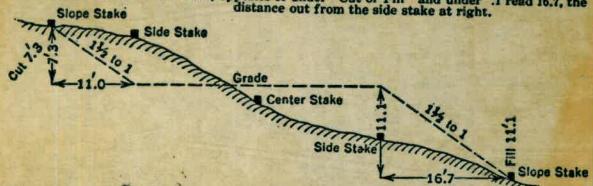


DISTANCES FROM SIDE STAKES FOR CROSS - SECTIONING

Roadway of any Width. Side Slopes $1\frac{1}{2}$ to 1.

In the figure below: opposite .7 under "Cut or Fill", and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	Cut or Fill
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

KEUFFEL & ESSER CO., N. Y.

10,455. cm, h, ai. cM.

588

MICROFILMED

JAN 13 1965

The paper in this book No. F370A

is made of 50% high grade rag stock

with a WATER RESISTING surface sizing.

PARTIAL ESTIMATES
NOV. 1941

Item

pg

Levels on X-section control (East k)	4
X- Sections - East Keyway	5-10
X- Sections - West Keyway	10-20
" " "	35-37
Levels on X-Section Control (East K)	38-39
X- Sections East Keyway	40-61

Profile of axis (east slope)

12+25 to 9+50 - also profile 62-66
line 50' south of axis 11+75 to
9+75 (Dec 12.)

Profile of Axis - W. side 67-68

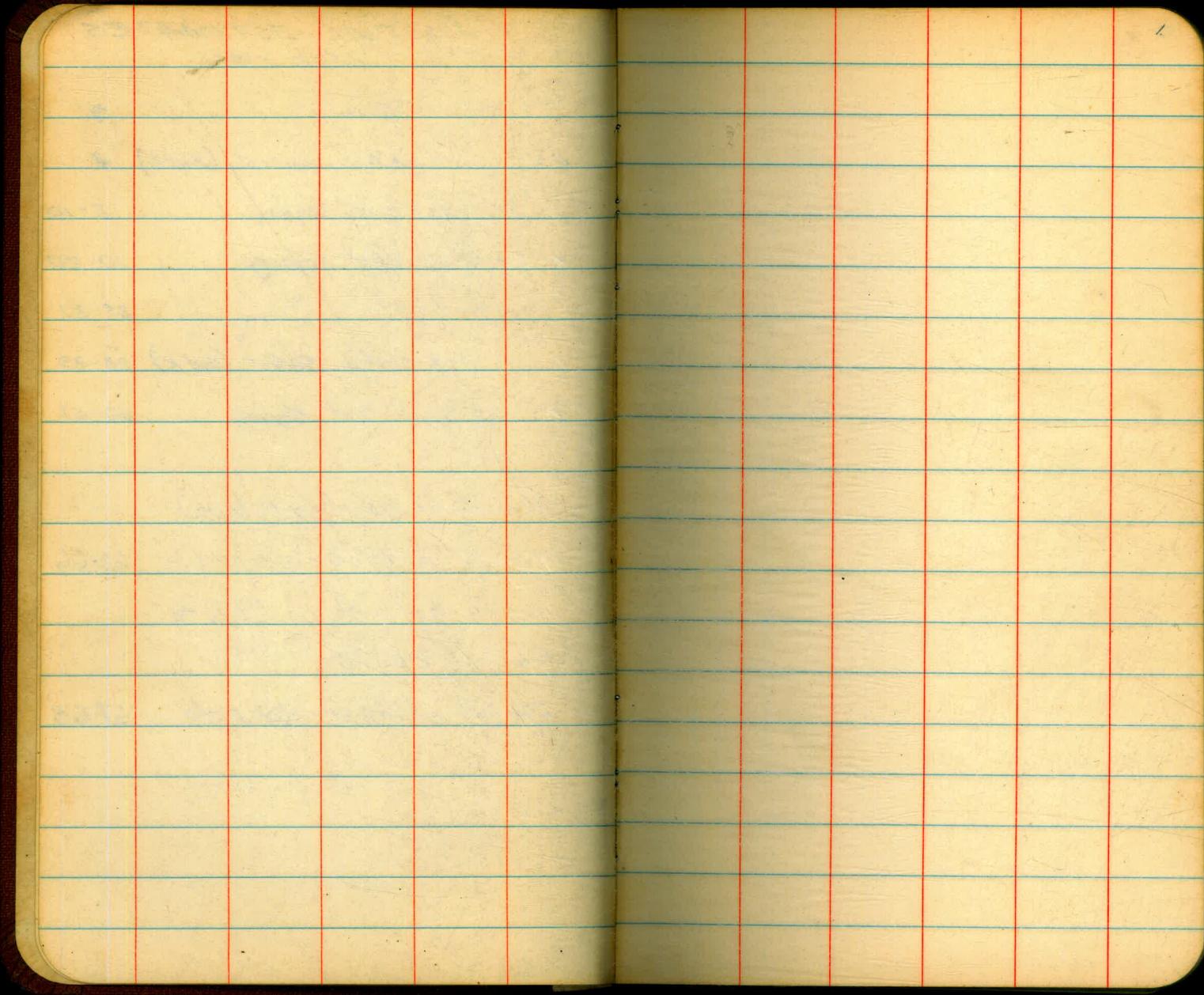
MICROFILMED

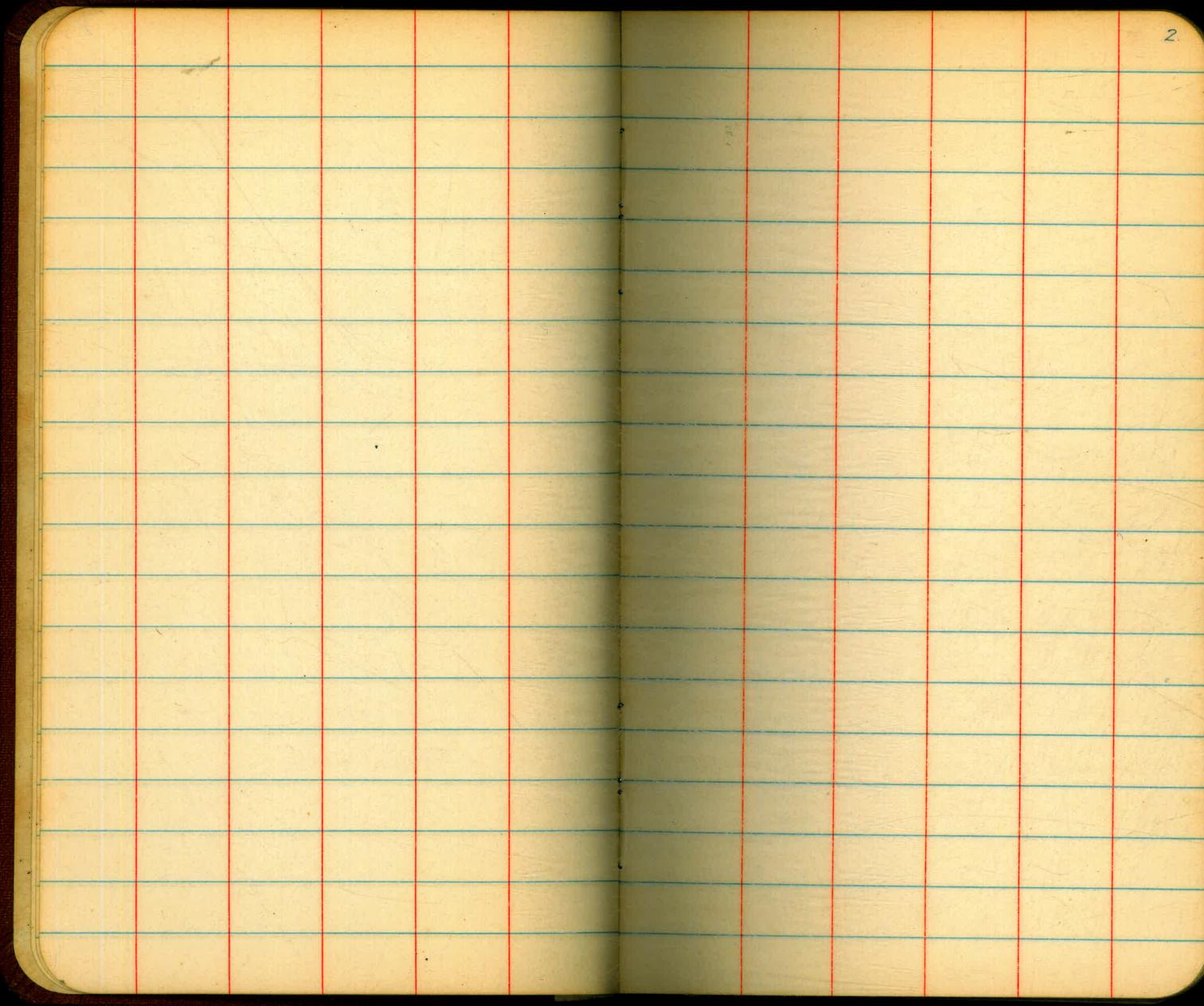
20161

AUTER on south side of bridge 12+
Kings and others 10+75 to 11+75
negative section 10+75 to 11+75

10+75 to 11+75

In
C
Cut or
Fill
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40





LEVELS ON X-SECTION CONTROL

overcast
Warm11/26/61 4
Ecker
King
Bruce

8.M #32

626.06

12.86 638.92 ✓

12+50/
150N

8.77 630.15 ✓

TP

0.57 638.35 ✓

12.20 650.55 ✓

12+60/
50N

10.21 640.54 ✓

12+70/
150N

4.05 646.50 ✓

12+80/
50N

0.38 650.17 ✓

TP

1.57 649.18 ✓

13.06 662.24 ✓

12+90/
50N

5.79 656.45 ✓

TP

2.48 659.76 ✓

7.13 666.89 ✓

13+00/
150N

2.44 664.45 ✓

8.M #31

3.79 663.10 663.09

X-SECTION - EAST KEYWAY

13 + 00

NOTES

11-26-41
Dickinson
Ecker
Jackson
Cote
Loing
King
Polak

5.

STA	V.A.	FUNCT.	DIST	DIFF.	EL	Notes
50N	T				664.45 ✓ Level Elevation (pg 4)	<u>soil</u>
30S	+16°35'	297	80	✓ 23.8	688.3 ✓ W. edge headtower rd	LR
20S	+15°35'	279	70	✓ 19.5	684.0 ✓	LR
10S	+13°53'	247	60	✓ 14.8	679.3 ✓	LR
AXIS	+12°28'	221	50	✓ 11.1	675.6 ✓	LR
10N	+10°41'	189	40	✓ 7.6	672.1 ✓	R
20N	+11°12'	198	30	✓ 5.9	670.4 ✓	LR
30N	+9°05'	160	20	✓ 3.2	667.7 ✓	LR
40N	+8°04'	142	10	✓ 1.4	65.9 ✓	LR

12 + 90

56.6N	T				656.45 ✓ Level elevation (pg 4)	
40 N	+4°02'	.071	✓ 16.6	✓ 1.2	57.8 ✓	LR
30 N	+7°16'	.128	✓ 26.6	✓ 3.4	59.9 ✓	LR
20 N	+9°02'	.159	✓ 36.6	✓ 5.8	62.3 ✓	LR

Elevs. comp. by OWL 12-1-41
checked RRE 12-2-41

STA	VA	FUNCT	DIST	DIFF	FL	NOTES	11-26-41
			12 + 90		656.45 ✓		
10 N	+5°17'	.092	46.6	4.3 ✓	660.81	R	
AXIS	+4°02'	.071	56.6	4.0 ✓	660.51	R	
10 S	+14°26'	.257	66.6	17.1 ✓	73.61	R	
20 S	+14°05'	.251	76.6	19.2 ✓	75.71	LR	
30 S	+16°55'	.304	86.6	26.3 ✓	82.81	LR	
40 S	+16°53'	.304	96.6	29.4 ✓	85.91	2 of headtower rd.	LR
			12 + 80				
50 N					650.17 ✓	Level elevation (avg)	
40 N	+8-21	.147	10.0	1.5 ✓	51.71	LR	
30 N	+10-10	.179	20.0	3.6 ✓	53.81	LR	
20 N	+7-20	.129	30.0	3.9 ✓	54.11	LR	
10 N	+1-05	.019	40.0	0.8 ✓	51.01	R	
AXIS	-0-16	.005	50.0	-0.3 ✓	49.91	R	
10 S	+6-15	.110	60.0	6.6 ✓	56.81	R	
20 S	+11-05	.196	70.0	13.7 ✓	63.91	R	
30 S	+16-13	.291	80.0	23.3 ✓	73.51		
						Elevs comp by D.W.C. 12-1-41 checked R.R.E. 12-2-41	R

STA	VA	FUNCT	DIST	DIFF	EL	NOTES	11/26/41	7
					650.171			
12+80							soil	
40S +19-45	.359 ✓	90.0	32.3 ✓	682.51			R 0P	
50S +18-30	.335 ✓	100.0	33.5 ✓	683.71	WEST edge Headtower (dirt) road		LR	
12+70								
AT 4IN				647.4 ①	Ground elevation		LR	
50S +20-14	.369 ✓	91.0	33.6 ✓	81.0 ✓	Top of bank		LR	
60S +18-39	.338 ✓	101.0	34.1 ✓	81.5 ✓	W. edge HeadTower rd.		LR	
40S +19-19	.351 ✓	81.0	28.4 ✓	75.8 ✓			R	
30S +15-53	.285 ✓	71.0	20.2 ✓	67.6 ✓			R	
20S +9-14	.163 ✓	61.0	9.9 ✓	57.3 ✓			R	
10S -1-43	.030 ✓	51.0	-1.5 ✓	45.9 ✓			R	
AXIS -11-12	.198 ✓	41.0	-8.1 ✓	39.3 ✓			R	
10N -5-44	.106 ✓	31.0	-3.1 ✓	24.3 ✓			R	
20N -2-28	.043 ✓	21.0	-0.9 ✓	16.5 ✓			R	
30N -4-55	.084 ✓	11.0	-0.9 ✓	16.5 ✓			LR	
50N				646.5	Refer To page 4 for level elev.		LR	

12+60 - Next page

Elevs comp'd by D.W.L. 12-1-41
checked RPE 12-2-41

STA.	VA	FUNCT.	DIST.	Diff.	Elev.	NOTES	11/26/41	Soil
		12+60					8	
50 N			18.9		640.34	Level elevation (Page 4)		LR
40 N			8.9		642.7			LR
31.1 N		AT 9T			643.4	Ground level		LR
20 N	-13-25	.239	11.1	-2.7	40.7			R
10 N	-11-12	.198	21.1	-4.2	39.2			R
AXIS	-20-09	.367	31.1	-11.4	32.0			R
10 S	-7-16	.128	41.1	-5.3	38.1			R
20 S	+5-27	.095	51.1	+4.9	48.3			R
30 S	+12-48	.227	61.1	13.9	57.3			VR
40 S	+16-17	.292	71.1	20.8	64.2			R
50 S	+20-02	.365	81.1	29.6	73.0			LR
60 S	+19-35	.356	91.1	32.4	75.8			LR
70 S	+19-08	.347	101.1	35.1	78.5			LR
12+50	—	—	—	—	AT 15.4 N			
80 S	+24-09	.448	95.4	42.7	75.7			LR
70 S	+24-44	.461	85.4	39.4	72.4			LR
60 S	+25-13	.471	75.4	35.5	68.5			R
			633.0			Elv. comp. by D.W.L 12-1-41 checked RRE 12-2-41		

STA VA FUNCT DIST DIFF. EL.

Notes 11/26/41

9

12+50

Soil

50 S	+25-23	474	65.4 ✓	31.0 ✓	664.0 ✓	R
40 S	+25-10	470	55.4 ✓	26.0 ✓	59.0 ✓	R
30 S	+25-06	468	45.4 ✓	21.2 ✓	54.2 ✓	R
20 S	+15-33	278	35.4 ✓	9.8 ✓	42.8 ✓	R
10 S	-4-33	080	25.4 ✓	-2.0 ✓	31.0 ✓	R
Axis	-19-33	355	15.4 ✓	-5.5 ✓	27.5 ✓	R
10 N	+4-34	080	5.4 ✓	+0.4 ✓	33.4 ✓	R

15.4 N π at 633.0 Ground elevation R

20 N +1-55 .033 4.6 ✓ 0.2 ✓ 33.2 ✓ R

30 N +1-45 .031 14.6 ✓ 0.5 ✓ 33.5 ✓ R

40 N -2-25 .042 24.6 ✓ -1.0 ✓ 32.0 ✓ LR

50 N 34.6 ✓ 630.15 Level Elev. (Page 4) LR

12+40

40 N -8-20 .146 15.0 ✓ -2.2 ✓ 28.2 ✓ LR

30 N -2-12 .038 5.0 ✓ -0.2 ✓ 30.2 ✓ LR

25 N π at 630.4 Ground elev. R

checked by RRE 12-2-41

STA	YA	FUNCT	DIST	DIFF	EI.
-----	----	-------	------	------	-----

			12 + 40	630.4	Soil
20 N	-0-16	.005	5.0	0.0	R
10 N	-0-45	.013	15.0	-0.2	R
AXIS	-17-02	.306	25.0	-7.7	R
10 S	-8-06	.142	35.0	-5.0	R
20 S	-4-55	.086	45.0	-3.9	R
30 S	+16-39	.299	55.0	+16.4	R
40 S	+15-20	.274	65.0	17.8	R
50 S	+18-39	.338	75.0	25.4	LR
60 S	+18-18	.331	85.0	28.1	LR
70 S	+19-59	.363	95.0	31.5	LR
80 S	+20-31	.374	105.0	39.3	LR
90 S	+20-12	.368	115.0	42.3	West edge Headtower rd. LR

Elev. comp. by D.W.C. 12-1-41
checked - RRE - 12-2-41

Cross-Sections on W. side
of Dam

11/29/41
Cool - cloudy

Jackson
King
Loing

"

Sta. + H.L. - Elev

A-16
B.M.

649.55

1.56 651.11

3+61

40's ✓ 0.40 650.7'

30's ✓ 6.1 645.0'

3+71

30's ✓ 9.8 641.3'

40's ✓ 1.1 650.0'

3+81

40's ✓ 7.9 43.7'

3+91

40's ✓ 8.6 42.5'

30's ✓ 11.1 40.0'

T.I.

Reductions + check
by DWL + RRE
12-2-41

11/29/41

Notes

12

Sta. + H.I - Elev.

651.11 ✓

T.P.

12.67

638.49 ✓

0.66

639.10 ✓

3+81

305 ✓

2.2

36.9 ✓

3+61

20's ✓

4.4

34.7 ✓

10's ✓

7.0

32.1 ✓

Axis ✓

11.7

27.4 ✓

10'N ✓

8.8

30.3 ✓

20'N ✓

1.6

37.5 ✓

30'N ✓

1.7

37.4 ✓

40'N ✓

3.2

35.9 ✓

3+71

90'N ✓

9.8

34.3 ✓

11/29/41

Notes

13.

STU YA FWD DIST DUE ELEV

Sta + HI - Elev.

63910 ✓

3+71

30'N ✓ 6.3 32.8 ✓

20'N ✓ 6.3 32.8 ✓

10'N ✓ 8.7 30.4 ✓

10'S ✓ 12.9 26.2 ✓

20'S ✓ 10.9 28.2 ✓

3+81

40'N ✓ 10.1 29.0 ✓

30'N ✓ 11.9 27.4 ✓

20'N ✓ 11.9 27.2 ✓

T.P. 11.95 627.15 ✓

1.35 628.50 ✓

11/29/41

Notes

14

Sta + H.I - Elv

628.50

3491

40'N ✓ 3.6 624.9 ✓

30'N ✓ 4.2 24.3 ✓

20'N ✓ 5.1 23.9 ✓

10'N ✓ 10.2 18.3 ✓

Axis ✓ 12.6 15.9 ✓

10'S ✓ 11.6 16.9 ✓

20'S ✓ 10.1 18.4 ✓

3471

Axis ✓ 5.9 23.1 ✓

3481

10'S ✓ 7.5 21.0 ✓

20'S ✓ 4.9 23.6 ✓

Axis ✓ 7.6 20.9 ✓

11/29/41

15

Sta. + H.I. - Elev.

628.50 ✓

4+01

90°N ✓ 5.8 622.7 ✓

30°N ✓ 7.4 21.1 ✓

T.P. 13.01 615.99 ✓

5.51 621.00 ✓

4+01

20°N ✓ 6.3 14.7 ✓

10°N ✓ 8.3 12.7 ✓

Hx15 ✓ 9.8 11.2 ✓

18°S ✓ 8.3 12.7 ✓

20°S ✓ 7.7 13.3 ✓

30°S ✓ 0.9 20.1 ✓

11/29/41

16

Sta. + H.I - Elav

621.00✓

4+11

40°S ✓ 2.3 618.7 ✓

30°S ✓ 8.4 12.6 ✓

20°S ✓ 11.1 09.9 ✓

10°S ✓ 12.2 08.8 ✓

Axis ✓ 12.0 09.0 ✓

10°N ✓ 10.8 10.2 ✓

20°N ✓ 9.1 11.9 ✓

30°N ✓ 8.7 12.3 ✓

40°N ✓ 7.9 13.6 ✓

4+21

40°N ✓ 10.7 10.3 ✓

30°N ✓ 11.0 10.0 ✓

20°N ✓ 11.3 09.7 ✓

11/29/41

17

Stg + H.I - E hrs.

621.60 ✓

4+31

10°N ✓ 11.8 09.2 ✓

Axis ✓ 13.2 09.8 ✓

10's ✓ 12.0 09.0 ✓

30°S ✓ 12.3 08.1 ✓

40°S ✓ 6.7 14.3 ✓

4+31

50°S ✓ 8.3 12.9 ✓

40°S ✓ 8.6 12.4 ✓

10°N ✓ 13.2 07.8 ✓

20°N ✓ 11.8 09.2 ✓

30°N ✓ 11.5 09.5 ✓

40°N ✓ 10.9 10.1 ✓

11/29/41

18.

Stg. + H.I. - Elev

621.00 ✓

T.P. 1003 610.97 ✓

3.49 614.46 ✓

4+21

20's ✓ 7.5 607.0 ✓

4+31

Hx's ✓ 7.9 06.6 ✓

10's ✓ 8.9 05.6 ✓

20's ✓ 10.2 04.3 ✓

30's ✓ 9.0 05.5 ✓

50's ✓ 2.9 11.6 ✓

T.P. .77 613.69 ✓

12.64 626.33 ✓

Cross-sections for W. side
of Dam

11/29/41
Cool-Cloudy

Jackson
King
Loing

19

Sta. + H.I - Elev.

626.33 ✓

T.P. (X)

1.80 624.53 ✓

11.23 635.76 ✓

4+11

50's ✓ 12.5 623.3 ✓

4+21

50's ✓ 17.2 18.6 ✓

B.M.
H-13

6.40
5.48
~~6.36~~
629.36

629.33 (See L.B. 554 Page 66)

B.M.
A-13

6.33 635.66

TP (X)

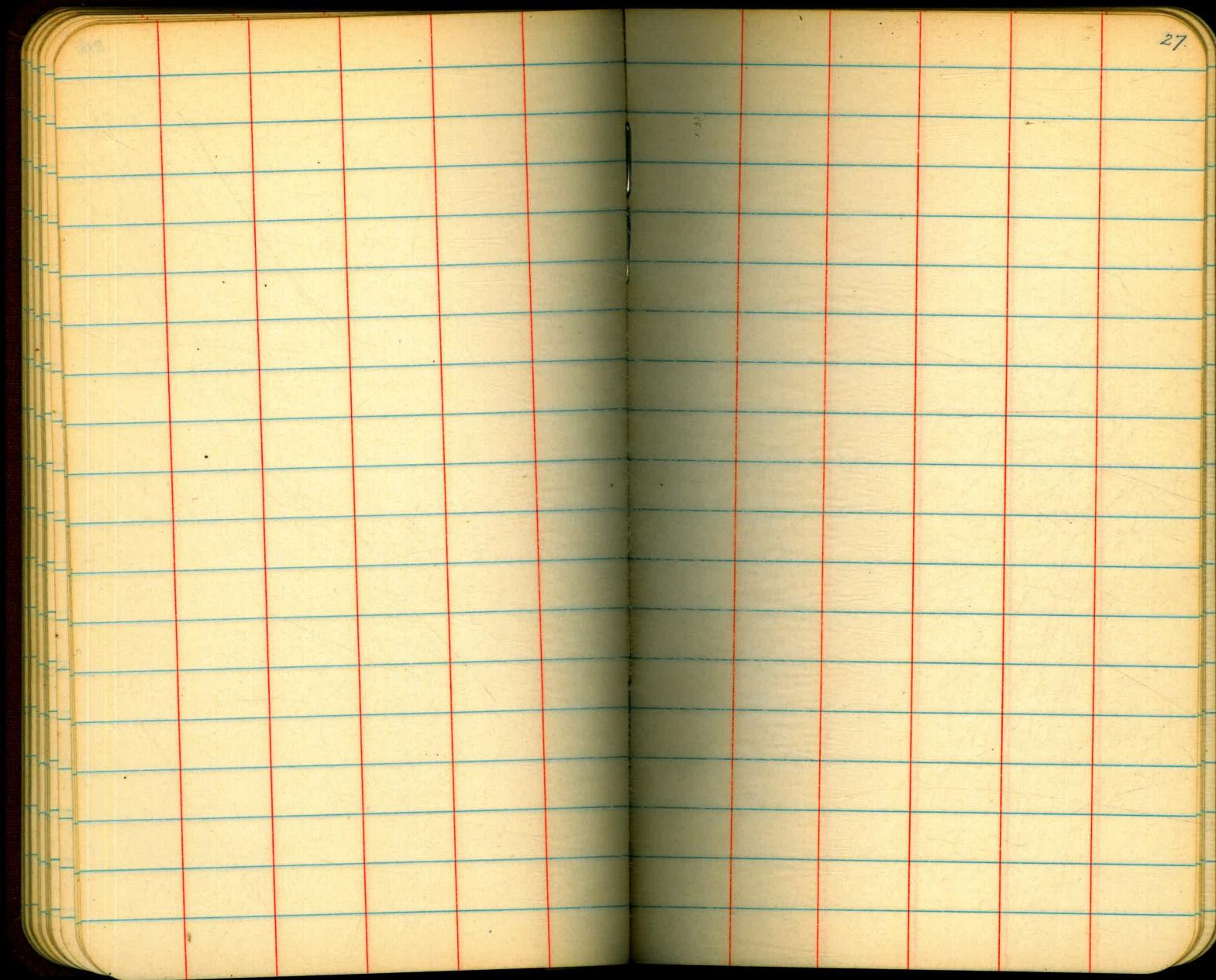
11.16 624.50

Check

Dec 1, 1941

Dickinson
Jackson

26.



29

30.

52.

✓ d)

X-SECTION- WEST KEYWAY

NOTESM Ecker
S. Coke
? Polak

35

1/28/41

A-16 649.58

12 78 662.29 ✓

3+11 / 10N 1.2 661.1 ✓

AXIS 2.5 59.8 ✓

10S 2.2 60.1 ✓

3+21 / 20S 2.9 59.4 ✓

10S ✓ 9.5 52.8 ✓

AXIS ✓ 7.5 54.8 ✓

10N ✓ 41 58.2 ✓

3+31 / 10N ✓ 9.4 52.9 ✓

20S ✓ 5.5 56.8 ✓

10S ✓ 12.7 49.6 ✓

TP 0.50 661.79

10.34 672.13 ✓

3+01 / 10N 6.4 15.7 ✓

AXIS 8.0 64.1 ✓

(These partial estimate elevations)
 determined by engineer's level

4/29/41

672 13

3+01 / 105 6.0 666.1 ✓

205 21 70.0 ✓

3+11 / 205 1.3 667.8 ✓

TP 11.78 660.35 ✓

133 661.68 ✓

TP 1175⁴ 649.94 ✓

2.80 652.74 ✓

3+31 / AXIS ✓ 5.6 47.1 ✓

3+41 / 10N ✓ 9.7 43.0 ✓

AXIS ✓ 12.2 40.5 ✓

105 ✓ 8.5 44.2 ✓

205 ✓ 2.0 50.7 ✓

3+51 / 205 ✓ 7.7 45.0 ✓

20N ✓ 12.5 40.2 ✓

TP 12.80 639.94 ✓

133 641.17 ✓

14/28/41

64117

3+51 /
105 ✓ 3.2 638.0 ✓

AXIS ✓ 8.1 33.1 ✓

10N ✓ 2.3 38.9 ✓

TP ✓ 084 640.33 ✓

1067 651.00 ✓

3+51 /
305 ✓ 0.6 50.4 ✓

TP ✓ 111 649.89 ✓

10.64 660.53 ✓

3+41 /
305 ✓ 2.2 58.3 ✓

TP ✓ 649.89

10.56 660.45 ✓

BM #A16 ✓ 10.90 649.55 649.58 ✓

Level Control for V.A. X-section

11/28/41

Jackson
Loing

38.

Sta + H.I. - Elev

A-32
B.M.

626.06

0.16 626.22

12+30

44 621.8

50' N of Ax in

T.P.

11.39 614.83

0.36 615.19

12+20

2.7 612.5

" " "

12+10

80 607.2

12+00

8.1 607.1

11/28/41
Fair-Warm

Jackson
Laing

59

Sta + H.I. - Elev

✓
615.19

11+90 8.0 607.2 ✓

T.P. 11.79 603.40 ✓

1.01 604.41 ✓

11+80 4.3 600.1 ✓

A-33
BM. 9.69 594.72 594.72 ✓

Cross-section on E side of dam

11/28/42
Fair-Warm
Jackson
Loring

40.

Sta + Hl - Elev

12+30
50N 6.5 628.3 ✓
10N 4.6 623.7 ✓

Refer To page 38

12+30

STA VA FUNCT DIST DIFF Elev

Soil

X AT 10N 0.0' - 623.7'

Ground Elevation

R

50N 40.0' ✓ 621.8'

Refer To page 38

LR

40N -0-18 .005' 30.0' -0.8' 623.7'

LR

30N +1-10 .020' 20.0' +0.4' 624.1'

LR

20N +2-48 .049' 10.0' +0.5' 624.2'

LR

AXIS -3347 .669' 10.0' -0.7' 617.0'

R

10S -9-45 .172' 20.0' -3.4' 620.3'

R

20S -6-58 .122' 30.0' -3.7' 620.2'

Cont. on Page 42

R

12+20

X AT 10S ✓ 609.9

Ground Elec.

R

50N ✓ 612.5

Refer To page 38

LR

Composed & checked by
DWL & RRE 12-1-41

STA	YA	FUNCT	DIST	DIFF.	ELEV	Notes	11/28/41
			12+20		609.9		41

40 N	+3-30	.061	50.0	+3.2	613.0	LR
30 N	+4-30	.079	40.0	3.1	613.0	LR
20 N	+3-16	.057	30.0	1.7	611.6	LR
10 N	+5-32	.097	20.0	1.9	611.8	R
AXIS	-2-55	.051	10.0	-0.5	609.4	R
20 S	-3-58	.069	10.0	-0.7	609.2	R
30 S	+1-12	.021	20.0	+0.4	610.3	R
40 S	+14-06	.251	30.0	± 1.5	617.4	R
	12+10					

Cont. on Page 43

50 N	AT		607.2	Refer To page 38	LR	
40 N	-0-43	.013	10.0	-0.1	607.1	LR
30 N	+1-18	.023	20.0	+0.5	607.7	LR
20 N	+1-56	.034	30.0	+1.0	608.2	LR
10 N	-1-29	.026	40.0	-1.0	606.2	R
AXIS	-2-14	.039	50.0	-2.0	605.2	R
10 S	-2-25	.042	60.0	-2.5	604.7	R

STA	VA	FUNCT	DIST	DIFF	Elev
			12+10		607.2

Notes 11/28/41

⁴²
Soil

205	-1-36	.028	70.0	-2.0	605.2	R
305	-0-54	.016	80.0	-1.3	605.9	R
405	-0-41	.012	90.0	-1.1	606.1	R
505	+7-25	.130	100.0	+13.0	620.2	R
605	+12-53	.229	110.0	+25.2	632.4	R
705	+16-58	.305	120.0	+36.6	643.8	R
805	+18-53	.342	130.0	+44.5	651.7	LR
905	+18-51	.341	140.0	+47.8	654.9	LR

Cont From Page 40

12+30

AT	10 N	623.7	Ground elev. Refer To page 40
----	------	-------	-------------------------------

305	+11-14	.199	40.0	+80	631.7	R
405	+19-03	.345	50.0	-11.3	641.0	R
505	+18-36	.337	60.0	-20.2	643.9	R
605	+22-16	.409	70.0	-28.6	652.3	R
705	+24-16	.451	80.0	-36.1	659.8	LR

STA	VA	FUNCT	DIST	DIFF	FLER	Notes	11/28/71	43 Soil
			12+30		623.7			L
80S	+23-28	.434 ✓	90.0	391 ✓	662.8			LR
90S	+23-30	.435 ✓	100.0	43.5 ✓	667.2			

Con. from Page 41

12+20

AT 105

90S	+32-21	.633 ✓	80.0	50.6	660.5
80S	+34-14	.680 ✓	70.0	47.6	657.5
70S	+35-01	.701 ✓	60.0	42.1	652.0
60S	+30-23	.586 ✓	50.0	29.3	639.2
50S	+28-43	.548 ✓	40.0	21.9	631.8

Ground elevation

LR

LR

LR

R

R

R

12+00

AT 50 N

90S	+17-15	.311 ✓	140.0	43.5	626.5
80S	+16-48	.302 ✓	130.0	39.3	646.4
70S	+11-39	.206 ✓	120.0	24.7	631.8

Ground elevation Refer To Page 38 LR

LR

LR

R

STA. VA FUNCT DIST DIFF ELEV

		12+00		607.1
60 S	+7-50	.138 ✓	110.0	15.2 622.3
50 S	+0-33	.010 ✓	100.0	1.0 608.1
40 S	-6-54	.121 ✓	90.0	-10.9 596.2
30 S	-9-00	.158 ✓	80.0	-12.6 594.5
20 S	-10-50	.191 ✓	70.0	-13.4 593.7

NOTES 11/28/41

44
Soil

R

R

R

R

R

At 30 N

		608.1	Ground elevation	LR
10 S	-18-39	.338 ✓	40.0 -13.5 594.6	R
AXIS	-23-32	.436 ✓	30.0 -13.1 595.0	R
10 N	-24-46	.461 ✓	20.0 -9.2 598.9	R
20 N	-15-46	.282 ✓	10.0 -2.8 605.3	R
40 N	-4-50	.085 ✓	10.0 -0.9 607.2	LR

11+90

At 30 N		608.0	Ground elevation	LR
50 N		20.0	607.2	Ground elevation refer to page 39 LR

STA	VA	FUNCT	DIST.	DIFF	Elev.	Notes	45 Soil
			11+90		6080		
40 N	-2-30	.044	110.0	-0.4	607.6		LR
20 N	-35-26	.712	10.0	-7.1	600.9		R
10 N	-41-11	.875	20.0	-17.5	590.5		R
AXIS	-29-50	.573	30.0	-17.2	590.8		R
10 S	-23-56	.444	40.0	-17.8	590.2		R
20 S	-20-10	.367	50.0	-18.4	589.6		R
30 S	-16-22	.294	60.0	-17.6	590.4		R
40 S	-12-30	.222	70.0	-15.5	592.5		R
50 S	-7-10	.126	80.0	-10.1	597.2		R
60 S	+3-34	.062	90.0	+5.6	613.6		R
70 S	+10-47	.190	100.0	190	627.0		R
80 S	+17-32	.316	110.0	34.8	642.8		R
90 S	+17-55	.323	120.0	38.8	646.8		LR

11+80

AT 34.5 N

607.2

Ground Elevation

LR

STA.	V A	FUNCT	DIST	DIFF	E1er	Notes	11/28/41	(46)
			11480		6052 ^{7.2}			
90 S	+16-09	.290 ✓	124.5	+36.1 ✓	643.3 ✓		LR	
80 S	+15-41	.281 ✓	114.5	-32.2 ✓	639.4 ✓		LR	
70 S	+7-43	.171 ✓	104.5	-17.9 ✓	625.1 ✓		R	
60 S	+1-19	.073 ✓	94.5	-2.2 ✓	609.4 ✓		R	
50 S	-7-11	.126 ✓	84.5	-10.6 ✓	596.6 ✓		R	
40 S	-13-40	.243 ✓	74.5	-18.1 ✓	589.1 ✓		R	
30 S	-17-07	.308 ✓	64.5	-19.9 ✓	587.3 ✓		R	
20 S	-21-58	.403 ✓	54.5	-22.0 ✓	585.2 ✓		R	
10 S	-28-05	.534 ✓	44.5	-23.8 ✓	583.4 ✓		R	
AXIS	-34-12	.680 ✓	34.5	-23.5 ✓	583.9 ✓		R	
10 N	-37-33	.769 ✓	24.5	-18.8 ✓	588.4 ✓		R	
20 N	-32-43	.642 ✓	14.5	-9.30 ✓	597.9 ✓		LR	
30 N	+2-55	.051 ✓	4.5	+0.2 ✓	607.4 ✓		LR	
40 N	-3-49	.067 ✓	5.5	-0.4 ✓	606.8 ✓		LR	
50 N	-24-14	.450 ✓	15.5	-7.0 ✓	600.2 ✓		LR	

Levels for Crown-section on
E side of Dam

11/29/41
Cool - cloudy

Jackson
40139

47.

Sta + H.L - Elev

A-34

B.M.

553.58

12.8456642

10+50 5.6 560.8

10+60 5.3 561.1

10+70 4.5 561.9

10+80 3.5 562.9

T.P. 0.87 565.55

12.96 578.51

10+90 10.0 567.6

11+00 0.7 577.8

T.P. 0.88 577.63

11.28 588.91

Levels for Cross-sections on
E. side of Dam

Sta + H.L. - Elev.

11/29/41
Cool - cloudy

48

58891

11+10 5.5 583.4

11+20 6.2 582.7

11+30 5.5 583.4

11+40 3.6 585.3

11+50 1.4 587.5

T.P. 0.24 588.67

9.71 598.39

11+60 9.3 589.1

11+70 4.6 593.8

B.M. 3.66 594.72 594.72

Cross-sections on E side
of Dam

Sto. V.A Fundt Dist Diff Elev

TAT 30 N.

601.2

50 N

593.8

40 N -3-26 .060 ✓ 10.0 -0.6 ✓ 600.6 ✓

20 N -35-33 .715 ✓ 10.0 -7.2 ✓ 594.0 ✓

10 N -42-30 .916 ✓ 20.0 -18.3 ✓ 582.9 ✓

Axis -39-06 .813 ✓ 30.0 -24.2 ✓ 576.8 ✓

10 S -31-51 .621 ✓ 40.0 -24.8 ✓ 576.4 ✓

20 S -27-04 .511 ✓ 50.0 -25.6 ✓ 575.6 ✓

30 S -20-50 .381 ✓ 60.0 -22.9 ✓ 573.3 ✓

40 S -16-46 .301 ✓ 70.0 -21.1 ✓ 580.1 ✓

50 S -5-57 .104 ✓ 80.0 -8.3 ✓ 592.9 ✓

60 S +5-37 .098 ✓ 90.0 +8.8 ✓ 610.0 ✓

70 S +9-28 .167 ✓ 100.0 16.7 ✓ 617.9 ✓

80 S +15-58 .286 ✓ 110.0 31.5 ✓ 632.7 ✓

90 S +17-55 .323 ✓ 120.0 38.8 ✓ 640.0 ✓

11/29/41
Cool - cloudy

Sto. ? H+70

49

soil

LR

LR

LR

LR

LR

LR

R

R

R

R

R

R

R

R

R

LR

LR

STA VA FUNCT DIST DIFF. ELEV.

11/29/41

Notes

50

Sect

11+60

AT 30 N

594.3

Ground elevation

90 S +17-57 .324 ✓ 120.0 38.9 ✓ 633.2 ✓ LR

80 S +17-48 .321 ✓ 110.0 35.3 ✓ 629.6 ✓ LR

70 S +10-53 .192 ✓ 100.0 19.2 ✓ 613.5 ✓ R

60 S +4-07 .072 ✓ 90.0 6.5 ✓ 600.8 ✓ R

50 S -3-36 .063 ✓ 80.0 -5.0 ✓ 589.3 ✓ R

40 S -14-51 .265 ✓ 70.0 -18.6 ✓ 575.7 ✓ R

30 S -18-19 .331 ✓ 60.0 -19.9 ✓ 574.4 ✓ R

20 S -23-33 .436 ✓ 50.0 -21.8 ✓ 572.5 ✓ R

10 S -27-57 .531 ✓ 40.0 -21.2 ✓ 573.1 ✓ R

- AX13 -33-50 .670 ✓ 30.0 -20.1 ✓ 574.2 ✓ R

10 N -38-35 .798 ✓ 20.0 -16.0 ✓ 578.3 ✓ R

20 N -34-54 .698 ✓ 10.0 -7.0 ✓ 587.3 ✓ LR

40 N -14-46 .264 ✓ 10.0 -2.6 ✓ 591.7 ✓ LR

50 N 20.0 ✓ 589.1 Ground elevation refer to page 48 LR

STO VA FUNCT DIST DIF ELEV.

11/29/41

Notes

51
Soil

11 + 50

AT 30 N

588.7

Ground elevation

LR

50 N

20.0

587.5

Ground elevation - Refer to page 48

LR

40 N

-8-31

150'

10.0'

-1.5 ✓

587.2'

LR

20 N

-45-02

1001'

10.0'

-10.0' ✓

578.7'

LR

10 N

-33-14

655'

20.0'

-13.1 ✓

575.6'

LR

AXIS

-30-36

591'

30.0'

-17.7 ✓

571.0'

R

10 S

-23-48

421'

40.0'

-17.6 ✓

571.1'

R

20 S

-18-46

340'

50.0'

-17.0 ✓

571.7'

R

30 S

-14-24

257'

60.0'

-15.4 ✓

573.3'

R

40 S

-10-18

182'

70.0'

-12.7 ✓

571.0'

R

50 S

-0-18

005'

80.0'

-0.4 ✓

588.3'

R

60 S

+5-04

089'

90.0'

+8.0 ✓

596.7'

R

70 S

+11-21

201'

100.0'

20.1 ✓

608.8'

R

80 S

+17-16

311'

110.0'

34.2 ✓

622.9'

LR

90 S

+17-21

312'

120.0'

37.4 ✓

626.1'

LR

STA	YA	FUNDT	DIST	DIFF.	ELEV.
					11+40

11/29/41

Notes

52
Soil

T AT 40 N		584.9
90 S +16-17 .292	130.0	38.0 ✓ 622.9 /
80 S +16-44 .301	120.0	36.1 ✓ 621.0 /
70 S +9-95 .172	110.0	18.9 ✓ 603.8 /
60 S +6-25 .112	100.0	11.2 ✓ 596.1 /
50 S +1-18 .028	90.0	2.0 ✓ 587.0 / 586.9
40 S -4-18 .075	80.0	-6.0 ✓ 578.9 /
30 S -9-26 .166	70.0	-11.6 ✓ 573.3 /
20 S -13-07 .233	60.0	-14.0 ✓ 570.9 /
10 S -6-22 .112	50.0	-5.6 ✓ 579.3 /
AXIS -21-23 .392	40.0	-15.7 ✓ 569.2 /
10 N -24-98 .462	30.0	-13.9 ✓ 571.0 /
20 N -25-05 .468	20.0	-9.4 ✓ 575.5 /
30 N -10-39 .188	10.0	-1.9 ✓ 583.0 /
50 N	10.0	585.3

Ground elevation -

LR

LR

LR

R

LR

LR

LR

LR

R

R

R

R

R

LR

LR

LR

LR

STA VA FUNCT DIST

11/29/41

53

11+30

STA	VA	FUNCT	DIST		Ground elevation		LR
						"	
						"	Refer To page 42
							LR
50 N			15.5		583.4		LR
40 N	+2-00	.035	-5.5	✓ 0.2	584.11		LR
30 N	-17-50	.322	4.5	✓ -1.4	582.51		LR
20 N	-32-11	.629	14.5	✓ -9.1	574.81		LR
10 N	-29-53	.575	24.5	✓ -12.1	569.81		R
AXIS	-23-21	.032	34.5	✓ -14.9	569.01		R
10 S	-17-31	.316	44.5	✓ -14.1	569.81		R
20 S	-14-26	.257	54.5	✓ -14.0	569.91		R
30 S	-10-42	.189	64.5	✓ -12.2	571.71		R
40 S	-4-48	.084	74.5	✓ -6.3	577.61		LR
50 S	+1-14	.022	84.5	✓ +1.9	585.81		LR
60 S	+6-26	.113	94.5	✓ 10.7	590.61		LR
70 S	+9-10	.161	104.5	✓ 16.8	600.71		LR
80 S	+16-54	.304	114.5	✓ 34.8	618.71		LR
90 S	+16-46	.301	124.5	✓ 37.5	621.41		LR

Sta	YA	FUNCT	DIST	DIFF	Elev.
-----	----	-------	------	------	-------

11+20

					583.1
T	07	32.3 N			
90S	+16-03	.288 ✓	122 3 ✓	35.2 ✓	618.3 ✓
80S	+15-39	.280 ✓	112 3 ✓	31.4 ✓	614.5 ✓
70S	+9-19	.164 ✓	102.3 ✓	16.8 ✓	599.9 ✓
60S	+6-16	.110 ✓	92.3 ✓	10.2 ✓	593.3 ✓
50S	-0-58	.017 ✓	82.3 ✓	-1.4 ✓	581.7 ✓
40S	-5-58	.105 ✓	72.3 ✓	-7.6 ✓	575.5 ✓
30S	-10-44	.190 ✓	62.3 ✓	-11.8 ✓	571.3 ✓
20S	-15-42	.281 ✓	52 3 ✓	-14.7 ✓	568.4 ✓
10S	-18-48	.340 ✓	42.3 ✓	-14.4 ✓	568.7 ✓
A/15	-26-18	.494 ✓	32.3 ✓	-16.0 ✓	567.1 ✓
10N	-35-53	.723 ✓	22.3 ✓	-16.1 ✓	567.0 ✓
20N	-50-09	1.198 ✓	12.3 ✓	-14.7 ✓	568.4 ✓
30N	-16-06	.289 ✓	2.3 ✓	-0.7 ✓	582.4 ✓
40N	-0-35	.010 ✓	7.7 ✓	-0.1 ✓	583.0 ✓
50N			17.7		582.7

11/29/41

Notes

54
Soil

Ground elevation

LR

LR

LR

LR

LR

LR

R

R

R

R

R

R

R

LR

LR

LR

Ground elevation Refer To Page 48 LR

11/29/41

55

STA	VA	FUNCT	DIST	DIFF	Elev.	Notes
			11+10			
AT	36.5 N				581.6	LR
50 N			13.5		583.4	Ground elevation refer to page 48 LR
40 N	+4-22	.076 ✓	3.5	0.3 ✓	581.9	LR
30 N	-44-09	.971	6.5	-6.3 ✓	575.3	LR
20 N	-44-50	.994 ✓	16.5	-16.4 ✓	575.2	LR
10 N	-31-46	.619 ✓	26.5	-16.4 ✓	565.2	R
AXIS	-23-21	.432 ✓	36.5	-15.8 ✓	565.8	R
10 S	-17-20	.312 ✓	46.5	-14.5 ✓	567.1	R
20 S	-13-31	.240 ✓	56.5	-13.6 ✓	568.0	R
30 S	-9-03	.159 ✓	66.5	-10.6 ✓	571.0	R
40 S	-6-05	.107 ✓	76.5	-8.2 ✓	573.4	LR
50 S	-2-11	.038 ✓	86.5	-3.3 ✓	578.3	LR
60 S	+4-18	.075 ✓	96.5	+7.2 ✓	583.8	LR
70 S	+7-40	.135 ✓	106.5	19.4 ✓	596.0	R
80 S	+14-15	.254 ✓	116.5	29.6 ✓	611.2	LR
90 S	+14-26	.257 ✓	126.5	32.5 ✓	614.1	LR

Sta. VA Funct DIST DIFF Elev.

11/29/41

56
Soil

11+00

TOT ZON		564.4	Ground elevation	R
90 S	+22-50 .421 ✓	110.0	46.3 ✓ 610.7 ✓	LR
80 S	+23-10 .428 ✓	100.0	42.8 ✓ 607.2 ✓	LR
70 S	+18-05 .327 ✓	90.0	29.4 ✓ 593.8 ✓	LR
60 S	+16-13 .291 ✓	80.0	23.3 ✓ 587.7 ✓	LR
50 S	+13-14 .235 ✓	70.0	16.5 ✓ 580.9 ✓	LR
40 S	+12-02 .213 ✓	60.0	12.8 ✓ 577.2 ✓	LR
30 S	+9-19 .162 ✓	50.0	8.2 ✓ 572.6 ✓	LR
20 S	+5-41 .100 ✓	40.0	4.0 ✓ 568.4 ✓	R
10 S	+2-A9 .049 ✓	30.0	1.5 ✓ 565.9 ✓	R
AXIS	+1-19 .023 ✓	20.0	0.5 ✓ 564.9 ✓	R
10 N	+0-52 .015 ✓	10.0	0.2 ✓ 564.6 ✓	R
30 N	+23-43 .439 ✓	10.0	4.4 ✓ 568.8 ✓	LR
40 N	+24-11 .449 ✓	20.0	9.0 ✓ 573.4 ✓	LR
50 N		30.0	577.8	Ground elevation refer to page 47 LR

Sta VA Funct Dist Dif Eler

10 + 90

Tot 20 N

563.5

50 N

567.6

Ground clear, refer to page 47 LR

40 N +9-46 .172 ✓ 20.0 3.4 ✓ 566.9

LR

30 N -0-15 .004 ✓ 10.0 0.0 ✓ 563.5

LR

10 N +2-04 .036 ✓ 10.0 0.4 ✓ 563.9

R

AXIS +3-15 .057 ✓ 20.0 1.1 ✓ 564.6

R

10 S +4-48 .084 ✓ 30.0 2.5 ✓ 566.0

R

20 S +5-37 .098 ✓ 40.0 3.9 ✓ 574.4

R

30 S +8-17 .146 ✓ 50.0 7.3 ✓ 570.8

LR

40 S +11-20 .200 ✓ 60.0 12.0 ✓ 575.5

LR

50 S +14-15 .254 ✓ 70.0 17.8 ✓ 581.3

L

60 S +17-22 .313 ✓ 80.0 25.0 ✓ 589.5

70 S +19-35 .356 ✓ 90.0 32.0 ✓ 595.5

80 S +22-35 .416 ✓ 100.0 41.6 ✓ 605.1

90 S +22-18 .410 ✓ 110.0 45.1 ✓ 609.6

11/29/41

Notes

57
S6,1

STA VA FUNCT DIST DIFF ELEV.

NOTES 11/29/41

58
Soil

70 + 80

50 N. T 9T

5629 ✓

Refer To page 47

LR

90 S. +17-01 .306 ✓ 140.0 42.8 ✓ 605.7 ✓

LR

80 S. +17-24 .313 ✓ 130.0 40.7 ✓ 603.6 ✓

LR

70 S. +15-17 .273 ✓ 120.0 32.8 ✓ 595.7 ✓

LR

60 S. +12-03 .213 ✓ 110.0 23.4 ✓ 586.3 ✓

LR

50 S. H0-27 .184 ✓ 100.0 18.4 ✓ 581.3 ✓

LR

40 S. +7-14 .127 ✓ 90.0 16.4 ✓ 574.3 ✓

LR

30 S. +5-21 .092 ✓ 80.0 7.5 ✓ 570.6 ✓

R

20 S. +3-45 .066 ✓ 70.0 4.6 ✓ 567.5 ✓

R

10 S. +2-11 .038 ✓ 60.0 2.3 ✓ 565.2 ✓

R

AXIS +1-13 .021 ✓ 50.0 1.1 ✓ 564.0 ✓

R

10 N. H0-49 .014 ✓ 40.0 0.6 ✓ 563.5 ✓

R

20 N. -0-18 .005 ✓ 30.0 -0.2 ✓ 562.7 ✓

R

30 N. -0-30 .009 ✓ 20.0 -0.2 ✓ 562.7 ✓

R

40 N. -0-52 .015 ✓ 10.0 -0.2 ✓ 562.7 ✓

R

R

STA.	VA	FUNCT	DIST	DIFF.	ELEV.
------	----	-------	------	-------	-------

11/29/41

59
Soil

10 + 70

50N	T 0T		561.9	✓	Ground elevation (page 47)	R
40N	+0-31	.009	100.0	0.1 ✓	562.0	R
30N	+0-54	.016	20.0	0.3 ✓	562.2	R
20N	+1-27	.025	30.0	0.8 ✓	562.7	R
10N	+1-51	0.32 0.35	400	1.3 ✓ 0.6	563.2	R
Axis	+2-00	.035	50.0	1.8 ✓	563.7	R
10S	+2-39	.046	60.0	2.8 ✓	524.7	R
20S	+3-53	.068	70.0	4.8 ✓	566.7	R
30S	+5-52	.103	80.0	8.2 ✓	570.1	R
40S	+9-06	.160	90.0	12.4 ✓	576.3	LR
50S	+10-26	.184	100.0	18.4 ✓	580.3	LR
60S	+13-00	.231	110.0	25.4 ✓	587.3	LR
70S	+15-54	.285	120.0	34.2 ✓	596.1	R
80S	+17-27	.314	130.0	40.8 ✓	602.7	LR
90S	+17-06	.308	140.0	42.1 ✓	605.0	LR

STA	VA	FUNCT	DIST.	DIFF	ELEV		1/129/41	Salt
-----	----	-------	-------	------	------	--	----------	------

10+60

(6)

Salt

50N		TOT		561.1	Refer to page 47. Ground elevation	R
80S	+	16-49	.3021	130.0	39.3 ✓ 600.41	LR
70S	+	18-04	.3261	120.0	39.1 ✓ 600.21	R
60S	+	14-37	.2611	110.0	28.7 ✓ 589.81	R
50S	+	9-31	.1681	100.0	16.8 ✓ 577.91	LR
40S	+	7-23	.1301	90.0	11.7 ✓ 572.81	LR
30S	+	4-56	.0961	80.0	6.9 ✓ 578.01	LR
20S	+	4-12	.0731	70.0	5.1 ✓ 566.21	R
10S	+	3-49	.0671	60.0	4.0 ✓ 565.11	R
A/15	+	3-12	.0561	50.0	2.8 ✓ 563.91	R
10N	+	3-02	.0531	40.0	2.1 ✓ 563.21	R
20N	+	2-35	.0451	30.0	1.4 ✓ 562.51	R
30N	+	1-52	.0331	20.0	0.7 ✓ 561.81	R
40N	+	1-43	.0301	10.0	0.3 ✓ 561.41	R

STA VA FUNDT DIST DIFF. ELEV.

11/29/41

61
5011

10 + 50

50N	T 95	560.8'	Refer To page 47. Ground elevation	R
40N	+0-13	.004 ✓ 10.0° 0.0 ✓ 10.8'		R
30N	+2-02	.036 ✓ 20.0° 0.7 ✓ 61.5'		R
20N	+3-00	.052 ✓ 30.0° 1.6 ✓ 62.4'		R
10N	+3-54	.068 ✓ 40.0° 2.7 ✓ 63.5'		R
AXIS	+3-53	.068 ✓ 50.0° 3.4 ✓ 64.2'		R
10S	+4-03	.071 ✓ 60.0° 4.3 ✓ 65.1'		R
20S	+4-05	.071 ✓ 70.0° 5.0 ✓ 65.8'		A
30S	+5-09	.090 ✓ 80.0° 7.2 ✓ 68.0'		R
40S	+6-09	.108 ✓ 90.0° 9.7 ✓ 70.5'		LR
50S	+8-09	.143 ✓ 100.0° 14.3 ✓ 75.1'		LR
60S	+12-10	.228 ✓ 110.0° 25.1 ✓ 85.9'		R
70S	+14-16	.254 ✓ 120.0° 30.5 ✓ 91.3'		R
80S	+14-47	.264 ✓ 130.0° 34.3 ✓ 95.1'		LR
90S	+16-20	.293 ✓ 140.0° 31.0 ✓ 101.8'		LR

C 1/20. Comptd by D.W.K. 12-1-41
Checked by

Profile of Axis - E Keyway

Sta. + H.I. - El/ev

A-32 626.06

B.M. 629.06

0.24 626.30
629.30

T.P. 614.43
11.87 617.43

0.22 614.65
617.65

12+25 2.0 612.7

12+19 64 608.3

12+11 12.7 602.0

T.P. 601.57
13.08 601.57

1.56 603.13
606.13

12+07 6.0 597.1

12+00 11.6 591.5

T.P. 590.46
12.67 593.46

1.24 591.70
594.70

11+98 5.9 585.8

11+91 11.4 580.3

12/11/41
Fair-Worm
Dickinson 62.
Loring
Jackson
Potak
King
Cole.

Note For profile of axis betw.

12+25 and 12+88 use elev's

1 taken for monthly est.

taken 11/26/41 - Pages 4 to 10

Profile of Axir-E Keyway

12/11/41
Fair-WarmDickinson
Jackson
Polar
Loing
King
Cote.

63

Sta. + H.I. - Elev

591.70
594.70T.P. 579.31
12.39 582.311.27 580.58
583.58

11+75 49 575.7

T.P. 567.87
12.71 570.871.44 569.31
572.31T.P. 556.79
12.52 559.79A-34 560.09
B.M. 3.30 563.096.50 553.58
556.59 553.58

Profile of Axir - East Side

Sta + Hl - Elev

T.P. 579.31

180 581.11

11+50 11.2 569.9

T.P. 1260 568.51

0.47 568.98

11+25 1.5 567.5

11+00 9.0 560.0

T.P. 12.71 556.27

0.24 556.51

10+75 2.5 554.0

10+50 3.8 552.7

10+25 8.3 548.2

10+00 9.7 546.8

T.P. 1244 544.07

0.27 544.34

12/12/41
Fair-WormDickinson
Jackson
Long
Poole
King
Cole.

64

Profile of Axis - E slope

Sta. + H.I. - Elev.

544.34

9+75

100.35

10.9 533.4

12/12/41
Cool - cloudyDickinson
Tackson
Loring
Poloit
King
Cole

65

9+50

128 531.5

toe of bench -

Wedge of bench - top of bank

Profile - 50's of Axis

9+75

4.0 540.3

T.P.

0.99 543.35

12.97 556.32

10+00

7.4 548.9

T.P.

0.45 555.87

12.85 568.72

10+25

10.5 558.2

10+50

0.0 568.7

T.P.

0.54 568.18

944 577.62

10+75

2.9 574.7

Block #16

Profile of Axis - E slope

Sta + H.I. - Elev

577.62

11+00 46 573.0

11+25 38 573.8

11+50 0.1 577.5

11+75 +0.4 578.0

T.P. 0.67 576.95

3.47 580.42

T.P. 1.12 579.30 579.31

12/12/41
Cool - cloudyDickinson
Tackson
Loring
Polak
King
Cole.

66

E 81K #18

→ Starting point of this circuit

This T.P. checked into B.M. See F.B.

587 Page 38

Profile of Axin-Wridge

Sta + H.I - Elev
A-16
B.M.

64955

0.09 64964

3+41 90 6406

T.P. 12.30 637.34

0.74 638.08

3+50 6.3 631.7 Break

T.P. 12.63 625.45

1.01 626.46

3+69 21 624.4

"

T.P. 12.65 613.81

0.37 614.18

3+98 8.0 606.2

"

1 4+01 7.9 606.3

T.P. 13.09 601.09

0.48 601.57

4+26 10.8 590.8

12/12/41
Cool-CloudyJackson
Polar
King
Cote

67

Profile of Axir - W. side

Sta + H.I. - Elev.

60157

T.P.

12.70 58887

0.03 58890

4+53

5.0 5839

4+96

8.3 580.6

T.P.

1.07 587.83

10.48 59831

C-2
T.B.M.

1.87 596.44 596.48

Cut in on H.I. 594.61

Bench - top of dirt bank

See pg 71 BK 587

4+40 12.6 82.0

TP 12.7⁶ 581.85

1 0.63 82.48

4+70 5.2 77.3

TP 11.92 70.56

280 73.36

Cont Pg #71

12/12/48
Cool - cloudyJackson
Dolat
Loing
King
Cote.

68

Profile of 50's of Axis-E side

12/16/41
Fair-WarmDICKINSON 69
JACKSON
POLE
Loring
King
Cole.Sta. + H.I. - Elev.
A-23
BM. 523.86

12.39 536.25

9+42 13.2 523.0

9+59 11.2 525.0

9+69 6.6 529.6

9+79 3.1 533.7

T.P. 0.63 535.62

12.88 548.50

9+88 10.0 538.5

10+03 9.0 539.5

T.P. 0.99 547.51

12.94 560.45

10+25 1.1 559.3

T.P. 0.06 560.39

13.06 573.45

10+50 5.2 568.2

Profile of 50's of Ax in E. side

Sta + H.I. - Elev.

57345

T.P.

3.98 564.52

A-34

B.M.

17.91 569.54

10.94 553.58 553.58

12/16/45
Fair-Warm

Dickinson
Jactron
Polar
Loing
King
Cote.

70

533.51

9+94

2.6 530.9

+42

8.6 524.9

See pg 69 BK 587 - Cot In as H.I.

12/20/45 RF

PROFILE West Keyway Avs

12/20/41

71.

73.36

4+90

5.6 67.8

5+20

7.0 66.4

TP

165' 571.71

3.45 575.16

BM#7

9.26 575.90

12-20-41

PROFILE AXIS EAST KYNX

BM 134

553.58

1143 565.01

TP

5.34 559.67

8.63 568.30

11+70

1.5 66.8

11+47

9.1 59.2

TP

12 76 556.54

0.96 556.50

11+20

4.3 52.2

10+64

9.0 47.5

10+47

6.9 49.6

10+10

14.0 42.5

TP

11.31 545.19

0.83 546.02

12 66 533.36

1.10 34.46

Eckers
Cole
Polak
Dickinson

72

AXIS PROFILE 12-20-41 (Cont)

73.

534.46

9170

71 527.4

TP

13.00 521.46

161 523.01

9160

58 17.3

9120

98 13.3

TP

461 518.46

10 74 529.20

BM 16

5.36 523.84 529.86

VA Fwdt Dist DIFF ELEV.

GR.

12 + 60

50N

20'

30N

30'

20N

40'

10N

50'

AXIS

462.30 (Level)

VA Fwdt Dist DIFF E

198.4

46

193.8

624.53
11.16
635.69
633
629 36

10+75

11+25

11+70

36

80

11.0

606.2

13.0

649.2

2.2

0

640.6

640

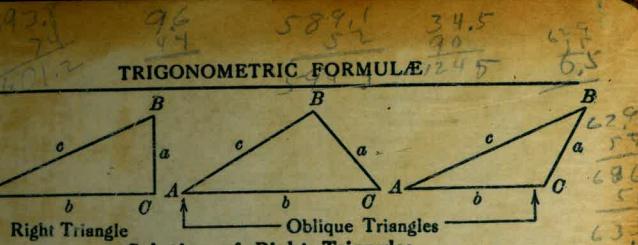
631.7

8.7

645.4

4.4

636.0



TRIGONOMETRIC FORMULAE

Solution of Right Triangles

or Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{b}$, $\cosec = \frac{c}{a}$

Given a, b Required A, B, c $\tan A = \frac{a}{b} = \cot B, c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$

a, c A, B, b $\sin A = \frac{a}{c} = \cos B, b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$

A, a B, b, c $B = 90^\circ - A, b = a \cot A, a = \frac{a}{\sin A}$

A, b B, a, c $B = 90^\circ - A, a = b \tan A, c = \frac{b}{\cos A}$

A, c B, a, b $B = 90^\circ - A, a = c \sin A, b = c \cos A$

Solution of Oblique Triangles

Given $1, B, a$ Required b, c, C $b = \frac{a \sin B}{\sin A}, C = 180^\circ - (A+B), c = \frac{a \sin C}{\sin A}$

$1, a, b$ B, c, C $\sin B = \frac{b \sin A}{a}, C = 180^\circ - (A+B), c = \frac{a \sin C}{\sin A}$

$1, b, C$ A, B, c $A+B=180^\circ - C, \tan \frac{1}{2}(A-B) = \frac{(a-b) \tan \frac{1}{2}(A+B)}{a+b}, c = \frac{a \sin C}{\sin A}$

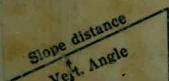
$1, b, c$ A, B, C $s = \frac{a+b+c}{2}, \sin \frac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{bc}}, \sin \frac{1}{2}B = \sqrt{\frac{(s-a)(s-c)}{ac}}, C = 180^\circ - (A+B)$

$1, b, c$ Area $s = \frac{a+b+c}{2}, \text{area} = \sqrt{s(s-a)(s-b)(s-c)}$

$1, b, c$ Area $\text{area} = \frac{b c \sin A}{2}$

B, C, a Area $\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL



Horizontal distance

When the rise is known, the horizontal distance is approximately:—the slope distance less the square of the rise divided by twice the slope distance. Thus: rise=14 ft.

slope distance=302.6 ft. Horizontal distance=302.6 - $\frac{14 \times 14}{2 \times 302.6}$ = 302.6 - 0.32 = 302.28 ft.

Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = $5^\circ 10'$. From Table, Page IX, $\cos 5^\circ 10' = .9958$. Horizontal distance = $319.4 \times .9958 = 318.09$ ft.

Horizontal distance also = Slope distance minus slope distance times (1—cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\cosine 5^\circ 10' = .9958$. $1 - .9958 = .0041$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.08$ ft.

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