

W 568

43° 35'

City Engr # 1541

**MICROFILMED**

26 32

N 1° 30' E

3° 37'

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
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**THE FREDERICK POST CO.**  
**ENGINEERING and DRAFTING SUPPLIES**  
**IRVING PARK STATION**  
**CHICAGO, ILL.**

# Index (cont.)

Atchison Toll Road Loc.	63-71
Add. topog. Meridian saddle to M3	72
Alternate line M3 to D33	73-75
Alt. lines from above line.	70-78

# Index

154

Page	
1-13	Lower Otay 150' Contour Survey Re Land Exchange Birch & City of SD
14	Levels on Upper Otay Dam
15-16	Ties on Tr "A" " " " "
20-21	Plane Accident. Lower Otay San Vicente Rd Survey.
22	1st Saddle to Foster
26	"C" Line Survey.
29	"S" Line "
32	"M" Line "
40	"M" Line (cont.)
47	N Line
51	"C" Line
51	"L" Line
57	Sec. line ties near Foster
59	Triang. to Keith semiphores.
62	"M" Line Alternate from M-71

LT M4-1 RT

$\frac{-8\%}{100} \quad \frac{+11\%}{55} \quad \frac{+15\%}{75} \quad \pm \quad \frac{-4\%}{150}$

---

$\frac{-19\%}{80} \quad \frac{-6\%}{60} \quad \frac{+2\%}{50} \quad \pm \quad \frac{-3\%}{70} \quad \frac{-7\%}{100}$

opposite saddle M4-5

---

M4-2

$\frac{-21\%}{200} \quad \frac{-9\%}{35} \quad \pm \quad \frac{\text{Level}}{200}$

---

M4-3

$\frac{-22\%}{200} \quad \frac{-9\%}{35} \quad \pm \quad \frac{-3\%}{200}$

---

M4-4

$\frac{-22\%}{150} \quad \frac{-7\%}{45} \quad \pm \quad \frac{+2\%}{40} \quad \frac{\text{Level}}{160}$

---

M4-6

$\frac{-8\%}{100} \quad \frac{-25\%}{100} \quad \pm \quad \frac{+12\%}{100} \quad \frac{+6\%}{75}$

Sta	Stadia	Hgt L	Vert. V	H. I.	Rad.	Mdg. Bem.
To #28		15'13"80" L.				
To #29	B.S. on M4-7	14'29" L.	-4'06'	5.1	5.1	N. 63° E.
To #18		13'56" L.	-3'22'	5.1	2.1	N. 63° 30' E.
To #17	B.S. on M4-4	30'55" 30" R.	-4'46'	4.9	5.9	N. 77° 30' E.
To #16		30'55" 30" R.	-6'35'	4.9	8.9	N. 77° 30' E.
To #15	B.S. on M4-2	18'00" R.	-2'55'	5.1	8.1	S. 46° 30' W.
To #14		0'00'	-2° 57'	5.1	10.1	N. 46° 30' E.
To #13		0'00'	-3° 59'	5.1		N. 46° 30' E.
To #12	B.S. on M3-4		+1'56'	5.1		
To #11		0'00'	-0'45'	5.1		
To #10	B.S. on M3-3			5.1		

Lt

M<sup>4-7</sup>

Rt

$$\frac{-69}{100} \quad \frac{-129}{65} \quad \frac{319}{65} \quad \neq \quad \frac{+289}{50} \quad \frac{+139}{75}$$

Lower Otay Res. 150' Contours

	11.60	150.93	139.33	El. water Res. gauge Aug. 31-37
T.P. 1/2" Rev.		0.93	150.00	

R.S. # 558

USGS

El. check of water at 633+00

0.36 497.31 496.95

USGS  
Spike in  
Fence Post

10' W. of E. of Rd. approx. 633+00

El. of Lake Aug. 31-37 11.42 485.89

Set B.M. 4.40 492.91

Set B.M. Ely. Cor. of conc. base of Garbage Stand,  
approx. 50' SW of above B.M.

Contour check levels from Res. Gauge Aug. 31-37

16.35 155.68 139.33 Res. Ga. Aug. 31-37

# 294 Hub 2x2 c.T. 2.98 152.70

# 295 " " " 2.95 152.73

# 292 " " " no good 2.37 153.31 (?)

# 289 Top of Hub rotted away 2.85 152.83

# 288 Hub 2x2 c.T. 3.11 152.57

Check USGS to 150' Contour A # 358

BM USGS 5.66 502.61 496.95

T.P. 10.38 507.81 5.18 497.43

on old 2x2 Hub # 358 7.15 500.66

USGS  
Spike  
in fence  
post

10' W. of 633+00

Otay Lake 150' Contour Ties  
to R.S. #558.

Contour & pts #292 and #293

NOTE!

See County Books  $\frac{685}{228-7}$  for other ties

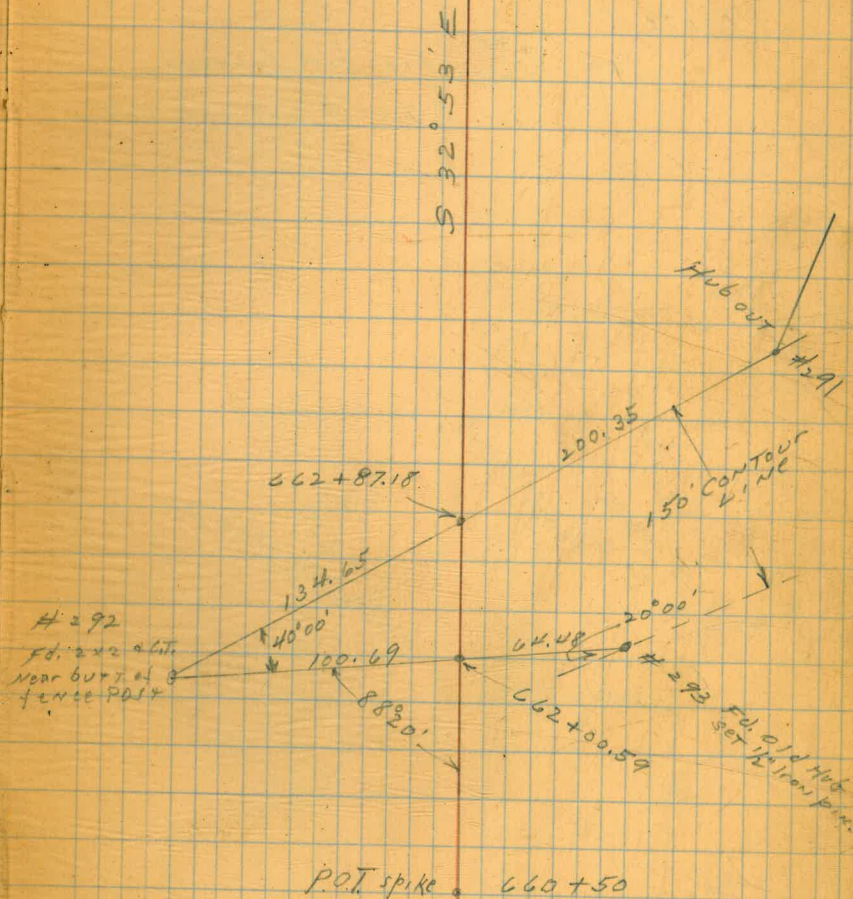
" " "  $\frac{726}{234-13}$  " " "

" " " BK 717 p.5 for xsec.

Williams  
Moore  
Jensen  
Northern  
8-31-37

R.S. #558  
OTAY RES.

2



OTAY Lake 150' Contour Ties  
to P.S. #558

Note!

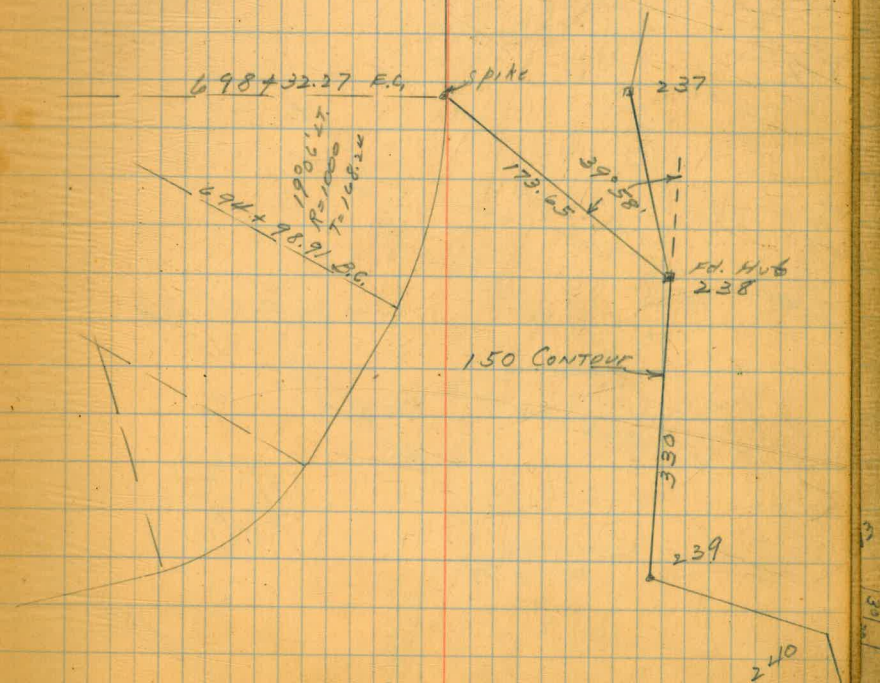
See  $\frac{685}{223-7}$  P13 for Contour  
Ties # 227 and 228

P.S. #558

3

579°23'E

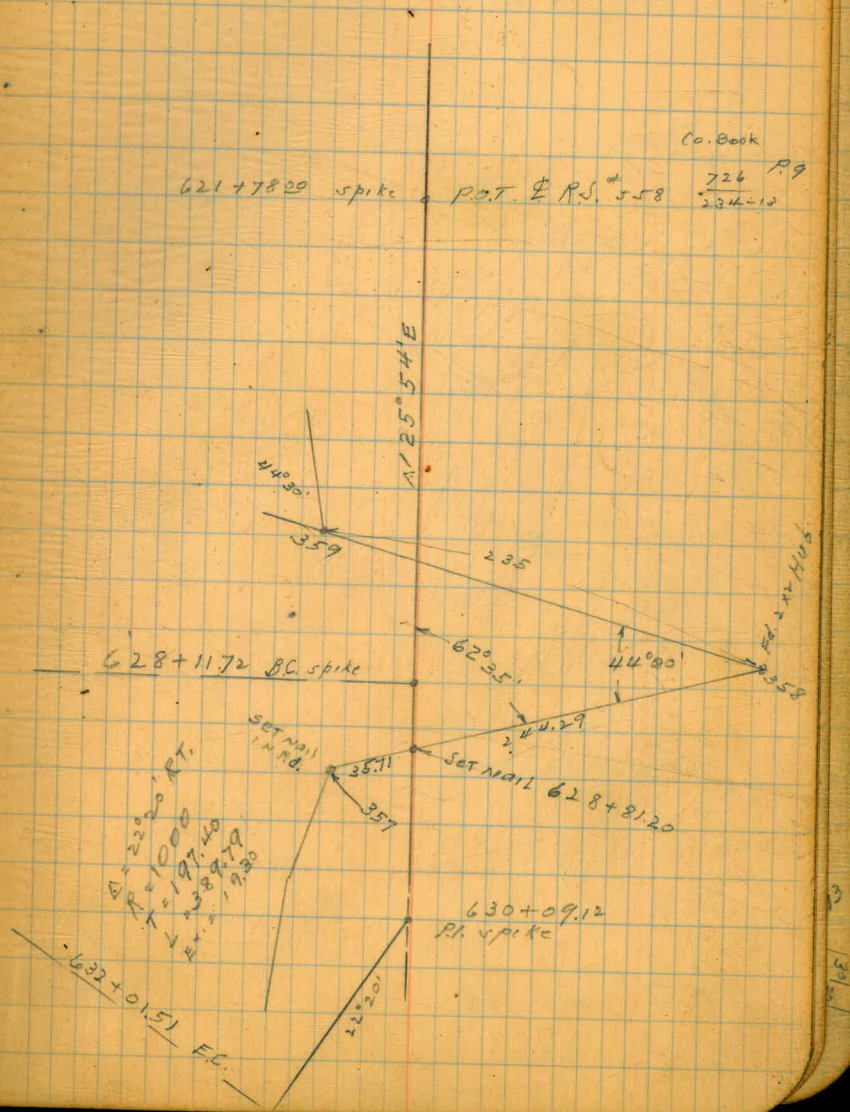
see Co. Bk.  $\frac{685}{223-7}$  P8





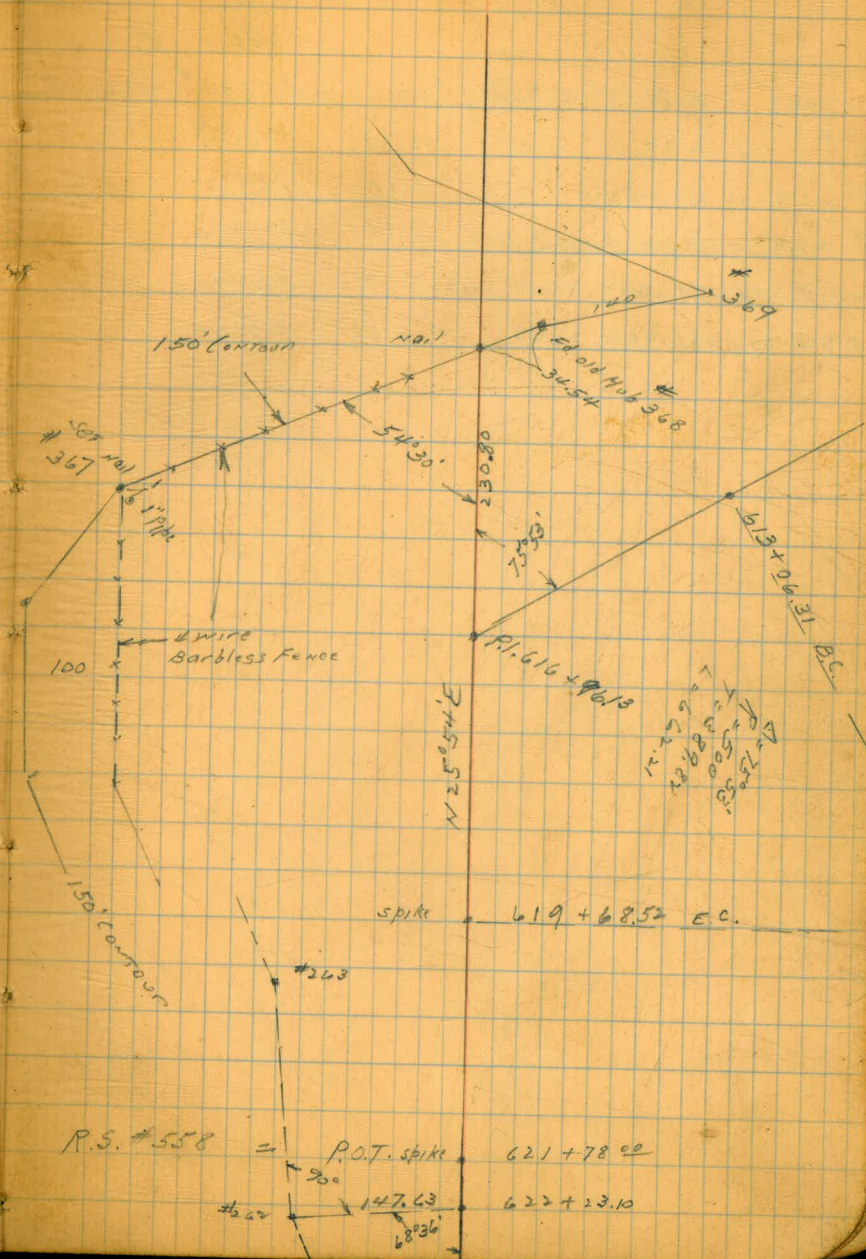
Otay Lake 150 Contour Ties  
to P.S. #558

Contour Δ pts. 357 + 358



150'  
 Otay Lake Contour TIES  
 to R.S. #558

Ties to Δ pts #367 & 368



Check Levels U.S.G.S. To 150' Contour

Δ pts. # 228 + 229

28' LT. of				U.S.G.S.	OK.
716+50	5.80	513.15		507.35	B.M.
T.P.	1.90	503.87	12.18	500.97	
# 229 on old 1x2 Hub			4.26	499.61	
# 228 " 1/2 pin driven Hub			4.14	499.73	
on 2x2 RW Hub. Iron CONCAVE Tack	2.42			501.45	
El. atay Lake Sept. 2-37	17.85			486.02	

Iron pin U.S.G.S. see Co. BK.  $\frac{6.56}{524-12}$  p 58

used by Judson at #227

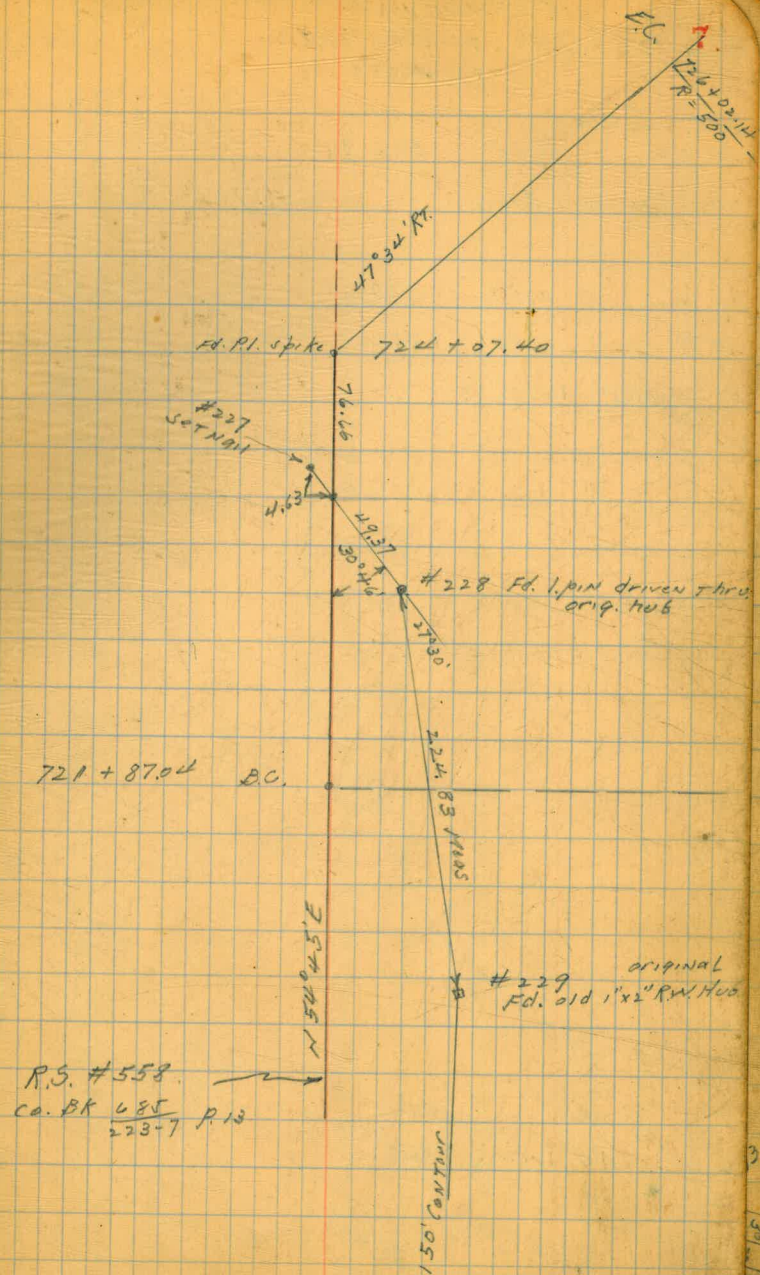
Not Original Hub  
Do NOT check this  
see page 7 for Tie

3/21/37

Otay Lake 150' Contour Ties

# 228 + 229 to R.S. 558

See  $\frac{685}{223-7}$  p 13 for ties to #227  
which Rancho Line has been changed  
from original.

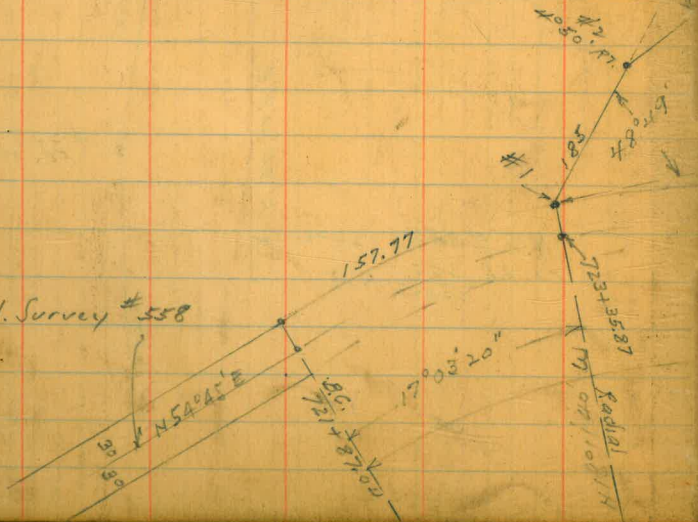


Estuary Ties & Survey

Sta. 723+35.87 to 728+16.20  
 Co. R.B. 685 P13  
 R.S. #558

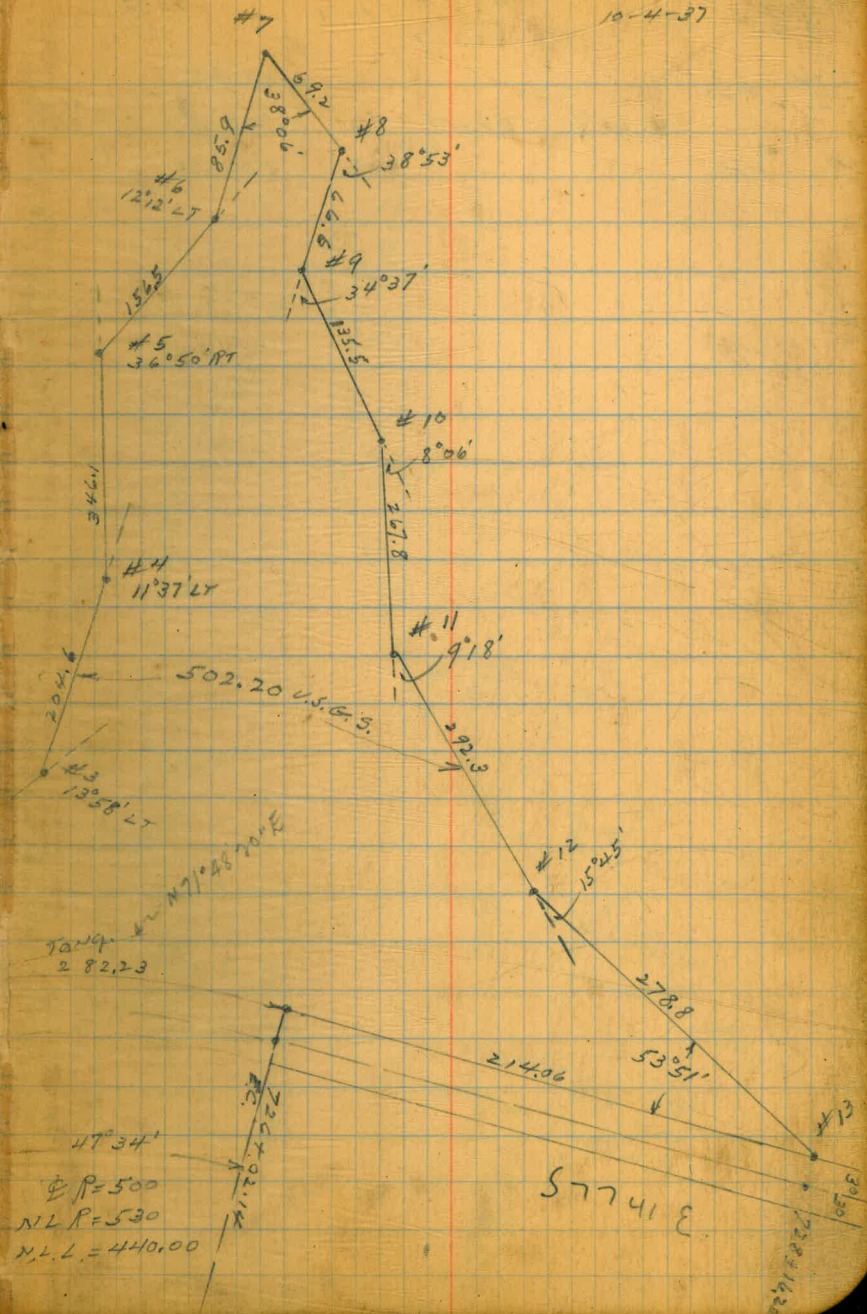
B.M. $\times \times$ Hub Iron Concave tack				U.S.G.S.
See p 6	5.45	506.90		501.45
NEW CONTROL Elev.	4.70			502.20
	0.89	502.04		501.45
T.P.	2.30	491.68	12.66	489.38
El. water Oct 5. 37		7.08		484.60

Rd. Survey #558



Savage Dam

Moore  
 Wilson  
 Northern  
 10-4-37



47°34'  
 E.P. = 500  
 N.L.P. = 530  
 N.L.L. = 440.00

ESTUARY TIES & SURVEY  
Savage Dam

Co. Level Bank

R.S. #558

$\frac{685}{223-7}$  P. 15

$\frac{654}{224-12}$

$\frac{654}{224-12}$  P. 63

4.80 508.47

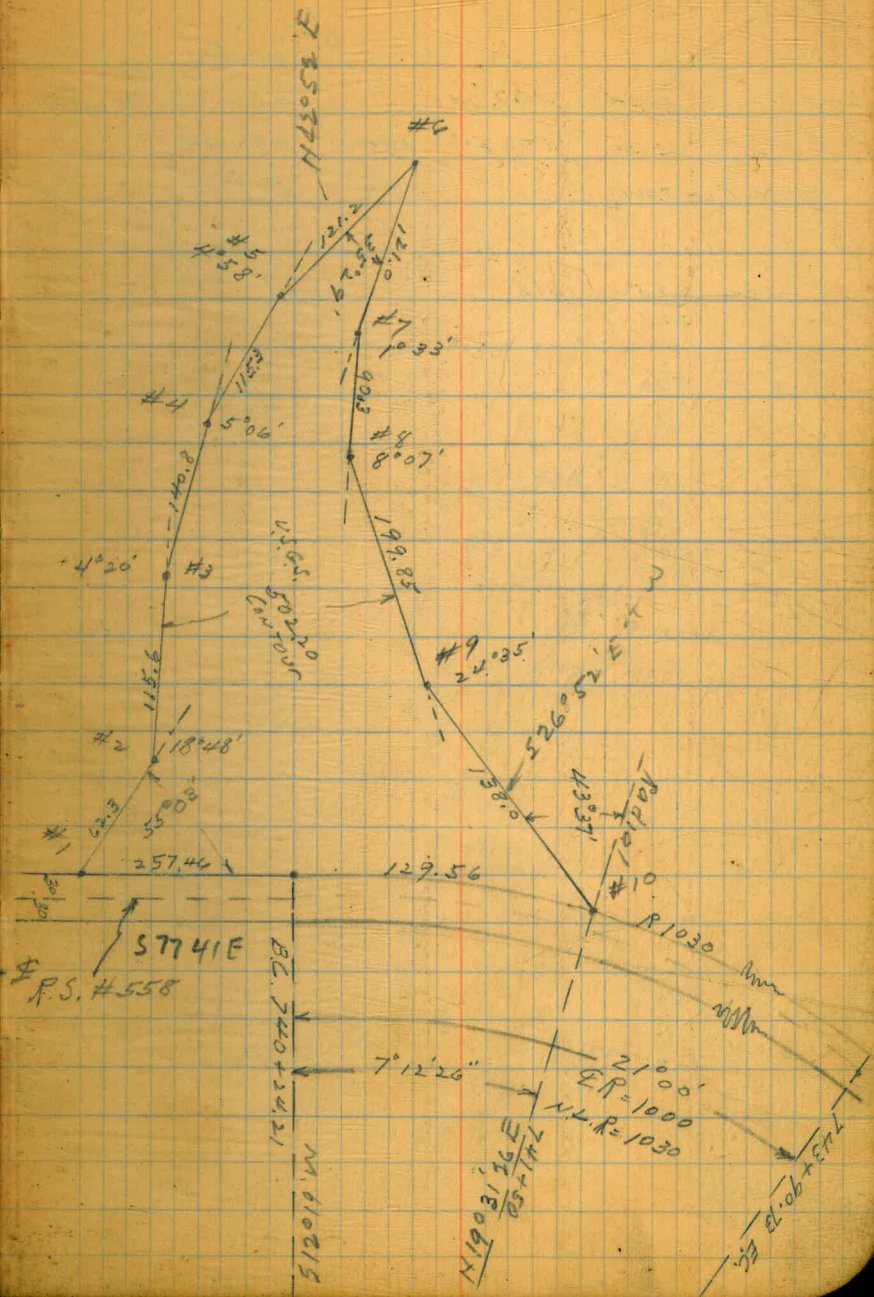
V.S.G.S.

503.67 BM IRON PIN

#1  
T.P. on Hub

6.27

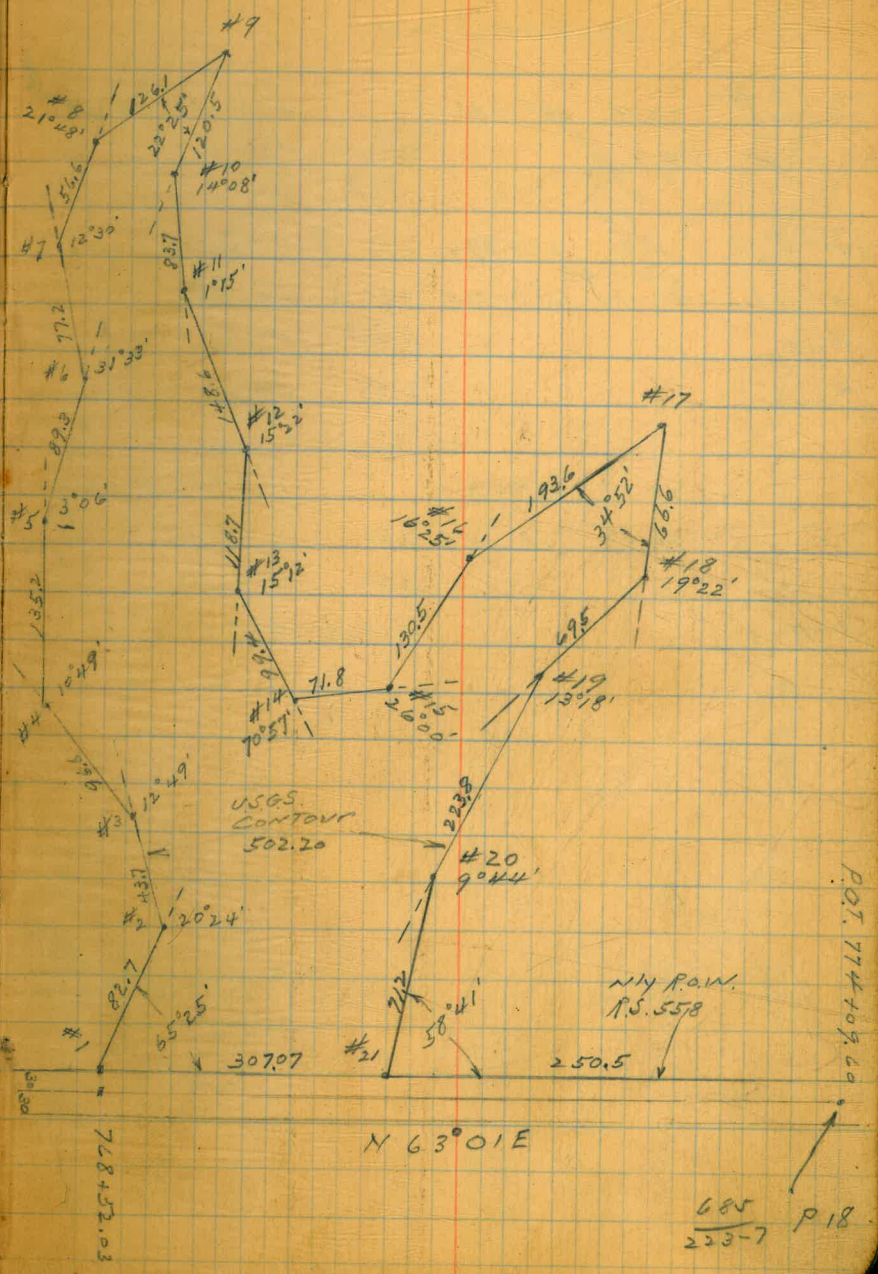
502.20



ESTUARY TIES + Survey Moore  
 Otay Lake (Savage Dam) 10-5-27  
 R.S. #558

	USGS	El. Water
Seep 8	1304	497.64
T.P.	12.30	50624 370
NEW CONTOUR	404	50220

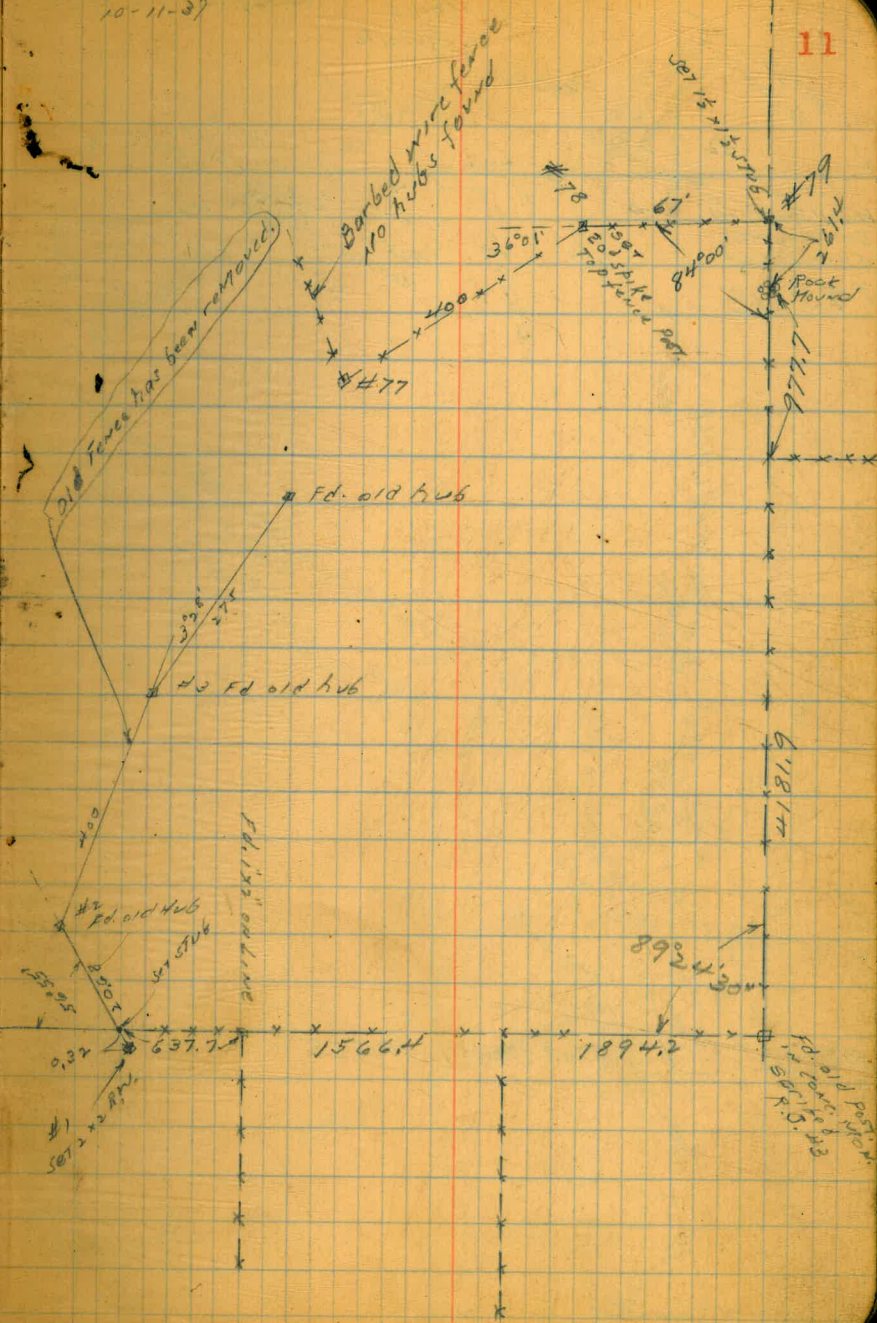
see 685 p18  
 223-7



Ties to Original 150' Contour of  
OTAY LAKE and Ely + Sly Lines  
of Rancho Javal

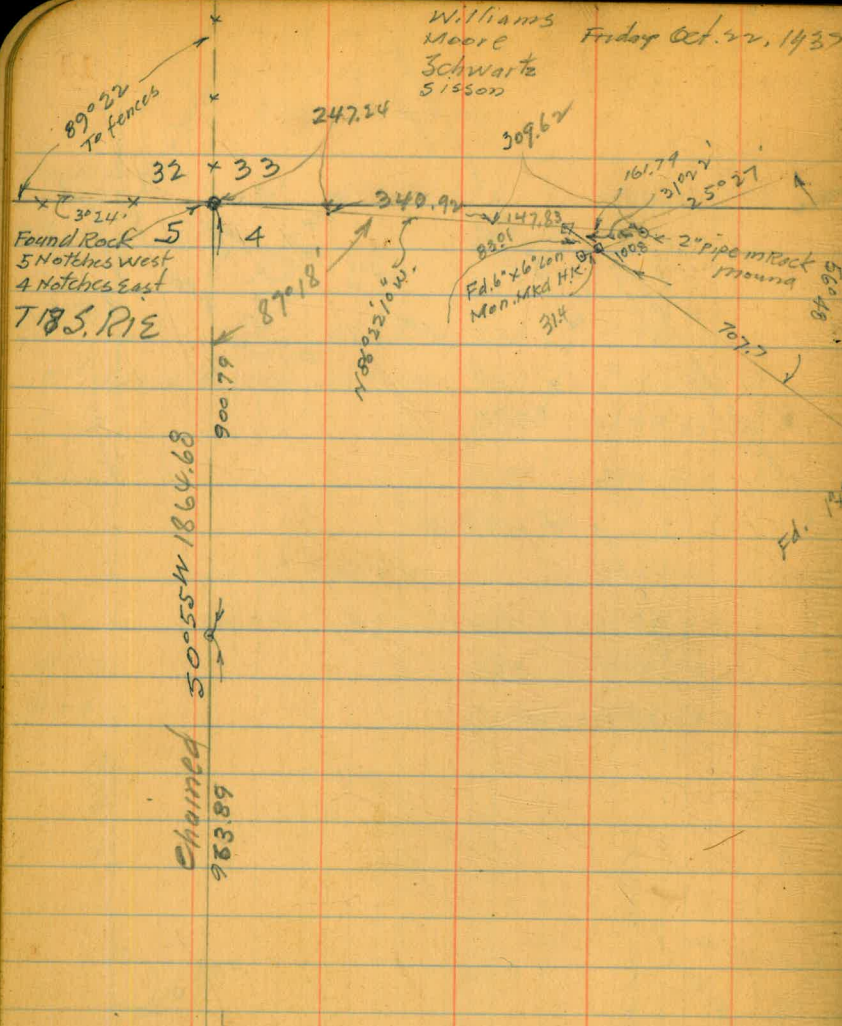
Top of Roadway on DAM	12.75	504.95		492.20	U.S.G.
El. WATER OCT. 11, 37			20.34	484.61	
T.P.	10.25	507.57	7.63	497.32	
Jan. 1917					
#1 of Lower OTAY RES 150' Contour		650		501.07	
#2		7.80		499.77	
#3		7.53		500.04	
<hr/>					
U.S.G.					
12.11'		496.71		484.60	El. WATER
T.P.	10.67	504.67	2.71	494.00	10-11-37.
#78			5.30	499.32	
#79			5.10	499.52	

Moore  
10-11-37





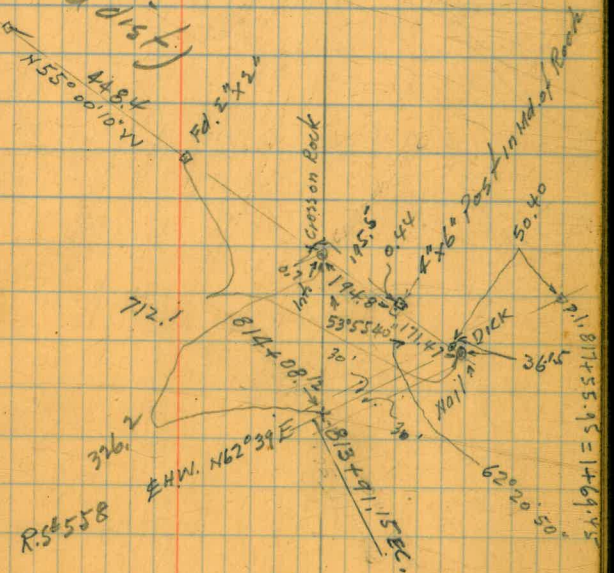
Williams  
Moore  
Schwartz  
Sisson  
Friday Oct. 27, 1937



Jamal  
Rancho

1/4 Sec. Cor  
Found Mkd Rock  
In Rock Mound

Studia (sec chained dist)  
586  
Pd. 2722  
Pd. 2722  
Pd. 2722  
Pd. 2722  
N 55° 00' 10" W  
448.4



588° 09' E Road survey No 558

562° 39' W
62 20 50
126 59 50
179 59 60
55 00 10

(H.K. = H. Kurnstead Surveyor)

1/4 Sec. Cor



Levels on Upper Otay Dam  
for Res. Cont 72.4

Nov. 18 1937

William J.W.  
Moore Chas.  
Sisson A.  
Northern Geo.  
Schwartz

14

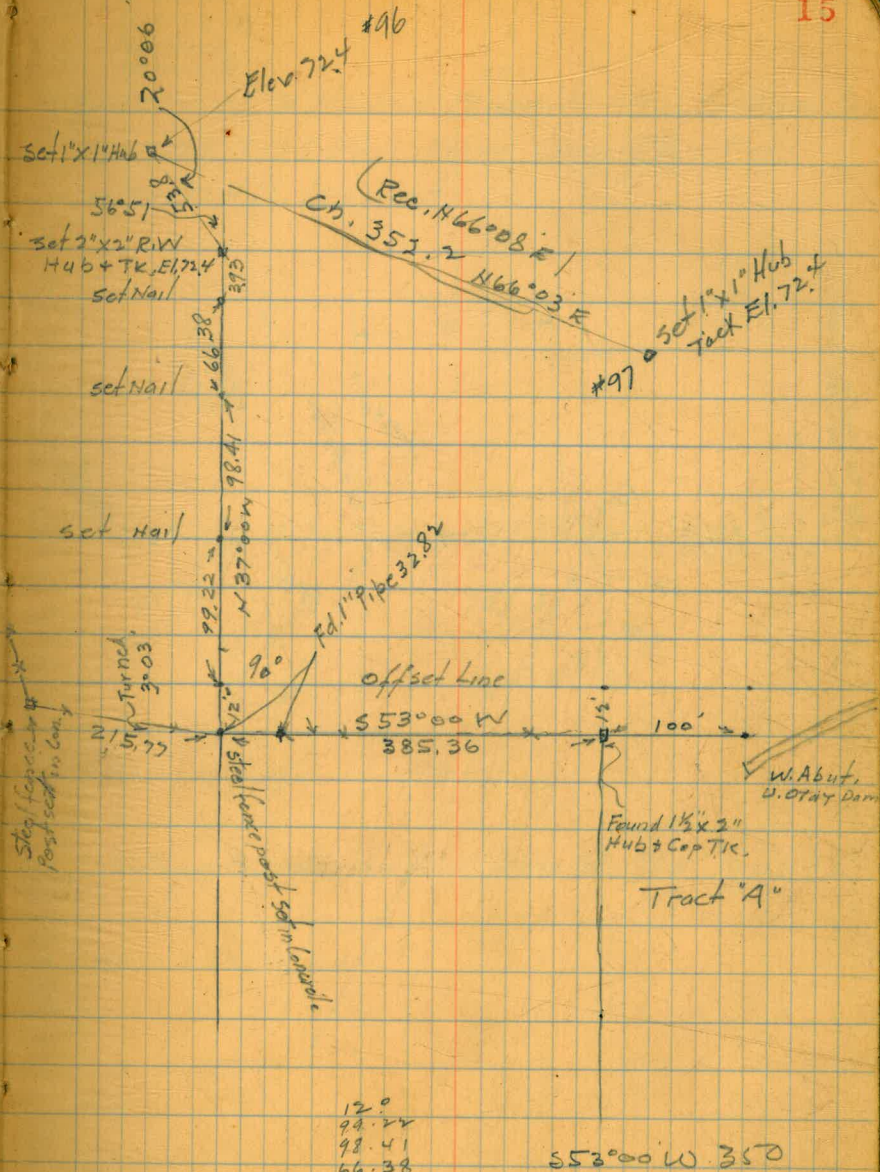
	T		E.L.	B.M.
4.91	82.11			77.2
		7.99		
		9.90	72.21	
		9.71	72.40	
4.85	77.25	4.85	72.40	
5.25	77.65	3.80		

Top Dam W.E. Rod 4.88 Center Rod 4.91 E. End Rod 4.91  
Lowest of 3 Notches in Dam 7.99 7.82 7.93  
Tip of New Spillway East end Dam  
Set Hub.

Williams, J.W.  
Mason Chas. Ch. Party  
Sisson A. Invt.  
Northern Geo. Co.

R.A. Schwartz  
11-18-37

Survey of Ties from Tract "A"  
Upper Clay Dam to Res. Cont. 724



Stop tape at Post set in cont.

12.0
98.22
98.41
66.38
3.93
279.94

552°00' W 350

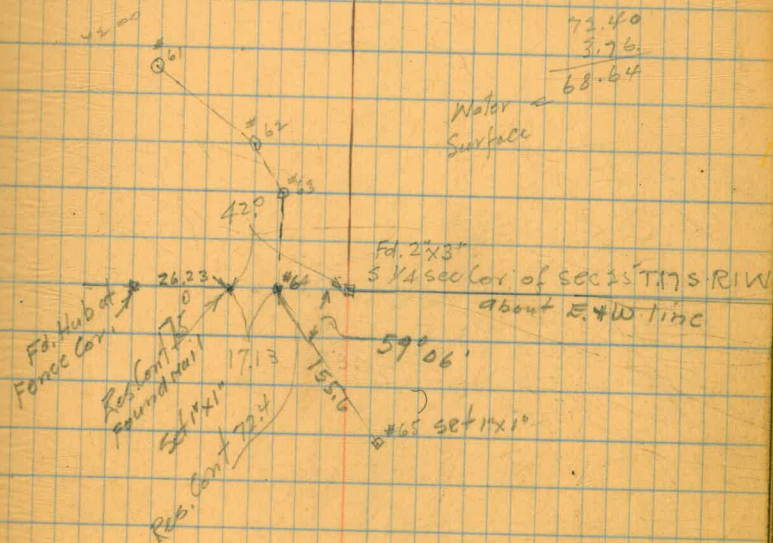
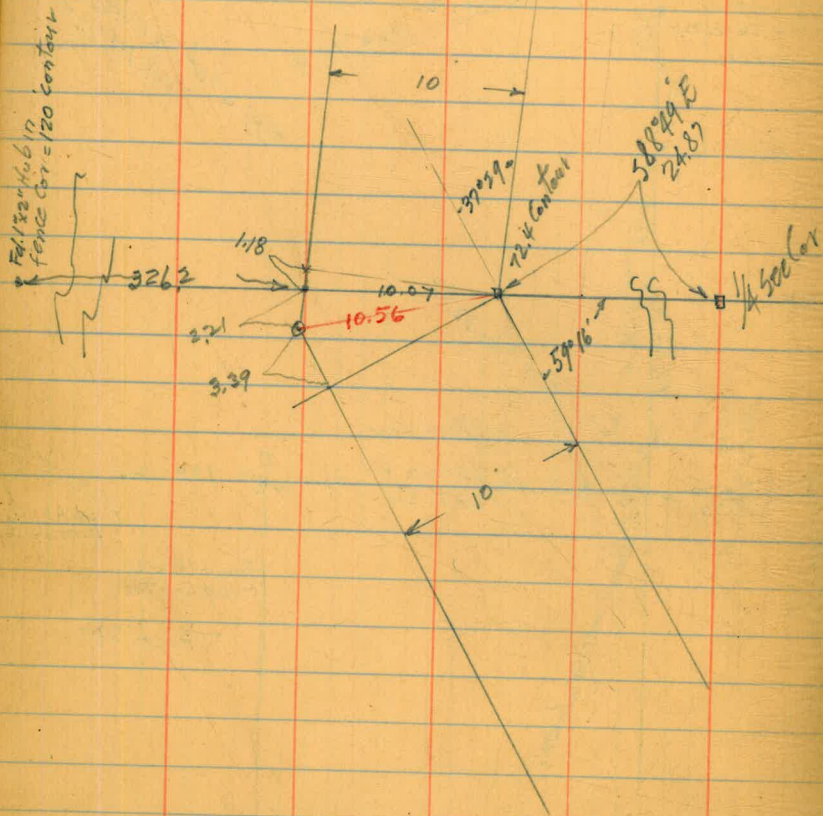
Williams  
Moore  
Dyson  
Northern  
Schwarz

11-18-37

16

Survey of M. Haubert Property & Ties to 1/4 Sec. Cor  
Sec. 25, T17S, R1W, S18M Upper Clay Res.  
also 72.4 ft. Res. Cont.

$\frac{59.2}{22.6}$   
3.76



Distance to Water Surface from Sta. #64. Horiz. 22'

Flow Lake 68.9

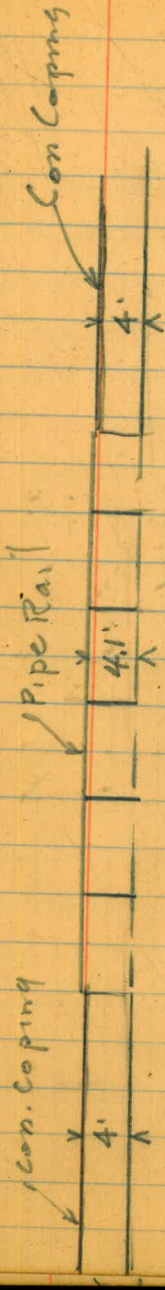
Res. Ga. 68.70 Sat Nov. 19. 1937  
B.M. 68.74 " " " "







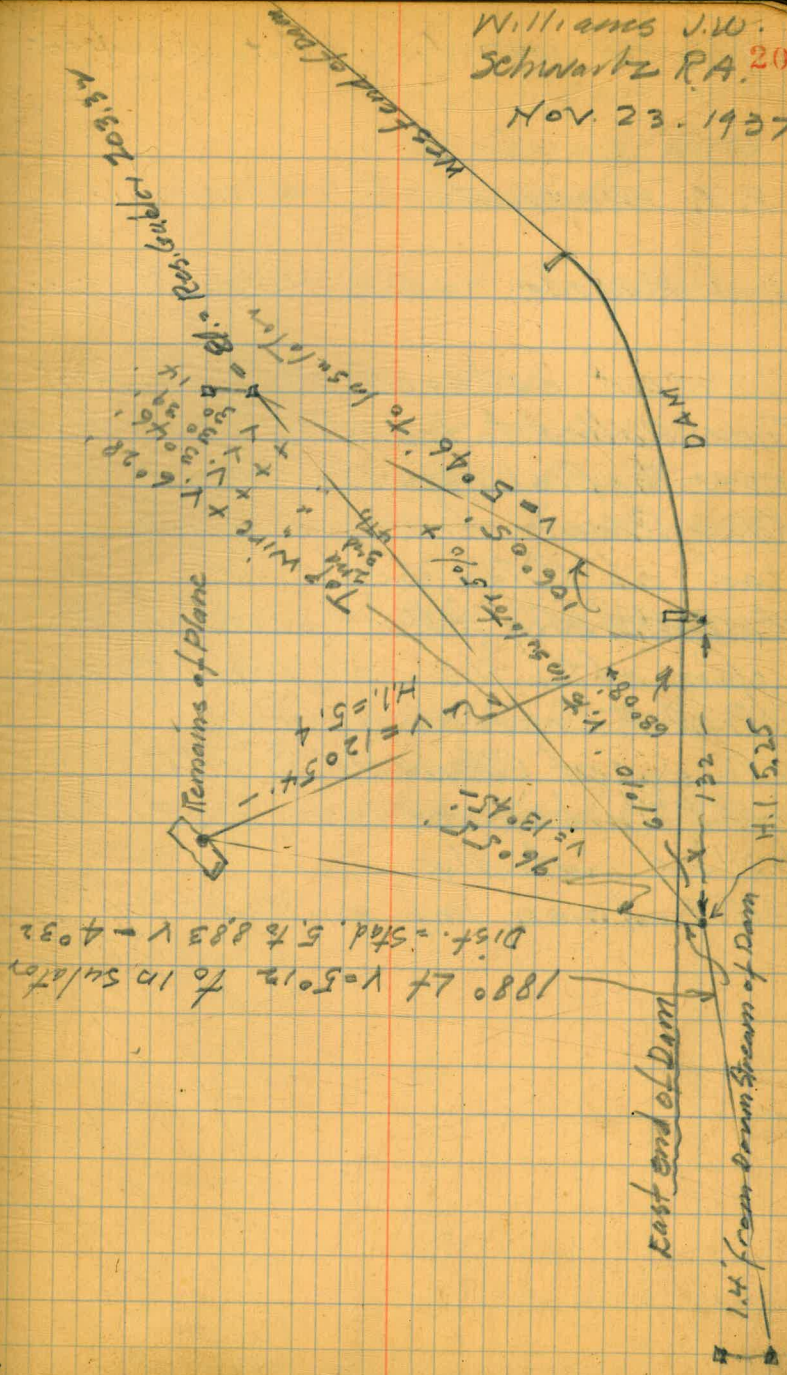
# Lower Otay Plain Disaster



fall intercept

Williams J.W.  
Schwartz P.A. 20

Nov. 23. 1937



Nov. 20. 1937 Visibility perfect

F. X. McGrath S. D. Naval Airport

E. J. Holze S. D. Naval Airport

accident occurred at 11.45 AM.  
They called to I. D. Miller assistant  
how the fishing was then headed  
Otay Creek and flew into wire  
bed of Otay Creek

Mr Bittelburg filter operator at L.O.  
plain after the accident then I. D.

Mr A. F. Crowell notified R. G. Mues  
McCauley at Chula Vista who arrived  
Naval <sup>Hospital</sup> Ambulance last one to arrive  
killed instantly

F. H. Eastman. Inf. on Nov. 23. 1937.

Sun shining. (Flying too low <sup>21</sup>  
Just cleared railing on  
Dam flew into Wires  
Riding Died immediately

Pilot Died about 1 hr. afterward

Saturday Nov. 20. 1937

keeper on the lake asked him  
down over the dam south over  
he saw them fall into rocky

was first to reach the wrecked  
Miller next.

te immediately and then called Dr  
in about 30 minutes  
22d man was then dead 1st man

Line from first saddle to Foster

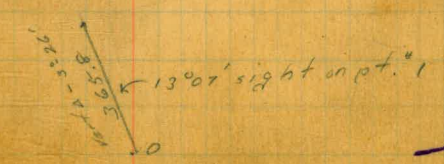
6/3/38 Williams Hill Osborn Isbell

22

Sta.	Cor Dist	Hor. Δ	Vert. Δ	H.I.	Elev.	Mag. B.
3+5	572.0 (573)	10°23' L	-3°26'	5.0	884.3 884.4	S13°00' E
3+4 (not a fence pt.)	412.0 (413)	10°35' L	-3°26'	4.9	724.7 918.7	S13°00' E
2+3	168.4 (168)	1°54' L	-3°26'	5.2	-10.1 913.1	S3°00' E
1+2	387.8 (388)	25°02' L	-3°26'	5.2	-23.3 913.1	S1°00' E
0+1	1057.5 (1060)	13°07' R	-3°26'	5.0 H.I. 15.0	-73.4 976.6	S. 23°00' W



o Point on saddle Elev. 1050 (Aneroid)  
 Note called grade for 6% survey  
 1040 making 10' out in saddle  
 See Page 47 for N.L.



Sta. Cor. dist. Hor. A Vert. A H.L. Elev. Mag. B.

cont. in book #239

7 to 8	84.7 (107)	21°39' L	-3°26'	5.1	-5.1 875.1 <del>873.8</del>	S 7°00' W
6 to 7	198.3 (199)	16°24' R	-3°26'	5.1	-14.0 883.2 <del>878.9</del>	S 71°00' W
5 to 6	230.2 (230)	27°33' R	-3°26'	5.2	-13.8 875.1 <del>870.7</del>	S 14°00' W

June 7. 1938

24

0+00 to 4000 + 3 1/2 %

B Line 5%  
Station Cor. dist. Horiz. Vert. H.L. Elev. Mag. B.

6/9/58

cool

Williams  
Hill  
Osborne  
Isbell  
Leakey

25

Abandoned

0

(105)

-2°52

5.1

S. 60°30' W

1/9/38

C Line - 6% From saddle about 1 mile S.E. of Apiary 26

Station Cordist Hora Vert. Δ H.I. Elev. Mag. B. Diff. Elev. Eley.

7 to 8 97.6 (197) 15°20'R -3°26' 10.0 -15.8 S89°30'W (grade) -38% 125' -50% 60' +34% 150' sta. 8

5 to 7 271.0 (271) 52°55'L -3°26' 5.0 -11.0 S71°W (c.s.o.) -40% 150' -39% 90' +24% 125' sta. 7

5 to 6 125.5 (125) 3°57'L -3°26' 5.0 H.I. 15.0 rd -17.5 (F.s.o.) -17% 125' +39% 100' 120' 100' sta. 6

4 to 5 86.7 (86) 25°16'R -3°26' 5.0 H.I. 0.0 rd 0 on line from 5 to 7 -44% 70' +23% 65' N55°30'W (c.s.o.) -44% 70' +40% 125' sta. 5

3 to 4 143.5 (143) 43°51'R -3°26' 5.0 -8.6 N80°W -8% 90' -58% 70' +45% 125' sta. 4

2 to 3 65.8 (65) 14°55'R -3°26' 4.5 -3.9 S55°30'W -47% 150' +39% 100' "C" 2 El. 11687 sta. 3

1 to 2 389.7 (390) 10°12'L -3°26' 5.0 -27.3 S 10°20' W +15% 150' +34% 100' -46% 125' +31% 50' +22% 100' sta. 2

1149% +21% +12% -12% -29% +18% -13% 155' ft. #1 to #1A

+27% -1% +20% -22% +19% +14% sta. 1

100 125' 90' 90' 65' 100' +31% 125' +2% 35' +10% 75' sta. 0

0 to 1 285.0 (285) -3°26' 5.0 -17.1 S 50°W Pt. 0 = saddle S.E. of bee man's place. Aneroid 1175.

C Line (cont.)

Sta.	Cor dist	Hor. Δ	Vert Δ	H.I.	Elev	Mag. B.
15 to 16	66' (68')	137°08'R	+11°08'		1106.9	(Cut 10.0)
14 to 15	210.3 (210)	20°21'L	-3°26'	4.7	1096.9	S. 83° W
12 to 14	170.4 (170)	29°07'L	-3°26'	4.9		N 77° W
12 to 13	109.6 (109)	22°05'L	-3°26'	4.9		
10 to 12	289.0 (289)	5°26'L	-3°26'	12.5		N 18° W (grade)
10 to 11	226.2 (226)	7°40'R	-3°26'	12.5		(grade)
9 to 10	222.2 (222)	13°56'R	0.0	Rad 10.9 H.I. 5.00	-5.9	N 43° 30' W (C. 7.5)
8 to 9	118.6 (118)	37°18'R	-3°26'	5.0	-7.1	N. 57° W

Revised - see page 151

-26%  
60'    -44%  
50'    +11%  
70'    +34%  
75'



## C Line (cont.)

28

Sta. Cor. dist. Hor. A. Vert. Δ H.I. Elev. Mag. B.

22 on C line  
 21 to pt. X (157') 116°17'R +5°09' 5.0

See page 51

26 on N line  
 20 to 21 (686.5 (687')) 17°28'R -2°43' 5.0 1056.4 S. 19°W

19 to 20 (296.2 (295')) 110°45' +3°02' 5.0 1089.0 S. 10°W

15 to 19 (374.7 (375')) 29°01'R -3°26' 5.0 1073.4 N. 68°30'W

15 to 18 (333.9 (334')) 50°43'R -3°26' 5.0 1070.6 (grade)

15 to 17 (214.3 (214')) 56°15'R -3°26' 1.3 1083.0 (C. 3.7)

S Line +2.5%

Williams  
Hill  
Osborne  
Isbell  
Leakey  
6/10/38  
Drizzling rain

29

Sta. Cor. dist. Hor. Δ Vert. Δ H.L. Elev. Mag. B.

Dist. bet. transit pts  
on this page = 1013.5'

7 to 8	88.0 (87')	5°55'R	+1°26'	4.9	+2.2	✓	S.26°30'E
6 to 7	76.0 (75')	1°40'R	+1°26'	5.0	+1.9	✓	S.32°30'E
5 to 6	98.9 (98')	5°37'L	+1°26'	5.0	+2.4	✓	S.34°30'E
4 to 5	108.9 (108')	14°01'R	+1°26'	5.0	+2.7	✓	S.29°E
3 to 4	167.9 (167')	0°11'R	+1°26'	5.0	+4.2	✓	S.43°E
2 to 3	164.9 (164')	20°18'L	+1°26'	5.0	+4.1	✓	S.43°E
1 to 2	93.9 (93')	0°13'R	+1°26'	5.0	+2.3	✓	S.23°E
0 to 1	215.0 (214')	5°06'L	-0°24'	5.0	-1.5	✓	S.24°E

Pt. 0 = sta 142± on  
State Hwy pave.

Elev. pt. 0 = 1295.2

Highway to "0" = N10°59'W,  
Pt. 0 = Pt. of Hwy curve 100±  
N. of 15' corner curb

## S Line (cont.)

30

Sta	Cor. dist	Hor. Δ	Vert Δ	H.I.	Elev.	Mag. B.
15 to 16	128.0 (127)	19° 06' L	+1° 26'	4.6	+3.2	S. 59° E
14 to 15	96.0 (95)	19° 10' R	+1° 26'	4.5	+2.4	S. 40° 30' E.
13 to 14	69.0 (68)	17° 01' L	+1° 26'	4.9	+1.7	S. 60° E
11 to 13	133.0 (132)	56° 04' L	+1° 26'	4.9	+3.3	S. 42° E.
11 to 12	94.0 (93)	3° 53' R	+1° 26'	4.9	+2.3	S. 17° 30' W.
10 to 11	57.0 (56)	29° 09' R	+1° 26'	4.7	+1.4	S. 13° W
9 to 10	33.0 (32)	21° 41' R	+1° 26'	5.0	+1.8	S. 15° 30' E
8 to 9	81.0 (80)	11° 10' L	+1° 26'	4.2	+2.0	S. 37° 30' E.

Dist. bet. transit pts.  
on this page = 691.0'

## S. line (cont.)

31

sta.	Cor. dist	Hor. $\Delta$	Vert. $\Delta$	H.I.	Elev.	Mag. B.
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see book p 169

17 to 18	91.0 (90)	10° 22' R	+1° 26'	5.4	+2.31	S 47° E
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16 to 17	63.0 (62)	1° 25' R	+1° 26'	4.7	+1.5	S. 57° E.
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Meridian Saddle Line  
(marked Man stakes)

Williams  
Hill  
Osborne  
Isbell  
Leakey

6/11/38

cloudy & cool

32

Sta.	Cor. dist	Hor. Δ	Vert. Δ	H.I.	Elev.	Mag. B.
5 to 8	558.0 (558)	20°41'R	0.0	4.0	00	Red 4.0 Cut 6.6

5 to 7	504.0 <sup>✓</sup> (503)	18°38'R	-0°34'			-5.0
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3 to 6	467.0 <sup>✓</sup> 466.0 (466)	29°00'R	-0°34'	4.9		-4.7
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3 to 5	367.0 <sup>✓</sup> (366)	36°45'R	-0°34'	4.9		-3.7
--------	-----------------------------	---------	--------	-----	--	------

3 to 4	267.0 <sup>✓</sup> (266)	39°56'R	-0°34'	4.9		-2.7
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2 to 3	50.9 <sup>✓</sup> (50)	35°20'R	-2°27'	5.0	-4.2	N. 74° W
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1 to 2	989.4 <sup>✓</sup> (970)	1°33'R	-2°27'	5.0	-42.4	S 72° W
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0 to 1	541.1 <sup>✓</sup> (541)		-2°27'	5.0	-23.2	S 70° 30' W
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Pf. 0 = high point in saddle  
S.E. of wire gate

Aneroïd  
1500.0

Sta.	Cond. dist.	Hor. A	Vert. A	H. I.	Elev.	Mag. B.
12 to 15	435.6 (436')	76°00'L	-1°43'	4.8	-13.0	
12 to 14	314.7 (314')	70°25'L	-1°43'	4.8	-9.40	
12 to 13	187.8 (187)	78°20'L	-1°43'	4.8	-18.6	(6/12/38)
10 to 12	364.7 (364')	<sup>10°58' P / 11/38</sup> 98°7'R	-1°43'	5.0	-10.9	N50W (6/11/38)
10 to 11	230.7 (230')	152°57'R	+2°11'	5.0	+8.8	Note for loc. line run from *7 to *11
9 to 10	334.9 (334')	23°45'R	+2°29'	4.9	+14.5	N. 59° W. *10 Saddle central pt.
3 to 9	757.0 (757')	10°44'L	0.0	4.9	Same as 3	N. 83° 30' W (C. 7.6)

Sta.	Cardist.	Hor. A	Vert. A	H. I.	Elev.	Mag. B
21 to 23	354.7 (354)	19°21'R	-1°45'	5.0	-10.6	
21 to 22	221.8 (221)	32°24'R	-1°43'	5.0	-6.6	
18 to 21	570.5 <sup>✓</sup> (570)	37°23'L	-1°43'	5.0	-17.1	S 2° E
18 to 20	522.7 <sup>✓</sup> (522)	7°13'L	-1°43'	5.0	-9.7	
18 to 19	190.8 <sup>✓</sup> (190)	8°46'R	-1°43'	5.0	-5.7	
17 to 18	290.7 <sup>✓</sup> (290)	1°33'R	-1°43'	4.8	-8.7	S 35° 30' W
12 to 17	912.2 <sup>✓</sup> (912)	8°13'L <del>8°13'L</del>	-1°43'	4.8	-27.3	S 33° 30' W S 35° W
12 to 16	660.4 <sup>✓</sup> (660)	85°20'L	-1°43'	4.8	-19.8	

Sta.	Cor. dist	Hor. Δ	Vert. Δ	H.L.	Elev.	Mag. B
30 to 31	114.9 (114)	4°21'R	-1°43'	5.0	-3.4	S 41° W
29 to 30	226.8 226	15°43'R	-1°43'	4.8	-6.7	S 37° W
28 to 29	101.9 (101)	24°28'R	-1°43'	4.9	-3.0	S 20° 30' W
27 to 28	51.0 (50)	22°49'R	-1°43'	4.8	-1.5	S 3° E
25 to 27	372.7 (372)	2°30'R	-1°43'	5.0	-11.2	S 28° E
25 to 26	115.9 (115)	9°09'R	-1°43'	5.0	-3.4	
21 to 25	488.6 (488)	29°11'L	-1°43'	5.0	-14.6	S 30° E
21 to 24	365.7 (365)	26°33'L	-1°43'	5.0	-10.9	



Sta. Candist Harva Varkka H.L. Eler

See page 40

~~29 to 35~~ 115-205 11°00' - 5°03' 5.0

S 7° E

To saddle

29 to 34 145.3 (145) POT. +4°01' 6.7 +10.1

pt. 2

31 to 33 141.7 (140) 32°14' +10°19' 2.7 +80.3 S 8°30' W

31 to 32 160.7 (160) 20°38' -1°13' 4.7 -4.9 S 17° W

Area of 1520 at pt. 32

Check Map 8

31-34-35

In 2020' Instead of 20' right on 33  
Varkka + 100'

6/14/38 warm

Hill  
Isbell  
Leckey  
Brooks

37

sta Cordist Hor. A Vert. A H. I. Elev. Mag. B.

37 to 40	(605)	17°53'-R.	-1°43'	4.8	
37 to 39	(420)	18°49'-R.	-1°43'	4.8	
37 to 38	135.9 (135)	37°52'-R.	-1°43'	4.8	S. 24° W.
36 to 37	305.7 (305)	30°33'-R.	-1°43'	4.8	S. 15° E.
35 to 36	100.9 (100)	29°37'-R.	-1°43'	4.7	S. 48° E.
34 to 35	125.9 (125)	34°27'-R.	-1°43'	4.4	S. 77° 30' E.
33 to 34	300.7 (300)	8°36'-L.	-1°43'	4.4	N. 69° 30' E.
32 to 33	450.6 (450)	117°06'-L.	-1°43'	5.0	N. 77° 30' E.

Abandoned

Sta.	Cor. Dist.	Hor. L.	Vert. L.	H. I.	Elev.	Mag. Ber.
42 to 46	(1015)	15°57'-L.	-1°43'	4.7		S. 28° E.
42 to 45	(690)	13°43'-L.	-1°43'	4.7		
42 to 44	(625)	11°31'-R.	-1°43'	4.7		S. 0°30' E.
42 to <sup>44</sup> Saddle	(750)	15°01'-R.	+0°59'	4.7		S. 2° W. in Saddle
42 to 43	(502)	20°41'30"-R.	-1°43'	4.7		S. 8° W.
37 to 42	(820)	2°53'-R.	-1°43'	4.8		S. 12° E.
37 to 41	(660)	8°02'-R.	-1°43'	4.8		

~~Abandoned~~

Sta.	Car. Dist.	Hor. L.	Vert. L.	H. I.	Elev.	Mag. Ber.
47 to 51	(737)	101°50'-L.	-1°30'	4.9		S. 22° E.
47 to 50	(392)	88°43'-L.	-1°30'	4.9		
47 to 49	(310)	33°05'-L.	-1°30'	4.9		
47 to 48	(485)	25°58'-R.	-3°44'	4.9		
46 to 47	(124)	6°24'-R.	-1°30'	4.9		S. 82° W.
45 to 46	(123)	53°20'-R.	-1°30'	4.6		S. 76°30' W.
Saddle 44 to 45	(206)	20°42'-R.	-1°30'	4.8		S. 22° W.

~~Abandoned~~

M. Line (cont.) from page 36

6/15/38 Hot

Williams  
Hill  
Isbell  
Leakey  
Brooks

40

Sta.	Cor. dist.	Hor. Δ	Vert. Δ	H.I.	Elev.	Mag. B.
41 to 42	80.8 (80')	86° 23' L	-2° 52'	5.1		
39 to 41	356.1 (356')	170° 40' R	-2° 52'	4.9		N 43° 30' W
39 to 40	216.5 (216')	25° 46' R	-2° 52'	4.9		N 37° W
38 to 39	63.8 (63')	21° 15' R	-2° 52'	4.9		N 61° W
37 to 38	135.7 (135')	43° 45' R	-2° 52'	5.0		N 82° 30' W
36 to 37	60.8 (60')	28° 00' R	-2° 52'	4.9		S 52° 30' W
35 to 36	340.2 (340')	32° 19' R	-2° 52'	5.0		S 26° W
34 to 35	72.7 (72')	11° 44' L	-3° 47'	5.0	-4.6	S 89° E

Back sight on # 33

See Book 239 - Pg 29 for Revision

Sta	Cor. dist.	Hor. Δ	Vert. Δ	H.I.	Elev.	Mag. B.
49 to 50	1187 (1185)	29°20'R	-2°52'	4.8		S 19°E
48 to 49	153.6 (153)	9°32'R	-2°52'	4.8		S 47°30'E
47 to 48	467.7 (460)	18°03'L	-2°52'	4.8		S 56°30'E
46 to 47	355.1 (355)	46°30'L	-2°52'	4.8		
45 to 46	2664 (266)	39°41'L	-2°52'	4.8		
44 to 45	1327 (132)	22°47'L	-2°52'	4.8		
43 to 44	435.9 (436)	196°36'L	-2°52'	5.1		S 10°E
42 to 43	2185 (218)	179°26'L	-2°52'	5.1		S 6°E

Sta.	Cor. dist	Hor. A	Vert. A	H.I.	Elev	Mag. B.
56 to 58	237.5 (237)	7006 L	-2°52'	5.0	-11.8	
56 to 57	189.6 (184)	24°00 L	-2°52'	5.0	-9.2	
55 to 56	112.8 (112)	2°12 R	-2°52'	5.0	-5.6	56° E should be (117)
59 to 55	135.7 (135)	18°40 <sup>W</sup> / 135 19°42 R	-1°01'	4.9		50°30 E
51 to 54	362.1 (362)	31°11 L	-2°52'	4.7		52°30 E
51 to 53	171.6 (171)	POT.	-2°52'	4.7		
51 to 52	105.6 110.7 (110)	POT.	-12°48'	4.7		
50 to 51	78.8 (78)	24°53 R	-2°52'	4.6		55°30 W

Sta.	Cardist.	Hoc. A	Vert. a	H.I.	Diff Elev.	Mag. B.
65 to 66	157.6 (116.7)	14°14'L	-2°52'	4.7	-7.8	
61 to 65	254.4 (254)	7°43'L	-2°52'	4.8	-12.7	S 22°30'E
63 to 61	252.4 (252)	0°05'L	-2°52'	4.8	-12.6	S 19°E
62 to 63	196.5 (196)	6°40'R	-2°52'	4.7	-9.8	S 18°30'E
61 to 62	186.6 (186)	1°22'L	-2°52'	4.8	-8.2	S 26°E
60 to 61	161.6 (161)	21°57'L	-2°52'	5.0	-8.0	S 23°30'E
59 to 60	174.5 (174)	6°07'R	-2°52'	5.0	-9.7	S 1°E
56 to 59	305.3 (305)	2°29'L	-2°52'	5.0	-15.2	S 7°30'E

should be 176



Sta. Cor. dist. Hor. Δ Vert. Δ H.I. Elev. Mag. B.

73 to 74  $\frac{30.5}{30.7}$   
30 P.O.T. -7°03' 4.8 -3.7

Pt. 73 about inter-sec of  
3% grade from E. side

72 to 73  $\frac{167.6}{167}$  ✓ 83°01' R -2°52' 5.0 -8.3 S 21°30' W

71 to 72  $\frac{105.7}{105}$  ✓ 29°09' R -2°52' 4.9 -5.2 S 43°0' E

70 to 71  $\frac{146.6}{146}$  ✓ 9°38' L -2°52' 4.9 -7.3 S 31° E

69 to 70  $\frac{121.7}{121}$  ✓ 8°22' L -2°52' 4.8 -6.1 S 21° E

65 to 69  $\frac{407.0}{407}$  ✓ 11°38' R -2°52' 4.7 -20.3 S 11° E

65 to 68  $\frac{270.3}{270}$  ✓ 10°54' R -2°52' 4.7 -13.5

65 to 67  $\frac{190.5}{190}$  ✓ 1°31' R -2°52' 4.7 -9.5

Sta	Cor. dist	Hor. a	Vert. a	H.I.	Elev.	Mag. B.
79 to 82	265.7 (265)	33°55'L	+2052'	5.0	+13.3	Rocky pt.
79 to 81	170.6 (170)	19°21'L	+2052'	5.0	+8.5	
79 to 80	104.7 (104)	6°27'R	+2052'	5.0	+5.2	
78 to 79	215.5 (215)	15°14'R	+2052'	4.7	+3.3	S 14°W (grade)
76 to 78	295.7 (296)	83°09'L	+418'	4.7	+22.2	S 2°E (C.T.A.)
76 to 77	127.7 (127)	76°35'L	-2052'	4.7	-6.4	
73 to 76	141.6 (141)	POT	0.0	4.8	0	
73 to 75	72.5 82.8 (82)	POT	-11047	4.8	-16.6	

Sta. Cordist. Hora. Verta. H.I. Elev. Mag. B. D.F.

See Page 26 for  
continuation of cline

C1  
86 to C2  
Backsight on 85

118°39' R -3°26'

S 81° W

See Rev Book 239 P 28

C1  
85 to 86

253.1  
(254) 40°44' L -5°06' 1.8

S 77°36' E

84 to 85

115.1  
(116) P.O.T. -5°05' 1.7 -10.5

83 to 84

84.1  
(84) 7°35' L +5°04' 1.9 +7.4

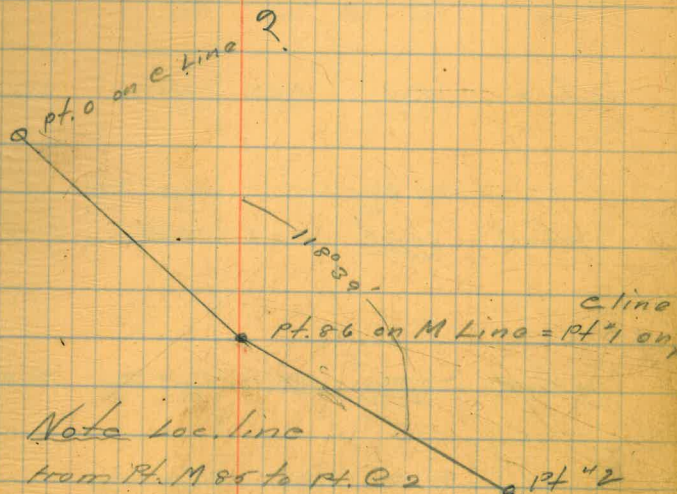
S 36°30' E (C. 33)

Pt. 84 = saddle

79 to 83

449.3  
(450) 43°09' L +2°52' 5.0 +22.5

S 50° E



Note Loc. line

from Pt. M 85 to Pt. C 2



Sta	Cor dist	Hor A	Vert A	H.I.	Rad	Elev	Mag	B				
15 to 16	128.0 (127')	37°11'L	0°	5.0	5.0	1022.1 1053.4	100° to back Tan.	+27% 125'	-29% 125'	-25% 100'	sta 16 in draw 90° to back tan.	
14 to 15	367.0 (366')	17°21'L	-0°34'	4.9	4.9	1022.1 1058.4	-3.6 N. 70°30' W	+26% 150'	-25% 50'	-40% 50'	-62% 100'	sta. 15
13 to 14	186.0 (185')	2°33'L	-0°34'	5.0	16.0	1025.7 1060.1	-12.8 N 82°30' W	+31% 150'	+43% 50'	-40% 125'	-57% 100'	sta. 14
12 to 13	108.0 (107')	P.O.T.	-0°45'	5.0	5.0	1038.5 1072.9	-1.4	+40% 150'	-48% 75'	-53% 125'		sta. 13
10 to 12	246.8 (247')	P.O.T.	+4°06'	4.9	4.9	1039.9 1074.3	+17.7	+36% 100'	+54% 75'	-45% 35'	-64% 150'	sta. 12
10 to 11	59.0 (62')	P.O.T.	-14°36'	4.9	4.9	-15.4		+28% 100'	+50% 65'	-67% 60'	-54% 150'	90° to line sta. 11 in draw
6 to 10	330.2 (330')	P.O.T.	-2°53'	5.0	5.0	1022.2 1066.6	-16.6	+43% 150'	-25% 100'	-47% 150'		sta. 10
6 to 9	282.9 (283')	P.O.T.	-3°30'	5.0	5.0	-17.7		+45% 150'	-25% 60'	-44% 150'		sta. 9

Sta.	Cor. dist.	Hor. Δ	Vert. Δ	H.I.	Rod	Elev. Mag. B.							
22 to 20	321.0 (320')	26°09'R	0°	5.1	5.1	1022.1 1056.4	1.15% 150'	-25% 50'	-18% 75'	sta. 25			
							Draw +177 150'	-30% 40'	-26% 30'	-6% 100'			
22 to 24	240.0 (239')	9°42'R	0°	5.1	5.1	1022.1 1056.4	+41% 100'	+26% 50'	+28% 50'	-35% indraw 65'	+60% level 35'	sta. 24	
22 to 23	108.0 (107')	12°09'R	0°	5.1	5.1	1022.1 1056.4						6/20/58 sta. 23	
							+36% 100'	+25% 35'	-28% 90'	-8% 90'			
20 to 22	638.0 (637')	25°17'L	0°	4.8	4.8	1022.1 1056.4	N 49°30'W	+26% 100'	+16% 35'	-22% 100'	-8% 100'	sta. 22	
20 to 21	249.0 (248')	To observed pt. 29°39'L	0°	4.8	12.9	1014.8	-8.1					sta. 21	
								+24% 125'	+13% 25'	-19% 75'	-68% 50'		
19 to 20	221.0 (220')	35°11'R	0°	4.9	4.9	1022.1 1056.4	N 24°W					sta. 19	
												observed pt. 58' 20'	
												pt. 19 backsight on 17 8009'	
17 to 19	831.0 (830')	12°34'R	0°	5.5	5.5	1022.1 1056.4	N 50°20'W	+15% 70'	+28% 100'	-65% 150'		pt. 20 sta. 19	
								+27% 125'	-98% 150'			sta. 18	
15 to 17	334.0 (333')	2°50'L	0°	5.0	5.0	1022.1 1056.4	N 72°30'W	+17% 100'	+36% 100'	-60% 75'	-14% 60'	-30% 100'	sta. 17

Sta Cordist Hara Verta H.L. Rod; Elev. Mag. B.

see hook up to e line 79.

22 to 26

430.0  
(+29')

34° 26'

0

5.0

5.0

1022.1

~~1055.1~~

N 16° W

+13%

+8%

-21%

-14%

to Wash

std. N. 26

" C. 27

125'

75'

100'

60'

C Line Revision - cont from page 27

Sta.	Cardist	Hor. a	Vert. a	H.I.	Rad.	Elev.	Mag. B						
16 to 17	1307 (136)	P.O.T.	-12°28'	5.0	5.0	-26.9	-28.9	to wash -22% 70'	+18% 150'	in draw	sta. 17		
15 to 16	1332 (134)	P.O.T.	-6°42'	5.1	5.1	1110.5	-15.4	-21% 125'	-17% 80'	+16% 40'	+27% 150'	sta. 16	
13 to 15	2189 (218)	P.O.T.	-1°00'	5.0	5.0	1126.1	-3.8	-19% 70'	-47% 70'	6%	+34% 150'	sta. 15	
13 to 14	1107 (111)	35°17' L	-6°18'	5.0	5.0	-12.7	N70°30' W	-17% 90'	-39% 40'	+55% 75'	+48% 75'	sta. 14	
10 to 13	2980 (298)	P.O.T.	-3°26'	5.0	0.5	1129.9	-13.5	6%	-30% 150'	+49% 75'	+46% 75'	sta. 13	
13 to 12	1085 (113)	on back tang. P.O.T.	-12°49'	5.0	5.0	-24.7				-13 150'	+30% 125'	in draw	sta. 12
10 to 11	987 (98)	P.O.T.	-3°26'	5.0	12.5	-13.4		-3% 125'	-21% 65'	+29% 125'	grade	sta. 11	
10	pt. on intermediate saddle cut 7.5					1143.3		-12% 125'	+21% 20'	+40% 125'		sta. 10	



(cont.)

Sta.	Cor dist	Hor. a	Vert. a	H.I.	Rod	Elev.	Mag. B.					
23 to 25	251.0 <sup>✓</sup> (254')	P.O.T.	-7°15'	5.0	10.0	-31.9	to wash	-15% 120'	level 50'	-4% 60'	+3% 100'	sta. 25
23 to 24	144.1 <sup>✓</sup> (149')	33°19'	-11°23'	5.0	5.0	-29.0	S 7°30' W	-18% 125'	-8% 75'	+4% 125'		sta. 24
22 to 23	131.4 <sup>✓</sup> (131')	P.O.T.	-3°50'	5.0	5.0	-8.8 1087.9			-17% 150'	+25% 100'		sta. 23
18 to 22	356.0 <sup>✓</sup> (356')	P.O.T.	+3°08'	5.0	5.0	+19.5 1096.7			-26% 100'	-15% 75'	+24% 125'	sta. 22
18 to 21	230.6 <sup>✓</sup> (230')	P.O.T.	-2°29'	5.0	5.0	-9.6			-14% 150'	+10% 150'		sta. 21
18 to 20	136.2 <sup>✓</sup> (137')	P.O.T.	-0°33'	5.0	5.0	-15.6	to wash	-16% 60'	-8% 60'	+8% 150'		sta. 20
18 to 19	68.7 <sup>✓</sup> (77')	61°14'	-20°15'	5.0	5.0	-25.3	S 41°30' W	-8% 150'	+4% 150'	in draw		sta. 19
										+25% on top. P.O. E. from 19 125'		
10 to 18	217.9 <sup>✓</sup> (222')	P.O.T.	-8°41'	5.0	5.0	-33.3 1077.2			-25% 67' 60'	+10% 125'	on split of angle	sta. 18
							F. G. O.				P.I. about 30' ahead from back tang.	

Sta. Cond. dist. Horiz. Vert. H.I. Rod Elev. Mag. B.

See hook up to N line

C 27 to N 25 (120') 1025.1 1.8 1.8 1056.4 S 6°W

C 27 to N 22 2100.2 1056.4 S. 11°30'E

N 26  
23 to 27 5799.4 (5800) P.O.T. -3007' 5.0 5.0 -31.5  
1056.4

23 to 26 4086 (4150) P.O.T. -7°45' 5.0 5.0 -55.6  
to wash  $\frac{-4\%}{150'}$   $\frac{+4\%}{150'}$  in draw

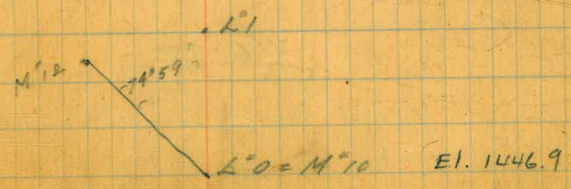
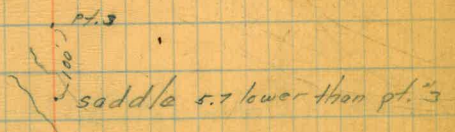
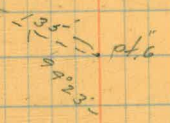
L Line - From Pt. M<sup>10</sup> to State Hwy.

7/5/58 elev  
Williams  
Hill  
Osborne  
Isbell  
Lecky  
Brooke's

Sta. Cor. dist. Hor. Δ Vert. Δ H.L. Rod Elev. Mag. B

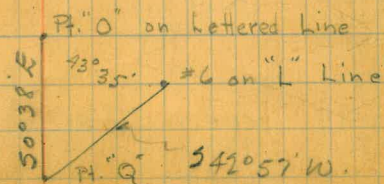
6 to 2 of <i>(letterline)</i>	1098.0 <i>(1100)</i>	13°11'L	-3°02'	5.0	5.0	-58.1	N26°30'E
5 to 6	1126.0 <i>(1125)</i>	P.O.T.	+0°16'	5.0	5.0	+4.8	
4 to 5	1018.5 <i>(1020)</i>	26°07'R	-2°53'	5.0	5.0	-57.2	N70°E
3 to 4	88.9 <i>(88)</i>	P.O.T.	-1°58'	5.1	6.1	-3.0	
2 to 3	630.1 <i>(630)</i>	7°02'R	+2°11'	4.9	8.0	+24.0	N19°30'E
1 to 2	745.3 <i>(750)</i>	19°12'L	+5°06'	5.0	9.0	+66.5	N7°30'E
0 to 1	548.6 <i>(558)</i>	74°49'R <i>top of saddle 1952</i>	+6°12'	5.0	9.0	+58.7	N.26°E

37.3 lower  
than pt. 6  
saddle



0 = M<sup>10</sup>

Sta.	Cor. dist	Hor. Δ	Vert. Δ	H.I.	Rod	Elev.	Mag. B.		
13 to 14	288.8 (288')	10° 58' L	-1° 35'	5.5	5.5	-2.9	N. 16° 30' E	cut 9.7	on ridge
9 to 13	574.1 (575')	12° 17' R	-3° 27'	5.3	5.3	-34.6	N. 26° E		Note Recommended location is to move pt. "8" about 50' east and run to pt. "13" <del>etc.</del>
9 to 12	429.0 430	8° 38' R	-3° 27'	5.3	5.3	-25.9		plotting shot	point of ridge
9 to 11	424.6 (425')	17° 53' L	-3° 27'	5.3	5.3	-20.6		plotting shot	bottom of wash
9 to 10	188.1 (188')	33° 58' L	-3° 27'	5.3	5.3	-11.3		Plotting shot	(Begin. of 6% grade)
8 to 9	295.8 (295')	13° 10' R	+1° 39'	5.2	5.2	+8.5	N. 14° 30' E		
7 to 8	2119.1 (2126')	26° 32' L	-3° 37'	5.1	5.1	-132.9	N. 1° 30' E		
		<u>7/6/38</u>							
6 to 7	2360.8 (2360')	12° 35' L	-0° 45'	5.0	5.0	-30.9	N. 27° E N. 42° 18' E		



Sta.	Cor. dist.	Hor. Δ	Vert. Δ	H.I.	Rod	Elev.	Mag. B.	
21 to forward	201.0 (200')	5°21' R	+0°23'	5.3	5.3		N 17° W	N 31° 42' W Highway
19 to 21	316.9 (316')	P.O.T.	-1°01'	4.9	4.9	-5.6	N 67° W	* 21. Note P.I. of bay = 175' N. of cul. C.M. 4.03
19 to 20	86.4 (84')	19°06' L	-4°47'	4.9	4.9	-7.2		Plotting shot
18 to 19	135.7 (135')	25°05' L	-2°45'	4.7	4.7	-2.5	N. 34° W.	
17 to 18	191.7 (140')	8°27' R	-14°58'	5.0	5.0	-35.2	N. 7° W.	Fill 4.7, Cut 2.4 Note In plotting alignment run from 16A to 18
16 to 17	268.4 (270')	8°44' L	-5°49'	5.3 38.3	8.3	-30.3	N. 16° 30' W	22.0 Cut. 24.0 to grade 33.7 116' 59.5' = 16-A Lower.
14 to 16	401.0 (400')	23°45' L	-0°05' 0.0	14.5 4.7	5.5 9.7	-9.1	N. 7° 30' W.	Cut. 24.6 37.0 to 69. 14
14 to 15	105.6 (105')	7°58' L	-3°27'	14.5	14.5	-16.1 - 6.3	grade	plotting

Section Line, ties near Footer

Sta. Angle Mag B. C.C.

26+388 P.O.T.  
(1577)

19+80.1 P.O.T. 0  
(103.4)

16+77 P.O.T. 0  
(91.5)

7+61 P.O.T. 0  
(76.0)

1+21 P.O.T.

N 74° 30' W

0

Williams  
Hill  
Osborn  
Isbell  
Leekay  
Brooker

7/9/38  
hot

57

26+56.5  
30.5-0 Set 12"x12"x8" stone  
on edge in rock mound

26+10 0 1/4 cor. not found

State Hwy 1+21

90°

Coner. Men 0

SW. cor  
of N.W. 1/4 S. 31

S.E. cor TWS 14 S.

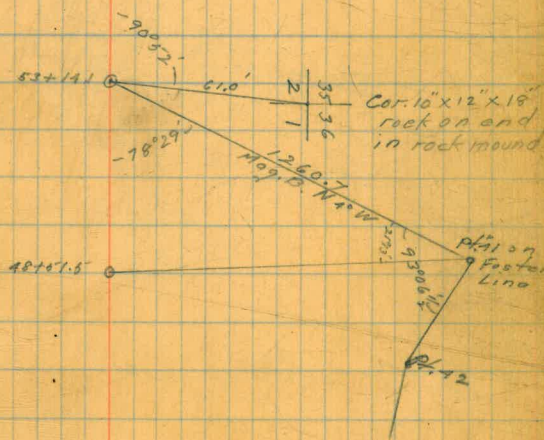
R. 1 W. & N.E. cor  
of Rancho El Cajon

Sta. Angle Mag. S.

53+14.1 90°52' R Tie to cor.  
(142.6)

48+51.5 P.O.T. @  
(1310.6)

35+40.9 P.O.T. @  
(1560.5)

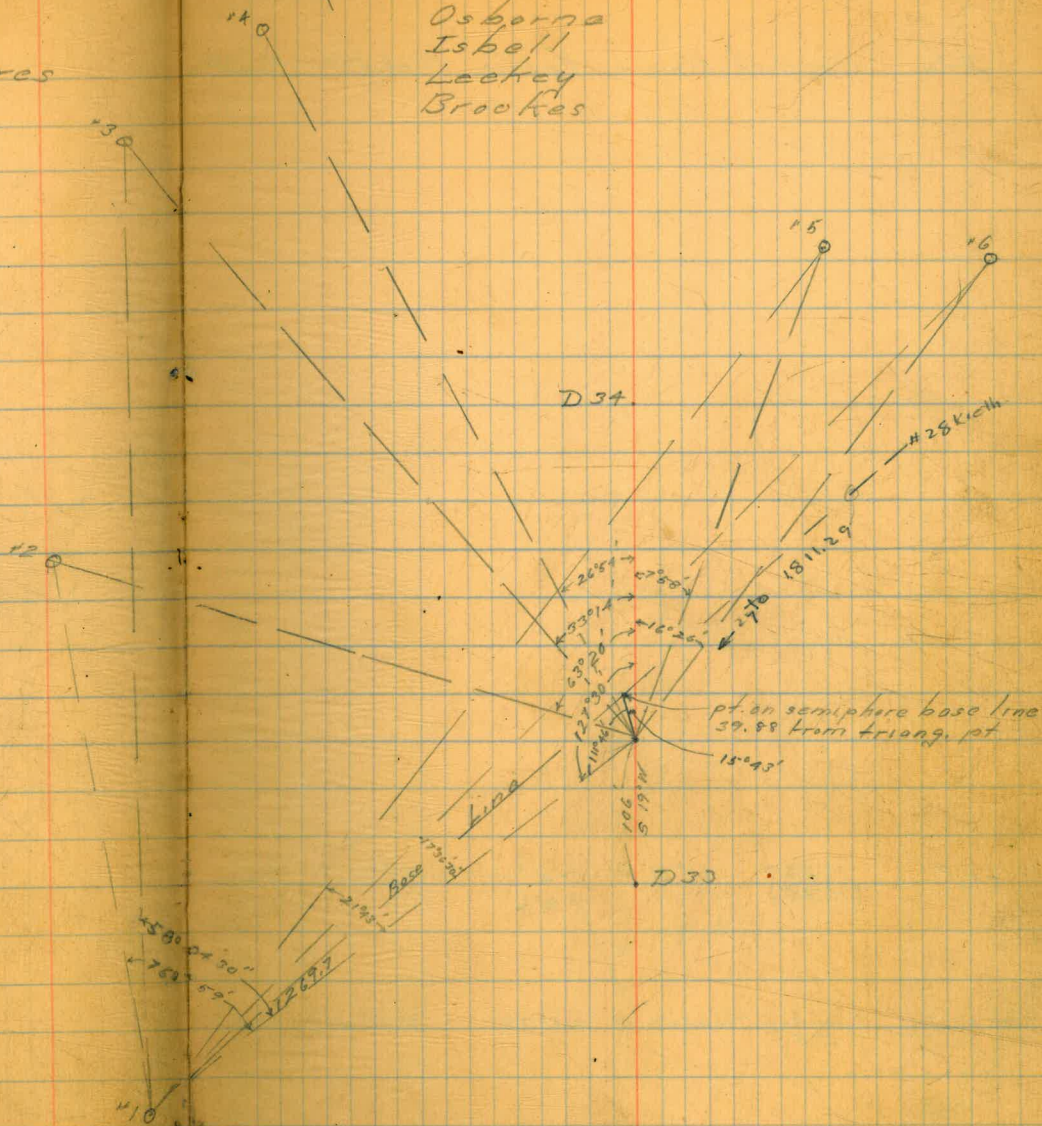


7/9/38

(Westh.)  
Triangulation to semiphores  
From D Line.

Williams  
Hill  
Osborna  
Isbell  
Leekey  
Brookas

59





R' Line

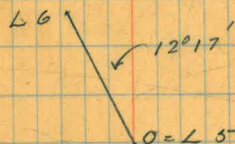
7/11/88  
with  
Lookay

60

Sta. Cordist Hor. & Vert. H.L. Rod. Elev. Mag. B.

1 to 2 (030.5  
(1035) 30°21'R -4°10' 5.1 5.1

N 83°15'E



0 to 1 (218.8  
(218') 12°17'R -1°39' 5.1 10.1

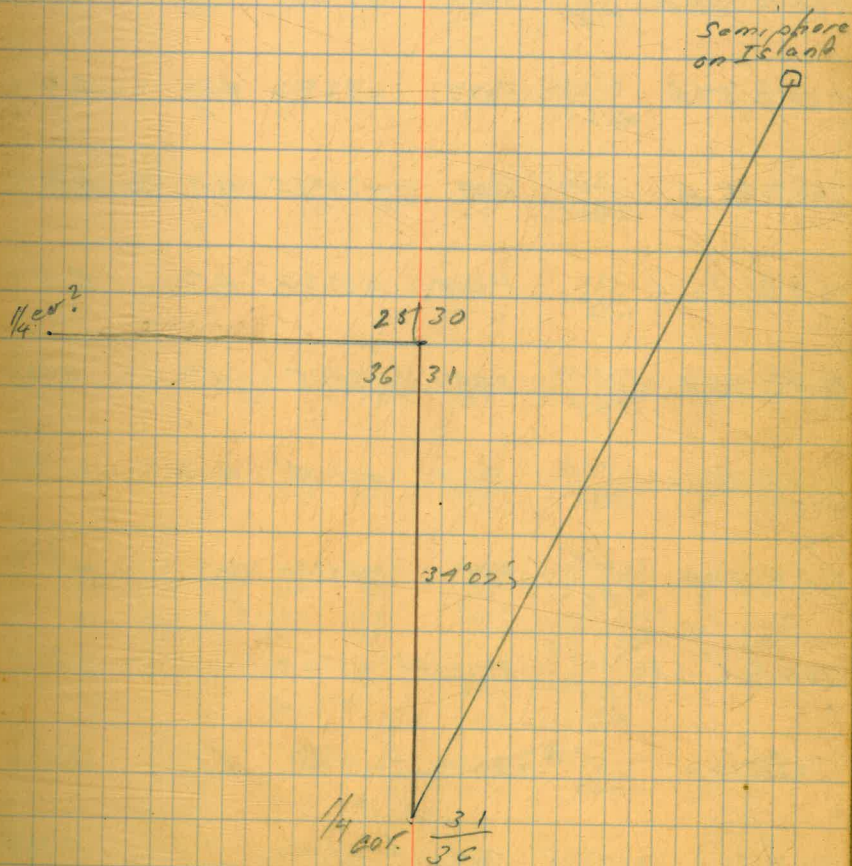
N 51°30'E

L5 = R' 0

8/3/58

61

Tie from sec. cor  $\frac{25}{36} \frac{30}{31}$  to  $\frac{1}{4}$   
cor  $\frac{1}{2}$  mile west and tie from  
 $\frac{1}{4}$  cor  $\frac{31}{36}$  (dam axis) to Island



"M" Line Alternates from M 71

Sta.	Dist.	Horiz A	Vert A	H.I.	Rod
73A to Dn. Str.	397.5 455'	29°39' Lt	-21°00'	4.7	4.7
73A to Upstr. FS. to C.O.	420' 475'	23°23' Rt	-19°22'	4.7	4.7
73A to 78 A	(428.0) 460'	P.O.T.	-15°30'	4.7	4.7
73A to 79 A	(500.9) 515'	P.O.T.	-9°55'	4.7	4.7
73A to 77 A	(350.5) 412'	P.O.T.	-32°12'	4.7	4.7
73A to 76 A	(260.1) 290'	P.O.T.	-21°55'	4.7	4.7
73A to 80 A	(686) 685'	P.O.T.	+0°22'	4.7	4.7
73A to 75 A	1262.1 144	P.O.T.	-21°15'	4.7	4.7
73A to 81 A	130.9 730	P.O.T.	+0°48'	4.7	4.7
73A to 74 A	(416) 53'	P.O.T.	-24°44'	4.7	4.7
73A to C.O.	(825.1) 825'	33°00' Rt	+1°09'	4.7	4.7
72A to 73 A	147.8 147	35°40' Lt	-2°18'	5.1	5.1
71A to 72 A FS. M 71	(114.7) 224	74°02' Lt	-2°18'	5.0	5.0

Williams  
Osborn  
Isbell  
Lecker  
Brooks

62  
Sept. 28, 1938

74°02'

-152.5  
-143.9

shot was 6' above str + 16' near last.

M 81 A  $\frac{+31\%}{75'}$   $\frac{+17\%}{35'}$   $\frac{-19\%}{40'}$   $\frac{-42\%}{40'}$   $\frac{+25\%}{45'}$   $\frac{+5\%}{100'}$

-87.5 M 80 A  $\frac{+38}{100'}$   $\frac{-17\%}{25'}$   $\frac{-37\%}{60'}$   $\frac{-17\%}{40'}$   $\frac{-17\%}{100'}$

-144.4 M 79 A  $\frac{-24\%}{50'}$   $\frac{+5\%}{55'}$   $\frac{+25\%}{25'}$   $\frac{-13\%}{65'}$   $\frac{-37\%}{75'}$

-100.8 M 78 A  $\frac{-31\%}{65'}$   $\frac{-4\%}{60'}$   $\frac{+14\%}{85'}$   $\frac{-1\%}{55'}$   $\frac{-22\%}{100'}$

+4.4 M 77 A ← Creek 1% Grade

-49.0 M 76 A  $\frac{-20\%}{100'}$   $\frac{-10\%}{50'}$   $\frac{+1\%}{25'}$   $\frac{-8\%}{20'}$   $\frac{-29\%}{50'}$   $\frac{+52\%}{20'}$   $\frac{+18\%}{30'}$   $\frac{-12\%}{40'}$   $\frac{-47\%}{50'}$

+10.2 M 75 A  $\frac{-9\%}{100'}$   $\frac{-15\%}{40'}$   $\frac{-30\%}{70'}$   $\frac{-17\%}{35'}$   $\frac{+55\%}{35'}$   $\frac{+30\%}{30'}$   $\frac{-66\%}{70'}$  to Bot. Draw

-20.5 M 74 A  $\frac{-38\%}{100'}$   $\frac{+15\%}{40'}$   $\frac{+42\%}{40'}$   $\frac{-37\%}{55'}$   $\frac{-24\%}{60'}$   $\frac{+38\%}{55'}$   $\frac{\text{level}}{20'}$   $\frac{-70\%}{\text{to Bot. Draw}}$

M 73 A  $\frac{+22\%}{50'}$   $\frac{+59\%}{80'}$   $\frac{-54\%}{35'}$   $\frac{-39\%}{90'}$   $\frac{+30\%}{50'}$   $\frac{\text{level}}{20'}$   $\frac{-70\%}{\text{to Bot. Draw}}$

M 72 A  $\frac{+34\%}{150'}$   $\frac{-30\%}{65'}$   $\frac{\text{level}}{25'}$   $\frac{+6\%}{59'}$  M 72 A

split of angle

V = +18°06'

V = -16°02'

155'

75'

M 71 A

M 71 = 81.1177

M 70

V = +18°07'

22.5

Atchison Toll Road Loc.  
Co. designation #8

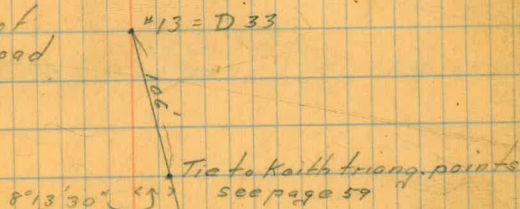
10/11/38  
Hill  
Isbell  
Leckey  
Brooks  
Rod & Elev. Mag B.

63

Sta.	Dist.	Hor. Δ	Vert. Δ	H.L.	Rod & Elev.	Mag B.
3 to 5	317 (317')	16° 06'	23° 03' L - 0° 45'	5.3	5.3	N 34° E - 4.1
3 to 4	176.0 (174')	43° 31'	21° 45' L - 0° 42'	5.3	5.3	N 34° 30' E - 2.1
2 to 3	235.9 (235')	18° 23'	9° 12' L - 1° 18'	5.2	5.2	N 58° E - 5.3
#1 to 2	174.8 (174')	11° 12'	5° 36' L - 2° 05'	5.1	5.1	N 67° 30' E - 6.3
#8.0 to #1	256.9 (256')	130° 47' 30"	65° 23' 30" R - 0° 55'	5.0	5.0	N 73° 30' E - 4.1
M-0 to #8.0 break sight on N#	37.0 (31')	201 28' 30"	100° 42' L - 1° 42'	5.0	5.0	- 1.0
M'3			S 70° 51' E			

Sta	Dist	Horiz	Vert	H.L.	Red. H. Mag. B.
10 to 11	80.0 (79')	35°48'R	-0°57'	5.2	5.2 - 1.3
9 to 10	241.0 (240')	41°19'30" 20°39'30"R	-0°20'	5.0	5.0 N 24°30'E - 1.4
7 to 9	337.8 (337')	21°47' 10°53'R	-1°23'	5.1	5.1 N 33°0'E - 8.1
7 to 8	227.9 (228')	14°38'R	-1°10'	5.2	5.2 - 4.6
6 to 7	251.0 (250')	52°50'30" 26°25'30"R	-0°16'	5.0	5.0 N 7°W - 3.3
5 to 6	168.0 (168')	31°33' 15°46'30"L	-0°19'	5.1	5.1 N 18°E - 2.4 H <sub>0</sub> Wedge of present road

Sta.	Dist.	Hor. Δ	Vert. Δ	H.I.	Red. El.	Mag. B
16 to 17	132.8 (133)	38°28'	19°14' R	-5°37'	5.0	5.0 N 25° E - 13.0
15 to 16	209.7 (209)	33°52'30"	16°56' L	+2°00'	5.0	5.0 N 8° E + 7.32
13 to 15	631 (630)	34°38'	17°19' L	+0°06'	5.1	5.1 N 25° E + 1.1 #15 25' W. of present road
13 to 14	357 (357)	12°48' L	-0°41'	5.1	5.1 - 4.3 #14 <sup>W</sup> edge of present road	
12 to 13	181 (180)	46°53'	23°27' L	-0°39'	5.2	5.2 N 42° E - 2.1 #13 center of present road
10 to 12	269.0 (268)	82°18'30"	41°09' R	-0°03'	5.0	5.0 N. 66° E - 0.2



Sta.	Dist.	Hor. A	Vert. A	H.I.	Red. Elev.	Mag. B	
22 to 23	281.0 (280')	11° 22'	5° 41' L	-0° 48'	5.1	5.1	N 57° E -3.9
20 to 22	385.9 (385')	9° 40' 30"	4° 50' L	-1° 05'	4.7	4.7	N 62° E -7.3 +22 center of present road
20 to 21	215.9 (215')	0° 40' 30" R		-1° 02'	4.5	4.5	-3.9
19 to 20	276 (275')	48° 50'	24° 25' R	-0° 35'	4.8	4.8	N 61° E -2.8 +20 N. edge of present road
18 to 19	285.2 (287')	37° 06'	18° 33' R	-1° 38'	4.6	4.6	N 42° 30' E -23.0 +19 N. edge of present road
17 to 18	102.0 (103')	7° 20'	5° 40' 30" L	-8° 06'	5.0	5.0	N 23° 30' E -14.5 +18 S. edge of present road

Sta.	Dist.	Hor. A	Vert. A	H.I.	Rodr. Elev.	Mag. B.	
28 to 30	367 (367')	$0^{\circ}05'$ $0^{\circ}02'30''$	$+0^{\circ}39'$	5.1	5.1	$N 18^{\circ} W$	-4.2
28 to 29	224.0 (223')		$+0^{\circ}41'$	5.1	5.1		+2.7
27 to 28	161.0 (160')	$95^{\circ}55'$ $47^{\circ}57' L$	$+0^{\circ}56'$	5.0	5.0	$N 17^{\circ} 50' W$	+2.6 +28 W. edge present road
26 to 27	136.0 (136')	$59^{\circ}52'30''$ $29^{\circ}56'30'' L$	$-0^{\circ}42'$	5.1	5.1	$N 30^{\circ} E$	-1.7 -27 center of present road
25 to 26	445 (444')	$3^{\circ}49'$ $1^{\circ}54' R$	$-0^{\circ}35'$	5.0	5.0	$N 60^{\circ} 30' E$	-4.5
23 to 25	566.9 (567')	P.O.T.	$-0^{\circ}41'$	5.0	5.0		-6.7
23 to 24	184.0 (183')	$4^{\circ}28'30''$ $2^{\circ}14' R$	$-0^{\circ}21'$	5.0	5.0	$N 57^{\circ} E$	-1.1



Sta.	Dist.	Hor. A	Vert. A	H.I.	Rod. Elev.	Mag. B.	
33 to 37	595.4 (597')	152°51'30" 76°26'R	-3°05'	5.0	5.0	N57°E	-32.1 1.87 center of present road
233 to 36	480 (480')	75°15'R	-2°49'	5.0	10.0		-23.6
33 to 35	296.0 (297')	75°47'R	-4°47'	5.0	5.0		-24.6
33 to 34	148.0 (148')	73°11'30"R	-4°48'	5.0	5.0		-12.3
							10/13/38
32 to 33	81.0 (85')	39°23' 17°41'30"R	-8°13'	5.0	5.0	N20°W	-12.8
31 to 32	138.5 (139')	54°58' 27°29'L	-6°07'	5.1	5.1	N39°50'W	-14.8
30 to 31	93.0 (92')	110°54'50" 5°05'7"R	+0°26'	4.8	4.8	N12°W	+0.7

Sta.	Dist.	Hor. Δ	Vert. Δ	H.I.	Red. EL	Mag. B.
41 to 43	190.8 (191')	67° 56'	33° 58' R - 1° 55'	4.2	4.2	N 20° 30' E - 6.4
41 to 42	69.4 (69')		50° 05' 30" R - 5° 11'	4.2	4.2	- 6.3
40 to 41	140.5 (142')	16° 24' 30"	2° 12' 30" L - 5° 09'	4.5	4.5	N 13° W - 15.0
39 to 40	298.7 (303')	2° 51' 30"	1° 25' 30" R - 8° 05'	5.0	5.0	N 6° 30' W - 47.3
38 to 39	246.1 (248')	28° 25' 30"	14° 13' L - 6° 12'	5.2	5.2	N 8° W - 26.7
37 to 38	156.5 (156')	99° 45'	19° 52' 30" L - 3° 21'	5.1	5.1	N 6° 30' E - 9.1 + 38 center of present road

steel rod in  
1/4" pipe in  
cap. man.  
marked  
G.B.

99.0  
709.0 N.W. 1/4  
Pt. 39

76.12' (160')  
- 12° 52'

1" pipe in rock  
mound marked  
INT. 1/4 cor. sec. 7

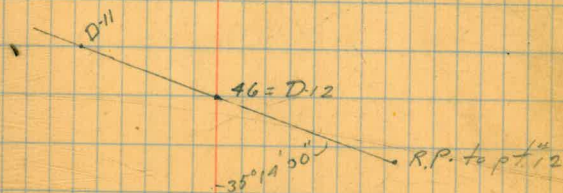
Sta. Dist. Hor. A Vert. H. I. Rod &amp; El. Mag. B.

351430

45 to 48	291.9 (291')	P.O.T.	-1°14'	5.1	5.1	-6.3	Center state highway (part)
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45 to 47	216.8 (217')		12°58' L - 1°48'	5.1	5.1	-6.8	47 = center of present road
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D12 45 to 46	36.0 (35')		47°26' 23°43' L + 0°35'	5.1	5.1	+3.6	
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43 to 45	304.7 (304)		14°19' 2°09'30\" R + 1°50'	5.0	5.0	+9.7	N27°30'E 45 = center present road
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43 to 44	124.6 (124)		11°53' L + 3°22'	5.0	5.0	+7.3	44 = Center of present road
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Hill  
Isbell  
Leakey  
Brooks

10-24-38

71

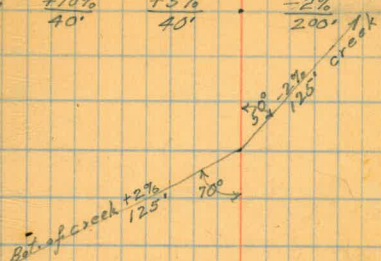
Inter of "D" "A" line & "D" on split of angle

+38%  
30'

+10%  
40'

+5%  
40'

-2%  
200'



-5%  
60'

-26%  
100'

+22%  
100'

-4%  
60'

Approx 100' from 19A

-32%  
80'

-34%  
100'

+14%  
25'

-20%  
100'

D19A

-5%  
100'

-22%  
100'

+20%  
50'

Level  
25'

-10%  
100'

Approx 100' from 19A

-3%  
100'

-15%  
60'

+18%  
50'

+45%  
80'

on E. & W. center 1/4 sec. line

10/31/58

72

Add topog. over M'line from pt. 0, Meridian saddle, to pt. 3

13 1030.9  
 2 1495.8  
 5 70°51' E

Sta. Dist. Hor. Δ Vert. Δ H.I. Rod & Elev.  
 Note For topog. on pts. 1, 2 & 3 see M'line pt. 0 to pt. 8

Sta.	Dist.	Hor. Δ	Vert. Δ	H.I.	Rod & Elev.	small island				
1 to 1 <sup>2</sup>	457.5 (458')		-1°50'	5.2	5.2	-14.6	$\frac{-23\%}{75'}$	$\frac{+17\%}{75'}$	$\frac{+23\%}{30'}$	$\frac{+30\%}{150'}$
1 to 1 <sup>2</sup>	305.7 (305')		-1°46'	5.2	5.2	-9.4	$\frac{-10\%}{70'}$	$\frac{-30\%}{60'}$	$\frac{+20\%}{80'}$	$\frac{+9\%}{100'}$
1 to 1 <sup>2</sup>	210.1 (210')	P.O.T.	-3°50'	5.2	13.2	-22.1	$\frac{-3\%}{80'}$	$\frac{-7\%}{90'}$	$\frac{+18\%}{150'}$	
P+1 to 1 <sup>2</sup>	71.9 (71')	P.O.T.	-7°40'	5.2	5.2	-2.1	$\frac{-14\%}{150'}$	$\frac{-28\%}{60'}$	$\frac{+27\%}{150'}$	
0 to 0 <sup>3</sup>	408 (408')	P.O.T.	-0°02'	5.1	12.1	-7.1		$\frac{-12\%}{150'}$	$\frac{+15\%}{75'}$	$\frac{+25\%}{100'}$
0 to 0 <sup>2</sup>	331 (330')	P.O.T.	-0°18'	5.1	5.1	-1.7	$\frac{-13\%}{100'}$	$\frac{-30\%}{25'}$	$\frac{+36\%}{60'}$	$\frac{+19\%}{125'}$
0 to 0 <sup>1</sup>	87.8 (87')	P.O.T.	-2°33'	5.1	5.1	-3.9	$\frac{+20\%}{200'}$	$\frac{+6\%}{30'}$	Adj	$\frac{+9\%}{50'}$ $\frac{+22\%}{60'}$ $\frac{+4\%}{100'}$

Alternate line from M<sup>3</sup> to

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D 33.

Sta.	Dist.	Hor. A	Vert. A	H.L.	Rod Elev.							
M <sup>20</sup> to 7	808.8 (808')	P.O.T.	+1005'	5.2	12.2	* 8.3	+37% 75'	+11% 30'	71% Pt. 7 60'	-24% 25'	-15% 100'	+8% 125'
M <sup>20</sup> to 6	720.8 (720')	P.O.T.	+0056'	5.2	5.2	+11.7 ✓	+30% 125'	+16% Pt. 6 35'	-15% 40'	+8% 40'	-27% 80'	
M <sup>20</sup> to 5	645.9 (645')	P.O.T.	+0045'	5.2	2.2	+5.3 ✓	+40% 100'	+25% Pt. 5 35'	-16% 150'			
M <sup>20</sup> to 4	545.8 (545')	P.O.T.	+1008'	5.2	5.2	-10.8 +10.1	+25% 100'	+51% 75'	+20% Pt. 4 20'	-22% 35'	-4% 80'	-28% 100'
M <sup>20</sup> to 3	382.6 (382')	P.O.T.	-2016'	5.2	15.2	-21.1 15.1	+43% 200'	+4% 30'	Pt. 3 -6% 200'			
M <sup>20</sup> to 2	263.7 (263')	P.O.T.	-2007'	5.2	17.2	-18.7 ✓	+44% 200'	+27% 30'	Pt. 2 -21% 40'	-10% 160'		
M <sup>20</sup> to 1	160.8 (160')	61°20' 30°40' L	-2018'	5.2	5.2	-6.5 ✓ N78°E	+35% 160'	+22% 80'	Pt. 1 -22% 80'	-10% 100'		

M<sup>3</sup> to M<sup>20</sup> → S 70° 48E

Backsight  
on M<sup>3</sup>

Sta.	Dist	Hor. & Vert. A	H.L.	Rdg Elev						
12 to 13	175.6 (175)	45° 18' R 22° 38' 30" R -1° 20'	5.2	5.2	-16.9 ✓ N 86° 30' E	+12% 100'	+2% 100'	+13 200	+2%	
11 to 12	173.9 (173)	22° 35' 30" R 45° 11' -1° 33'	5.2	5.2	-4.7 ✓ N 64° E	+22% 100'	+6% 90'	Pt. 12 125'	+8% 125'	+25% 75'
10 to 11	307.3 (307)	40 11' L 8° 21' 30" -2° 46'	5.2	5.2	-14.8 ✓ N 41° E	+8% 200'	Pt. 11 100'	+7% 100'	+25% 70'	
7 to 10	567.5 (565)	P.O.T. -1° 35'	5.1	5.1	-45.1 ✓	+7% 150'	+4% 45'	Pt. 10 200'	+9% 200'	
7 to 9	402.3 (404)	P.O.T. -1° 43'	5.1	10.4	-38.7 ✓	+20% 80'	+8% 85'	Pt. 9 100'	+4% 100'	+17% 100'
M 7 to 8	265.0 (266)	67° 56' 22° 28' L -5° 02'	5.1	5.1	-23.2 ✓ N 45° E	+12% 125'	Pt. 8 70'	-7% 70'	+6% 100'	+2% 100'

Sta.	Dist.	Hor. & Vert.	H.I.	Rod & Elev.
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15 to D32		38°30' 19°15' L		N 25° E
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13 to 15	<sup>D33</sup> 551.0 (3550)	81°09' 12°04'30" R - 0°05'	5.2	5.2	+0.8 N 44° E	+7% 150	-1% 100	-5% 150	level
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13 to 14	356.0 (355)	POT +0°31'	5.2	5.2	+3.2 N 94° E	+9% <sup>14</sup> 150	-5% 35	level	100
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Alternate from M<sup>2</sup> 11 to M<sup>2</sup> 31

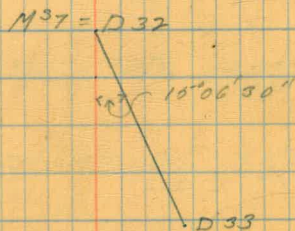
10/31/38

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Sta.	Dist.	Hor. A	Vert. A	H.I.	Rod Elev.								
4 to 5	340.9 (340)	92°40'	16°19'30" R. -1°02'	5.2	5.2	5.87° E	-6.1	+20% 75'	+8% 75'	Level 100'	Pt. 5	+4% 70'	+27% 100'
3 to 4	516.0 (515)	37°01'	18°30'30" R. -0°19'	5.1	5.1	N41° E	-2.8			+17% 100'	Level 150'	+12% 100'	
2 to 3	356.9 (356)	28°18'30"	14°09'30" L. -1°03'	5.2	5.2	N28° E	-6.5			+3% 200'	Pt. 3	+4% 100'	-7% 100'
M <sup>2</sup> 11 to M <sup>2</sup> 2	360 (363)	P.O.T.	-0°36'	5.2	5.2	N42° E	-3.8			+2% 100'	Pt. 2	-6% 25'	+5% 100'
M <sup>2</sup> 11 to M <sup>2</sup> 7	234 (233)	2°01'15"	1°00'30" R. -0°36'	5.2	5.2	N42° E	-2.4			+26% 125'	Pt. 1	-9% 50'	-2% 100'
back-sight on pt. 7b													

Sta.	Dist.	Hor. L.	Vert. L.	H.I.	Rod. + Elev.	Mag.
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Note An apparently improved location can be made by setting a point 250' perp. in the north to line between pt. 4 & 5 and 240' distant from #4. This line to hook up with pt 31 or 30 of D line. See page 78



D32 6 to 7	2010 (200')	103°05' 51°57'30\"	+0°54'	5.1	5.1	+3.1 N. 91°E	+11% 100	+17% 75	-8% 25'	level 200
4 to 6	610.8 (610)	R.O.T.	-1°06'	5.2	5.2	-11.7	+25% 100'	+4% 80'	level 200'	

Alt. line from explanatory note page 77

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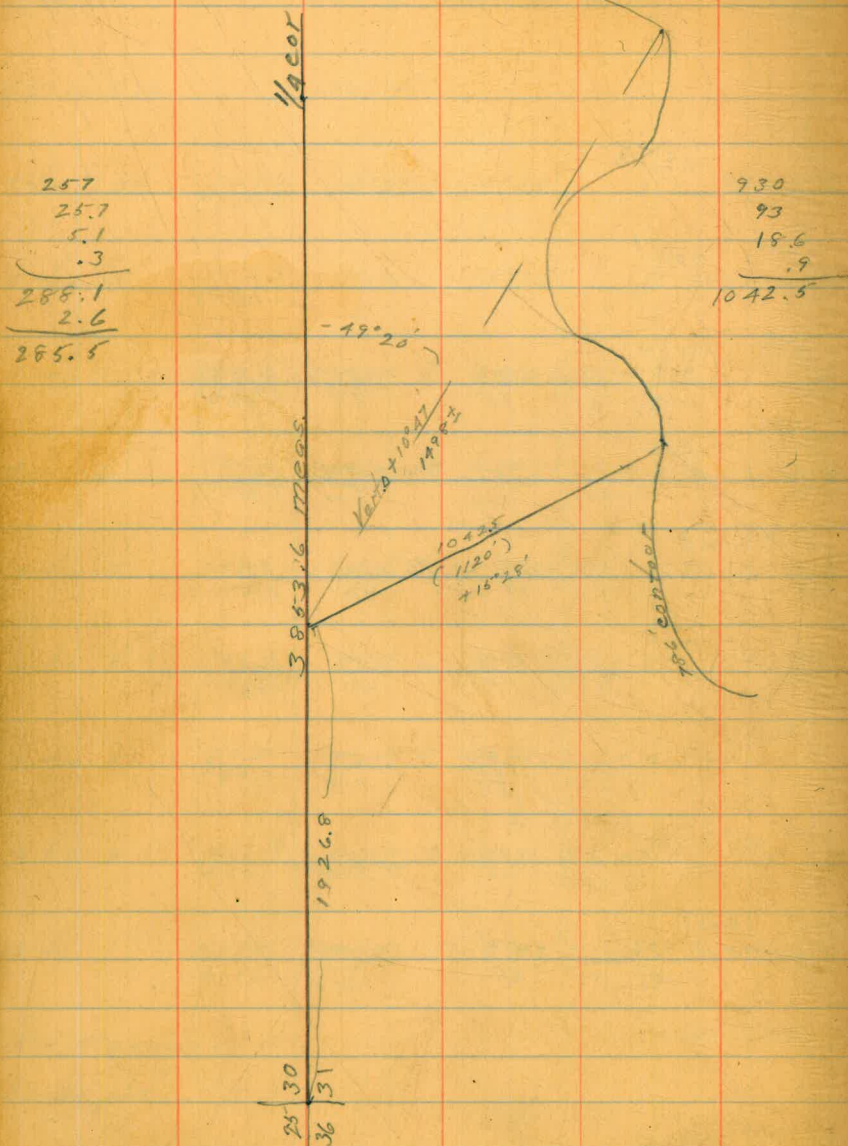
Sta.	Dist.	Hor. & Vert. A	H.L.	Rod & Elev.	Mag.	L	Φ			
D29 to D28		13°13'30"								
7 to D29	157.2 (157')	14°29' -4°06'	5.1	5.1	11.3 -11.1 N 63° E 1435.3					
7 to 8	192.3 (192')	13°56' -3°22'	5.1	2.1	8.3 -13.2 N 63° 30' E 1438.1					
4 to 7	267.2 (268')	P.O.T. -4°46'	4.9	5.9	25.2 -23.0 1446.4 -6% 100'	-12% 65'	-31% 65'	*7	+28% 50'	+13% 75'
4 to 6	173.8 (175')	30°55'30" R -6°35'	4.9	2.9	24.0 -23.9 1445.7 N 77° 30' E	-8% 100'	-25% 100'	*6	+12% 100'	+6% 75'
4 to 5	108.7 (108')	180°00' R -2°55'	5.1	8.1	8.4 -8.4 1461.3 S 46° 30' W	-19% 80'	-6% 60'	+2% *5 50'	-3% 90'	-7% 100'
2 to 4	140.7 (140')	P.O.T. -2°57'	5.1	10.1	12.1 -12.1 1469.7	-22% 150'	-7% 45'	*4	+6% 40'	Level 160'
2 to 3	89.7 (89')	P.O.T. -3°33'	5.1	5.1	5.5 -5.5 1476.4	-22% 200'	-9% 35'	*3	-3% 200'	
4 to 2	466.0 (466')	P.O.T. +1°56'	5.1	5.1	15.7 -15.7 1481.9	-21% 200'	-9% 35'	*2	Level 200'	
4 to 1	219.0 (218')	P.O.T. -0°48'	5.1	5.1	3.6 -3.6 1463.4 N 46° 30' E	-8% 100'	+11% 55'	+15% 75'	*1	-4% 150'

21.5 to 4 - 1466.2

P.M. page 76  
backsight on #3

Tie to 186' contour on W. of N.E. 1/4  
of NW. 1/4 of sec. 31

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Instr. at 36 F.S. on 37

S 74°06' W  
67°01' L  
S 70°5' W  
2148.2  
S 28°53' W

N 35°30' W

18.11  
S 25°16' W

761  
916  
303  
1980

36736  
211  
5156

127°30'

+5°40' 1270

-2°6'0"

+8°43'

1264130

7268'

63°20'

10°56'

33°14'

66°29'

16°25'

26°53'00"

76°58'30"

53°48'

153°58'00"

26°14'

153°59'55"

21°43'

76°29'00"

43°26'

58°09'30"

116°09'

17°36'30"

35°13'

999.0  
269.7  
1268.7

-4.07

6.00

-9.07

24.0

C-14.9

9.7

C-24.6

Bench Mark U.S.G.S. Lower Otay Dam

Lower Otay Dam, 33 feet S.E. of E. End  
of sec. 18. T18. S. R1E 70' E. of  
Int. of filled road with dam on  
N.W. face of Bldr. 4'x3'x2' Bronze  
Tablet stamped 486-5D. Sl. 486.569

450.0 Elev. ground at W. dam San Vicente  
452.0 bot. at W. end  
455.0 " " mid pt.  
457.0 " " E. end

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IMPROVED TABLES  
AND  
INFORMATION

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TABLE X.  
MIDDLE ORDINATES OF RAILS  
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.  
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

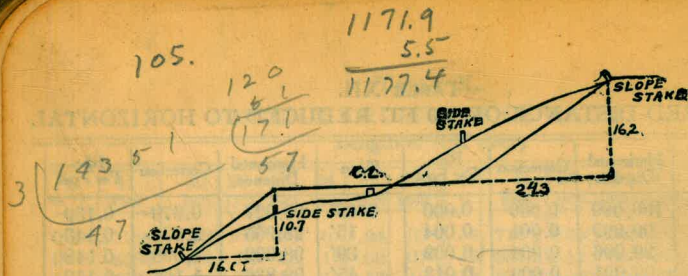
To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.  
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.  
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

722  
1177.4  
86611

1171.9  
5.5  
1177.4

72.40  
5.015  
77.415  
8.675  
68.740

27-24-30  
954-49

12.6  
2.4  
15.0

883

500

3,83

1080.6

2.7

1077.9

10.3

1056.6

V4032

5313

2656.4

13.0

101

3.8

9.3

15.6

8.1

7.5

21.3

7.5

13.8

21.1

6.0

1

28.1

8.2

19.9

19.4

13.8

5.6

33.1

13.3

19.8

13.8

6.0

13.1

46.1

1270 - 5°18'

61.

991.9

198.9

70.4

1260.7

916

761

167.7

3.03.4

1980.4

65.9.4

2639.8

303.4

306

15°20'

977.3

298.2

40.1

1310.6

86611

2.7

95611

4228

1051

1980.4

1560.4

3540.9

1310.6

4851.5

462.6

5314.1





438.6  
6.6  
432.1

over

940833  
929944  
5987  
394.8

970633  
963333  
670  
970633

281151  
279  
279

9024

298

Lot 107

state of Iowa  
car. 107

8738  
780

5400

City Man

719  
1228  
1208  
1274  
1202  
1228  
1239  
340  
639  
035  
134  
020  
219  
8514  
6506  
838  
33722  
33860  
367210  
1037  
35838

0.28  
0.03  
0.46  
0.55  
0.67  
0.58  
0.52  
12.76  
12.91  
12.83  
13.03  
6.10  
2.45  
87.06  
386.77  
386.77  
1.5

8+8  
748032  
21378  
5400

8738  
780  
57.7

Sta	Elev	H.I.	Hor. Δ	Vert. Δ	Dist.	Rod Elev.	Vert. Δ	Dist.	Rod Elev.
0+00	428.9								
+50	433.9								
1	438.6	443.4	90°	-2'00"	187	4.8			
+50	443.4								
2	447.8	452.6	90°	-2'32"	102	5.1	-1'59"	388	11.1
+50	447.8								
3	449.0	451.0	90°	-2'03"	297	11.0	-1'30"	480	17.0
+50	449.0								
4	442.2	443.0	90°	+0'22"	570	6.2			6.2
+50	442.2								
5	433.5	431.7	90°	+1'24"	440	9.0			
+50	433.5								
6	426.7	426.0	90°	+0'06"	200	4.9	+1'22"	320	7.9
+50	426.7								
7	421.1	419.1	90°						
+50	421.1								
8	418.3	418.2	90°						
+50	418.3								
9	416.6	416.6	90°	-1'50"	660	5.0	+0'31"	660	5.0
+50	416.6								
10	414.2								

(over)

16.0  
3.00

$$\begin{array}{r} 449.0 \\ -12.6 \\ \hline 436.4 \end{array}$$

$$\begin{array}{r} 445.8 \\ -10.0 \\ \hline 435.8 \\ -3.7 \\ \hline 442.1 \end{array}$$

$$\begin{array}{r} 432.8 \\ -2.9 \\ \hline 429.9 \\ -3.6 \\ \hline 436.4 \end{array}$$

$$\begin{array}{r} 420.0 \\ -10.0 \\ \hline 410.0 \\ -10.0 \\ \hline 400.0 \end{array}$$

$$\begin{array}{r} 416.6 \\ -12.4 \\ \hline 404.2 \end{array}$$