

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	II
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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of a high grade 50% Rag Paper
having a WATER RESISTING surface.

MICROFILMED

JAN 13 1965

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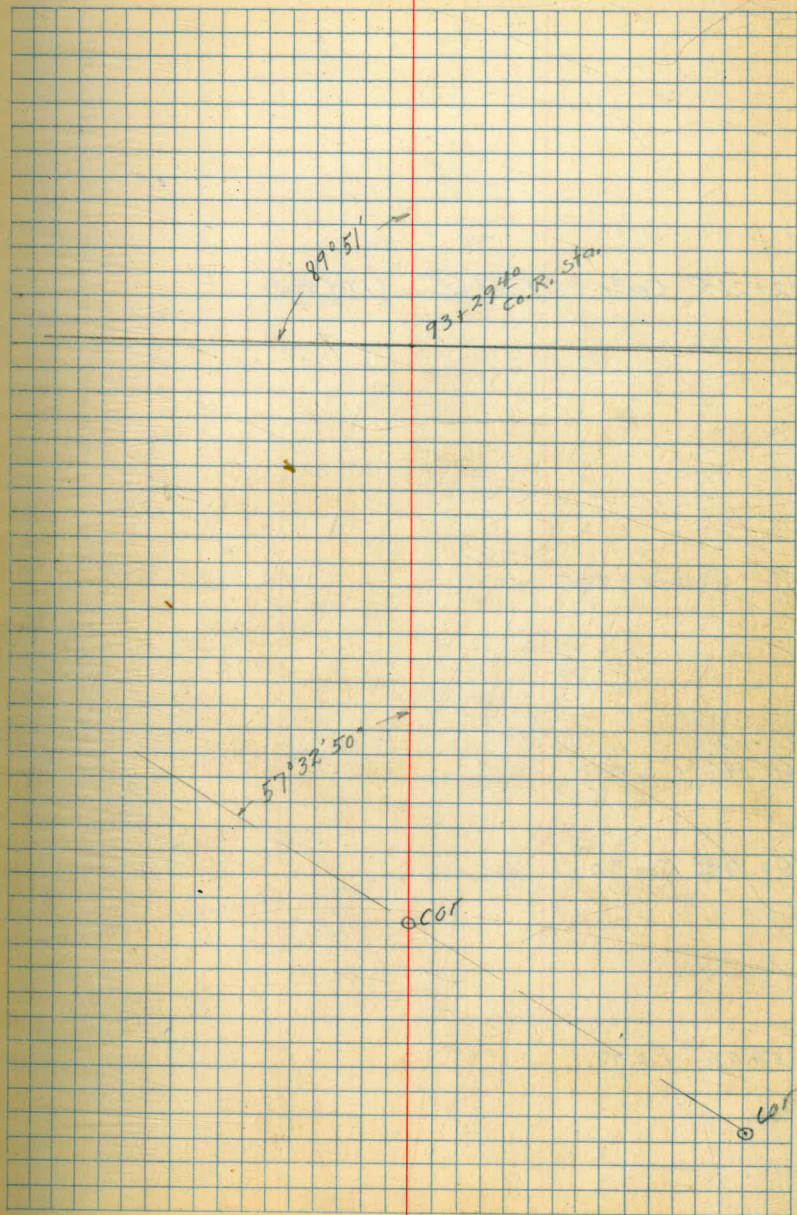
Survey of Hazard property, to pumping plant site

2+32⁶⁹ P.O.T. on boulder

0+60⁵⁰ P.O.T. Intersection with County Road Survey

0+00

1/7/42
Hill
Soper
Davis

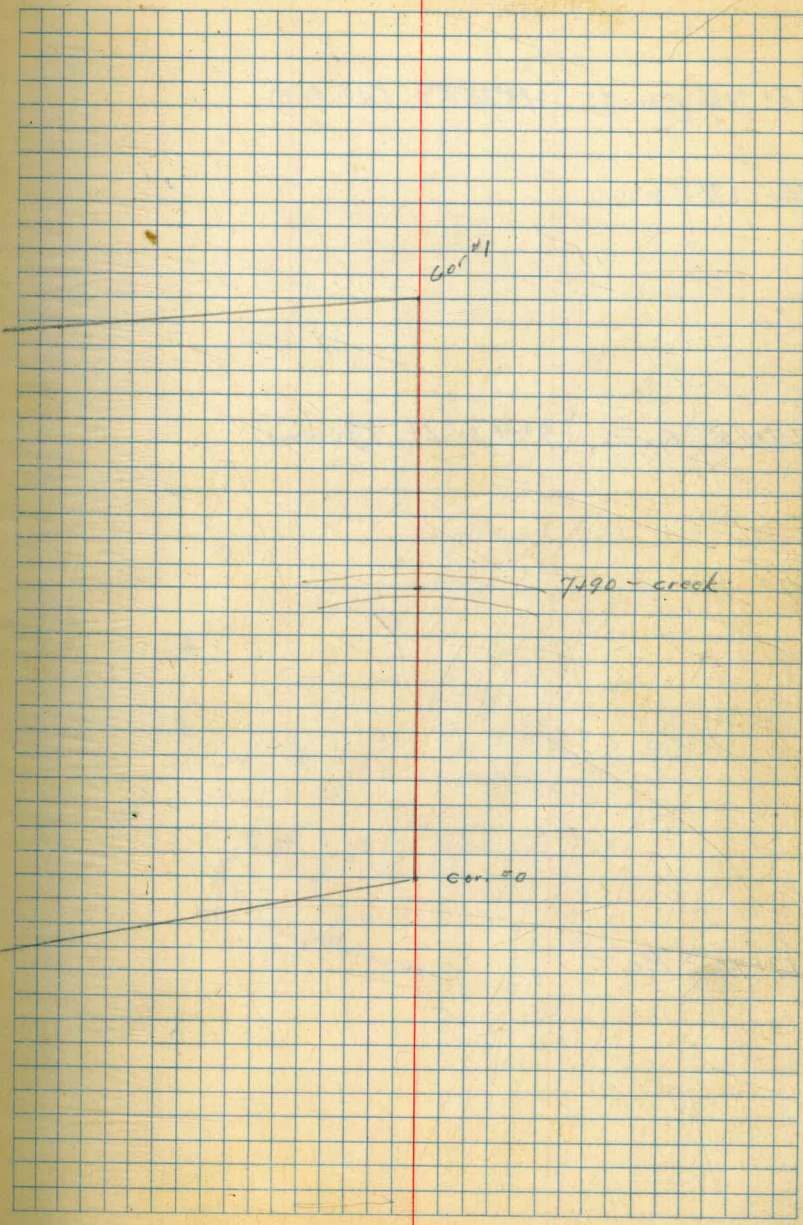


12+21²⁵ Cor #1 - 94°58' Lt (1714 feet)

6+34⁷¹ P.O.T.

6+13²⁵ Cor #0

5+04⁰⁰ P.O.T.



38+70²⁵ Cor. #3 13°34' RT (436 feet)

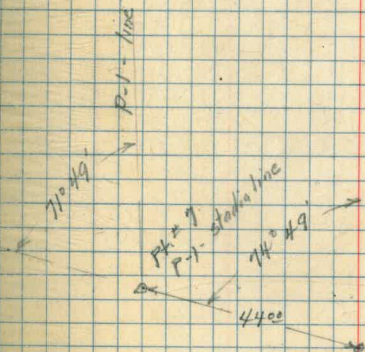
36+02²¹ P.O.T.

29+40²⁵ Cor. #2 - 9°41'30" LT (930 feet)

12+90⁸³ P.O.T.

Cor. #3

Cor. #2



56+64⁸⁷ P.O.T.

55+65²⁵ P.O.T.

43+06²⁵ Cor = 4 - 6° 11' Lt (1572 feet)

42+79⁴⁸ P.O.T.

42+38⁵⁹ P.O.T.

41+05²⁶ P.O.T.

40+35²⁶ P.O.T.

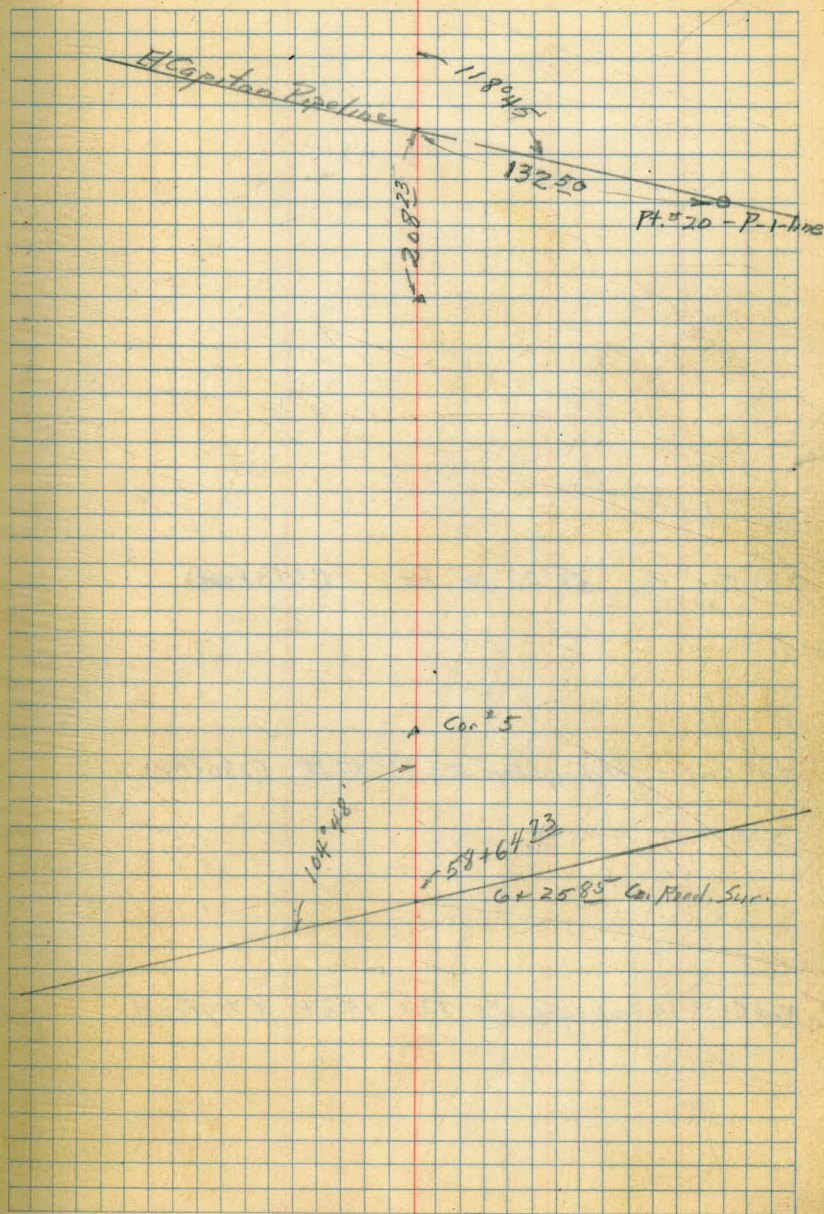
39+28⁴⁷ P.O.T.

58+78²⁵ - 10°48'40" RT - (416.3 feet)

Note: set Corner #12, from Cor. #5

58+78²⁵ Cor. #5 - 146°08'40" RT (1283 feet)

58+60¹² Intersection with Co. Road Survey



X at Cor. #13 - $51^{\circ}22'50''$ Rt (343 feet)

X at Cor. #12, backsight on #5 - $83^{\circ}17'$ Lt (280 feet)

X at Cor. #12 backsight on #5 $122^{\circ}15'$ Rt (700 feet)

— See Page 42 —

Topography at Pumping Plant site.

	16.6	122.64	U.S.G.S.	
0+00 - ϕ			15.0	107.6 ✓
110' RT Edge of wash			14.0	108.6 ✓
138' LT Toe slope			3.0	119.6 ✓
1+00 - ϕ			11.4	111.2 ✓
100' RT Edge wash			11.7	110.9 ✓
130' LT Toe slope			1.5	121.1 ✓
2+00 - ϕ			7.5	115.1 ✓
125' RT edge wash			9.0	113.6 ✓
152' LT			+7.0	129.6 ✓
180' LT			+15.0	137.6 ✓
TP	13.1	133.84	1.9	120.74 ✓
3+00 - ϕ			13.5	120.3 ✓
152' RT			18.4	115.4 ✓
245' RT edge wash			17.5	116.3 ✓
100' LT			5.2	128.6 ✓
154' LT			+4.0	137.8 ✓
178' LT			+10.5	144.3 ✓
4+00 - ϕ			11.6	122.2 ✓ ←
150' RT			16.0	117.8 ✓
40' LT			10.0	123.8 ✓
90' LT			0.0	133.8 ✓
170' LT			+8.5	142.3 ✓

1/12/42
Supt.
Nodgason
Davis

7

Top of El Capitan P.D.
at air valve 60.5' to
left of Pt # 20 - P-1 line

F.L. Grade 103.0
36" Steel Pipe 3.0
106.0
Thickness of Pipe .04
U.S.G.S. 106.04

Note: elev 99.8 city
datum - see page 27

El Capitan P.D.

4+00

3+00

2+00 = Pt # 20 of P-1 line

1+00

0+00

To San Diego

on edge of wash
from canyon to left.

Topography at alternate Pump Plant site.

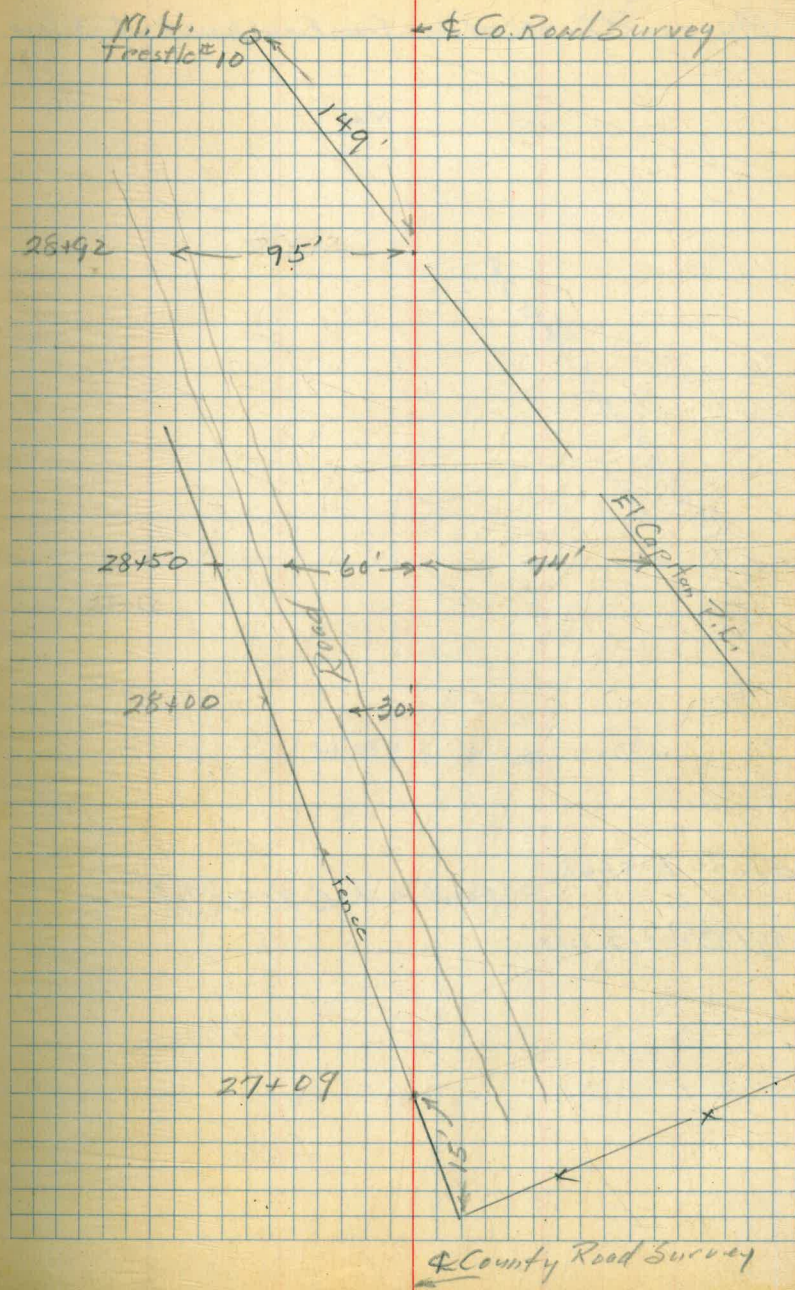
B.M.	12.06	H.I. 144.53		132.47 ✓
27409 - County road Sta.			11.7	132.8 ✓
35' RT			9.2	135.3 ✓
63' RT			5.2	139.3 ✓
83' RT			0.0	144.5 ✓
28400 - ♀			8.0	136.5 ✓
50' RT			2.2	142.3 ✓
75' RT			+4.0	148.5 ✓
15' LT			9.6	134.9 ✓
66' LT (fence line)			12.3	132.2 ✓
26450 - ♀			5.8	138.7 ✓
54' RT			0.5	144.0 ✓
74' RT			+3.0	147.5 ✓
93' RT			+9.0	153.5 ✓
40' LT			8.0	136.5 ✓
46' LT			11.5	133.0 ✓
82' LT (fence)			12.8	131.7 ✓

Cont'd on next page

1/12/42
super
Hodgeson
Davis

County B.M.
City or U.S.G.S. elev?
OK

	144.53			
28+92 - Φ pipe line	5.5	139.0	✓	
51' RT	1.0	143.5	✓	
77' RT	+7.0	151.5	✓	
64' LT	10.3	134.2	✓	
72' LT	15.1	129.4	✓	
115' LT (fence)	17.1	127.4	✓	



Murray P.L. location - from focal point - L-3 line

Mag

Realignment - Page 28

N 80° W

0400 - L-3 line

=

Focal Point - Δ 25° 22' RT

67+33⁵⁰ - L-2-line

1/21/42
H. H.
Soper
Hodgeson
Davis

10

< 9' \rightarrow 0+83 power pole

Mag
S 80° W

12+05³⁰ v. 2° 57' Rt.

11+84 - Test hole

S 77° 30 W

9+95⁵⁸ E.C.

+95⁵⁸ - 11° 12.5

+50 - 10° 20.3

9+00 - 9° 23.0

+50 - 8° 25.7

L = 22° 25' Lt

8+00 - 7° 28.4

R = 1500'

+50 - 6° 31.1

T = 297.24

7+00 - 5° 33.8

L = 586.88

+50 - 4° 36.5

B.C. - 4+08⁷⁰

6+00 - 3° 39.2

E.C. = 9+95⁵⁸

+50 - 2° 41.9

def. I = 1.146

5+00 - 1° 44.6

1° 58' = 0° 57.30

4+50 - 0° 47.3

4+08⁷⁰ B.C.

N 80° W

1/23/42
Hill
Soper
Hodgeson
Davis

11

31+76⁸⁶ F.C.

L = 10°00'14"

R 1500

+76⁸⁶ - 5°00.0

T = 131²³

450 - 4°29.2

L = 261⁸¹

31 - 3°31.9

B.C. =

150 - 2°34.6

F.C. =

30 - 1°37.3

def. 1' = 1.146

29+50 - 0°40.0

def. 50' = 0°57.30

29+15⁰⁵ B.C.

28+84 Test hole - 30' Rt

17+98⁶⁷ P.O.T.

580°W

Mag

561°W

41406²⁶ E.C.

L = 997²⁶ Lt

R = 1500

T = 1217⁸

L = 243⁰⁴

BC = 38+63²²

E.C. = 4140²⁶

def. 1' = 1.146

1.50' = 0°57.30

+06²⁶ - 4°38.5

41+00 - 4°31.3

+50 - 3°34.0

40+00 - 2°36.7

+50 - 1°39.4

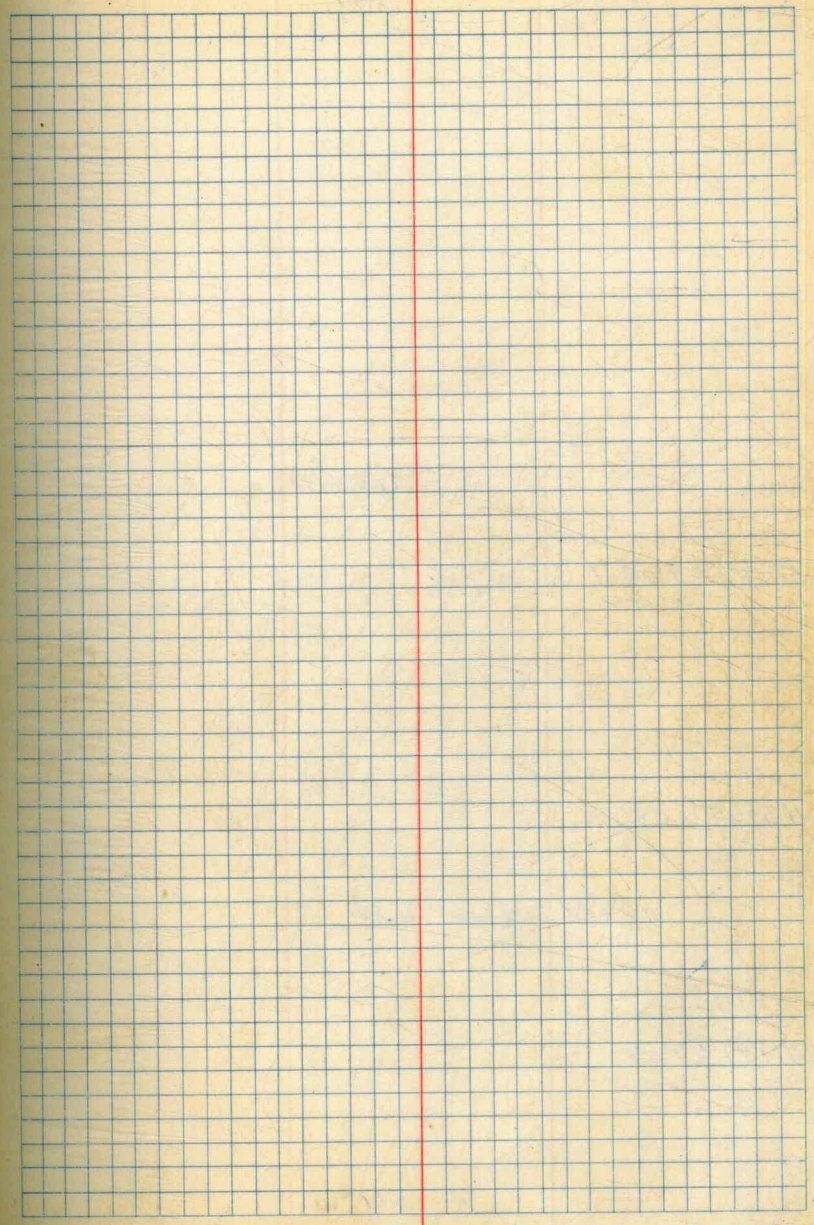
39+00 - 0°42.1

38+63²² BC

33+80⁰⁰ P.O.T.

33+08⁹⁵ P.O.T.

570°W



Mag.

559°30' W

51450° L. 1°29' Lt

43+35⁰⁰ P.O.T.

42+20 Test hole - 70' Rt

41489³⁸ P.O.T.

561° W

1/24/42
Hill
Soper
Hodgeson
Davis

14

RP. 202 p 4000
on split of C

4000 + RP. 202
on split of C

52+75 - Test hole

553°W

55+71⁴⁷ EC

L = 6046' Lt

R = 1500

T = 8868

L = 177¹³

BL = 53+94³²

EC = 55+71⁴⁷

dec 1' = 1.146

" 50' = 0.5730

+71⁴⁷ 3023'

+50 = 258.4

55+00 = 201.1

+50 = 103.8

54+00 = 006.5

53+94³² B.L.

559°30'W

1/26/42 15

L.I.I.
Soper
Hodgeson
Davis
Bowlin

R.P. 1x1" □

40°

30°

□ R.P. 2x2

R.P. 2x2 □

40°

40°

□ R.P. 2x2

22.79 changed 12/23/42
63+25²⁵ = Pt. #20 - P1-line — R.P. tubes 50' 94' 45" - 84' 60"

63+00 - Test hole

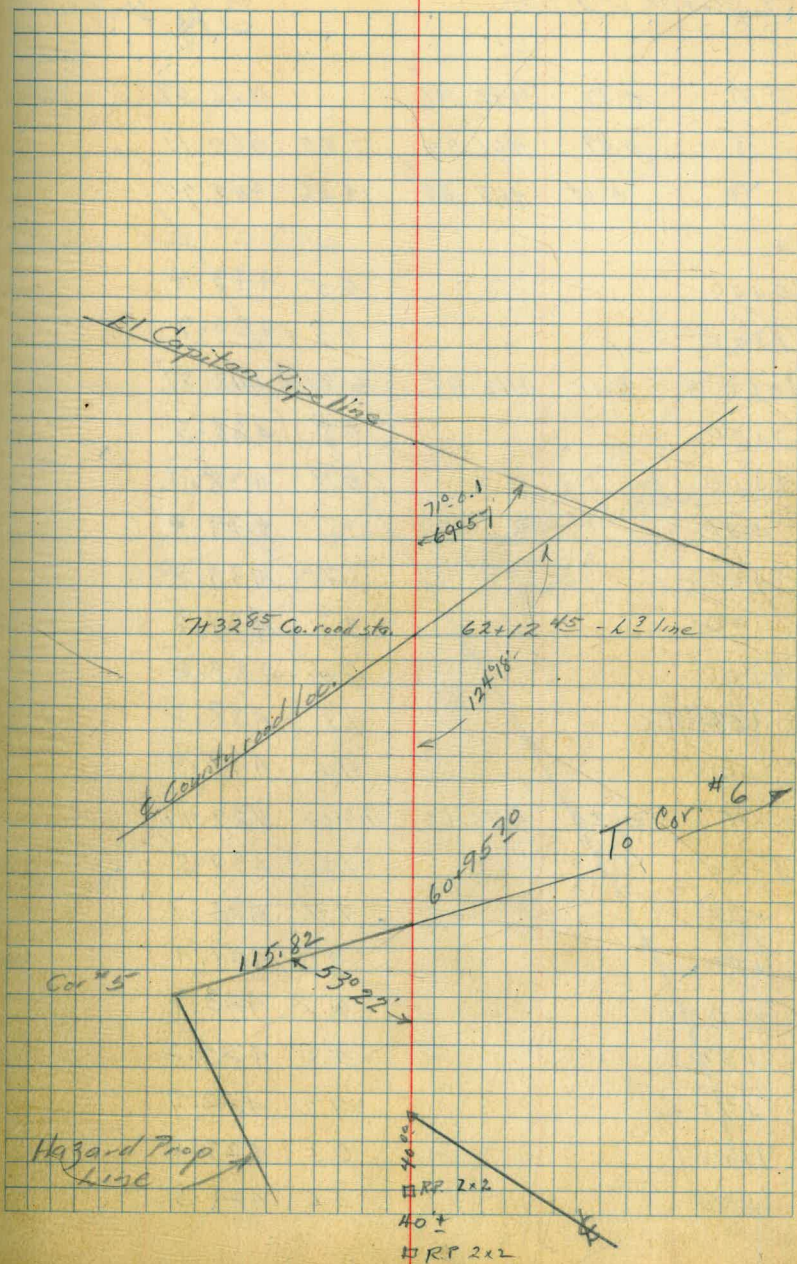
60+90 - Test hole - 175 Lt.

N83°30'W

59+36⁰⁰ 43°21' RT
41°21' changed 12/23/42

R.P. 33' Lt. 78'

S53°W



Profile L-3 line

City Datum

B.M.	0.37	472.96		472.59	✓
TP	0.89	461.00	12.85	460.11	
TP	0.14	448.88	12.26	448.74	✓
0+50			5.5	443.4	✓
1+00			8.2	440.7	✓
Set B.M.	0.11	442.98	6.01	442.87	✓
1+50			4.5	438.5	✓
2+00			4.9	438.1	✓
2+50			3.6	439.4	✓
3+00			3.7	439.3	✓
3+50			3.7	439.3	✓
4+00			4.4	438.6	✓
+087° BC.			4.8	438.2	✓
4+50			9.1	433.9	✓
TP	0.24	430.13	13.07	429.91	✓
5+00			1.6	428.5	✓
+25			4.4	425.7	✓
+50			8.7	421.4	✓
6+00			6.2	423.9	✓
+50			5.9	424.2	✓
+75			7.2	422.9	✓
7+00			6.5	423.6	✓
+50			5.6	424.5	✓

1/26/42
Super
Bowling
Hedgeson
Davis

17

Nail in power pole

0+00 = 67+33⁵⁰ L-2 line

Nail in power pole, 9' RT 0+83

See Pg. 33 for "L" 3 Revision
Notes

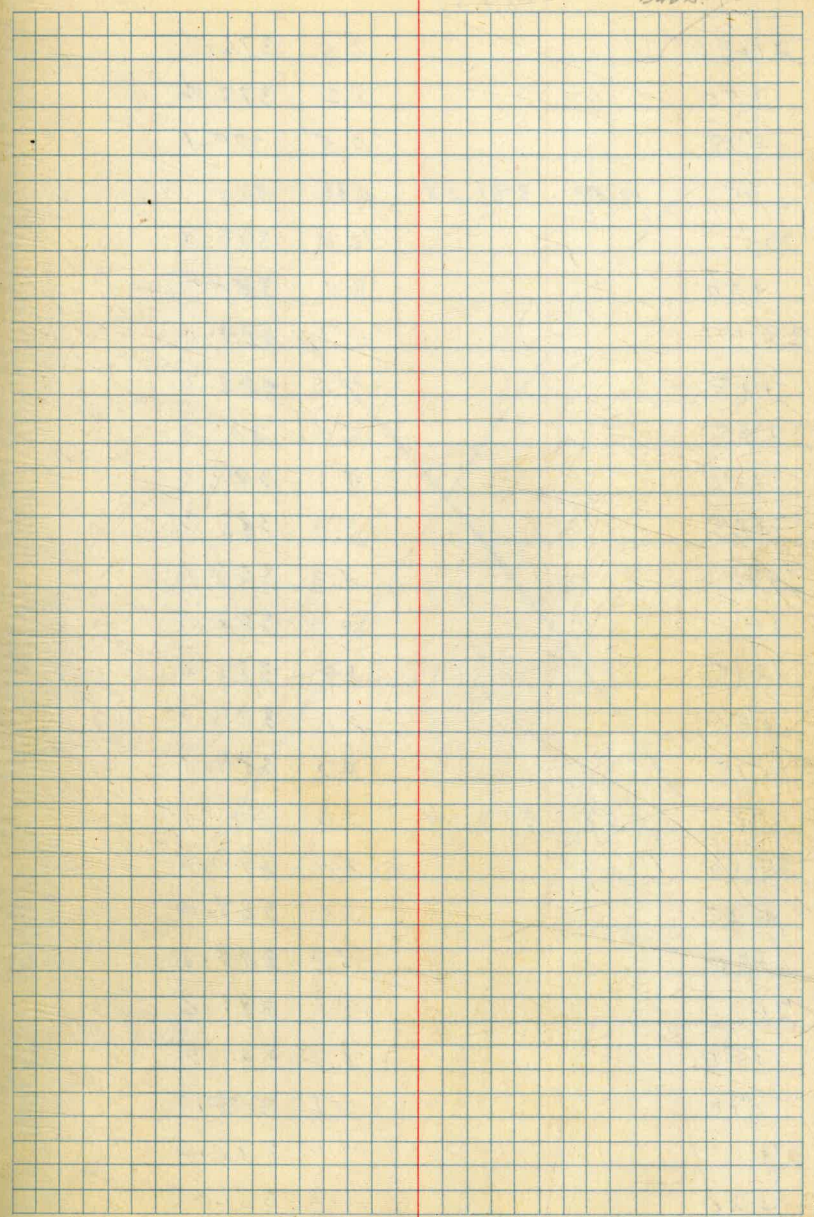
430.13

8+00			7.1	423.0	✓
+50			8.7	421.4	✓
9+00			9.8	420.3	✓
+26			10.7	419.4	✓
+50			8.3	421.8	✓
195 ⁵² FL			7.7	422.4	✓
10+00			7.6	422.5	✓
+30			5.1	425.0	✓
+50			6.1	424.0	✓
TP	4.19	428.52	5.80	424.33	✓
10+80			2.4	426.1	✓
11+00			3.3	425.2	✓
+30			1.9	426.6	✓
+50			3.7	424.8	✓
+83			4.1	424.4	✓
12+05 ³⁰			3.2	425.3	✓
+25			4.8	423.7	✓
+40			4.2	424.3	✓
+50			5.3	423.2	✓
13			7.9	420.6	✓
+50			10.5	418.0	✓
Set B.M.	0.69	416.26	12.95	415.37	✓
14+00			1.7	414.6	✓
+20			4.3	412.0	✓
+50			6.1	410.2	✓

Nail in 2x2 - 53 RT 14+00

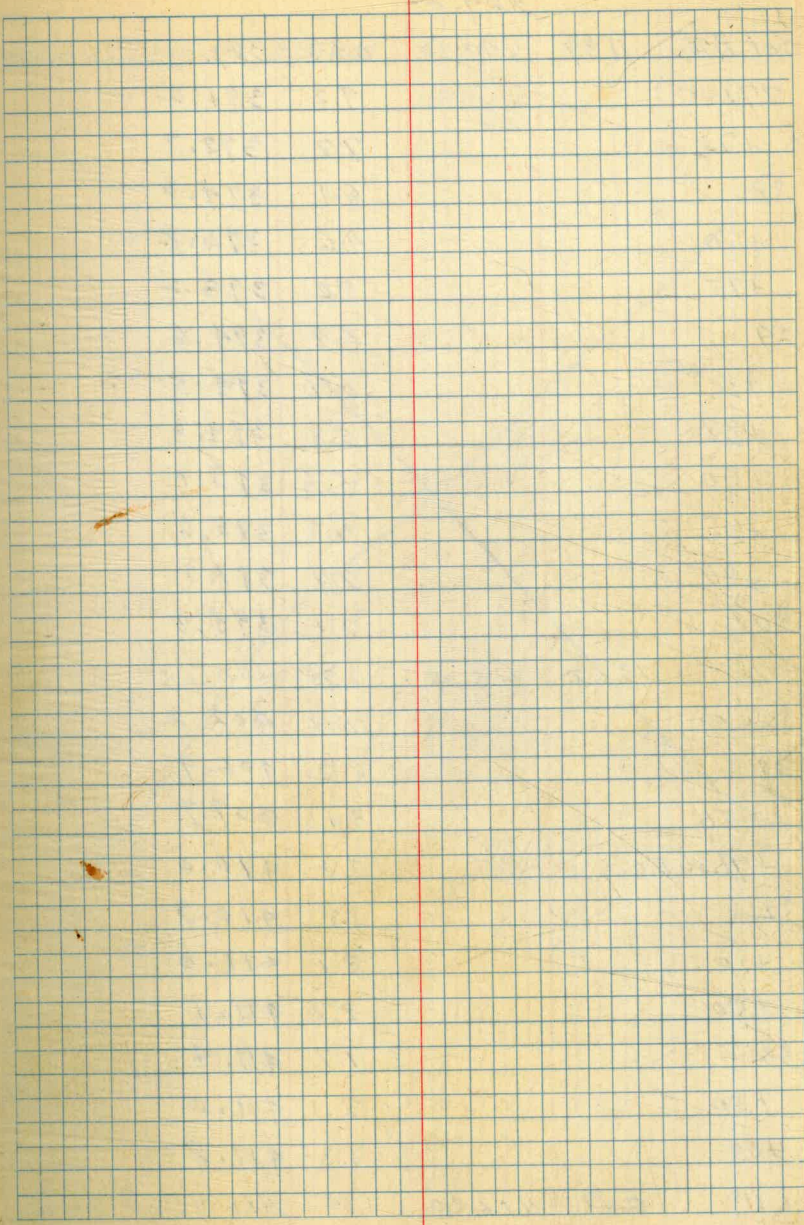
Soper
Bowling
Hedgeson
Davis

		416.26		
15400			10.0	406.3 ✓
+20			11.3	405.0 ✓
TR	0.36	403.78	12.84	403.42 ✓
15450			2.9	400.9 ✓
16			8.2	395.6 ✓
+20			10.5	393.3 ✓
+45			13.9	389.9 ✓
+50			13.4	390.4 ✓
17			12.5	391.3 ✓
TR	1.03	392.43	12.38	391.40 ✓
17450			2.9	389.5 ✓
18400			4.8	387.6 ✓
+20			5.5	386.9 ✓
+50			7.9	384.5 ✓
+75			9.4	383.0 ✓
19400			11.0	381.4 ✓
+30			13.1	379.3 ✓
TR	0.10	379.57	12.96	379.47 ✓
19450			2.9	376.7 ✓
+80			6.9	372.7 ✓
20408			13.8	365.8 ✓
+30			11.8	367.8 ✓
+60			9.7	369.9 ✓
+80			8.4	371.2 ✓
21400			5.8	373.8 ✓



379.57

21430		3.5	376.1	✓
150		2.2	377.4	✓
+75		0.5	379.1	✓
TP	12.59	0.88	378.69	✓
22		10.4	380.9	✓
+50		8.8	382.5	✓
23		6.7	384.6	✓
+15		4.6	386.7	✓
+35		5.4	385.9	✓
+50		4.3	387.0	✓
165		3.0	388.3	✓
+85		3.3	388.0	✓
24		2.4	388.9	✓
+15		1.9	389.4	✓
+50		2.1	389.2	✓
+75		2.2	389.1	✓
TP	0.67	2.31	388.97	✓
25+00		2.0	389.6	✓
+25		2.6	387.0	✓
+50		4.8	384.8	✓
26		7.8	381.8	✓
+50		8.2	381.4	✓
+70		6.1	383.5	✓
27		4.0	385.6	✓
+20		1.6	388.0	✓



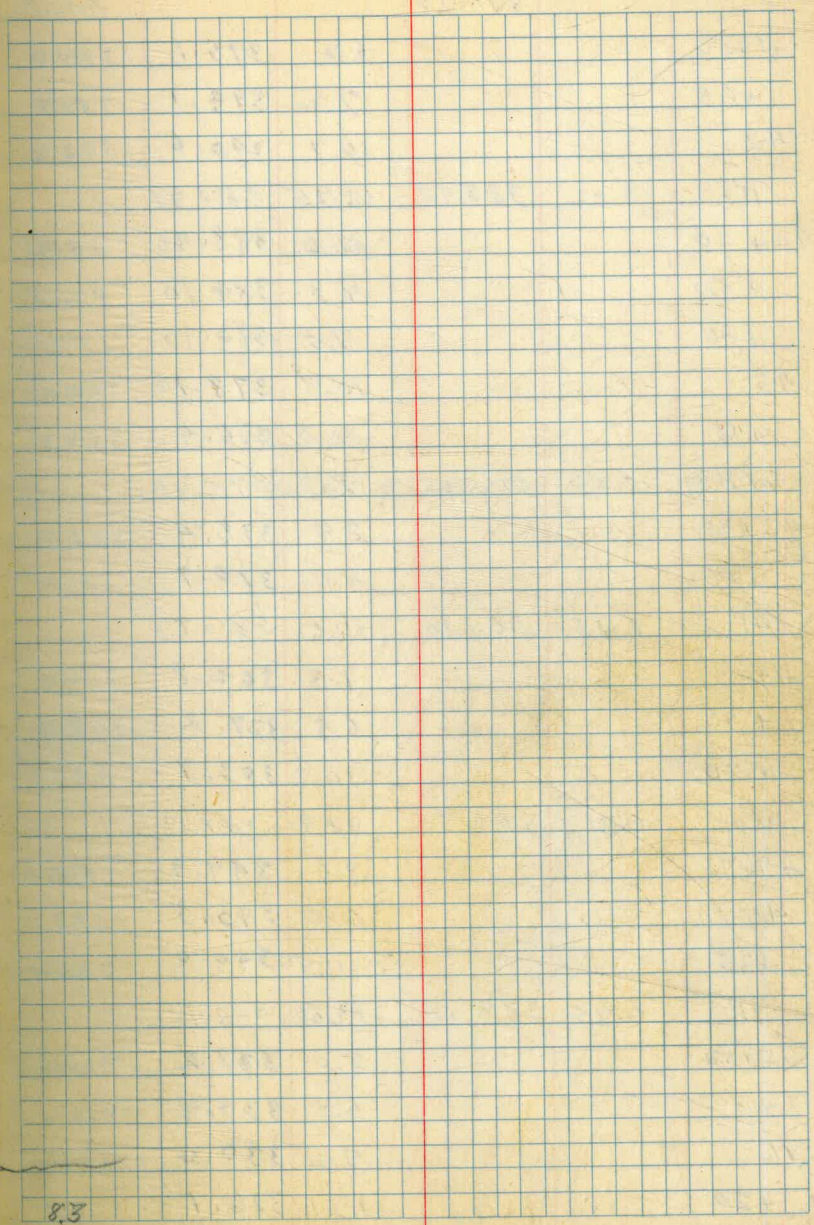
		389.64		
Set B.M	11.39	400.40	0.63	389.01
27+50			9.2	391.2 ✓
+75			7.7	392.7 ✓
28			6.1	394.3 ✓
+50			4.6	395.8 ✓
+75			5.2	395.2 ✓
29			5.8	394.6 ✓
+15 ⁰⁵ B.C.			5.7	394.5 ✓
+38			5.8	394.6 ✓
+50			5.3	395.1 ✓
+65			4.8	395.6 ✓
+80			2.7	397.7 ✓
30			2.1	398.3 ✓
TP	13.62	413.07	0.35	400.05 ✓
30+50			10.9	402.2 ✓
31			6.2	406.9 ✓
+56			3.9	409.7 ✓
+76.86 F.C.			3.1	410.0 ✓
32			2.8	410.3 ✓
+10			2.1	411.0 ✓
+50			2.0	411.1 ✓
33			1.7	411.4 ✓
+50			2.1	411.0 ✓
+80			1.3	411.8 ✓
TP	0.47	412.20	1.34	411.73 ✓

Nail in 2x2-31 RT 27+75

on 4 hub 6th 33+80

412.20

34+00			2.0	410.2	✓
+50			3.9	408.3	✓
35			6.2	406.0	✓
+50			8.2	404.0	✓
+75			8.6	403.6	✓
36			10.3	401.9	✓
TR	3.97	405.97	10.20	402.00	✓
36+50			6.2	399.8	✓
+75			7.3	398.7	✓
37			7.0	399.0	✓
+50			6.8	399.2	✓
38			5.3	400.7	✓
+50			5.0	401.0	✓
+63 ²³ BC.			4.9	401.1	✓
39			4.6	401.4	✓
+20			3.4	402.6	✓
+50			3.5	402.5	✓
+70			2.9	403.1	✓
40			3.1	402.9	✓
+25			2.7	403.3	✓
+50			4.5	401.5	✓
+85			5.6	400.4	✓
TR	0.23	401.33	4.87	401.10	✓
41			2.3	399.0	✓
41 + 06 ²⁶ EC, ahead			2.7	398.6	390.3
+1+96.38 back					



	401.33		Grade
41+50		6.2	395.1 ✓ 387.0
+65		7.2	394.1 ✓ 385.7
42		10.7	390.6 ✓ 382.3
TP	0.02	388.40	12.95 388.38
42+20		0.0	388.40 ✓ 380.1
+50		4.3	384.10 ✓ 376.5
+80		7.5	380.90 ✓ 372.8
43		10.3	378.10 ✓ 370.1
+18		12.0	376.4 ✓ 367.3
Set B.M	0.56	376.28	12.68 375.72
43+35		2.9	373.4 ✓ 365.0
+50		5.6	370.7 ✓ 362.6
TP	0.43	364.10	12.61 363.67
44		1.3	362.8 ✓ 354.9
+35		6.9	357.2 ✓ 348.9
+50		10.2	353.9 ✓ 346.3
TP	0.31	351.50	12.91 351.19
44+75		1.6	349.9 ✓ 342.0
45		6.0	345.5 ✓ 337.7
+35		11.5	340.0 ✓ 332.0
TP	0.73	339.18	13.05 338.45
45+50		2.0	337.2 ✓ 329.6
+80		5.8	333.4 ✓ 325.1
46		9.2	330.0 ✓ 322.1
+25		13.1	326.1 ✓ 318.3

Cut
8.1
8.4
8.3
8.3
7.6
8.1
8.0
9.1
Nail in 2x2 bulb - 40' RT 43+50
8.4
8.1
7.9
8.3
7.6
7.9
7.8
8.0
7.6
8.3
7.9
7.8

		288.36		Grade
51+50	L		3.8	284.6 ✓ 275.4
52			9.3	279.1 ✓ 269.6
+10			10.4	278.0 ✓
Set B.M.	0.23	276.83	11.76	276.60 ✓
52+40			4.1	272.7 ✓
+50			6.7	270.1 ✓ 262.2
+62			9.1	267.7 ✓
TP	0.26	264.10	12.93	263.90 ✓
53			2.1	262.0 ✓ 253.9
+50	"		10.6	253.5 ✓ 246.4
TP	0.28	257.33	13.05	251.05 ✓
53+94 ³²	B.C.		3.8	247.5 ✓
54			4.5	246.8 ✓ 238.9
+50			12.3	239.0 ✓ 231.4
TP	0.15	238.68	12.80	238.53 ✓
54+15			3.4	235.3 ✓
55+00			7.1	231.6 ✓ 223.9
+25			10.3	228.4 ✓
TP	0.49	226.07	13.10	225.58 ✓
55+50			1.5	224.6 ✓ 216.3
+71 ⁴⁷	F.C.		4.9	221.2 ✓
56			9.2	216.9 ✓ 208.6
TP	0.20	213.42	12.85	213.22 ✓
56+22			0.2	213.2 ✓
+50			5.6	207.8 ✓ 199.4

Cut	
9.2	
9.5	
Nail in 2x2-40' RT 52+30	
7.9	
8.1	
9.1	X
7.9	
7.6	
7.7	
8.3	
8.3	
8.4	

		213.42		Elev	Grade
56+78			12.1	201.3	✓
TP	0.53	201.19	12.76	200.66	✓
57+00			4.2	197.0	189.1
+20			7.4	193.8	✓
Set B.M.	0.49	188.71	12.97	188.22	✓
57+50			1.0	187.7	179.1
+35			7.6	181.1	✓
58			10.8	177.9	169.1
TP	0.37	176.34	12.74	175.97	✓
58+20			3.8	172.5	✓
+35			6.0	170.3	✓
+50			9.5	166.8	158.7
+65			12.6	163.7	✓
TP	0.54	163.97	12.91	163.43	✓
59			6.6	157.4	148.0
+17			10.2	153.8	✓
TP	0.93	151.97	12.93	151.04	✓
59+26			1.3	150.7	✓
+36 ⁰⁰ L			4.1	147.9	139.3
+50			7.2	144.8	135.8
+68			12.3	139.7	✓
TP	0.13	139.27	12.83	139.14	✓
59+75			2.4	136.9	129.1
TP	0.47	126.66	13.08	126.19	✓
60+00			2.7	124.0	116.0

Cut

7.9
Nailin 2x2 - 56 Lt 56+65
8.6
8.8
8.1
9.4
8.6
9.0
7.8
7.7

Note in computing
 Quantities use new align-
 ment & grades from Am.
 Pipe Co. sheets
 See page 69

	126.66		Elev	Grade
60+13			8.1	118.6
+25			11.1	115.6 104.0
+30			13.0	113.7
TP	0.70	114.60	12.76	113.90
60+50			6.0	108.6 ✓ 102.1
+80			7.8	106.8 ✓
+87			6.4	108.2 ✓
61			6.4	108.2 ✓ 100.1
+20			7.0	107.6 ✓
+30			8.7	105.9 ✓
+40			9.0	105.6 ✓ 100.1
+45			7.3	107.3 ✓
+50			6.9	107.7 ✓ 100.3
62			6.8	107.8 ✓ 101.3
+50			6.4	108.2 ✓ 102.2
Set B.M.	7.60	115.38	6.82	107.78 ✓
63+00			6.6	108.8 ✓ 103.2
+25 ²⁵			6.6	108.8 ✓
TP	3.13	105.45	13.06	102.32 ✓
TP	4.48	97.63	12.30	93.15 ✓
cken B.M.			6.93	90.70 ✓
B.M.	1.65	109.43		107.78 ✓
			9.60	99.8 ✓ City datum

11.6
6.5
8.1
5.5
7.1
6.5
6.0
S.K. Cor. Man hole chamber 68 Lt, 63+25 ²⁵
6.6
County B.M. (U.S.G.S etc) Marked elev 96.63 6.12 90.51 City datum
Top of Al Capitan Pk. at air valve 605 Lt of FT #20 - P-1-line See page 7 this book

Alignment revision - L-3-line

Mag.

577°30'W

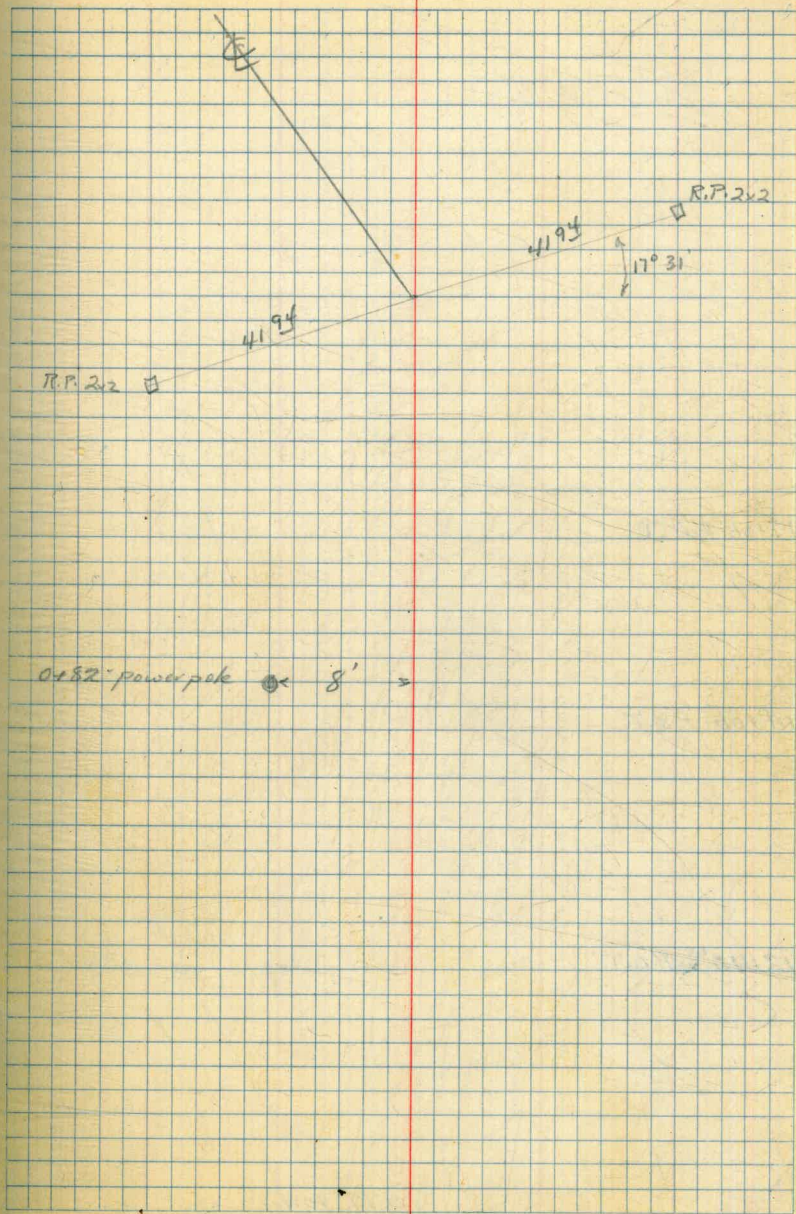
5483⁰⁰ L 35°02' Lt.

N67°W

0+00 - L-3-line (Focal point) L 38°03'30" Rt
67+33⁵⁰ - L-2-line

2/6/42
Hill
Soper
Bowlin
Davis

28



19+00 P.O.T.

14+00 P.O.T.

12+70⁰⁰ P.O.T.

577°30W

R.P. 2m \square 40⁰⁰ 40⁰⁰ \square R.P. 2x2

Mag.

West

26+91⁴⁵ E.G.

$\Delta = 12^{\circ} 37' R$

R = 1000'

T = 110.55

L = 220.20

B.C. = 24+71²⁵

E.G. = 26+91⁴⁵

def. 1' = 1.719

def. 50' = 1^o 25.944

+91⁴⁵ - 6^o 18.5

+50 - 5^o 07.2

+26+00 - 3^o 41.3

+50 - 2^o 15.4

+25+00 - 0^o 49.4

24+71²⁵ B.C.

577^o 30' W

2/7/42

Hill

Soper

Bowling

Davis

30

RP 2x2 40^o 40^o RP 2x2

RP 2x2 40^o 40^o RP 2x2

Mag

561'30" W

34+9714 EC

$\Delta = 29^{\circ} 01' 14''$

$R = 1000'$

$T = 258.77$

$L = 506.44$

BC 29+9070

BC 34+9714

def 1 = 1.719

def 50 = 1°25.744

19714 = 14°30.5

+50 = 13°09.5

34+00 = 11°43.5

+50 = 10°17.6

33+00 = 8°51.6

+50 = 7°25.7

32+00 = 5°59.8

+50 = 4°33.8

31+00 = 3°07.9

+50 = 1°41.9

30+00 = 0°15.9

29+90.70 BC

2/9/42
Hill
Super
Bowlin
Davis

31

R.P. 2x2 @ 40°

40° @ R.P. 2x2

R.P. 2x2 @ 40°

40° @ R.P. 2x2

(To page 13)

41406³⁶ ahead (E.G. of prev. line)
 =
 41496³⁸ back (P.O.T.)

P.I. of curve on prev. line.
 =
 40474⁶⁰ P.O.T.

RP 2x2 = 4000

4000 = RP 2x2

± profile, L-3 revision

			Elev	Grade
B.M.	4.90	447.77	442.87	✓
0+00			446.2 ⁴	438.3
0+50			448.1 ⁴	435.9
1+00			441.8	434.1
1+50			440.3	433.2
2+00			440.4	433.2
+50			441.6	433.1
3+00			442.4	433.1
+50			443.4	433.0
4+00			442.6	433.0
+50			441.1	432.7
+80			442.0	432.4
5+00			440.8	432.3
+20			439.0	431.8
+50			440.1	✓
+83 A			438.5	✓
6+00			437.9	✓
+30			438.3	✓
+50			436.8 ²	428.1
7+00			435.3	426.3
TP	0.75	435.65	434.90	
7+50			433.1	424.5
+75			431.2 ⁸	423.6
8+00			430.6	422.7

2/9/42

33

Super
Bowlin
Davis

cut

Nail in power pole, 9' Pt. 0+83

8.1
8.2
7.7
7.1
7.2
8.5
9.3
10.4
9.6
8.4
9.6
8.5
7.2
8.1
9.0
8.6
8.1
9.6
8.6
8.2
7.9

Note: cut 5+83 replaced by curve.
See Am. Pipe & Const. Co. drawing
"4-2958"

Sta	Elev	Grade	Cut
5+23.74 ahead			
5+20.15 back			
5+39.54	439.3	431.3	8.0
5+71.14	439.2	430.6	8.6
6+02.74	438.0	429.9	8.1
6+34.34	438.3	428.7	9.6

	435.65 ✓		Elev	Grade	Cut
8+05		5.6	430.1 ✓	422.5	7.6
+27		4.6	431.1 ✓	421.7	9.4
+50		6.5	429.2 ✓	420.9	8.3
+90		7.5	428.2 ✓	419.5	8.7
9+10		8.7	427.0 ✓	419.1	7.9
+35		9.9	425.8 ✓	417.9	8.0
+50		9.7	426.0 ✓	417.3	8.7
+90		11.6	424.1 ✓	416.5	7.6
10+00		11.2	424.5 ✓	416.3	8.2
+20		9.9	425.8 ✓	416.3	9.5
+50		11.1	424.6 ✓	416.2	8.4
+80		11.1	424.6 ✓	416.2	8.4
11+00		9.9	425.8 ✓	416.2	9.6
+20		10.3	425.4 ✓	416.2	9.2
+50		11.1	424.6 ✓	416.1	8.5
12+00		11.2	424.5 ✓	416.1	8.4
+17		10.8	424.9 ✓	416.0	8.9
+50		12.0	423.7 ✓	416.0	7.7
+65		10.4	425.3 ✓	415.9	9.4
+90		12.4	423.3 ✓	415.4	7.9
TP	0.70	424.55	11.80 423.85 ✓		
13+00		1.0	423.6 ✓	415.1	8.5
+25		2.8	421.8 ✓	414.0	7.8
+50		2.7	421.9 ✓	412.9	9.0
+70		4.3	420.3 ✓	411.7	8.6

		424.55		Elev	Grade
14+00			5.2	419.4	409.8
+20			8.1	416.5	408.2
+50			8.4	416.2	405.8
+65			9.8	414.8	404.6
+78			13.4	411.2	403.6
ck. on B.M.			8.98	415.57	Rec elev 415.57
TP	0.52	412.15	12.92	411.63	✓
15+00			1.9	410.3	406.8
+50			7.5	404.7	397.1
+75			9.4	402.8	394.8
16+00			11.8	400.4	392.5
TP	1.26	400.55	12.86	399.29	✓
16+10			0.6	400.0	391.5
+35			3.9	396.7	388.9
+50			5.9	394.7	387.3
+70			57	394.9	387.3
+85			6.6	394.0	387.3
17+00			5.4	395.2	387.3
+15			4.6	396.0	387.2
+50			4.9	395.7	387.2
18+00			4.4	396.2	386.7
+50			6.4	394.2	385.4
19+00			9.6	391.0	382.7
TP	0.65	388.64	12.56	387.99	
19+50			2.3	386.3	379.1

5'4
14+54

cut	
9.6	
8.3	
10.4	
10.2	
7.6	
Nail in 2x2 5' H 14+54	
8.5	
7.6	
8.0	
7.9	
8.5	
7.8	
7.4	
7.6	
6.7	
7.9	
8.8	
8.5	
9.5	
8.8	
8.3	
7.2	

	388.64		Elev.	Grade	Cut
19+70			3.4 385.2	377.3	7.9
20+00			6.4 382.2	374.3	7.9
+30			9.1 379.5	370.6	8.9
+50			12.1 376.5	367.9	8.6
IT	1.89	377.93	12.60 376.04		
21+00			9.8 368.1	360.1	8.0
+35			16.6 361.3	353.3	6.0
+50			14.8 363.1	355.7	7.4
+70			9.7 368.2	358.0	10.2
22			8.7 369.2	361.4	7.8
+25			4.8 373.1	363.8	9.3
+50			3.3 374.6	366.2	8.4
IT	12.72	390.24	0.41 377.52		
22+70			13.2 377.0	367.8	9.2
+85			13.4 376.8	368.9	7.9
23			11.0 379.2	370.1	9.1
+40			8.8 381.4	372.5	8.9
+50			8.6 381.6	373.1	8.5
60			8.9 381.3	373.7	7.6
24+00			6.5 383.7	376.1	7.6
+50			3.5 386.7	378.1	8.6
+71 ²⁵ BC			2.1 388.1	378.7	9.4
IT	3.69	391.77	2.16 388.08		with hub
25			4.0 387.8	379.1	8.7
+25			4.4 387.4	379.0	8.4

	391.77		Elev.	Grade
25+50			4.8 387.0	378.5
26			7.5 384.3	376.3
+50			11.1 380.7	372.9
+91.45 EC			13.5 378.3	370.7
27+00			12.6 379.2	370.3
+25			12.8 379.0	371.4
+50			10.3 381.5	372.9
28			6.9 384.9	376.8
+50			3.3 388.5	380.2
+60			2.4 389.4	380.6
TP	13.01	403.53	1.25 390.52	
28+85			13.0 390.5	381.4
29			13.1 390.4	382.1
+50			12.3 391.2	382.9
+80			11.5 392.0	383.3
+90.70 BC			12.0 391.5	383.4
30			12.2 391.3	383.5
+25			11.5 392.0	384.2
+50			9.9 393.6	384.9
31			8.5 395.0	387.2
+50			4.6 398.9	390.4
+65			4.1 399.4	391.6
32			0.9 402.6	394.7
TP	12.71	415.41	0.83 402.70	
+30			10.4 405.0	396.6

Cut
8.5
8.0
7.8
7.6
8.9
7.6
8.6
8.1
8.3
8.8
9.1
8.3
8.3
8.7
8.1
7.8
7.8
8.7
8.8 X
8.5
7.8
7.9
8.4

	415.41		Elev.	Grade	Cut
32+50			9.5 405.9	397.7	8.2
33+00			7.4 408.0	400.0	8.0
+50			5.1 410.3	401.4	8.9
34+00			4.8 410.6	401.9	8.7
+18			4.6 410.8	401.7	9.1
+50			5.0 410.4	401.4	9.4
+97.4 F.C.			6.0 409.4		
35+00			6.1 409.3	400.1	9.2
+50			8.1 407.3	399.0	8.3
36			9.5 405.9	397.9	8.0
+50			10.4 405.0	397.0	8.0
37			11.7 403.7	395.9	7.8
+50			12.6 402.8	394.8	8.0
TP	4.58	407.61	12.38 403.03		
38			6.2 401.4	394.0	7.4
+30			5.7 401.9	394.0	7.9
+50			5.7 401.9	394.0	7.9
+75			4.8 402.8	394.0	8.8
39			4.8 402.8	394.0	8.8
+50			5.0 402.6	394.0	8.6
40			5.0 402.6	394.0	8.6
+20			4.4 403.2	394.0	9.2
+50			4.4 403.2	394.0	9.2
41			4.5 403.1	393.7	9.4
+20			4.6 403.0	393.2	9.8

	407.61	✓	Elev.	Grade
41+50			6.4 401.2	392.5
170			7.0 400.6	391.7
41+96.35 Back			9.0 398.6	390.3
41+66.26 ahead				
TP	0.62	395.19	13.04	394.57
TP	0.48	383.66	12.01	383.18
ck on B.M.			7.97	375.69
				Rec. elev 375.92

Cut

87

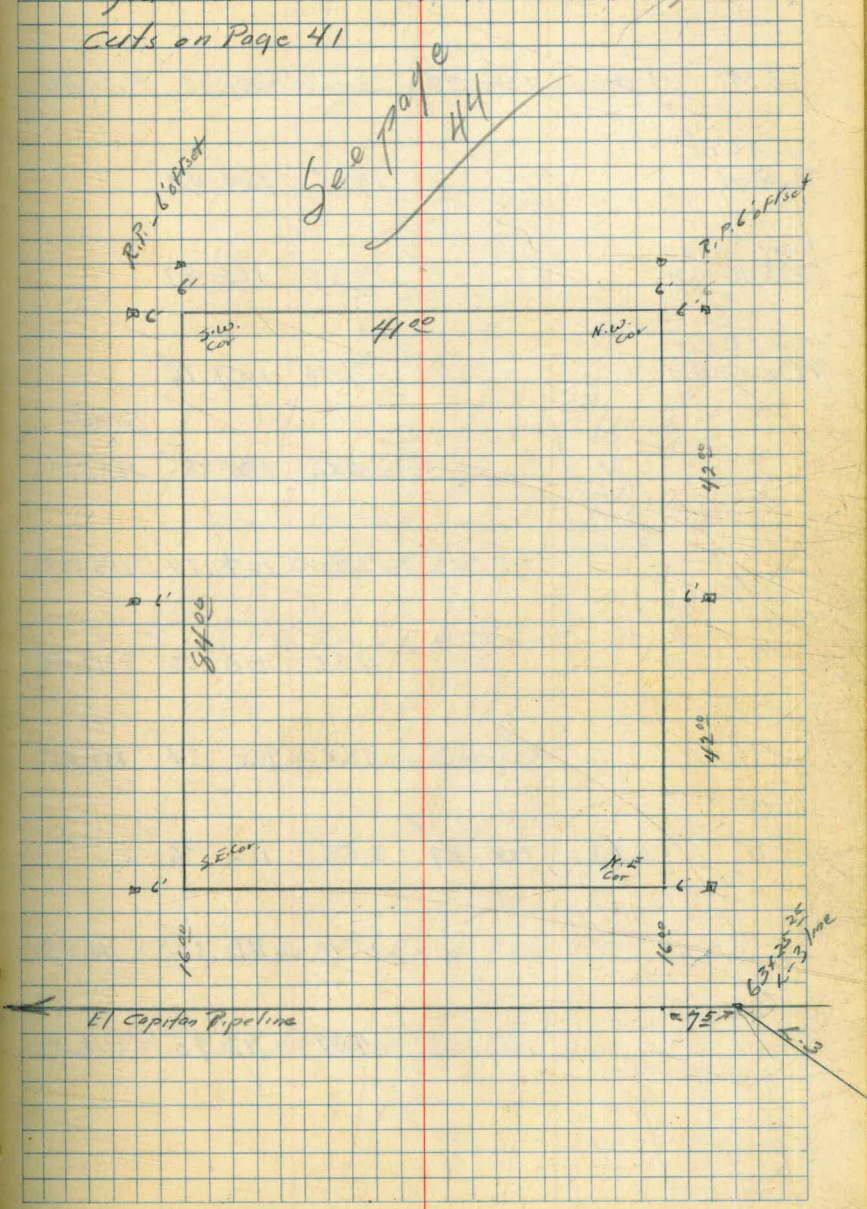
89

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See bottom page 22

Nail in 2x2 hub 40' R4.43+50

Layout for excavation - Alvarado Pump Plant
cuts on Page 41



Offset cuts for Alvarado Pump Plant.

B.M.	716	114.94	107.78	City datum
Top. E.C.P.L. By M.H.		10.45	104.49	
Top. E.C.P.L. 33' N. M.H.		9.07	105.87	
Top. E.C.P.L. 74' N. of M.H.		7.18	107.76	
				Grade
	4.56	110.38	111.55	
	7.20	107.74	111.55	
	4.39	110.55	111.55	
	2.60	112.34	111.55	
TP	5.93	118.29	2.58	112.36
		1.97	116.32	111.55
		4.39	113.90	111.55

See page 45

2/19/42
Hill
Soper
Bowlin
Davis

S.E. Cor M.H. Chamber	68' Lt	63.25
F-1.17	R.P. to No. of N.E. Cor.	
F-3.81	R.P. to So. of S.E. Cor.	
F-1.00	R.P. to So. on E of cut	
C-0.79	R.P. to No. on E of cut	
C-4.77	R.P. to No. of N.W. Cor.	
C-2.35	R.P. to So. of S.W. Cor.	

X-sections for topog. - Alvarado Pump Plant.

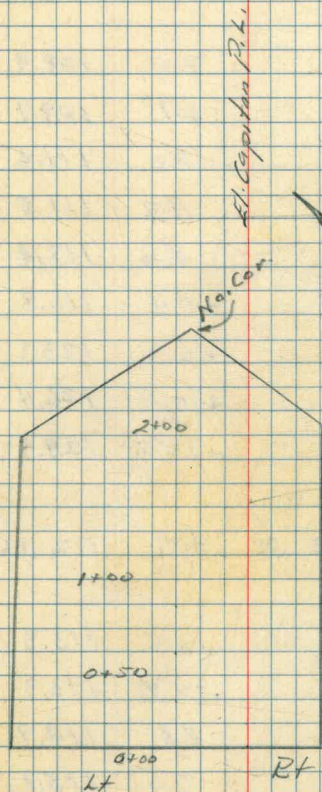
	8.57	116.35	107.78	City datum
0+00 - ϕ			12.7	103.7
25' RT			13.6	102.8
0+00 - 50' LT			11.0	105.4
" 100' LT			6.2	110.2
" 121' LT			2.4	114.0
" 150' LT			+7.5	123.9
" 177' LT			+16.3	132.7
0+50 - 25' RT			11.1	105.3
0+00 - ϕ			11.1	105.3
" 40' LT			9.4	107.0
" 100' LT			4.1	112.3
" 136' LT			0.0	116.4
" 150' LT			+4.6	121.0
" 181' LT			+14.8	131.2
1+00 - 25' RT			8.6	107.8
" ϕ			9.2	107.2
" 50' LT			5.7	110.7
" 100' LT			1.7	114.7

2/19/42

Hill
Joper
Bowling
Davis

42

All sections taken at 90°, Rt or Lt of
El Capitan Pipeline



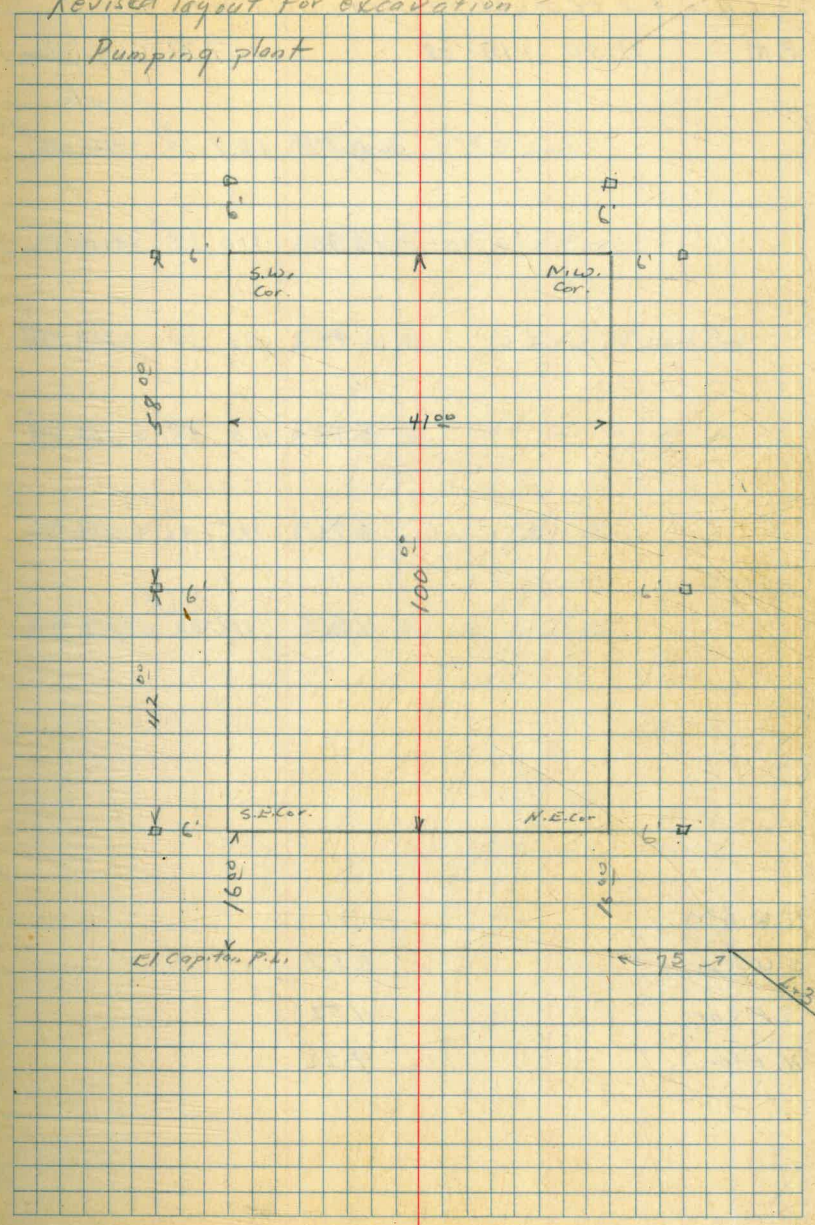
	116.35		
1+00-125' Lt		+1.5	117.9
" 140' Lt		+4.5	120.9
" 173' Lt		+12.5	128.9
1+50-25' Rt		7.5	108.9
" ϕ		6.7	109.7
" 11' Lt		5.0	111.4
" 30' Lt		4.9	111.5
" 50' Lt		4.0	112.4
" 100' Lt		+0.4	116.8
" 150' Lt		+6.9	123.3
" 164' Lt		+10.0	126.4
" 174' Lt		+13.5	129.9
IP	11.56	123.72	4.19
			112.16
2+00-25' Rt		10.4	113.3
" ϕ		10.4	113.3
" 38' Lt		8.8	114.9
" 50' Lt		7.9	115.8
" 100' Lt		3.3	120.4
" 142' Lt		+2.7	126.4
" 164' Lt		+7.8	131.5
On No. Con. Pump. Plant.		7.6	116.1

see sketch - page 42

2/29/42
Super
Bowling
Downs

Revised layout for excavation

Pumping plant



Saper
Davis
Bowlin

Cuts for excavation - Pumping Plant

B.M.	11.50	119.28	107.78	City datum
				Grade
	11.54	107.74	110.32	
	8.90	110.38	110.32	
	6.94	112.34	110.74	
	8.73	110.55	110.74	
	3.92	115.36	111.32	
	1.26	118.02	111.32	

N.W. Cor.	1.71
S.W. Cor.	3.57
S.E. Cor.	11.52
N.E. Cor.	9.22

F-2.58	R.P. to So. of S.E. Cor.
C-0.06	R.P. to No. of N.E. Cor.
C-1.60	R.P. to No. - 42' West of East line
F-0.19	R.P. to So. " " " " "
C-4.04	R.P. to So. of S.W. Cor.
C-6.70	R.P. to No. of N.W. Cor.

B.M. 8.60 116.38 107.78

6.61 109.77 110.32

5.92 110.46 110.32

5.73 110.65 110.74

5.36 111.02 110.74

4.14 112.24 111.27

4.49 111.89 111.27

B.M. 12.56 120.34 107.78

3.87 116.47 111.32

2.29 118.05 111.32

F-0.6 S.E. Cor

C-0.2 N.E. Cor

F-0.1 42' West - No. side

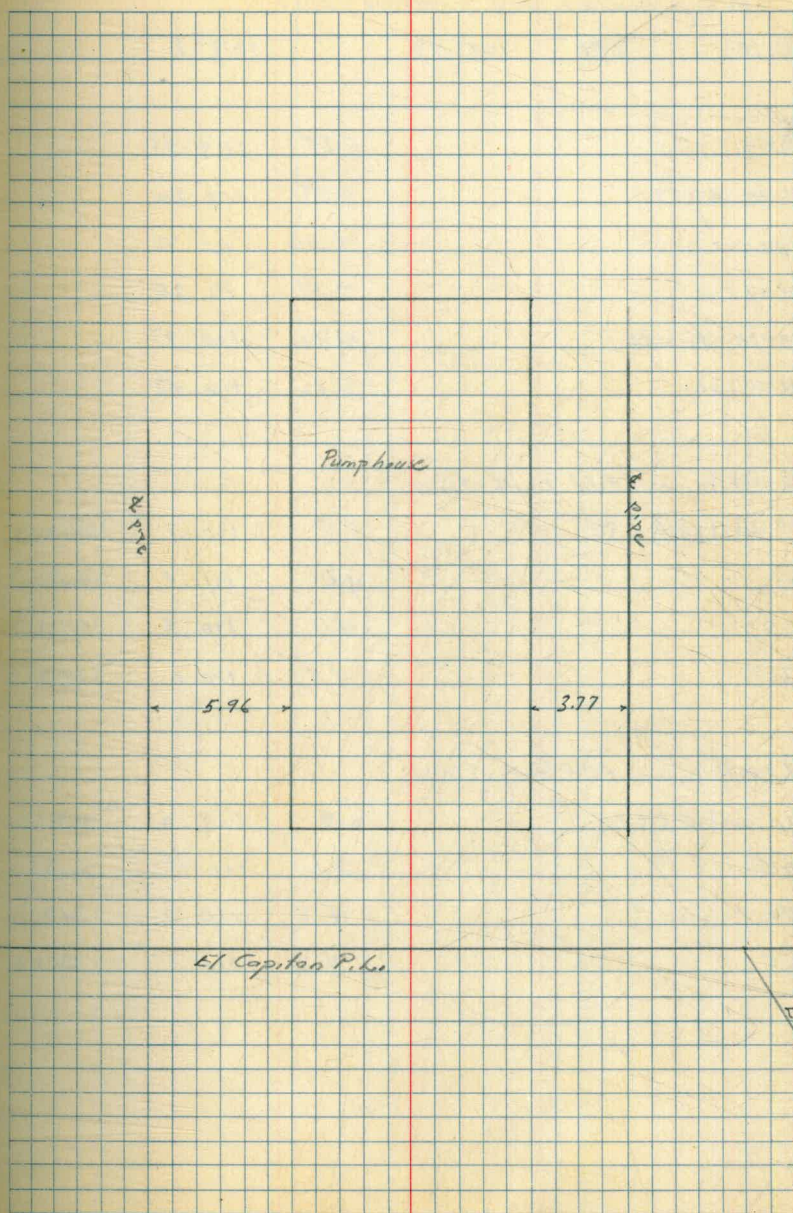
C-0.3 42' West - So. side

C-1.0 95' West - So. side

C-0.6 95' West - No. side

S-1.5 R.P. 6' west of S.W. Cor

L-7.3 R.P. 6' West of N.W. Cor.



Pump house - and pipeline cuts.

B.M.	7.81	115.59	107.78
SE. Cor Bldg.		5.84	109.75
center So. side		4.49	114.90
SW cor		4.20	111.39
N.W. cor		4.24	111.35
center - No. side		4.72	110.87
N.E. Cor.		5.12	110.47

Profile, manifold North of house

15' west of F.C.P.L.	5.5	110.1	104.2
40' " " "	4.6	111.0	104.2
65' " " "	4.7	110.9	104.2
86' " " "	4.5	111.1	104.2

Profile, manifold South of house

15' west of F.C.P.L.	6.4	109.2	104.3
25' " " "	5.2	110.4	104.3
50' " " "	4.7	110.9	104.3
65' " " "	4.3	111.3	104.3

C 5.9
C 6.8
C 6.7
C 6.9
C 4.9
C 6.1
C 6.6
C 7.0

3/23/42

49

N.H.
Super
Bowler
Davis

Grades - Pump house

B.M.	8.02	115.80	107.78	sub grade
S.E. Cor. 2' off			5.90	109.90
NE. " "			5.46	110.34
center N. side 2' off			5.00	110.80
" S. Side "			4.66	111.14
S.W. Cor 2' off			4.29	110.51
N.W. " "			4.57	111.23

(bottom of cone)

F - 0.07

C - 0.37

C - 0.63

C - 0.97

C - 1.14

C - 0.86

Res. at N.W. cor. pump plant tract

	13.01	120.79	107.78
S.E. Cor. Residence			1.10
R	8.25	129.02	0.02
N.E. Cor. Residence			7.6
N.W. " "			2.6
S.W. " "			4.7

Cuts for Manifold pipe

B.M. 8.18 115.96 107.78

N.E. Cor	3.98	111.98	104.21
" 1	3.98	111.98	"
" 2	3.99	111.97	"
" 3	4.01	111.95	"
" 4	3.98	111.98	"
" 5	3.99	111.97	"

S.W. Cor	3.93	112.03	104.27
" 1	3.93	112.03	"
" 2	3.94	112.02	"
" 3	3.95	112.01	"
" 4	3.95	112.01	"
" 5	3.97	111.99	"

7.77
7.77
7.76
7.74
7.77
7.76
7.76
7.76
7.76
7.75
7.74
7.74
7.72

check on top of Manifold pipes

B.M. 4.26 112.04 107.78

4.73 107.31

4.67 107.37

B.M. 4.63 112.41 107.78

5.10 107.31

B.M. 3.82 111.60 107.78

4.25 107.35

Top of North 36" I.D. Pipe (0.02 ft wrapping)

" " South " " " " " "

Top of So. 36" I.D. Pipe No wrapping

Soundings to determine loc. of old earth dam at Murray

10/20/42 - 10/21/42 ⁵²

BM. 4.95 440.71 5-35-46
 4.92 535.49 = 100.0' cm

But 24 (East end)

Stadia dists from $\frac{1}{2}$ walk of multiple arch dam.

23

22

21

20

19

18

17

16

15

14

Take this one

Res. gauge	Res. gauge	Res. gauge	Res. gauge	Res. gauge	Res. gauge	Res. gauge	Res. gauge
73.1	72.7	71.8	70.1	66.6	63.1		
13.5	13.9	15.2	16.5	20.0	23.5		
29	40	52	96	150	182		
62.4	61.6	60.4	59.4	60.8	60.6	61.6	65.4
17.4	13.0	26.0	26.8	25.8	26.0	27.0	30.8
32	65	60	80	100	128	155	210
58.8	58.3	62.6	65.4	66.5	89.5	84.6	52.4
27.8	28.3	24.0	21.0	20.3	27.3	32.0	34.0
47	66	81	94	125	167	191	220
62.4	62.4	62.4	62.4	62.4	62.4	62.4	62.4
22.0	22.0	20.6	20.2	22.2	25.0	32.0	40.2
33	112	119	129	145	192	230	257
62.4	60.4	60.3	65.6	66.4	80.6	80.6	44.6
22.3	26.0	26.3	21.0	20.4	32.0	36.0	42.0
33	77	112	127	136	185	215	266
54.4	51.6	57.3	65.4	66.6	49.6	48.6	42.4
27.2	28.0	29.3	24.8	20.1	37.0	38.0	42.2
42	72	110	135	146	190	227	253
29.0	29.0	32.3	32.0	20.3	21.0	46.0	46.0
32	63	75	130	140	154	199	240
50.4	50.6	48.6	65.9	66.9	46.2	31.6	20.6
36.0	36.0	38.0	20.7	20.7	40.4	55.0	66.0
43	77	102	148	160	185	205	250
45.6	41.6	40.4	40.8	65.1	64.4	42.6	28.6
41.0	22.0	46.0	45.8	20.9	21.7	44.0	58.0
48	56	71	105	152	183	195	220
43.2	44.4	31.0	37.3	65.6	65.6	53.6	34.6
48.4	57.2	55.0	49.3	21.0	21.0	32.0	52.0
49	81	101	113	100	175	193	220
29.6	20.1	28.6	66.4	65.6	26.9	18.6	15.3
47.0	66.5	58.0	21.2	21.0	60.7	68.0	73.1
57	89	109	164	176	255	286	325

(cont.)

But

13

12

11

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6

25

	22.4	14.0	14.6	65.1	66.1	25.1	22.6	15.6	26.1	28.6
Gaugo 86.6	64.2	72.6	72.0	21.5	21.5	61.5	64.0	71.0	60.8	58.0
	61	78	84	171	180	281	287	282	380	425
	12.6	20.6	65.6	65.6	28.6	41.0	36.6			
	70.0	66.0	21.0	81.0	40.0	45.0	50.0			
	70	99	178	193	270	322	210			
	2.6	3.6	38.1	45.6	65.6	51.6	52.6	55.1	44.1	
	65.0	63.0	28.5	21.0	21.0	35.0	29.0	21.5	42.5	
	73	100	129	186	197	228	223	319	390	
	34.0	31.6	34.6	46.1	66.1	65.6	48.6	58.6	51.0	51.5
	44.5	52.6	55.0	52.0	40.5	20.5	21.0	38.0	28.0	29.0
	48	58	91	108	154	195	206	242	267	276
	13.9	33.8	46.6	63.9	66.0	57.6	62.5	63.7	58.1	
	42.7	52.8	40.0	20.7	20.6	29.0	27.1	22.9	28.5	
	52	70	133	200	213	232	253	315	488	
	44.6	44.6	46.5	58.5	65.0	67.6	71.6	73.8	72.3	
	40.0	42.1	40.1	28.3	21.6	19.0	15.0	12.8	14.3	
	43	60	92	158	187	225	250	267	360	
	53.7	62.9	64.7	78.7	86.6					
	32.9	31.7	21.9	7.9	0.0					
	47	83	128	183	197					
	61.4	64.2	10.9	86.6						
	26.2	22.4	15.7	0.0						
	38	59	98	139						
	70	74.8	75.3	71.9	66.8					
	96	11.8	11.3	14.7	19.8					
	25	70	84	120	170					

← approx. old barn

Profile 10' offset hubs - Murray P.h.

King
Hymark
12-23-42

	BS	HI	FS	Elev.	Grade
B.M.	Top of air valve Cham.	El Capitan P.h.	107.78		
	4.65	112.43			
63+00			4.0	08.4	107.7
62+50			4.8	07.4	102.7
62+00			4.6	07.8	101.3
61+50			5.3	07.1	100.3
61+40			5.7	06.7	100.1
61+00			5.3	07.1	100.1
60+75			4.7	07.7	100.1
60+50			1.5	10.9	102.7
T.P.			0.85	111.58	
	12.12	123.70			
60+25			8.2	15.5	104.0
T.P.	0.46		0.46	123.24	
	12.09	135.33			
60+00			10.6	24.7	116.6
T.P.			0.26	135.07	
	12.59	147.66			
59+75			10.5	37.2	129.1
59+50			6.1	41.6	135.8
T.P.			0.61	147.25	
	12.51	159.56			
Δ 59+36			16.4	43.2	139.3
59+25			9.5	50.1	142.1

10' offset grades

54

Cut

Cut

~~12.52~~
~~5.7~~

47.54

6.5

6.8

6.6

7.0

7.6

8.2

11.5

8.1

8.1

5.8

3.9

8.0

Used Am. Pipe Co.
align. & grades,
see page 69.

	B.S.		I.S.	Elm.	Grade
59+00		159.56	4.5	55.1	148.0
58+75			0.1	59.5	153.5
T.P. ^{offset} hub	12.86	172.32	0.10	159.46	
58+50			7.7	64.6	158.7
T.P.	13.06	185.10	0.28	172.04	
58+00			8.6	76.5	169.1
T.P.	12.75	197.13	0.72	184.38	
57+50			10.0	87.1	179.1
57+00			0.4	96.9	189.1
B.M. 56+Lt.			8.95	188.22 188.12	correct
T.P. ^{hub} 57	12.30	209.10	0.37	196.86	
56+50			2.3	86.8	199.4
T.P.	12.95	221.28	0.77	208.35	
56+00			6.3	215.0	208.6
E.C. 55+71 ⁴⁷			1.6	219.7	213.1
T.P.	12.66	233.84	0.10	221.18	
55+50			11.5	22.3	216.3
55+00			5.8	28.0	223.9
T.P.	12.19	245.67	0.31	237.52	
54+50			10.2	35.5	231.7
54+00			1.5	44.2	238.9
53+99 ²			0.6	45.1	
T.P.	12.85	249.97	9.05	236.62	
T.P.	12.65	261.90	02.2	249.25	

55
X

cut
7.1
6.0
5.9
7.4
8.0
7.6
7.4
6.4
6.6
6.0
4.1
4.1
5.3
T.P. on Hub - 48' Lt. 53+99 ²

		241.90			
53+50			10.4	51.5 ✓	246.4
53+00			2.0	59.9 ✓	253.9
T.P.	12.76	273.42	0.84	61.06 ✓	
52+75			9.6	63.8 ✓	257.9
52+50			5.2	68.2 ✓	262.2
TP	12.77	^{286.03} 285.99	0.20	²⁶ 273.22 ✓	
52+25			11.5	74.5 ✓	266.1
52+00			7.8	78.2 ✓	269.6
51+75			4.7	81.3 ✓	272.7
51+50			2.2	83.8 ✓	275.4
T.P.	12.77	⁹² 297.88	0.88	¹⁵ 285.4 ✓	
51+25			11.5	86.4 ✓	277.7
51+00			9.9	88.6 ✓	279.6
50+75			8.8	89.1 ✓	281.1
50+50			7.6	90.3 ✓	282.3
50+00			5.4	92.5 ✓	284.8
49+50			2.5	95.4 ✓	287.3
49+00			0.4	97.5 ✓	289.8
T.P. ^{ON} _{Q19}	12.67	²¹ 310.46	³⁸ 0.39	^{297.84} 299.49 ✓	
48+50			10.00	300.2 ✓	292.6
48+25			7.6	02.6 ✓	294.3
48+00			6.5	03.7	296.3
47+75			4.3	05.9	298.6
47+50			1.0	09.2 ✓	301.2
T.P. ^{NEW} _{Q19}	12.90	¹³ 322.44	⁰⁹⁸ 1.62	²³ 309.44 ✓	

56
x

Cut	
5.1	
6.0	
5.9	
6.0	
8.4	
8.6	
8.6	
8.9	
8.7	
8.9	
8.0	
8.0	
7.7	
8.1	
7.9	
7.6	
3.3	
7.9	
7.3	
8.0	

		13 322.24		King Hyman 12-30-42	
47+25			10.4	11.6 ⁷	304.1
47+00			7.1	15.9 ^{15.9}	307.3
46+75			3.5	18.6 ⁶	310.8
46+50			0.3	21.7 ⁸	314.5
T.P. ^{enging} 46+50	12.81	334.55 ^{.64}	0.32 ^{.30}	321.72 ^{.83}	
46+00			5.3	29.3 ⁷	322.1
T.P.	12.43	346.47 ^{.60}	0.47 ^{.47}	339.34 ^{.13}	
45+50			10.2	36.5 ⁴	329.6
45+00			1.9	44.2	337.7
T.P.	12.46	358.27 ^{.51}	0.57 ^{.55}	345.94 ^{.60}	
44+50			5.8	52.7	346.3
T.P.	12.62	370.58 ^{.73}	0.41 ^{.40}	359.96 ^{.51}	
44+00			9.2	36.4 ⁵	354.9
43+50			1.1	69.6	362.6
T.P.	12.45	382.05 ^{.60}	1.13	369.45	
43+25			8.6	73.6	366.5
43+00			5.4	76.7	370.1
42+75			1.7	80.4	373.4
T.P.	12.53	394.62 ^{.23}	0.27 ^{.35}	381.55 ^{.70}	
42+25			7.5	86.7	379.6
42+00			5.2	89.0	382.3
41+75			2.5	91.7	384.8
T.P.	12.65	406.69 ^{.29}	0.22 ^{.64}	393.44 ^{.59}	
41+40			10.8	395.4	387.9
41+06.26E			8.5	97.7	390.3

41+96.38 Back

7.6					
7.7					
7.8					
7.3					
7.2					
6.8					
7.0					
6.9					
6.6					
7.0					
7.0					
6.6					
7.0					
7.1					
6.7					
6.9					
7.5					
7.4					

		406. ²⁴ ₂₉			
41+75			6.7	99.5	391.5
41+50			5.7	100.5	392.5
41+00			3.9	02.3	393.7
40+50			3.8	02.4	394.0
40+00			4.0	02.2	394.0
39+50			4.0	02.2	394.0
39+00			4.3	01.9	394.0
38+50			5.0	01.2	394.0
T.P. ⁴⁶⁶ _{392.00}	7.93	409. ²⁴ ₀₈	^{4.93} 4.94	³¹ 401.45	
38+00			8.5	100.7	394.0
37+50			7.1	02.1	394.8
37+00			5.5	03.7	395
36+50			4.7	04.5	397.0
36+00			3.7	05.5	397.9
35+50			1.5	07.7	399.0
35+00			0.2	09.0	400.1
T.P. ^{9.111} ₃₅₁₀₀			0.24	109.02 408.84	
B. 111	L734+60 - 80'			411.73	
	3.40	415.13			
34+50			4.6	10.5	401.4
34+00			4.4	10.7	401.9
33+50			5.0	10.1	401.4
33+00			7.0	08.1	400.1
32+50			8.7	06.4	397.7
32+00			12.0	03.1	394.5

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86
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KING
OTTUM
2-17-43

60

		3.97.12		Elev	Grade
B.C. 24+71 ²⁵			3.7	389.4	378.7 379.4
T.P.	12.12	401.47	3.77	289.35	
B.M. hubb + 90' - 24+71			6.05	395.42	X
24+25	0.37	395.81	8.4	87.4	377.4 OK
24			9.5	86.3	376.1
23+50			12.11	83.7	373.1
T.P.	080		12.62	383.19	
23		383.99	2.4	81.6	370.1
22+50			2.5	79.5	366.2
22			10.5	72.5	361.4
T.P.	791		12.09	371.10	
21+40		379.01	12.6	66.4	354.6
21+20			12.8	66.2	357.2
21+00			9.6	69.4	360.1
20+75			8.6	70.4	364.1
20+50			5.0	74.0	367.7
20+25			0.3	78.7	371.3
T.P.	984		0.33	378.68	
20+00		388.52	7.2	81.3	374.3
19+75			5.0	83.5	376.9
19+50			4.4	84.1	379.1
T.P. G.M. 19730	12.79		4.36	384.76	
19+00		396.95	8.0	89.0	382.7
18+50			4.2	92.8	385.4
18+25			2.8	94.2	386.3
17+75			2.4	94.6	87.2
17+50			2.6	94.4	87.2
17			3.2	93.8	87.3
16+50			1.0	96.0	87.3

					10.7
					10.0
					10.2
					10.6
					11.5
					13.3
					11.1
					11.8
					9.0
					9.3
					6.3
					6.1
					7.4
					7.0
					6.6
					5.0
					6.3
					7.4
					7.9
					7.4
					7.2
					6.5
					8.7

445.58

6+3429	8.2	37.4	29.1
6+02.74	7.6	38.0	29.9
5+71 ¹⁰	6.4	39.2	30.6
5+19.59	6.3	39.3	31.3
5+00	5.7	39.9	32.3
4+50	4.8	40.9	32.7
4+00	3.2	42.4	32.0
3+50	2.8	42.8	33.0
3+00	3.7	41.9	33.1
2+50	4.5	41.1	33.1
2+00	6.0	39.6	33.2
1+50	5.8	39.8	33.2
1+00	4.2	41.4	34.1
0+50	2.2	43.4	35.9
0+00	0.0	45.6	38.3
B.M. 1+450	10.57	34.96 35.01	

62

8.3
8.1
8.6
8.0
7.6
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8.6
6.9
6.6
7.3
7.5
7.3

		53.90			
+25			1.2	52.7	446.2
47			0.2	53.7	46.5
+75			1.4	525	46.3
+58			0.8	53.1	45.6
+25			2.0	H.L. 51.7 51.9	44.4
96				H.L. 50.0	42.8
+75				H.L. 48.6	40.7
+50				45.3	38.2
T.P.	0.47	46.83	7.54	46.36	
+25			4.6	42.2	35.7
45			6.6	40.2	32.7
+75			8.5	38.3	29.2
T.P.	0.41	34.31	12.93	53.90	
+25			5.7	28.6	21.0
4.4				H.L. 25.0 23.9	16.5
T.P.	2.93	24.07	12.67	21.64	
43+45			10.2	H.L. 14.0 13.8	06.3
43+85			10.0	19.1	06.8
+58			5.0	19.1	12.8
T.P.	12.29	35.95	0.41	23.66	
42			9.1	26.9	19.3
+75			6.9	29.1	22.8
+58			4.5	31.5	24.2
+25			3.1	32.9	25.9
41			1.4	34.6	27.2
+50			1.0	35.0	29.8

65					
7.2					
6.2					
7.5					
7.3					
7.2	-Rd.				
7.9					
7.1					
6.5					
7.5					
9.1					
7.6					
8.5					
7.4					
7.9					
7.5					
7.3					
6.3					
7.6					
7.1					
7.3					
7.0					
7.4					
5.2					

1.9
28.6
49.4
5.4
6.4

14.1
3.2

17.3
3.7
14.6

2.6
2.1
3.0
3.4
2.5

		35.95			
T.P.	11.90	47.35	0.50	35.95	
40			9.5	38.9	32.9
+50			5.4	42.0	35.0
39			2.3	45.1	37.6
+50			0.4	47.0	39.3
T.P.	9.34	56.55	0.14	47.21	
38			8.8	47.8	40.9
+50			6.7	49.9	42.6
37			4.9	51.7	44.3
+50			3.7	52.9	45.2
36			2.9	53.7	46.1
+50			3.1	53.5	46.1
35			3.9	52.7	45.7
+50			4.4	52.2	45.3
34			4.8	51.8	44.9
+50			5.1	51.5	43.5
T.P. ³³⁺⁵⁰ ginnery			5.11	51.44	
	5.53	56.97			
33			8.0	49.0	41.3
+50			9.6	47.1	40.2
32			9.8	47.1	40.1
+50			8.6	48.1	40.0
31			8.8	48.2	39.9
+75			10.2	46.8	39.8
+50			10.5	46.0	39.3

					6.5
					7.0
					7.5
					7.7
					6.9
					7.3
					7.4
					7.7
					7.6
					7.4
					7.0
					6.9
					6.9
					8.0
					7.7
					7.2
					7.0
					8.4
					8.3
					7.0
					5.7
					6.2

		56.97			
30			8.0	49.0	42.1
+50			6.3	50.7	43.9
29			4.4	52.6	45.7
+50			2.1	54.9	48.3
T.P.	11.54	67.76	0.75	56.22	
28			10.6	57.2	57.0
+70			9.1	58.7	52.5
27			5.9	61.9	55.9
+50			3.6	64.2	58.2
+25			2.7	65.1	58.9
26			2.3	65.5	59.1
+75			2.1	65.7	59.5
+50			1.9	65.9	59.5
+25			1.9	65.9	59.5
25			2.3	65.5	59.2
+75			2.6	65.2	58.9
24+50			3.2	64.6	58.3
24			4.6	63.2	57.0
+50			5.5	62.3	55.8
23			6.4	61.4	54.5
22+50+T.P.			7.77	59.99	53.3
	0.75	60.74			
22+25				59.4	52.3
22+50			2.7	58.0	50.8
+75			3.8	56.9	46.6
+50			5.6	55.1	46.3

6.9
6.8
6.9
6.6
6.2
6.2
6.0
6.0
6.2
6.4
6.2
6.4
6.4
6.3
6.3
6.3
6.2
6.5
6.9
0.7
7.1
7.2
8.1
8.8

H. 4 4-20
 KING
 POLAR
 OFFICE

		H.I		Elev	Grade
B.M.	9.85	44.35		34.50	
0+75			11.7	33.7	429.5
1+00			12.9	31.5	428.3
1+40			17.2	27.2	428.3
1+46.3			13.8	30.6	428.3
1+68.3			13.0	31.4	429.2
2+00			7.3	37.1	434.4
T.P.	12.35	55.99	0.71	43.64	
2+50			10.4	45.6	442.1
2+93			2.1	53.9	448.6
3+09			0.2	55.8	449.8
3+25			0.2	55.8	449.8
3+50			2.0	59.0	449.4
3+75			4.0	52.0	448.6
4+00			5.0	51.0	447.9
4+50			5.6	50.4	445.0
4+75			5.9	50.1	444.2
5+00			5.9	50.1	443.8
5+50			6.1	49.9	443.0

Cut

N. in abutment
4.2
3.2
F.L. culv.
2.3
2.1
2.7
3.5
5.3
6.0
6.0
4.6
3.4
3.6
5.4
5.9
6.3
6.9

£ 4 offsets - Murray P.h.

B.M.	9.73	117.51		107.78	
62+50			9.4	108 106.1	102.2
62			9.7	107.8	101.3
61+52			9.8	107.7	100.3
61+36			10.8	106.7	99.9
61+20			10.5	107.0	99.6
61+04			10.6	106.9	99.7
60+72			9.6	107.9	99.3
60+56			7.7	109.2	100.4
60+40			5.9	111.6 112.6	102.9
60+24			7.9	115.6	106.8
T.P.	11.50	127.07	1.94	115.57	111.3
F.C.60+09.5			6.0	121.1	114.7
£			6.6	120.5	
T.P.	12.27	138.71	0.63	126.44	
59+94.88			10.3	128.4	117.7
£			10.4	128.3	
59+80.76			1.4 ^{12'}	137.3	124.8
£			1.3	137.4	
59+66.81			2.0	136.7	138.8
£			0.0	138.7	
T.P.	12.59	151.27	0.03 ²⁰	139.68	
59+51.95			9.2	142.1	135.6
£			5.9	145.4	
59+36.30			2.0 ^{12'}	149.3	179.4

Top air valve chamber

5.9

6.5

7.4

6.8

7.4

7.8

8.6

9.4

8.7

8.8

9.3

6.4

10.7

12.5

5.9

6.5

9.9

		151.27			
Q			0.4	150.9	
T.P	12.97	163.76	0.48	156.79	
59+20.98			11.3	132.5	147.0
E			8.7	155.1	
59+05.58			9.3	154.5	146.7
E			7.9	156.4	
58+90.19			6.7	157.1	150.2
E			4.4	159.3	
T.P	12.85	176.33	0.28 ¹⁹	163.48	
58+50			12.0 ¹⁴	169.3	157.1
58			0.7	175.6	167.8
T.P	12.86	188.94	0.25 ¹⁴	176.08	
57+50			2.1	186.8	178.4
T.P	13.08	201.90	0.12 ¹⁴	188.82	
57			6.0 ¹⁴	195.9	189.1
T.P	12.67	214.48	0.09 ¹⁴	201.81	
56+50			9.5 ¹⁴	205.0	199.4
T.P	8.72	221.46	1.74	212.74	
<u>Cuts unit = 1</u>			6.47	14.99	
15.71 15+50	9.72	466.62	4.9	61.70	447.0
15+00			7.7	58.9	447.1
14+50			11.8	54.8	447.2
14+25			11.4	55.2	447.3
14+00			9.4	57.2	447.4
13+75			6.8	59.2	449.0

9.5
7.8
6.9
Equation $\frac{58+79.67 \text{ West}}{58+67.01 \text{ East}} =$ Grade 153.6 for 1633 See pipe Co. drawing
7.2
7.8
8.4
6.8
5.6
Hub + 15+50
14.7
11.8
7.6
7.9
9.3
10.8

466.62

13+50	4.7	61.9	450.6
13+25	4.1	62.5	452.2
13+00	1.8	64.8	453.3

13+25

13+50

13+75

71

C

11.3	
10.3	
11.5	

Murray P.L.

4-29-43

M. J. G.
D. T. M.
Potak

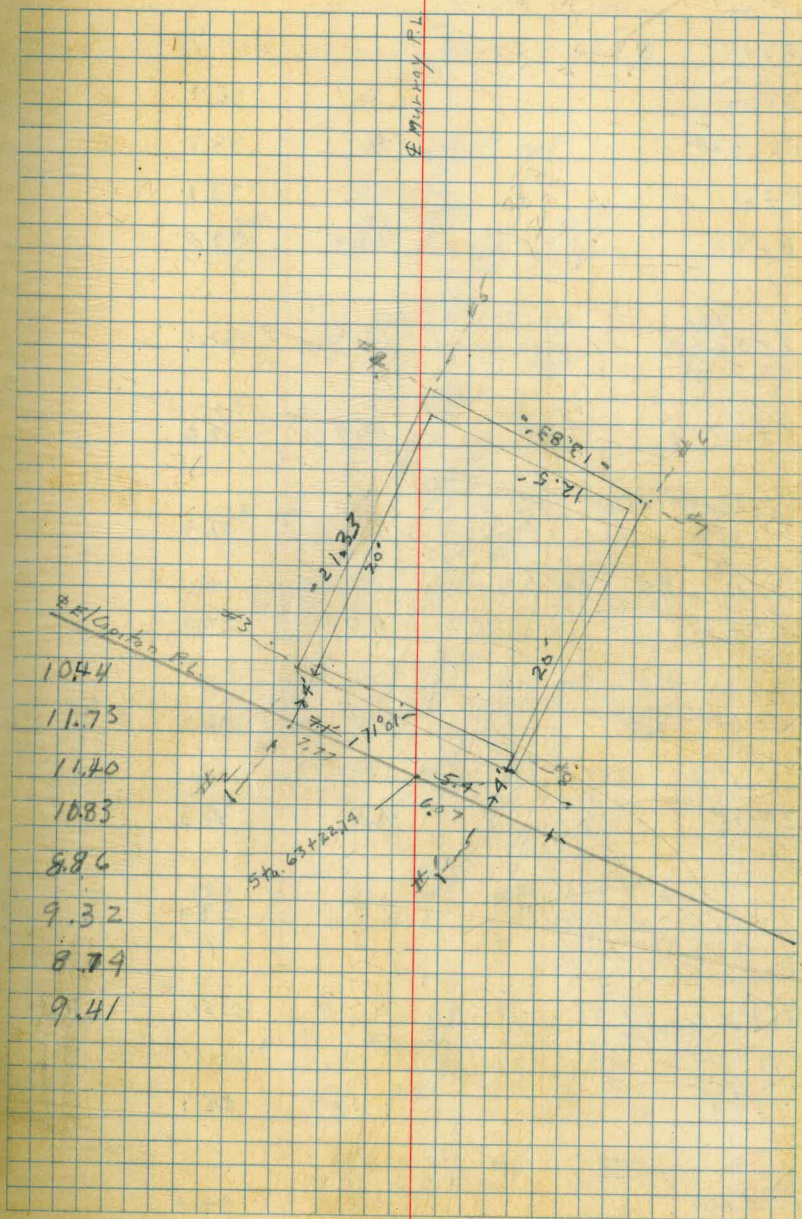
72

Levels Valve Chamber - sta. 63+00

Levels	B.M.	4.79	112.57	107.78	Top air V.Ch.
#1 N. Cor			2.79	109.78	
#2 N. Cor			2.93	109.64	
#3 E. Cor			3.29	109.33	
#4 E. Cor			3.27	109.30	
#5 S. Cor			4.17	108.40	
#6 S. Cor			4.34	108.23	
#7 W. Cor			4.16	108.41	
#8 W. Cor			3.84	108.73	
Hub 63+22.74			3.39	109.18	

Levels - Valve Chamber - 8' offsets

Levels	B.M.	5.81	113.59	107.78	
#1			4.45	109.14	98.7
#2			3.16	110.43	98.7
#3			3.99	110.10	98.7
#4			3.76	109.83	99.0
#5			5.73	107.86	99.0
#6			5.27	108.32	99.0
#7			5.85	107.74	99.0
#8			5.92	108.11	98.7
Top 5" Pipe			5.76	107.83	
" Con P			5.56	108.03	



		455.42		
2+50			8.4	47.0
2+62			6.0	49.4
2+80			3.1	52.3
2+92			1.2	54.2
3+00			0.3	55.1
T.P.	2.21	457.34	0.29	55.13
3+13			1.4	55.9
3+21			Top Pipe	
3+25			2.0	55.3
3+41			2.3	55.0
3+48			2.5	54.8
3+56			3.0	54.3
3+75			4.6	52.7
4+00			6.1	51.2
4+50			7.3	50.0

		45.5	447.0	47.1	52.8
Top slab		-1.5	8.4	+0.1	+5.8
		16		1.5	8'
		48.0	449.2	49.1	54.4
		-1.2	6.2	-0.1	+5.2
		17		6'	10'
		51.1	452.3	52.3	59.1
		-1.2	3.1	0.0	+6.8
		17'		4'	21'
		53.3	454.2	54.2	63.6
		-0.9	1.2	0.0	+9.4
		19'		2.5	8.5
		55.8	55.0	55.1	63.0
	C.	+0.7	-0.1	0.3	+7.9
		29.5	2.3	2.5	25'
		59.4	56.1	455.9	55.9
	C.	+2.5	+0.2	1.4	0.0
		28'	22'	4'	+6.6
					4.5'
End of slab		54.0	455.5	56.6	59.6
		-1.5	1.8	+1.1	+4.1
		30'		6'	6.5
					14'
		53.3	454.0	54.0	60.2
		-0.7	3.3	0.0	+6.2
		25		4.5	13'
		52.6	454.2	54.2	56.2
		-1.6	3.1	0.0	+2.0
		24		4	13.5
		53.1	453.6	54.3	60.8
		-0.5	3.7	+0.7	+7.2
		25		15.0	25'
		51.9	451.6	53.0	59.9
		+0.3	5.7	+1.4	+8.3
		26		13.5	18.5
		50.1	451.0	52.0	59.6
		-0.9	4.3	+1.0	+8.6
		25		13	15'
		47.7	448.9	50.2	59.0
		-1.2	8.4	+1.3	+2.1
		25		11	14'

This cut ordered by P.S. for this amount

	457.34	Top Pipe	
4+70	8.5	48.8	
4+77	8.9	48.4	
4+84	9.3	48.0	
5+00	9.9	47.4	
5+10	10.2	47.1	
5+40	10.5	46.8	
5+53	10.4	46.9	
5+78	10.5	46.8	
5+85	10.5	46.8	
B.C. 5+97 ¹⁸	10.4	46.9	
6+00	10.3	47.0	
6+10	10.3	47.0	
6+20	10.1	47.2	
6+28	10.0	47.3	

47.9 -0.6 24	448.5 8.8	50.0 +1.5 10	56.7 +8.2 18	
47.9 -0.8 25	448.1 8.6	50.1 +1.4 10	56.5 +8.8 18.5	
48.3 -0.4 25	448.7 8.6	50.1 +1.4 13.0	56.9 +8.2 14.0	
	448.7 8.6			
48.0 -0.5 27	448.5 8.8	50.0 +1.5 10	56.9 +8.4 14	
47.5 -0.4 30	447.9 9.4	50.2 +2.8 11.5	59.8 +11.9 17	
46.8 -0.9 26	447.7 9.6	48.9 +1.2 9	51.0 +3.3 11	60.8 +13.1 12
46.8 0.0 23	446.8 10.5	48.7 +1.9 8.5	53.6 +6.8 13	65.9 +19.1 14.0
46.3 -0.5 23	446.8 10.5	48.4 +1.6 8		66.4 +19.6 14.0
46.6 -0.4 20	447.0 10.3	48.7 +1.7 8.5		69.5 +22.5 17
	447.0 10.3			
	447.2 10.1			
47.6 -0.3 17	447.9 9.4	48.3 +0.4 1.3	69.4 +21.5 17	

	457.34	Top Pipe		
6+40		9.9	47.4	
6+50 ^v		9.8	47.5	
6+70 ^v		9.7	47.6	
6+80		9.7	47.6	
6+90 ^v		9.8	47.5	
7+00 ^v		9.7	47.6	
T.P.	1.85	53.62	5.57	51.77
7+15		5.8	47.8	
7+25		5.7	47.9	
7+35		5.6	48.0	
7+50		5.4	48.2	
7+55		5.4	48.2	
7+65		5.2	48.4	

48.0	447.4	48.2	51.4	71.8
+0.6	9.9	+0.8	+10.0	+21.1
<u>14</u>		<u>14</u>	18.5	20
	448.5			
	8.8			
	448.5			
	8.8			
48.5	448.7	49.7	56.0	72.0
-0.2	8.6	+1.0	+7.3	+23.3
<u>8</u>		<u>14</u>	<u>16</u>	<u>22</u>
	448.4			
	8.9			
	448.6			
	8.7			
R.H. Nail R+8'-7+25'-in Rock				
49.6	449.2	49.2	62.2	
+0.4	4.4	0.0	+13.0	
<u>8</u>		<u>13</u>	<u>17</u>	
50.3	448.9	48.9	64.1	
+1.4	4.7	0.0	+15.2	
<u>8</u>		<u>13</u>	<u>18</u>	
	450.1			
	2.5			
	451.1			
	2.5			
	451.1			
	2.5			
	451.2			
	2.4			

	53.62		
7+80	5.1	48.5	
7+90	5.0	48.6	
8+00	4.9	48.7	
8+45	4.7	48.9	
8+50	4.7	48.9	
Ec. 8+68 ⁵⁸	4.8	48.8	
8+90	5.0	48.6	
9+00	5.2	48.4	
9+10	5.5	48.1	
9+20	5.7	47.9	
9+40	6.2	47.4	
9+45			
9+54	6.8	47.0	
9+62	6.7	46.9	

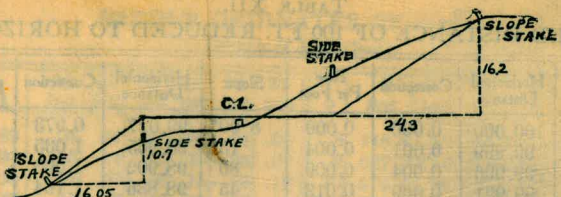
	52.8	451.8	52.8	69.3
	+1.8	1.5	+1.0	+17.5
	13'		16	23'
		452.1		
		1.5		
	52.6	452.1	52.1	60.0
	+0.5	1.5	0.0	+7.9
	19'		75'	18
	51.5	452.1	54.8	60.9
	-0.6	1.5	+2.7	+8.8
	30'		11'	13.5'
		452.1		
		1.5		
	51.6	451.7	56.4	59.5
	-0.1	1.9	+4.7	+7.8
	28		10.	12
	50.1	449.8	53.2	58.9
	+0.7	3.8	+3.9	+9.1
	25		10	13
		449.7		
		3.9		
		449.4		
		7.2		
	46.6	447.9	47.9	52.9
	-1.3	5.7	6.0	+5.0
	23'		18.5	21.0
	43.9	444.4	45.1	50.0
	-0.5	9.2	+0.7	+5.6
	20'		21.5	27.5
-24" curv.	41.0	444.0	44.9	52.4
	-3.0	9.6	+0.5	+8.4
	24	17	19	29
	43.0	442.9	44.9	52.2
	+0.1	10.7	+2.0	+9.3
	13'		20'	27

	53.62	Top Pipe		
9+87		6.9	46.7	
10+00		7.0	46.6	
10+15		6.9	46.7	
10+27		6.6	47.0	
10+35		6.4	47.2	
10+50		6.1	47.5	
10+60		5.7	47.9	
10+88 ^{TS}		3.2	50.4	Use 49.2 A.R.
T.P.	12.46	62.11	3.97	49.65
11+00		12.4	49.7	
11+10		11.5	50.6	
11+25		10.0	52.1	
11+42		8.1	54.0	
11+50		7.3	54.8	
11+80		5.7	56.4	
12+00		5.3	56.8	
12+10 ⁹²		5.1	57.0	
12+50		4.0	58.1	
T.P.	6.10	66.69	1.57	60.54
T.P.		4.22	62.42	62.4 Ginney 11+25

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43.9	443.8	45.1	54.2
+0.11	9.8	+1.3	+10.9
12.1		12	14.5
44.5	443.9	44.6	51.2
+0.6	9.7	+0.7	+2.3
8		6.3	12
444.8			
8.8			
446.0			
7.6			
44.4	446.2	47.1	56.7
+0.2	7.4	+0.9	+10.5
15.5		9	15
447.5			
6.1			
447.9			
50.5	5.7	51.2	59.5
+0.7	44.6	+1.6	+9.9
25	4.0	6	12
451.5			
10.6			
53.6	53.1	53.1	60.7
+0.5	9.0	0.0	+2.6
59.1	5.8	6.0	13
22	58.3	58.3	62.5
59.3	458.0	58.0	12
20	+0.3	9.0	+7.5
58.3	4.1	0.9	12
+0.3	5.2	58.9	67.5
16	5.2	0.0	+2.6
59.4	459.8	60.8	65.1
-0.4	2.3	+1.0	+5.3
59.3	15	4.5	61.4
-1.1	17	1.0	8
21	60.4	60.4	68.5
59.6	40.2	60.2	72.0
-0.6	1.9	0.0	+11.5
22.1	0.0	6	13
-0.7	59.2	60.4	68.6
22	2.2	+0.5	+8.7
		9	13

Reck-R+3' 10+84



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

21950
9.75
4 11.60
9.75
401.85
7
401.1



Ties to pipe from 4 as staked

4 Pipe	6+00	0' RT	4 Pipe - 12+50 - 2 RT
"	6+20	0.4 "	" - 12+00 - 3.8'
"	6+40	0.7 "	11+50 - 2.3
"	6+50	0.9 "	11+92 - 0.8
"	6+70	1.0 "	
"	6+80	1.5 "	
"	6+90	1.8 "	
"	7+00	3.5 "	
"	7+15	4.3 "	
"	7+25	5.5 "	
"	7+35	5.7 "	
"	7+50	5.8 "	
"	7+55	5.6 "	
"	7+65	5.4 "	
"	7+80	5.0 "	
"	7+90	4.5 "	
"	8+00	4 "	
"	8+15	3.0 "	
"	8+50	2.8 "	
"	8+60	1.4 RT	

43
43
82

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

Handwritten calculations and notes on the left page of the notebook, including various arithmetic problems and measurements.

330
149
1084
107.21
103.9
103.2
112.04
102.07.31
63 + 22.78
72.78
50
63 + 25.25
62 + 12.45
12.50
108.90
97
102.93
97
101.96
97
100.99
108.0

430.6
1.8
428.8
100.80
1.91
102.71
195
190

5.02
3.6
18.0
5.105.8
104.27
72.78
50
63 + 25.25
62 + 12.45
12.50

68 + 25.25
59 + 10600
3 89.25

27 + 50 7/10
54.30
262
309
220

68 + 25
90
51.68

459.3
11
453.2

54.53
6.36
48.17

21.28
5.82
15.46

49.6
9.9
59.5
53.6
56.0

52.55
6.36
50.19

15.4
12.1
21.7

21.1
9.1
30.2
18.4
28.4

15.4
12.1
21.7

21.1
9.1
30.2
18.4
28.4

X-Sectron - Back Fill - Murray P.h. Sta 0+39 - 12+50

11399
Polok
07-11-43
5-2143

Sta.	F.S.	H.T.	B.S.	Elev	Sta.	F.S.	H.I.	B.S.	Elev
	9.65	444.15		439.50	2+15			4.9	39.3
0+38			7.6	36.6				-1.3 16' R	38.0
0+68 ²⁹			9.1	35.1				+0.1 8' R	39.4
			0.0 4.5' L	35.1	2+23			3.5	40.7
			-0.3 3.6' R	34.8				-1.3 18' L	39.2
0+81			9.4	34.8	2+27			+0.1 2.5' R	40.8
			+0.1 12' L	34.9				2.6	41.6
			0.0 2.8' R	34.8				+1.5 19' L	40.1
			-1.4 6' R	33.4	2+29			+0.4 2.5' R	42.0
0+97			10.2	34.0				2.0	42.2
			-0.5 8.5' L	33.5	T.P.	10.32	453.65	-0.82	443.33
			0.0 2.5' R	34.0	2+39			9.4	44.3
			-1.9 6.5' R	32.6				-0.8 19' L	43.5
1+02			10.9	33.3				0.0 2.5' R	44.3
			-0.3 11.6' L	33.0	2+50			6.7	47.0
			0.0 2' R	33.3				-1.5 18' L	45.5
			-0.7 6.5' R	32.6	2+62			+0.1 4.3' R	47.1
1+30			11.1	33.1				4.3	49.4
			-0.4 10.7' L	32.7				-1.5 18' L	47.9
			+0.2 6' R	33.3	2+80			+0.9 5' R	49.8
1+50			10.5	33.7				1.4	52.3
			-0.5 10.5' L	33.2	T.P.	4.43	457.38	-1.0 11' R	51.3
			+0.2 5' R	33.9	2+92			+0.2 4' R	52.5
1+68			9.7	34.5				3.3	54.1
			-0.5 9.2' L	34.0				+0.2 3' R	54.3
			+0.3 3.5' R	34.8	3+00			-0.2 18.5' L	53.9
2+00			6.7	37.5				2.3	55.1
			-1.0 16' L	36.5	3+13			+0.10 2.5' R	55.2
			+0.1 4.5' R	37.6				-0.10 19' R	55.0
								1.5	55.9
								+0.2 2.5' R	56.1
								-0.8 20' R	55.1

Sta. F.S. H.I. B.S. Elev.
463.62

11+50

	5.1	58.5
$\frac{+0.4}{6'R}$		58.9
$\frac{-0.3}{20' Lt}$		58.2

11+80

	4.1	59.5
$\frac{0.0}{4.5'R}$		59.5
$\frac{0.0}{20.5' Lt}$		59.5

12+00

	3.9	59.7
$\frac{+0.1}{4'R}$		59.8
$\frac{0.0}{21' Lt}$		59.7

12+10.82

	3.8	59.8
$\frac{+0.2}{5'R}$		60.0
$\frac{0.0}{23' Lt}$		59.8

12+50

	3.8	59.8
$\frac{+0.9}{7'R}$		60.7
$\frac{-0.1}{22' Lt}$		59.7

615

T.P. 2.30 966.6 Bumpy 10 +50 -61.5

Sta	F.S.	H.I. 456.87	I.S.	Elev	Sta	F.S.	H.I. 456.97	B.S.	Elev
7+80			4.6	51.9	9+62			8.6	47.9
			+0.4 9'R	52.3				0.0 6'R	47.9
			-0.2 9'L+	51.7				-2.2 11'R	45.7
8+00			4.2	52.3				-0.3 7'L+	47.6
			+0.2 8'R	52.5				-4.7 14.5'L+	43.2
			-0.1 9'L+	52.2				9.1	47.4
8+45			4.4	52.1	9+87			+0.2 9'R	47.6
			+0.2 7'R	52.3				-0.2 9'L+	47.2
			+0.3 14'L+	52.4				-4.5 15.2'L+	42.9
8+68 ⁵⁸			4.7	51.8	10+00			9.0	47.5
			+0.5 5'R	52.3				+0.1 8'R	47.6
			+0.5 15'L	52.3				-0.4 10.5'L+	47.1
8+90			5.9	50.6	10+35			8.7	47.8
			+0.4 7'R	51.0				+0.2 10'R	48.0
			-0.2 13'L+	50.4				-0.5 14'L+	47.3
9+20			7.0	49.5	10+88 ⁵			5.3	51.2
			+0.2 8'R	49.7				+0.7 8'R	51.9
			-2.0 8'R	47.5				-0.7 17'L+	50.5
			-0.3 10'L+	49.2	T.P.	9.41	463.62	2.26	959.21
			-2.0 13'L+	47.5	11+10			9.4	54.2
9+40			8.0	48.5				+0.6 9'R	54.8
			+0.2 5'R	48.7				+0.6 19'L+	53.6
			-0.6 7'R	47.9	11+25			7.1	56.5
			+0.1 9'L+	48.6				+0.4 8.5'R	56.9
			-5.0 14'L+	43.5				-0.1 20'L+	56.4
9+54			8.4	48.1	11+92			5.5	58.1
			0.0 7'R	48.1				+0.4 8'R	58.5
			-2.3 10'R	45.8				-0.2 20.5'L+	57.8
			0.0 8'L+	48.1					
			-4.9 14'L+	43.2					

3
97

Sta	F.S.	H.I.	B.S.	Elev.	Sta	F.S.	H.I.	B.S.	Elev.
		457.38					453.83		
3+21			1.5	55.9	5+10			4.5	49.3
			+0.2 25' R	56.1				+0.5 6' R	49.8
			-1.2 20' L	54.7				-1.2 21' L	48.1
3+25			1.3	56.1	5+40			4.8	49.0
			-0.2 35' R	55.9				+0.9 6' R	49.4
			-1.8 22' L	54.3				-1.5 22' L	47.5
3+41			1.7	55.7	5+53			5.4	48.4
			+0.6 8' R	56.3				+0.5 6' R	48.9
			-2.0 25' L	53.7				-1.3 21' L	47.1
3+48			2.1	55.3	5+78			5.9	47.9
			+0.6 8' R	55.9				+0.2 5.5' R	48.1
			-1.6 24' L	53.7				-0.9 17' L	47.0
3+56			2.2	55.2	5+85			5.7	48.1
			+0.5 9' R	55.7				+0.6 5.5' R	48.7
			-2.1 24' L	53.1				-0.9 16' L	47.2
3+75			3.0	54.4	5+97.8			5.4	48.2
			+1.0 9' R	55.4				+0.6 5' R	48.8
			-2.7 23' L	51.7				-0.7 14' L	47.5
4+00			5.1	51.3	T.P.	6.37	456.47	3.73	450.10
			-0.1 9' R	51.2	6+28			7.9	48.6
			-1.1 22' L	50.2				+0.3 7' R	48.9
T.P.	2.10	453.83	-5.65	451.73				-1.0 13' L	47.6
4+50			3.3	50.5	6+40			7.8	48.7
			+0.2 7' R	50.7				+0.6 8' R	49.3
			-2.0 20' L	48.5				-0.9 13' L	47.8
4+70			4.4	49.4	6+80			7.5	49.0
			+0.9 8' R	50.3				+0.5 8' R	49.5
			-1.2 20' L	48.2				+0.1 8' L	49.1
4+77			4.5	49.3	7+15			6.5	50.0
			+0.2 8' R	50.1				+0.5 10' R	50.5
			-1.1 18' L	48.2				-0.1 2' L	49.9
4+84			4.5	49.3	7+25			6.1	50.4
			+0.2 7' R	50.1				+0.6 10' R	51.0
			-1.0 20' L	48.3				0.0 8' L	50.4

Ground line #544 p. 73

5+97 - 16+50

↑

#543 p. 50-60

67+33.5 to Filter Plant

#578 p 33-39

41+06.26 - End #578 p 22-27

First 1200' bench exc.

Orig. x-sec. #543 p. 71-72

0+38 - 1+68

1+68 - 12+50 #543 p 61-69

Final bench

0+00 - 12+50 #578 p. 73-78

backfill hauled in
final sections on yellow sheet

67+33.5 #578 p. 33-39

