

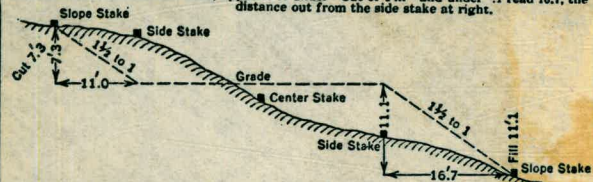
W

593

5
~~293~~
 593

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 Roadway of any Width. Side Slopes 1 1/2 to 1.

In the figure below: opposite 7 under "Cut or Fill" and under 3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	Distance out from Side or Shoulder Stake										Cut or Fill
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

KEUFFEL & ESSER CO., N. Y.

10,892-2. y. cc. ys. cM.

MICROFILMED

JAN 13 1965

The paper in this book No. F370A
 is made of 50% high grade rag stock
 with a WATER RESISTING surface sizing.

533

MICROFILMED

JAN 14 1968

The above is the book no. 6104

It is held in 600 mill. grade microfiche

with a WATER RESISTANT COATING

FORNERS & CO., INC.

—INDEX—

PAGES

Unit No. Sorrento Pipe Line

1 to 11 Level Notes - Item 1

1-11 T.P.s & ϕ Levels Sta 0+0 to 73+12⁰⁰

16 Resurvey of Pipe Line at Sorrento

17 Tie to Cassidy Tract

STA B.S. HI F.S. ELEV.

2.03 ✓

BM - City Brass Plug South end SW wing
of concrete abutment on Sorrento
RR bridge over old highway.

π 1 3.73 5.76

TP 1 4.64 1.12

π 2 5.32 6.44

TP 2 5.19 1.25

π 3 7.66 8.91

TP 3 3.04 5.87

π 4 4.25 10.12

TP 4 5.75 4.37

π 5 2.03 6.40

TP 5 5.40 1.00

π 6 4.10 5.10

TP 6 3.38 1.72 2.54 "22 On Tel. Pole

π 7 4.98 6.70

TP 7 3.33 3.37 ✓ 3.73 "21 On Tel. Pole

2.03

32.07

34.10

30.73

3.37

30.73

1
K Messersmith
& Snyder
Oct. 29, 1941

✓

STA	BS	HI	F.S.	ELEV.
-----	----	----	------	-------

TP 8	4.03	7.40		337 ✓
------	------	------	--	-------

TP 8			7.34	0.06
------	--	--	------	------

TP 9	4.06	4.12		
------	------	------	--	--

TP 9			1.29	2.83	384 - #20 Nail in Tel. Pole No. 652
------	--	--	------	------	-------------------------------------

TP 10	12.18	15.01		
-------	-------	-------	--	--

TP 10			0.36	14.65
-------	--	--	------	-------

TP 11	12.86	27.51 ✓		
-------	-------	---------	--	--

0+00 ±			2.50	25.0
--------	--	--	------	------

+50 ±			4.3	23.2
-------	--	--	-----	------

1+00 ±			6.1	21.4
--------	--	--	-----	------

+50 ±			7.3	20.2
-------	--	--	-----	------

2+00 ±			8.9	18.6
--------	--	--	-----	------

+50 ±			10.5	17.0
-------	--	--	------	------

{ TP #11 2+55 ± PI			10.67	16.84	2x2 Hub 2-2" Water Lines have to be moved
-----------------------	--	--	-------	-------	---

TP 12	1.82	18.66		
-------	------	-------	--	--

3+00 ±			2.80	15.9
--------	--	--	------	------

STA	BS	HI	F.S.	ELEV.
BC 3+41 1/2		18.66	3.8	14.9
3+50 ±			4.0	14.7
4+00 ±			5.1	13.6
+50 ±			6.3	12.4
5+00 ±			7.3	11.4
+50 ±			8.3	10.4
TP #12			8.21	10.45
TP #12	3.06	13.51		
6+00 ±			4.1	9.4
+50 ±			5.2	8.3
7+00 ±			5.6	7.9
+50 ±			6.6	6.9
+80 ±			7.0	6.5
+90 ±			8.0	5.5
8+00 ±			8.7	5.3
{ TP #12 8+13			8.30	5.21

STA.	B.S.	HI.	F.S.	ELEV.
				5.21 ✓
π #13	3.78	8.99		
8+50 †			2.2	6.8
9+00 †			4.6	4.4
+50 †			4.9	4.1
10+00 †			5.4	3.6
10+00			10.6	-1.6 Water Surface
+50 †			5.8	3.2
11+00 †			6.1	2.9
11+17 ⁷² E.C.			6.32	2.67
π #14	3.15	5.82		
11+50			3.4	2.4
12+00			4.5	1.3
12+50			6.4	-0.6
12+84			6.90	-1.08 Top piling
13+25			8.10	-2.28 Water Surface

STA.	B.S.	HI.	F.S.	ELEV.
13+00		5.82 ✓	8.10	-2.3
13+50			7.8	-2.0
14+00			7.2	-1.4
13+40			6.90	-1.08 Top piling
14+50			5.1	0.7
15+00			4.3	1.5
15+50			4.5	1.3
16+00			4.5	1.3
16+50			4.5	1.3
T.P. #15			4.55	1.27 old. T.P. #18
π #15	4.69	5.96		
17+00			4.8	0.2
+50			4.8	0.2
18+00			4.6	0.4
+50			4.9	0.1
19+00			7.0	-1.0

Sta.	B.S.	HI	F.S.	Elev.		Sta.	B.S.	HI	F.S.	Elev.	
		5.96 ✓									5
19+50			8.2	-2.2	Water Sur/acc	26+00		6.02 ✓	4.5	1.5	
20+00			8.7	-2.7		+50			4.4	1.6	
+50			8.4	-2.4		27+00			4.9	1.1	
21+00			7.8	-1.8		+50			4.6	1.4	
+30			4.6	0.4		T.P.#17			4.35	1.67	27+54
+50			3.8	1.2		T.#17	3.92	5.59 ✓			
T.P.#16			3.98	1.98		28+00			4.0	1.6	
T.#16	4.04	6.02				+50			4.4	1.2	
22+00			4.1	1.9		29+00			4.3	1.3	
+50			4.3	1.9		29+50.13			4.1	1.5	
23+00			4.3	1.9		30+00			4.3	1.3	
+50			4.5	1.5		30+25			7.8	-2.2	Water Surface
24+00			4.5	1.5		+50			4.3	1.3	
+50			4.5	1.5		31+00			4.1	1.5	
25+00			4.7	1.3		+50			4.2	1.4	
+50			4.4	1.6		32+00			4.2	1.4	

Sta.	B.S.	H.I.	F.S.	Elev.
		5.59 ✓		✓
32+50			4.0	1.6
33+00			4.0	1.6
+50			3.8	1.8
34+00			3.9	1.7
T.P.#18			3.91	1.68 34+00
π#18	4.33	6.01		
34+50			4.2	1.8
34+98.93			4.3	1.7
35+50			4.2	1.8
36+00			4.1	1.9
NOTE 36+25			8.0	-2.0 Water Surface
+50			4.1	1.9
37+00			4.0	2.0
+50			4.2	1.8
38+00			4.0	2.0
+50			4.5	1.5

Sta.	B.S.	H.I.	F.S.	Elev.	
		6.01 ✓		✓	6
39+00			4.0	2.0	
T.P.#19			4.04	1.97 39+00	
π#19	4.20	6.17 ✓			
39+50			4.2	2.0	
40+00			4.0	2.2	
40+50			4.1	2.1	
41+00			4.2	2.0	
+50			4.3	1.9	
42+00			4.4	1.8	
+50			4.6	1.6	
NOTE 42+75			8.5	-2.3 Water Surface	
43+00			4.7	1.5	
+50			3.9	2.3	
44+00			4.0	2.2	
+50			3.7	2.5	

Sta	B.S.	H.I.	F.S.	Elev.
		6.17 ✓		✓
T.P.#20			4.20	1.97 45+00
π#20	4.82	6.79		
45+00			4.5	2.3
+50			4.3	2.5
46+00			4.3	2.5
+50			4.3	2.5
47+00			4.5	2.3
+50			4.5	2.3
47+75			8.5	-1.7 Water Surface
48+00			4.4	2.4
+50			4.4	2.4
49+00			4.3	2.5
+50			4.2	2.6
50+00			3.8	3.0
+50			3.8	3.0
51+00			3.6	3.2

Sta	B.S.	H.I.	F.S.	Elev.
T.P.#21			3.63	3.16 ✓
π#21	4.80	7.96 ✓		
51+50			4.7	3.3
52+00			4.7	3.3
52+50			4.7	3.3
53+00			4.4	3.6
53+50			4.2	3.8
54+00			4.0	4.0
54+50			3.6	4.4
55+00			3.3	4.7
55+50			3.2	4.0 ✓
T.P.#22			2.40	5.56 ✓
π#22	7.32	12.88		
T.P.#23			3.51	9.37
π#23	3.78	13.15		
T.P.#24			4.85	8.30 ✓

Sta.	B.S.	HI.	FS	Elev.					
					8.30				
π#24	4.26	12.56							
TP#25			4.56	8.06	8.00				
π#25	4.64	12.70							
TP#26			2.12	10.58	10.52				
π#26	2.35	12.93							
TP#27			4.51	8.42	8.36				
π#27	1.76	10.18							
TP#28			3.93	6.25	6.19				
π#28	2.08	8.33							
TP#29			3.70	4.63	4.57				
π#29	3.11	7.74							
TP#30			2.55	5.17	5.13				
π#30	2.48	7.67							
TP#31			2.86	4.82	4.76				
π#31	5.50	10.32							
TP#32			2.55	7.27	7.11				

Sta	B.S.	H.I.	F.S.	Elev.	Sta	B.S.	H.I.	F.S.	Elev.	
							13.58✓			
π#32	7.90	^{15.61} 15.67			58+50			7.9	5.7	
T.P.33			8.09	^{7.52} 7.58	58+86.53			7.8	5.8	
π#33	3.16	^{10.68} 10.74			59+00			10.4	3.2	
T.P.34			8.78	^{1.90} 1.96	59+11			9.2	4.4	Toe Slope
					59+21			4.5	9.1	Shoulder
					59+29.52			2.6	11.0	Top of Rail
T.P.#22				5.56✓	T.B.M.	59+32		3.3	10.3	E of track
π	7.52	13.08			59+34.52			2.9	10.7	Top of Rail
T.P.#1			3.26	2.82	59+47			4.7	8.9	Shoulder
π 1	3.76	13.58✓			59+50			7.1	6.5	
					59+55			10.2	3.4	Toe Slope
56+13.32			8.5	5.1	5.1	60+00		9.4	4.2	
56+50			8.6	5.0		+50		10.6	3.0	
57+00			8.5	5.1 ✓		61+00		9.5	4.1	
+50			8.5	5.1 ✓		T.P.#2		9.49	4.09	61+00
58+00			8.5	5.1 ✓		π#2	4.20	8.29✓		

Sta	B.S.	H.I.	F.S.	Elev.	Sta	B.S.	H.I.	F.S.	Elev.
		8.29 ✓					8.29 ✓		
61+50			4.0	4.3	66+57			5.0	3.3 Bot. Cut
62+00			5.1	3.2	Shoulder	66+62		4.1	4.2 Shoulder
62+08			7.1	1.2	Bot. Cut	67+00		4.5	3.8
62+13			5.1	3.2	Shoulder	TP#3		3.89	4.40 4.49 67+25
+50			4.9	3.4	TP#3	12.02	16.42 76.44		
63+00			4.5	3.8	67+50			12.7	3.7
+50			4.4	3.9	67+61			12.0	4.4 Shoulder
64+00			4.6	3.7	67+65			13.0	3.4 Bot. Cut
+50			4.5	3.8	67+74			13.1	3.3 Bot. "
65+00			4.0	4.3	67+83			12.7	3.7 Shoulder
+50			4.0	4.3	68+00			12.1	4.3
66+00			4.4	3.9	68+50			12.2	4.2
66+35			4.3	4.0	Shoulder	68+75		12.5	3.9
66+43			5.0	3.3	Bot. Cut	68+95		9.5	6.9
66+50			4.4	3.9	Shoulder	69+00		9.6	6.8
66+55			4.2	4.1	"	+50		6.1	10.3

Sta.	B.S.	H.I.	F.S.	Elev.
		16.42 16.44		
70+00			1.5	14.9 16.10
T.P.#4			0.32	16.12
π #4	12.55	28.65 28.67		
70+50			9.6	19.1
71+00			5.1	23.6
71+50			1.4	27.3
T.P.#5			0.21	28.44 28.46
π #5	9.54	37.98 38.00		
72+00			6.6	31.4
72+13.05			5.1	32.9
72+50			1.9	36.1
73+00			1.3	36.7
73+12.80			3.3	34.7

on pipe Top Bell.

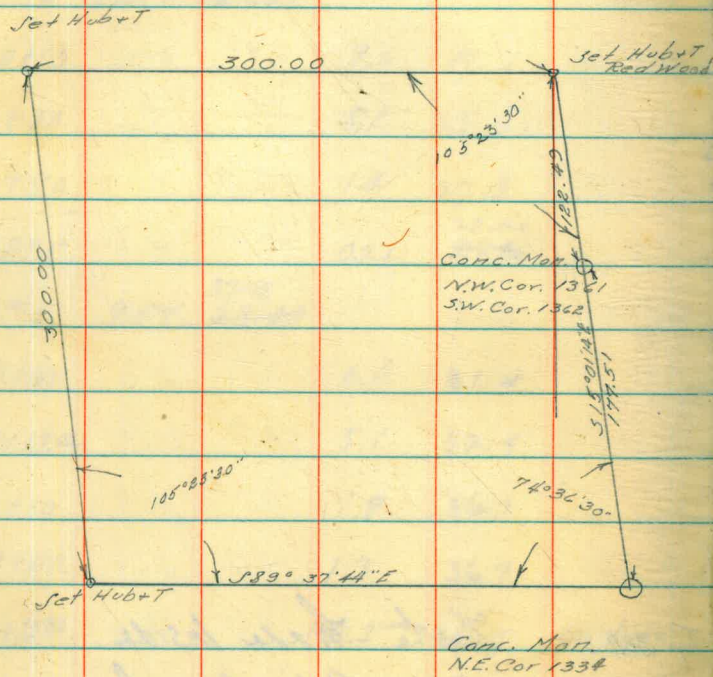
Note from inside
18" C.I. Pipe should be -1.75
or 33.0

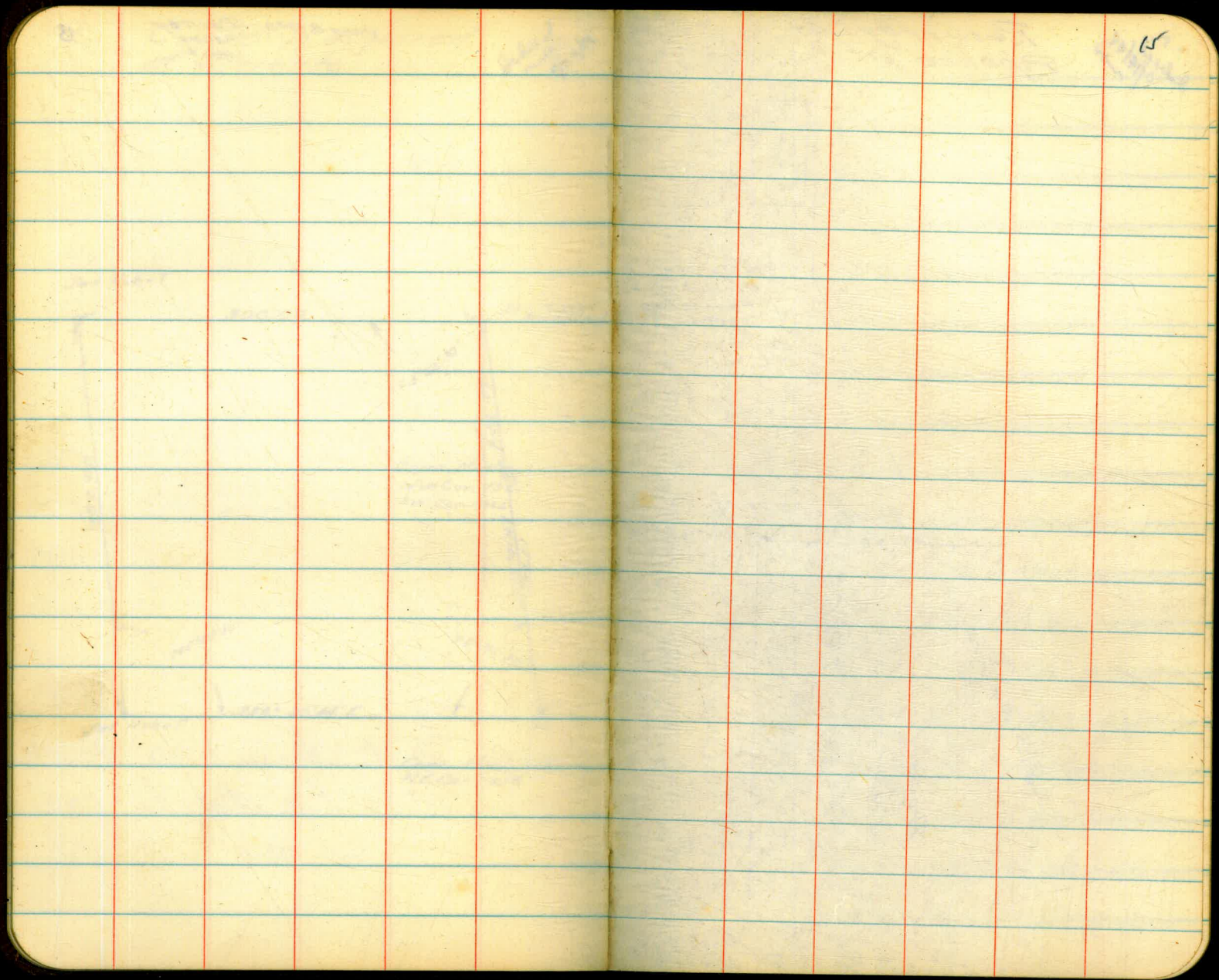
City Prop. acquired
at Sorrento

Index of
map
07/9/48

June 8, 1948 Rainey
Baker
West

13

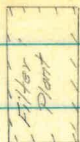




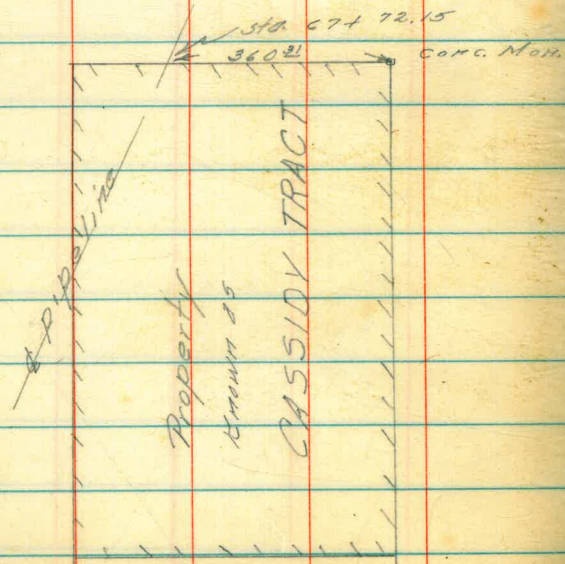
Subst
of
Pipes

Resurvey of Pipeline at Sorrento

17-



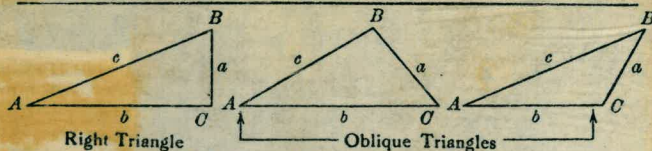
3rd Sta 72+13.85
Reestablished
as per P10
E.B. 686



Frederick
Earl, Messersmith 5A9-12-2183

14+00	135.00	
+50	134.233	134.61
		133.95
15	133.466	133.09
+50	132.700	132.31
16+0	131.933	
	39	131.56
+50	131.166	
		130.79
1740	130.4	
	766	
	32	

TRIGONOMETRIC FORMULÆ



Solution of Right Triangles
For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{a}$, $\text{cosec} = \frac{c}{b}$

Given	Required	Formulas
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B$, $c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$, $b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$, $b = a \cot A$, $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$, $a = b \tan A$, $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$, $a = c \sin A$, $b = c \cos A$

Solution of Oblique Triangles

Given	Required	Formulas
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$, $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$, $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$, $C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}$, $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = $5^\circ 10'$. From Table, Page IX, $\cos 5^\circ 10' = .9959$. Horizontal distance = $319.4 \times .9959 = 318.09$ ft.
Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\text{Cosine } 5^\circ 10' = .9959$. $1 - .9959 = .0041$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.09$ ft.
When the rise is known, the horizontal distance is approximately:—the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft. slope distance = 302.6 ft. Horizontal distance = $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.