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EUGENE DIETZGEN CO.

531

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS
Chicago New York San Francisco New Orleans Pittsburg Toronto

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	II
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

This Field Book is manufactured
of a high grade 50% Rag Paper
having a WATER RESISTING surface.

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.

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Grade breaks Sta 260+41.87-268+06.20

B.M. 31

460.90

0.65 461.55

Grade

260+41.8695

11.5802 449.9698 449.9698

264+00.3695

13.050 448.500 448.500

TP.

13.05 448.50

11.69 460.19

268+06.20

12.71 447.48 447.48

TP.

12.71 447.48

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Isbell
Remmen

Aug. 28 1936

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2

Grades in ditch sta 268+25 - 276+43.02

B.M. # 32

457.69

2.33

460.02

Grade

chongrade
268+06.20

12.54 47.48 447.48

268+25

12.59 47.43 47.43

+50

12.65 47.37 47.37

+75

12.71 47.31 47.31

269

12.77 47.25 47.25

+25

12.84 47.19 47.18

+50

12.90 47.12 47.12

+60.16

12.92 47.10 47.10

+75

12.96 47.06 47.06

269+97.4945

13.018 447.002 447.002

TP

11.67 448.35

Contd from page 21

448.35

2.72 451.07

272+06.6195

5.5856 45.4844 445.4844

276+43.0230

6.70 44.37 44.37

TP

6.70 444.37 on grade hub
sta 276+43.02

Grades in ditch sta. 276+50 - 288+21.69

				Grade
B.M. #33			458.00	
	0.58	458.58		
P.			11.52	447.06
	1.16	448.22		
P.			4.08	444.14
	4.67	448.81		
Ch. on grade				
276+43.02			4.44	444.37
276+50			4.46	443.5
+75			4.52	442.9
277+00			4.59	442.2
+25			4.65	441.6
+50			4.72	440.9
+75			4.78	440.3
278			4.84	43.97
+25			4.91	43.90

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1 Sbell
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Cont'd from page 4

448.81

278+50 4.97 43.84 43.84

+62.9765 5.00 43.81 43.81

TP 5.22 443.59

6.99 450.58

281+02.37 Bk 7.3878 443.1922 443.1922

TP 6.87 443.71

1.79 445.70

286+77.87 Bk 4.60 41.10 441.10

288+21.09 B.C. 5.26 40.44 40.44

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Grades in ditch sta 288+50 - 296+29.60

Grade at sta

288+21.09

11.81

452.25

440.44

288+50

11.77

40.28

40.28

175

12.10

40.15

40.15

289+00

12.24

40.01

40.01

108.8070

12.286

439.964

439.964

125

12.35

39.90

39.90

150

12.45

39.80

39.80

175

12.55

39.70

39.70

290+00

12.65

39.60

39.60

125

12.75

39.50

39.50

150

12.85

39.40

39.40

291

13.05

39.20

39.20

Cont'd from page 6

452.25

R

13.05 439.20

11.66 450.86

291.425

11.76 39.10 39.10

+47.307

11.85 39.01 39.01

+75

11.88 38.98 38.98

292

11.90 38.96 38.96

+25

11.92 38.94 38.94

150

11.94 38.92 38.92

+75

11.97 38.89 38.89

293

11.99 38.87 38.87

+25

12.02 38.84 38.84

+55.9945

12.0404 38.8196 438.8196

175

12.11 38.75 38.75

7

Cont'd from page 7

450.86

294 12.20 38.66 38.66

+25 12.29 38.57 38.57

+50 12.37 38.49 38.49

+75 12.46 38.40 38.40

295 12.55 38.31 38.31

TP 12.55 438.31

10.50 448.81

295125 10.59 38.22 38.22

296 10.86 37.95 37.95

+29.10 KC 10.96 37.85 37.85

ck on B.M.
34 5.22 443.59 Rec. elev.
443.61

Grades in ditch sta - 296+29.60 - 309+33.09

Grade sta
296+29.60

437.85

9.76 447.61

300+12.682

11.1225 31.4875 436.4875

T.P.

11.47 436.14

10.04 446.18

304+90.682

11.3331 34.8469 434.8469

T.P.

12.76 433.42

10.15 443.57

306+99.807

10.57 33.00 433.00

309+33.09

11.03 32.54 432.54

T.P.

11.03 432.54

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Grades "raked in" sta 296+29.60 - 300+12.682

" " 300+12.682 - 304+90.682

" " 304+90.682 - 306+99.807

" " 306+99.807 - 309+33.09

Grades in ditch sta 313+01.26 - 317+25

B M³⁵

438.93

2.43 441.36

313+01.26

8.84 32.52 432.52

313+20.76

8.84 32.52 432.52

313+25.76

9.18 32.18 432.18

313+55.76

9.34 32.02 432.02

313+70.26

9.36 32.00 432.00

+87.80

9.56 31.80 431.80

314+05.34

9.77 31.59 431.59

314+16.23

9.79 31.57 431.57

+25

9.81 31.55 31.55

+50

9.86 31.50 31.50

+75

9.91 31.45 31.45

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11

441.36

315+05.79 9.98 31.38 431.38

IP. 9.98 431.38

10.62 442.00

315+25 10.66 31.34 31.34

+50 10.71 31.29 31.29

+75 10.76 31.24 31.24

316+00 10.81 31.19 31.19

+11.775 10.83 31.17 31.17

+06.41

316+25 10.87 31.13 31.13

+50 10.91 31.09 31.09

+75 10.96 31.04 31.04

317+00 11.01 30.99 30.99

+25 11.06 30.94 30.94

Not Original x-section

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12

Cuts on offsets - Valve Chamber 312+21

BM# 35			438.93	
3.83	442.76			
				Sub-grade
312+17.32 (9.08RT) 2' offset	4.73	38.03	430.35	
312+17.32 (2.58LT) 2' offset	4.06	38.70	30.55	
312+25.48 (9.08RT) 2' offset	4.89	37.87	30.45	
312+25.48 (2.58LT) 2' offset	4.11	38.65	30.65	

Cut on 3' offset

7.68

8.15

7.42

8.00

Cuts on offsets - Pressure Reg. Chamber 313+63.

313+58.18 (3.83RT) 2' offset	10.14	32.62	30.35	
313+58.18 (3.83LT) 2' offset	8.96	33.80	30.35	
313+67.84 (3.83RT) 2' offset	8.57	34.19	30.25	
313+67.84 (3.83LT) 2' offset	7.90	34.86	30.25	

Cut on 2' offset

2.27

3.45

3.94

4.61

Grades in ditch sta 309+50 - 311+98.43

B.M. 35			432.93
	3.89	442.82	
ck on			
309+33.09	10.28	32.54	432.54
309+50	10.32	32.50	32.50
+75	10.36	32.46	32.46
+98.057	10.4122	32.4078	432.4078
310+25	10.47	32.35	32.35
+50	10.52	32.30	32.30
+75	10.57	32.25	32.25
311	10.62	32.20	32.20
+25	10.67	32.15	32.15
+50	10.72	32.10	32.10

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Contd from page 13

442.82

311+75.807

10.772

432.048

177.96 EC

10.79

32.04

311+98.43

10.82

432.00

Offset stakes for V. Chamber - 312+21

B.M. 35

438.93

4.35 443.28

Subgrade

312+25.48 (9.08 RT) 2' offset

6.20

37.08

430.45

at 6.63

312+17.32 (9.08 RT) 2' offset

7.17

36.11

430.35

at 5.76

ck on

312+17.32 (12.58 RT) 2' offset

4.52

39.70

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15

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16

Grades in ditch sta 319+50 - 329+54.33

B.M. 36

441.06

Grade

4.31 445.37

329+54.33

11.30 434.07 434.07

TP

12.24 433.13

8.86 441.99

325+45.927

11.6947 30.2953 430.2953

321+87.427

11.964 30.026 430.026

TP

11.96 430.03

11.31 441.34

319+50

10.85 30.49 430.49

ck on grade

317+25

10.40 30.94

Grades in ditch - sta. 329+93.907 - 335+01.03

B.M. 36

441.06

5.32 446.38

ck on grade

329+94.33

12.31

434.07

329+75

12.17

34.26

34.26

329+93.907

11.9374

34.4426

434.4426

330

11.92

34.46

34.46

125

11.85

34.53

34.53

150

11.98

34.60

34.60

175

11.71

34.67

34.67

331

9.64

36.74

34.74

135

11.57

34.81

34.81

150

10.50

35.88

34.88

175

34.95

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Cut 2.00 (2.88 out)

Cut 1.00 (2.63 out)

446.38

332+00 11.36 35.02 35.02

+25 11.29 35.09 35.09

TR 11.29 435.07 00

12.35 447.44

+50 12.28 35.16 35.16

+62.22 12.25 35.19 435.19

+75 11.75 35.69 35.69

333 10.77 36.67 36.67

+25 9.77 37.65 37.65

+45.65 EC 8.98 38.46 38.46

335+01.03 2.88 44.56 444.56

TR on grid sheet 2.88 444.56

Final x-section of ^{Ext. for} Valve chamber - 312+21

B.M. 35 438.93

2.98 441.91

312+17.32 (9.08RT) 11.6 430.3

312+17.32 (12.58H) 11.4 430.5

312+25.48 (9.08RT) 11.5 430.4

312+25.48 (12.58H) 11.3 430.6

Final x-section of
Pressure Reg. Chamber. Sta 313+63

313+58.18 (3.83RT) 11.6 430.3

313+58.18 (3.83H) 11.6 430.3

313+67.84 (3.83RT) 11.7 430.2

313+67.84 (3.83H) 11.7 430.2

Sept 16 1936

Super

Label

above

(Copied from scribble pad.)

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Grades in ditch sta 317+50 - 319+00

Grade at
317+00

430.99

10.57 441.56

ck on grade
317+25

10.62 30.94 30.94

317+50

10.67 30.89 30.89

+75

10.72 30.84 30.84

318+01

10.78 30.78 30.78

+25

10.82 30.74 30.74

+50

10.87 30.69 30.69

+75

10.92 30.64 30.64

319

10.97 30.59

Sept 18 1936

So per

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Moore

20

Grades in drain ditch for Valve chamber sta 13+00

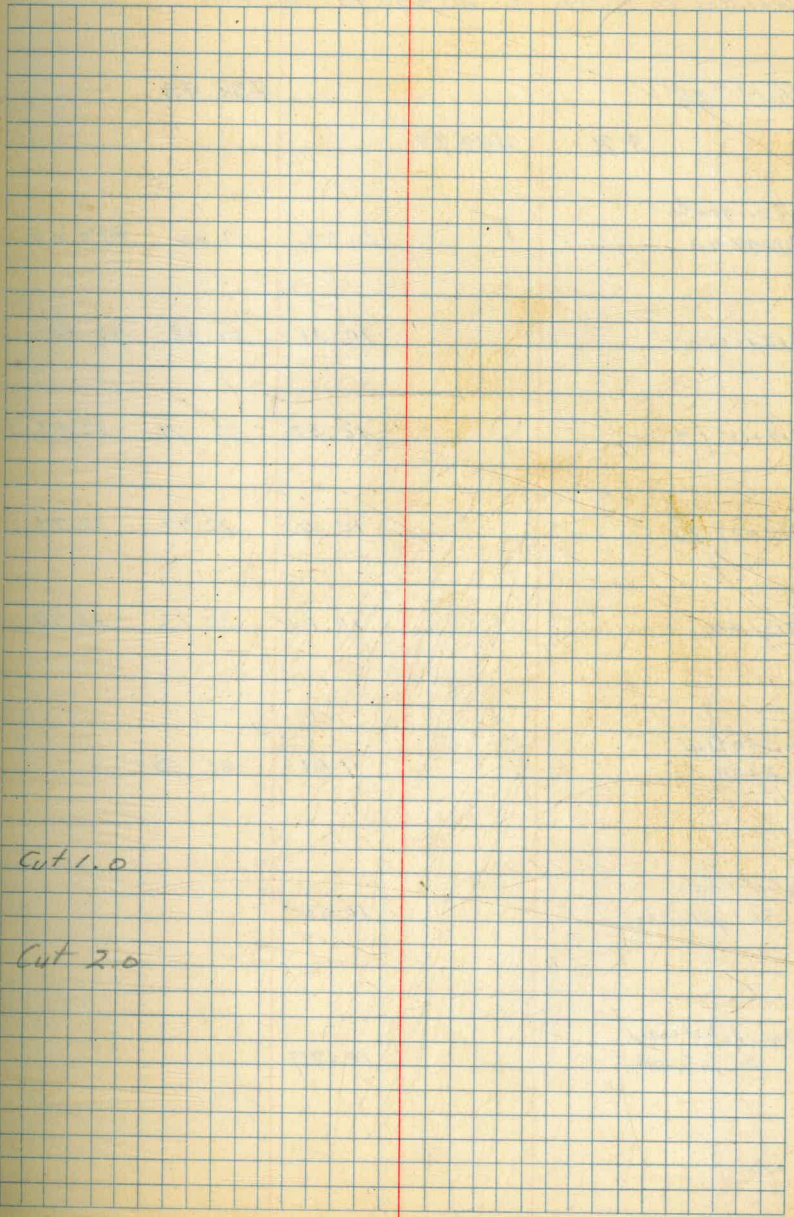
0+00 = outside of concrete chamber. Grade = -1.00% (except under boulder)

B.M.			570.22	
	2.38	572.60		
IP.			10.10	562.50
	8.51	571.01		

Bottom of drain tile at V. Chamber. Grade for bottom of Pipe.

0+15			10.55	560.46	60.46
IP.			11.82	559.19	
	7.26	566.45			
+23.6			9.28	57.17	57.17
+35.6			9.40	57.05	57.05
+49.6			8.54	57.91	56.91
+78.6			7.83	58.62	56.62

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Cut 1.0
Cut 2.0

Grades in ditch sta 311+98.43 - 312+40

B.M. # 35			438.93	
	3.86	442.79		
ck on grade				
311+98.43		10.79	32.00	432.00
312+10.02		10.31	32.48	32.48
312+15.03		10.32	32.47	32.47
312+27.76		10.02	32.77	32.77
312+40		10.66	32.73	32.73
Nail in floor				
312+24		11.61	31.18	
top of steel under				
30" gate valve		10.55		
top of steel under				
20" gate valve		10.27		

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Grades in ditches sta 333+45.65 - 341+87.425

TP on grade
333+45.65

444.56

12.66 457.22

TP

0.94 456.28

12.82 469.10

338+88.80

7.3052 61.7748 461.7748

TP on grade

13.84 465.26

12.52 477.78

340+67.94

7.7696 68.0104 468.0104

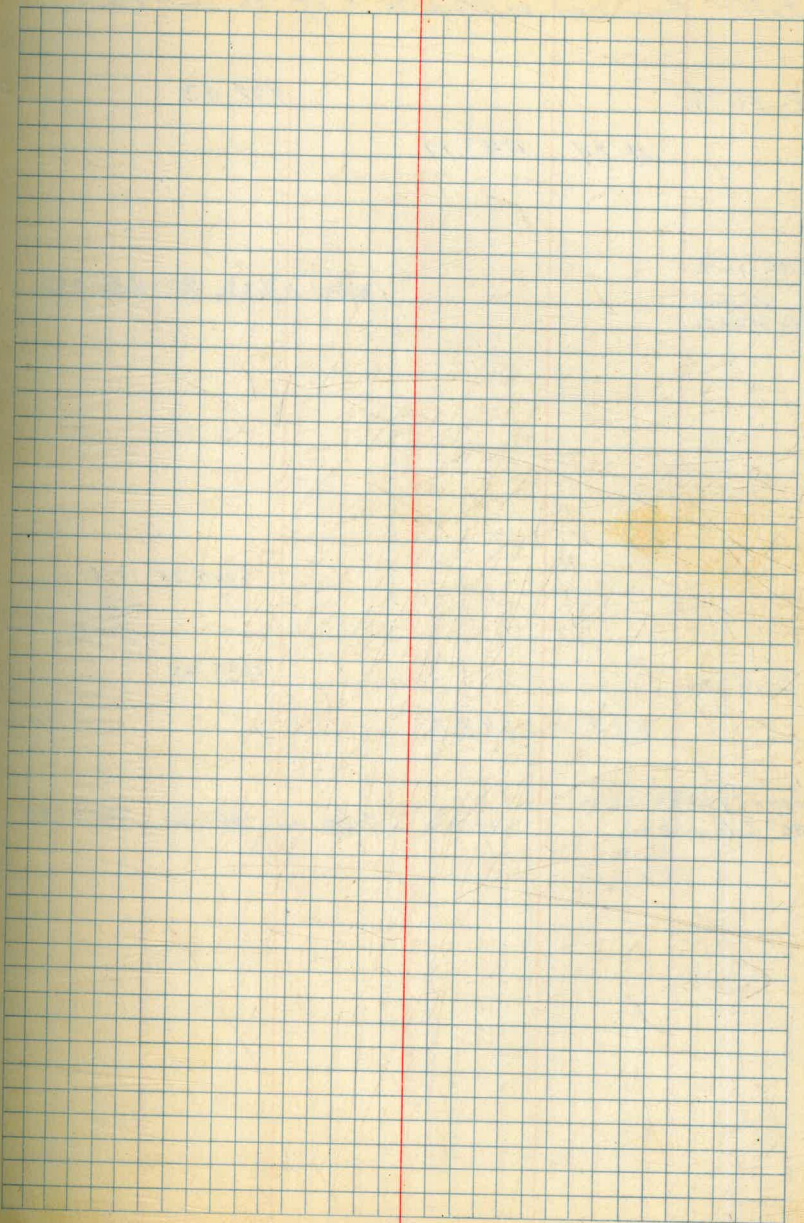
341+87.425

8.82 68.96 468.96

TP on grade
341+87.425

9.82 468.96

Grades "raked in" between grade breaks



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Fill - from nail in floor to E of 30" Gate Valve

B.M. 35 438.93

4.24 443.17

Elev. of E
of 30" G.V.
Sta 312+21

12.20 430.77 433.98

Fill 3.01 to E of 30" G.V.

Sept 28 1936

Super
Isbell
Moore

B.M. 35 438.93

4.28 443.21

top of flange -
30" Gate valve

7.60 35.61 435.59

435.39 = Grate for top of flange

433.98
1.25
0.36
435.07

Final x-section of drain ditch sta 13+00

0+00 = outside of valve chamber.

B.M. 570.22

0.79 571.01

0+00 10.8 560.2

0+15 11.1 599

0+18.5 4.2 648

0+25.5 4.0 670

T.P. 11.82 559.19

7.26 566.45

0+26 9.7 55.7

0+46 9.9 56.5

0+46 9.5 56.9

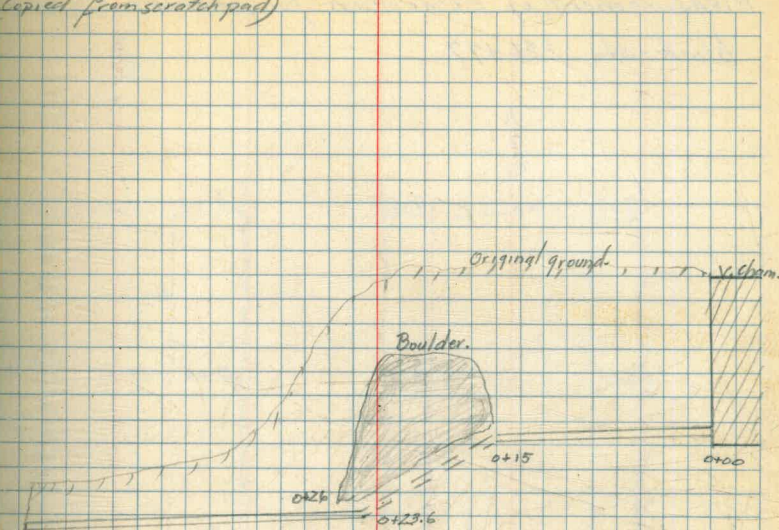
0+82 9.8 56.6

Note: 0+00-0+46 was excavated 0.50 below pipe grade and filled with concrete.

Sept 18 1936

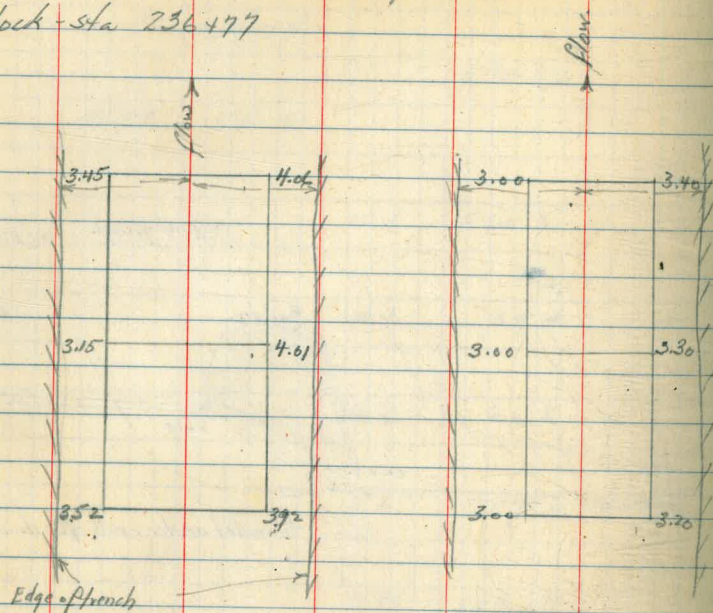
Soper
Isbell
Moore
(Copied from scratch pad)

25



Note: tunneled under rock for drain ditch.

Measurement of excavation for anchor
block - sta 236477



1.0 above pipe

1.0 below pipe

Cal. $\frac{524}{56}$

Sept 18 1936

Super

12 bell

Moore

(Copied from scratch, post)

26

Grades in ditch sta 341+87.425-356+19.53

TP
Grade 341+87.425

468.96

11.15 48 0.11

Ken B.N. 38

3.79 476.32 Recd. 476.32

Grade

343+225

11.71 468.40 468.40

343+36.795

12.01 469.10 468.10

343+66.87

12.34 467.77 467.77

TP

11.18 469.73

1.37 470.30

346+135.41

10.49 59.97 459.87

346+160

10.75 59.55 59.55

+90

10.12 60.18 59.18

348+00

12.52 57.78 57.78

TP

12.52 457.78

Sept 22 1986

Soper
Isbell
Moore

27

Cut 1.00 (2.47 cut)

Cont'd from page 27

29

457.78

6.45 464.23

Grade

351173.12

11.20 53.03 453.03

P

16.13 454.10

11.65 465.75

356119.5376-

19.79 55.96 455.96

Grades raked in between grade breaks.

Sept 23 1936

29

Soper
Shell
Moore

Final x-section - blowoff ditch and box, 134+50

0+00 - 2.8 from top of pipe.

Top of pipe (Sta 134+50)

502.5

5.3

507.8

0+00

9.8

498.0

0+10.2

9.9

97.9

Bottom of
blowoff box
excavation.

12.3

95.5

used final sec

508
55
60

M

Sept 25 1936

Soper
Isbell
Moore

30

Grades in ditch sta 346+35.41 - 347+35

Grade-sta
348+00

Grade

457.78

11.40 469.18

347+35

9.58 59.60 58.60

Cut 1.0

347+10

9.26 59.92 58.92

Cut 1.0

346+60

9.63 59.55 59.55

346+35.41

9.31 59.87 59.87

Original x-section for anchor block 423+19.78

ground elev.
423+19.78

409.6

5.3 414.9 ✓

"A" 5.4 409.5 ✓

"B" 5.1 09.8 ✓

"C" 5.3 09.6 ✓

"D" 5.0 09.9 ✓

Final x-section for anchor block

Oct. 14 1936
Soper
Isbell
Nore

Grade-sta
423+12.28

400.83

4.05 404.88

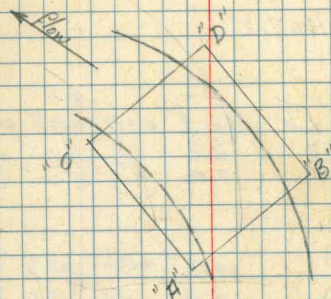
"E" 5.2 399.7

Hand for Cal
526
57 m

Sept 25 1936

Soper
Isbell
Nore

31



Bottom of anchor excavation

Yatre Chamber

Original x-section for blowoff box - 426+38.67

2 Elev. Sta
426+38.67

401.9

5.3 407.2

	LT	X		RT	
	403.0	401.9	401.7	402.5	402.3
	5.2	5.3	5.5	4.7	4.9
426+34.6	5.3	0.0	3.0	5.0	9.1

	401.9	401.8	401.6	402.5	402.3
	5.3	5.4	5.6	4.7	4.9
426+42.8	5.3	0.0	3.0	5.0	9.1

Copy of
chart 5/28/58
M

Yatre Chamber

Final x-section for blowoff box - 426+38.67

od 7193
Soper
Isbell
Moore

County B.M.

400.22

5.27 405.49

426+34.59 (5.33 LT)

12.6 392.9

426+34.59 (9.08 RT)

12.7 92.8

426+42.75 (5.33 LT)

12.5 93.0

426+42.75 (9.08 RT)

12.6 92.9

Copy of
chart 5/28/58
M

Sept 25 1936

Soper
Isbell
Moore

Grades in ditch - 356+19.53 - 360+06.89

Grade - sta
356+19.53

455.96

11.39

467.35

Grade

356+21.83

11.38 55.97 55.97

+37.50

11.59 55.76 55.76

+50

11.76 55.59 55.59

+62.50

11.92 55.43 55.43

+75

12.08 55.27 55.27

+87.50

12.25 55.10 55.10

357+00

12.41 54.94 54.94

+12.5

12.57 54.78 54.78

+25

12.74 53.61 54.61

+37.5

12.90 54.45 54.45

TP

12.90 54.45

Sept 26 1936

Soper

Isbell

Moore

33

Cont'd from page 33

		454.45	
9.23	463.68		
357.40		9.39	54.29 54.29
+63.5		9.56	54.12 54.12
+75		9.72	53.96 53.96
+87.5		9.88	53.80 53.80
358+01.96.65		10.07	53.61 53.61
360+06.89		12.75	450.93 450.93

39

17

86

34

Re-set grades in ditch 340+67.745 - 343+66.67

Grade - sta
343+25

468.40

11.17 479.57

340+67.745

11.5596

468.0104

343+36.775

11.47

468.10

343+66.67

11.80

467.77

Sept 28 1936

Super

15 Bell

Moore

35

Final x-section for blowoff trench and box 154475

Top of pipe
154475

498.8

5.3

504.1

0+00

9.7

94.4

0+10.2

9.8

94.3

Bottom of
blowoff box
excavation

11.6

492.5

OK
not sub
5' to

Sep 28 1936

Soper
Isbell
Moore

36

Sept 29 1936

Soper
H. B. N.
Moore

37

Original x-section blowoff trench and box - 258400

0+00 = 28 from end of pipe
top of pipe
Sta 258400 450.1 ✓

5.3 455.4 ✓

0+00 4.3 51.1 ✓

0+10.2 4.3 51.1 ✓

0+17 4.3 51.1 ✓

Final x-section blowoff trench and box 258400

top of pipe
258400 450.1 ✓

5.3 455.4 ✓

0+00 10.2 45.2 ✓

0+10.2 10.2 45.2 ✓

Bottom of
box excavation 12.1 43.3 ✓

used in the data - Cal

528
56.60
27.74

Original x-section for blow off trench 227+20

0+00 = 2.8 from E of pipe

top of pipe
227+00 5.3 479.8 ✓ 474.5

0+00 3.3 76.5 ✓

0+19 3.2 76.6 ✓

0+25.2 10.3 69.5 ✓

Final x-section for blow off trench 227+20

top of pipe
227+00 5.3 479.8 ✓ 474.5

0+00 10.2 69.6 ✓

0+25.2 10.3 69.5 ✓

Class. Sec

Rel

528
60
X 227

Sept 29 1936

Soper
Isbell
Moore

39

Grades in ditch - 360+06.89 - 377+38.4318

grade - sta
360+06.89

450.93

5.86 456.79

ck. on B.M. #40

3.75 453.04

TP

12.61 444.18

2.32 446.50

Grade

367+98.35

3.50 443.00 443.00

369+91.96

10.22 436.28

TP

12.65 433.85

2.47 436.32

373+20.50

7.72 428.60 428.60

ck. on B.M. #41

5.09

TP

12.93 423.39

0.50 423.89

376+19.0218

6.8171 417.0729

377+38.4318

11.4278 412.4622

Sept 29 1936

Soyer
Isbell
Moore

39

Rec. elev. 453.02

Rec. elev. 431.23

Grades in ditch - 377+32.4318 - 400+08.213

B.M. 42

404.45

6.28 410.73

Grade

383+00

5.49 405.24 405.24

388+13.8468

11.0894 398.6406 398.6406

Cut - 1.00

387+33.1268

9.204 401.526

B.M. 42

404.45

12.61 417.06

390+82.311

8.3558 408.7042 408.7042

371+42.022

5.947 411.113 411.113

392+31.589

2.7215 414.3385 414.3385

T.P.

2.73 414.33

12.50 426.83

395+60.103

3.9284 427.9016

Cont'd from page 40

426.83

397+39343

2.1368 424.6932 424.6932

TR

2.14 424.69

5.10 429.79

400+08.213

4.1463

425.6437

Grades in ditch 400+08.213 - 409+34.14

Grade - sta
400+08.213

425.6437

1.24 426.8837

402+47.17

5.8290 421.0547 421.0547

TP

11.5337 415.35

0.25 415.60

405+75.14

4.545 411.055 411.055

409+34.14

4.97 410.63 410.63

TP

5.84 409.76

9.23 418.99

den BM #44

1.95 417.04

Oct 1, 1936

Soper
16bell
Moore

42

Recorder 417.06

Grade break - sta 360+06.89 - Reset.

358+07.86

453.61

8.54 462.15

360+06.89

11.22

450.93

Oct 1 1936

Saper

156011

Moore

43

Elevation of top of existing 36" line.

County B.M.

400.72

6.24 406.46

8.30 399.16

423+19.78
385.55
427+05.33 = end of pipe
 .25 cut .25 off existing pipe
427+05.58 for bulkhead removal.

Sta of end of trench excavation = 427+07.0

Oct 3 1936

Super
Isbell
Moore

44

top of existing Lakeside - San Diego 36" line.

thickness = $\frac{19}{64}$ "

Oct 5 1936
Soper
Isbell
Moore

45

Grades in ditch - 423+12.28 - 424+71.733

County B.M.

400.22

6.40 406.62

IP

9.35 397.27

9.92 407.19

424+71.733

10.846

396.344

IP

7.33 399.86

8.97 408.83

424+22.301

8.887

399.943

423+62.551

8.05

400.78

Grade - sta 4 -

423+62.551

400.78

12.34 413.12

423+50

12.33

400.79

423+25.15

423+27.28

12.30

400.82

423+12.28

12.29

400.83

Oct 6 1932

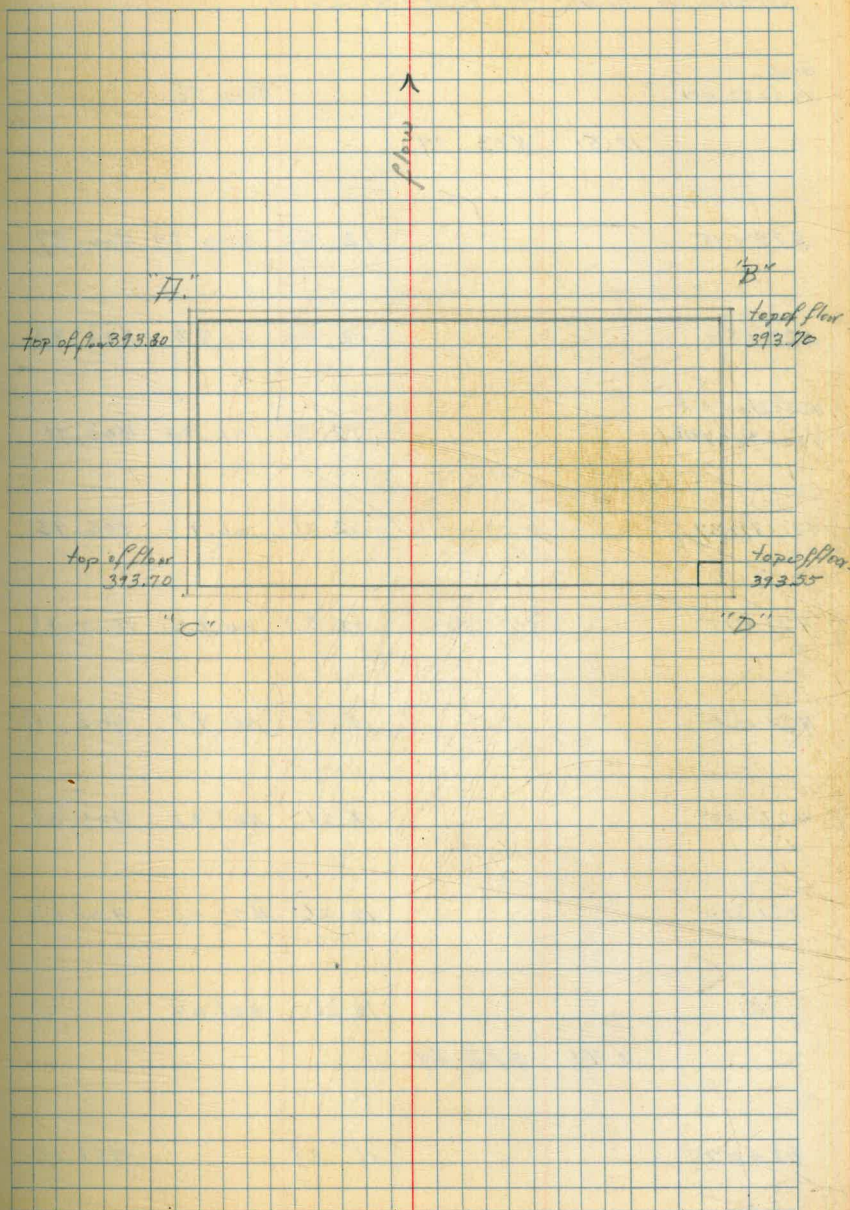
Soper
Isbell
Moore

Offsets for Valve chamber - 426+38.67

County B.M.		400.22	
	4.89	405.11	
TP		3.10	402.01
	4.84	406.85	
			<u>Subgrade</u>
"A" (2' offset)	4.56	402.29	393.05 (cut - 7.24)
"B" (2' offset)	5.65	401.20	392.95 (cut - 8.25)
"C" (2' offset)	4.42	402.43	392.95 (cut - 9.48)
"D" (2' offset)	7.80	399.05	392.80 (cut - 6.25)

426+25 11.19 95.64 95.66

426+50 11.40 95.45 95.45



Grades in ditch - 412+50 - 422+75

Grade - Sta
423+62.551

400.78

12.51 413.29

422+75

12.42 400.97 400.87

422+60

12.41 00.88 400.88

423+21.02 Bk
422+76.68 Hk

12.38 00.91 400.91

421+99.37

12.36 00.93 400.93

421+75

12.33 00.96 400.96

421+50

12.31 20.98 400.98

421+25

12.28 401.01 401.01

421+00

12.26 401.03 401.03

77

12.26 401.03

11.41 412.44

420+75

11.38 401.06

Oct C 1936
Super
Isbell
Moore

47

Contd from page 47

48

412.114

420+48.9386

11.35 401.09 401.09

420+35

11.33 01.11 01.11

420+00

11.30 01.14 01.14

419+75

11.28 01.16 01.16

419+66.7786

11.27 01.17 01.17

419+50

11.25 01.19 01.19

419+25

11.23 01.21 01.21

419+10.4486

11.21 01.23

TP.

11.61 400.83

11.61 412.44

417+55.01

11.05 401.39

412+50

9.04 403.40

Original x-section for blow off trench & box 312+12

0+00 = 2.3 from top of 36" pipe

B.M. # 35 438.93

1.87 440.80

0+00 3.5 37.3

0+03 3.7 37.3

Blow-off box 3.7 37.1

Cal class 3

Cal class 4

528
57

548
60

Final x-section for blow off trench and box 312+12

0+00 9.1 31.7

0+03 9.1 31.7

Blow off box 11.5 429.3

Oct 2 1936

Soper

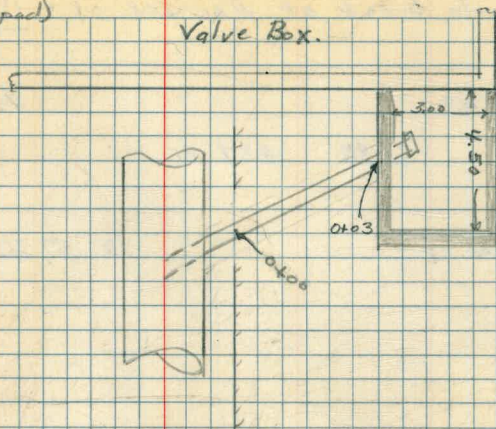
1st bill

Moore

(Copied from pad)

49

Valve Box.



Note: This blow off box enlarged
by Bob Watson to enable
valve to be taken off.
3.00 x 4.50 inside.

Grade break at 400 + 08.21 - Reset.

B.M. 43

435.33

1.88

437.21

400 + 08.21

12.57 424.64 425.64

Oct 7 1936

Soper
Isbell
Moore

50

Fill - 100

Grades in ditch 409+34.14 - 412+43.19

Grade - sta
409+34.14

410.63

3.92 414.55

409+50

3.94 10.61 410.61

+75

3.97 10.58 10.58

410+80

4.00 10.55 10.55

410+23.77

4.03 10.52 410.52

410+53.64

4.15 410.40 410.40

410+75

4.94 09.61 409.61

11 P.

4.81 409.74

5.42 415.16

411+73.35

9.17 05.99 405.99

411+80.67

411+81.05

9.44 05.72 05.72

change grade

412+50

11.76 03.40 403.40

412+43.19

11.733 03.427 403.427

Oct 7, 1936

Super
Isbell
Moore

51

Original x-section of blowoff trench and box - 322+01

0+00 = 2.3 from E of 36" pipe

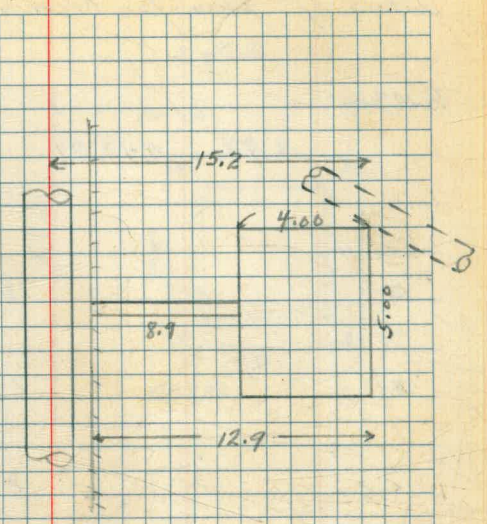
Top of pipe 322+00.			433.0
	5.3	438.3	
0+00		2.5	435.8 ✓
		2.6	435.7 ✓
Blowoff box		2.6	435.7 ✓

Final x-section B.O. trench & box 322+01

Top of pipe 322+00			433.0	Clear 3x4 5x8 59x61 Oct. 15, 1936 Super Isbell Moore
	5.3	438.3		
0+00		9.3	429.0 ✓	
0+02.9		9.4	428.9 ✓	
Blowoff box		11.1	427.2 ✓	

Oct 7 1936

52



Note: Box moved in to clear County Culvert

Oct 7 1936

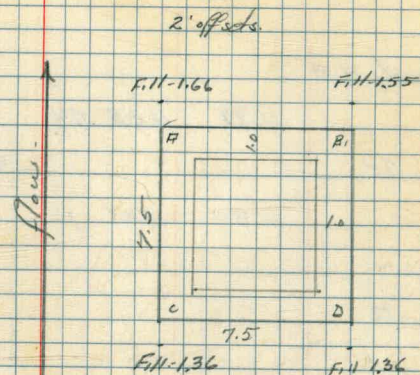
53

Elevs of floor for Recording sta 313+00

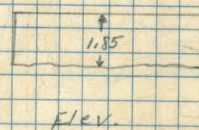
B.M. #35			438.93
	3.94	442.87	
			Floor elevation
"A"	6.53	36.34	438.00 F.II-1.66
"B"	6.42	36.45	438.00 F.II-1.55
"C"	6.23	36.64	438.00 F.II-1.36
"D"	6.23	36.64	438.00 F.II-1.36
Average ground elev.	6.40	436.47	

Calc.

$\frac{528}{65}$



Measurement of
foundation thickness
after pouring.



Oct 7 1936

54

Soper
Isbell
Moore

Grades in valve chamber -426+38.67

County B.M.		✓		400.22
	4.82		405.04	
TP		✓	3.23	401.81
	4.35		406.16	<u>floor grade</u>
M		✓	12.36	393.80 393.80
B		✓	12.46	93.70 393.70
C		✓	12.46	93.70 393.70
D		✓	12.41	93.55 393.55

Original x-section for blowoff trench 388+27

0+00 = 2.3 from top of 36" pipe

top of pipe
388+25

401.9

9.5 411.4

0+00

0+00 8.2 403.2

0+16 8.4 403.0

0+20 10.7 400.7

0+30 10.7 400.7

Final x-section blowoff trench 388+27

calculation

top of pipe
388+25

401.9

5.3 407.2

0+00 9.5 397.7

0+24.4 10.2 97.0

0+24.4 10.7 96.5

0+27.9 10.7 96.5

Oct 8 1936

Super
labell
Moore

55

Oct 16 1936

Super
labell
Moore

Oct. 29 1936

Super
labell
Moore

528
61

528
61

Original x-section for blowoff trench 351175

0+00 = 2.3 from k of 36" Pipe

Top of pipe
351175

456.0

8.9 464.9 ✓

0+00

8.4 456.5 ✓

0+12

10.3 454.6 ✓

0+25

10.5 454.4 ✓

Final x-section for blowoff trench 351175

Top of pipe
351175

456.0

5.3 461.3 ✓

0+00

9.6 451.7 ✓

0+10.7

9.9 451.4 ✓

0+10.7

11.2 450.1 ✓

0+14

11.2 450.1 ✓

Cre

Need $\frac{5.75}{61}$ ✓

Oct 8 1936

Soper
Isbell
Moore

56

Original x-section for blow off trench and box
Sta 426 + 14.3 0+00 = 2.3 from 2 36" pipe

Grade at 426+25 12.2 407.9 395.7

0+00 5.3 402.6

0+11 5.9 402.0

Box 5.9 402.0

Final x-section for blow off trench and box 426+14

Grade at Top Pipe at 426+25 5.3 404.1 401.0 398.8 395.7

0+00 9.1 395.0 391.9

0+11 9.1 395.0 391.9

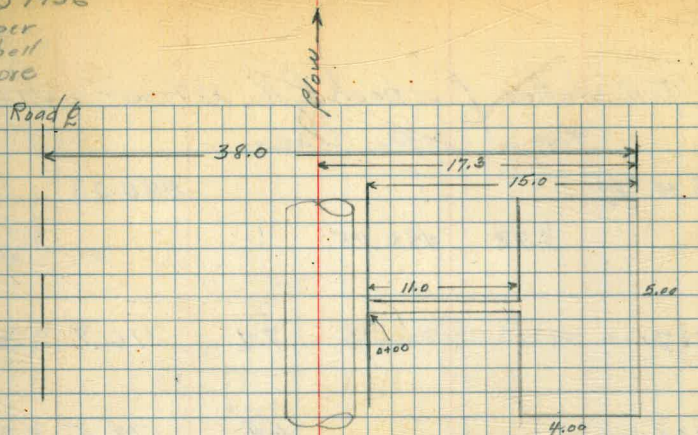
Box 11.2 392.9 389.8

(Lowest Grade 395.87)

Oct. 13 1936

Soper
Isbell
Moore

57



Note: 4" boiler flange on pipe moved back 12.0 to sta
426+14.3 on account of tree & blow off
changed accordingly.

Fill stakes for back fill. 227100 - 229174.24
For Insp. Use.

B.M. #27		480.23
	3.72	483.95
227100	7.1	476.8
228100	4.4	79.5
229100	4.3	79.6
229150	2.3	81.6
229174.24	+0.3	84.2

Oct 13 1931

Soper
15 bell
Mare.

top of pipe

74.7	2.1	Above top of pipe
75.9	3.1	"
78.4	1.2	"
79.9	1.7	"
80.6	3.6	"

Fill stakes in Value Chamber - 126 + 38

County B. 19

400.22

6.29 406.51

Invert grade

12.83 393.68 395.80

12.78 393.73 395.80

Oct. 14 1936

Soper
Isbell
Moore

59

Fill 2.12

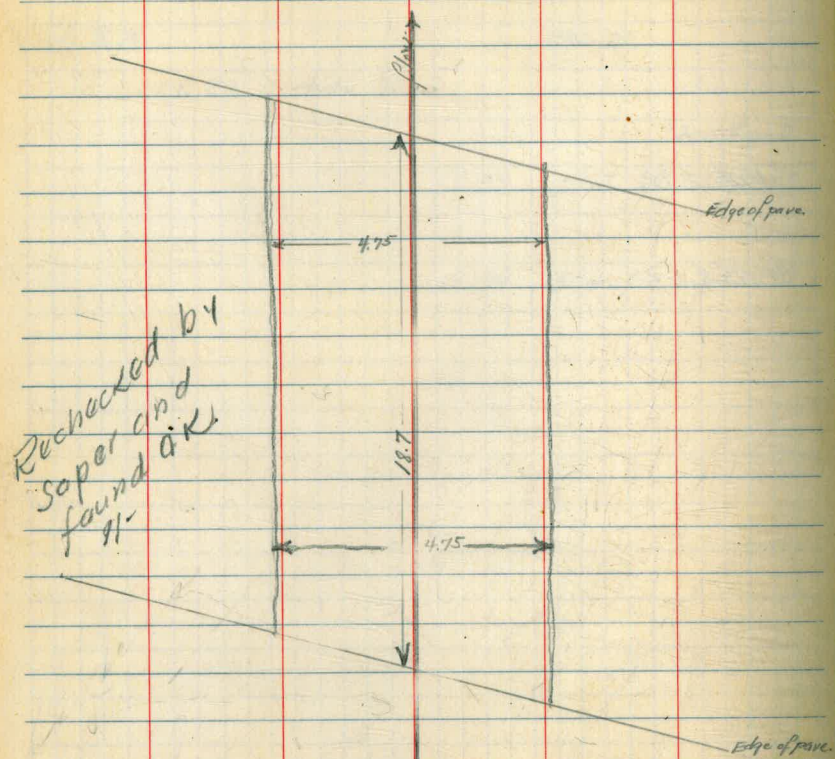
Fill 2.07

Oct 14 1936

Soper
Isbell
Moore

60

Concrete excavation - State Highway crossing 423+00



Pavement - $18.7 \times 4.75 \times 0.50$

Pipe

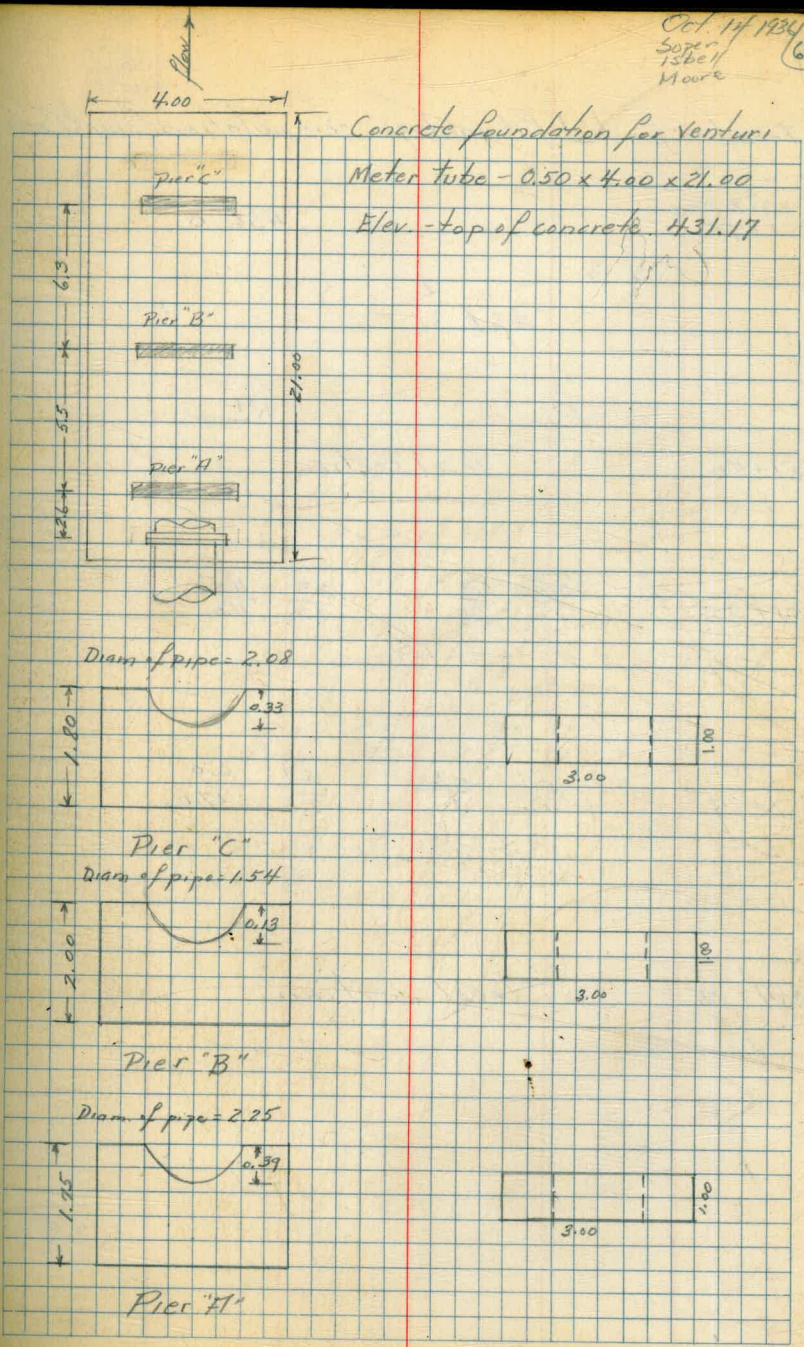
Elev. of concrete under Venturi Meter

3.11.35		438.93
4.14	#114	443.07
11.90		431.17
11.90		431.17

528
57

used in cal

Oct. 14 1934
Soper
1. Steel
Moore
(61)



X-section for back fill yardage computation Oval Creek.

top of pipe
351+75

456.0

5.3

✓
461.3

LT

RT

351+50

level section

351+55

$\frac{5.2}{10.0}$

$\frac{5.4}{3.0}$

$\frac{3.3}{3.0}$

$\frac{4.5}{11.0}$

351+69

$\frac{5.6}{10.0}$

$\frac{5.6}{3.0}$

$\frac{5.7}{3.0}$

$\frac{6.0}{17.0}$

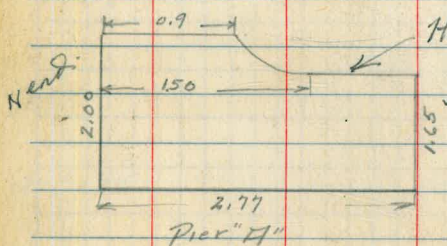
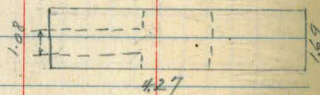
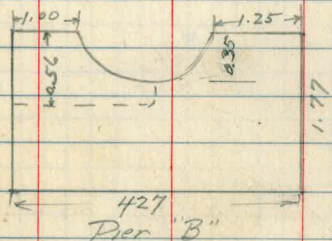
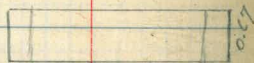
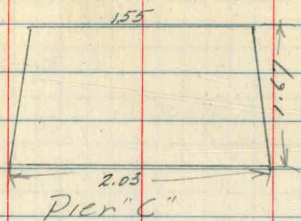
351+85

level section

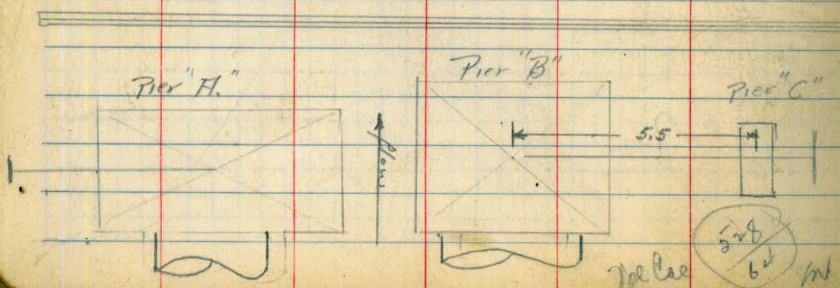
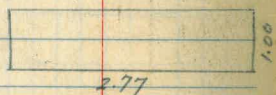
Oct 14 1936
Soper
Isbell
Moore

62

Piers in Valve Chamber - 3/24/21



Housing of the gate rests on this



Oct 14 1936

Soper
Isbell
Moore

63

± 30" Gate Valve to Outside Bi. Pass = 3.2
 ± 20" " " " " " " = 2.2
 7" Clearance between Bi. Pass on
 20" + 30" Valve

Original x-section anchor block 411+77.21

B.M.# 417.06

1.07 418.13

"A" 6.9 411.2

"B" 6.8 11.3

"C" 7.1 11.0

"D" 7.3 10.8

Final x-section anchor block 411.77.21

Oct. 23 1936
Soper
13 Bell
Moore

B.M.#44 1.08 418.14 417.06

"A" 13.44 404.70

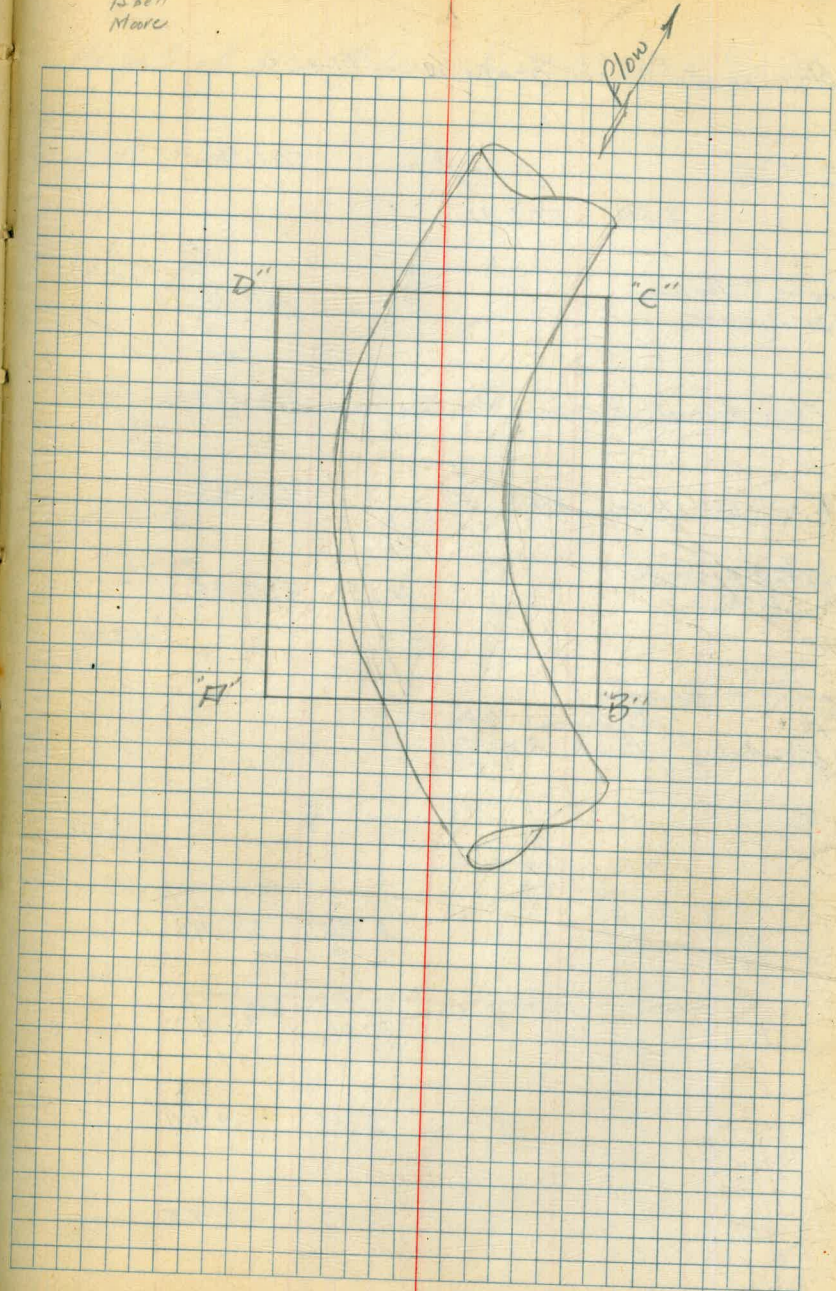
"B" 13.44 404.7

"C" 13.64 404.5

"D" 13.64 404.5

Oct. 19 1936
Soper
13 Bell
Moore

64



Elev. top of Valve Chamber - 160+00

B.M. 21 501.12
8.80 509.92

top of V. Chamber
Sta 160+00 3.72 506.70

Elev. top of Pressure Reg. Chamber 313+63

B.M. 35 3.60 442.53 438.93

top of conc. pressure
Regulator chamber 4.68 437.85

(Elev. top of V. Chamber 312+21)

"H" 3.55 38.98

B. 3.61 38.92

"C" 3.46 39.07

"D" 3.58 38.95

Oct. 21 1936

Super
Shell
Mare

65

Height of blow off boxes - top of floor to top of box

134+50 8.4

154+75 9.0

258+00 8.25

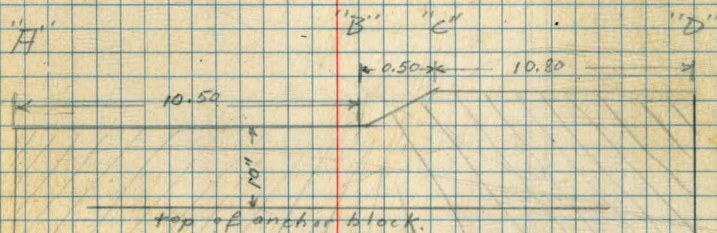
312+18 5.65

322+01 8.35

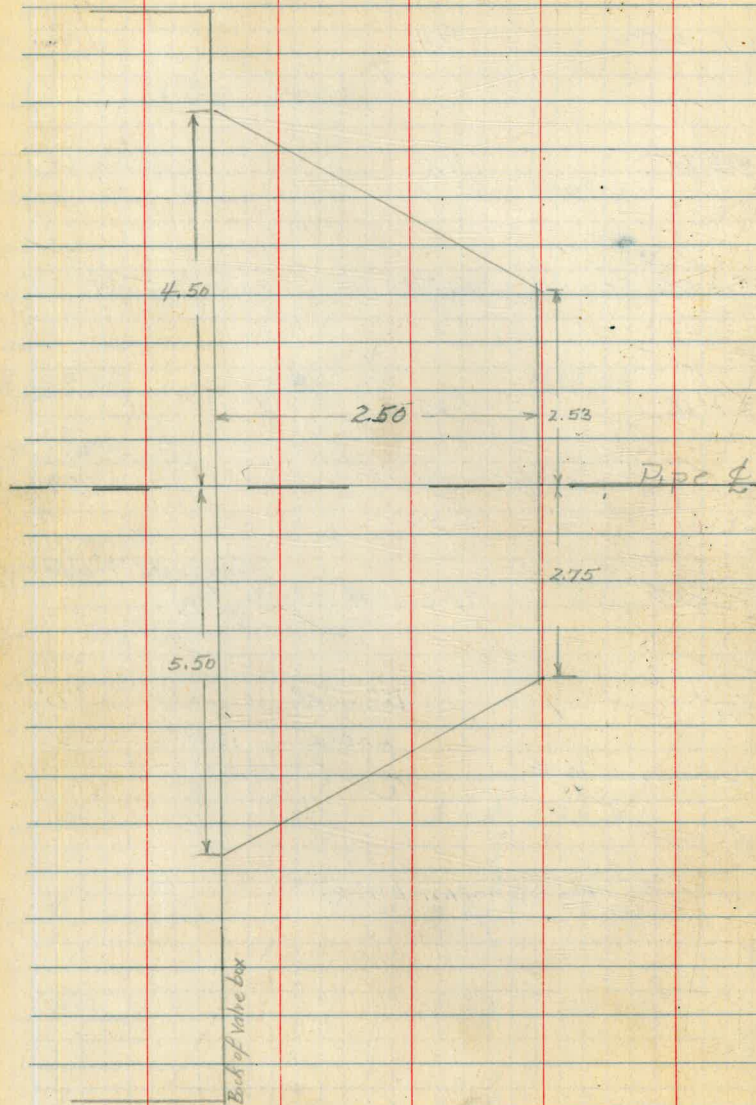
426+14 7.62 (Add 0.50 for top)

5.28
6.3 etc
m

Concrete Top (Remor-
-able)



Flange block on Valve Chamber 476 + 38



Oct 22 1936
Super
15611
Moore

66

Check on floor of Valve Chamber 426438.67

(Requested by Inspector Shreiber.)

County B.M.

400.22

4.90 405.12 ✓

TR

3.29 401.83 ✓

4.75 406.58 ✓

"A"

12.77 93.81 393.80 ✓

"B"

12.88 93.70 393.70 ✓

"C"

12.89 93.69 393.70 ✓

"D"

12.97 93.61 393.55 ✓

Grades on page 46

Oct. 22 1936

Super
Isbell
Moore

67

Set road grades by air valve covers sta 72 + 52 (pipe sta)

B.M. 9 537.23

6.59 543.82

2' lt of pipe 1.84 541.98

2' Rt of pipe 1.36 542.46

Road sta = 338 + 30

Grade = 538.50

Super elev = .120 per foot

& grade carried on inside of curve.

Oct. 23 1936

Soper
Isbell
Moore

68.

top of Valve chamber 426+38

✓
H00.72

5.52 H05.74

4.24 H01.50

✓
m

Oct. 29 1936

Soper
Isbell
Moore

69

top of Valve chamber
(anchor runs to top of Valve box)

Original x-section of drain ditch from valve
chamber sta 160 (0+00 = outside of V. Chamber)

top of V. Chamber ✓ 506.70 $\frac{5.31}{6.5}$
2.3 509.0

0+00 4.3 504.7

0+21 4.3 504.7

0+41 10.7 498.3

Final x-section of drain ditch

Nov. 9 1936
Soper
Isbell
Moore

top of V. Chamber 506.70

1.0 507.7

0+00 11.3 496.4

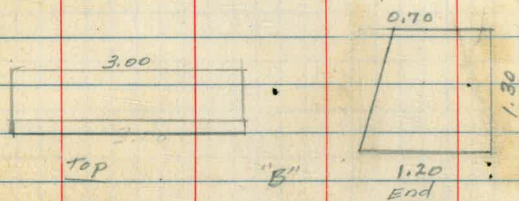
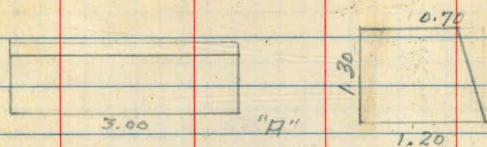
0+42 11.7 496.0

Oct 30 1936

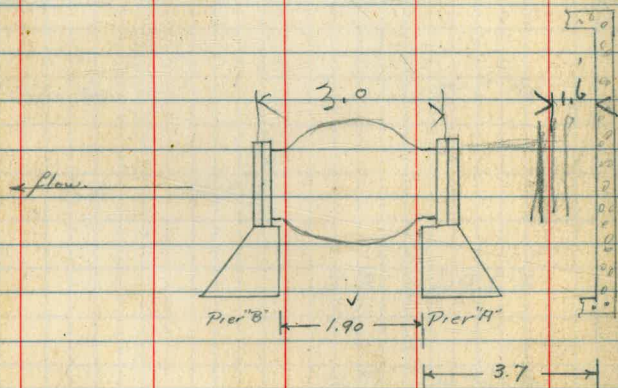
Soper
Isbell
Moore

70

Piers in Pressure Regulator Chamber. 313463



5/8
cal. hole

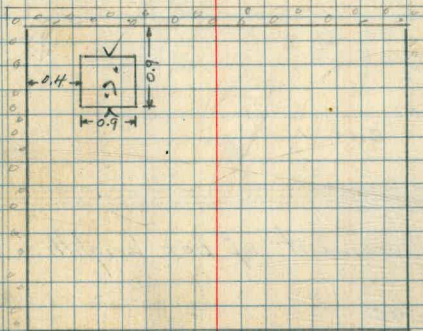


Oct. 29 1936

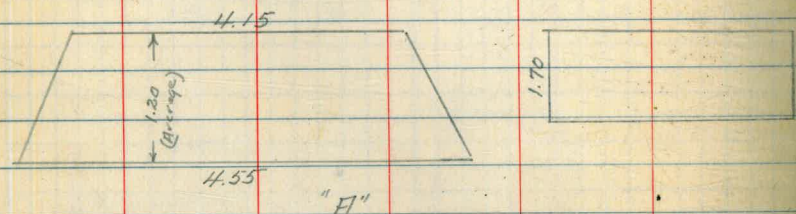
Soper
Isbell
Moore

(copied from scratch pad)

Location of outlet in East wall of Pressure Reg. Chamber
for copper tube connections to panel.
Measurements from inside of Chamber.



Piers in Valve Chamber 426+38.



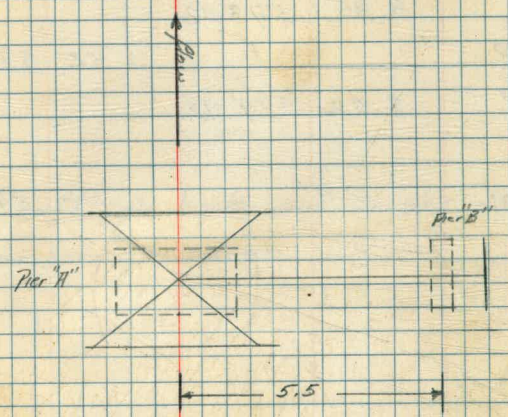
see 528/67 m

Inside measurement of box height = 24 m + Roof + 2 m less for

- 6.95
- 6.90
- 7.09
- 6.97

4) 27.91 / 6.98 Average height

see 528/67 m



B.M on Valve Chamber sta 13+00

B.M#2 570.57

3.35 573.92

TP 2.52 571.40

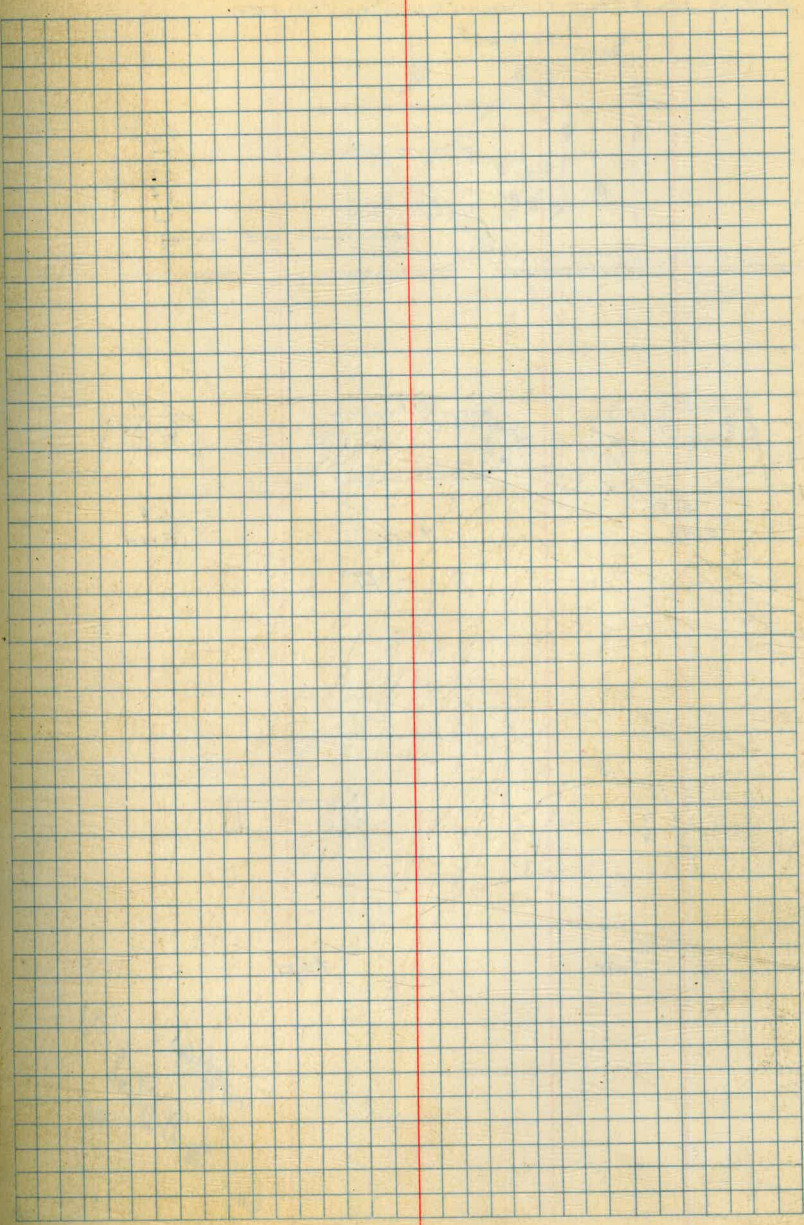
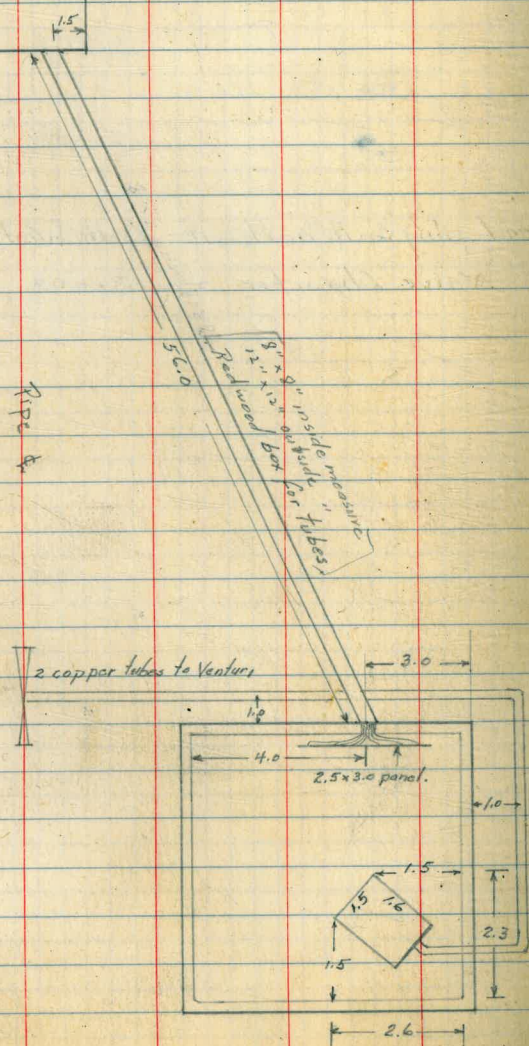
8.52 579.92

B.M 2.55 577.37

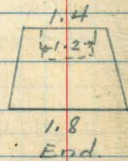
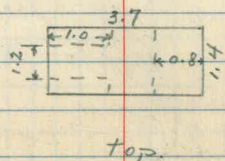
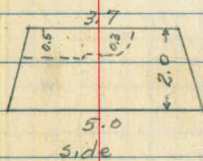
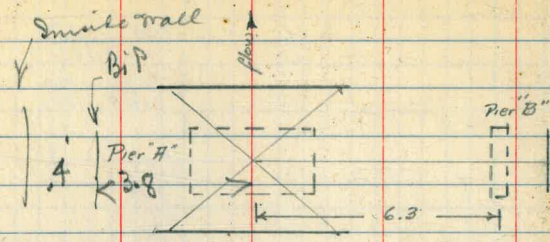
Lead plug with nail in North West Corner of
Valve Chamber sta 13+00

Detail of Recording sta and connections

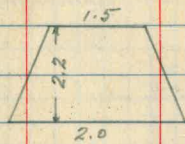
Pressure Rec. Chamber.
See page 71 for detail



Piers in Valve Chamber Sta 160+00



Pier "H"

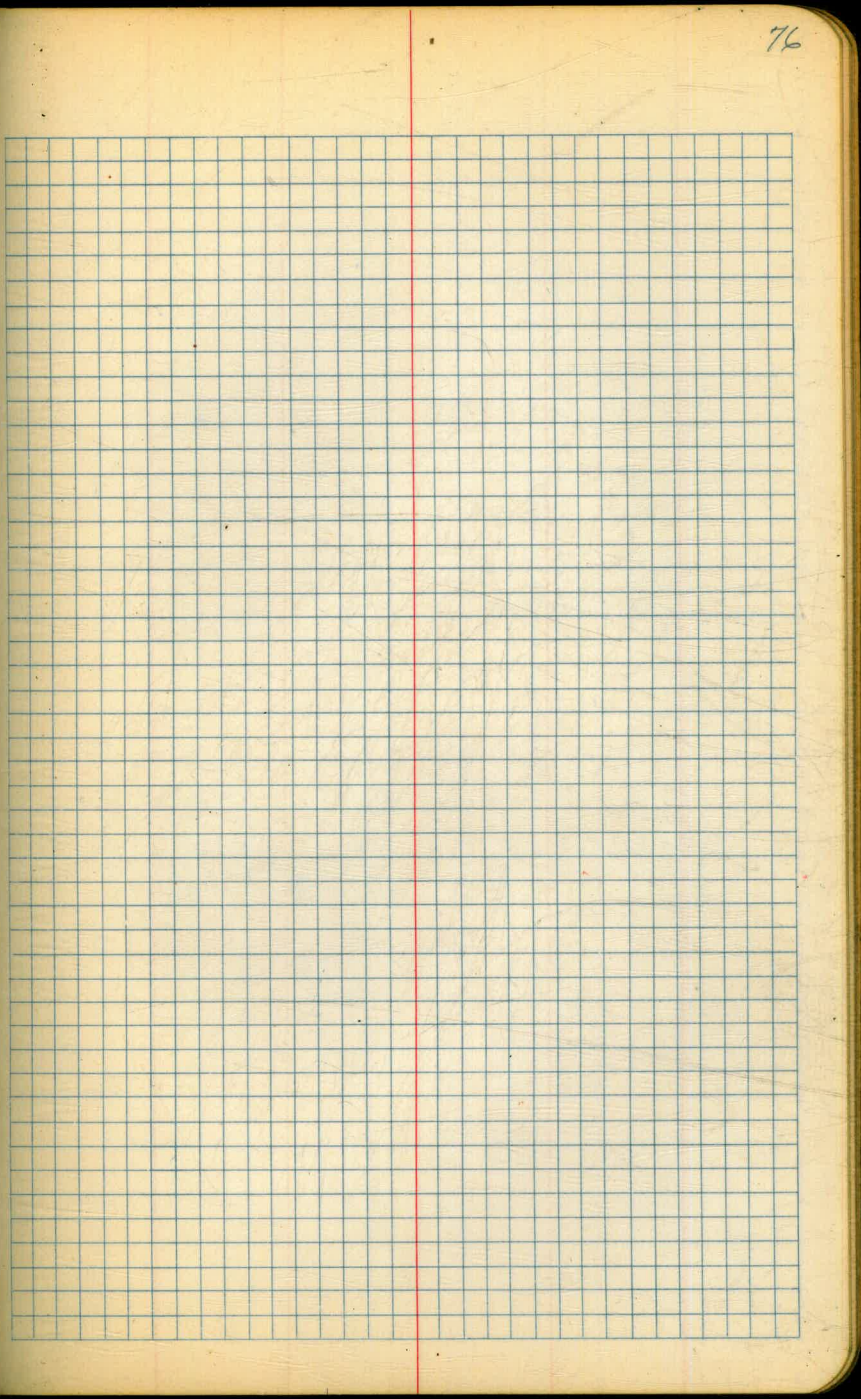
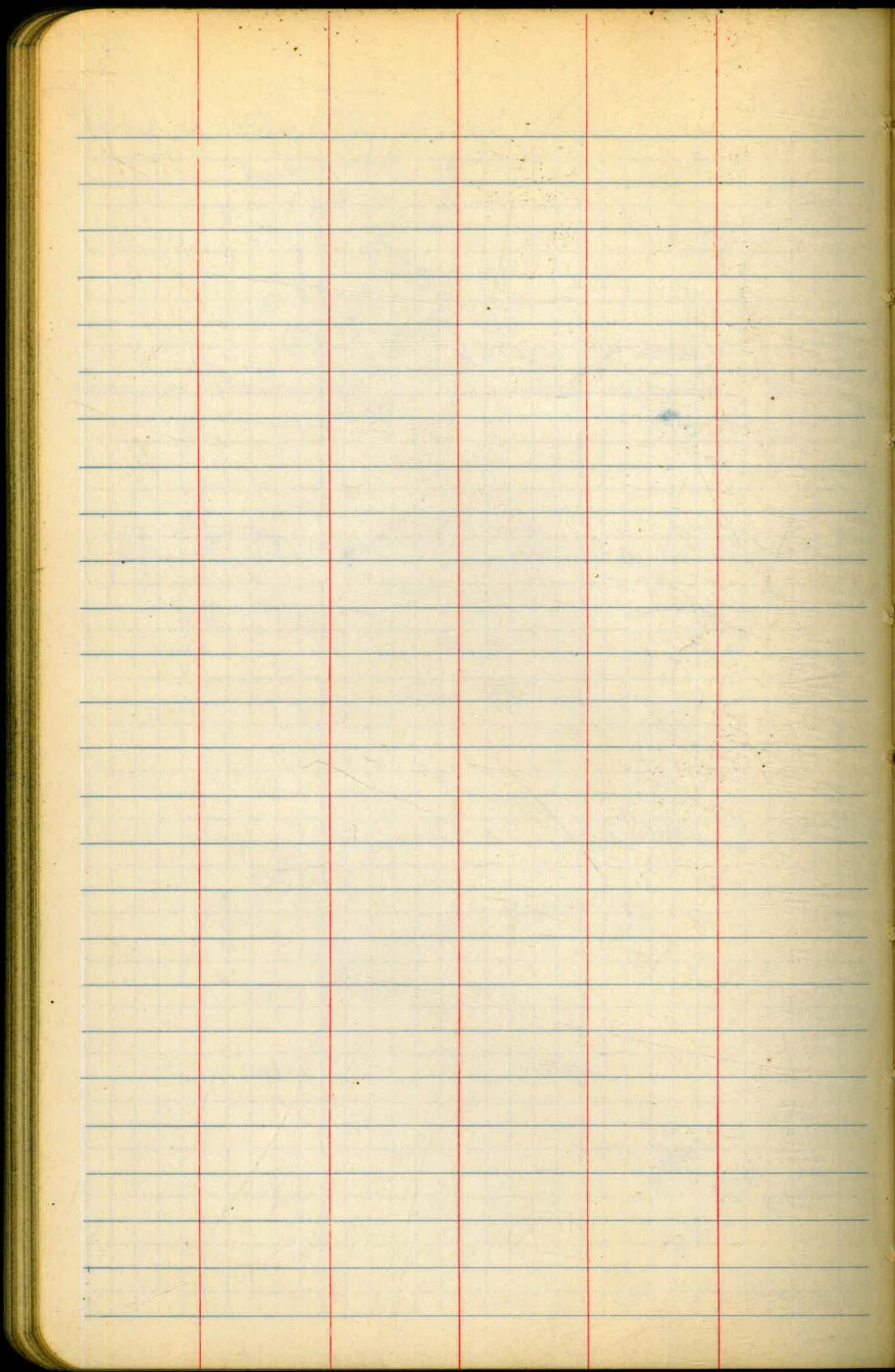


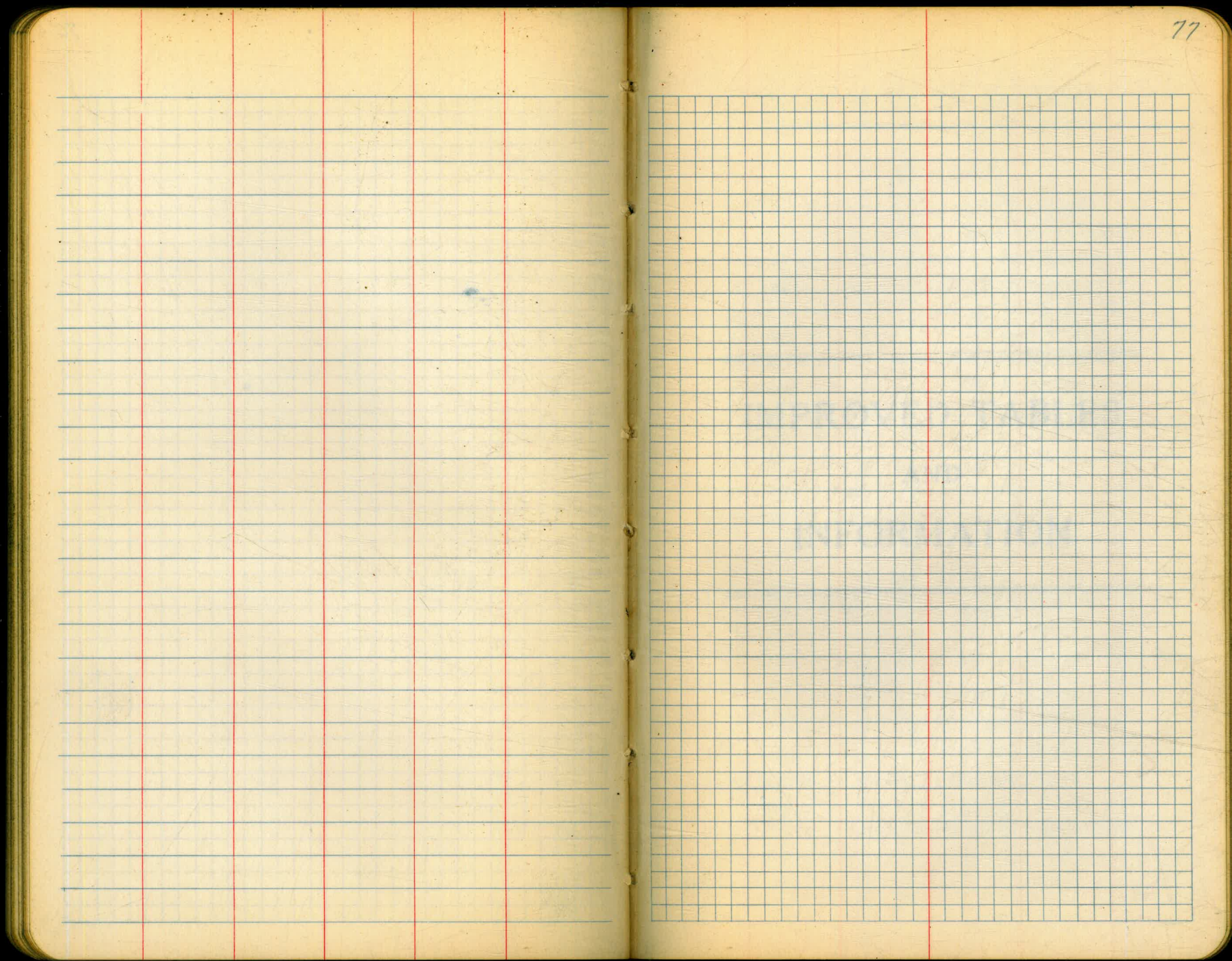
Side



top

17/5/06.
 Au 778564
 22





DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by division tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.