

Levels on San Vicente
Pipe Line —

— South of River —

— B —

Dec. 29th 1926

McGetchin T

Butzine Notes

P Rod

Sta.	+	H.I.	-	Elev.
5+00			3.75	413.22
+50		416.97	5.20	411.77
T.P.	6.65	418.35	0.03	418.32
4+00			0.10	418.25
+50			1.50	408.85
^{1.20} 3+75			3.90	406.45
3+00			2.50	407.85
+50			5.10	405.35
2+00			7.50	402.85
+50			8.40	401.95
1+00			9.00	401.35
0+50			8.90	401.45
0+00			9.10	400.95
B.M.#1	1.48	410.35		408.87

Robert Thomas
17/30/76

1912

1913

1914

1915

1916

1917

1918

1919

1920

1921

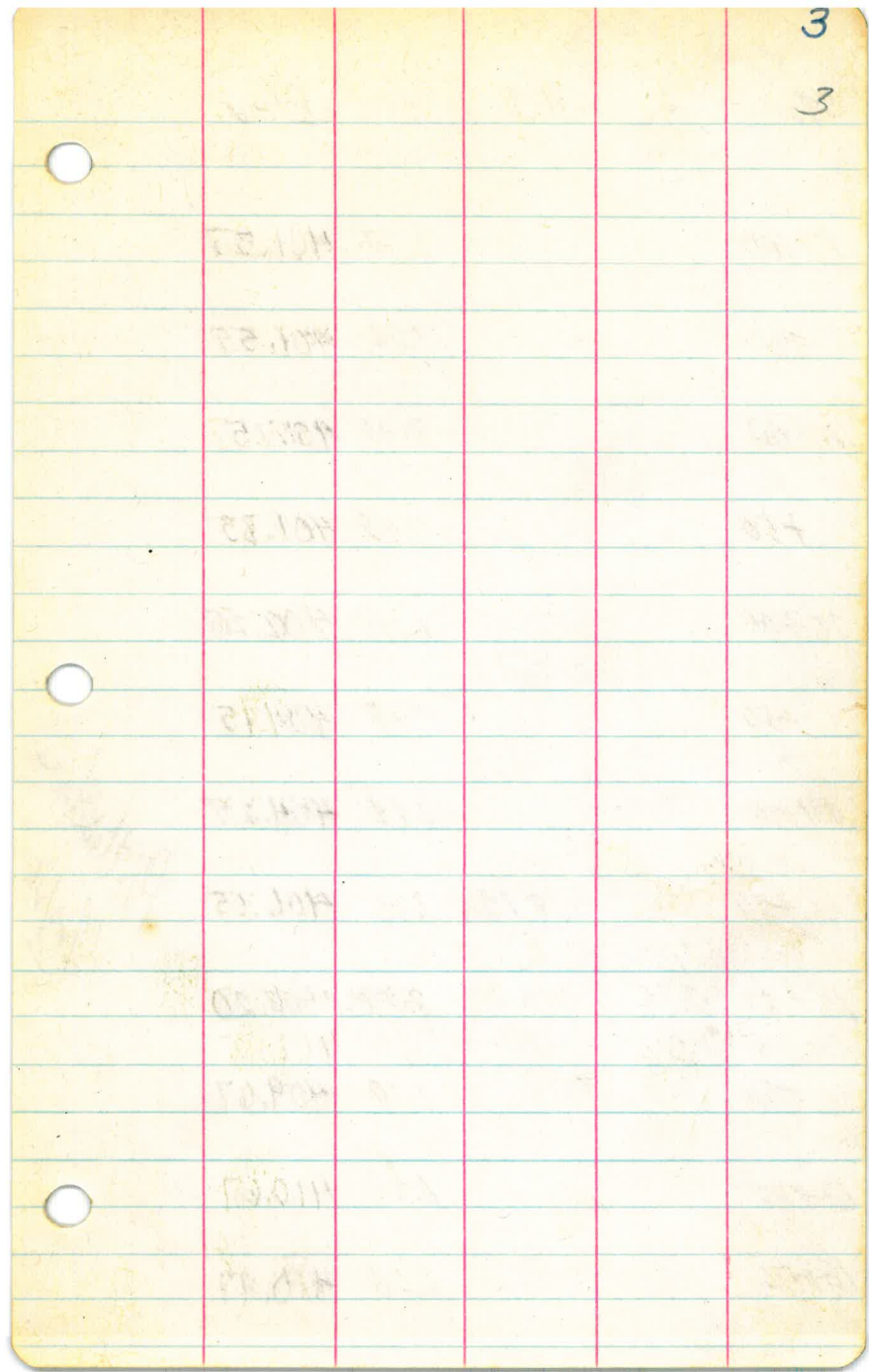
1922

1923

1924

Sta.	+	H.I	-	Elev.	
11+00			5.40	411.57	✓
+50			7.10	409.87	
10+00			8.40	408.57	
+50			7.40	409.57	
9+00			4.20	412.77	
+50			3.30	413.67	
8+00			3.20	413.77	
+50			2.60	414.37	
7+00			2.30	414.67	✓
6+85	4.5 I.D Pipe 6"		4.20	412.77	✓
+50			2.00	414.97	✓
6+00			1.90	415.07	✓
5+50			2.80	414.17	✓

Butler
 June
 7/30/26



3

3

Sta.	+	H.I	-	Elev.
17+00			7.60	401.55 ✓
+50			7.60	401.55
16+00			7.40	401.75
+50			7.40	401.75
15+00			6.90	402.25
+50			5.00	404.15
14+00			4.90	404.25
+50		409.15	3.10	406.05
13+00	0.95	416.98	8.77	408.20
+50			7.30	409.67
12+00			6.30	410.67
11+50			6.00	410.97

Plotted
 1/20/26

4

4

192

22.800

22.800

22.800

22.800

22.800

21.400

22.800

22.800

20.500

20.500

20.500

20.500

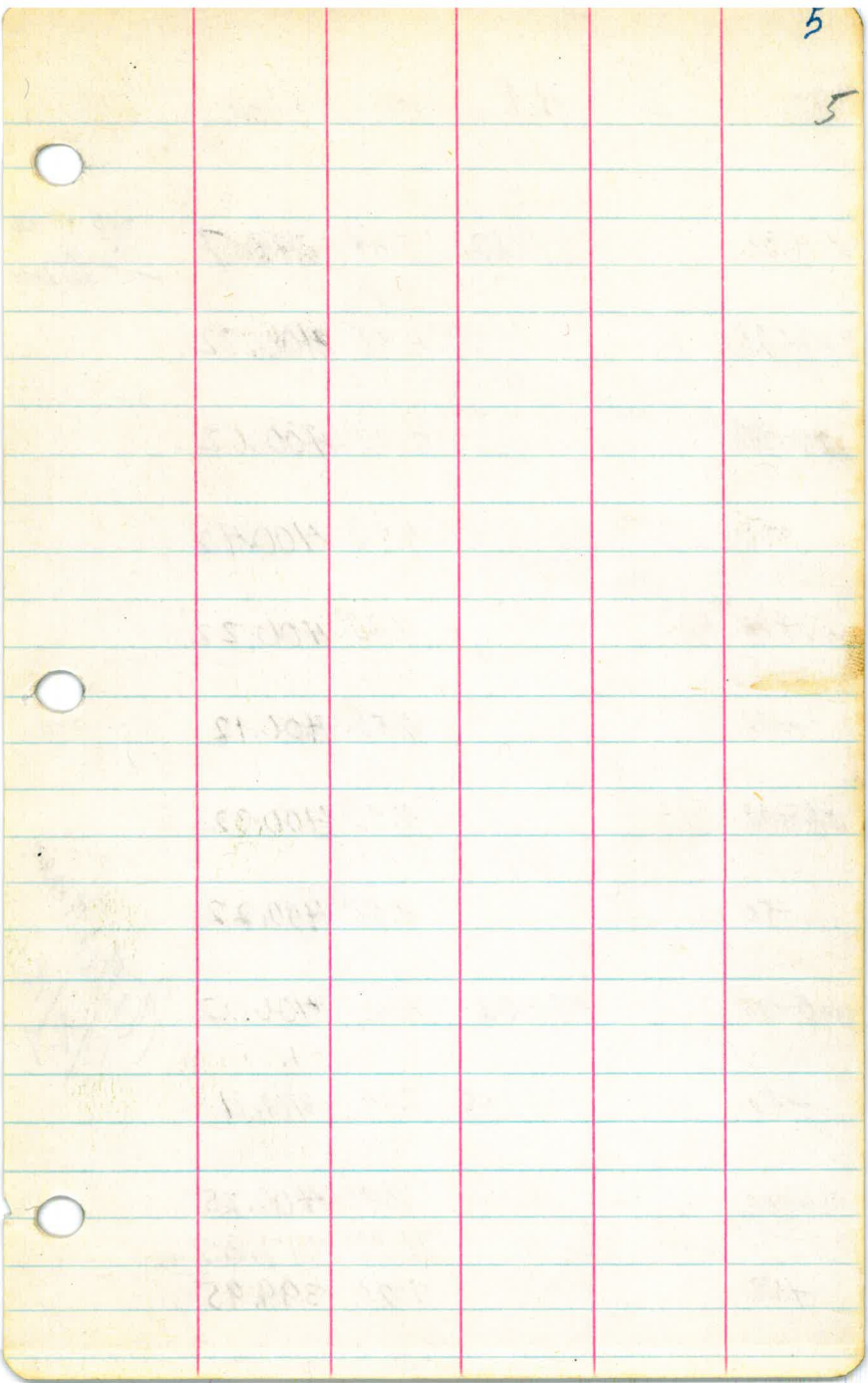
20.500

Sta.	+	H.I.	-	Elev.
23+00			9.70	399.45
+50			9.80	399.33
22+00			9.70	399.45
+50			9.60	399.55
21+00			9.50	399.65
+50			9.70	399.45
20+00			9.70	399.45
+50			9.90	399.25
19+00			7.10	402.05
18+58			7.80	401.95
+50			5.70	403.45
18+00			6.40	402.75
+50			7.20	401.95

R. L. ...
 1/30/76

5

5



Sta.	+	H.I.	-	Elev.	
B.M. #23		404.62	5.45	399.17	399.21 B.M. 399.18 .03 Error
28+40.16			4.40	400.22	
28+00			4.60	400.02	
+50			4.20	400.42	
27+40			4.40	400.22	
+50			4.50	400.12	
26+00			4.30	400.32	
+50			4.40	400.22	
25+00		404.62	4.40	400.22	Plotted 1/20/24
+50	4.71	409.15	9.24	399.91	
24+00			8.90	400.25	
23+90			11.30	397.85	
+50			9.20	399.95	
	ditch				

Profile
Level Notes

'B' Lakeside-San Vicente
Sta. 28+ - 47

Levels on B³ Pipe Line from
 STA. 28+85" = (28+40'⁶) To INT. B¹ Line 43+48'⁹⁵

STA.	+	HI	-	Elev.
28+40' ⁶				400.22
BC.	3.87	404.09		
28+85"			3.43	400.66
EC.				
29+84' ²⁶			7.73	396.36
T.P.	8.46	404.82		
30+00 ⁰			8.90	395.92
30+50 ⁰			9.36	395.46
31+00 ⁰			8.62	396.20
31+50 ⁰			5.10	399.72
32+00 ⁰			5.11	399.72
32+50 ⁰			7.70	397.12
33+00 ⁰			7.10	397.72
33+50 ⁰			7.21	397.61
34+00 ⁰			6.35	398.47
34+50 ⁰			5.45	399.37
T.P.	5.86	405.23		
35+00 ⁰			5.75	399.48
35+50 ⁰			5.20	400.03
36+00 ⁰			5.20	400.03
36+50 ⁰			4.00	401.23
37+00 ⁰			3.70	401.53
37+50 ⁰			5.00	400.23
38+00 ⁰			4.35	400.88
38+19' ⁶¹			4.55	400.68

47+55'
B¹ Line

T.P. EC. - Top Hub

T.P. - P. 1. - Top of Hub

Sta.	+	H.I.	-	Elev.
38+19 ⁴				400.68
T. P.	6.16	406.84		
38+50 ⁰			6.18	400.66
39+00 ⁰			5.00	401.84
39+50 ⁰			4.60	402.24
40+00 ⁰			4.84	402.00
40+50 ⁰			4.76	402.08
41+00 ⁰			4.98	401.86
41+50 ⁰			4.75	402.09
42+00 ⁰			4.70	402.14
42+50 ⁰			5.24	401.60
43+00 ⁰			5.50	401.34
43+48 ⁹			2.31	404.53
			3.85	402.99

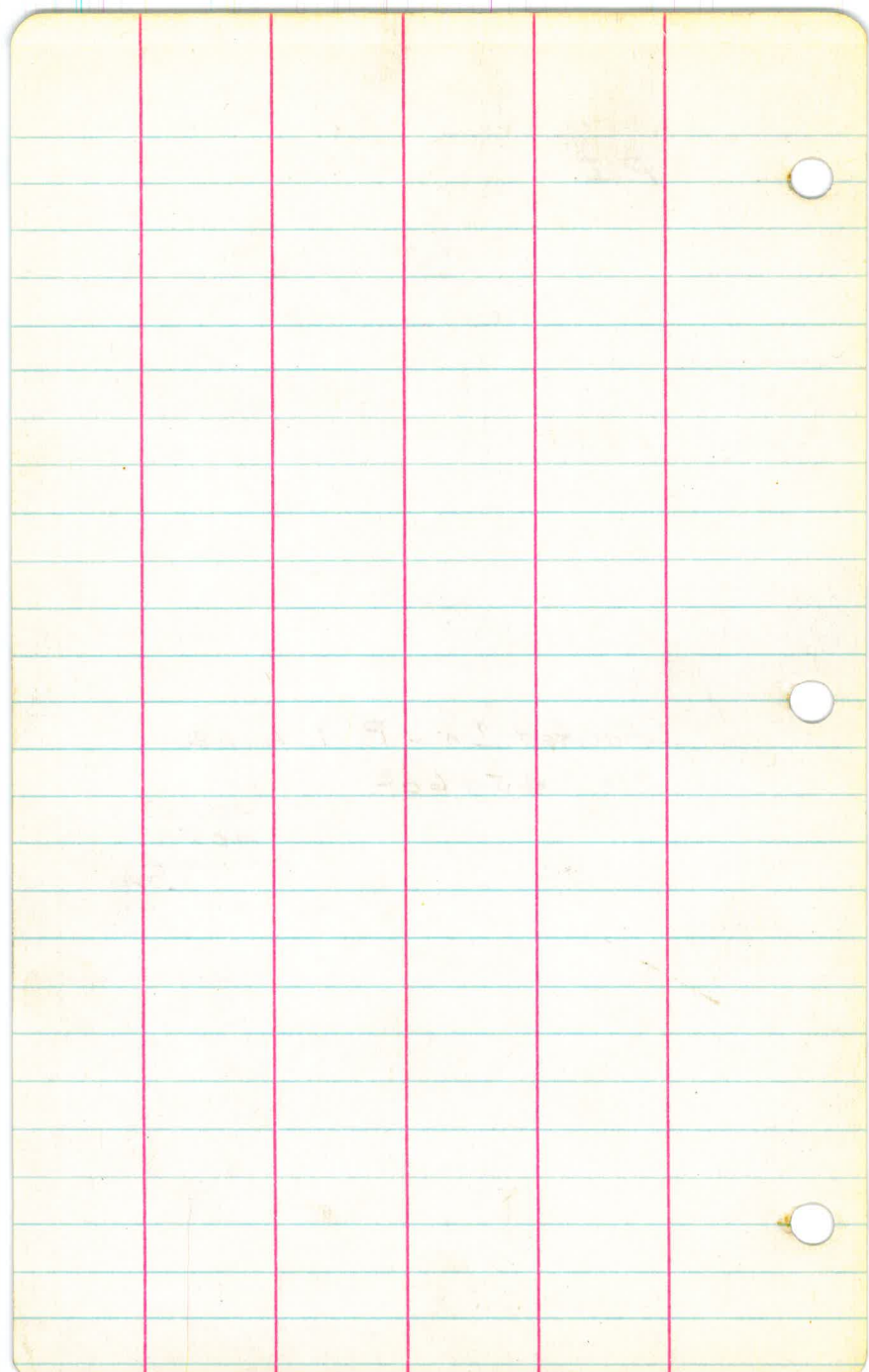
P.I.

Checked In - B. l. line.
Sta. 45+60⁰

403.03

402.99

.04



430
428.44
2.00

6
6

Levels San Vicente

— Pipe Line —

— North Side River —

— Dec 29th 1926 —
Mr. Getchin T
Butzine Notes
? Rod

(Showing Error in B.M. # 26)

B.M. West end San Vicente Bridge

El. 413.94 + 450 417.94

B.M. # 26
- 6.00 411.94 = 419.94

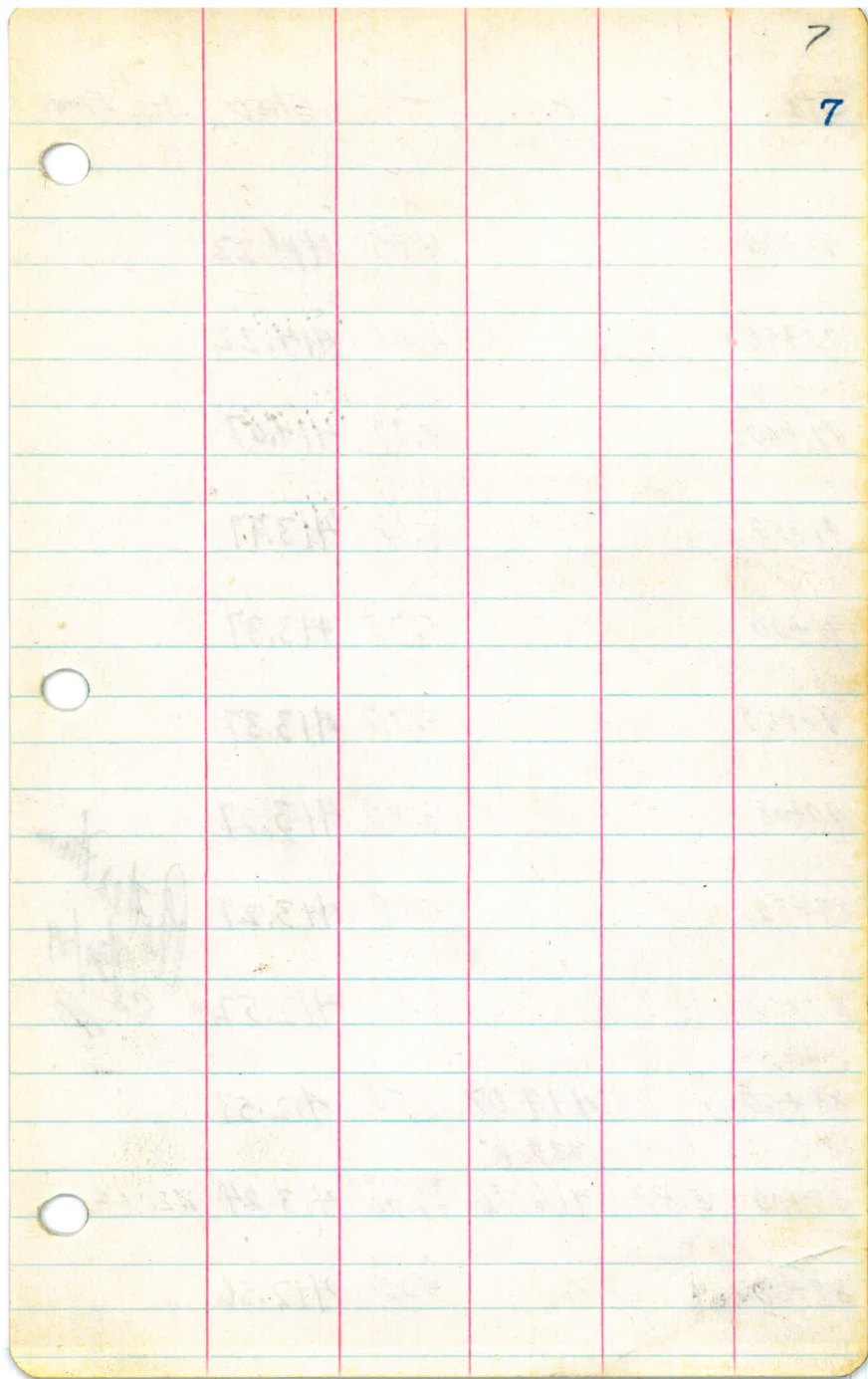
B.M.
Sheet

Sta	T	H.I	-	El.
87+00			3.85	412.91
86+50			4.55	412.21
86+00			5.60	411.16
85+50			4.60	412.16
85+00			4.90	411.86
84+50			5.25	411.51
84+00			4.75	412.01
83+50			4.60	412.16
83+00			5.25	411.51
82+83 ³⁸			5.20	411.56
B.M. ²⁰	4.82	416.76		411.94
County B.M. # 26				
El. 411.94				

*Plotted sheet
1/24/16
CCB*

7

7



Sta.	+	H.I.	-	Elev.	Sta Elev.
93+00			4.85	414.22	
92+50			4.85	414.22	
92+00			5.00	414.07	
91+50			5.10	413.97	
91+00			5.70	413.37	
90+50			5.70	413.37	
90+00			5.80	413.27	
89+50			5.80	413.27	
89+00			6.55	412.52	
88+50		419.07	6.50	412.57	
88+00	5.83	416.76	3.52 T.P. Top. Stake	413.24	420.64
87+50			4.20	412.56	

Robert Hines
 1/20/79
 CRB

Г.С.И.И.

Г.С.И.И.

Г.С.И.И.

Г.С.И.И.

Г.С.И.И.

Г.С.И.И.

Г.С.И.И.

Г.С.И.И.

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Г.С.И.И.

Г.С.И.И.

Г.С.И.И.

Sta.	+	H.I.	-	Elev.	Sta. Elev.
			2.15		
99+00			2.50	416.57	
			2.50		
98+50			2.70	416.37	
98+00			2.90	416.17	
97+50			3.00	416.07	
97+00			3.50	415.57	
96+50			3.60	415.47	
96+00			3.70	415.37	
95+50			3.80	415.27	
95+00			4.00	415.07	
94+50			3.65	415.42	
94+00			4.40	414.67	
93+50			4.50	414.57	

17/30/16
 cc B

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12.11.14

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12.11.14

sta	+	H.I	-	Elev.	sta. Elev.
105+00			5.90	419.59	
104+50			6.10	419.39	
104+00			6.60	418.89	
103+50			7.00	418.49	
103+00			6.80	418.69	
102+50			7.10	418.39	
102+00			7.60	417.89	
101+50			6.55	418.94	
101+00			8.10	417.39	
100+50		425.49	8.30	417.19	
100+00	8.56	419.07	2.14	416.93	
99+50			2.10	416.97	

Proctor
 1/20/26
 CKB

PC. 124

PC. 124

PC. 124

PC. 124

PC. 124

PC. 124

PC. 124

PC. 124

PC. 124

PC. 124

PC. 124

PC. 124



Sta.	+	H.I.	-	Elev.	Sta.	Elev.
121+00			3.75	421.74		
+50			4.95	420.54		
110+00			4.45	421.04		
+50			4.10	421.39		
109+00			3.80	421.69		
+50			4.30	421.19		
108+00			4.60	420.89		
+50			4.40	421.09		
107+00			4.85	420.64		
+50			4.90	420.59		
106+00			4.90	420.59		
105+50		425.49	5.90	419.59		

Potted
 shms
 at 12/21/26

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Sta.	+	H.I.	-	Elev	Sta. Elev.
117+00			8.00	421.57	
+50			7.45	422.12	
116+00			8.05	421.52	
+50		429.57	9.00	420.57	
115+00	860	425.49	4.52	420.97	
+50			6.10	419.39	
114+00			6.00	419.49	
+50			5.80	419.69	Added lines 12/30/16 OK
113+00			5.00	420.39	
+50			4.20	421.29	
112+00			4.60	420.89	
111+50		425.49	4.50	420.99	

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Sta.	+	H.I.	-	Elev.	
123+00			5.10	424.47	
+50			5.20	424.37	
122+00			4.80	424.77	
+50			7.70	421.87	
121+00			4.90	424.67	
+50			4.70	424.87	
120+00			5.90	423.67	Plotted Ames 1/20/10 CK B
+50			6.15	423.42	
119+00			6.50	423.07	
+50			6.60	422.97	
B.M. 204 423.00			6.56	423.01	
118+00			8.00	421.57	
8.00					
117+50		429.57	7.30	422.27	

13

13

Pole County S.H.# 282 marked E1.423"

431.01
4.23
<hr/>
801

Sta.	+	H.I.	-	Elev.
129+00			7.00	426.73
^{B.M. 29} 428.81		433.73	5.41	428.32 ✓
+50			7.55	426.18
128+00			8.00	425.73
+50		433.73	8.20	425.53
127+00	6.55	429.57	2.39	427.18
+50			3.00	426.57
126+00			3.70	425.87
+50			3.70	425.87
125+00			4.30	425.27
+50			5.00	424.57
124+00			4.00	425.57
123+50		429.57	4.20	425.37

Rotten
 Kimo
 1/21/6
 CKB

ETCH

On Palo 425.499

436	3
428	1
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8	02

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Sta.	t	H.I.	-	Elev.
135+00			6.00	427.73
+50			5.70	428.03
134+00			5.60	428.13
50			5.35	428.38
133+00			5.75	427.98
+50			6.35	427.38
132+00			7.70	426.03
+50			6.00	427.73
131+00			6.15	427.58
+750			6.40	427.33
130+00			7.25	426.48
129+50			7.10	426.63

B. J. Jones
 1/20/26

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114

115

Sta.	x	H.I.	-	Elev.	
147+00			3.50	430.58	
+50			3.90	430.18	
140+00			3.30	430.78	
+50			4.00	430.08	
139+00			4.60	429.48	
+50		434.08	4.40	429.68	
138+00	5.12	433.74	4.77	428.96	Potted lines 1/20/16 OK B
+50			4.55	429.18	
137+00		433.74	4.50	429.23	
+50			4.60	429.13	
136+00			4.80	428.93	
135+50			5.00	428.73	

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Sta.	f	H.I.	-	Elev.	
147+00			5.80	428.28	
+50			6.65	427.43	
146+00			6.40	427.68	
+50			6.90	427.18	
145+00			6.75	427.33	
+50			7.00	427.08	
144+00			7.50	426.58	
+50			6.90	427.18	Putter
143+00			5.20	428.88	lines
+50			2.00	432.08	11/30/16 CR B
142+00			3.80	430.88	
141+50			3.55	430.53	

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04.02.17

05.02.17

06.02.17

07.02.17

08.02.17

09.02.17

10.02.17

11.02.17

12.02.17

13.02.17

14.02.17

Sta.	+	H.I.	-	Elev.
153+00			11.50	429.50
B.M. #30E "436.70			4.28	436.73
+50			8.90	432.10
			9.85	431.15
152+00			11.00	430.00
+50			11.20	429.80
151+00			11.45	429.55
+50		441.00	4.52	429.56
150+00	11.44	434.09	4.60	429.48
+50			4.80	429.28
149+00			4.90	429.18
+50			5.00	429.08
148+00			5.40	428.68
147+50				

*Partial
lines
at
B*

DATE	DESCRIPTION	AMOUNT	BALANCE
11/10/20
11/11/20
11/12/20
11/13/20
11/14/20
11/15/20
11/16/20
11/17/20
11/18/20
11/19/20
11/20/20
11/21/20
11/22/20
11/23/20
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11/26/20
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11/28/20
11/29/20
11/30/20

Sta.	+	H.I.	-	Elev.
159+00			4.75	436.25
+50			4.90	436.10
158+00			5.40	435.60
+50			5.00	436.00
157+00			6.70	434.30
+50			5.75	435.25
156+00			4.70	436.30
+50			5.20	435.80
155+00			5.60	435.40
+50			5.50	435.50
154+00			5.50	435.50
153+50			6.25	434.75

Plotted
 this
 1/20/26
 CKB

19

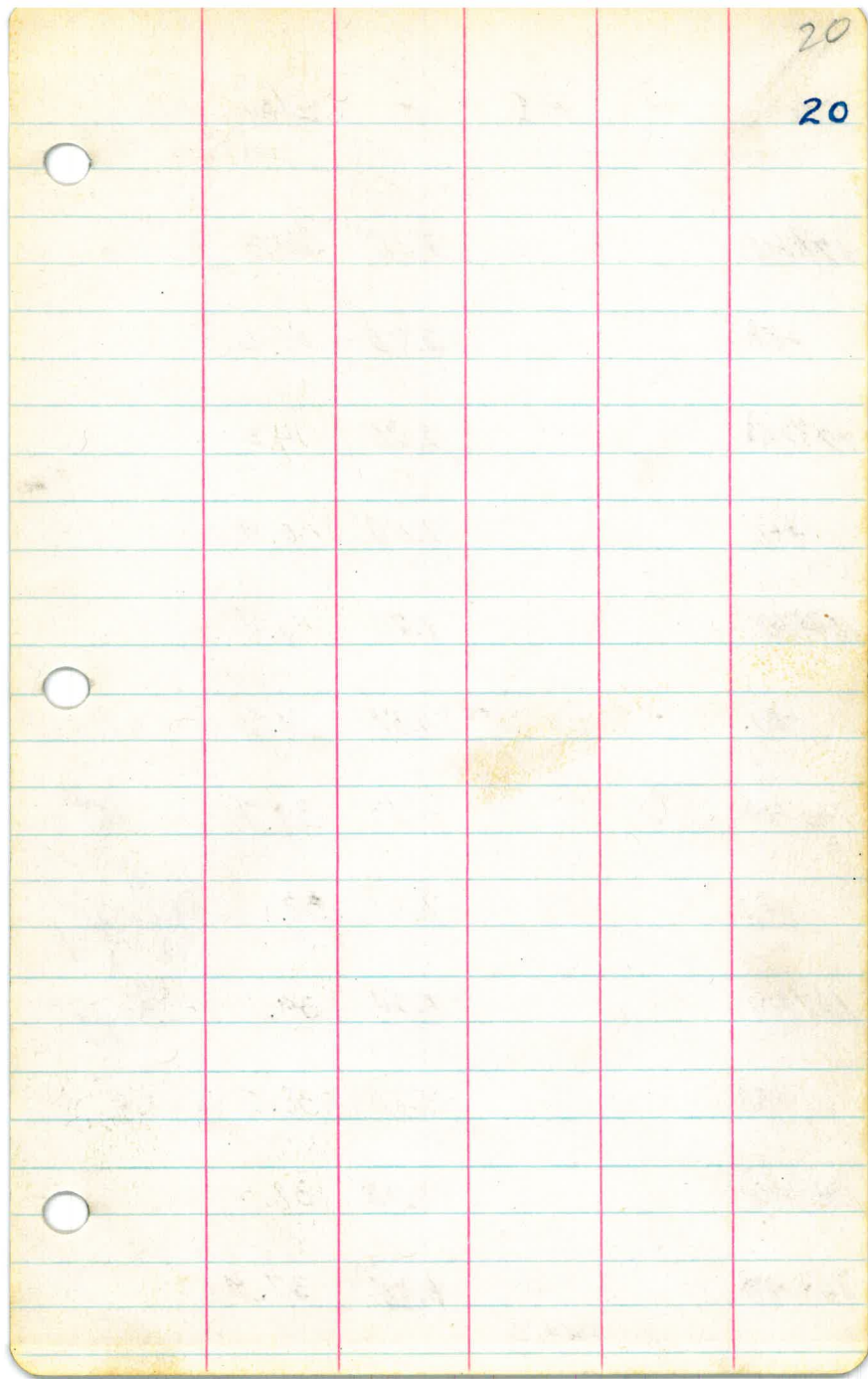
19



Sta.	+	H.I.	-	Elev.	
165+00			6.50	37.8	
+50			6.80	37.5	
164+00			6.90	37.4	
+50			7.20	37.1	
163+00			7.50	36.8	
+50		³ 444.27	7.60	436.7	-
162+00	7.37	441.01	4.10	436.90	
+50			4.80	436.20	-
161+00			5.00	436.00	- Pitted Areas
+50			4.50	436.50	- at 1/30/26 S
160+00			4.65	436.35	
159+50			4.70	436.30	-

20

20



Sta.	+	H.I.	-	Elev.	
171+00			3.00	41.3	
+50			2.70	41.6	
170+00			3.00	41.3	
+50			3.40	40.9	
169+00			3.90	40.4	
+50			4.50	39.8	
168+00			4.60	39.7	
+50			5.20	39.1	Checked 11/20/16
167+00			5.20	39.1	OK B
+50			5.80	38.5	
166+00			6.10	38.2	
165+50			6.40	37.9	

444.3
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Sta	+	H.I.	-	Elev.
177+00			6.40	40.9
+50			6.70	40.6
176+00			6.70	40.6
+50			6.35	40.9
175+00			5.00	47.3
+50			4.80	47.5
174+00			4.50	47.8
+50			5.50	41.8
+25			5.60	41.7
173+00		445.29	1.35	45.94
B.M. #21	3.68	447.29	3.68	443.61
+50	3.56	444.28	0.55	443.73
172+00			1.00	43.3
171+50			3.30	41.0
		44.3		

Plotted
 Hines
 1/30/76
 et B

22

22

459
11.3
57.2

Sta.	+	H.I.	-	Elev.	
183+00			4.40	45.3	
+50			4.70	45.0	
182+00			5.00	44.7	
+50			4.90	44.8	
181+00			5.10	44.6	
+50			5.60	44.1	
180+00			5.60	44.1	
+50			6.00	43.7	Plotted lines 11/10/76 CKB
179+00			6.30	43.4	
+50		449.69 ^{7.1}	6.20	43.5	
178+00	6.82	447.29	4.42	442.87	✓
177+50			4.50	42.8	

Sta.	+	H.I.	-	Elev.	
189+00		452.86 ⁹	5.90	47.0	
+50	6.20	449.69	3.09	446.60	
188+00			3.10	46.6	
+50			3.00	46.7	
187+00			3.10	46.6	
+50			3.40	46.3	
186+00			3.60	46.1	
+50			3.90	45.8	Plotted Amis Ct 13
185+00			4.20	45.5	
+50			4.10	45.7	
184+00			4.10	45.6	
+50		449.7	4.30	45.4	

24

24

Sta.	+	H.I.	-	Elev.	
195+00			4.60	48.3	
194+50			4.50	48.4	
194+00			4.40	48.5	
193+50			4.40	48.5	
193+00			4.40	48.5	
192+50			4.60	48.3	
192+00			4.80	48.1	
191+50			5.20	47.7	Putted fines
191+00			5.50	47.4	11/30/76
190+50			5.80	47.1	CK B
190+00			5.50	47.4	
189+50			5.90	47.2	
		452.9			

Sta.	+	H.I.	-	Elev.	
207+00			4.70	52.7	
+50			5.10	52.3	
200+00			5.70	51.7	
+50			4.30	53.1	
199+00		457.40	4.10	53.3	
T.P.	5.22	459.72	7.54	452.18	✓
+50			7.80	51.9	
Top Bank 198+25			4.40	55.3	
198+00			4.40	55.3	
+50			4.20	55.5	Plotted
197+00		459.72	4.50	55.2	Axis
+50	9.89	452.86	2.97	449.89	✓ 17/3/16
196+00			4.60	48.3	OK B
+50			4.50	48.4	
		452.9			

26

26

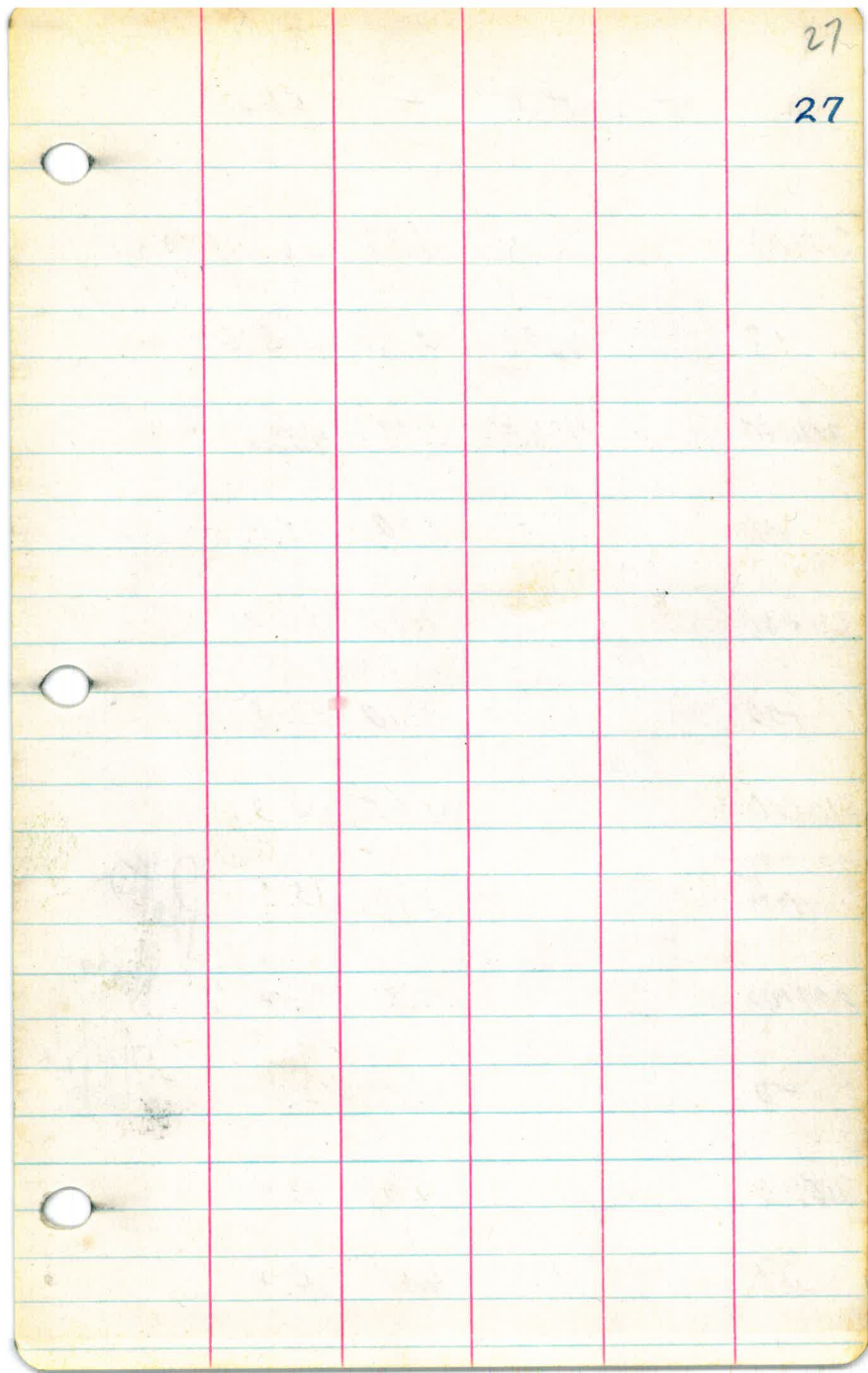
1	1.1	1.2	1.3	1.4
2	1.1	1.2	1.3	1.4
3	1.1	1.2	1.3	1.4
4	1.1	1.2	1.3	1.4
5	1.1	1.2	1.3	1.4
6	1.1	1.2	1.3	1.4
7	1.1	1.2	1.3	1.4
8	1.1	1.2	1.3	1.4
9	1.1	1.2	1.3	1.4
10	1.1	1.2	1.3	1.4
11	1.1	1.2	1.3	1.4
12	1.1	1.2	1.3	1.4
13	1.1	1.2	1.3	1.4
14	1.1	1.2	1.3	1.4
15	1.1	1.2	1.3	1.4
16	1.1	1.2	1.3	1.4
17	1.1	1.2	1.3	1.4
18	1.1	1.2	1.3	1.4
19	1.1	1.2	1.3	1.4
20	1.1	1.2	1.3	1.4
21	1.1	1.2	1.3	1.4
22	1.1	1.2	1.3	1.4
23	1.1	1.2	1.3	1.4
24	1.1	1.2	1.3	1.4
25	1.1	1.2	1.3	1.4
26	1.1	1.2	1.3	1.4
27	1.1	1.2	1.3	1.4
28	1.1	1.2	1.3	1.4
29	1.1	1.2	1.3	1.4
30	1.1	1.2	1.3	1.4
31	1.1	1.2	1.3	1.4
32	1.1	1.2	1.3	1.4
33	1.1	1.2	1.3	1.4
34	1.1	1.2	1.3	1.4
35	1.1	1.2	1.3	1.4
36	1.1	1.2	1.3	1.4
37	1.1	1.2	1.3	1.4
38	1.1	1.2	1.3	1.4
39	1.1	1.2	1.3	1.4
40	1.1	1.2	1.3	1.4
41	1.1	1.2	1.3	1.4
42	1.1	1.2	1.3	1.4
43	1.1	1.2	1.3	1.4
44	1.1	1.2	1.3	1.4
45	1.1	1.2	1.3	1.4
46	1.1	1.2	1.3	1.4
47	1.1	1.2	1.3	1.4
48	1.1	1.2	1.3	1.4
49	1.1	1.2	1.3	1.4
50	1.1	1.2	1.3	1.4
51	1.1	1.2	1.3	1.4
52	1.1	1.2	1.3	1.4
53	1.1	1.2	1.3	1.4
54	1.1	1.2	1.3	1.4
55	1.1	1.2	1.3	1.4
56	1.1	1.2	1.3	1.4
57	1.1	1.2	1.3	1.4
58	1.1	1.2	1.3	1.4
59	1.1	1.2	1.3	1.4
60	1.1	1.2	1.3	1.4
61	1.1	1.2	1.3	1.4
62	1.1	1.2	1.3	1.4
63	1.1	1.2	1.3	1.4
64	1.1	1.2	1.3	1.4
65	1.1	1.2	1.3	1.4
66	1.1	1.2	1.3	1.4
67	1.1	1.2	1.3	1.4
68	1.1	1.2	1.3	1.4
69	1.1	1.2	1.3	1.4
70	1.1	1.2	1.3	1.4
71	1.1	1.2	1.3	1.4
72	1.1	1.2	1.3	1.4
73	1.1	1.2	1.3	1.4
74	1.1	1.2	1.3	1.4
75	1.1	1.2	1.3	1.4
76	1.1	1.2	1.3	1.4
77	1.1	1.2	1.3	1.4
78	1.1	1.2	1.3	1.4
79	1.1	1.2	1.3	1.4
80	1.1	1.2	1.3	1.4
81	1.1	1.2	1.3	1.4
82	1.1	1.2	1.3	1.4
83	1.1	1.2	1.3	1.4
84	1.1	1.2	1.3	1.4
85	1.1	1.2	1.3	1.4
86	1.1	1.2	1.3	1.4
87	1.1	1.2	1.3	1.4
88	1.1	1.2	1.3	1.4
89	1.1	1.2	1.3	1.4
90	1.1	1.2	1.3	1.4
91	1.1	1.2	1.3	1.4
92	1.1	1.2	1.3	1.4
93	1.1	1.2	1.3	1.4
94	1.1	1.2	1.3	1.4
95	1.1	1.2	1.3	1.4
96	1.1	1.2	1.3	1.4
97	1.1	1.2	1.3	1.4
98	1.1	1.2	1.3	1.4
99	1.1	1.2	1.3	1.4
100	1.1	1.2	1.3	1.4

Sta	+	H.I.	-	Elev	
207+00			4.40	54.1	
+50			4.30	54.2	
206+00			4.50	54.0	
+50		⁵ ✓ 458.46	4.80	52.7	
205+00	4.68	457.40	3.62	453.78 ✓	
+50			3.50	53.9	
204+00			3.50	53.9	
+50			3.50	53.9	
203+00			4.60	52.8	
+50			6.10	51.3	
202+00			5.20	52.7	
+50			4.80	52.6	

Plotted
Hines
1/12/26
OK B ✓

27

27



Sta.	+	H.I.	-	Elev.
213+00			11.30	56.7
+50		468.04	12.40	55.6
212+00	12.57	458.46	2.99	455.47 ✓
+50			3.30	55.2
211+00			3.60	54.9
+50			3.70	54.8
210+00			4.20	54.3
+50			5.00	53.5
209+00			5.30	53.2
+50			4.80	53.7
208+00			4.60	53.9
+50			4.80	54.2

Plotted
 Hous
 11/20/26
 ok P.B.

1-3-27
 Van Horn
 Drebert
 Super
 Madley
 Bisby

28

Profile of Pipe Line
 Lakeside to San Vicente

222+34.82	470.26	-9.05	61.3
+50	465.51	-7.20	63.1
+75	477.76	-8.40	61.9
223+00	476.89	-8.15	62.1
+25		-9.20	61.1
+50		-10.15	60.1
+75		-8.60	61.7
224+00		-8.60	61.7
+26.84		-10.25	60.0
+50		-10.05	60.3
225+09.44		-10.05	60.3
# on rock		-4.75	465.51
+12.25	477.76		
B.M. on culvert (476.82)		-0.87	476.89

Arthur Decker
December 1927

Vanishing
Beeper
Spor
12/29-26

Cut stakes @ Sump Lakeside

on 544				378.01
	+4.75	382.76		376.35
'A'	-4.73		C. 1.70	378.03
'B'	-4.52		C. 1.91	378.24
'C'	-4.79		C. 1.64	377.97
'D'	-4.71		C. 1.72	378.08
'E'	-4.62		C. 1.81	378.14
'F'	-4.68		C. 1.75	378.08
'G'	-4.96		C. 1.53	377.80
'H'	-4.76		C. 1.67	378.00
on 0	-5.06			377.70

on 544				378.01
	+4.75	382.76		377.435
			-5.325	
	+3.035	380.470		374.07
			-6.40	
	+4.60	378.67		373.73
on switch			-4.94	

29.

12-30-26
Van Hoyt
Drebert
Soper
Mackey
Bisby

29

Profile of Pipe Line Lakeside to San Vicente.

TP On rock 218+35 5'L				464.47
	+5.73	470.20 ✓		
218+25			-8.34	461.9'
+50			-11.02	459.2'
+75			-7.89	462.3'
219+00			-6.26	463.9'
+26.41 (E.C.)			-7.70	462.5'
+40			-11.48	458.7'
+50			-9.80	460.4'
+80			-9.20 ✓	461.0'
TP 220+66 5'R on rock	+2.45	469.25	-3.40	466.80 ✓
219+90.97 (B.C.)		10 39	-7.85	6 1.3
220+00		456.86 11 40	-9.75	59.5
+25		476 76	-7.60	61.6
+50			-8.20	61.0
+75			-8.20	61.0
221+00			-8.80	60.4
+25			-10.00	4' above stream bed 59.3
+50			-10.70	58.5
TP 221+49 on line			-10.39	458.86 ✓
	+11.40	470.26		
221+75			-12.30	58.0
222+00			-10.30	60.0

Profile of Pipe Line
Lakeside to San Vicente

DATE	DESCRIPTION	AMOUNT	BALANCE
1950			
1951			
1952			
1953			
1954			
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2022			
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2025			
2026			
2027			
2028			
2029			
2030			

12-30-26
 Van Horn
 Drebe
 Sobbe
 Mackay

Profile of Pipe Line Lakeside
 to San Vicente

Port Rock 218+35 5L.	470.20		462.47
+5.73			
+25	-8.31	Granite Boulders	461.86
+50	-11.02	"	459.18
+65	-6.85	"	463.55
+75	-7.89	"	462.31
219+00	-6.26	"	463.94
+26.41 E.C.	-7.70	"	462.50
+40	-11.48	"	458.72
+50	-9.8	"	460.40
+80	-9.2	"	461.00
220+00	10.1	"	460.1
+35	1.3	"	468.9
+50	1.9	"	468.3
TP 220+66 5 R.	474.61	-3.40	466.80
+2.81	5.00	"	469.6
A220 +49.33	5.20	"	469.4
221+00	8.10	"	466.5
+35	3.5	"	471.1
+50	6.7	"	467.9
222+00	8.3	"	466.3
+50	8.9	"	465.7
+61.33 E.C.	8.8	"	465.8
+75	7.1	"	467.5

Wrong
 line change
 see page 29

~~Sta. + H.I. - E/O.~~

228400

+50

224400

+50

223400

+50

222400

+50

221400

+50

220400

+50

12/30-26 90
Party same

Profile Pipeline Lakeside
to San Vicente (Con)

			Granite Boulders	
	474.61			
223+00	'	-6.90	"	467.7
+25		-9.20	"	465.4
+50		-7.10	"	467.1
TP +42 3' R		-6.12	"	468.19
	+7.96	476.15	"	
+75		-11.1	"	465.0
224+00		-10.5	"	465.6
+131 LEC		-10.20	"	465.9
+21		-9.4	edg. Dump	466.7
+30		-5.1	on "	471.0
+43		-4.6	on "	471.5
+50		-7.5	edg. Dump	468.6
225+00		-1.6	Granite Ledge	474.5
+10.92 (2x) 5' R		-1.47	"	474.68
TP on Rock 20' Upstream From Bx 52 10' From Pave		-1.96		474.19
	+6.39	480.58		
B.M. on Hd w/ll Culv.		3.71		476.87 (476.83)?

W
600
Line Change
See page 29

Sta.	+	H.I.	-	Elev.
231+00				
	+50			
232+00				
	+50			
233+00				
	+50			
234+00				
	+50			
235+00				
	+50			
236+00				
	+50			

28

30



Sta.	+	H.I.	-	Elev.	
219+00					
+50					
T.P.		474.21	9.74	464.47	
218+00			9.40	64.8	
217+75			8.20	66.0	
+50			10.10	64.1	
217+00			10.60	63.6	
+50		474.21	6.60	67.6	
T.P.	8.72	468.04	2.55	465.49	✓
216+00		465.89	5.70	67.3	
+50			7.40	60.6	
215+00			7.60	60.4	
+50			7.70	60.3	
214+00			8.80	59.2	
+50			11.60	56.4	

Checked
 1/31/17

Checked
 1/31/17
 [Signature]

Profile Pipe Line Lakeside to San Vicente

#4 in Cottonwood Eriess Garage	404.22		399.21
+5.01			
B.C. 28+40.16		-2.1	400.1
29+00		-3.6	400.6
P		-5.26	398.96
+4.05	403.01		
29+39.58		-8.50	394.50
+50		-8.80	394.20
30+00		-7.30	395.29
+50		-7.90	395.10
31+00		-7.15	395.86
+50		-6.20	396.81
32+00		-6.00	397.01
+50		-4.40	398.61
32+83.0970.7		-7.00	396.01
33+00		-7.2	395.81
+50		-8.5	394.51
34+00		-7.7	395.31
+10	Fence	-7.5	395.51
+4588 B.C.		-7.0	396.01
+50	Plotted Benchmark	-6.70	396.31
+75		-6.10	396.91
35+00		-7.10	395.91
+25		-6.80	396.21

		40301		
TP+50			-6.13	396.88
	+3.54	40042		
River channel 35+75		⁹³	-4.50	395.92
Fence 35+93			-4.60	395.82
36+00			-4.60	395.82
+25			-5.40	395.02
+50			-5.10	395.32
+68.70 (E.C.)			-5.00	395.42
River channel +70			-4.90	395.52
37+00			-3.50	396.92
+50			-4.10	396.32
38+00			-4.90	395.52
+50			-4.80	395.62
39+00			-4.80	395.62
+50			-4.90	395.52
40+00			-5.00	395.42
+50			-4.90	395.52
41+00			-4.40	396.02
+50			-4.40	396.02
42+00			-4.10	396.32
+50			-4.00	396.42
43+03.50 (P.O.t.)			-3.70	396.72
+50			-3.30	397.12
44+00			-2.50	397.92
+50			-2.80	397.62

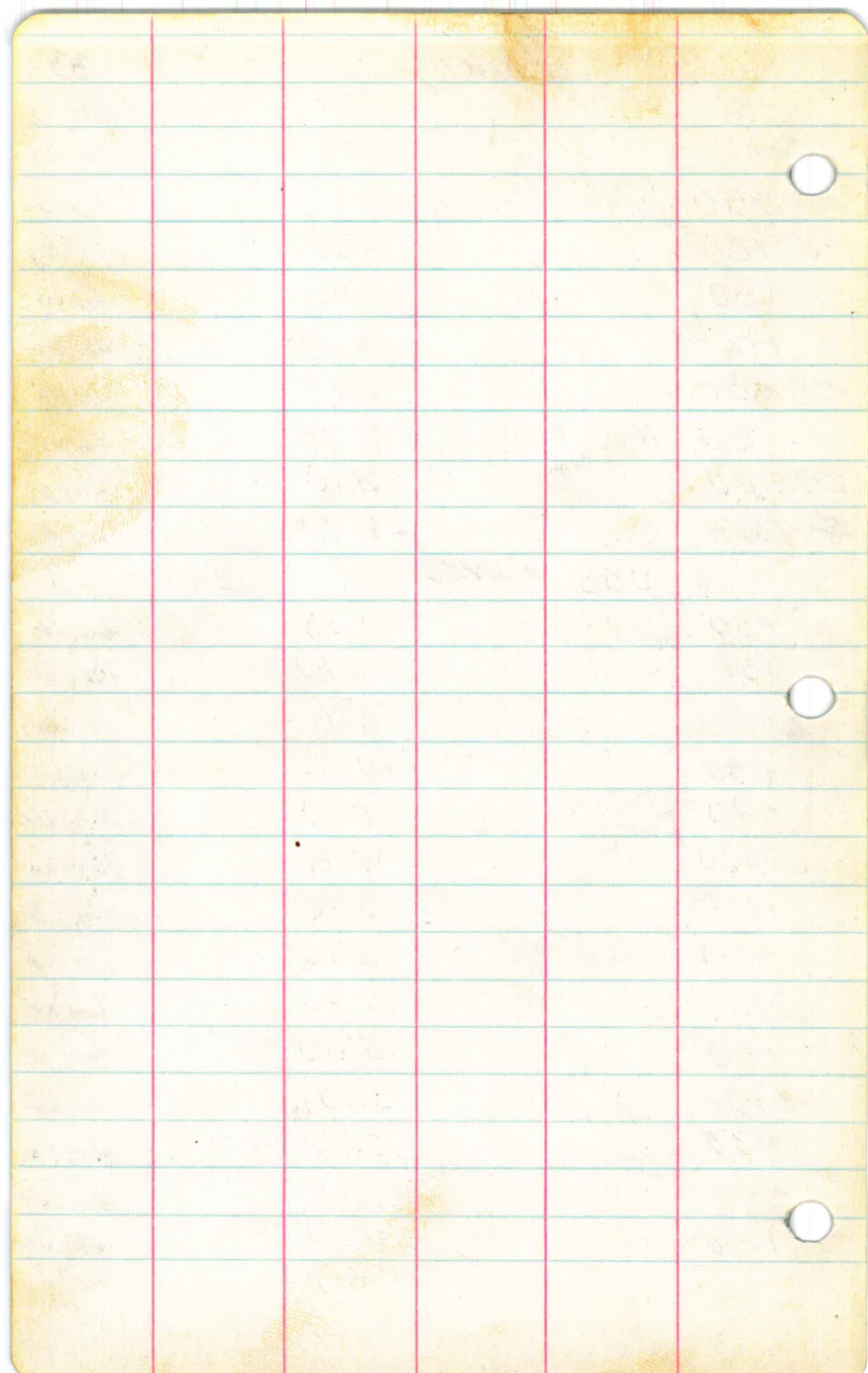
	00 ^(T)		
	5+50	-2.90	397.52
	+50	-1.10	399.32
P		404.67	-0.93
	+5.18		399.49
	46+00	4.40	400.27
	46+40	7.10	397.57
	46+50	6.60	398.07
	47	6.30	398.37
	47+50	5.90	398.77
	48+00	5.90	398.77
	+50	5.80	398.87
	49+00	6.0	398.67
	50+00	5.20	399.47
	50+50	4.80	399.87
	51+00	4.90	399.77
	51+50	4.80	399.87
	52+00	4.90	399.77
	52+60	4.80	399.87
	53+00	5.00	399.67
	53+50	4.50	400.17
	4.40	4.30	400.37
	+50	3.80	400.87
	55+00	3.20	401.47
	+14	5.00	399.67

*Probed
Recessed*

*Fence &
edge of
channel*

SE					
		112			
		113			
		114			
		115			
		116			
		117			
		118			
		119			
		120			
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		136			
		137			
		138			
		139			
		140			

			33
+50		4.90	399.77
56+00		4.80	399.87
+50	N. edge of Main channel	4.80	399.87
57+00		4.80	399.87
+50		3.80	400.87
+92 ⁴⁴		2.70	401.97
58+00		2.70	401.97
50	N. edge of chan.	2.70	401.97
59+00		3.10	401.57
Turn		-2.70	401.97
	10.55	412.52	402.97
+50	INTERPS	10.38	402.14
+58		10.60	401.92
60+00		11.10	401.42
+50		10.50	402.02
+90	by Bank	10.10	402.42
61+00		5.50	402.02
+15 ²²		5.50	402.02
+50	Plotted Perimeter	5.10	402.42
62+00		5.80	406.72
+50		5.60	406.92
63+00	← Bank edge	5.90	406.62
+35	→ Bank edge	5.90	406.62
+70		10.30	402.22
+50		10.10	402.42



		412.52		34
67+00	+6.10	408.64	9.98	402.54
6				9
64+00			5.50	403.14
+50			6.10	402.54
65+00			6.80	401.84
+80			8.0	400.64
+75			5.60	403.04
+50			5.50	
66+00			5.50	403.14
+85			6.80	401.84
+69			6.70	401.94
66+00			7.10	401.54
+50			6.50	402.14
67+00			6.20	402.44
+50			6.30	402.34
68+00			5.30	403.34
+50			4.70	403.94
69+00			4.90	403.74
+50			5.00	403.64
+75			5.70	402.94
70+00			4.30	404.34
+50			5.60	403.04
71+00			5.40	403.24
+50			5.80	402.84
72+00			5.80	402.84

*Plotted
Remains*

$$\begin{array}{r} 13.3 \\ \times 5.7 \\ \hline 8.2 \end{array}$$

$$\begin{array}{r} 411.9 \\ \times 0.6 \\ \hline 5.4 \end{array}$$

$$\begin{array}{r} 13.3 \\ \times 5.7 \\ \hline 2.7 \end{array}$$

$$\begin{array}{r} 411.9 \\ \times 0.6 \\ \hline 0.1 \end{array}$$

$$\begin{array}{r} 916 \\ \times 2.8 \\ \hline 12.5 = 12.5 \end{array}$$

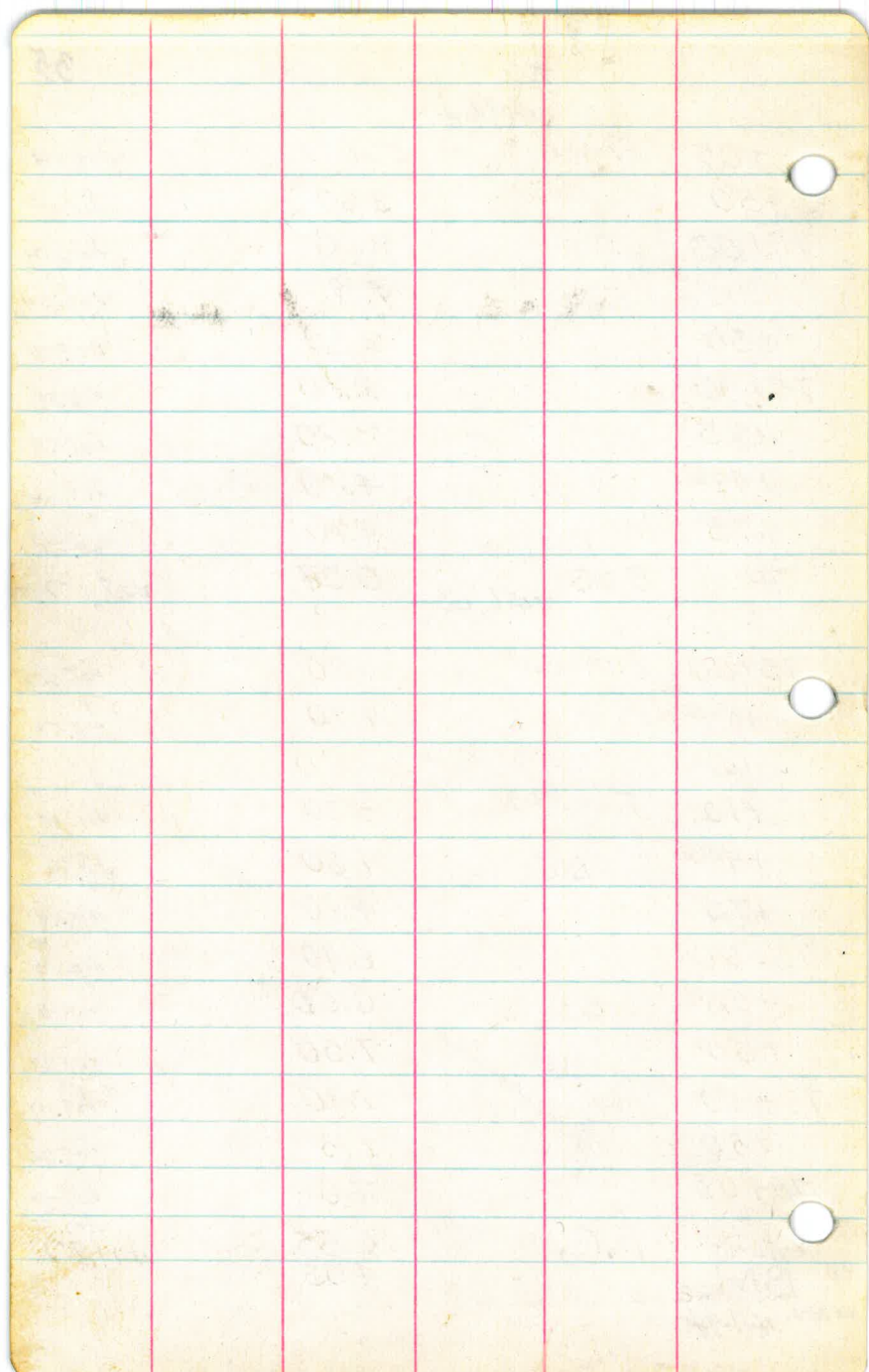
$$\begin{array}{r} 406 \\ \times 1.3 \\ \hline 19.8 \\ \times 12.4 \end{array}$$

$$\begin{array}{r} 412.1 \\ \times 7.4 \end{array}$$

$$419.4 \quad 12.3 + 0.6 = 12.9$$

$$\begin{array}{r} 109.4 \\ \times 0.6 \\ \hline 2.9 \end{array}$$

		↑ 408.64		
○ +05	Fence		5.60	403.04
+50			3.60	405.04
73+00	B		2.10	406.04
			2.40	406.24
+50			3.60	405.04
74+00			2.30	406.34
+25			2.80	405.84
+44 ⁵¹			4.40	404.24
+75			4.70	403.24
FF	8.33	↑416.40	0.57	408.07
○ 75+00	Bottom		11.20	405.20
+074			7.90	408.50
00	Bottom of Bank			
+10	Top of Bank		5.30	411.10
+44 ⁰³	B.C.		4.60	411.80
+75			4.80	411.60
76+00			6.40	410.60
+02 ⁹⁶	EC		6.60	409.80
+50			7.50	408.90
77+00			7.30	409.10
+50			7.15	409.25
78+00			7.0	409.40
○ equas	B.C.		6.55	409.85
CO BM ₂₆			4.53	411.87
alt. 411.94				



~~30.~~

12-30-26
Party Same.

3b

Profile of Pipe Line
Lakeside to San Vicente.

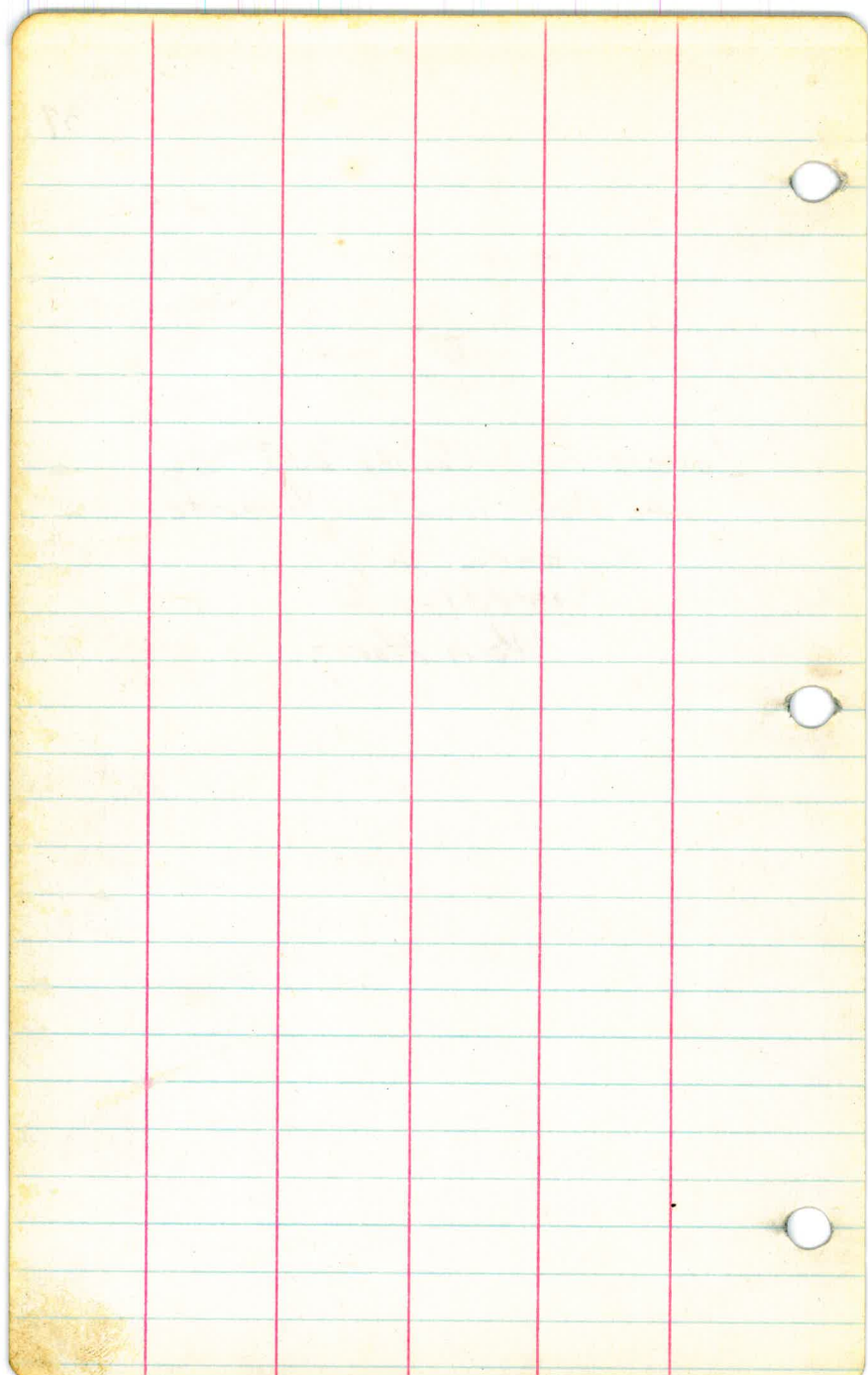
Stadia Ties to Road (Over)

Instrument on 222+34.82 with
bearing of line from there to P.I.
221+14.41 being 0 (Rod 4.9)

Angles X L	Ob. Dist.	V.A.
0° 30'	695	+0° 22'
9° 40'	550	+0° 45'
50° 40'	171	+4° 30'
119° 25'	190	+4° 11'
162° 27'	339	+3° 02'

7105
B

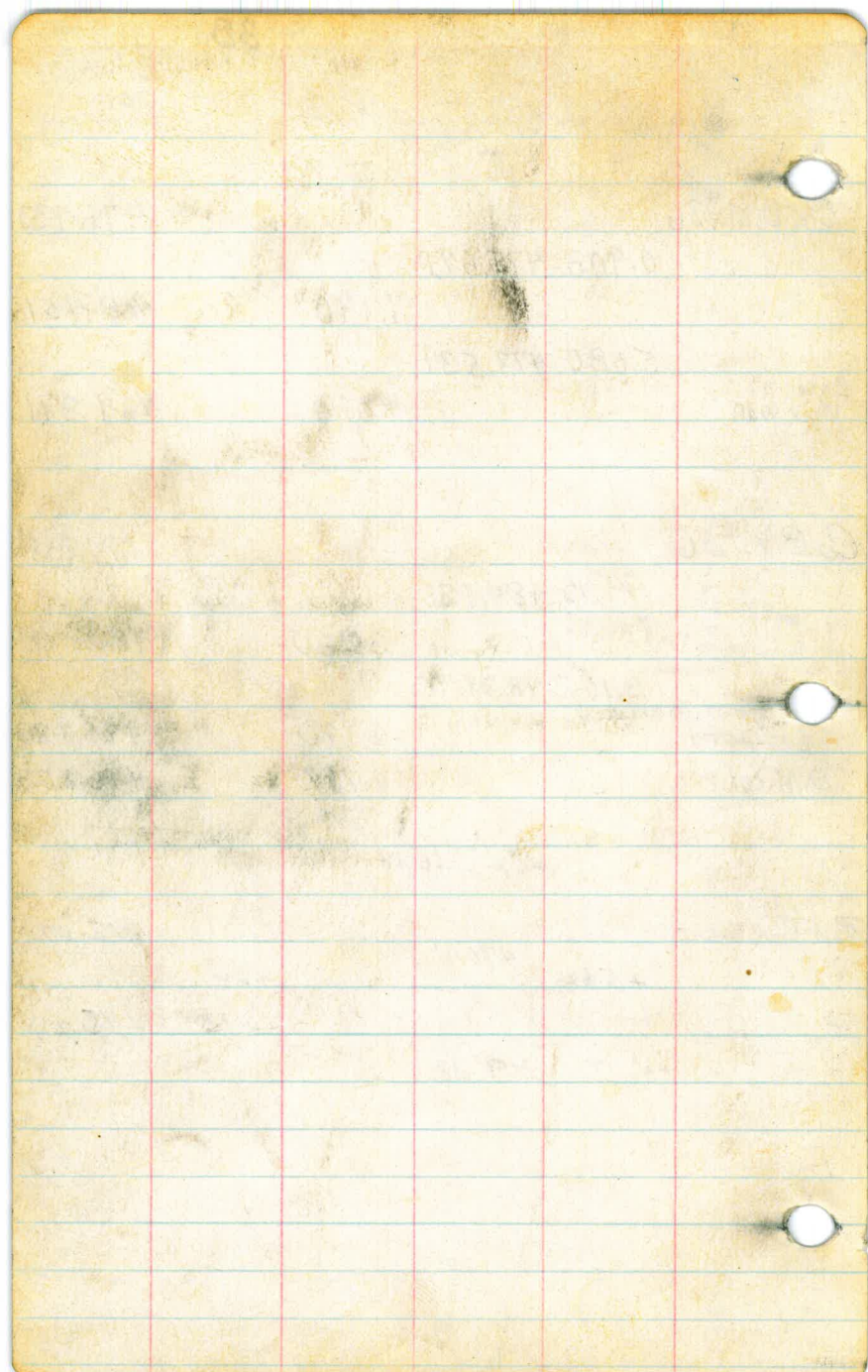
Levels From County B.M. #36
to Weir in San Vicente
Creek Bed.
12/31-26
Van Horn



30 12/31/26
 Drebert
 Soper
 Mackey

Levels on base of Wier

	+	π	-	
Co. B.M. #36				474.733
	0.908	475.641		
			7.190	468.451
	5.080	473.531		
Base of Wier wall			4.660	469.871
Co. B.M. #36				474.733
	9.705	484.438		
			3.960	480.478
	3.192	483.670		
Edge of Road & of Dam			6.790	476.880
B.M. culvert			6.797	476.873
464 Contour				
Red Rock 218230				464.47
	+5.64	470.11 64	464	
IP			-4.82	465.29
	+4.19	369.48 64		



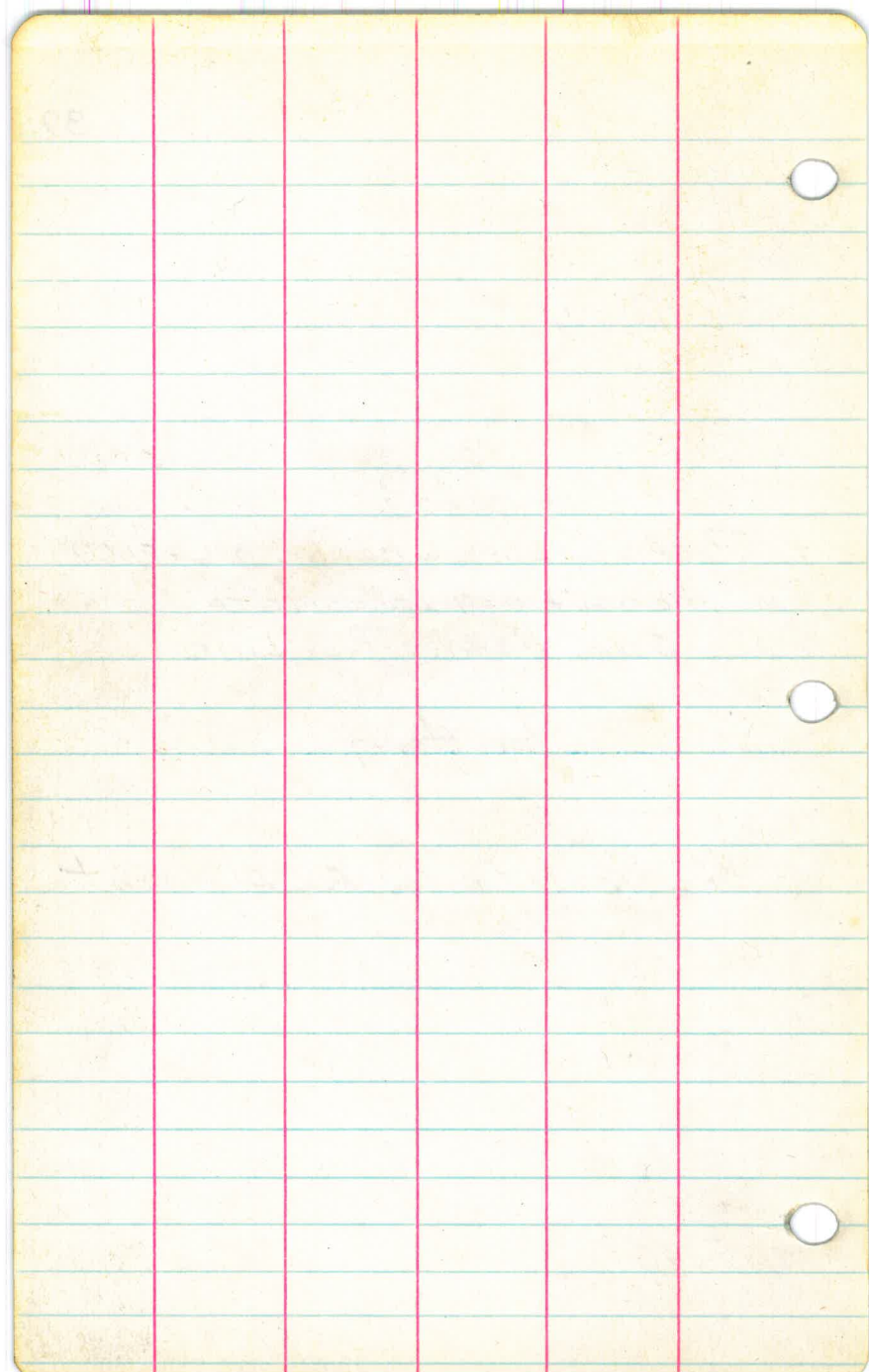
'B'

1-12-77

Profile Line Change 216+81.67
to 216+10.09 Lakeside to
San Vicente Pipe Line

Van Horny 2

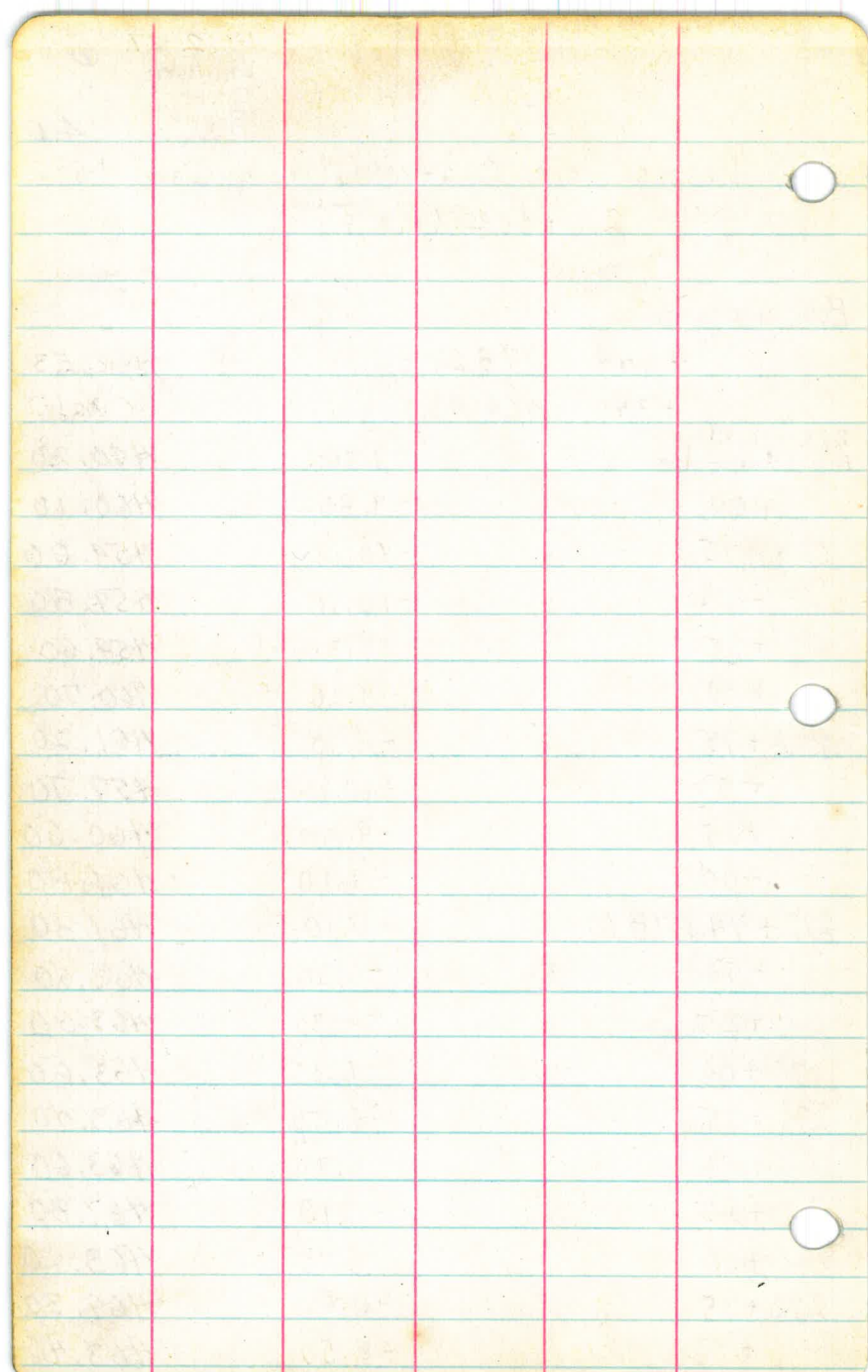
See Transit notes for Alignment +



1-12-27
 Van Horn
 Drebert
 Soper
 Mackey 40

Levels From 225+10.09 (Axis of Dam) to
 216+60.00 (P.O.T.)

B.M. (on culvert)			476.83
+1.44	478.27	-11.74	466.53
+3.40	469.93		466.53
225+10.09 E.C. & Axis of dam		-9.70	460.20
+00		-9.80	460.10
224+75		-10.00	459.90
+50		-10.10	459.80
+25		-10.30	459.60
+00		-9.20	460.70
223+75		-8.70	461.20
+50		-10.20	459.70
+25		-9.30	460.60
+00		-8.10	461.80
222+74.15 (B.C)		-8.10	461.80
+50		-6.30	463.60
+25		-6.30	463.60
+00		-6.30	463.60
221+75		-6.50	463.40
+50		-6.30	463.60
+25		-2.10	467.80
+00		-6.70	463.20
220+75		-0.60	469.30
+50		-6.50	463.40



1-12-27
 Van Horn
 Drebert
 Soper
 Mackey 41

	469.93		
P^{220+38} (on rock)		-3.11	466.82
+222	469.04		
220+25		-6.50	462.54
+00		-10.40	458.60
219+75		-10.90	458.10
+50		-11.00	458.00
+25.20 (B.C. & E.C.)		-7.40	461.60
+00		-6.30	462.70
218+75		-7.30	461.70
+50		-10.20	458.80
$\text{Mac's P}^{(35)}$		-4.57	464.47
+25		-9.70	459.34
+00		-4.10	464.94
$\text{P}^{(218+02.3'L)}$ (on rock)		-0.00	469.04
+3.85	472.89		
217+75		-6.00	466.90
+50		-8.80	464.10
+25		-10.40	462.50
+00		-9.40	463.50
216+81.67 (B.C.)		-7.15	465.74
+60.00 (P.O.T.)		-5.01	467.88
+3.34	471.22		
216+50		-4.30	466.9

		471.22		
216			- 9.10	462.1
+50			-10.7	460.5
215			-10.7	460.5
+50			-10.8	460.4
7			-10.0 7	461.18
	+324	464.02	41	
214			- 5.20	459.2
+50			- 8.10	456.3
213			- 8.10	456.3
+50			8.80	455.6
212			8.90	455.5

'B'

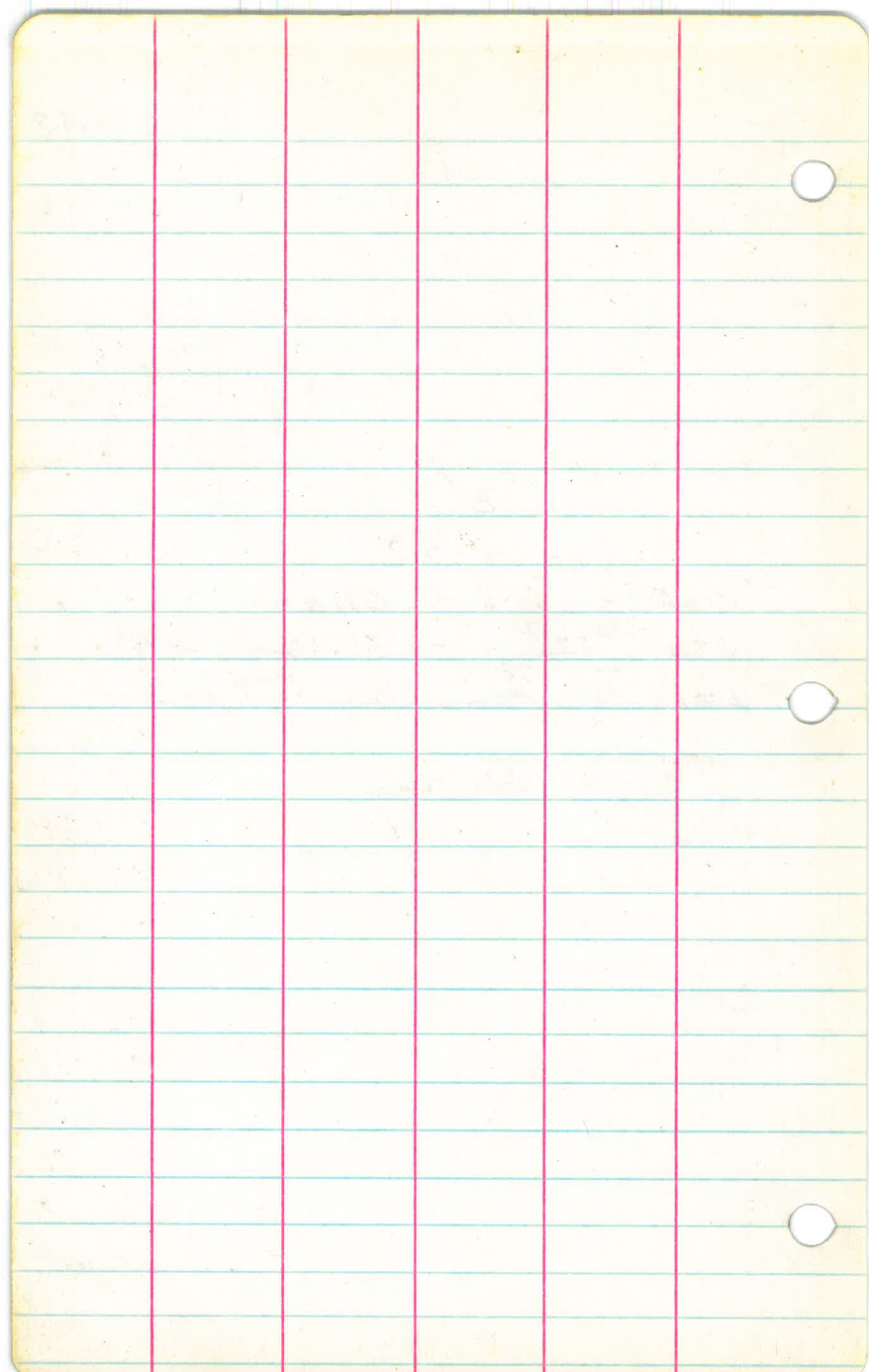
1-12-27

Profile of Line Change

Sta $\frac{78+46.84}{78+09.78}$ to E.C. Sta 83.38

Lake side to San Vicente Pipeline

Van Horn



1-12-27
 Van Horn
 Drebert
 Sopov
 Mackey 43

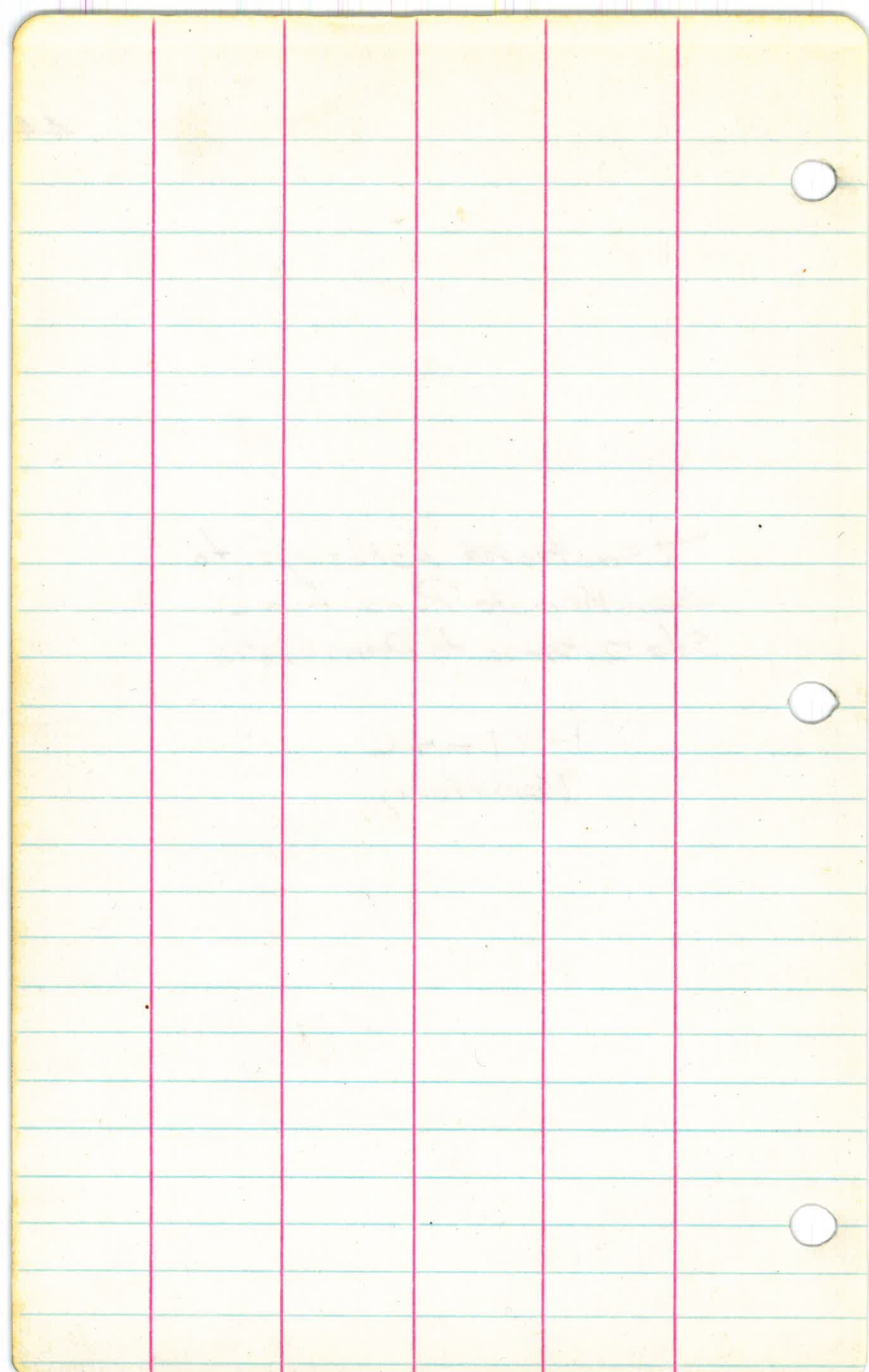
○ Levels connecting McGetchin's and Van Horn's
 C.B.M. #26 Lines. 411.94

	+4.33	416.27	
Eq. B.C. $(\frac{78+46.84}{78+09.78})$		-6.13	410.14
78+25		-6.00	410.30
+50		-5.30	411.00
+75		-6.00	410.30
79+00		-5.90	410.40
+25		-5.80	410.50
+50		-5.70	410.60
+75		-5.50	410.80
○ 80+00		-5.40	410.90
+25		-5.30	411.00
+50		-4.80	411.50
+75		-5.30	411.00
81+00		-5.20	411.10
+25		-5.10	411.20
+50		-5.10	411.20
+75		-4.80	411.50
82+00		-4.80	411.50
+25	Plotted Determined	-4.80	411.50
+50		-4.80	411.50
+75		-4.80	411.50
○ 82+03.38 (E.C.)		-4.73	411.54

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7 sections Lakeside to
San Vicente Pipe Line
Sta 212400 to Dam Axis

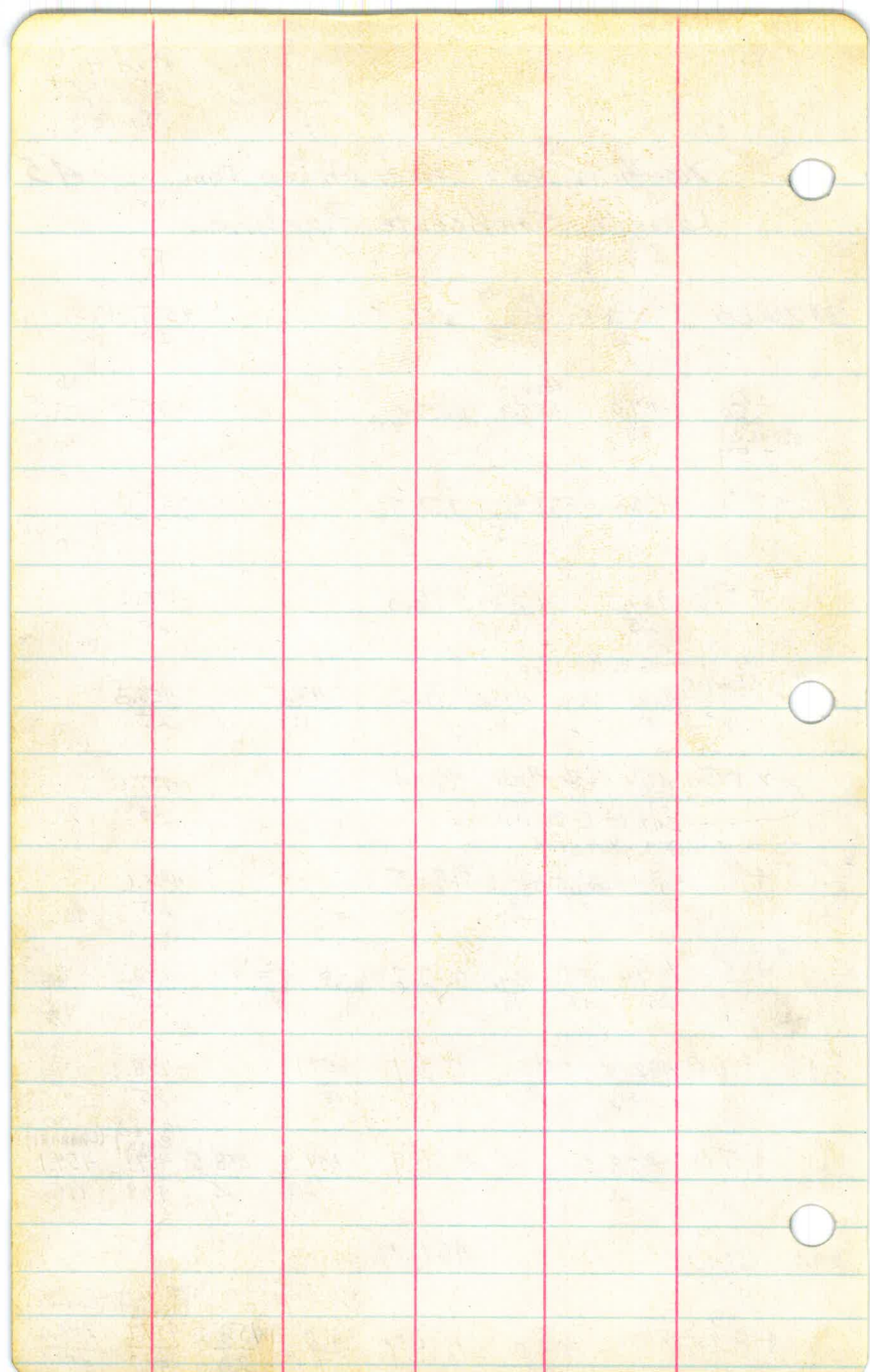
1-17-26
Van Horn



1-17-27
 Van Horn
 Orbert
 Super
 Mackey

1.
 X sections sta 212+00 to Axis of Dam 45
 Lakeside - San Vicente Pipeline

	L.		C.		R.	
212+00	455.4 25	(fence) 455.6 15.5	455.5		455.4 25	} Soil and D.G. Small rock.
+50 (fence) +57	457.0 25	(fence) 457.9 12	457.6		455.3 25	
213+00	458.8 25	457.9 11	456.1 5	456.3	455.6 25	
+50	460.3 25	458.6 10	456.3		456.2 25	
214+00	G.B. Outcrop. 466.9 20	464.0 7	459.8 6	459.2	456.5 11	456.8 25
+50	467.6 25	468.6 20	460.1 6	460.4	457.6 25	
	End of G.B. Outcrop					
215+00	G.B. Outcrop 466.1 20	464.5 14	460.9 8	460.5	458.6 25	
+50	477.4 25	474.0 15	464.1 10	460.5	460.2 8	458.3 13
216+00	482.5 25	470.8 18	462.1	459.1	458.9 25	
+50	479.5 25		466.9	459.1 20	458.5 25	(River Bank) (Channel) 457.1 109 454.1 115
216+60.00	(P.O.T.)		467.9			
+87.67	(B.C.)	476.0 20	465.7	461.0 7	458.2 20	(River Bank) (Channel) 457.7 50 456.0 55



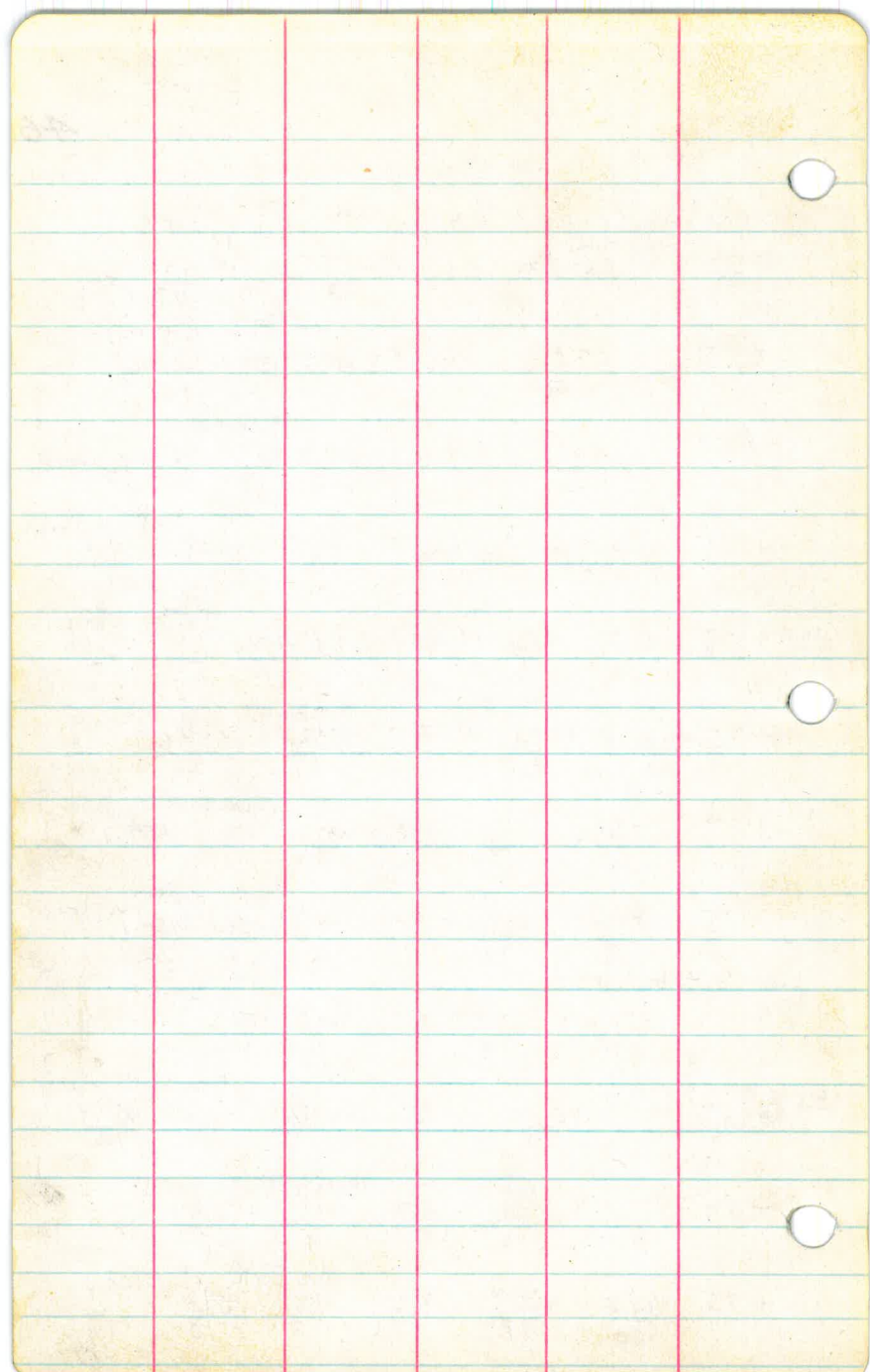
2.

1-17-27
Van Horn
Drebert
Soper
Mackey

46

X Sections Sta 212+00 to Axis of Dam
Lakeside - San Vicente Pipe Line

	L.	C.	R.		
217+00	474.3 20	463.5	458.5 13	457.5 40	455.5 49
+25	472.3 20	462.5	459.3 10	458.3 31	458.9 40
+50	474.1 20	464.1	459.3 10	458.1 27	456.1 33.5
+75	476.8 20	466.9	459.9 17	458.9 27	457.3 33
218+00	475.9 22	468.8 3	464.9 6	462.6 7	459.0 22
+25	470.5 20	465.3 10	464.1 4	459.3 17	457.6 20
+50	470.2 20	459.8 3	458.8	457.2 2	456.1 13
+75	473.3 20	467.2 12	461.7	457.3 6	456.1 19
Loose G.B. begin here					
219+00	473.4 25	467.5 11	462.7	460.3 7	457.3 10
(B.C. & E.C.) +25.20	472.60 20	461.60	457.1 9	456.6 15	454.9 18
+50	469.7 20	468.2 16	458.0	456.6 9	454.7 15
+75	469.6 20	463.3 10	458.1	456.9 6	454.8 10



3.

1-11-21
Van Horn
Drebert
Soper
MacKey

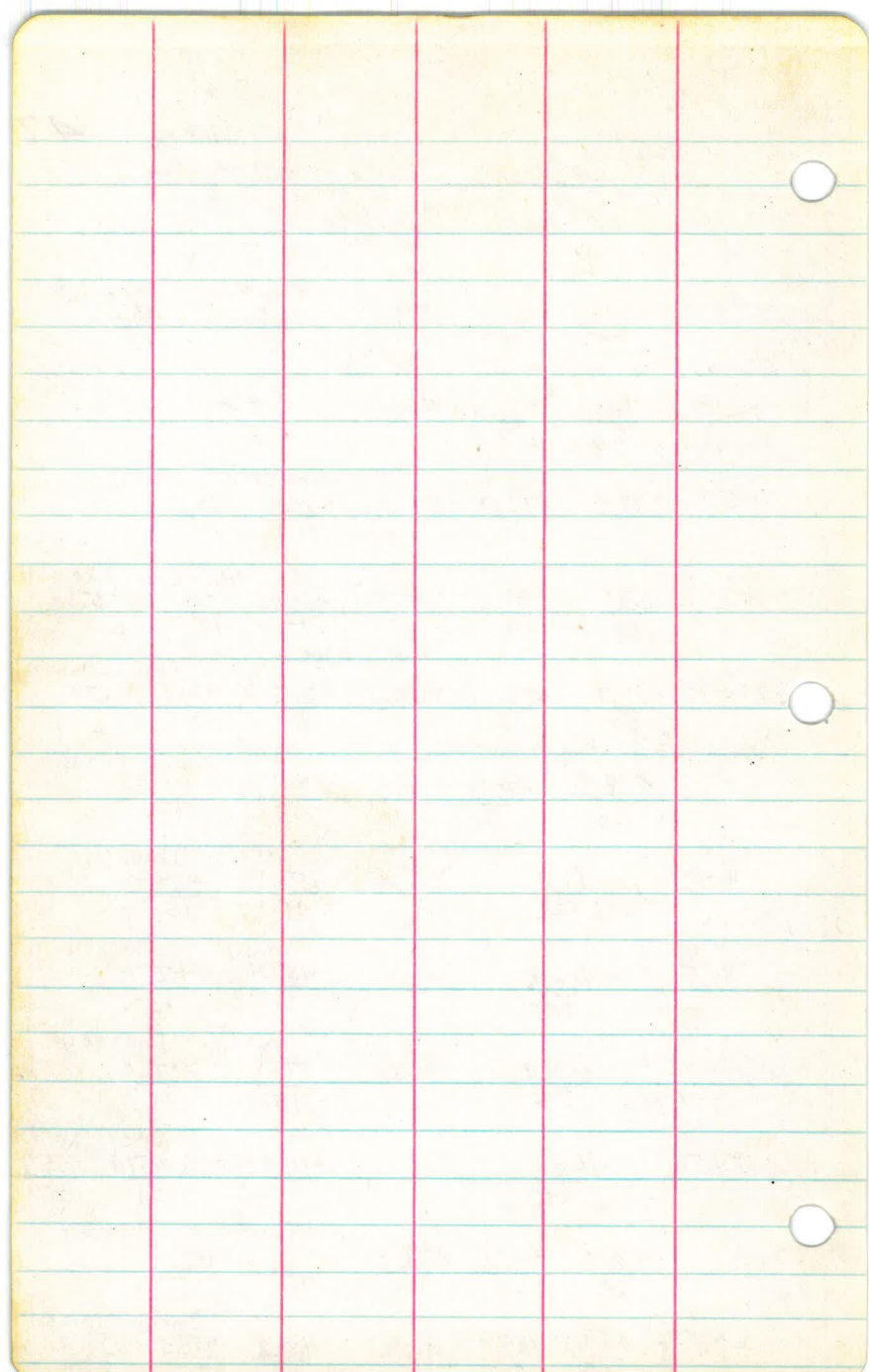
47

X Sections Sta 212+00 to Axis of dam

Lakeside - San Vicente Pipe Line

L C R

220+00	471.6 20	467.6 15	458.6	(River Bank) 456.3 8	(Channel) 455.1 12
	Granite cliff begins here (Solid)				
+25	476.0 20	474.5 18	462.5	(Channel) 455.5 12	
+50	489.9 20	477.9 16	463.4	(River Bank) 458.0 11	(Channel) 455.2 14
+75	488.3 20	481.3 14	469.3	460.0 5	(River Bank) (Channel) 456.0 15 455.3 18
	Granite ledge				
221+00	482.7 20	475.20 16	463.20	460.7 4	(Bank) (Channel) 460.7 10 455.9 16
	Loose G.B. begin here				
+25	478.8 20	470.3 6	467.8	(Bank) 457.0 13	(Channel) 455.8 16
+50	471.1 20		463.6	(Bank) 457.1 11	(Channel) 455.6 15
+75	468.6 25		463.4	(Bank) 457.4 11	(Channel) 455.7 15
222+00	468.9 25		463.6	(Bank) 457.6 15	(Channel) 456.0 18
+25	468.1 25		463.6	460.4 8	(Bank) (Channel) 459.9 14 457.4 21 455.7 27
+50	468.3 25	465.6 20	463.6	(Bank) 457.6 22	(Channel) 455.5 26
+74.15	(B.C.) 469.0 25	464.8 16	461.8	460.2 15	(Bank) (Channel) 458.5 22 456.3 26



4.

1-17-27
Van Horn
Drebert
Soper
Mackey

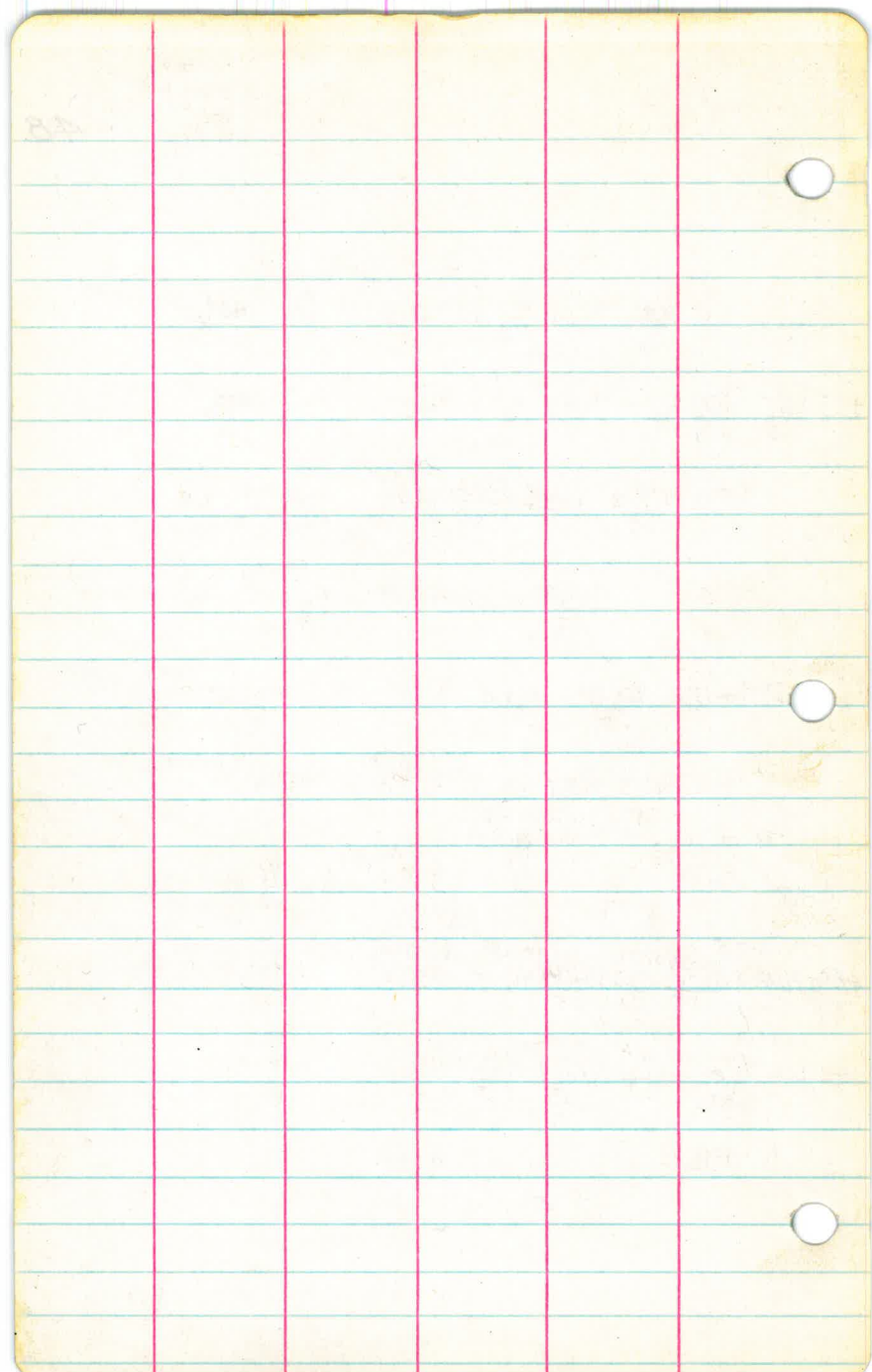
48

	L.	C Rock ledge	R
223 + 00	469.2 25	464.1 14	462.2 4
		461.8	459.1 18 (Channel)
+25	461.7 25	466.5 18	464.5 17
		464.5 12	461.9 8
		460.6	458.6 13 (Channel)
+50	468.2 25	462.3 7	460.5 5 (Pocket)
		459.7	459.9 15 (Channel)
+75		465.9 25	461.2
			461.1 9 (Bank)
			460.0 11 (Channel)
224 + 00	464.4 25	463.5 20	460.7
			459.5 20 (Channel)
+25	466.3 25	465.7 22	463.3 20 (Bank)
			459.6 15 (Channel)
			459.4 15 (Channel)
Top of dump	475.1 27	460.3 9	459.8 12 (Bank)
			460.0 12 (Channel)
+75		Granite ledge (bank)	459.9 11 (Channel)
474.2 34	468.2 31	468.1 24	463.4 20
		463.4 15	460.5 13
			459.9 11
+00	472.1 30	471.1 22	471.1 15
			460.3 5
			460.1 11
+1099			460.2

Toe of slope to dump

Granite ledge

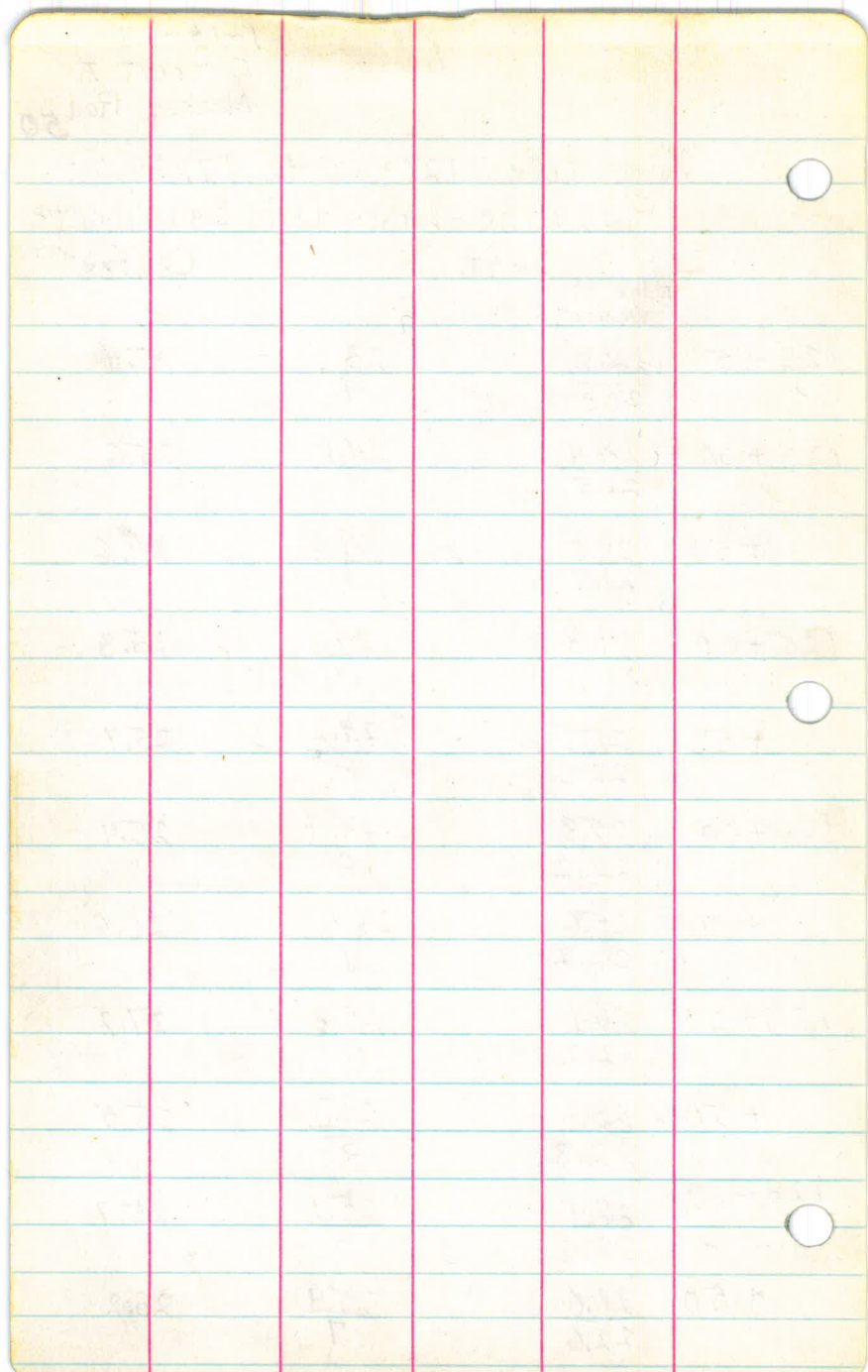
Large Granite Boulder



1-18-27
 Drebert &
 Mackey Rod 50

X sections 123+50 to 171+00
 Pipe Line - Lakeside to San Vicente
 Left. Center

	Edge of Pavement		
123+50	$\frac{424.2}{21.5 \text{ Edge of Pav}}$	$\frac{23.6}{9}$	25.4
124+00	$\frac{24.4}{21.5}$	$\frac{24.1}{11}$	25.6
+50	$\frac{24.5}{21.7}$	$\frac{24.2}{11}$	24.6
125+00	$\frac{24.8}{21.7}$	$\frac{24.1}{10}$	25.3
+50	$\frac{25.1}{22.0}$	$\frac{24.2}{8}$	25.9
126+00	$\frac{25.3}{22.2}$	$\frac{24.4}{8}$	25.9
+50	$\frac{25.6}{22.2}$	$\frac{24.6}{9}$	26.6
127+00	$\frac{26.1}{22.2}$	$\frac{25.8}{11}$	27.2
+50	$\frac{26.1}{22.3}$	$\frac{25.1}{5}$	25.5
128+00	$\frac{26.4}{22.6}$	$\frac{25.1}{8}$	25.7
+50	$\frac{26.6}{22.6}$	$\frac{25.9}{7}$	26.2



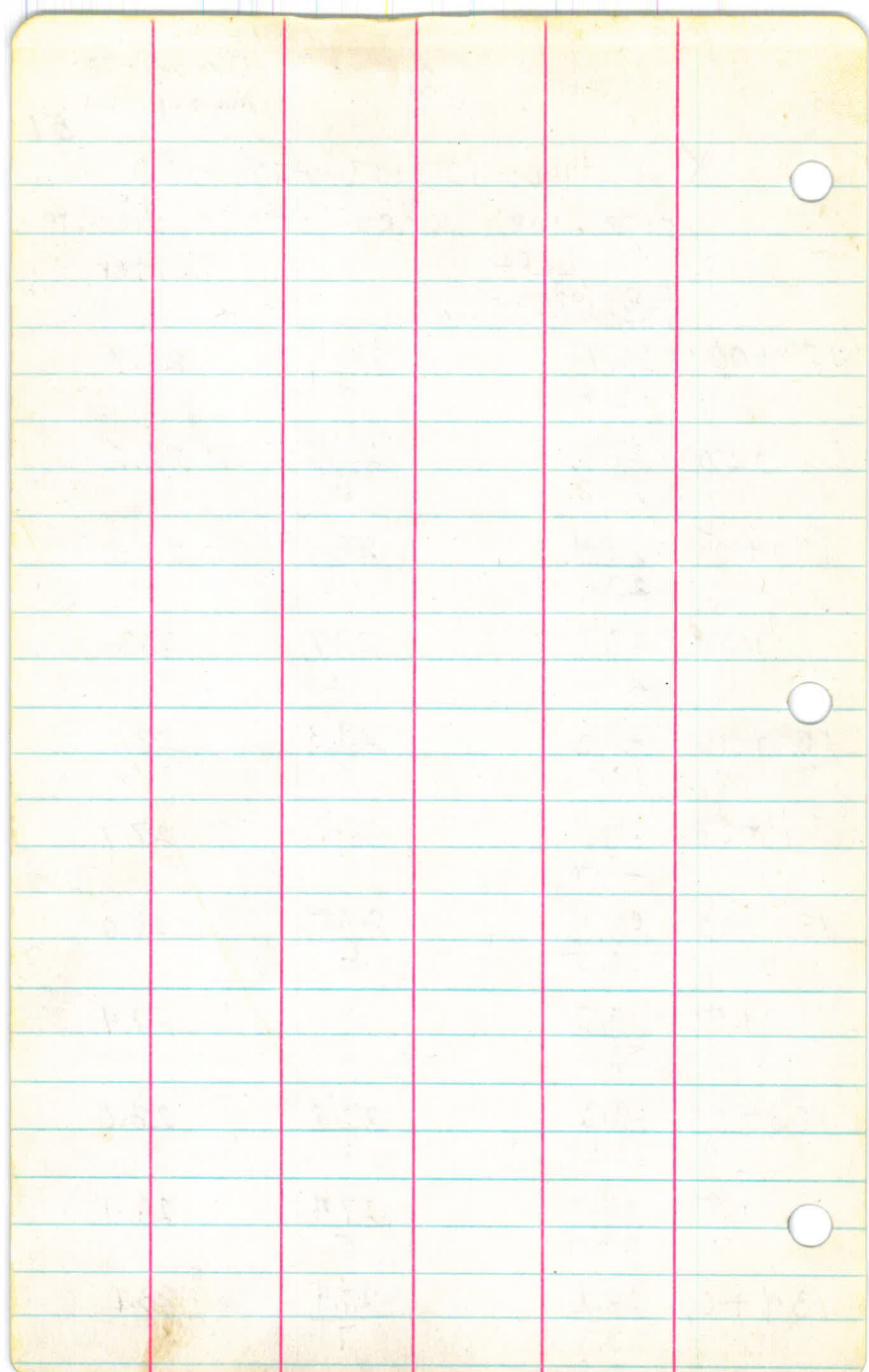
2.

1-18-21
Drebert &
Mackey Rod

51

○ X Sections 123+50 + 171+00
Pipe Line - Lakeside to San Vicente
Left Center

	Edge of Pavement		
129+00	$\frac{26.9}{22.8}$	$\frac{26.1}{8}$	26.7
+50	$\frac{27.2}{23.0}$	$\frac{26.3}{8}$	26.6
130+00	$\frac{27.4}{23.1}$	$\frac{28.0}{12}$	26.5
+50	$\frac{27.7}{23.2}$	$\frac{27.9}{12}$	27.3
○ 131+00	$\frac{27.8}{23.2}$	$\frac{28.3}{7}$	27.6
+50	$\frac{28.1}{23.4}$	$\frac{26.7}{5}$	27.7
132+00	$\frac{28.4}{23.5}$	$\frac{27.5}{8}$	26.0
+50	$\frac{28.3}{23.6}$		27.4
133+00	$\frac{28.3}{23.5}$	$\frac{27.5}{8}$	28.0
○ +50	$\frac{28.3}{23.4}$	$\frac{27.4}{5}$	28.4
134+00	$\frac{28.2}{23.3}$	$\frac{27.4}{7}$	28.1

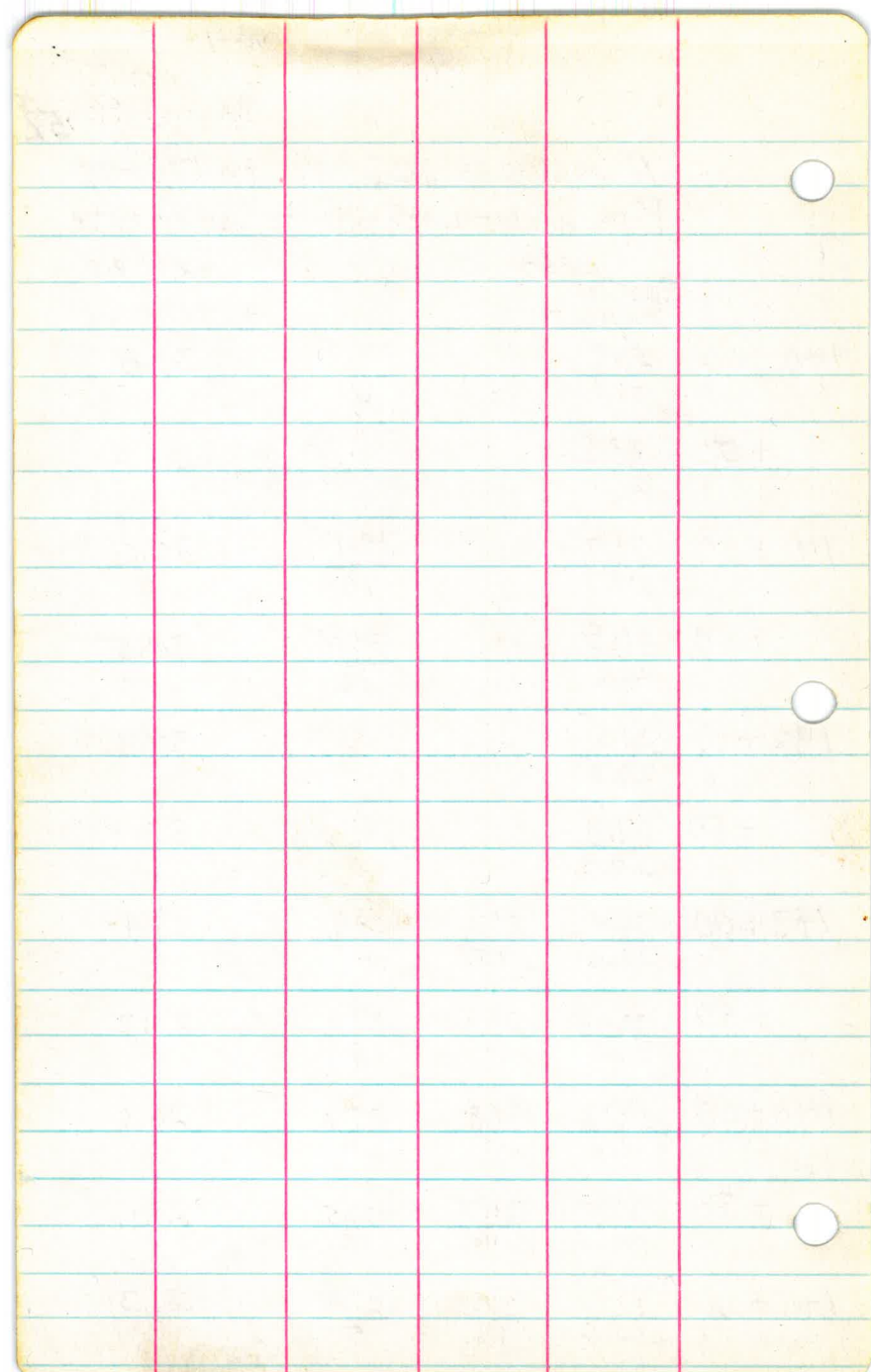


4.


1-18-27
Drebert π
Mackey Rod 52⁺

X Sections 123+50 to 171+00
Pipe Line - Lakeside to San Vicente

	Edge of Pavement	Left		Center
140+00	$\frac{31.3}{21.1}$		$\frac{30.1}{7}$	30.8
+50	$\frac{31.6}{21.0}$			30.2
141+00	$\frac{31.7}{20.7}$		$\frac{30.1}{10}$	30.6
+50	$\frac{31.8}{20.5}$		$\frac{30.4}{10}$	30.5
142+00	$\frac{31.8}{20.3}$			30.9
+50	$\frac{31.9}{20.0}$			32.1
143+00	$\frac{31.9}{20.2}$	$\frac{31.7}{15}$	$\frac{28.9}{6}$	28.9
+50	$\frac{32.0}{20.0}$	$\frac{31.5}{14}$	$\frac{27.0}{6}$	27.2
144+00	$\frac{32.3}{19.8}$	$\frac{31.8}{15}$	$\frac{27.2}{6}$	26.6
+50	$\frac{32.5}{20.0}$	$\frac{31.7}{14}$	$\frac{27.5}{6}$	27.1
145+00	$\frac{32.7}{20.0}$	$\frac{32.2}{14}$	$\frac{27.9}{5}$	27.3



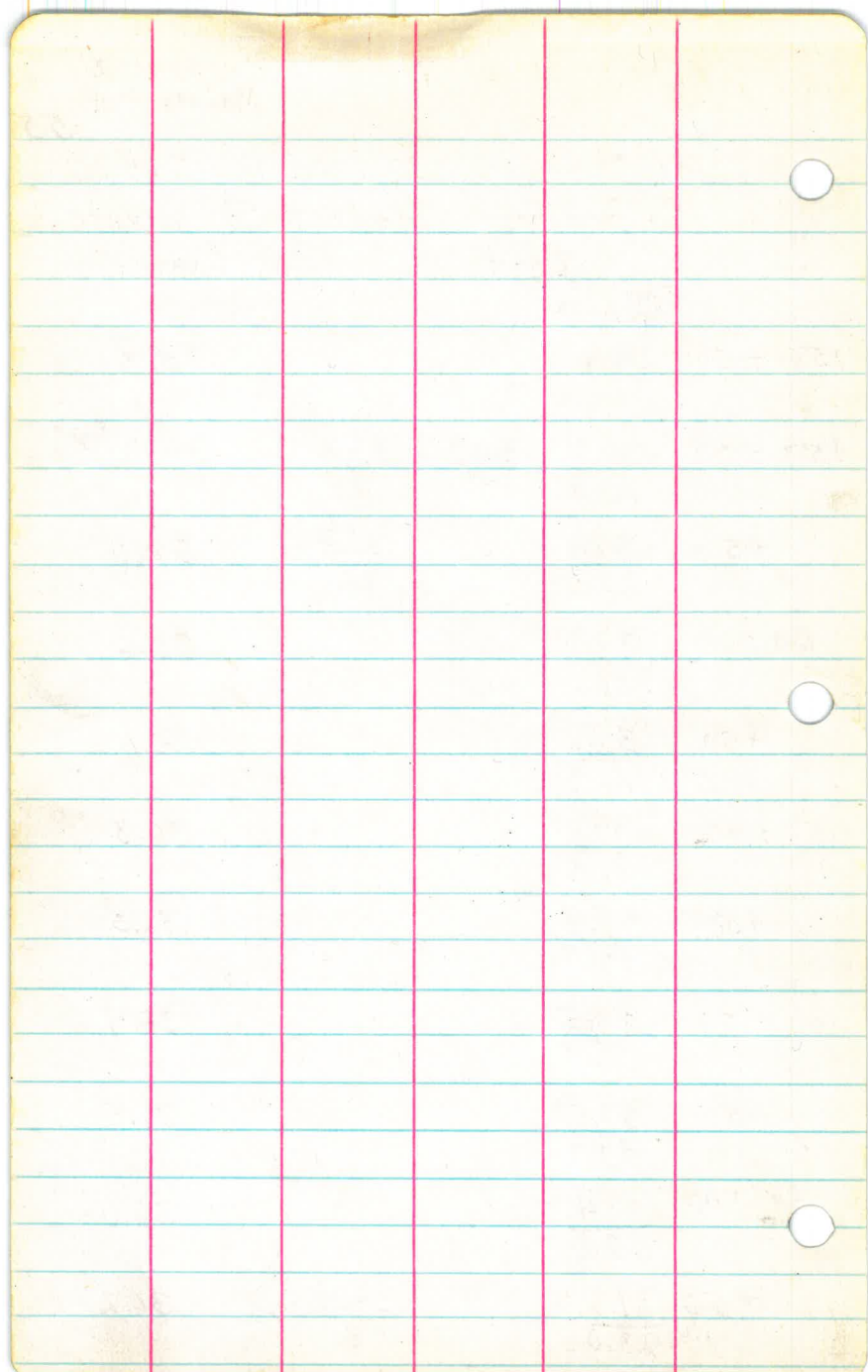
7.

1-18-27
Drebert & Mackey Rod 
55

X Sections 123+50 to 171+00
Pipe Line - Lakeside to San Vicente
Left Center

Edge of Pavement

156+50	$\frac{36.9}{22.1}$			35.3
157+00	$\frac{36.9}{22.1}$	$\frac{368}{17}$	$\frac{33.3}{6}$	34.3 ^{Rock File}
+50	$\frac{37.0}{22.2}$		$\frac{35.8}{16}$	36.0
158+00	$\frac{37.0}{22.2}$			36.6
+50	$\frac{37.2}{22.5}$			36.1
159+00	$\frac{37.5}{22.5}$			36.3
+50	$\frac{37.4}{22.5}$			36.3
160+00	$\frac{37.5}{22.8}$			36.4
+50	$\frac{37.5}{22.7}$			36.5
161+00	$\frac{37.4}{22.8}$			36.0
+50	$\frac{37.5}{23.0}$		$\frac{37.4}{6}$	36.2



8.

1-18-27
Drebert π
Mackey Rod 56

○ X Sections 123+50 to 171+00
Pipeline - Lakeside to San Vicente
Left Center

Edge of
Pavement

162+00 $\frac{37.5}{23.0}$ 39.9

+50 $\frac{37.6}{23.1}$ 36.7

163+00 $\frac{38.0}{23.2}$ 36.8

+50 $\frac{38.1}{23.3}$ 37.1

○ 164+00 $\frac{38.5}{23.4}$ 37.4

+50 $\frac{38.6}{23.4}$ 37.5

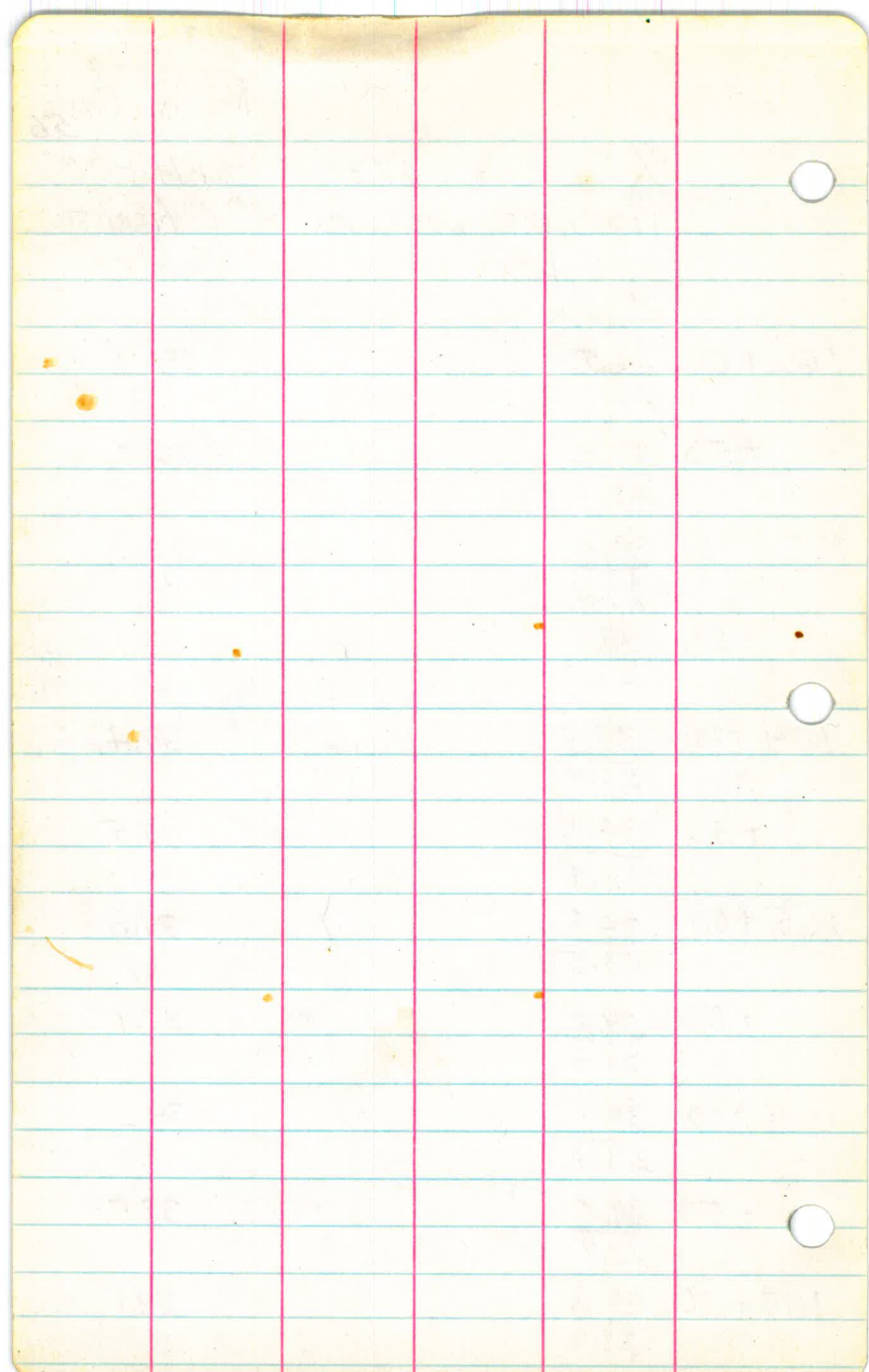
165+00 $\frac{38.8}{23.5}$ 37.8

+50 $\frac{39.2}{23.8}$ 37.9

166+00 $\frac{39.4}{23.9}$ 38.2

○ +50 $\frac{39.6}{23.9}$ 38.5

167+00 $\frac{39.8}{23.9}$ 39.1



9,

1-18-27
Drebert &
Mackey Rod 57

X Sections 123+50 to 171+00
 Pipe Line - Lakeside to San Vicente
 Edge of Left Pavement Center

167+50	$\frac{40.0}{24.0}$		39.1
--------	---------------------	--	------

168+00	$\frac{40.2}{24.0}$		39.7
--------	---------------------	--	------

+50	$\frac{40.5}{24.0}$		39.8
-----	---------------------	--	------

169+00	$\frac{40.7}{24.2}$		40.4
--------	---------------------	--	------

+50	$\frac{40.7}{24.4}$		40.9
-----	---------------------	--	------

170+00	$\frac{41.0}{24.3}$		41.3
--------	---------------------	--	------

+50	$\frac{41.5}{24.3}$		41.6
-----	---------------------	--	------

171+00	$\frac{41.5}{24.5}$	$\frac{42.2}{4}$	41.3
--------	---------------------	------------------	------

58

Jan. 10, 1927.

N. Glover - M

S. Bichet - P

R. Bush - top

H. Butzine Ave.

Woodside Ave. and Vine St.

Cross Sections.

2

Sta.	+	H.I.	-	Elev.
BM #1				408.87

	1.38	410.25		
--	------	--------	--	--

1+00

1+50

1+84

2+00

2+50

2+59

2+75

2+84

$\frac{10.2}{25}$	fence $\frac{19}{19}$	8.9	edge of pavement $\frac{7.95}{12}$
-------------------	--------------------------	-----	---------------------------------------

$\frac{8.6}{25}$	fence $\frac{20}{20}$	8.3	$\frac{7.00}{12}$
------------------	--------------------------	-----	-------------------

beginning of row of pepper trees
 $\frac{10}{10}$

$\frac{5.5}{25}$	fence $\frac{19}{19}$	7.4	$\frac{6.37}{12}$
------------------	--------------------------	-----	-------------------

$\frac{2.5}{25}$	$\frac{19}{19}$	$\frac{3.6}{8}$	5.1	$\frac{4.71}{12}$
------------------	-----------------	-----------------	-----	-------------------

line of pepper trees
 $\frac{10}{10}$

fence ends here, property line on W. side Fliver St.
power pole guy post
 $\frac{19}{19}$

power pole
 $\frac{21}{21}$

3)	Sta.	+	H.I.	-	Elev.
			410.25		
	3+00				
	3+30				
	3+50				
	3+62				
	BM ^{#1}			1.38	408.87
		7.92	416.79		
	4+00				
	4+50				
	5+00				
	5+50				
	5+95				

$\frac{17}{25}$

3.4

 $\frac{293}{12}$ fire hydrant
 $\frac{20}{20}$ E. property
fence starts here
line of River St. $\frac{20}{25}$

79

1.4

 $\frac{1.46}{12}$

power pole guy post.

Auto Club sign post.

 $\frac{6}{6}$ $\frac{2}{2}$

pepper trees

 $\frac{49}{25}$ $\frac{76}{76}$

6.5

 $\frac{6.45}{11.5}$ $\frac{3.5}{25}$

5.1

 $\frac{4.93}{11}$ $\frac{3.0}{25}$ $\frac{24}{14}$

3.8

 $\frac{3.61}{11}$ $\frac{21}{25}$ $\frac{18}{17}$

3.1

 $\frac{2.81}{9.5}$ line of
 $\frac{76}{76}$ pepper trees

4

Sta	+	HI	-	Elev
-----	---	----	---	------

6+00		416.79		
------	--	--------	--	--

T.P.			1.36	415.43
------	--	--	------	--------

	386	419.29		
--	-----	--------	--	--

6+50

6+89

6+98 Concrete fence on north side of \mathcal{L} running
north on E side of Maine Ave.

7+00

7+13 West end of Lakeside Development Co. office.

7+30 East end " " " "

7+50

8+00

$$\frac{21}{25}$$

$$\frac{1.6}{12}$$

2.6

$$\frac{2.43}{2}$$

edge of pavement on curve.

$$\frac{5.27}{45}$$

$$\frac{3.51}{8}$$

3.9

$$\frac{4.0}{25}$$

fire hydrant
18concrete fence.
2

$$\frac{4.5}{25}$$

$$\frac{12}{12}$$

line of pepper trees.

4.5

$$\frac{4.5}{25}$$

$$\frac{N.W. Cor.}{22}$$

$$\frac{S.W. Cor.}{32}$$

$$\frac{N.E. Cor.}{22}$$

$$\frac{S.E. Cor.}{32}$$

$$\frac{35}{25}$$

50

$$\frac{48}{25}$$

$$\frac{38}{25}$$

54

$$\frac{52}{25}$$

51

Sta.	+	H.I.	-	Elev.
8+50		419.29		

8+91 ²⁰	BC.	on Woodside Ave.		
--------------------	-----	------------------	--	--

9+08	End of line of pepper trees.			
------	------------------------------	--	--	--

T.P.			9.11	410.18
	4.78	414.96		

9+25	Point on curve.			
------	-----------------	--	--	--

9+50				
------	--	--	--	--

9+61 ⁹⁶	E.C.	on Vine St.		
--------------------	------	-------------	--	--

10+00				
-------	--	--	--	--

10+37	Line of pepper trees start here.			
-------	----------------------------------	--	--	--

62

Left

Right

$$\frac{6.0}{25}$$

5.6

$$\frac{5.8}{25}$$

$$\frac{6.4}{25}$$

6.3

$$\frac{7.0}{25}$$

end of line of pepper trees
 $\frac{12}{12}$

$$\frac{2.2}{25}$$

$$\frac{2.4}{15}$$

4.6

$$\frac{5.6}{25}$$

$$\frac{4.4}{25}$$

5.2

$$\frac{6.3}{25}$$

$$\frac{4.0}{25}$$

5.5

$$\frac{6.9}{25}$$

$$\frac{4.6}{25}$$

5.9

$$\frac{6.7}{18}$$

$$\frac{4.4}{22}$$

$$\frac{4.2}{25}$$

pepper tree.
 $\frac{12}{12}$

6)

Sta	+	H.I.	-	Elev
10+50		414.96		
10+60		Fence starts here going north on Virze St.		
11+00				
11+50		End of fence that started at 10+60		
12+00				
12+50				
T.P.				
13+00				
13+25		End of line of pepper Trees		
T.P.			8.62	406.34
	2.08	408.42		
13+50				

L.

R

fence of tennis court. 63

$$\frac{5.2}{25}$$

4.9

$$\frac{3.1}{3}$$

76

$$\frac{4.6}{25}$$

fence.
 $\frac{3}{3}$

$$\frac{5.0}{25}$$

$$\frac{4.7}{3}$$

3.4

$$\frac{4.7}{25}$$

end of fence

pepper trees

$$\frac{4.4}{25}$$

$$\frac{4.5}{4}$$

4.0

$$\frac{3}{3}$$

11

$$\frac{4.7}{25}$$

$$\frac{4.3}{25}$$

4.2

$$\frac{4.7}{25}$$

$$\frac{5.6}{25}$$

5.2

$$\frac{5.1}{25}$$

$$\frac{6.5}{25}$$

6.7

$$\frac{6.5}{25}$$

pepper tree
 $\frac{10}{10}$

$$\frac{1.9}{25}$$

2.3

$$\frac{2.6}{25}$$

7)					
Sta	+	H.I.	-	Elev	
14+00		408.42			
14+50					
15+00					
15+39	12" crockery culvert				
15+50					
16+00					
16+50					
17+00					
17+50					

$$\frac{3.4}{2.5}$$

3.3

$$\frac{4.5}{12}$$

$$\frac{5.1}{2.5}$$

$$\frac{3.5}{2.5}$$

4.4

$$\frac{6.8}{7}$$

$$\frac{7.5}{2.5}$$

$$\frac{4.9}{2.5}$$

$$\frac{4.6}{3}$$

6.2

$$\frac{6.8}{3}$$

$$\frac{9.6}{12}$$

$$\frac{10.3}{2.5}$$

$$\frac{10.4}{2.5}$$

bottom of culvert.
91 East end.bottom of culvert
West end.
$$\frac{8.4}{2.4}$$

$$\frac{6.4}{2.5}$$

$$\frac{5.7}{4}$$

6.6

$$\frac{10.5}{12}$$

$$\frac{11.3}{2.5}$$

$$\frac{6.0}{2.5}$$

$$\frac{5.4}{6}$$

6.5

$$\frac{8.2}{7}$$

$$\frac{10.5}{16}$$

$$\frac{9.7}{2.5}$$

$$\frac{5.8}{2.5}$$

$$\frac{5.2}{6}$$

6.8

$$\frac{7.6}{5}$$

$$\frac{10.2}{2.5}$$

$$\frac{5.4}{2.6}$$

$$\frac{5.4}{5}$$

6.9

$$\frac{7.6}{8}$$

$$\frac{10.0}{2.5}$$

$$\frac{5.3}{2.5}$$

$$\frac{5.4}{5}$$

6.4

$$\frac{7.8}{14}$$

$$\frac{10.1}{2.5}$$

Sta.	+	H.I.	-	Elev.
		408.42		
17+62	Pepper tree			
17+85	Pepper tree			
18+00				
18+00				
18+75				
19+00				
19+33				
19+50				
20+00	Fence starts here on E. side of Q			
T.P.		8.50		399.92

70

70

$\frac{5.2}{25}$

$\frac{4.9}{12}$

5.5

$\frac{7.3}{18}$

$\frac{9.0}{25}$

$\frac{4.0}{25}$

4.9

$\frac{5.7}{25}$

$\frac{6.1}{25}$

7.3

$\frac{9.2}{25}$

$\frac{7.0}{25}$

$\frac{7.3}{13}$

$\frac{6.1}{11}$

6.2

$\frac{8.7}{25}$

$\frac{7.0}{25}$

$\frac{7.3}{12}$

9.2

$\frac{9.4}{8}$

$\frac{6.2}{17}$

$\frac{6.1}{23}$

$\frac{7.2}{25}$

$\frac{7.4}{5}$

8.1

$\frac{10.2}{11}$

$\frac{7.5}{25}$

$\frac{9.7}{25}$

$\frac{8.5}{19}$

$\frac{8.2}{5}$

9.0

$\frac{12.0}{11}$

$\frac{7.4}{18}$

$\frac{10.0}{25}$

fence starts here

9)

Sta.	+	H. I.	-	Elev
T.P.				399.92
	4.44	404.36		
BM #3			5.56	398.80
	5.56	404.36		398.805
20+50				
21+00				
21+50				
22+00				
22+50				
23+00				
23+50				
23+62				
24+00				

Center of P. ...

$$\frac{6.0}{25} \quad \frac{4.8}{21} \quad \frac{4.3}{4} \quad 4.9 \quad \frac{8.2}{11} \quad \frac{5.8}{18} \quad \frac{5.8}{25}$$

$$\frac{5.7}{25} \quad \frac{4.7}{22} \quad \frac{4.5}{3} \quad 4.9 \quad \frac{5.6}{4} \quad \frac{7.4}{10} \quad \frac{5.1}{18} \quad \frac{5.1}{25}$$

fence ↑

$$\frac{5.6}{25} \quad \frac{4.5}{17} \quad \frac{4.6}{3} \quad 5.0 \quad \frac{6.7}{7} \quad \frac{4.9}{17} \quad \frac{5.2}{25}$$

fence ↑

$$\frac{5.5}{25} \quad \frac{4.6}{17} \quad \frac{4.5}{3} \quad 5.1 \quad \frac{6.3}{7} \quad \frac{4.6}{18} \quad \frac{5.0}{25}$$

$$\frac{5.3}{25} \quad \frac{4.5}{17} \quad \frac{4.4}{4} \quad 5.0 \quad \frac{6.8}{7} \quad \frac{4.2}{18} \quad \frac{4.7}{25}$$

$$\frac{5.3}{25} \quad \frac{4.5}{17} \quad \frac{4.6}{4} \quad 5.2 \quad \frac{6.1}{7} \quad \frac{4.2}{18} \quad \frac{4.6}{25}$$

$$\frac{4.8}{25} \quad \frac{4.2}{13} \quad 5.2 \quad \frac{5.2}{7} \quad \frac{4.1}{18} \quad \frac{4.6}{25}$$

$$\frac{4.3}{25}$$

4.1

tel. pole
15

$$\frac{4.2}{25}$$

10

Sta.	+	H.I.	-	Elev.
24+50		404.36		
T.P.			4.15	400.21
	5.25	405.46		
25+00				
25+50				
25+73	S.W. Cor. of corrugated iron shed.			
25+95	N.W. Cor. of corrugated iron shed			
26+00				
26+22				
26+50				
27+00				
27+50				
28+00				

Left.

67

$\frac{4.2}{25}$

$\frac{4.0}{9}$

4.3

$\frac{4.0}{8}$

tel. pole.

$\frac{14}{16}$

fence

$\frac{4.4}{25}$

$\frac{4.2}{25}$

$\frac{5.1}{7}$

5.5

$\frac{5.3}{10}$

fence

$\frac{15}{25}$

$\frac{5.1}{25}$

$\frac{5.2}{25}$

$\frac{4.8}{9}$

5.2

$\frac{5.5}{9}$

fence

$\frac{15}{25}$

$\frac{5.0}{25}$

24' to right of ϕ

24' to right of ϕ

$\frac{5.3}{25}$

$\frac{4.9}{9}$

5.2

$\frac{5.1}{9}$

fence

$\frac{15}{25}$

$\frac{4.6}{25}$

tel. pole.
 $\frac{15}{15}$

$\frac{5.9}{25}$

$\frac{4.8}{8}$

5.4

$\frac{5.2}{8}$

fence

$\frac{15}{25}$

$\frac{4.9}{25}$

$\frac{5.8}{25}$

$\frac{4.8}{10}$

5.3

$\frac{4.4}{10}$

fence

$\frac{15}{25}$

$\frac{4.8}{25}$

$\frac{5.4}{25}$

$\frac{4.6}{10}$

5.0

$\frac{4.7}{10}$

fence

$\frac{16}{25}$

$\frac{5.0}{25}$

$\frac{5.6}{25}$

$\frac{4.5}{10}$

5.5

$\frac{5.5}{10}$

fence

$\frac{15}{25}$

$\frac{4.7}{25}$

11)

Sta.	+	H.L.	-	Elev
28+05		Last of line of tel. poles.		

405.46

28+40¹⁶ P.I.

29+00

29+50

30+00

30+30

30+50

T.P.

9.20 396.26

tel. pole
 $\frac{15}{15}$

$\frac{5.1}{25}$	$\frac{4.5}{22}$	$\frac{4.1}{6}$	5.2	$\frac{5.3}{12}$	$\frac{\text{fence}}{15}$	$\frac{4.5}{25}$
------------------	------------------	-----------------	-----	------------------	---------------------------	------------------

$\frac{4.0}{25}$	$\frac{3.1}{8}$	4.7	$\frac{\text{fence}}{13}$	$\frac{4.4}{25}$
------------------	-----------------	-----	---------------------------	------------------

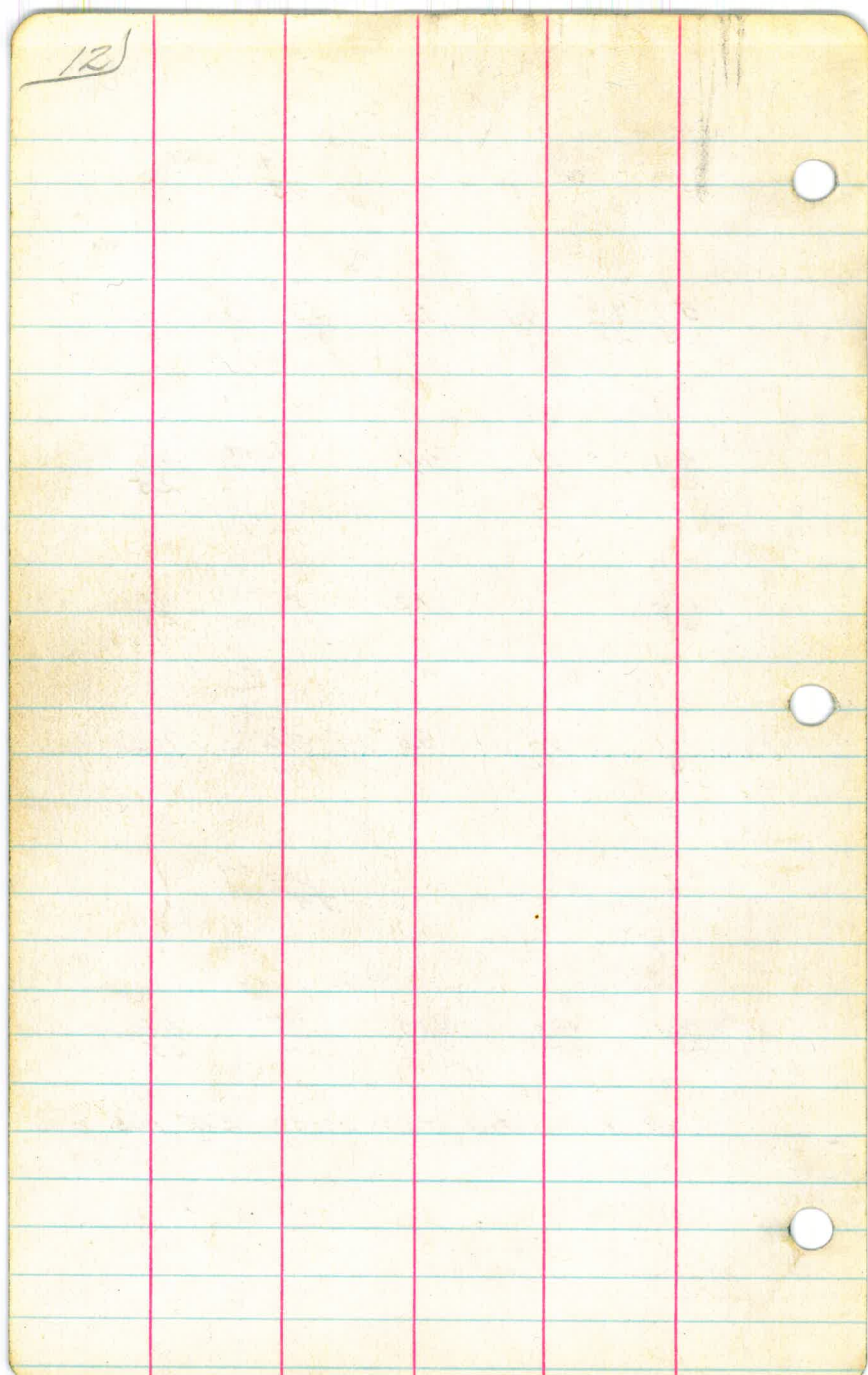
$\frac{11.0}{25}$	11.2	$\frac{\text{fence}}{11}$	$\frac{11.0}{25}$
-------------------	------	---------------------------	-------------------

$\frac{10.1}{25}$	$\frac{9.8}{12}$	9.8	$\frac{\text{fence}}{14}$	$\frac{10.0}{25}$
-------------------	------------------	-----	---------------------------	-------------------

Large tree
 $\frac{15}{15}$

$\frac{10.4}{25}$	$\frac{10.6}{12}$	10.3	$\frac{\text{fence}}{22}$	$\frac{9.3}{25}$
-------------------	-------------------	------	---------------------------	------------------

5' left of large tree at sta 30+30. 2"x2" hub.



Topography

From Sta. 43+83⁹⁴

To Sta. 62+80.

May 17.

L

Sta. 45+43² End of Building

45+00 69.1 Distance overall

44+74² Start of Building

+71 Fce. offset.

+50

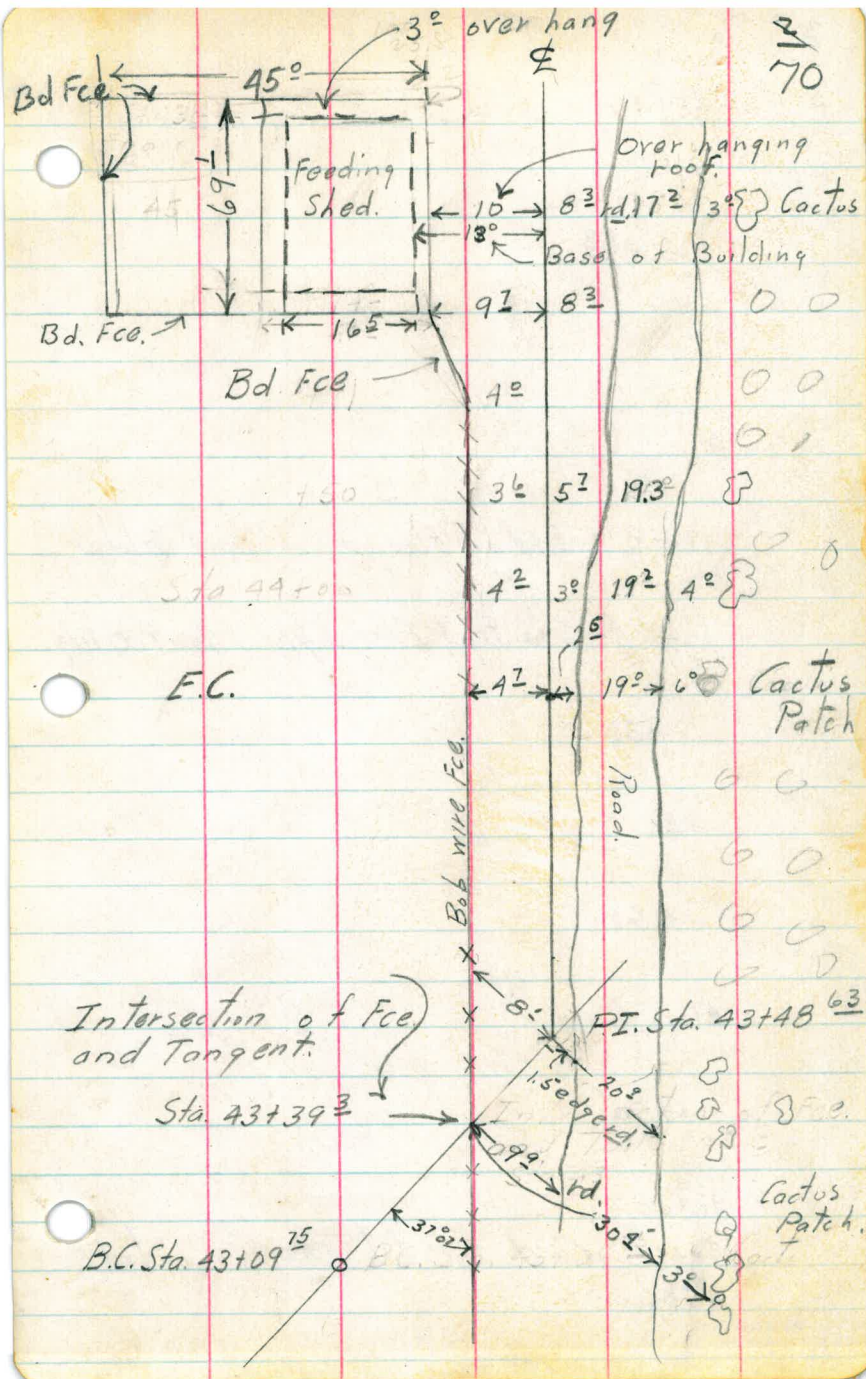
44+00

43+83⁹¹ E.C.

43.3

74.0

58.7



3

+2988

49

+89⁴ End of Elec. Light Plant Bldg.

+73³ Start of Elec Light Plant Bldg.

+50

48+00

+50

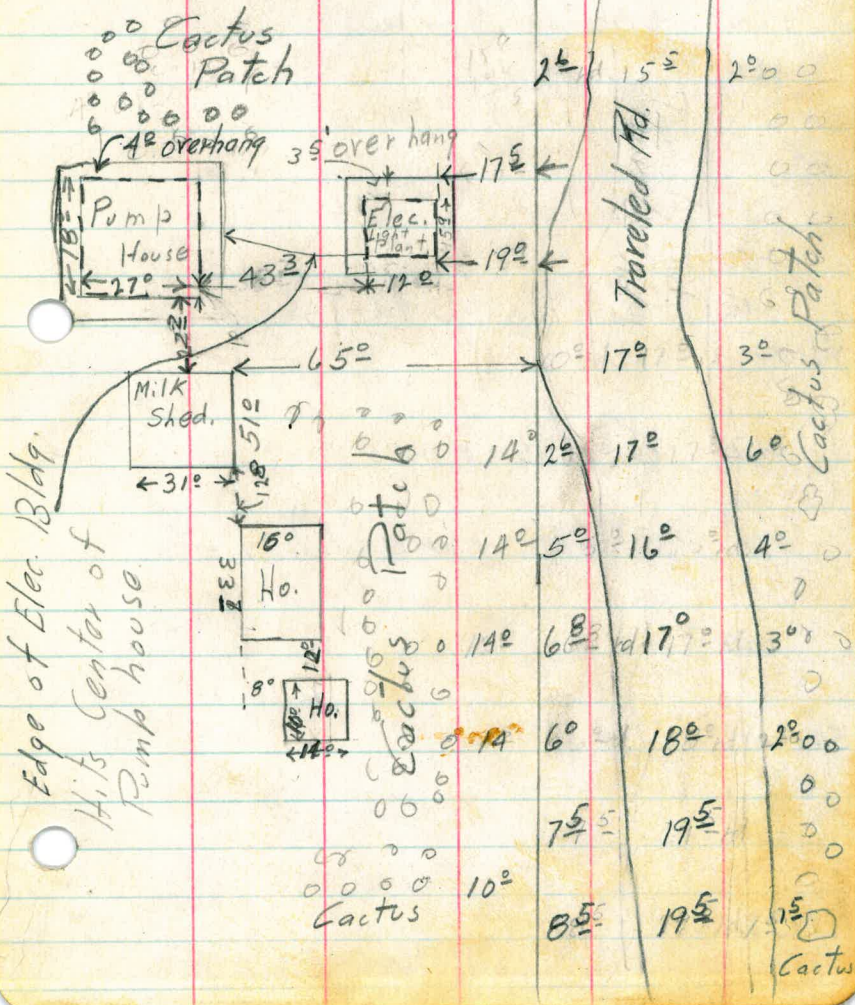
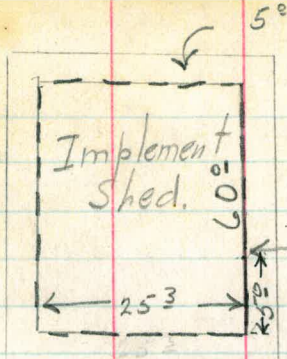
47

+50

46+00

+63 Cactus Patch starts on left.

45+50



5

+50

53° Cactus starts

+60 Cactus stops

+50

52

+50

+40 Cactus starts

51+00

+92 Cactus ends

+78 stable (far end.)

+92

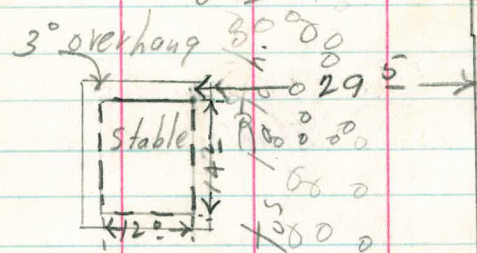
+50

50+00

+50

49+32

000	12°	10	15°	6°	00
000					00
000		5°	16°		00
000					00
00	12°	4°	16°		5°00
00					00
0000 ←	13°	5°	15°		0000
00					00
00		5°	15°		00
00					00
00		5°	15°		00
00					00
00		5°	15°		00
00					00
00		5°	15°		00
00					00
00		5°	16°		4°
00					00
00	10°	5°	16°		5°
00					00
00	10°	4°	16°		00
00					00
00					00



gac
tos

15
72

7

56+00

+50

55

54+50

54+30

Cactus Starts

53+99⁸⁵

E.C.

3°

36

+79⁸⁰

P.I Cactus Stops.

53+75°

9

61+00

60+00

+50

59

+50

From here on temporary
road in sand.

58+00

+75

+50

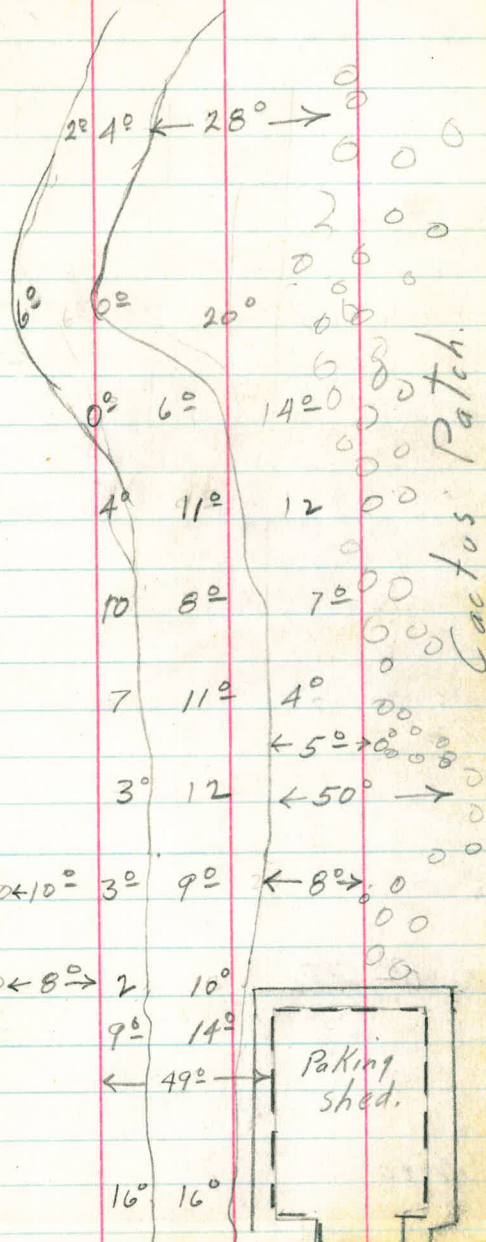
End of Cactus on Left.

57+06⁷⁹ E.C.

+88⁴³ P.I.

+50

56+00



Cactus Patch.



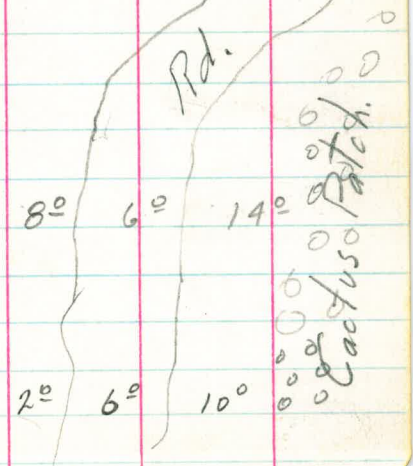
11

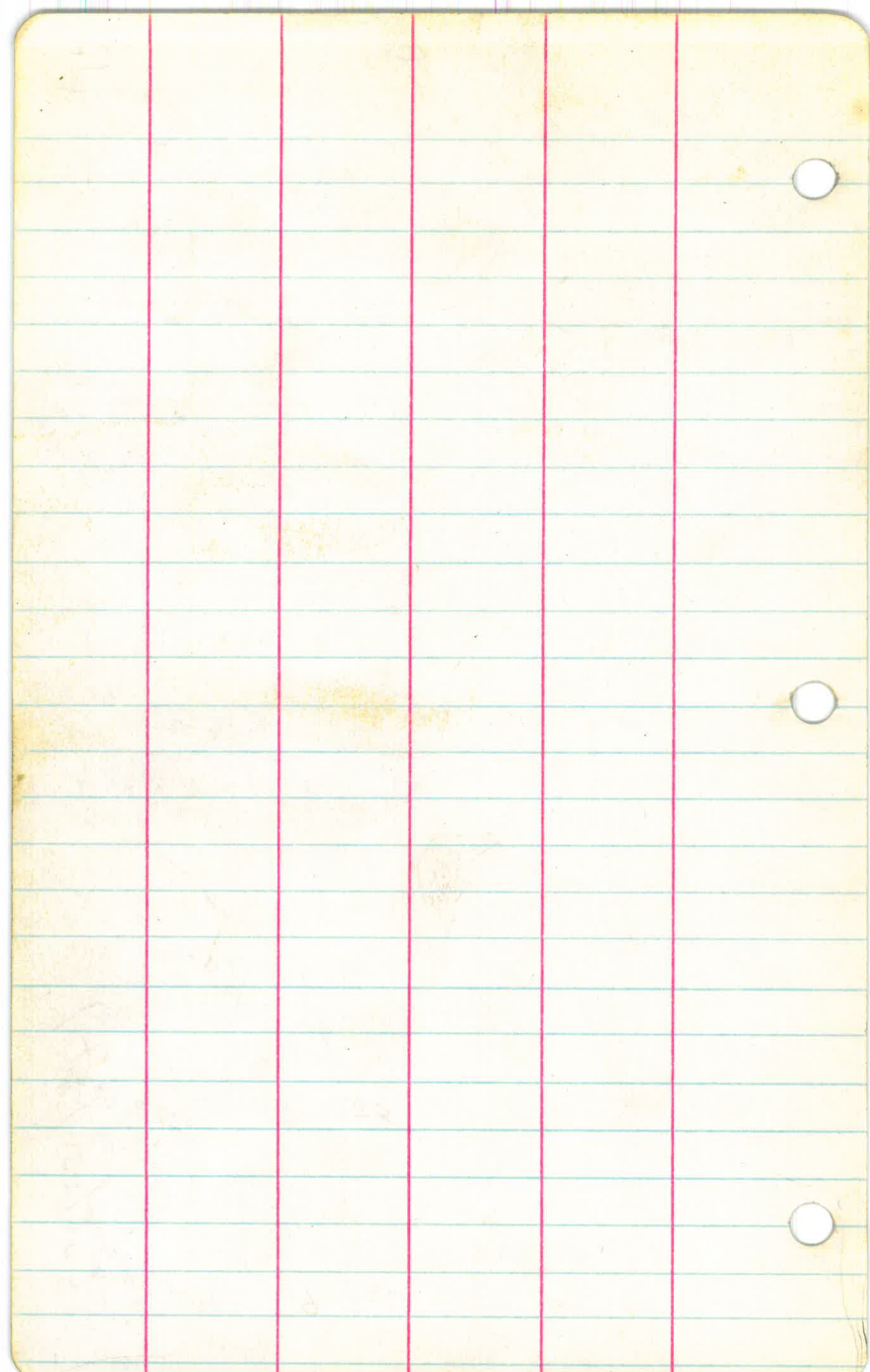
62+80²¹ P.I.

62+00

12
75

2





May 12, 1927.

Stations and
Elevations taken, of
Irrigation Pipes.

From Sta. 78+20⁶
To " 96+46³

San Vicente Pipe Line

Sta.	+	π	-	El.	B.M.
1				411.48	411.48
	3.84	415.32			

Top of Con Pipe			4.55	409.77	
Outside Diam. Pipe =				.92	11"
Bottom of Pipe				408.85	

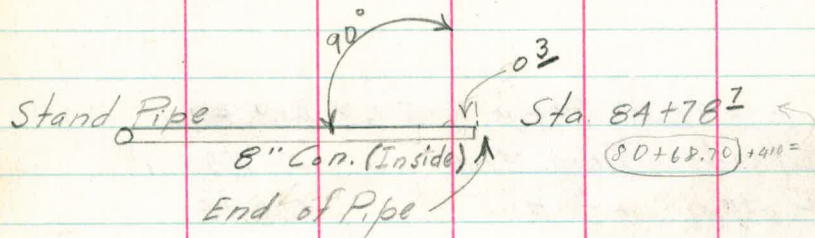
T.P.			4.07	411.25	
	4.25	415.50			

Top of Con. Pipe			5.37	410.13	
Outside Diam Pipe =				1.17	14"
Bottom of Pipe				408.96	

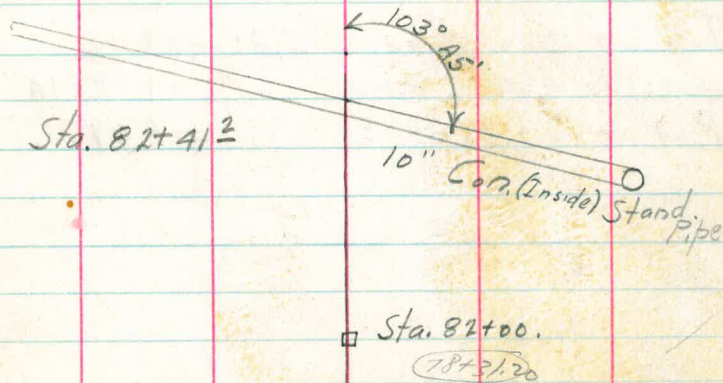
Party - Same.

77)

Note - This Pipe can be cut off so as not to interfere with grade.



Note



2 + π - El.
415.50

Top of Con. Pipe. 5.63 409.87
Outside Diam. Pipe .92 11"
Bottom of Pipe. 408.95

T.P. 4.39 411.11
4.06 415.17

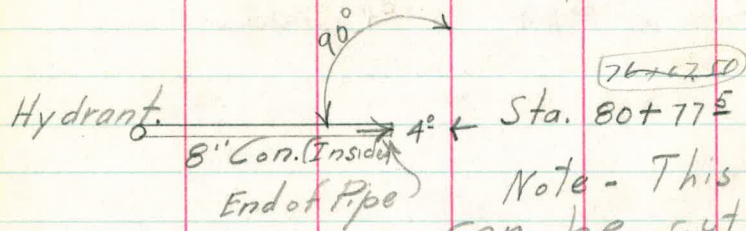
Top of Con. Pipe 5.41 409.76
Outside Diam. Pipe 1.17 14"
Bottom of Pipe = 408.59

May 12, 1927

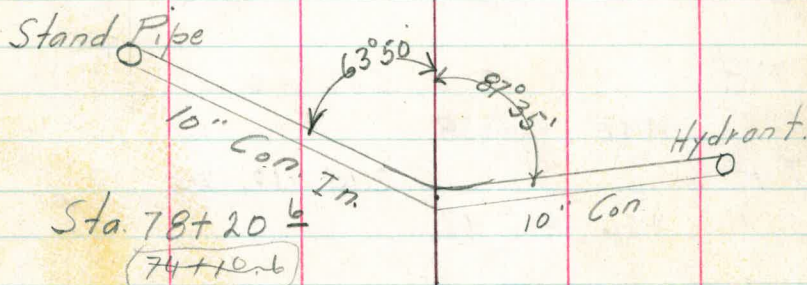
Party - Leach
Simpson
Clarett
Mattoon




78 →

Note - Add 4" for a 10" Pipe
and 2½" for an 8" Pipe.



Note - This Pipe
can be cut off
so as not to
interfer with
grade.



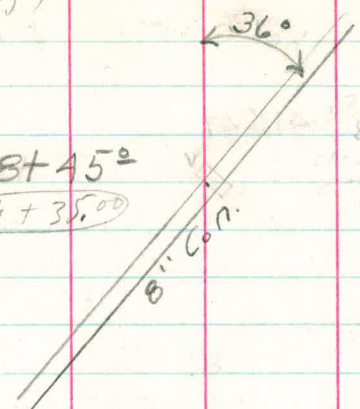
3	+	π	-	El.	Power Pole # 72670
BM.					411.48 
	4.05	415.53			
Top of Con. Pipe =	6.00	409.53			
Diam. Pipe =		.92		11"	
Bottom of Pipe				408.61	
Top of Con. Pipe	6.59	408.94			
Diam. Pipe		.92		11"	
Bottom of Pipe				408.02	
T.P.			5.32	410.21	
	4.17	414.38			
T.P.			3.15	411.23	
	4.26	415.49			
Top of Flange	5.63	409.86			
Diam of Pipe at Flange =		1.14			
Bottom of Pipe at Flange.				408.72	

92
22
114

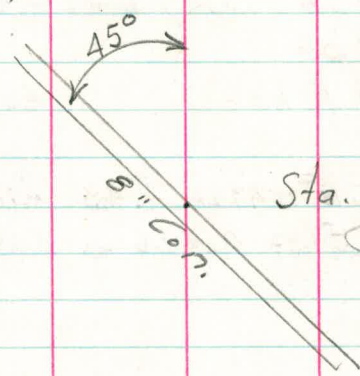
±

Party - Same
79 3

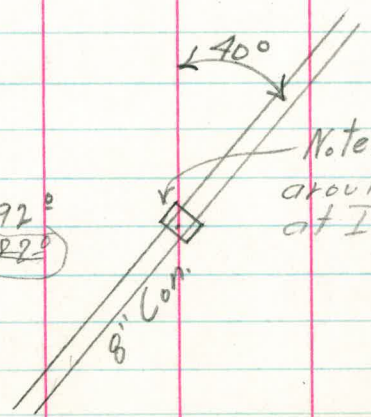
Sta. 88+45⁰
84+35.00



Sta. 89+24³
85+14.3



Sta. 94+92⁰
90+82⁰



Note: - 1 3/8" Flange
around Pipe
at Intersection

4 + π - El.

415.49

Top of Pipe 5.42 410.07

Diam. Pipe .92

Bottom of Pipe. 409.15

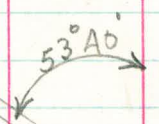
B.M. Power Pole # 24222 1.43 414.06

Recorded El. = 414.06 ← check

222

80
4

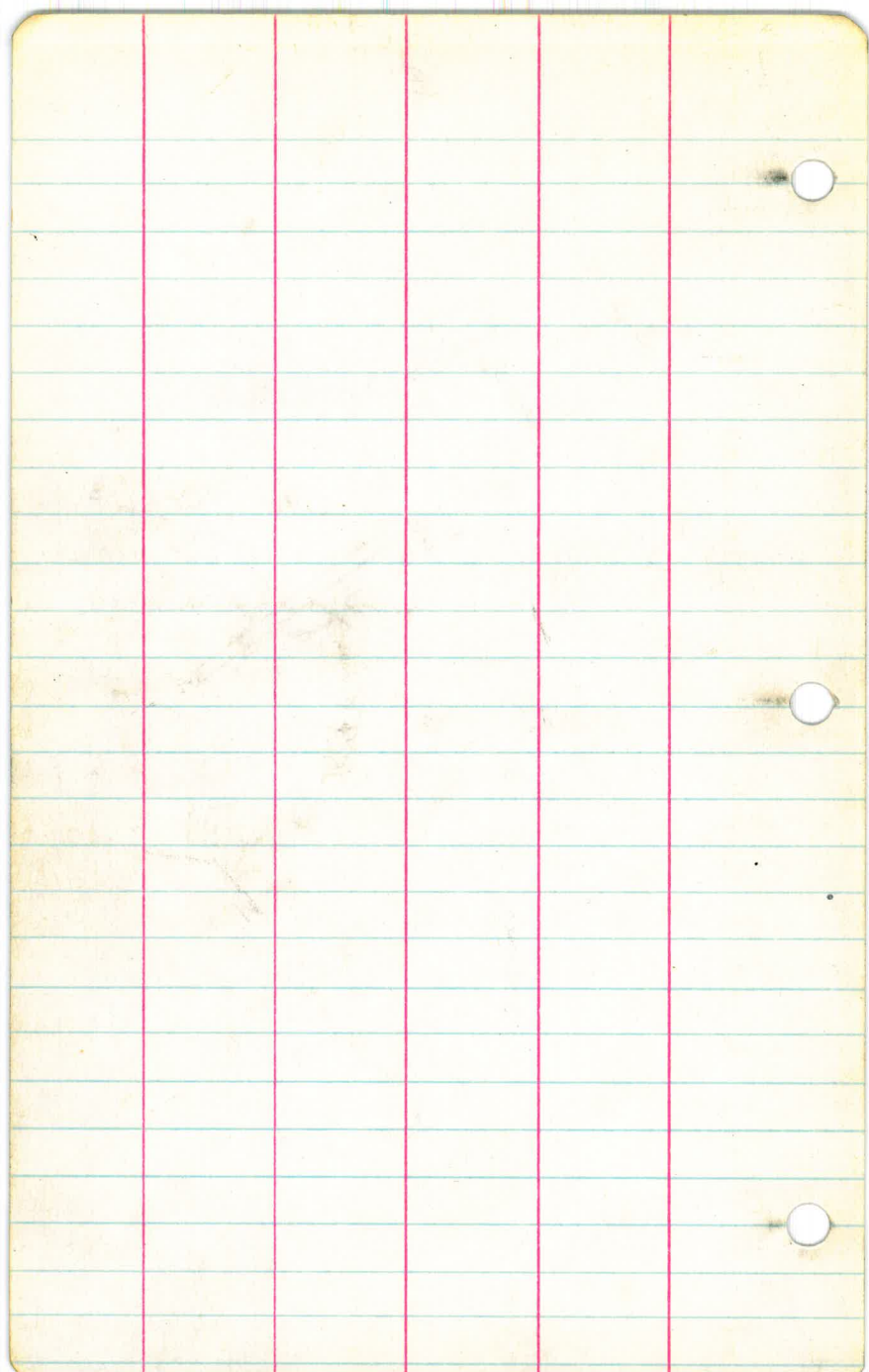
Hydrant.



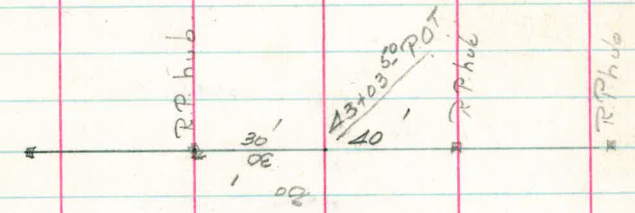
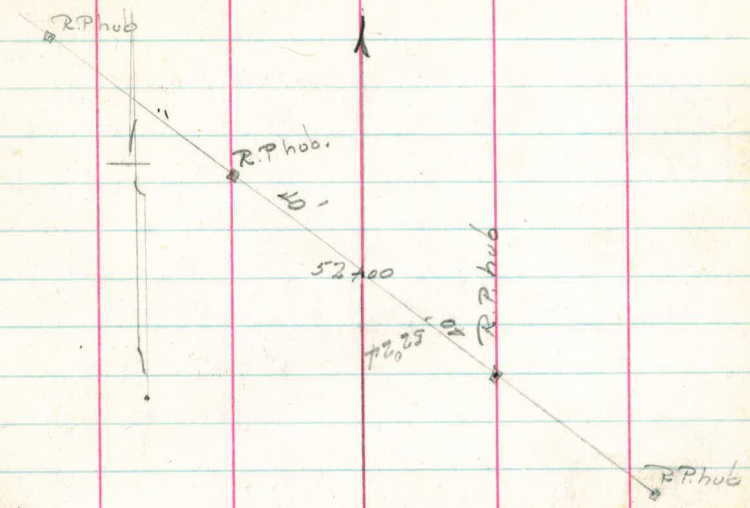
8"

Con. Pipe

Sta. 96+46.3
92+36.3



R.P. Lateral to San Vicente Pipe Line



12-27
Van Horn
Street
S. of
Mickey

Rock in
South
side of
Van Horn
about
1/2
mi. S. of
Bridge
Contact.

74+77.80 P.I.

60°
50°

74+44.51 B.C.

132

RR hub in
fence line

RR on left
10 feet

71. 74+77.80 P.I.

69°

45'

75+07

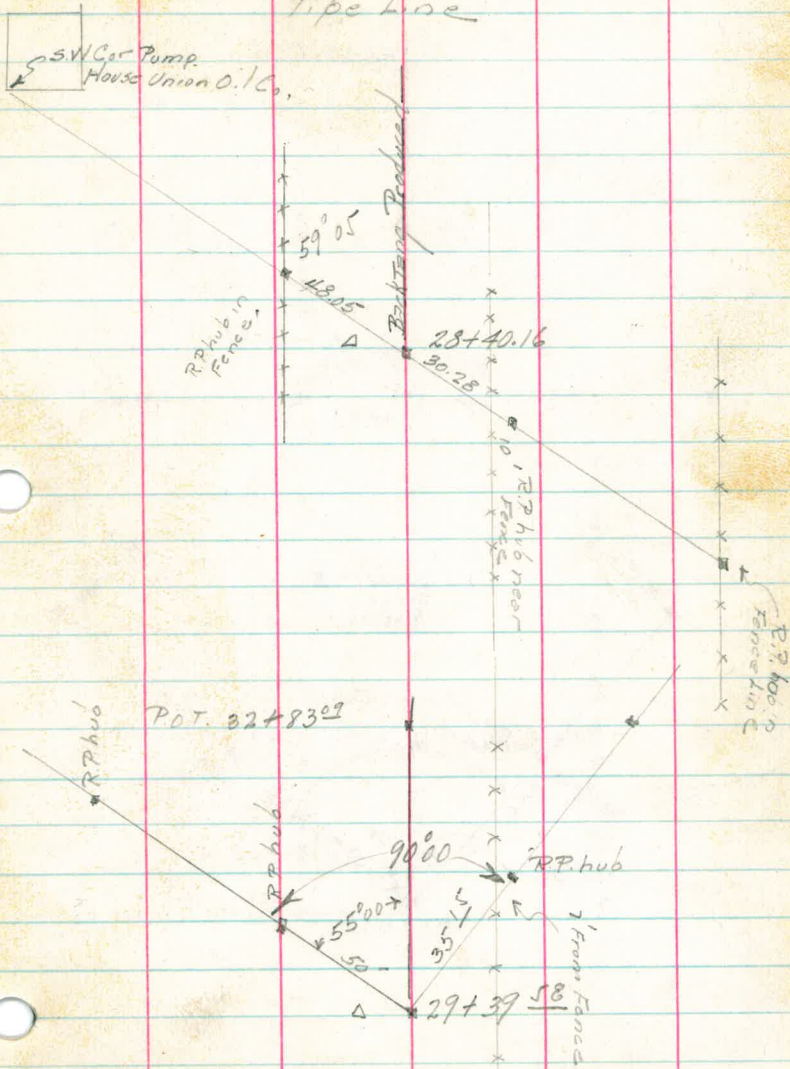
EL

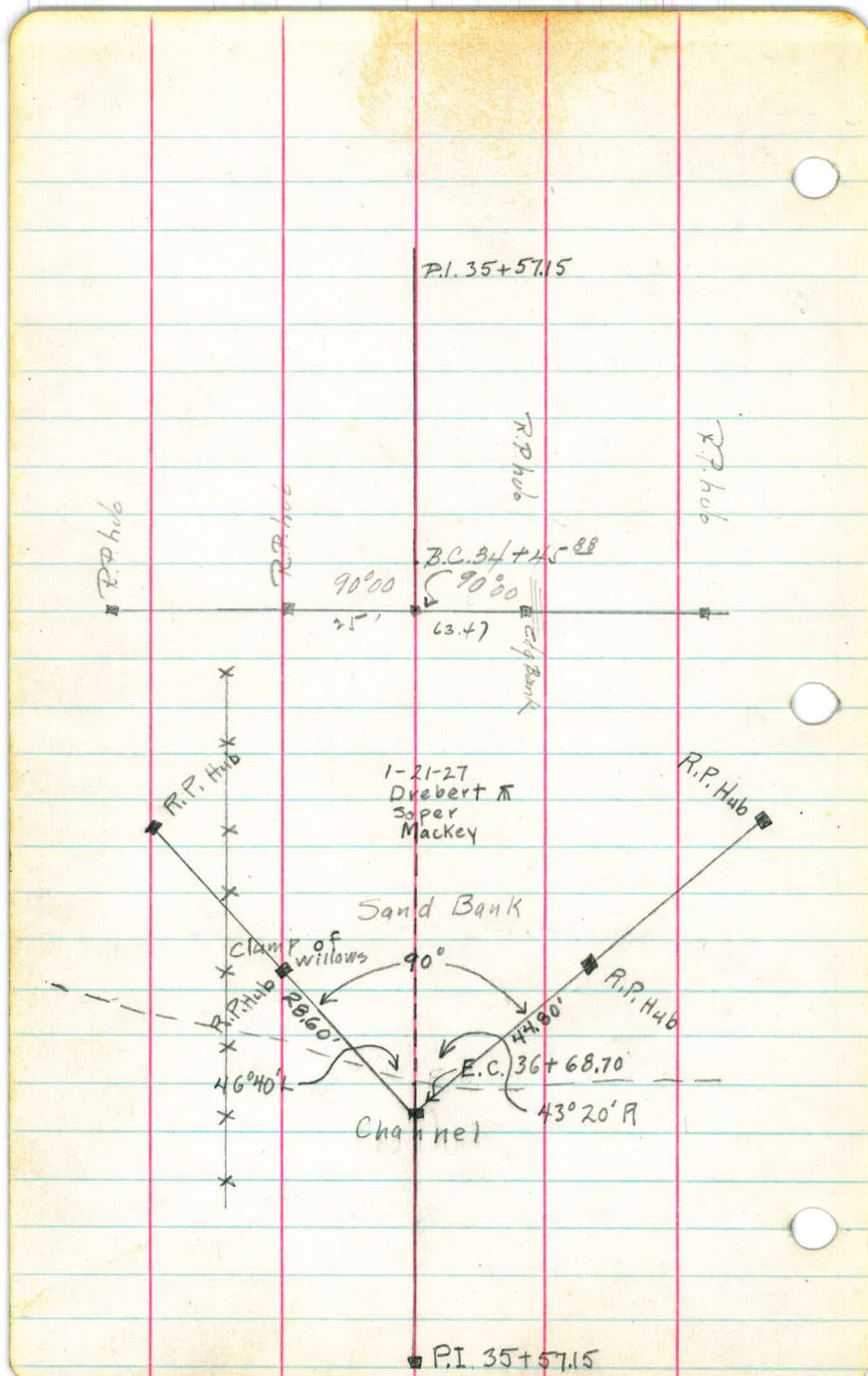
42.09

111°

on Bank
10 feet

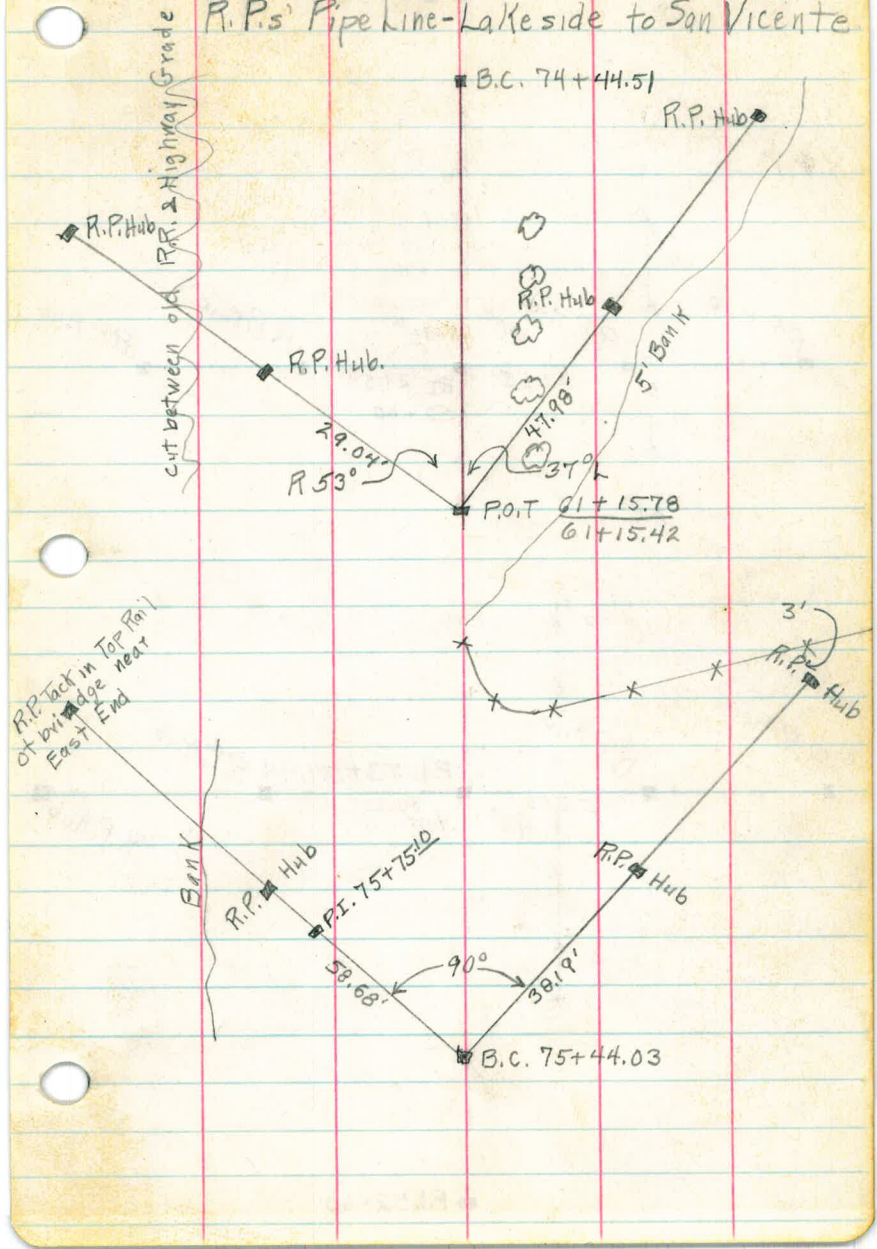
R.P.'s takeoffs to San Vicente
Pipe Line



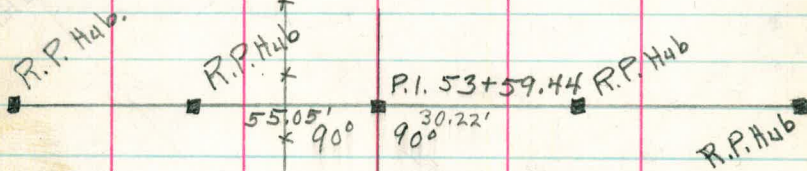
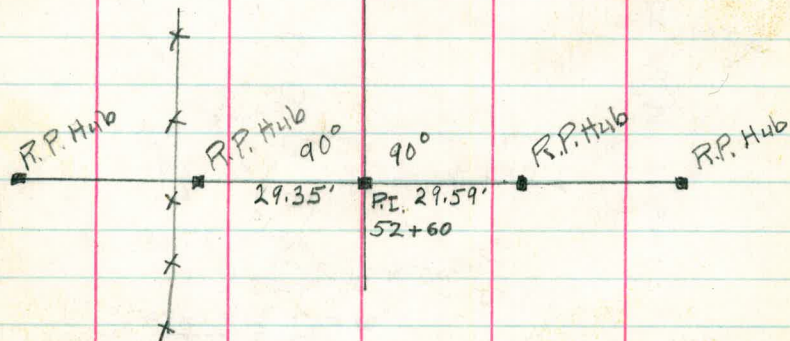


1-21-27
Drebert &
Soper
Mackey 83

R.P.s' Pipe Line - Lakeside to San Vicente



■ 53+59.44 P.I.

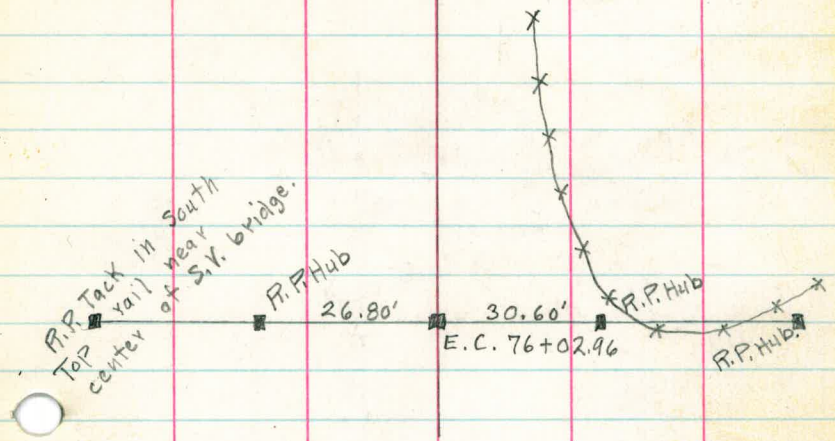


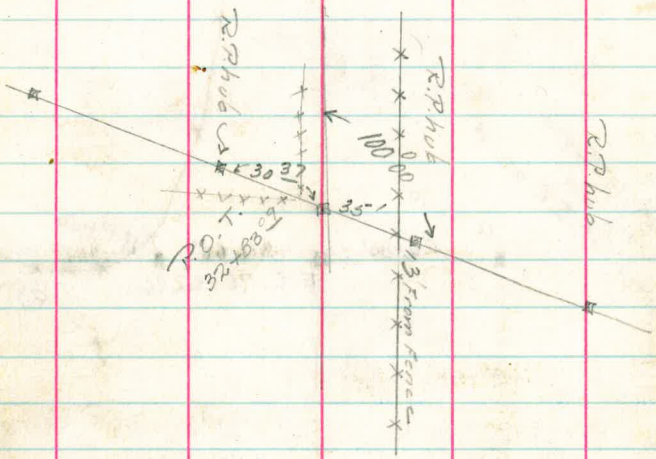
■ P.I. 52+60

1-22-27
Drebert π
Soper
Mackey 84

R.P.s' Pipe Line - Lakeside to San Vicente

Eq. B.C. $78+46.84$
 $78+09.78$





Sta

68+72

Sand River bottom.
& Tree roots

67+50

River bottom sand.

58+00

Soil some sandy loam.
Probably strike some red earth.

43+00.

River silt.

40+00

River silt and Trees

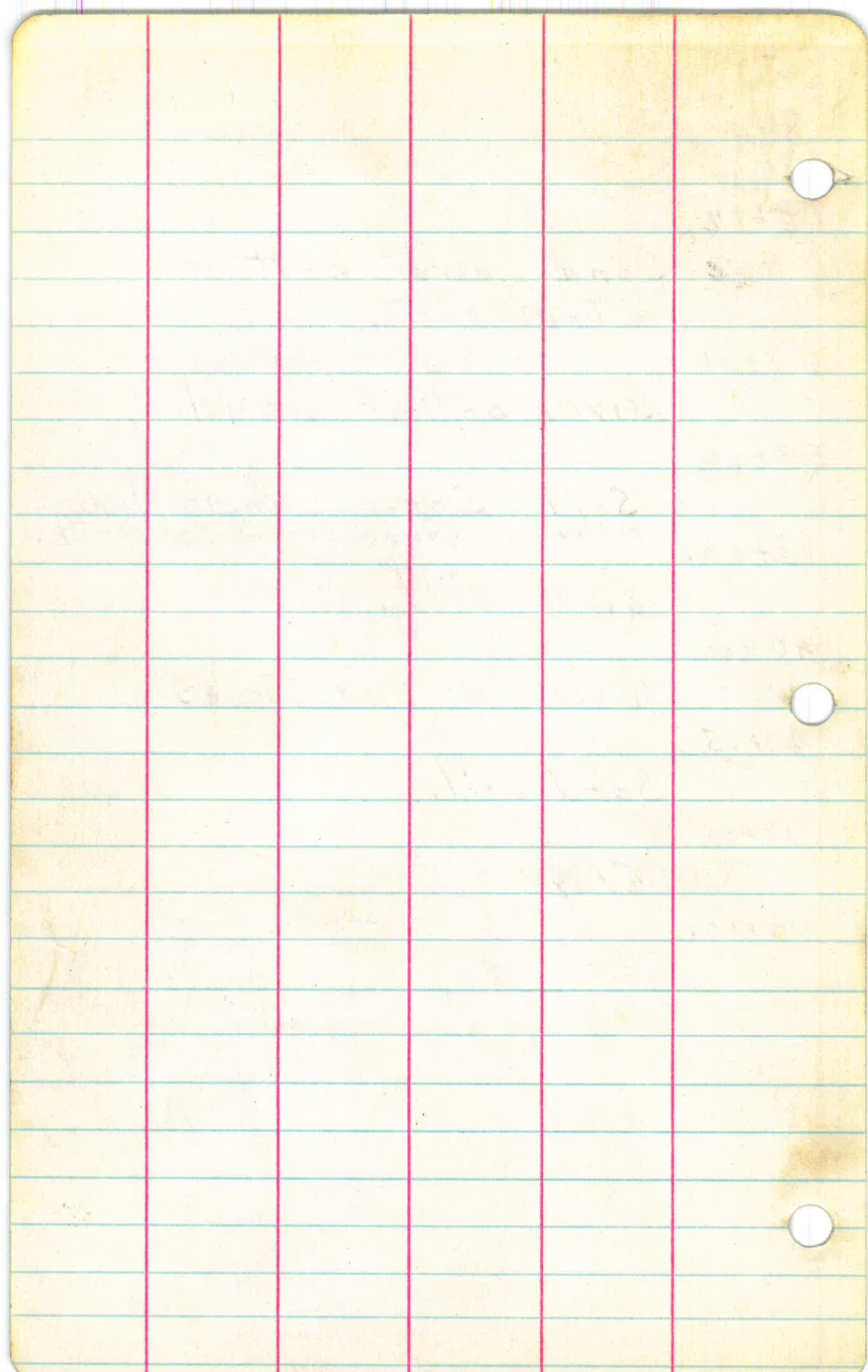
29+15

Sand soil.

19+00

Clay

0+00.



Classification

86

May 17, 1927.

Sta.

End of line

Outcropping of large
Boulders. (Brush) Practically (S.R.)

212+00.

Outcropping of smaller
Boulders & decomposed granite
& Brush.

209+61

River Silt & some Brush.

206+00

River Crossing

203+50

about 1' covered with sand
below that apparently
decomposed granite.

195+75

3' covered with loose sand.
decomposed granite below
that.

192+50

Sandy Soil

188

Sta.

188

Soil on Clay packed.
Probably some decomposed Granite

183+75

Decomposed Granite &
Hard Pan.

178+00

To Decomposed Granite Hardpan
& out cropping of rock.

172+50

Sandy Soil

98+21

Plowed Field. very sandy
to soil.

91+50

Alfalfa Field sandy soil

87+67?

to Road Crossing

to Plowed field.

74+25

Sandy soil & Tree roots.

71+15

River Crossing

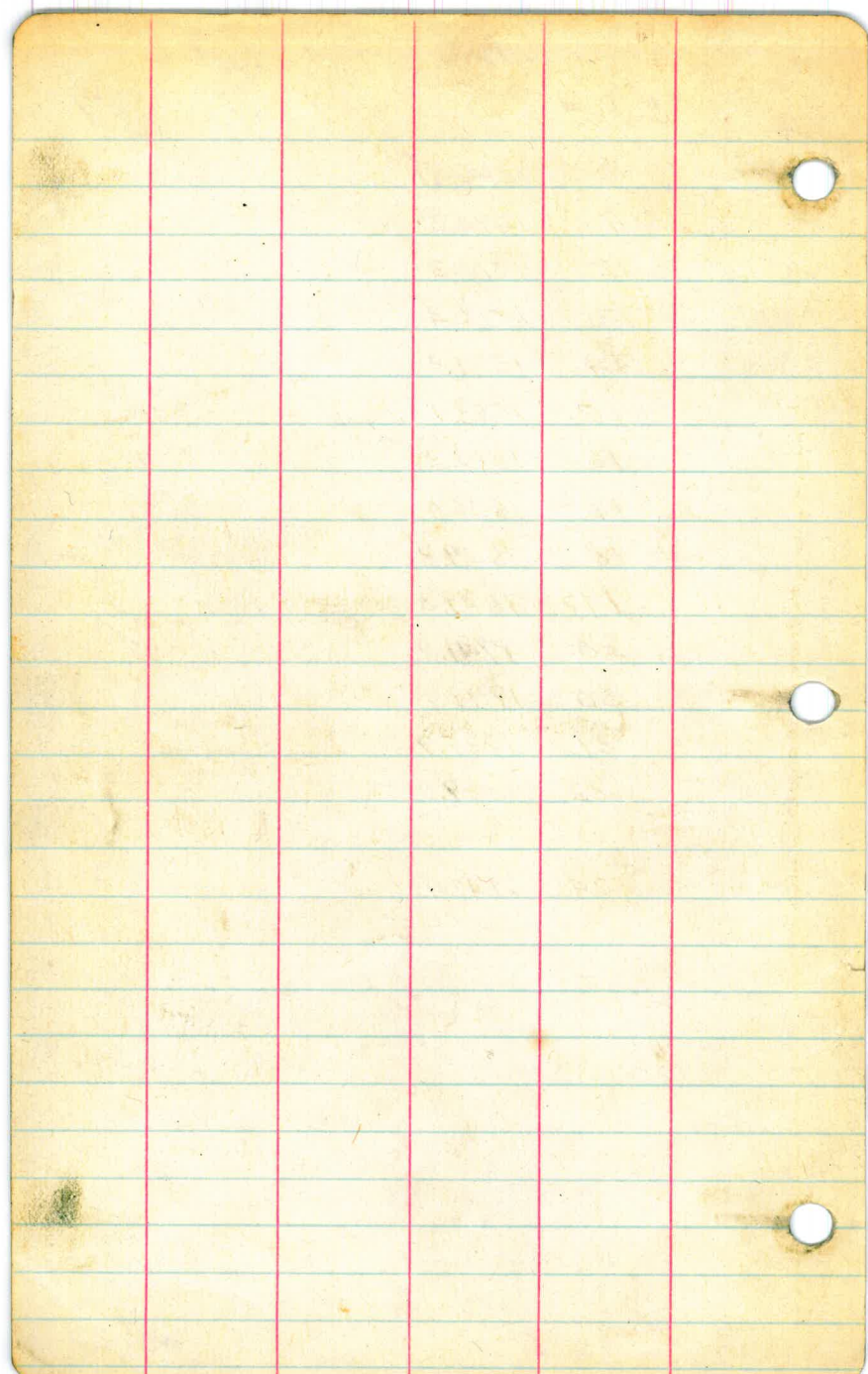
68+72

Bench Mark List

89

B.M. #

- | | |
|----|---------|
| 10 | 1486.31 |
| 11 | 1494.3 |
| 12 | 1510.3 |
| 13 | 1516.4 |
| 14 | 1531.8 |
| 15 | 1553.1 |
| 16 | 1610.3 |
| 17 | 1646.0 |
| 18 | 1649.8 |
| 19 | 1649.3 |
| 20 | 1741.8 |
| 30 | 1798.9 |
| 31 | 1835.9 |
| 32 | 1889.0 |
| | 18 |
| 34 | 2147.9 |



NAME

Class Course Party

FIELD NOTES

No. 403 P

ESPECIALLY ADAPTED
TO THE USE OF
ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

Index

Page 1 - Relocation of B1.

8 - Retracing of ϕ Pipe Line from
Sta. 85+56⁷⁵ to 171+49³¹

10 - Relocation of ϕ Pipe Line
from Sta 171+49³¹ to

April, 14, 1927

Relocations of B.I.

Set P.O.T. on C of pipe line at intersection of Vine St. and Laurel, for P.I. to new line E. on Laurel from Vine St.

Thence E. on Laurel to Ash and thence N. on Ash, + Crossing River.

Tying into old Pipe Line Survey at Sta. 357627

Refer to Loose Leaf B1 for notes on old line.

21

Sta. Dist. Angle

Ferguson
Glover
Elliott
Bailey
Lundy

45+60 P.I.

N 9°08'15"W

35+85.24

90°0'00" L

$\Delta 90^{\circ}00'00''$

R = 50'

S.T. 50'

L.A. 78.54

B.C. = 35+35.24

E.C. = 36+13.28

29+60.29

F.O.T.

1176.50

$\Delta 89^{\circ}46'30'' R$

S.T. = 49.80

B.C. = 23+80.20

N 80°51'45"E E.C. = 24+58.54

L = 78.34

R = 50 ft.

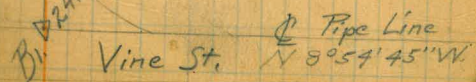
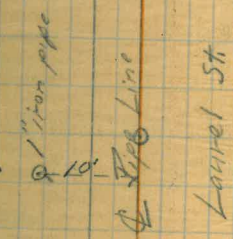
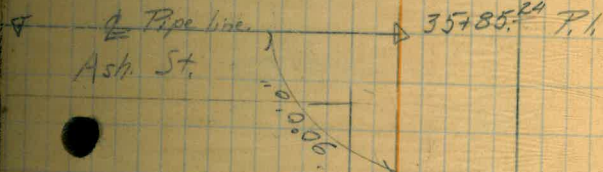
24+30.00

89°46'30" R

26+75.15

22

45+60



3)

Sta. Dist. Angle

$$\Delta = 23^{\circ}18'30''$$

$$R = 100$$

$$ST = 20.63$$

$$BC = 57 + 67.37$$

$$LA = 40.68$$

$$EC = 58 + 10.05$$

57+90⁰⁰

23°18'30" R

N. 37°31'15" E

53+35⁰⁰

5°45' R

N. 16°12'45" E

47+55⁰⁰

5°14'0" L

N. 10°27'45" E

$$\Delta = 24^{\circ}30'$$

$$R = 100'$$

$$ST = 22.02$$

$$BC = 45 + 87.28$$

$$LA = 43.34$$

$$EC = 45 + 81.32$$

45+60

24°50' R

N. 15°41'45" E

35+85²⁴

57+90

53+35⁰⁰

47+55⁰⁰

45+60

Ash St

Pipe Line

Laurel St.

35+85²⁴

Bc Line

Pipe Line

Farm Road

585

2561

2222

4

Sta. Dist. Angle

72+79 ↑ Edge of water

72+67²² ← 112
P.O.T.

70+94⁸¹ ↓
P.O.T.

406.86
↑

66+90¹¹ ↓ 37°35' L

A: 37°35'
75°47'30"
R=100
S.T.=34.03
BC=66+56²⁸
LA=65.60
EC=67+21⁹⁸

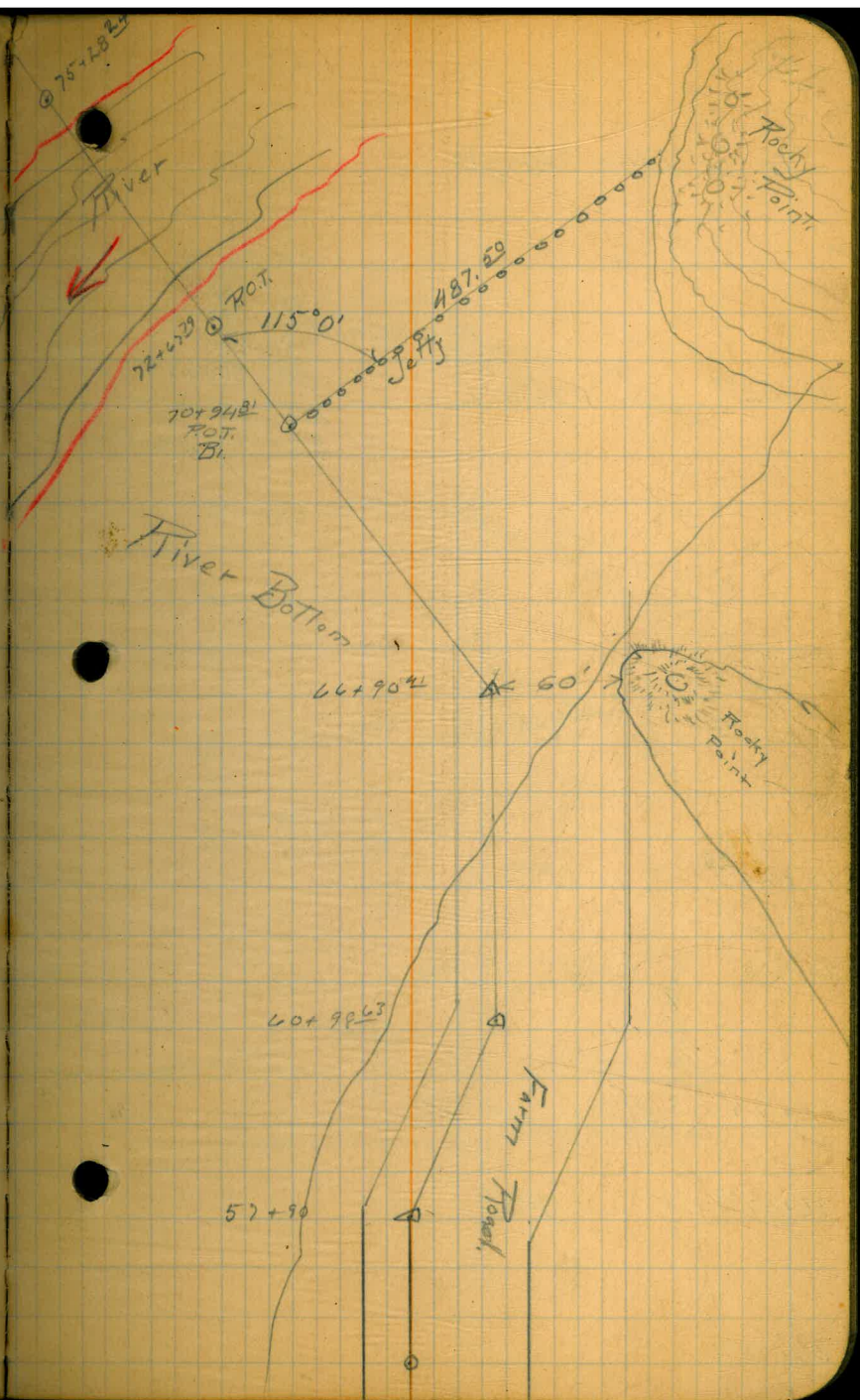
60+98⁶³ ↓ 21°14' L

N.18°17'15"E
D=21°14'
70°37'
R=100
S.T.=18.75
BC=60+79⁸⁸
LA=37.06
EC=61+16²⁹

57+90 ↓ 23°18'30" R

N.39°3'15"E

53+35



5

Sta. Dist. Angle.

$\Delta = \frac{36^\circ 12'}{18^\circ 06'}$
 $R = 100$
 $N. 55^\circ 27' 45" W.$ ST. 32.69
 $BC = 89 + 69.31$
 $LA = 63.18$
 $EC = 90 + 32.49$

90+02.00 36°12'L

76+50.42 P.O.T.

N 17° 17' 45" W.

75+28.24 P.O.T.

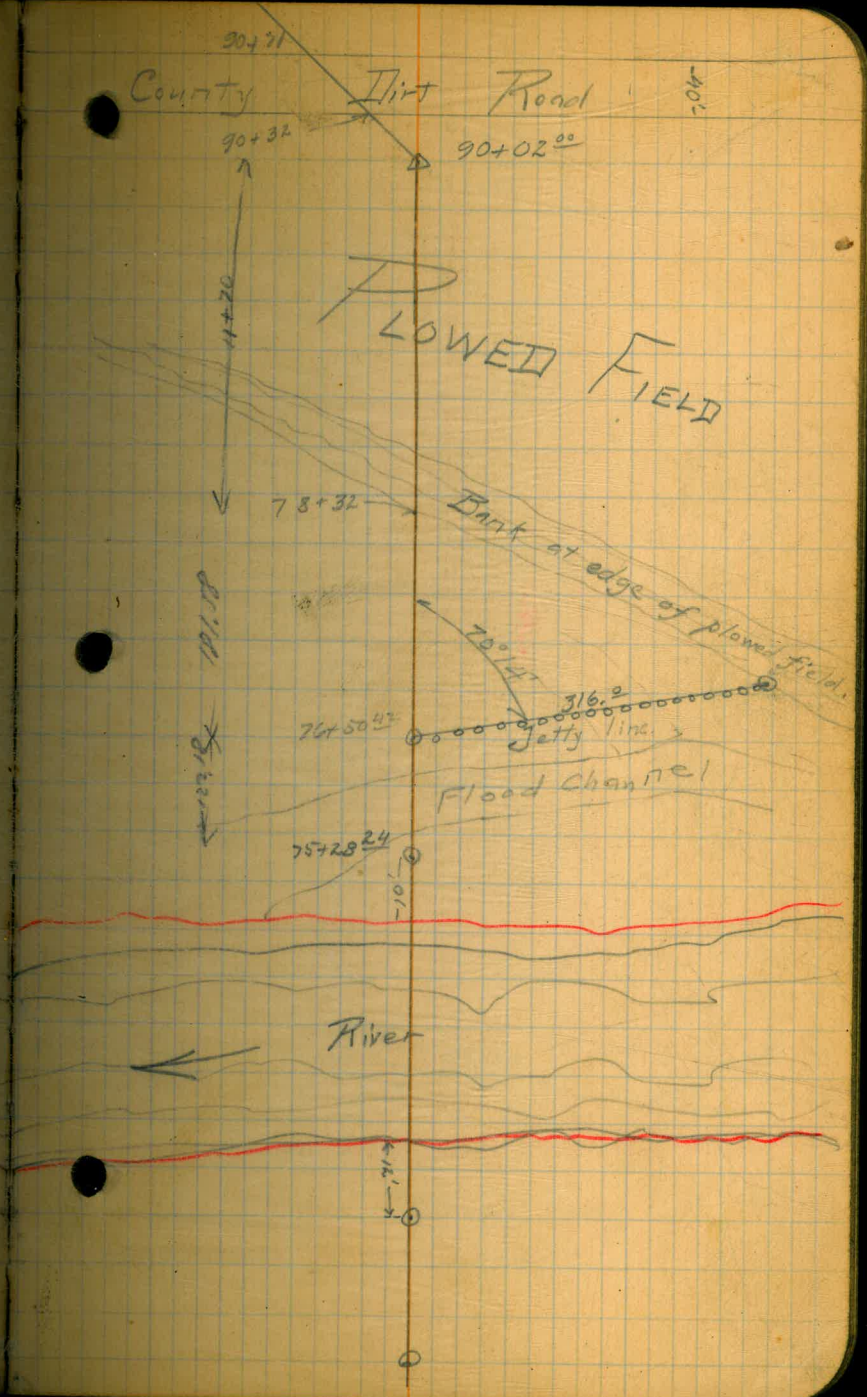
75+18 Edge of River

260.45

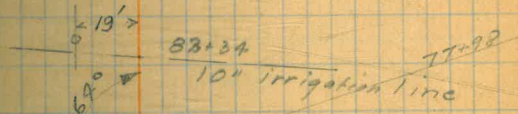
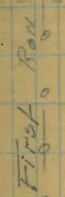
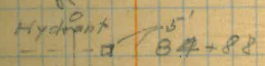
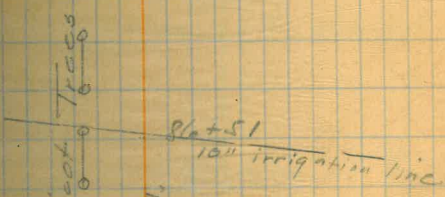
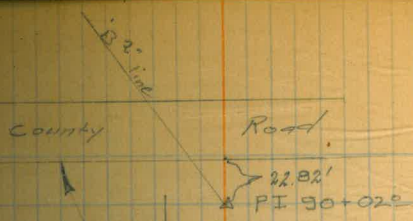
72+79 Edge of River.

72+67.79 P.O.T.

66+90.41



6



Sta. Dist. Angle

$N17^{\circ}02'15''W. = (17^{\circ}03'07\frac{1}{2}'')^{Old} Line$

$A = \frac{36^{\circ}27'30''}{18^{\circ}13'45''}$

$R = 100$

$S.T. = 32.94$

$BC = 102 + 30.29$

$LA = 63.63$

$EC = 102 + 94.46 = 85 + 56.76$

102+63.73

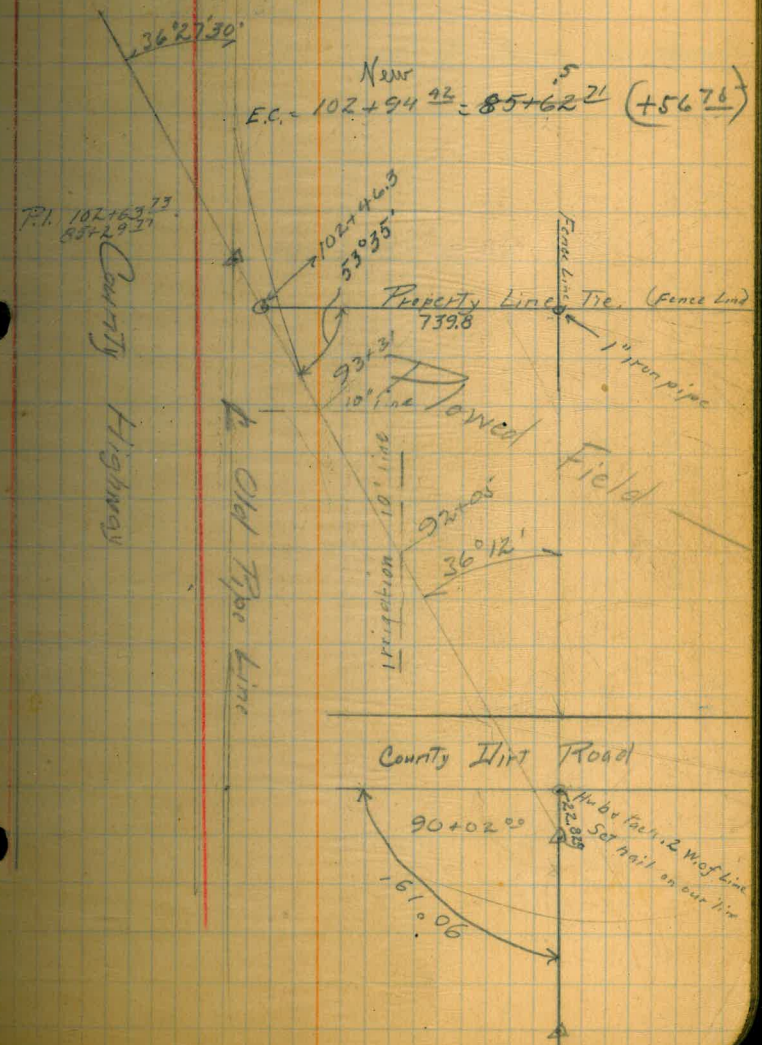
36°27'30" R

$N55^{\circ}29'45''W$

90+02.00

36°12' L

66+90.41



8)

Ferguson - Chief
Andrews T
Heffernan chain
Mattoon "

April, 18, 1927

Retracing of
¢ Pipe Line from Sta 85+56.75
to 171+49.31 and.

Relocation of ¢ from Sta 171+49.31
to the San Vicente Horn Site.

9) Def Angle

Sta. Left Right.

142+67¹² 0°22'52½"

133+00 0°19'07½"

85+56⁷⁵

82+83³⁸

Refer to Book B1
for original notes

142+67¹⁰

133+00

85+56⁷⁵ EC on New Location
across river

EC. 82+83³⁸

10) Def Angle

Sta L R
BC
174+87.86

N. 12° 52' 38" E. 353.07

EC
173+90.30 15° 56' 30"

173+58 13° 16' 30"

173+00 9° 58' 30"

172+50 6° 40'

172+00 3° 21' 30"

BC
171+49.2

31° 50' 45"
Δ = 31° 52'
S.T. = 123.70
R = 433.3
BC = 171+49.2
L.A. = 240.79
EC = 173+90.3

see page 20

Old & across river.

174+87.86 BC

173+90.30

171+49.2

N. 18° 57' 22" W.

142+67.10

115

Def Angle

L R

N. 40° 31' 38" E. (832)

PI, 7° 56' 30"
178+50 7° 58' 40"

N. 48° 30' 18" E. (232)

EC.
177+42.2 17° 46' 50"

177+00 14° 51' 09"

+50 11° 21' 07"

176+00 7° 51' 05"

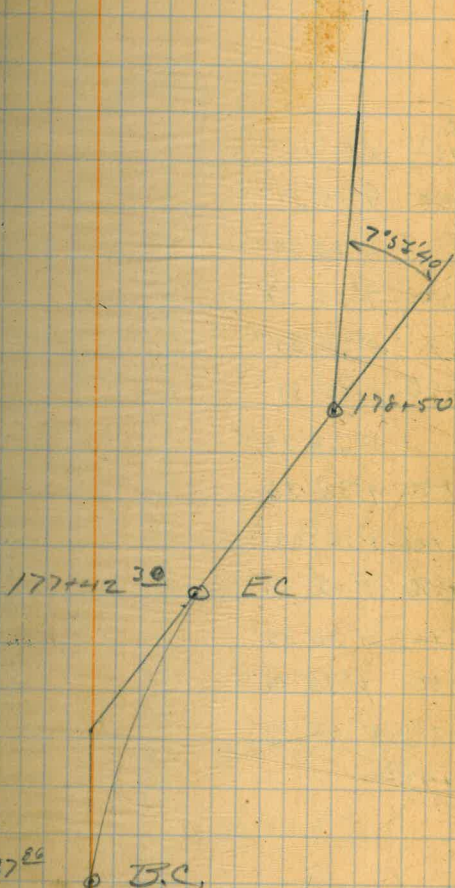
+50 4° 21' 03"

175+00 0° 51' 01"

BC
174+87.2

14° Curve
Δ = 85° 37' 40"
R = 410.25
S.T. = 131.81
BC = 174+87.25
LA = 254.44
E.C. = 177+42.20

35° 43' 15"



(12)

Def. Angle

Sta. L R

E.C. 190+13.21 16°03'10"
 +50 9°05'39"
 189 8°26'39"
 +50 7°35'39"
 188 6°50'39"
 +50 6°05'39"
 187 5°20'39"
 +50 4°35'39"
 186+00 3°50'39"
 +50 3°05'39"
 185+00 2°20'39"
 +50 1°35'39"
 184+00 0°50'39"
 183+43.22

N20°25'18"E (877.2)

20°05'

3° CURVE

A = 20°06'20"

TR = 1910.08

S.T. = 338.59

BC = 183+43.22

LA = 670.19

E.C. = 190+13.21

190+13.21 E.C.

20°06'20"

183+43.22 BC

3 338.59

186+43.21

(13)

Def. Angle

STA L. R. DIST

W. side Highway

P.O.T. $\Delta 203+10.08$ $36^{\circ}52'$ $195\frac{1}{2}$ FT

TANG Produced

E. River Bk.

P.O.T. $\Delta 203+10.08$ $31^{\circ}30'$ R

P.O.T.

$201+36.04$

P.O.T.

$201+36.04$ W. Side Highway

P.O.T.

$200+14.25$ E side Highway

P.I.

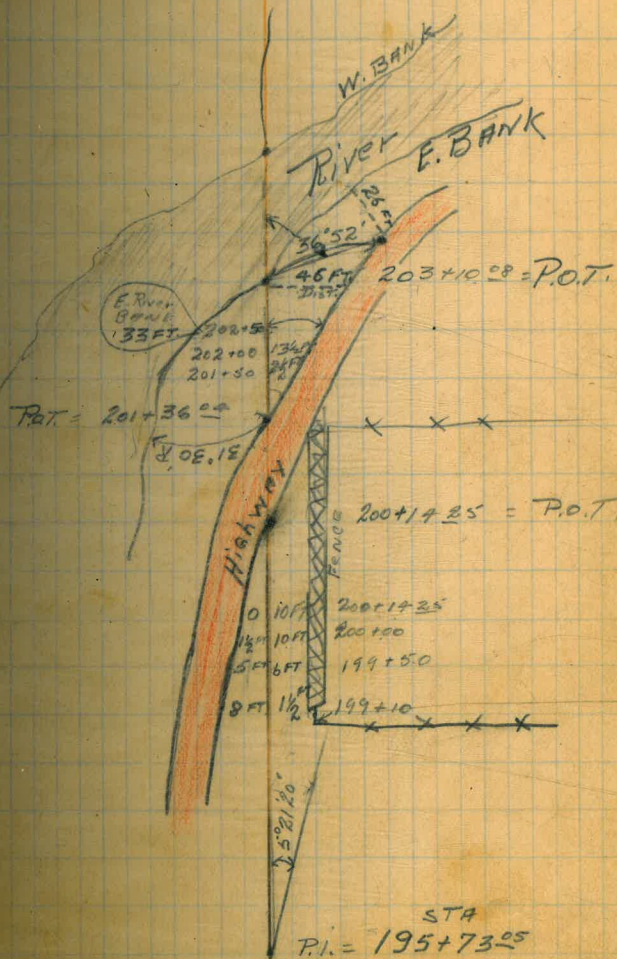
$195+73.25$ $5^{\circ}21'20''$

$N. 15^{\circ}03'58'' E$

(13442)

195 $\frac{1}{2}$ FT

CONTINUED ON
PAGE 18



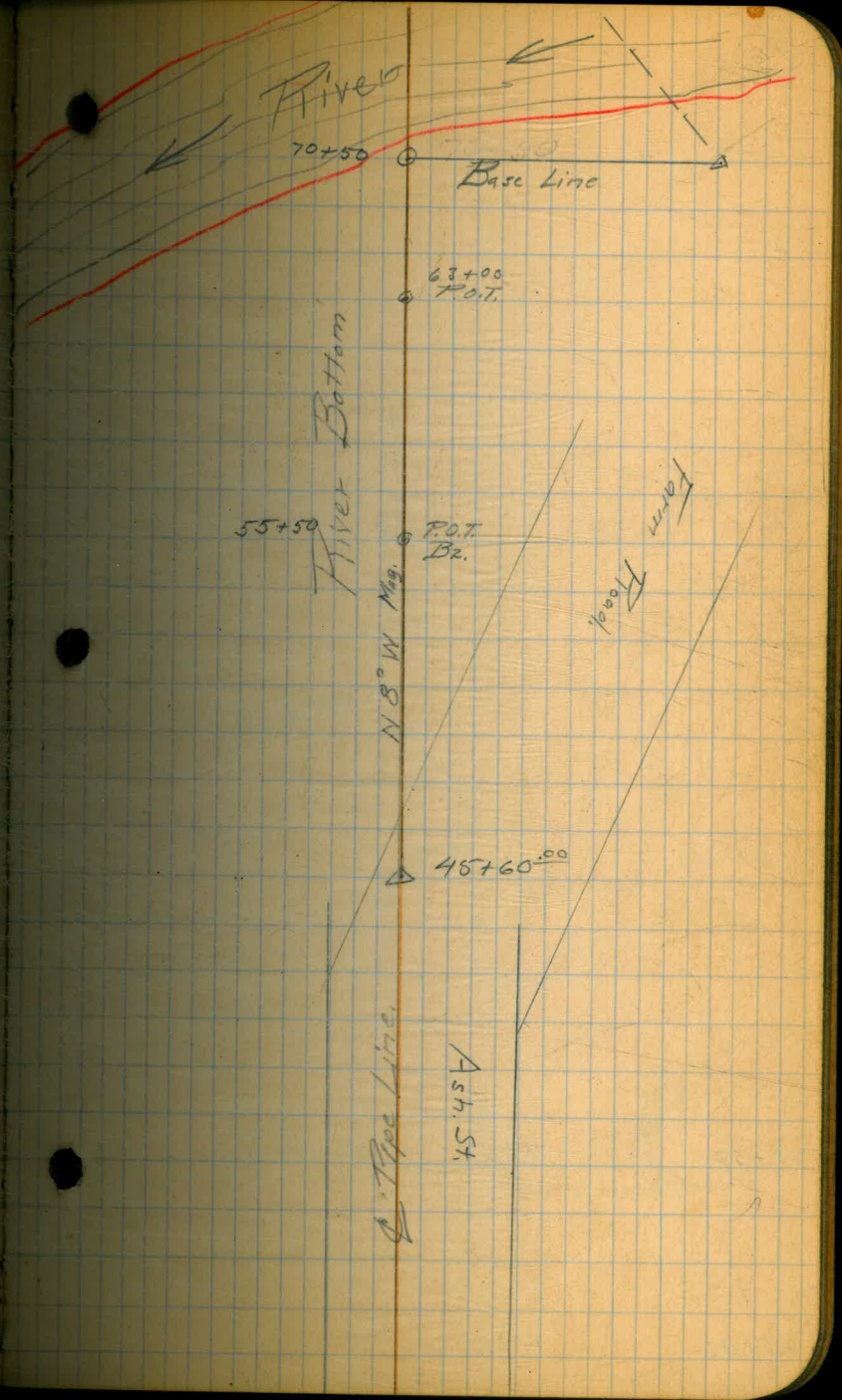
(14)

Relocation of Pipe Line

From Sta. 45+60⁰⁰ on Ash. St.
N 0° 8' W (mag. bear) across river bed
on long tangent.

(15)

Sta.	Dist.	Angle
70+50		P.O.T.
63+00		P.O.T.
55+50		P.O.T.
45+60 ⁰⁰		P.O.T.
35+85 ²⁴		

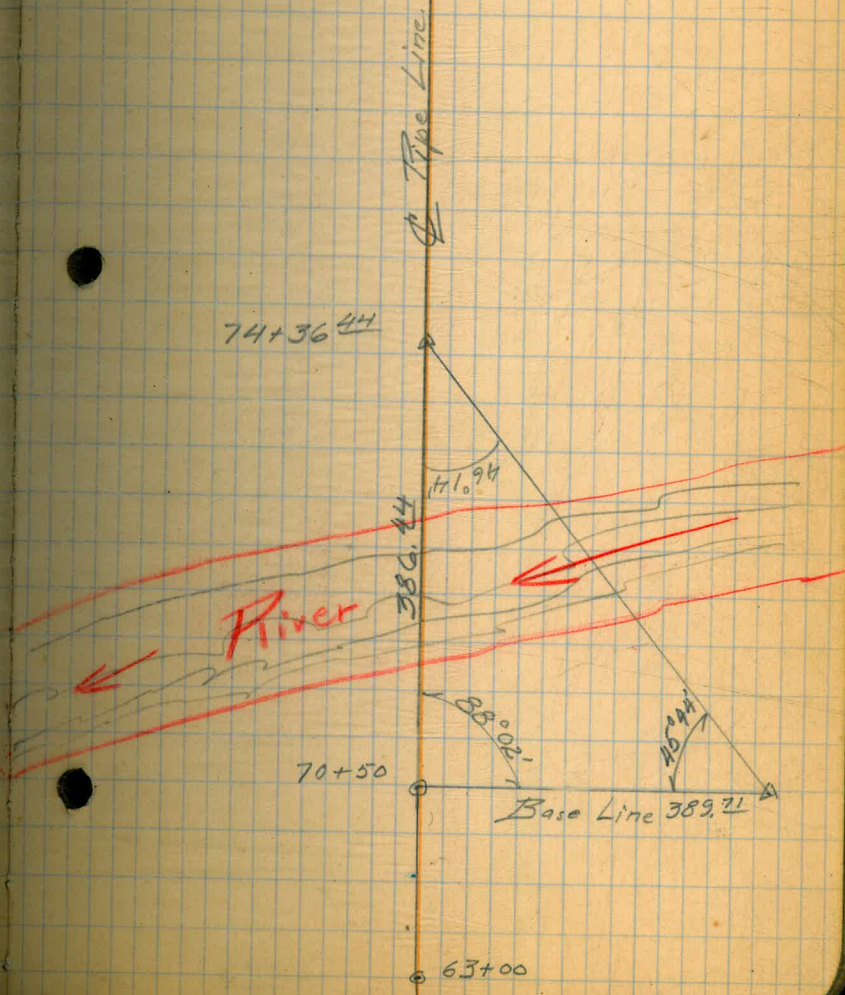


70+50

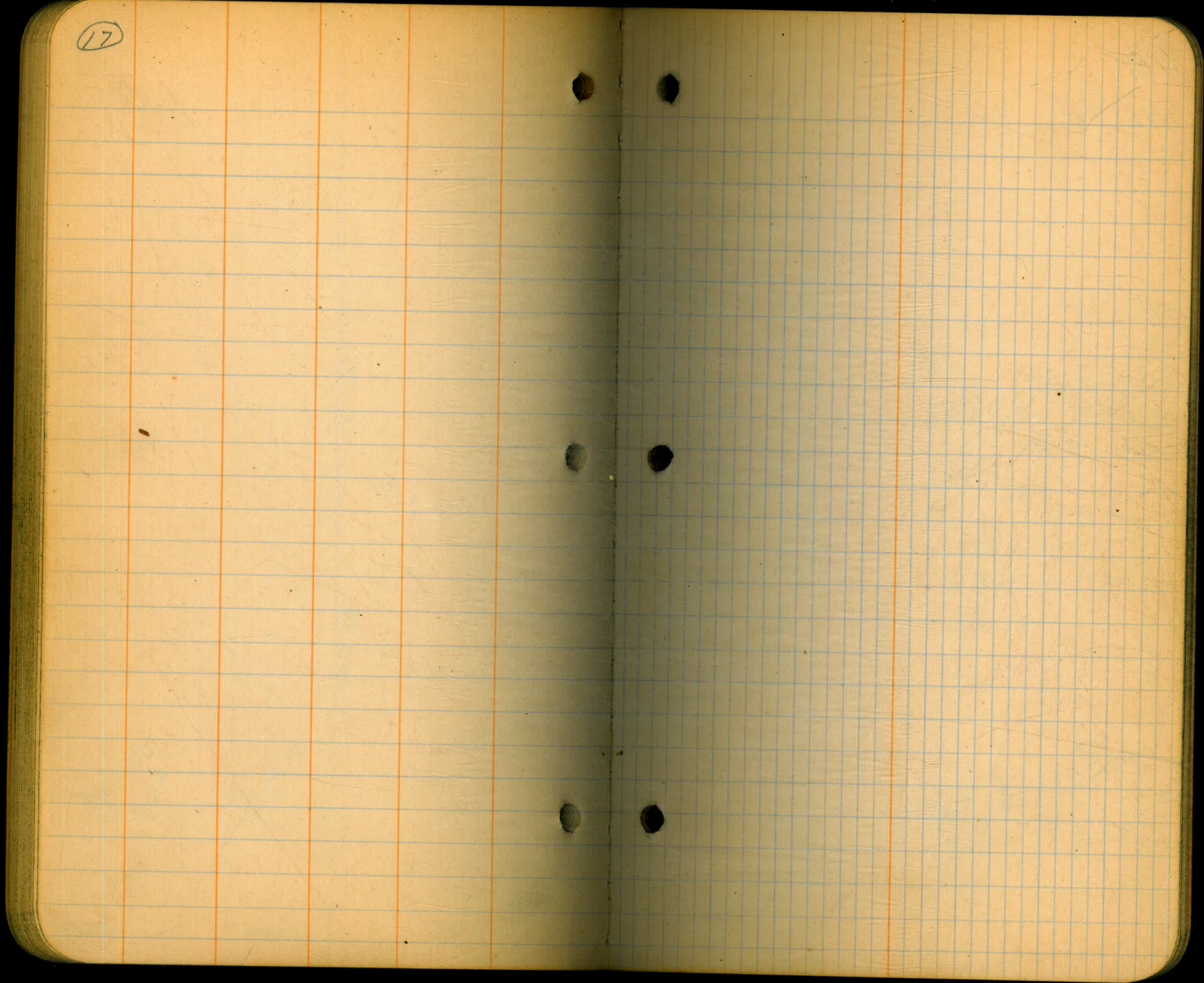
P.O.T.

63+00

P.O.T.



(17)



(18)

Def Angle

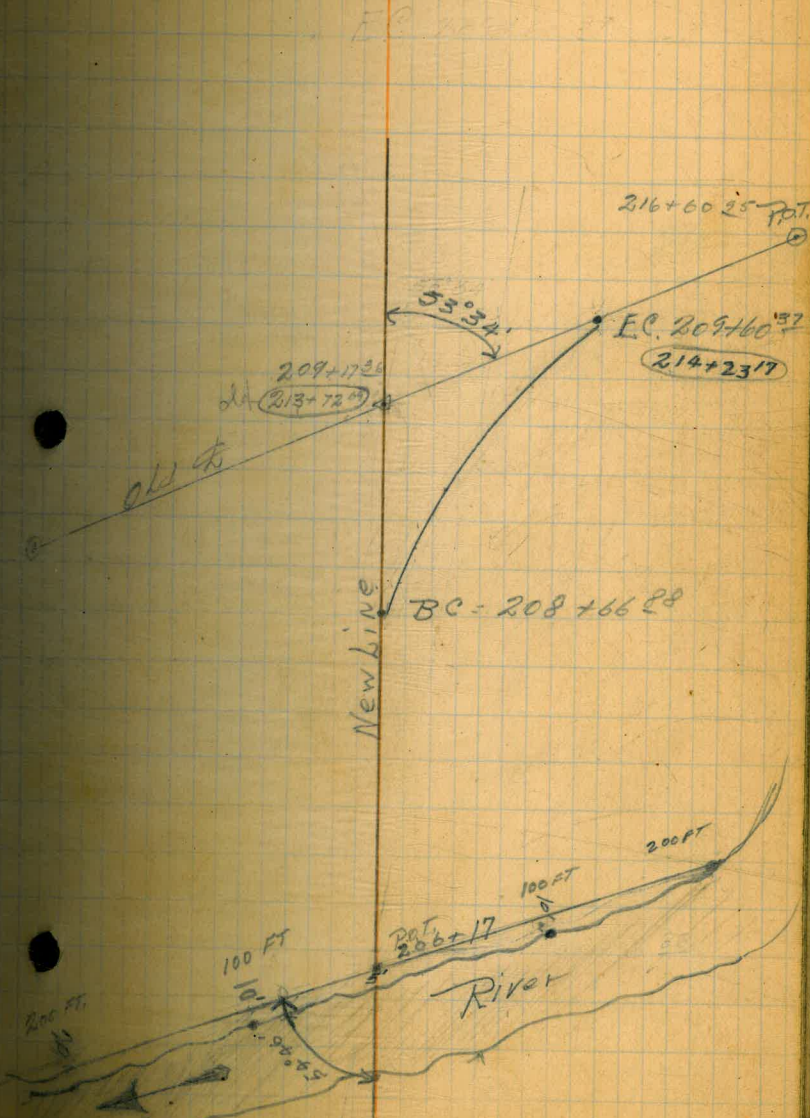
STA. Def. Chord L

N68°37'58"E

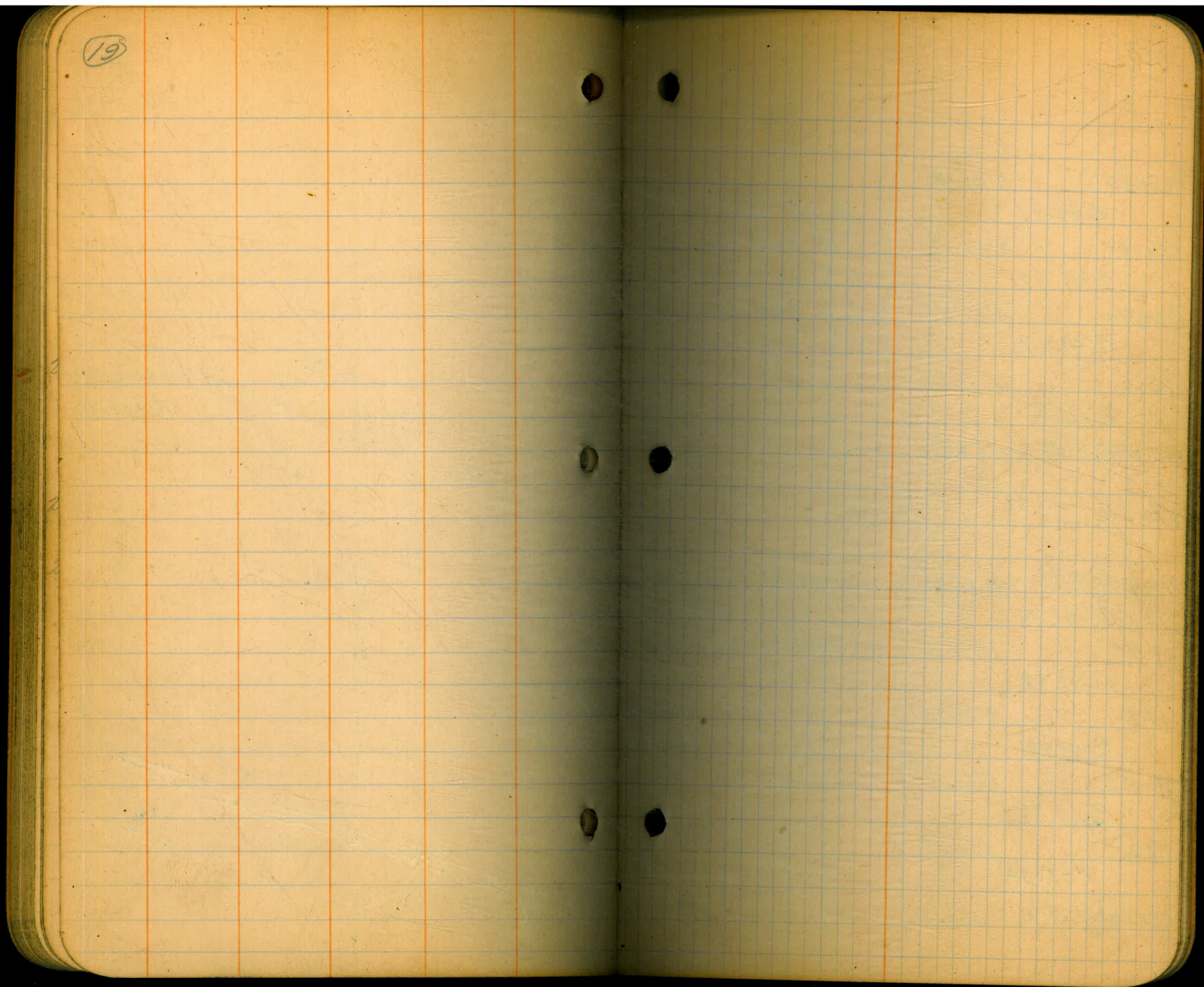
EC	209+60.37	26°47'	
			10.35
	+50	23°48'	
			49.48
	209+00	9°29'	
			32.95
BC	208+66.88		

$\Delta = 53.34$
 $R = 100'$
 $BC = 208+66.88$
 $LA = 93.49$
 $EC = 209+60.37$
 $ST = 56.78$

N15°03'58"E



19



(20)

176+50 $\overset{14.5125}{11^{\circ}21'19''}$
 C-49.97 $\overset{330.06}{}$
 176+00 $7^{\circ}51'13''$
 C-49.97 $\overset{330.06}{}$
 175+50 $4^{\circ}21'07''$
 C-49.97
 175+00 $0^{\circ}51'01''$
 C-12.14
 174+87 $\frac{86}{0}$ B.C. $0^{\circ}00'$
 174+50

$\Delta 35^{\circ}43'15'' R.$
 $R = 409.06$
 $S.T. = 131.81$
 $L.A. = 255.02$
 $P.I. = 176+19.67$

173+90 $\frac{30}{0}$ E.C. $15^{\circ}55'22''$
 C = 40.30
 +50 $13^{\circ}15'35''$
 C-49.98
 173 $9^{\circ}57'22''$
 C-49.98
 +50 $6^{\circ}39'08''$
 C-49.98
 172 $3^{\circ}20'56''$
 C-50.44
 171+49 $\frac{31}{0}$ B.C. $0^{\circ}00'$

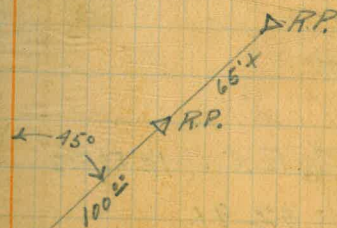
$\Delta = 31^{\circ}50'45'' R.$
 $S.T. = 123.70$
 $L.A. = 240.99$
 $R = 433.58$
 $P.I. = 172+73.01$

21

R.P. Hub+Track $\frac{182}{0}$ $\frac{470}{0}$ $174+87 \frac{86}{0} = B.C.$

R.P. Hub+Track $\frac{182}{0}$ $\frac{470}{0}$ $173+90 \frac{30}{0} = E.C.$

Paved Highway



R.P. Hub+Track $\frac{182}{0}$ $\frac{1942}{0}$ $171+49 \frac{31}{0} = B.C.$

(21)

182+50

182+00

181+50

181+00

180+50

180+00

179+50

179+00

178+50 $\frac{58}{0}$ P.I. $7^{\circ}58'30''$ L.

178+00

177+42 $\frac{58}{0}$ E.C. $17^{\circ}51'37\frac{1}{2}''$

C = 42.91

177+00 $14^{\circ}57'25''$

C = 49.97

EC = 177+42.88

(22)

185775 3°27'22"

185750 3°04'03"

185725 2°42'25"

185700 2°19'56"

184775 1°56'28"

184750 1°34'59"

184725 1°12'30"

184700 0°50'02"

183775 0°27'34"

183750 0°05'05"

183744³⁰/₁₀ P.C. 0°00'

183700

(23)

188+75 7°57'04"

188+50 7°34'35"

188+25 7°12'07"

188+00 6°49'38"

187+75 6°27'10"

187+50 6°04'41" $A = 20^{\circ}05' L.$

187+25 5°42'13" S.T. 338.59

187+00 5°19'44" R = 1911.98

186+75 4°57'16" L.A = 670.19

186+50 4°34'47" 2°59'48" = D.

186+25 4°12'19"

186+00 3°49'50"

(24)

190+14⁵⁴ P.T. 10°02'30" = EC 190+13.77 on page 12

190+00 9°49'26"

189+75 9°26'58"

189+50 9°04'29"

189+25 8°42'01"

189+00 8°19'32"

25

(26)

May 6, 1927

Ferguson

Glover

Lundy

Mattoon

Bush

B4-Line

Pipe Line Location.

Relocation of L from Sta 73+83⁹⁰ on
the B₁ Line, to Sta
on old B Line.

This line goes through the
E. end of an apricot orchard.

Refer to Loose Leaf "B₁" for notes on
old B Line.

Refer to Page 5, this book for
notes on B₁ Line.

(27)

Def Angle

Sta L R

74+22²⁴ EC

P.I. 31
74+03 21°58'

73+83²⁰ BC

$\Delta = \frac{21^{\circ}58'}{10^{\circ}59'}$
R = 100
S.T. = 19.41
BC = 73+83²⁰
LA = 38.34
EC = 74+22²⁴

87+54

County Road.

87+10

P.O.T. 87+03²⁵

B₂ Line

B₁ Line

21°58'

EC = 74+22²⁴

74+03²¹

BC = 73+83²⁰

(28)

Def. Angle

Sta L R

94+22.73
EC

P.I.
94+03.58

22°14'

93+83.93
BC

$$A = \frac{22^\circ 14'}{11^\circ 07'}$$

$$R = 100$$

$$S.T. = 19.65$$

$$BC = 93 + 83.93$$

$$LA = 38.80$$

$$EC = 94 + 22.73$$

B4 Line intersects
old B. line on S.I. of
old B line.

B Line

$$\text{Old EC. } P2 + P3 \frac{38}{95 + 16 \frac{69}{95}} =$$

22°14'

$$EC = 94 + 22.73$$

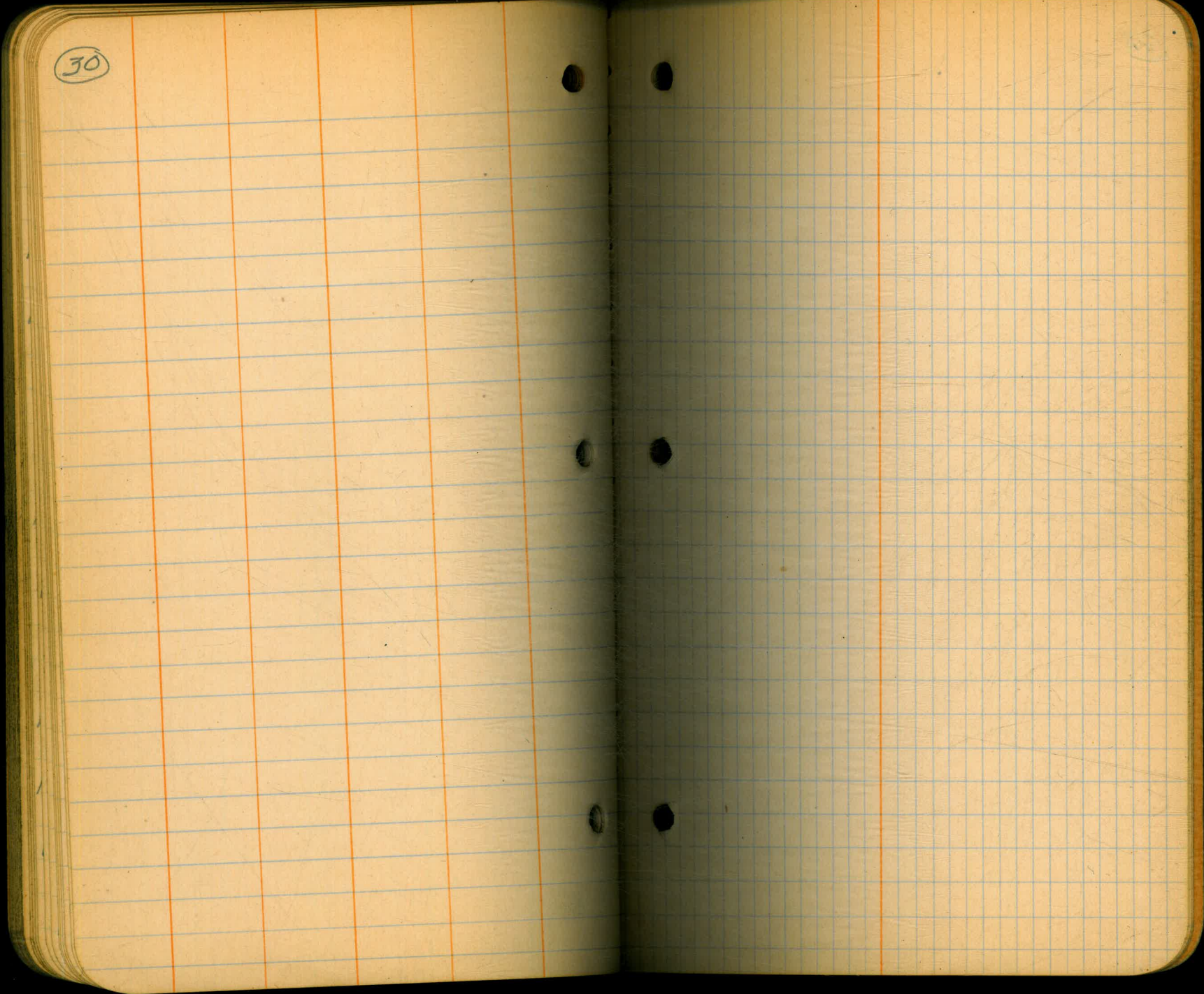
P.I. B4
94+03.58 =

$$BC = 93 + 83.93$$

B4
Line

29

30



(31)

32

33

34

35

125

(36)

$$\begin{array}{r} 171 + 49.31 \\ 1 \quad 2 \quad 3 \quad 70 \\ \hline 172 + 73.01 \end{array}$$

$$56 + 69.68$$

$$53 + 99.81$$

$$\hline 2 \quad 69.83$$

$$60 + 79.88$$

$$58 + 10.05$$

$$\hline 2 \quad 69.83$$

$$53 + 59.17$$

$$4.9 + 24.88$$

$$\hline 4 \quad 34.29$$

$$57 + 69.37$$

$$53 + 31$$

$$\hline 4 \quad 34.37$$

$$60 + 98.63$$

$$57 + 90$$

$$\hline 3 \quad 08.63$$

$$49 + 24.88$$

$$43 + 83.91$$

$$\hline 5 \quad 40.91$$

$$53 + 35.00$$

$$49 + 24.88$$

$$\hline 4 \quad 10.12$$

$$56 + 88.43$$

$$53 + 99.81$$

$$\hline 2 \quad 88.58$$

$$20.63$$

$$\hline 3 \quad 09.21$$

$$406.86$$

$$34.03$$

$$\hline 3 \quad 72.83$$

$$66 + 56.38$$

$$61 + 16.94$$

$$\hline 5 \quad 39.44$$

$$18.75$$

$$34.03$$

$$\hline 5 \quad 92.22$$

$$62 + 6.18$$

$$3 \quad 72.83$$

$$63 + 11.78$$

$$3 \quad 72.83$$

P.O.T. $66 + 84.61$

$$53 + 31$$

$$45 + 81.32$$

$$\hline 7 + 53.68$$

$$174 + 87.86$$

$$1 \quad 31.81$$

$$\hline 176 + 19.67$$

$$61 + 16.90$$

$$60 +$$

$$60 + 79.88$$

$$70 + 94.81$$

$$66 + 84.61$$

$$\hline 4 \quad 10.70$$

$$49.31$$

$$50.69$$

$$\hline 100.00$$

$$60 + 98.63$$

$$58 + 10.05$$

$$\hline 2 \quad 88.58$$

$$20.63$$

$$\hline 3 \quad 09.21$$

W 558