23'	683
S-12		332°44'	681	1°23'	681
S-13		370°30'	739	1°08'	739
S-14		311°05'	696	1°17'	696

Nov. 8, 1935.
Converse
Toper
Remmen.

From	To	Hor. Δ.	Stadia Dist	Vert. Δ	Hor. Dist.
π B	S-15	302°56'	763	1°12'	763
	S-16	298°07'	833	1°0'	833
	S-17	291°45'	864	1°0'	864
	S-18	286°53'	1032	0°50'	1032
	S-6	291°32'	868	1°18'	
	S-19	282°55'	1130	0°57'	1130
	S-20	278°0'	1196	0°51'	1196
	N-12	240°0'	158	3°52'	157
	N-13	264°03'	339	2°20'	338
	N-14	266°21'	468	1°56'	467
	G.	261°47'	413	6°34'	408

π C

B	00				
N-15	180°14'	233	6°37'	230	
N-16	182°06'	446	3°24'	444	
N-17	175°0'	466	7°0'	465+80 545	

80' Hor. to be added to ±466

From	To	Hor. Δ .	Stadia Dist	Vert. Δ	Hor. Dist.
------	----	-----------------	----------------	----------------	------------

π 6

N-18		175° 0'			605
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Add 60' Hor. to Hor. dist. of N-17.

N-19		178° 46'	738	2° 30'	737
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N-20		180° 15'	835	2° 0'	834
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B.M. #5.

579.73

6.92 586.65

Nov. 9, 1935

Converse

Soper

Remmen

30 + 04.88	B.C.	10.5	576.2
+ 75		8.6	78.1
+ 50		7.2	79.5
+ 59.05	E.C.	6.7	80.0
31 + 00		4.9	81.8
+ 50		5.0	81.7
32 + 00		6.4	80.3
+ 50		7.4	79.3
33 + 00		8.5	78.2
+ 32.81		9.0	77.7
+ 50		9.7	77.0
+ 75		10.8	75.9
34 + 00		11.5	75.2
+ 75		12.6	74.1

B.M.#5

579.73

0.79 580.52

34+50

7.8 572.7

+75

9.5 71.0

+87.34

10.1 70.4

35+00

10.9 69.6

35+30.02 = Equation

13.5 67.0

35+30.18

Revised pipe line alignment east
of City Camp.

35+30.18 B.C. = Equation
25+30.02 B.C.

S. 86° 50' N.

34+87.34 E.C.

$\Delta = 12^\circ 23'$
 $\frac{1}{2}\Delta = 6^\circ 11.5'$

34+87.34 - 6° 11.5'
P.I. 34+75 5° 42'
34+50 4° 42'
34+25 3° 42'
34+00 2° 42'
33+75 1° 41'
33+50 0° 41'

34+10.39 12° 23' L.

R = 715
T = 77.58
L = 154.53
d1' = 2.404
d25' = 1° 00.1

33+32.81 B.C.

N. 80° 47' N

30+59.05 E.C.

$\Delta = 6^\circ 28'$
R = 480'
T = 27.12
L = 54.17
d1' = 3.581
d25' = 1° 29.525

P.I.

30+32.00 L. 6° 28'

30+59 - 3° 14'
30+50 - 2° 41.5'
30+25 - 1° 17'

30+04.88 B.C.

N. 74° 19' N

29+33.62 E.C.

Nov. 9, 1935
Converse
Soper
Remmen.

1085	20944
715	669
5425	21613
1085	715
7595	108065
775775	21613
	151291
	15453295

34+10.39	50
77.58	32.81
33+32.81	17.19
154.53	2.404
34+87.34	6876
	3438
	4132476

41.325
00.404
41.425
00.1
41.5
00.1
41.6
00.1
41.7

05629	30+32.00
480	27.12
451920	30+04.88
22596	54.17
2711520	30+59.05

10472	25	1.188
00814	02.28	1.295
11286	20.42	2.415
480	3.58	2.415
902880	16096	1.12
45144	10060	1.295
	6086	2.415
	738196	
5417280	720296	

CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.18	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.16	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w=16.2$ and $h=5.3$, cu. yds. $=1.48+.028+.039=1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) $=h$, and $\frac{1}{2}$ the roadbed $=w$, add the triangles formed by taking the distance out to each break in turn ($=w'$) by the difference between the cuts (or fills) on each side of it ($=h'$) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9+(20-16) \div 2$ or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.