

FWA1
W units 5
6
626-A

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	II
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

Copyright, 1914, by Eugene Dietzgen Co.

This Field Book is manufactured
of a high grade 50% Rag Paper
having a WATER RESISTING surface.

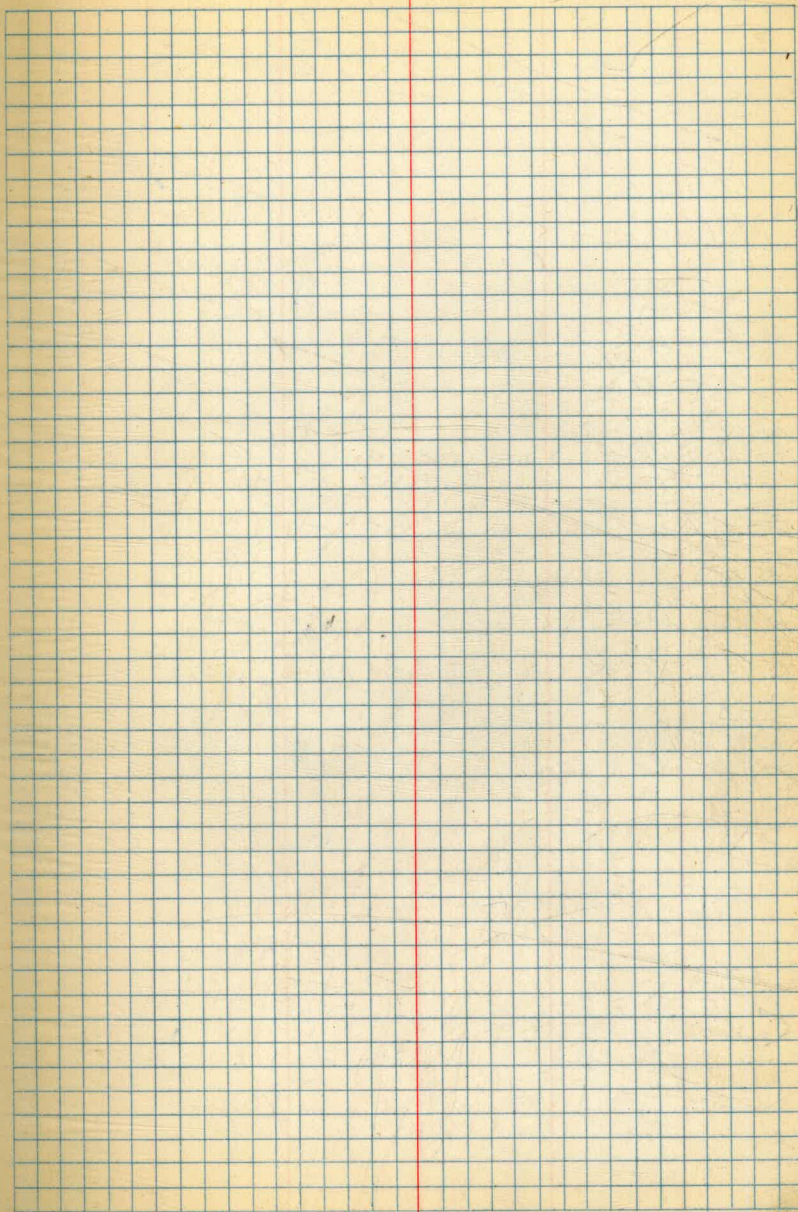
Please Return to
City of San Diego Water Dept.
Room 268 Civic Center
Telephone Main 5161

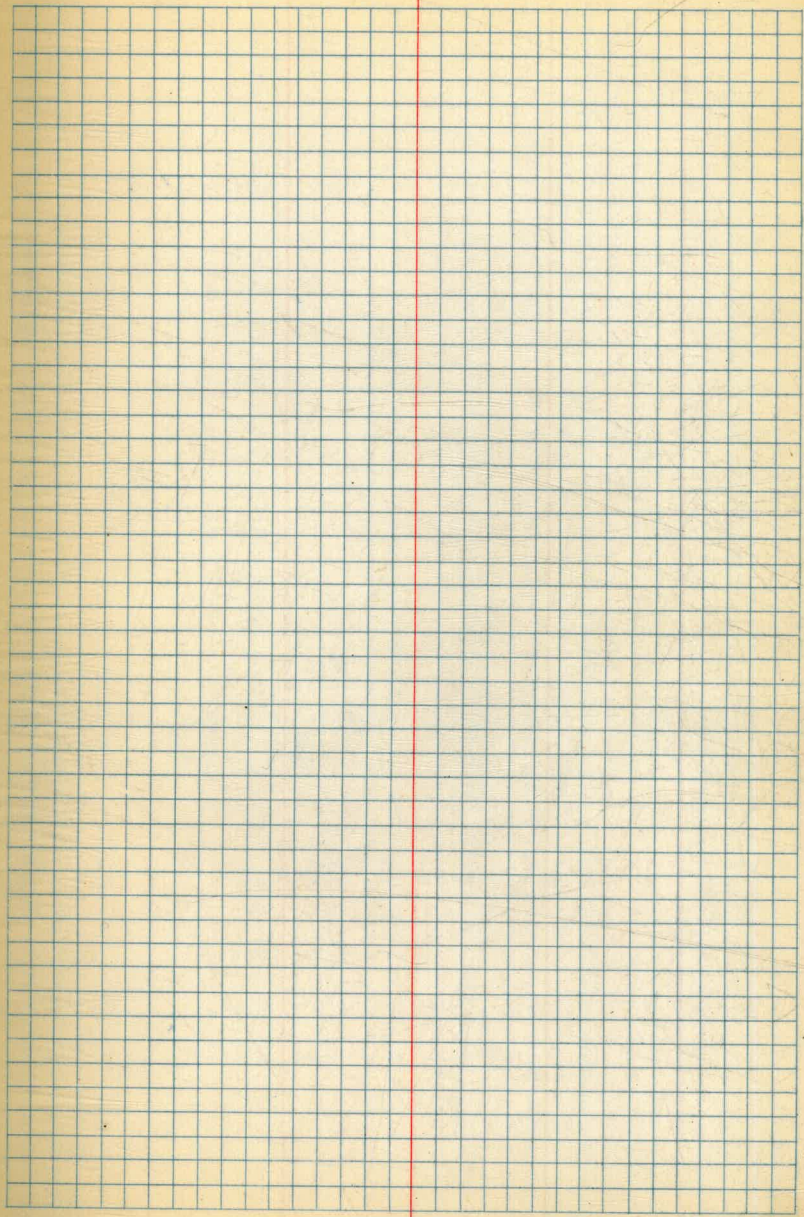
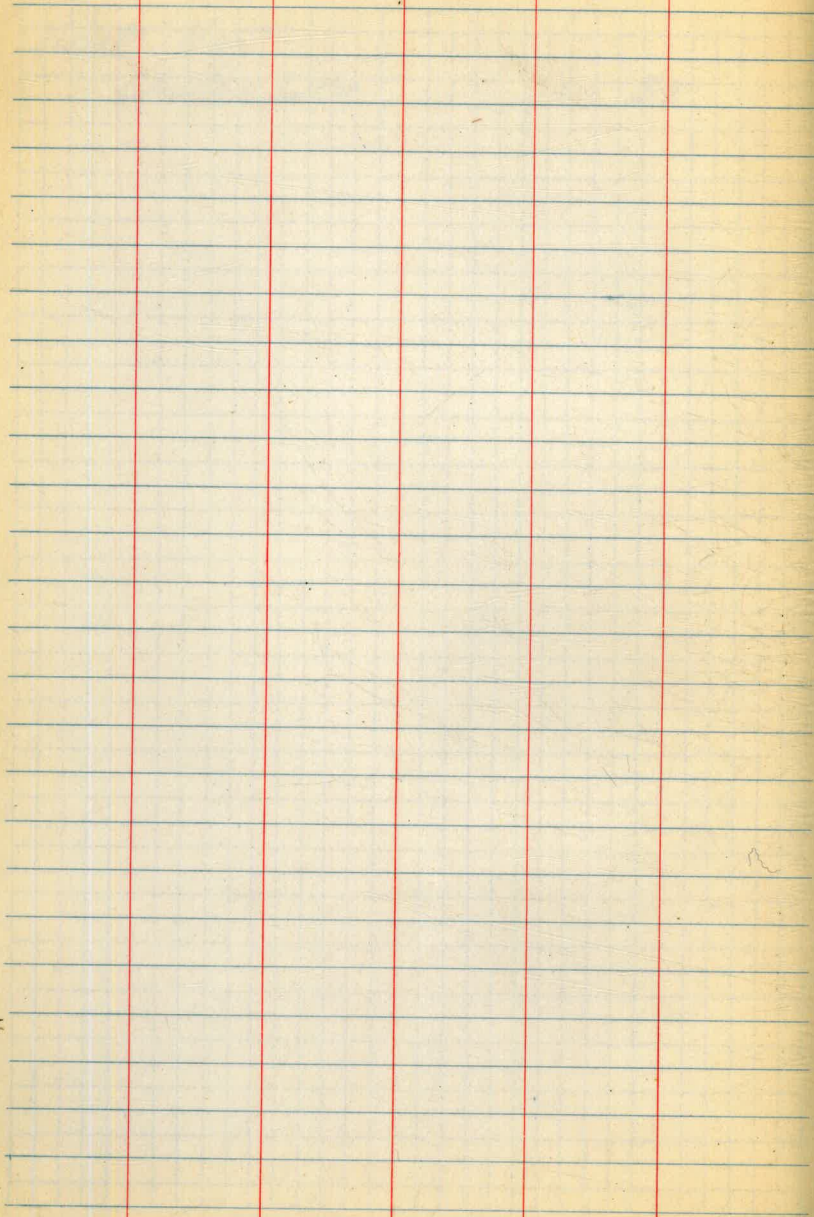
MICROFILMED

JAN 13 1965

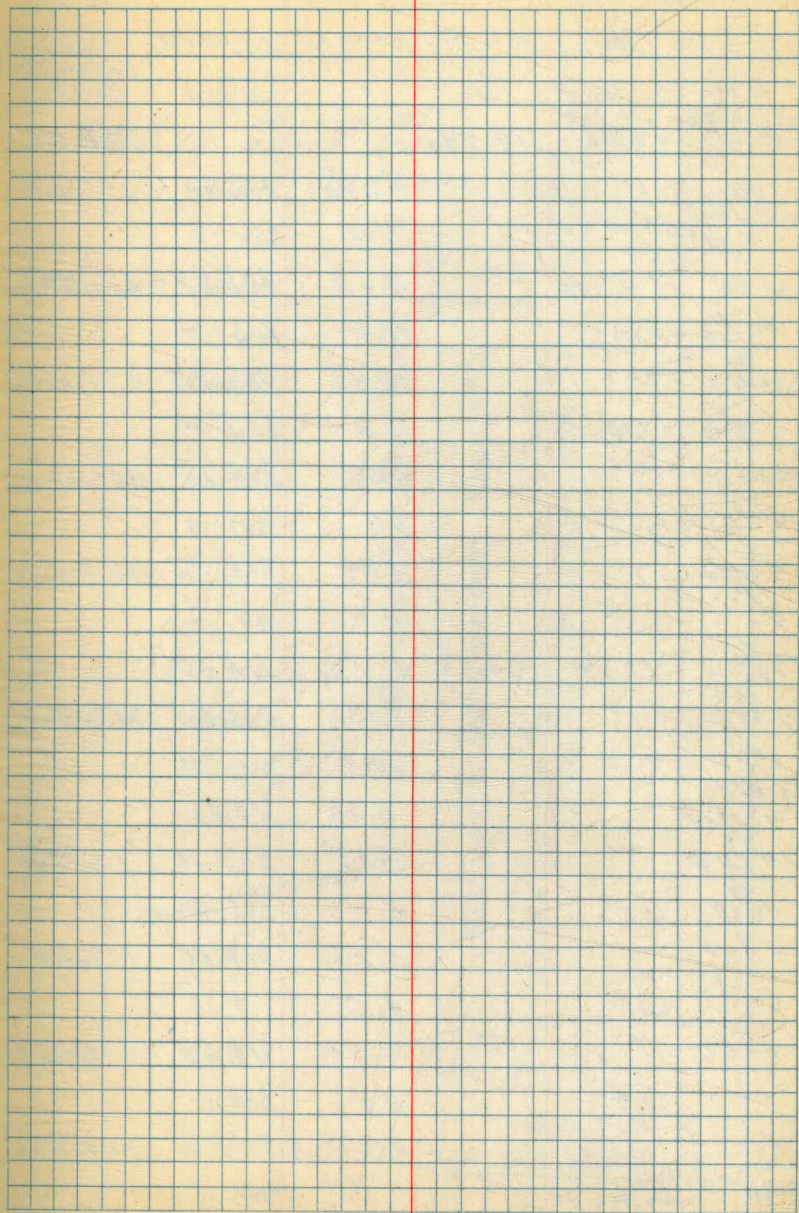
Unit No 5
Chollas Linn

1-33





3



4 SURVEY GRADES FOR HOLLAS PIPE LINE.

LEVELS - STATION		813+00 - WEST		
	+ HI	-	Elev	Bottom Trench Grade
T.P. #10	8.23	314.79		306.56
813+00		12.45	302.34	297.48
" 6" Pipe } Ground Elev.		12.0	302.18	
813+25	7' offset	11.73	303.06	297.50
" 6" Pipe } Gnd - Pipe		11.5	303.29	
813+50	7'	10.50	304.29	298.67
" 6" Pipe } Gnd Pipe		10.3	304.19	
814+00	7'	8.02	306.77	301.00
"	G-P	7.8	307.0	
814+50	7'	3.82	310.97	304.50
"	G.P.	4.2	310.6	
T.P.	10.37	324.39	0.77	314.02
815+00	7'	8.85	315.54	308.00
"	G.P.	10.3	314.09	
on old offset hub		8.36	316.03	
815+50	7'	7.29	317.10	310.00
"	G.P.	8.5	315.9	
816+00	7'	5.23	319.16	312.00
"	G.P.	6.6	317.8	
816+50	7'	4.75	319.64	314.00
"	G.P.	5.0	319.4	
816+91.9	East Edge Precast	3.45	320.94	313.92
817	G.P.	3.70	320.7	

NOTE = 7' = Hub on Offset = GP = Ground on Pipe Line

10 MAY 1942
Weather - Cold - Cloudy
H.S. Gierlich
Ed. Rottman
1422 - Landis St
Ph: R-3041

Selvey K. Hale
3402 - 22nd St
Ph: R-7019

D.M. Abate
3962 - 8th Ave

Cut on
7' offset
Stake

On T.P. #10 on original
offset line

4.80 on bank | 813+00

5.56 on bank

5.02 on bank

5.77 on bank

6.47 on bank

on rock in rd

7.54 on bank

7.10

7.16

5.64

7.02

NEW 36" PIPE LINE

NEW OFFSET LINE

Found Hubs Old Offset Line



7' 13.5

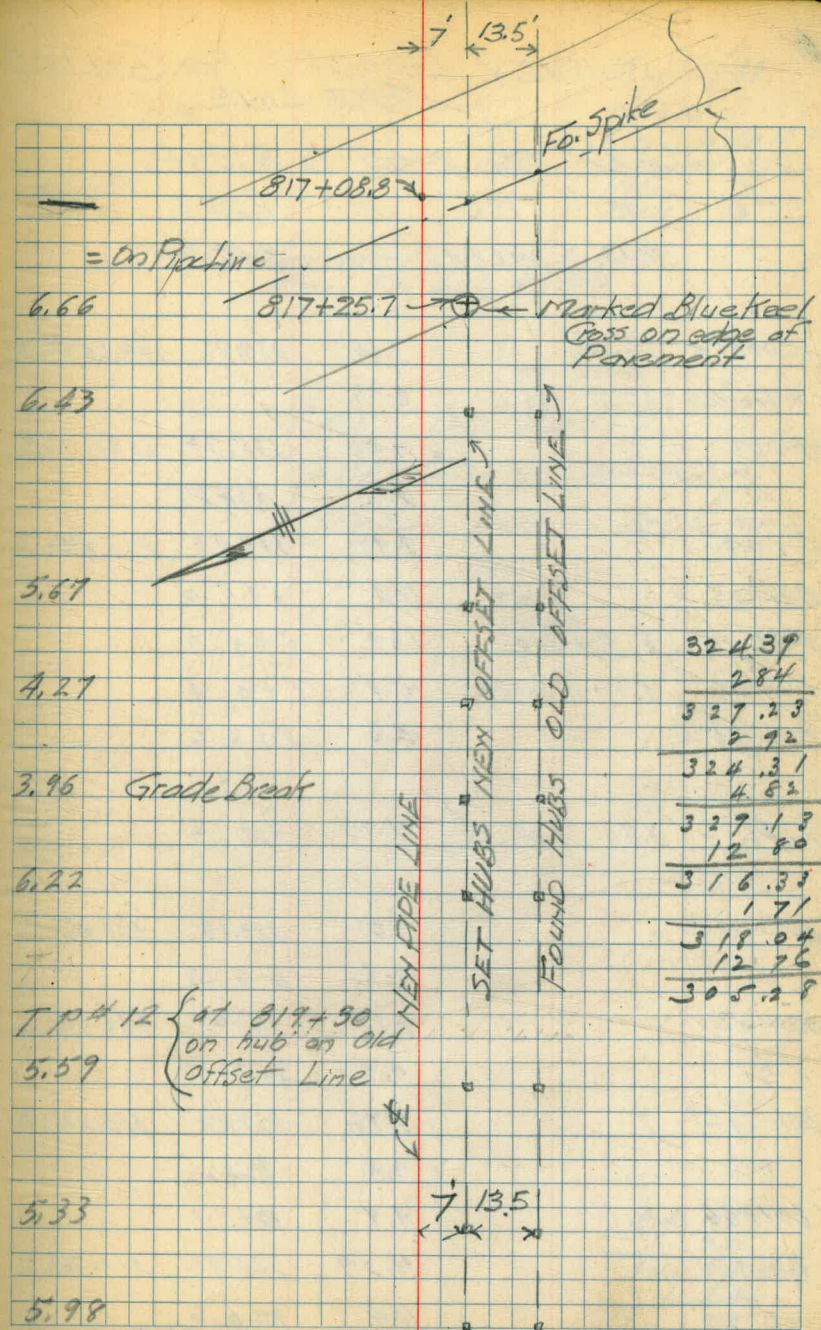
816+91.9

54th St

Marked Blue Keel Cross
in edge of Pav.

See pages 218 following for trench grades.

Sta.	+	H.I.	-	Elev.	Bottom of Trench Grade
		324.39			
817+08.8	± 64TH St.		3.57	320.82	313.89
"	On Pavement		2.62	320.97	
817+25.7	West Edge of Pavement		3.87	320.52	313.86
Ground 2.00	of Pipe Line		4.02	320.37	
817+50	7'		4.15	320.24	313.81
"	GP		4.50	319.89	
"	on old offset hub		2.92	321.47	
T.P.	2.84	324.31	2.92	321.47	
818+00	7'		4.87	319.44	313.77
"	GP		5.1	319.2	
818+50	7'		6.41	317.90	313.63
"	GP		6.1	318.21	
818+60	7'		6.74	317.57	313.61
"	GP		7.0	317.31	
819+00	7'		9.66	314.65	308.43
"	GP		9.5	314.81	
T.P.	4.82	316.33	12.80	311.51	
T.P.#10			2.72	313.61	
819+50	7'		8.78	309.55	301.96
"	GP		8.0	308.33	
T.P.	1.71	305.28	12.76	303.57	
820+00	7'		4.45	300.83	295.50
"	GP		4.3	300.98	
820+50	7'		10.30	294.98	289.00
"	GP		11.0	294.24	
"	on old offset line		12.38	292.98	



324.39
2.84
327.23
2.92
324.31
4.82
329.13
12.80
316.33
1.71
318.04
12.76
305.28

Use as B.M.

6

SURVEY GRADES FOR HOLLAS
PIPE LINE

Levels	Sta. 0+00 To 8+30.00				
STA	+	H.L.	-	ELEV.	TRENCH GRADE
	0.13	342.84		342.71	
800+67.4			3.00	339.83	339.00
"					
Gr & Trench			2.90		
801+00			7.50	335.34	327.11
"			8.0	334.84	
801+09.2			7.90	334.94	326.47
801+23			11.8	331.0	
801+25			13.8	329.0	
801+34			15.4	327.4	
801+35			14.2	328.6	
T.P.	0.84	331.98	11.70	331.14	
801+40.2			3.80	328.18	321.33
"			3.9	328.08	
801+50			5.13	326.85	320.67
"			4.9	327.08	
801+77.0			7.76	324.22	318.35
"			7.8	324.2	
801+96			9.9	321.1	
802+00			11.27	320.71	316.53
"			11.4	320.6	
	0.97		11.70		

5-17/42

Wilcox?
Gierlich's Ch of P.
Rathman Notes
Hala #
Abate #

Cut

NE Cor. Concrete Box. Sta 800+67.
Ref FB 626 Pg 29

5.87

8.23

8.47

Note. On May 16
Center lines marked out
staked, but no levels run

Wilcox
Hala
Abate
Charlie

6.85

6.28

5.87

7.18

342.71
97
343.68
11.70
331.98

7

Sta.		H.I		Elev.	Trench Grade
802+03	Profile	331.98	-	321.6	
802+14.97			10.4	321.24	315.39
"			10.8	321.2	
802+25	Profile		11.1	320.9	
802+50.2			13.06	318.92	313.27
"	±		13.1	318.9	
T.P.	1.06	319.98	(13.06)	318.92	311.50
802+87.39			3.35	316.63	311.50
"	±		3.3	316.7	
803+00			4.02	315.96	310.90
"	±		4.0	316.0	
803+24.05			6.26	314.72	309.83
"	±		6.4	314.6	
803+50			6.37	313.61	308.50
"	±		6.3	313.7	
803+60.22			6.83	313.15	307.99
"	±		6.8	313.2	
804+00			8.66	311.32	304.75
"	±		8.6	311.4	
check on old hub			7.86	312.12	311.9
803+00			3.49	316.49	316.50
check on old hub					
804+25	Profile		11.2	308.8	

Cut

5.9

5.65

5.13

6.06

4.89

5.11

5.16

6.6

(FB 620 P 30)

331.98
 1.06
 333.04
 13.06
 319.98

8

Sta.	H.I.	Elev.	Trench Grade
	319.98	-	
T.P.	0.48	308.03✓	12.43
			307.55
804+50		1.51	306.52
"	4	1.7	306.3
804+75	4	5.5	302.5
805+00		7.68	310.35
"	4	7.7	300.3
"			
805+25	Profile	9.4	298.6
805+40		10.90	297.13
"		10.1	297.9
805+49	Hub on south side	11.94	296.09
"	4	10.5	297.53
"	Hub on North side	10.55	297.48
805+75		11.3	296.7
806+00		14.10	293.93
"	4	11.74	296.29
806+25	Profile	11.2	296.8
806+50		11.51	296.52
"		11.1	296.9
806+75	Profile	10.1	297.9
807+00		8.80	299.23
"	4	8.9	299.1
807+25		6.8	301.2
807+50	old Hub check elev.	6.20	301.83

Cut

5.52

5.46

7.13

6.16

7.55

4.33

5.07

5.93

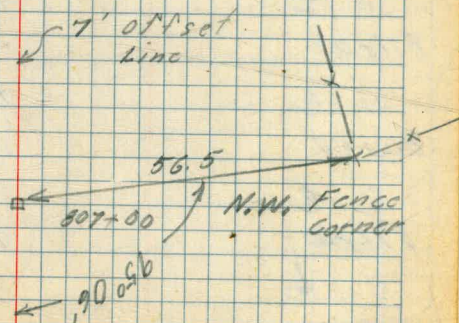
319.98

.48

320.46

12.43

509.03



9

Sta.	+	308.03v H.I.	-	Elev.	Trench Grade
807+50			5.38	302.65	295.15
"	±		5.6	302.4	
808+00			4.35	303.68	297.00
"	±		4.1	303.9	
808+50			3.62	304.41	297.05
"	±		3.3	304.7	
809+00			3.50	304.53	297.10
"			3.1	304.9	
808+50	check on old Hub		1.42	306.61	306.60
809+50			3.65	304.38	297.15
"			3.1	304.9	
T.P.	5.38	309.76	3.65	304.38	
810+00			5.32	304.44	297.19
"	±		4.80	304.96	
810+50			4.92	304.84	297.24
"	±		4.90	304.86	
811+00			5.25	304.51	297.29
"	±		5.0	304.76	
811+50			6.22	303.54	297.33
"	±		6.00	303.76	
812+00			7.15	302.61	297.38
"	±		6.7	303.08	
812+50			7.56	302.70	297.42
"	±		7.1	302.68	

Cut

7.50

6.68

7.36

7.43

7.23

7.25

7.60

7.22

6.21

5.23

4.78

308.03

5.38

313.41

3.65

309.76

Sta.	+	H.L.	-	Elev
813+00		309.76✓	7.50	302.26 302.34
B.M. #2			3.27	306.49
T.P.	9.31	312.20	6.87	302.89
T.P.	12.55	324.03	0.72	311.48
B.M.			2.05✓	<u>321.98</u>
816+50			4.45✓	319.58 319.64

Spike in Tel. Pole # 33519T North of Road at 810+60

Top of body flange of 4" gate valve on Air Valve at 818+00

11 27 May 1942

Stn	BS	HI	F.S	Red	Elev. Ground or Elev
B.M.	3.24	325.22			321.98 ✓
TP	0.36	312.84	12.74		312.48
TP	1.45	301.97	12.32		300.52
820+50.0				6.57	295.20
821+0-0				12.07	289.90
"				12.65	289.32
TP	0.64	291.12	11.49		290.48
821+10-0	5.69			5.92	285.20
"				6.11	285.01
822+0-0				8.99	282.13
"				8.99	282.13
822+50-0				10.26	280.66 ✓
"				10.65	280.47
TP			10.03		281.09 ✓
			46.58		
TP	0.35	281.44 ✓			281.09 ✓
823+0-0				2.96	278.48
"				2.65	278.79
823+50-0				4.39	277.05
"				3.86	277.58
824+0-0				4.06	277.38
"				4.27	277.17
824+50-0				5.28	276.16 ✓
"				5.09	276.35

May 28 -

E.H. Wilcox

Grade	Cut
283.20	
283.40	6.50 ✓
	5.92
278.20	6.80
276.30	6.61
276.30	5.83 ✓
274.20	6.46
272.10	6.38 ✓
272.10	6.69
271.52	5.53 ✓
271.42	5.96 ✓
	5.75
271.32	4.84

H.P. Sutliff

66 W. F St.

Chula Vista 11892J

Top of 4" Valve, see p. 10

321.98
5.05
327.03
250.6
301.97
321.98
5.69
327.67
46.58
311.09

X Red Rock off 822+702 on N. of grade

Helen Sutliff & Charles

823+12.5 see p. 10

321.98
6.04
328.02
46.58
281.44

12

B/S	B.S	H.I	FS	Red	Elev
		281.42 ✓			
BC 824+2 ⁵² φ				4.84	276.60
φ				4.92	276.52
B.W			4.41		<u>277.03</u> ✓
823+12 ⁵ 0				3.17	278.27 ✓
φ				3.13	278.31
B.W	4.46	281.49			<u>277.03</u> ✓
824+19 ⁷ 0				5.62	275.87 ✓
φ				5.89	275.60
825+15 ⁵² 0				5.93	275.56 ✓
φ				5.92	275.55
825+42.09 φ				4.92	276.57 ✓
φ				5.65	275.84
B.C. 825+68 ⁴² 0				4.50	276.99 ✓
φ				4.25	277.24
826+0 0				4.05	277.44 ✓
φ				4.07	277.40
B.W	369	280.72			<u>277.03</u>
	7.20	284.23 ✓			
824+50-φ				8.10	276.13
+62				7.65	276.58
+89				8.35	275.85 ✓
825+15				8.62	275.55 ✓
+4 ✓				7.67	276.56 ✓

Trench Grade Cut

271.79 ✓	5.31 ✓
271.60 ✓	6.67 ✓
271.24 ✓	4.63 ✓
271.19 ✓	4.37 ✓
271.14 ✓	5.43 ✓
271.08 ✓	5.91 ✓
	6.16
271.02 ✓	6.42 ✓

Top of Body Flange 4" Gab
Valer opp 826+

Note 840+50 φ 6.9
+40 6.9
841+0 φ 6.4

For check only

13

Sta	BS	HI	FS	Rod	Ele
		284.23			
825+68-φ				7.24	276.99
826+00-φ				6.81	277.42
+50 φ				7.31	276.92
φ				7.92	276.31
+60 φ					275.77
φ					275.12
29 May					
B.M.	4.42	281.45			277.03
827+0 φ				10.33	271.12
φ				11.05	270.40
T.P.	0.26	269.39	12.32		269.13
827+50 φ				6.95	262.44
φ				7.99	261.40
T.P.	1.55	258.66	12.28		257.11
828+00 φ				5.66	253.00
" φ				6.78	251.88
T.P.	0.56	247.09	12.13		246.53
828+50 φ				4.17	242.92
φ				4.20	242.89
T.P.	0.24	234.36	12.97		234.12
829+00 φ				3.55	230.81
φ				2.55	231.81
829+35 φ				10.94	223.42
φ				9.85	224.51
829+50 φ	1.42	223.50	12.29		222.08
φ	2.0			12.15	222.21

Transect	Grade	Cut	
			277.03
			8.45
			285.48
			61.98
			223.50
270.92	6.00		
	5.39		
270.92	4.87		
Holes, Suttiff.			
263.62	7.50		
	6.78		
		B.M. 8' φ	827+00
			269.39
254.51	7.93		
	6.89		
245.10	7.68		
	6.48		
235.40	7.52		
228.52	7.29		
215.20	8.22		
	9.31		
214.49	7.59		

Sta	B.S	I.I	F.S	Rod	Elev
14					
8		223.50			
830+00-φ				4.64	218.86
φ				5.11	218.39
830+50 φ				7.06	216.44
φ				7.28	216.22
831+00 φ				7.42	216.08
φ				7.44	216.06
B.M				8.27	215.23
831+15 φ				6.85	216.65
φ				6.90	216.60
<hr/>					
B.M	898	224.21			215.23
831+50 φ				6.05	219.16
φ				6.75	217.46
832+0 φ				6.12	218.09
φ				6.26	217.95
832+50 φ				5.50	218.71
φ				5.89	218.32
833+0 φ				5.30	218.91
φ				5.56	218.65
833+50 φ				3.67	220.54
φ				3.39	220.82
834+00 φ				0.00	224.21
				0.18	224.03
B.M	6.63	230.13	0.71		223.50

Trunk
Grade

Cut

211.14 7.72

209.79 6.65

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

209.48 6.60

Top of 1/2" Iron Strap on 36" Wood Stake
Pipe app 831+00, Res Rag

check Level Adjustant
minor error only,
Corrected Same

see above

215.23

15.61

230.84

0.71

230.13

0.63 offset

834+00

15 29 May A

Stn	B.S.	H.I.	I.S.	Pod	Elev
		230.13 ✓			
834+00 ♀				5.92	224.21
834+50 ♀				2.94	227.19
♀				3.19	226.94
TP	6.44	233.63	2.94		227.19
835+00 ♀				1.92	231.71
♀				2.16	231.47
BM			2.13		231.50 ✓
31 May					
	13.00	244.50			231.50
835+50 ♀				5.44	239.06
♀				5.71	238.79
835+75 ♀				1.18	243.32
♀				0.86	243.64
TP	12.22	255.54	1.18		243.32
835+90 ♀				8.21	247.33
836+00 ♀				5.36	250.18
♀				5.34	250.20
TP	13.03	268.16	0.41		255.13
TP	12.47	277.86 ✓	2.77		265.39
836+50 ♀				8.56	269.30
♀				8.43	269.43
836+70 ♀				0.96	276.90
♀				1.26	276.60
	5.072		4.36		

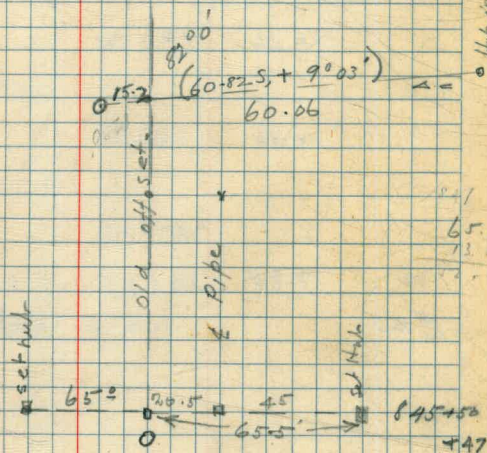
Trench	Grade	Cut
		or
	221.40	5.79
	224.40	7.31
		Old Nub 83540
		May 31-1942. Wilcox
		Hale
		Reid
		Banks
		Douglas Jacks.
BM	232.90	6.16
	238.40	4.92
		231.50
		50.72
		28.22
		4.36
		277.86
	243.90	6.28
	261.90	7.46
	269.10	7.80

Sta	BS	HI	I.S.	Rod	Elev
		277.86 ✓			
TR	12.70	289.42	0.64		277.22
836+75				10.94	278.50
" ϕ only				10.88	278.54
837+00 ϕ				3.87	285.65
" ϕ				3.47	285.95
TR	12.20	300.86	0.76		289.66
837+20 ϕ only				10.88	289.98
837+50 ϕ				6.94	293.94
" ϕ				6.33	294.53
838+0 ϕ				2.48	298.43
" ϕ				1.78	299.08
TR	12.90	313.53	0.23		300.63
838+50 ϕ				9.90	303.63
" ϕ				8.86	304.67
839+00 ϕ				2.24	311.29
" ϕ				2.10	311.43
TR	10.04	323.30	0.27		313.26
839+50 ϕ				7.50	315.82
" ϕ				7.09	316.21
839+75 ϕ				5.48	317.82
BM 728	9.32	322.67 ✓	3.95	(3.95)	319.35
840+00 ϕ				3.55	319.14
" ϕ				3.38	319.29

50.66

Fwd to page 18
835Trench
G/T

Trench G/T	G/T
270.90	7.60
270.90	
279.90	5.71
282.51	
286.44	7.50
292.98	5.45
299.52	4.11
306.06	5.23
312.60	3.22
313.38	5.76

65.5
20.5
45.0Note, 839+0 old 1" hole cut
+50 - 2.1277.86
50.66
328.52
5.85
322.67BM Top of Brey Flange to 4" Gate
on A.V. Sta 840+04

Note Checks of B.M. only

	Check	Levels			
	+	H.I	-	EL-	231.50
835+00					231.50
	12.97	244.47			
T.P.			0.56	243.91	
	13.00	256.91			
T.P.			1.91	255.00	
	12.66	267.66			
T.P.			0.12	267.54	
	12.70	280.24			
T.P.			0.88	279.36	
	12.66	292.02			
T.P.			1.45	290.57	
	12.30	302.87			
			0.32	302.55	
	12.77	315.32			
TP	9.38	321.10	3.60	311.72	
B.M.			1.73	<u>319.37</u>	

Note Check of level taken on p. 16

18

21-May 1942

Sta	Food from P/B		Rod	Elev
Sta	B.S	I.I	F.S	
		322.67		
840+40 (D)			2.82	319.85
±			2.23	320.44
840+50 (D)			2.71	319.96
±			2.22	320.45
841+00 (D)			5.39	317.28
±			4.65	318.02
BMJ	1.13	320.50		319.37
841+00 (D)			2.57	317.93
±			2.72	
841+50 (D)			5.60	314.90
" ±			5.63	314.77
842+00 (D)			7.08	313.42
±			6.92	313.58
842+50			7.34	313.16
±			7.32	313.18
843+00 (D)			6.63	313.87
±			6.62	313.88
843+50 (D)			5.74	314.76
±			5.93	314.57
844+00 (D)			5.36	315.14
" ±			5.41	315.09

Trench Grade	wt	
314.00	5.85	
313.66	6.30	
	6.79	
311.97	5.31	
		5 June 42
		see p. 16
311.97	5.96	Keeler Road Bunks Jacks
310.28	4.62	
308.60	4.82	
308.54	4.62	
308.48	5.39	
308.42	6.34	
308.36	6.78	

20

Sta	B.S.	HI	F.S.	Rod	Elev.
		302. ⁴⁷ 30	11.39		
T.P.			11.39		290. ⁰⁸ 7
	145	292. ⁵³ 36			
847+40.99 (7)				3.38	289.15 289.98
±				3.40	289.13
847+57.97 (7)				4.55	287.98 287.81
±				4.29	288.24
847+73.75 (7)				5.15	287.38 287.21
±				4.80	287.73
847+90.18 (7)				5.50	287.03 286.86
±				5.36	287.17
B.M.			5.38		287.15 286.98

287.15

9.82

Keeler
June 42Trench
Cord. Cut

B.S. of Curve		
286.21	2.93 ✓ 2.77	
		302.47 <u>1.45</u>
		283.92
284.85	3.13 ✓ 2.96	16.77
		<u>287.15</u>
283.49	3.89 ✓ 3.72	
282.71	4.34 ✓ 4.15	

±
conc. Man. on N₂ Line Winona Ave

B.M. above

Grades on Chollas Pipe Line
Unit # 5

Stn	Change of Grading Point	To grade Elev.	Grade Elev.
800+67 ⁴⁰	334.00		334.00
		-20.90	
801+0			827.18
+04.1			826.32
801+20	323.0		323.00
+40.73			321.33
+50		-8.09%	320.57
+77.40			318.35
802+0			316.53
+111.07			315.39
+25	314.50		314.50
802+50		-4.80%	313.30
+50.73			313.27
803+0			310.90
+24.05			309.83
803+50	308.50		308.50
+60.74			307.99
804+0		-7.50	304.75
804+50	301.00		301.00
805+0		-12.22	294.87
805+40	290.00		290.00
805+50		-0.67	289.93
806+0	289.60		289.60
+50		+3.70	291.45
807+0			293.30
+50			296.15
808+0	297.00		297.00

Note Grades given are bottom of

Trench	Change Point	%	Trench Grade	
808+00	297.00		297.00	
+50			.05	-13.9
809+0			1.0	2
+50			1.5	27.8
810+0			1.9	
+50			2.4	824+50 271.52
811+0			2.9	
+50			3.3	824+50.98 - 271.29
812+0			3.8	+99.29 271.24
812+50			4.2	825+15.69 271.19
813+0			4.6	+97.09 271.14
813+25	297.50		297.50	+68.49 271.08
+50			298.66	826+0 271.02
814+0	301.00		301.00	
+50			304.56	
815+0	308.00		308.00	
+50			310.06	
816+0		4%	312.00	
+50			314.00	
817+0			313.91	
+50			313.81	
818+0		-1.66	313.77	
818+50			313.63	
+60	313.61		313.61	
819+0			308.43	
+50		12.95	301.96	
820+0			295.50	
+50	289.00		289.00	
821+0		-10%	284.00	283.40 ✓
+50	279.00		279.00	278.40 ✓
822+0			276.70	276.30 -
+50		4.20	274.80	274.20 -
823+0			272.70	272.10 ✓
+12.5	272.20		272.20	271.60 ✓
+50			272.12	271.52 ✓
824+0		-0.20%	272.02	271.42 ✓
+50			271.92	271.32 ✓
825+0			271.82	271.22 ✓
+50			271.72	271.12 ✓
826+0			271.62	271.02 ✓
+50			271.52	270.92 ✓
+60	271.50		271.50	270.90 ✓
827+0			264.22	263.62 ✓
+50		7.21	255.11	254.51 ✓
828+0	246.0		246.00	245.40 ✓

Trench grades for concrete pipe

For Reformed C/P

22 Unit No 5.

Stn	Change Point	% grade	Trench Grade	T. Grade	Revised
828+0	246.00		246.00	245.40	
828+50	236.00	-20.00%	236.00	235.40	
829+0		-23.7%	224.12	223.52	
+35	215.80		215.80	215.20	✓
+50		-4.7%	215.09	214.49	
830+0			211.74	211.14	
830+50	210.39		210.39	209.79	
831+0		-0.616	210.08	209.48	
831+15	210.00		210.00	209.40	✓
+50		+2.82%	210.99	210.39	
832+00	212.40		212.40	211.80	
+50		+0.6%	212.70	212.10	
833+00	213.00		213.00	212.40	
+50		+6.00%	216.00	215.40	
834+0			219.00	218.40	32.90 15
+50			222.00	221.40	
835+0	225.00		225.00	224.40	32.90 43.90
835+50	233.50	+17%	233.50	232.90	76.90 38.20
836+0	244.50	+22.0%	244.50	243.90	
+50		+36%	262.50	261.90	
+70			269.50	268.90	
837+0	280+50		280.50	279.90	
+70			282.50	281.90	
+50		+13.08%	287.04	286.44	
838+0			293.58	292.98	
+50			300.12	299.52	

Stn	Change Point	% grade	Trench Grade	Revised
838+50		+13.08%	300.12	299.52
839+0			306.66	306.06
839+50	313.20		313.20	312.60
840+0		+1.55%	313.98	313.38
+40	314.60		314.60	314.00
+50		-3.37%	314.26	313.66
841+0			312.57	311.97
+50			310.88	310.28
842+00	309.20		309.20	308.60
+50		-0.123	309.14	308.54
843+0			309.08	308.48
+50			309.02	308.42
844+0			308.96	308.36
+50			308.89	308.29
845+0			308.83	308.23
+25	308.60		308.60	308.00
+50		-3.30	307.98	307.38
846+00			306.38	305.78
+40	305.00		305.00	304.60
846+50		-24.67	302.53	301.93
847+00	290.20		290.20	289.60
+50		-8.27%	286.07	285.47
847+75	284.00		284.00	283.40

846+25,
304.90

24

GRADES FOR BLASTING

CHOLLAS PIPE LINE

STA 839+00 TO 841+00

STA	+	H.L.	-	ELEV.	TRENCH GRADE
TP #30				302.52	
	10.89	313.41			
839 (205)			3.6	309.8	OLD EL- 309.8
839~			1.3	312.1	306.46
TP			0.81	312.60	
	10.07	322.67			
839+50			3.9	318.8	313.20 OLD EL
840~ (225)			4.4	318.8	318.4
840~			2.9	319.8	313.98
+40			2.1	320.6	314.60
+50			2.1	320.6	314.26
841~			1.5	318.2	312.57

5-16-42
Veto-Clouds
CoolX SIDNEY R. HALL
H.C. D. ABATE
R.C. C. SZYMCAK

Cut

Top of 8' offset hub Sta 838+50

1X1 Pine hub marked with Blue Kiel

Elev taken from fib 626 page 39

C-54

=Note=

Cuts were increased 0.2' to

C-56

CHECK with BM #128, fib 626
page 39,

C-58

C-62

C-63

C-56

25

STAKING of COLLAS PIPE LINE

UNIT #5

805+49²⁰

804

803+60²⁴ E.R.O.803+24⁰⁸802+87⁴¹802+50²⁴802+14⁰² P.R.C.801+77⁴¹801+40²⁴801+04²⁷800+67¹⁰ BC Point of beginning

X 0°44' RT
 on old
 Line

13° 7° 7°

Set 1X2 Pine hub
 7° RT &

EP IXI hub 13°

Set 2X2 Pine hub
 7° AT &

A 7° 09'
 R=2025.41
 ST. 73.38
 L=146.70

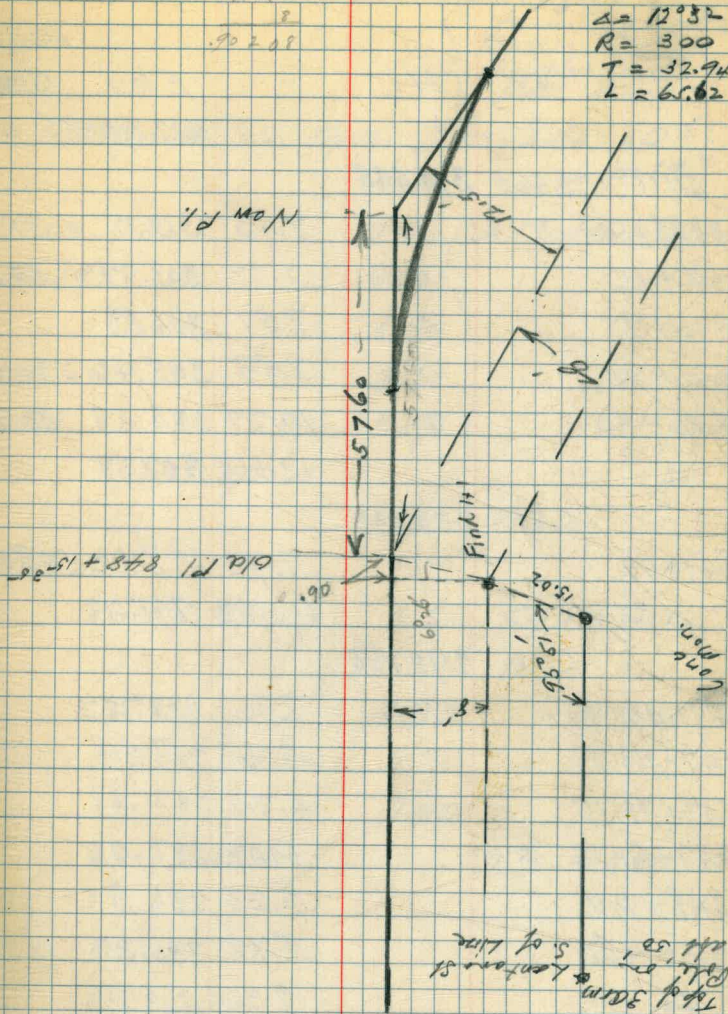
A 7° 09'
 R=2025.41
 ST. 73.38
 L=146.70

Found 2X2 RW
 Hub 8° 15' 7°
 of &

tan $6^{\circ}26' = .11276$

$\frac{8}{90} = .0888$

$\Delta = 12^{\circ}32'$
 $R = 300$
 $T = 32.94$
 $L = 65.62$



27

SURVEY & LEVELS
CHOLLAS PIPE LINE

	+	HI.	-	Elev	Revised Grade
				312.98	
BM	1.465	314.445			
845+50			2.45	312.0	307.38
846+00			5.53	308.92	305.73
846+25			7.57	306.88	
846+40			8.99	305.46	304.60
846+50			10.27	304.18	301.93
△			12.065	302.38	
	0.655	303.035			
847+00			7.92	295.12	289.6
BC △ 847+24.56			11.923	291.112	
	1.04	292.152			
847+40.99			2.96	288.782	
847+57.37			4.16	287.99	
847+73.75			4.74	287.41	
847+90.18 E.C.			5.09	287.06	
848+00			5.23	286.92	282.40
848+50			5.82	286.33	280.40
△			12.364	279.788	
	1.995	281.783			
849+00			3.24		273.40
△			12.29	269.493	
	1.986	271.479			

JUNE - 7th 1942.

M. S. Gierlich
Mami - Reid
Douglas Jack
Ross Banks

Cut.

On Flange 4" G.V. Opp. Sta. 845+50[±]
exp 19j

5.62	7.0 = Cut Marked on Witness
3.19	6.08
	4.90
0.86	3.34
2.25	5.92
5.52	7.49
	5.51
	4.93
	5.20
	7.40
	4.34

28

	+	HI	-	Elev
		271.479		
849+50			8.04	263.44 258.73
Δ			12.439	259.040
	0.963	260.003		
849+75			3.0	257.00
850+00			7.57	252.43
Δ 850+50			10.193	249.810 243.4 ✓
	3.493	253.303		
8 T'N			3.73	249.57
8+51+00 ⊙			4.42	248.88 ✓ 242.60
7'N			4.7	248.60
851+50 ⊙			4.67	248.73 241.80
7'N			5.3	248.00
851+93 7'N			4.3	249.00
852+00 ⊙			7.29	246.01 ✓ 241.00
7'N			6.9	246.40
852+15 7'N			7.2	246.10
852+25' ⊙			1.2	252.10 240.60
7'N			6.4	246.90
2.5' N			2.2	251.10
10' N			3.5	249.80
8+52+37				
BM-852+25 Δ			1.208	252.095
	11.53	263.625		

Check Levels on Conc. Monument

	+	HI	-	Elev
				291.112 = 297+24.56
0.385		291.497		
			4.33	287.167 } On- Conc. Monu.
848+50-			5.18	286.317

C/T

6.41 ✓

6.88 ✓

6.93

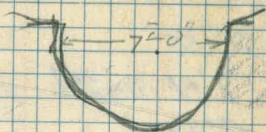
5.01

11.50

Edge of Bank

1/2 Creek Bottom

to Ditch



29

	+	H 1	-	Elev
852+50	⊙	263.625	4.95	258.67-
1.5 N			5.36	258.31
7' N	on stake in Ditch		10.8	252.82
10.3			7.5	256.12
Δ			0.41	263.215
		12.30		275.515
852+75			6.16	269.35-
Δ			0.25	275.265
		12.433		287.698
853+00			9.72	277.97
2.5 N			9.9	277.79
7' N	On Stake ⁱⁿ Ditch		13.4	274.29
11' N			9.3	278.39
Δ			0.83	286.868
		12.005		298.873
853+25			10.1	288.77
853+50	stake			
5' N			0.5	298.37
7' N	on stake in Ditch		2.05	296.82
9' N			0.3	298.57
12' N				
Δ	853+100		0.09	298.783
		12.54		311.323
853+75	Δ		1.315	310.008
		11.85		321.858

Trench	cut
Grade	
2+9.17	9.35

260.00	9.35
--------	------

270.80	7.17
--------	------

288.30	6.47
--------	------

293.80	4.98
--------	------

302.00	8.50
--------	------

	+	H.I.	-	Elev
854+00	①	321.858	5.23	316.62
3' N			5.2	316.65
7' N	2k in ditch		8.47	313.32
9' N			6.7	315.15
13' N			4.0	317.85
Δ			0.34	321.518
		11.645		333.163
854+25	①		10.50	322.56
854+50	②		5.25	327.91
1' N			5.2	327.96
7' N	2k in ditch		10.85	322.31
11' N			6.9	326.26
854+75			2.14	231.02
Δ			0.35	332.813
		10.346		343.159
8+55+08.91	Angle Pt.		8.36	334.80
2.5 N			8.8	334.36
7' N	2k		10.76	332.40
11' N			7.3	335.86
15.5 N			3.5	339.66
855+28.34			4.91	338.249
7' N			5.44	337.72
BM			4.165	338.994

Tf Grade	Cut
310.70	6.42
314.60	7.96
319.00	8.91
321.80	9.22

Keel ⊕ on sidewalk

On fig. 4" G.V.

31

9 June 1942

Checks Levels

Stn	B.S.	I.I.	F.S.	Rod	Elev
B.M.	0.21	313.19			312.98
TP	0.89	301.07	13.01		300.18
TP	1.86	290.44	12.49		288.58
847+73 75				303	287.41
B.M.				326	287.18
848+50 7				4.11	286.33
848+00 7				3.52	286.92
849+00 7	1.53	280.07	11.90	11.90	278.54
TP	0.60	268.83	11.84		268.23
849+50 7				5.45	263.38
TP	0.38	256.68	12.53		256.30
849+75	(5.47)		61.77		
850+00 7				4.31	252.37
850+50 7				6.94	249.74
" " 4				7.37	249.31
B.M.				7.18	50
851+00 7				7.86	248.82
" " 4				8.7	248.51
851+50 7				8.11	248.57
4				8.72	247.96
TP	5.63	253.64	8.67		248.01
B.M.				5.76	247.88
Creek on line				7.85	245.79
" ben				6.40	247.24

See page 19

v BK see p 27

Concrete B.M. @ Winona

290.40 5.93

292.40 4.52

273.40 5.14

258.73 4.65

251.40

245.40 6.97

243.40 6.34

242.60 6.22

241.80 6.77

Nail in N. Side Power Pole F.D.C. 64 E.G.
#3500, on N. Side
Auburn Ave, 100' S ofNail in Body flange of Gate Valve on
Blow-off

Bottom of Creek

20' from 4 up stream

Wilcox

Whites

Banks

Lakes

312.98

5.47

318.45

21.77

256.68

5.63

262.31

8.67

253.64

33

Stn	B.S	I.H	F.S	Rod	Elev
		330.50			
TP	12.62	342.89	0.23		330.27
854+75	⑦			12.02	330.87
855+00	⑦			7.77	335.12
+08.91	⑦			8.25	334.64
	⊕			10.64	332.25
B.W				4.07	338.82
855+28 ²⁴	⑦			4.82	338.07
	⊕			5.34	337.55

Trench
Grade

Grade	Cut	
		21.66
		- .09
		194.94
		21.66
		2834
		216
		17004
		1934
		56684
		6.12144
321.80	9.07	
324.60	10.52	
326.55	8.09	
326.55	5.70	
330.72	7.35	on
330.72	6.83	

Flange of most westerly 4' Gate Valve
on 2 Air Valves at 855+09

34

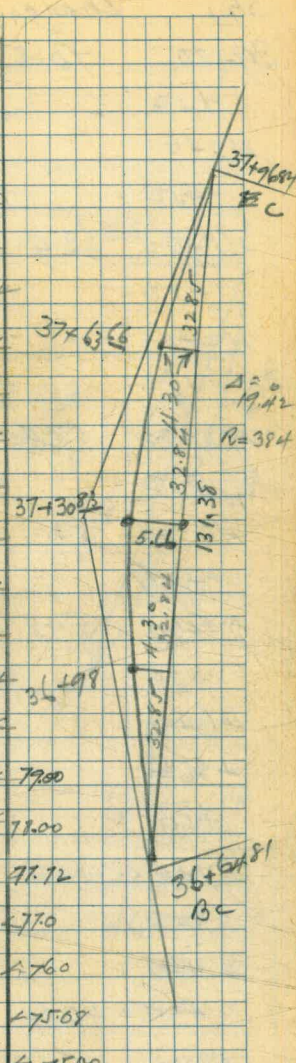
Unit No 6 Grades

Stn	Change of Grade	% Grade	Grade Elev
0+0	240.4		240.4
0+50		-7.87	236.47
0+75	234.5		234.50
1+0		-9.47	232.13
1+50	227.4		227.4
1+57		-18%	226.14
1+67			224.34
1+75	222.9		222.90
2+00	219.0		219.00
2+25	216.5		216.5
2+50		-7.33	214.67
3+00	211.0		211.0
+50		-9.75	206.13
4+0			201.25
+50			196.38
5+00	191.5		191.5
+50	185.5		185.50
5+75	183.5		183.50
6+00	180.6		180.60
6+25	176.2		176.2
6+50	171.0		171.0
7+00	158.5		158.5

Stn	Change Points	%	Elevation
7+00	155.0		155.00
7+38	152.5		152.5
7+57	151.2		151.2
8+0		-3.01	149.90
8+50	148.4		148.4
9+0		-3.80	146.50
9+50	144.6		144.60
10+0		-7.171	143.51
+50			142.42
11+0			141.34
+50			140.26
12+0			139.17
+50			138.09
13+00	137.00		137.00
+50		-2.0%	136.00
+65 BC			135.70
14+0	135.00		135.00
+50		-1.533	134.23
15+00		7.61	133.46
+50		3.90	132.70
16+00			131.93
538			131.17
17+00	130.4		130.4
17+50	1	-2.20	129.3
18+0	128.20		128.2

Station	Unit No.	Change	Grade	Elevation
18+0	1282			129.2
18+50		-7.70		124.6
18+75	122.8			122.80
19+0		-0.533%		122.67
+50				122.40
20+0				122.14
+50				121.87
21+00	121.6			121.6
+50		-6.66		118.27
21+75	116.6			116.6
22+0		-0.320		116.52
+50				116.36
23+00	116.2			116.2
+50		-2.90		114.50
24+00				113.40
24+50	112.00			112.00
25+00		-3.60		108.94
25+25				108.40
26+00	106.6			106.60
+50		-3.033		105.09
27+0				103.58
+50				102.06
28+0				100.55
+50				99.03
29+0	97.5			97.5

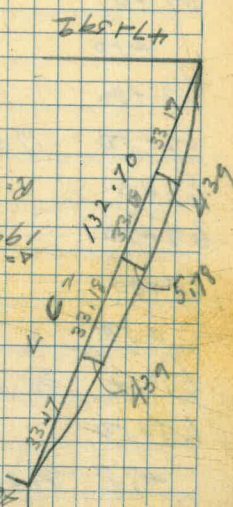
Stn	Change	Rate	Elev
29+00	97.5		97.50
+50		-4%	95.50
29+75	94.5		94.50
30+00		-1.333%	94.170
+50	93.5		93.50
31+0		-2.889	92.050
+50			90.610
32+0			89.160
+50			87.700
33+00			86.280
+50			84.830
34+00			83.390
+50			81.940
35+00	80.5		80.500
+50		-2.25	79.130
36+0			78.250
+50			77.130
36+42			77.08
37+00	76.00		76.00
+50		-1.50	75.250
37+68			74.55
38+00	74.5		74.50
+50		-3.70	72.65
39+00	70.8		70.8



36

Stn	Change	Rate	Elev
39+00	70.8		70.8 ✓
+50		-3.70	68.95 ✓
40+00			67.10 ✓
+50			65.25 ✓
41+00	63.4		63.40 ✓
+50		-2.30	62.25 ✓
42+00			61.10 ✓
+50			59.95 ✓
43+00	58.8		58.80 ✓
+50		-4.20	56.70 ✓
44+00	54.6		54.60 ✓
+50		-1.80	53.70 ✓
45+00	52.8		52.80 ✓
+50		-4.10	50.75 ✓
46+00			48.70 ✓
+26.50			47.61 (+59.2 46.24)
+50			46.65 (+93.2 44.82)
47+00	44.6		44.60
+50		-6.133	41.57 (47.52 43.00)
+60			40.93
+75	40.80		40.80 ✓
48+00		-2.00	39.50 ✓
+50			38.50 ✓
49+00			37.50 ✓
49+25	37.00		37.00 ✓

Stn	Change	Rate	Elev
49+25	37.00		37.00 ✓
+50		-4.12%	35.97 ✓
50+00			33.91 ✓
+50			31.85 ✓
51+00			29.75 ✓
+50			27.73 ✓
51+75	26.70		26.70
52+00		-0.93%	26.47
+50	26.00		26.00
53+00		-3.20	24.40
+50			22.80
54+00	21.20		21.20
54+50	18.20		18.20
55+00		-0.867	17.76
+50			17.33
56+00			16.90
+50			16.46
57+00			16.03
+50	15.60		15.60
58+00		-0.20	15.45
+50			15.30
59+00			15.15
59+50	15.00		15.00
60			



Stn	Change	Rate	Elev
59+00	15.00		15.00
60+0		+0.667	15.33
+50			15.67
61+0			16.00
+50			16.33
62+00			16.67
62+50	17.00		17.00
63+0		+1.20	17.60
63+50			18.20
64+00			18.60
+50			19.40
65.00	20.00		20.00
65+50		+1.333	20.66
+75	21.00		21.00
66+0		+0.267	21.07
+50			21.20
67+00			21.33
+50			21.47
68+0	21.60		21.60
+50		-0.60	21.30
69+0			21.00
+50			20.70
70+0			20.40
+50			20.10
71+0			19.80

Stn	Change	Rate	Elev
71+0		-0.6%	19.80
+50			19.50
72+0			19.20
+50			18.90
73+0	18.6	-1.257	18.60
+50			17.97
74+0			17.35
+50			16.72
74+75	16.4		16.40
75+0		+1.40	16.75
+50			17.45
76+0			18.15
+50			18.85
77+00			19.55
+50			20.25
78+00	20.95		20.95
+50		1.40	21.65
+75	22.00		22.00
78+92.5		-2.755	21.52
79+0			21.31
+50			19.93
80+00			18.56
+50			17.18
81+00	15.80		15.80
81+36	13.80		13.80

Sta	Change	Rate	Elev
81+36	13.80		13.80
+50		-1.25	13.62
82+00	13.00		13.00
+50		-2.025	11.99
83+00			10.98
+50			9.96
84+00	8.95		8.95
+50		-3.266	7.32
84+75	6.50		6.50
85+0		-1.304	6.17
+50			5.52
85+90	5.00		5.00
86+00		-2.00	4.80
+50			3.80
87+00			2.80
+50			1.80
88+0			0.80
+50			-0.2
89+0			-1.2
89+50	-2.2		-2.2
90+0			-2.83
90+50			-3.46
91+00	-4.08		-4.08
91+50	-4.70		-4.70
92+00			-4.62

	Rate	Elev
92+50		-4.54
93+00		-4.46
93+50		-4.38
94+00	-4.30	-4.30
94+50		-2.90
95+00	-1.50	-1.50
+50		-1.44
96+00		-1.38
96+50		-1.32
97+0		-1.26
97+50		-1.20
98+00		-1.13
98+50		-1.07
99+00		-1.01
99+50		-0.95
100+00		-0.89
100+50		-0.83
101+00		-0.77
101+50		-0.71
102+0		-0.65
102+50		-0.59
103+00		-0.52
103+30		-0.48

For grades beyond 103+30
see p 12

39

B.M. - Chger

Sta	+ F.S.	T	BS	Red	Elev
	183	2303			6120
T.P.			10.73		5230
	208	5438		5.90	48.47
⑥ 47130 ⁷⁰				9.64	44.74
T.P.			8.80		45.58

10 July - 1942

Check Levels

Cannot identify B.M. or T.P. as shown in FB # 600

I check on 7 different points on preliminary survey & find good accord & call set up from which these were determined as 49.03

see FB 600-78

H. 1

49.03

B.M.			2.11		46.92
B.M.			6.30		42.73

N.W. Cor of Canon & Willow sts

B.M. on W. side of Evergreen
City 49.51
1.03
48.48

Sta 7800 p 34 456.

419

Lead plug in center of E. side of steps to 1092 Evergreen

Top of Fire Hydrant S.W. Cor Addison & Evergreen

40

10 July 1942

Levels & Cuts on #6 Unit

Harbor Drive Pipe Line

Stn	BS	I.I	F.S	Rod	Elev
B.M.	3.00	45.73			<u>42.73</u>
51+50 (3)				13.09	32.64
⊥				13.00	32.73
51+00 (3)				11.65	34.08
⊥				11.54	34.19
50+50 (3)				9.60	36.13
⊥				9.53	36.20
50+00 (3)				7.57	38.16
⊥				7.47	38.26
49+50 (3)				5.67	40.06
⊥				5.62	40.11
49+25 (3)				4.89	40.84
⊥				4.80	40.93
49+00 (3)				4.27	41.46
⊥				4.20	41.53
48+50 (3)				3.59	42.15
⊥				3.44	42.29
48+00 (3)				2.45	43.28
⊥				2.29	43.44

Grade Cut

Top of Hydrant Addison & Evergreen

27.73 4.91

29.75 4.33

31.85 4.28

33.91 4.25

35.97 4.09

37.00 3.84

37.50 3.96

38.50 3.65

39.50 3.78

41

10 JULY 1942

Stn	B.S.	I.I.	F.S.	Rod	Elev
B.W.	9.02	55.94			<u>46.92</u>
	6.99	53.91			
47+70 = (5)				9.97	43.94
49				9.79	44.12
47+60 (3.5)				9.18	44.73
(3.4)				9.18	44.73
				9.05	44.86
47+264 (3)				7.16	46.75
				7.11	46.90
41+93 ¹⁰ (3)				5.79	48.12
				5.58	48.33
46+59 ¹⁰ (3)				4.85	49.06
				4.73	49.18
46+26 ⁵⁰ (3)				2.16	51.75
				2.36	51.55
TP	6.89	58.79	2.01		51.90
46+00 (3)				5.70	53.09
				5.49	53.30
45+50 (3)				3.36	55.43
				3.16	55.63
45+00 (3)				1.33	57.46
				1.17	57.62
TP.	8.86	66.28	1.37		57.42
44+50 (3)				7.18	59.10
				7.22	59.06
	2.2				
	22.74				
		3.38			

Grade

Cut

40.00 3.9

40.93 3.8

43.0 3.75

44.87 3.25

46.24 2.82

47.61 4.14

49.70 4.39

50.75 4.68

52.80 4.66

53.70 3.72

53.70 5.04

46.92

22.74

+8

69.66

3.38

66.28

42 10 July 1942

Stn B.S. H.I. F.S. Rod Elev

66.28 ✓

44+00 (3)				6.13	59.45
↓				5.80	60.49
B.M.				4.81	61.47
43+50 (3)				5.62	60.66
43+50 (3)				4.60	61.63
↓				4.56	61.72
43+00 (3)				3.27	63.01
↓				3.25	62.93
42+50 (3)				2.06	64.22
↓				1.98	64.30
42+00 (3)				0.81	65.47
↓				0.72	65.56
T.P.	10.45	76.54	0.19		66.09
41+00 (3)				8.49	68.05
↓				8.39	
40+50 (3)				6.64	69.90
↓				6.56	
40+00 (3)				4.68	71.86
↓				4.48	72.06
39+50 (3)				2.81	73.73
↓				2.52	
39+00 (3)				0.94	75.60
↓				0.76	

T.P. 9.98 85.66 ✓ 0.86 75.63 ✓

Grade Cut

54.60	4.85
56.70	4.98
58.80	4.21
59.95	4.27
61.10	4.37

Spk on Curb N.W. Wilcox & Canyon (City 61.20)

66.28
20.43
86.71
11.05
95.66

This T.P. ok, used on next page.

Continued from page 42 -

43

Sta	B.S.	I	F.S.	Red	Elev
			85.66 ✓		
38+50				8.07	77.59
℄				7.95	77.71
38+00				6.05	79.61
℄				6.03	
TP	0.63	76.31	9.98		75.68
41+50				9.63	66.53
℄				9.56	66.75
41+00				8.25	68.06
℄				8.16	68.15
40+50				6.40	69.91
℄				6.33	69.98
40+00				4.45	71.26
℄				4.23	72.09
39+50				2.57	73.74
℄				2.29	74.02
39+00				0.60	75.71
℄				0.51	75.80
T.P.	10.06	85.74	0.63		75.68
38+50				8.16	77.58
℄				8.03	77.71
38+00				6.13	79.61
℄				6.10	79.6
B.M.			2.19		83.55 ✓

10.69

282

July 10 - 1942

Whites

Reid, Jacks, Keeler

Grade Cut

NOTE Stations marked out in red not to be used Reason: Station skipped

62.25	4.08	
63.40	4.66	75.68
		10.69
		86.37
		12.82
		83.55 ✓
65.25	4.66	
67.10	4.76	
68.95	4.79	
70.80	4.91	
72.65	4.93	
74.50	5.11	
B.M. Fire Plug on	S.W. Corner of Ollman & Canon	

44

Sta	B.S.	I.	F.S.	Prod	Elev
B.M.	5.30		88.85		83.55 ✓
37+63 ⁸⁰				9.13	79.72
⊕				8.19	80.66
37+30 ⁸³				8.60	80.25
⊕				7.82	81.03
36+97 ⁸²				7.89	80.96
⊕				7.68	81.17
36+64 ⁸¹				7.17	81.68
⊕				7.26	81.59
36+50 ⁸⁰				6.89	81.96
⊕				6.94	81.91
36+00				5.86	82.99
⊕				5.88	82.97
35+50 ⁸⁰				4.68	84.17
⊕				4.72	84.13
35+00 ⁸⁰				3.35	85.50
⊕				3.44	85.41
34+50 ⁸⁰				2.00	86.85
⊕				2.06	86.79
34+00				0.52	88.33
⊕				0.62	88.23
T.P.	12.87	101.10 ✓	0.62		88.23
33+50 ⁸⁰				11.40	89.70
⊕				11.46	89.64
33+00 ⁸⁰				9.95	91.15
⊕				10.02	91.08

July-11-1952 Whites

Grade	Cut
41.8	4.31
75.25	5.00
76.06	4.90
77.08	4.60
77.13	4.83
78.25	4.74
79.13	5.04
80.50	5.00
81.94	4.91
83.39	4.94
84.83	4.87
86.28	4.80

Fire Plug S.W. Cor of Hazzard & Conroy
 36+64⁸¹ L.P.
 36+97⁸²
 37+30⁸³
 37+63⁸⁴
 E.C.
 $R = 69.25'$
 $AP = 390'$
 $T = 67.72'$
 Sub. Ch. 33.51'
 Sta def 82-27-45'

88.85
16.17
101.72
0.62
101.10

45

July-11-1942 - Whites

Sta	B.S.	I.	F.S.	Red	Flev
		101.10 ✓			
32+50 ^③				8.61	92.19
⊕				8.70	92.40
32+00 ^③				7.17	93.93
⊕				7.22	93.88
31+50 ^③				5.79	95.31
⊕				5.80	95.30
31+00 ^③				4.35	96.75
⊕				4.38	96.72
30+50 ^③				2.93	98.17
⊕				2.94	98.26
30+00 ^③				1.52	99.58 ✓
⊕				1.62	99.48
29+50 ^③				0.08	101.02
⊕			0.22	0.22	100.88 ✓
F.P.			0.22		
B.M.	2.18	85.73			83.55
37+96 ^②				5.98	99.75
⊕				6.12	
37+63 ⁷⁴	this sta-taken as		Check	6.00	99.73
			only	5.09	

Grate cut

HI 49 same as page #49		
87.70	4.79	101.10
89.16		83.55
89.14	4.77	218
		85.73
90.61	4.70	101.10
		22
92.05	4.70	100.88
93.50	4.67	
94.17	5.41	
95.50	5.52	
F.P. not made Reason found that Rodman had slipped station 37+96 so back to B.M. & a new HI for this reason stgs are not in order		
94.55	5.20	

July-12-1942 - Whites

46

Sta	B.S.	I	F.S.	Red	Elev
	10.49	111.37			100.88 ✓
29+75 ^③				11.06	100.31
⊕				11.15	100.19
29+00 ^③				8.97	102.46
⊕				9.05	102.32
28+50 ^③				7.63	103.74
⊕				7.68	103.69
28+00 ^③				6.20	105.17
⊕				6.28	105.09
27+50 ^③				4.71	106.66
⊕				4.81	106.56
27+00 ^③				3.29	108.08
⊕				3.31	108.06
26+50 ^③				1.76	109.61 OK
⊕				1.75 ←	
T.P.	13.05	122.67	1.75		109.62
26+00 ^③				11.38	111.29 = 09
⊕				11.28	111.39
25+50				9.63	113.04
⊕				9.47	113.20
F.C. 25+35 ^③				9.09	113.60
⊕			8.89	8.89	113.78
T.P.	12.72	126.50 ✓			113.78
25+00 ^③				11.70	114.80
⊕				11.40	115.10

36.26

1064

Grade cut

Sta.	Grade	Cut	Note
29.50	94.50	5.81	note 29+50 on preceding page
29.50	97.50	4.90	
29.50	99.03	4.71	
29.50	100.55	4.62	
29.50	102.06	4.60	
29.50	103.58	4.50	
29.50	105.09	4.52	
29.50	106.60	4.69	
29.50	108.10	4.64	
29.50	108.94	4.66	
29.50	110.20	4.60	

100.88

36.26

137.14

10.64

126.50

Sta	B.S.	I	F.S.	Prod	Elev
24+75 ^③		126.50-		10.87	115.63
☒				10.59	115.91
24+50 ^③				10.10	116.90
☒				9.84	116.66
24+25 ^③				9.40	117.10
☒				9.11	117.39
24+00				8.76	117.74
☒				8.45	118.05
23+75 ^③				8.06	118.44
☒				7.73	118.77
23+50 ^③				7.32	119.18
☒				6.99	119.57
23+25				6.68	119.82
☒				6.32	120.18
23+00				5.95	120.55
☒				5.59	120.91
22+75				5.25	121.25
☒				4.92	121.58
22+50				4.56	121.94
☒				4.18	122.32
22+25				3.89	122.61
☒				3.51	122.99
22+00				3.25	123.25
☒				2.92	123.58
21+75				2.62	123.88
☒				2.27	124.23

Grade	Cut
111.10	4.53
112.00	4.40
112.70	4.4
113.40	4.3
114.1	4.3
114.80	4.4
115.5	4.3
116.20	4.3
116.28	5.0
116.36	5.98
116.44	6.17
116.52	6.73
116.60	7.28

Sta	B.S.	I	F.S.	ROOF	Elev
21+50		126.50 ✓		1.91	124.59
⊕				1.58	124.92
21+25				1.17	125.33
⊕			0.89	0.89	125.61
T.P.	11.78	137.39 ✓	0.89		125.61
21+00 ⁽³⁾				11.46	125.93
⊕				11.15	126.24
20+75				10.89	126.50
⊕				10.52	126.87
20+50				10.22	127.17
⊕				9.83	127.53
20+25				9.58	127.81
⊕				9.17	128.22
20+00				8.98	128.51
⊕				8.62	128.77
19+75				8.43	128.96
⊕				8.09	129.13
19+50				7.92	129.47
⊕				7.55	129.84
19+25				7.35	130.09
⊕				6.98	130.41
19+00				6.88	130.51
⊕				6.51	130.89
18+75				6.44	130.95
⊕				6.06	131.33

Grade	Cut	
118.27	6.32	
		126.50
		11.78
120.00	5.33	
		137.28
		87
		137.39
121.60	4.33	
121.74	4.76	
121.87	5.3	
121.0	6.80	
122.14	6.37	
122.27	6.21	
122.40	7.0	
122.53	7.51	
122.67	7.84	
122.85	8.15	

Sta	B.S.	I	F.S.	Prof	Elev
18+50		137.39 ✓		5.94	131.45
☺				5.58	131.81
18+25				5.48	131.91
☺				5.09	132.30
18+00				4.98	132.41
☺				4.57	132.82
17+75				4.43	132.96
☺				4.07	133.32
17+50				3.89	133.50
☺				3.54	133.85
17+25				3.36	134.03
☺				2.99	134.40
17+00				2.82	134.57
☺				2.45	134.94
16+75				2.32	135.07
☺				1.98	135.41
16+50				1.80	135.59
☺			1.46	1.46	135.93
T.P	11.38	147.31 ✓			135.93
16+25				11.20	136.11
☺				10.84	136.57
16+00				10.62	136.69
☺				10.21	137.10
15+75				10.12	137.19
☺				9.74	137.57

Grade Cut

124.60	6.85		
		137.39	
		11.38	
		148.77	
		1.46	
		147.31	
126.4	5.5		
128.2	4.2		
128.75	4.2		
129.20	4.2		
129.55	4.18		
130.40	4.17		
130.78	4.29		
131.17	4.42		
131.55	4.56		
131.93	4.76		
132.11	5.08		

Sta	B.S.	I	F.S	Rod	Elev
15+50		147.31 ✓		9.64	137.69
⊕				9.27	138.04
15+25				9.12	138.19
⊕				8.77	138.54
15+00				8.63	138.68
⊕				8.21	139.10
14+75				8.10	139.21
⊕				7.70	139.61
14+50				7.64	139.67
⊕				7.28	140.03
14+25				7.25	140.06
⊕				6.90	140.41
14+00				6.81	140.50
⊕				6.52	140.79
B.C. 13+65				6.38	140.93
⊕				6.17	141.14
13+50				6.16	141.15
⊕				6.01	141.30
13+00				5.55	141.76
⊕				5.44	141.77
12+50				4.74	142.57
⊕				4.74	
12+00				3.64	143.67
⊕				3.70	143.61
11+50				2.62	144.69
⊕				2.64	144.67

Grade	Cut
132.70	4.97
133.08	5.11
133.47	5.21
133.85	5.36
134.23	5.44
134.61	5.45
135.00	5.5
135.70	5.23
136.00	5.1
137.0	4.76
138.09	4.48
139.17	4.50
140.26	4.43

Sta	B.S.	I	F.S.	ROD	ELEV
11+00		147.31 ✓		1.59	145.72
☺			1.61	1.61	145.70
T.P.	12.86	158.56			145.70
10+50				11.76	146.80
☺				11.76	146.80
10+00				10.63	147.93
☺				10.63	147.93
9+50				9.23	149.33
☺				9.28	149.28
9+00				7.55	151.01
☺				7.55	151.01
8+50				5.73	152.83
☺				5.77	152.79
8+00				3.58	154.98
☺				3.58	154.98
7+57				1.57	156.99
☺			1.55	1.55	157.01

Grade	Cut
141.34	4.38
	147.31
	17.86
	160.17
142.42	4.38
143.51	4.42
144.60	4.73
146.50	4.5
148.40	4.4
149.90	5.08

Temp B.M. Red Head nail - rather yellow head
To check within
.5"

52 15 July 1942

Checks Levels

B	B.S.	H.I.	F.S.	Red	Elev
B.M.	7.98	50.71			42.73
B.M.	3.80	50.72			46.92
		50.715			
TP	12.720	62.955	0.480		50.235
B.M.	10.780	72.210	1.525		61.430
TP	11.650	83.030	0.830		71.380
39+00③				7.375	75.655
+				7.4	
38+00③				3.48	79.55
B.M.					
TP	6.890	89.530	0.390		82.640
B.M.				6.010	83.520
37+63 ⁸⁹ ③				9.820	79.710
+30 ³⁰ ③				9.295	80.25
36+97 ⁸⁹ ③				8.560	80.91
36+64 ⁸⁹ ③				7.89	81.64
36+50③				7.58	81.95
36+0③				6.57	82.99
35+50③				5.37	84.16
35+00③				4.24	85.49
34+50③				2.69	86.84
34+00				1.22	88.31
T.P.			0.805		88.725
			21		
42.040			40.30		

Use 2 B.M.s as check on H.I.

top of Hydrant at Evergreen & Addison } sep 29
 Iron Plug at 1692 Evergreen }

Brass Plug, Willon & Canyon (61.47) p. 42 6.20 City

10.8 4.9

75.00 4.55

Top of Hydrant, Ullman & Canyon

top of Hydrant, Ullman & Canyon
 83.55 sep 43

75.75 3.96

76.40 3.95

77.07 3.95

77.72 3.92

78.0 3.95

79.0 4.00

50.715

42.640

72.755

4.030

78.725

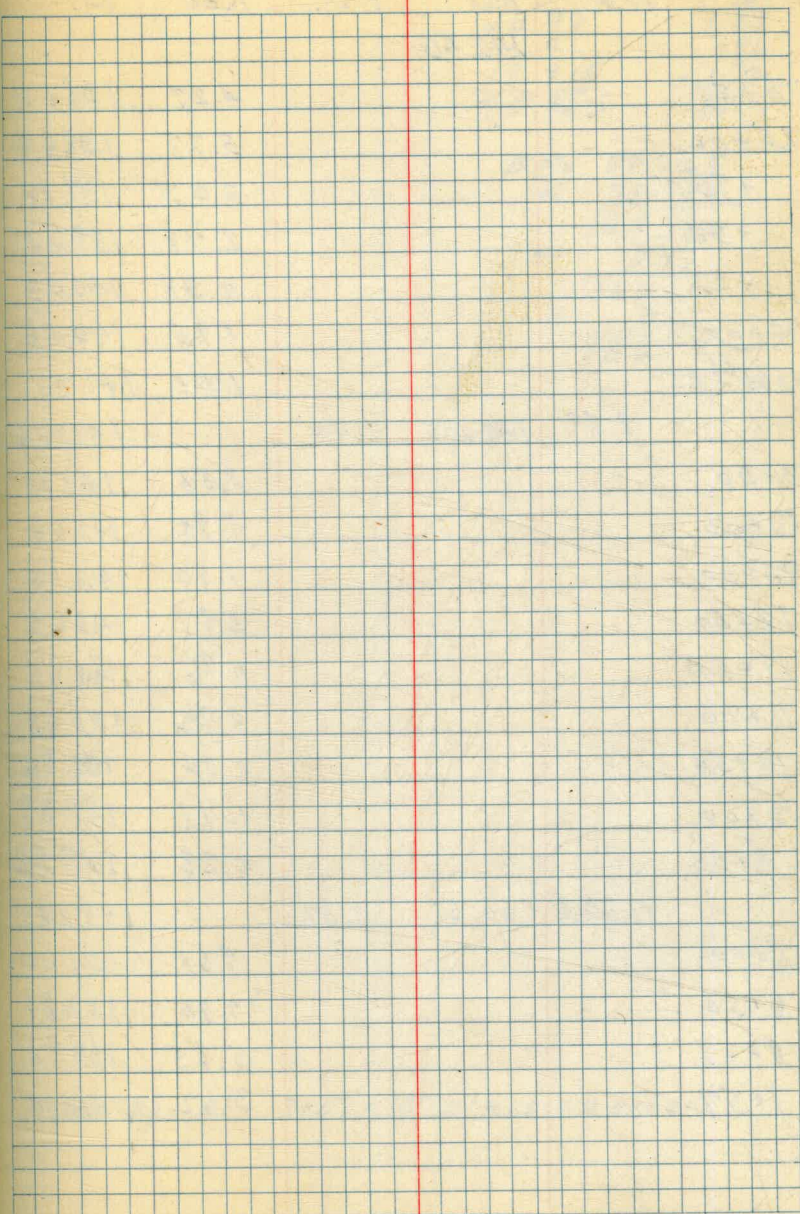
Turn for Page 53

53 Check Levels July 15 - 42 Keeler

Sta	B.S.	HI	F.S.	Rod	Elv.
	9.94	98.665			88.725
	10.81	108.975	0.500		98.165
	12.45	120.915	0.510		108.465
26+00				9.65	111.26
25+50				7.93	112.98
25+35 ¹⁸ EC.				7.37	113.54
25+00				6.17	114.74
24+75				5.34	115.57
+50				4.56	116.35
+25				3.87	117.04
24+00				3.20	117.71
23+75				2.51	118.40
+50				1.76	119.15
+25				1.10	119.81
23+00				0.38	120.53
	11.78	132.315	0.38		120.535
22+75				11.10	121.21
+50				10.41	121.90
+25				9.75	122.56
22+00				9.09	123.22
21+75				8.44	123.87
+50				7.76	124.53
+25				7.06	125.25
21+00				6.42	125.89
	44.98		139		

See turn bottom Page 52

Sta	B.S. +	H.I	F.S. -	Rod	Elv.
		132.315			
20+75			5.85		126.46
+50			5.19		127.12
+25			4.52		127.79
20+00			3.93		128.38
+75			3.37		128.94
+50			2.85		129.46
+25			2.30		130.01
19+00			1.83		130.48
+75			1.37		130.94
+50			0.87		131.44
	10.96	142.415	0.86		131.455
18+25			10.52		131.89
18+00			10.02		132.39
+75			9.48		132.93
+50			8.94		133.47
+25			8.41		134.00
17+00			7.88		134.53
+75			7.38		135.03
+50			6.87		135.54
+25			6.35		136.06
16+00			5.80		136.61
+75			5.29		137.12
+50			4.76		137.65
	10.96		0.86		



Sta	B.S.	H.I.	F.S.	Red	Elv.
		142.415			
15+25				4.27	138.14
15+00				3.77	138.64
+75				3.23	139.18
+50				2.78	139.63
+25				2.38	140.03
14+00				1.95	140.46
13+65 ⁶⁶ B.C.				1.51	141.01
	8.59	149.605	1.40		141.015
13+50				8.48	141.12
13+00				7.92	141.68
12+50				7.50	142.10
12+00				5.97	143.63
11+50				4.96	144.64
11+00				3.92	145.68
10+50				2.84	146.76
10+00				1.71	147.89
9+50				0.28	149.32
	11.325	160.61	0.32		149.285
9+00				9.61	151.00
8+50				7.80	152.81
8+00				5.65	154.96
7+57				3.62	156.99
	19.915		1.72		

B.S.	F.S.
44.98	1.39
10.96	1.86
19.915	1.72
<u>75.855</u>	<u>3.97</u>

BM = 88.725
+ 75.855
164.580
- 3.97
160.61
- 3.62
156.99 ✓

Sec Page 51 = 7+57 = 157.01 = 0.02 error

56 Cuts on Evergreen

Sta	B.S.	H.I.	F.S.	Rod	Elv.
	0.26	42.99			42.73
52+00 ^③				11.33	31.66
6'				11.26	31.73
	1.52	32.77	11.74		31.25v
52+50 ^③				2.83	29.94
6'				2.68	30.09
53+00 ^③				4.49	28.28
6'				4.35	28.42
53+50 ^③				6.09	26.68
6'				5.96	26.81
54+00 ^③				7.68	25.09
6'				7.57	25.20
54+50 ^③				7.92	24.85
6'				7.89	24.88
54+50 original				7.97	24.80
55+00 ^③				8.74	24.03
6'				8.58	24.19
55+50 ^③				9.70	23.07
6'				9.72	23.05
56+00 ^③				11.13	21.64
6'				11.10	21.67
56+50 ^③				12.17	20.60
6'				12.18	20.59
	5.24	25.83	12.18		20.59v

Harbor Drv. Pipe Line Unit # 6.

Keeler
July 16-42

Grade	Cut	BM top Hydrant, Addison & Evergreen
26.47	5.19	✓
26.00	3.94	✓
24.40	3.88	✓
22.80	3.88	✓
21.20	3.89	✓
18.20	6.65	✓
17.76	6.27	✓
17.33	5.74	✓
16.90	4.74	✓
16.46	4.14	✓

23 above City

57

Sta BS. HI FS. Rod Elev.

Sta	BS.	HI	FS.	Rod	Elev.
		25.83			
57+00 ⁽³⁾			5.73		20.10
			5.52		20.31
57+50 ⁽³⁾			5.90		19.93
			5.58		20.25
58+00 ⁽³⁾			5.83		20.00
			5.63		20.20
58+50 ⁽³⁾			6.03		19.80
			5.88		19.95
59+00 ⁽³⁾			5.82		20.01
			5.78		20.05
59+50 ⁽³⁾			5.66		20.17
			5.22		20.61
60+00 ⁽³⁾			5.40		20.43
			5.30		20.53
60+50 ⁽³⁾			4.65		21.18
			4.70		21.13
61+00 ⁽³⁾			2.88		22.95
			2.92		22.91
61+50 ⁽³⁾			1.84		23.99
			1.81		24.02
	8.87	33.92	1.78		24.05
62+00 ⁽³⁾			9.00		23.92
			8.93		23.99
62+50 original			8.93		23.99

Grade Cut

16.03	4.07 ✓
15.60 ✓	4.33 ✓
15.45	4.55 ✓
15.30	4.50 ✓
15.15	4.86 ✓
15.00	5.17 ✓
15.33	4.90 5.18 ✓
15.57	5.61 ✓
16.00	6.95 ✓
16.33	7.66 ✓
16.67	7.25 ✓

24.01

Sta	B.S.	HI	F.S.	Rod	Elev.
		32.92			
62+50 ^③				8.88	24.03
				8.83	24.09
63+00 ^③				7.60	25.32
				7.50	25.42
63+50 ^③				5.29	27.63
				5.47	27.45
64+00 ^③				5.09	27.83
				4.92	28.00
64+50 ^③				5.05	27.87
				5.10	27.82
original 65+00				5.99	26.93
65+00 ^③				5.90	27.02
				5.80	27.12
65+50 ^③				6.04	26.88
				5.97	26.95
66+00 ^③				6.52	26.40
				6.36	26.56
66+50 ^③				7.00	25.92
				6.83	26.09
67+00 ^③				7.40	25.52
				7.18	25.74
B.M.				4.59	28.33
	6.10	31.70	7.32		25.60 ✓

Grade | Cut.

17.00	7.03 ✓
17.60	7.72 ✓
18.20	9.43 ✓
18.80	9.03 ✓
19.40	8.47 ✓
20.00	7.02 ✓
20.66	6.22 ✓
21.07	5.47 5.33
21.20	4.72 ✓
21.33	4.19 ✓

B.M. Top Fire Hyd. S.E. Cor
Evergreen & Garrison.

59

Sta	B.S.	H.I.	F.S.	Rod	Elv
		31.70			
67+50				6.44	25.26
				6.23	25.47
68+00				6.20	25.50
				6.10	25.60
68+50				5.15	26.55
				5.04	26.66
69+00				4.92	26.78
				4.84	26.86
69+50				4.92	26.78
				4.78	26.92
70+00				5.22	26.48
				5.07	26.63
70+50				7.03	24.67
				6.93	24.77
71+00				7.16	24.54
				7.06	24.64
71+50				5.51	26.19
				5.30	26.40
72+00				5.37	26.33
				5.38	26.32
	3.10	29.42	5.38		26.32
72+50				4.74	24.68
				4.65	24.77

Grade Cut

21.47	3.79 ✓
21.60	3.90 ✓
21.30	4.75 5.25 ✓
21.00	5.78 ✓
20.70	6.08 ✓
20.40	6.08 ✓
20.10	4.57 ✓
19.80	4.74 ✓
19.50	6.69 ✓
19.20	7.13 ✓
18.90	5.78 ✓

Sta	B.S.	H.I.	FS	Rod	Elv
		29.42			
73+00 ⁽³⁾				5.09	24.33
6'				5.05	24.37
73+50 ⁽³⁾				5.95	23.47
6'				5.83	23.59
74+00 ⁽³⁾				7.70	21.72
6'				7.65	21.77
74+50 ⁽³⁾				9.36	20.06
6'				9.20	20.22
75+00 ⁽³⁾				9.55	19.87
6'				9.30	20.12
75 original				9.28	20.14
75+50 ⁽³⁾				8.40	21.02
6'				8.20	21.22
B.M.	10.55	32.85	7.12		22.30
76+00 ⁽³⁾				10.45	22.40
6'				10.33	22.52
76+50 ⁽³⁾				8.76	24.09
6'				8.70	24.15
77+00 ⁽³⁾				7.49	25.36
6'				7.25	25.60
77+50 ⁽³⁾				6.23	26.62
6'				6.02	26.83

Grade Cut

18.60	5.73 ✓
17.97	5.50 ✓
17.35	4.37 ✓
16.72	3.34 ✓
16.75	3.12 ✓
17.43	3.57 ✓
18.15	4.25 ✓
18.85	5.24 ✓
19.55	5.81 ✓
20.25	6.37 ✓

B.M. Pole # 429974 H
 Nail in Tel Pole S.E. Cor
 Evergreen & Koots

Sta	B.S.	HI	FS	Rod	Elv.
		32.85			
78+00 ⁽³⁾				6.00	26.85
6'				5.70	27.15
78+50 ⁽³⁾				5.61	27.24
4'				5.86	26.99
78+86.50 ⁽³⁾				6.43	26.42
4'				6.35	26.50
B.M.				7.42	25.43
Check Levels		32.85			
	7.93	30.23	10.55		22.30
	5.38	31.69	3.92		26.31 ✓
	7.16	32.75	6.10		25.59 ✓
	8.7			4.44	28.31
	1.91	25.84	8.72		24.03
	13.00	33.57	5.27	5.27	20.57
	12.20	43.43	2.34	2.34	31.23
			0.71	0.71	42.73

Grade	Cut	B.S.	F.S.
		35.64	45.52
			7.42
			52.94
20.95	5.90 ✓		BM = 42.73
			+ 35.64
			78.37
21.65	3.59		- 52.94
			25.43 OK
21.52	4.90		

Plug in Curb S.E. Cor.
Evergreen & Lowel. 25.296

B.M. Hyd.

Five Hyd Addison & Evergreen = Error 0.01

62 Cuts on Lowell St.

Keeler
July 17-42

Sta	B.S.	H.I.	F.S.	Rod.	Elv.
	1.53	26.96			25.43
79+50 ⁽³⁾				2.30	24.66
±				2.38	24.58
80+00 ⁽³⁾				3.80	23.16
±				3.85	23.11
+50 ⁽³⁾				5.33	21.63
±				5.35	21.61
81+00 ⁽³⁾				6.81	20.15
±				6.83	20.13
+50 ⁽³⁾				8.18	18.78
±				8.27	18.69
82+00 ⁽³⁾				9.35	17.61
±				9.49	17.47
+50 ⁽³⁾				10.19	16.77
±				10.46	16.50
	2.15	18.92	10.19		16.77
83+00 ⁽³⁾				3.65	15.27
±				3.73	15.19
+50 ⁽³⁾				4.70	14.22
±				4.92	14.00
84+00 ⁽³⁾				5.92	13.00
±				5.96	12.96
+50 ⁽³⁾				7.07	11.85
±				7.10	11.82

3.68

10.19

Grade Cut

Grade	Cut	Flag in cut b S.F. Car Evergreen & Lowell-
19.93	4.73 4.73	✓
18.56	4.60	✓
17.18	4.45	✓
15.80	4.35	✓
13.62	5.16	✓
13.00	4.61	✓
11.99	4.78	✓
10.98	4.29	✓
9.96	4.26	✓
8.95	4.05	✓
7.32	3.53	✓

Sta.	B.S.	HI	F.S.	Rod	Elv
		18.92			
85+00 ⁽³⁾			--	8.21	10.71
⊕				8.27	10.65
+50 ⁽³⁾				9.55	9.37
⊕				9.49	9.43
B.M.	7.65	17.14	9.43		9.49 ✓
BM24A			6.73	6.73	10.41 ✓

Check Levels

10.43	19.92			9.49
10.19	26.96	3.15		16.77
		1.51		25.45

Grade Cut

B.S.	F.S.	
11.33	26.35	
		25.43 = BM
		+ 11.33
		36.76
		- 26.35
		10.41 ✓

Piece of Storm Drain
Reinforcing Steel in W end
of Curb Ref. S.W. Cor Lowell &
Rosecrans Sts
Old elev. 9.50

B.M. at S.E. Cor. Evergreen & Lowell.

64 Cuts on Lowell St.

Sta	B.S.	HI	F.S.	Rod	Elv.
	4.15	13.64			9.49
87+00 (3)				5.32	8.32
±				5.32	8.32
+50 (3)				6.53	7.11
±				6.68	6.96
88+00 (3)				7.75	5.89
±				7.85	5.79
+50 (3)				9.04	4.60
±				9.23	4.41
89+00 (3)				10.42	3.22
±				10.50	3.14
+50 (3)				11.63	2.01
±				11.78	1.86
	3.45	6.55	10.54		3.10
90+00 (3)				5.03	1.52
±				5.03	1.52

Check Levels

		6.55			
	7.71	13.69	0.57		5.98
			4.19		9.50
	5.09	14.58			9.49
86+00 (3)				5.58	9.00
+50 (3)				5.21	9.37

Keeler
July 17-42

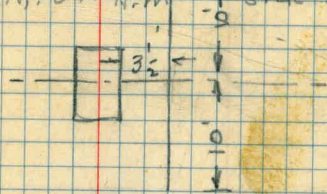
Grade	Cut	BS	FS
See BM described on Page 63		7.60	10.54
2.80	5.52 ✓		9.49 + 7.60 17.09 - 10.54 6.55
1.80	5.31 ✓		
0.80	5.09 ✓		
-0.2	4.80 ✓		
-1.2	4.42 ✓		
-2.2	4.21 ✓		
			S.D.G & E Pole # 2911 3/4 Curb Lowell Opp Sta. 89+40 B.M. Nail in Pole
			Check see Top of Page
4.80	4.20		
3.80	5.67		

Sta	B.S.	I	F.S.	Rod	Elev
	2.52	27.81			25.296
Locust & Lowell		sts	12.74		15.07
T.P.	0.72	15.97	12.56		15.25
			7.99		7.99
	0.41	8.40			
T.P.	5.17	5.01	8.56		-0.16
T.P.	7.62	9.33	3.30		1.71
T.P.	5.02	9.11	5.24		4.09
			5.03		4.08 B.M.
	5.03	9.11			4.08 B.M.
T.P.	5.36	9.66	4.81		4.30
T.P.	4.97	4.52	9.91		-0.25
T.P.	6.87	10.59	0.80		3.72
			2.59		8.00 B.M.
	6.33	10.41			4.08
Post 38					
T.P. #1	4.68	9.32	5.77		4.64
T.P. #2	4.26	8.05	5.53		3.99
115700			4.41		3.64 B.M.
			4.28		3.77 B.M.
	4.08		5.77		
	6.33		5.53		
	1.68		4.29		
	4.26		15.58		
	+19.35				
	-15.58				
	+2.77				

City data shows plug on S.W. Corner at 7th
 but we found did find plug on S.E. Corner as
 marked by Col. Wilcox on 7-23-42

note this plug has been destroyed but there
 is hole where plug has been
 all of these plugs are on
 S.E. Corners instead of S.W.
 Whiles
 This point is just 1' from
 end of curb return
 Rosellans & Lowell
 B.M. 8.063
 B.M. 7.99 = 7.99

Est on concrete Base on first post of new Highway
 north of old fence B.M. on N.W. side of post



Measure on B.M. at East Return of Curb Elev 7.99

	- 12.74	+ 25.29
	12.56	2.52
	7.98	0.72
	8.56	0.41
	3.30	8.17
Est on S.E. Curb Return 15' Radius	5.24	7.62
cut + in Top of Curb	5.03	5.02
Est on Curb Return 72 E. Corner	42.67	+46.75
in narrow streets		-42.67
		+4.08
	-48.7	+4.08
	9.91	5.03
	0.80	5.36
	2.59	4.77
	-18.11	6.87
		+26.11
		-18.11
		+8.00

66

Sta	B.S.	I	F.S.	Prod	Elev
	4.6	8.53			3.77 = B.M.
	5.85	8.98	5.00		3.13
			8.24		0.74 = B.M.
	8.26	9.00			0.74
	4.72	8.47	5.25		3.75
	5.32	8.97	4.92		3.65
	5.21	10.02	4.16		4.91
			5.93		4.09 = B.M.

Whites 7-27-1942

Est. on Curve Return NE Cor. of first st north
after entering reservation

2x2 - Set with Basket near Bay
77 20' south of sta 124+20

Est on #1 - Post north of old fence
this is closure on circuit

4.08
6.53
4.68
4.24
4.76
6.55
+29.96
+29.22
+0.74

5.77
5.53
~~5.40~~
4.25
5.40
8.24
-29.22

0.74
8.26
4.92
5.32
5.21
+29.25
-20.16
9.09

5.25
4.82
4.16
5.93
-20.16

Sta	B.S.	I	F.S.	rod	Elev	Grade	cut
	0.57	8.56			B.M. 7.99		
	7.21	6.89	8.88	8.88	-0.32		
92+00				7.421	-0.53	-4.62	4.09
92+50				7.19	-0.30	-4.54	4.24
93+00				7.12	-0.23	-4.46	4.23
93+50				7.00	-0.21	-4.38	4.17
94+00				6.15	+0.74	-4.30	5.04 ✓
94+50				4.99	1.90	-2.90	4.90
95+00				3.23	3.66	-1.50	5.16
	5.35	9.01	3.23		3.66		
95+50				3.91	5.10	-1.44	6.54
96+00				3.56	5.41	-2.38	6.79
96+50				4.04	4.97	-1.32	6.29
97+00				4.47	4.54	-1.26	5.80
97+50				5.30	3.71	-1.20	4.91
98+00				5.00	4.01	-1.13	5.14
98+50				4.24	4.77	-1.07	5.84
99+00				4.18	4.83	-1.01	5.84
99+50				4.80	4.21	-0.95	5.16
100+00				5.02	3.99	-0.89	4.88
	4.76	8.95	5.02		3.99		
100+50				4.30	4.65	-0.83	5.48
101+00				4.48	4.47	-0.77	5.24
101+50				5.04	3.91	-0.71	4.62

cup 60

7.99

18.09

26.08

8.25

17.83

8.88

8.95

1809

4.25

Sta	B.S.	I	F.S.	Red	Black
		8.95 ✓			
102+00				5.15	3.80
102+50				4.70	4.25
103+00				4.45	4.50
103+30				4.48	4.47
			4.77		4.18 ✓

Following is profiles and where in material change is apparent no reading taken on it

	6.27	10.36		B.M. 4.00
103+50 (6)			6.02	4.34
103+54 (30)			6.15	3.91
" (4)			5.95	4.41
104+02 (30)			5.56	4.80
" (4)			5.76	4.60
104+59 (6)			5.15	5.21
" (4)			5.21	5.15
105+04 (30)			5.12	5.24
" (4)			5.17	5.19
105+50 (6)			4.96	5.40
" (6)			4.89	5.17
106+00 (2)			5.28	5.08
" (6)			5.20	5.16
106+50 (4)			5.12	5.24
" (6)			5.10	5.26
107+00 (4)			4.58	5.78
" (6)			4.54	5.82

Grade Cut

5.65	4.45
0.59	4.84
0.52	5.02
0.48	4.95
should be 4.09	

$$\begin{array}{r} 104.04 \\ - 34.50 \\ \hline 69.54 \end{array}$$

				5.47
0.46	4.80			
				6.24
				5.23
				10.17
0.50	5.20			H.I. 10.45
				- 5.26
				5.29
				5.29
0.28	5.52	Sta 105+25	cut	5.54
				5.34
				- 5.00
1.43	6.90	106+25	cut	10.34
				5.56
				- 5.08
3.80	8.96	106+75	cut	10.55
				5.70
				5.55
5.00	10.26			
3.78	9.60			

70

Sta	B.S.	I	F.S.	Rod	Elev
113+32 ³⁹ R		9.48		5.76	3.72
(2)				5.82	3.66
113+50 R				5.96	3.52
(6)				4.94	4.54
T.P.	3.80	8.34	4.94		4.54
114+00 R				5.00	3.34
(6)				5.21	3.13
114+50 R				5.23	3.11
(6)				5.28	3.06
115+00 R				5.32	3.02
(2)				5.02	3.32
115+50 R				4.64	3.70
(6)				4.90	3.44
116+00 R				4.68	3.66
(6)				4.80	3.54
116+50 R				4.90	3.44
(6)				4.91	3.434
117+00 R				4.75	3.59
(6)				4.87	3.47 <
117+50 R				4.88	3.46
(6)				4.74	3.60 <
118+00 R				4.53	3.81
(6)				4.50	3.84 <
118+50 R				4.53	3.81
(6)				4.37	3.97

Grade	Cut
- 1.40	5.94
- 1.00	4.13
- 1.06	4.12
- 1.12	4.44
- 1.15	4.62
- 1.24	4.78
- 1.62	5.05
- 2.00	5.47
- 1.40	5.00
0.80	4.64
- 0.80	4.64
0.60	4.57

838

4.59

3.79

948

3.80

13.28

4.94

934

397

464

861

384

476

860

H I = 8.60

- 4.76

3.84

118+25 grade

- 0.50

Cut 4.34

Cut

72

From p 38-B

Stn	Grade Change	Rate	Elev.
103+30	-0.48		-0.48
+50			-0.46
104+0			-0.40
+50			-0.34
105+00			-0.28
105+25	-0.25		-0.25
+50			-1.43
106+00			-3.80
106+25	-5.00		-5.00
106+50			-5.00
106+75	-5.00		-5.00
107+0			-3.78
+50			-1.36
107+75	-0.15		-0.15
108+00			-0.19
+50			-0.28
109+00			-0.37
109+50			-0.45
110+00			-0.54
110+50			-0.63
111+00			-0.71
111+50	-0.80		-0.80
112+00			-1.29
+50			-1.76
112+75	-2.00		-2.00

	Change	Elev
112+75	-2.00	-2.00
113+0		-1.80
113+50		-1.40
114+00	-1.00	-1.00
114+50		-1.06
115+00		-1.12
115+50		-1.18
116+00	-1.24	-1.24
116+50		-1.62
117+00	-2.00	-2.00
117+50		-1.40
118+0		-0.80
118+25	-0.5	-0.50
118+50		-0.60
119+0		-0.81
119+50		-1.02
120+0		-1.23
120+50		-1.44
121+0		-1.65
121+50		-1.86
122+00		-2.07
122+50		-2.28
123+00	-2.5	-2.50

End to p. 76

73

8-1-1942 Whiles

Sta	B.S.	I	F.S.	Rad	Elev
	6.30	7.04			0.74
	5.91				1.13
	4.66				2.38
			2.23		4.81
			2.45		4.59
			2.53		4.51
			3.08		3.96
	7.00	7.74			0.74
#1	South side		6.59		1.15
#2	Curb south side		5.33		2.41
Bell Buoy			2.82		4.92
#1			3.03		4.71
#2			3.09		4.65
#3	Set up on East side		3.67		4.07
	6.30	7.04			0.74
			2.23		4.81
			2.45		4.59
			2.53		4.51
			3.08		3.96
					B.M. 4.86

= N.W. corner of n.w. corner pier of Bell Buoy

6.04	6.04
5.91	4.62
0.23	1.38

4.81
4.92
1.093
4.81

4.59
4.71
9.30
2.65

4.65
4.51
9.16
4.58

3.96
4.07
8.03
4.01

74

8-1-1942

Sta	B.S.	T	F.S.	Rod	Elev
1	3.39	8.25			4.86 B.M.
129+ ²⁰ 65				4.22	4.03
(6)				4.18	4.07
130+00				6.02	2.23
(6)				6.10	2.15
130+50				5.64	2.61
(6)				5.73	2.52
131+00				5.89	2.36
(6)				5.95	2.30
131+50				5.80	2.45
(6)				5.79	2.46
132+00				5.32	2.93
(6)				5.24	3.01
132+50				4.80	3.45
(6)				5.80	2.45
133+00				6.10	2.15
(6)				5.96	2.29
	3.66	5.95	5.96		2.29
133+50				4.12	1.93
(6)				4.32	1.63
134+00				4.76	1.19
(6)				4.97	0.98
134+50				4.85	1.10
(6)				4.96	0.97
135+00				5.10	0.85
(6)				5.22	0.73

Grade	Cut
08 of Page #73	4.86
	3.39
	3.66
	11.71
	5.96
	5.95
-4.00	
	6.30
-3.96	
	6.42
-3.92	
	6.93
-3.88	
	6.33
-3.84	
	6.13
-3.81	
	5.44
-3.77	
	4.75
-3.73	
	4.70
-3.69	
	4.42

FWD from P 72

Grades East of Channel

	rate	Elev
131+00	-4.00	-4.00 ✓
+50	-3.96	-3.96 ✓
132+00	-3.92	-3.92 ✓
+50	-3.88	-3.88 ✓
133+00	-3.84	-3.84 ✓
133+50	-3.81	-3.81 ✓
134+00	-3.77	-3.77 ✓
134+50	-3.73	-3.73 ✓
135+00	-3.69	-3.69 ✓
135+50	-3.65	-3.65 ✓
136+00	-3.61	-3.61 ✓
136+50	-3.57	-3.57 ✓
137+00	-3.54	-3.54 ✓
137+50	-3.50	-3.50 ✓
138+00		-4.25 ✓
138+50	-5.00	-5.00 ✓
139+00		-4.25 ✓
139+50	-3.50	-3.50 ✓
140+00		-3.54 ✓
140+50		-3.58 ✓
141+00		-3.62 ✓
141+50		-3.67 ✓
142+00		-3.71 ✓

		Elev
142+50		-3.75 ✓
143+00		-3.79 ✓
143+50		-3.83 ✓
144+00		-3.87 ✓
144+50		-3.91 ✓
145+00		-3.96 ✓
145+50	-4.00	-4.00 ✓
146+00		-4.50 ✓
146+50	-5.00	-5.00 ✓
147+00		-4.25 ✓
147+50	-4.00	-3.50 ✓
148+00		-3.44 ✓
148+50		-3.38 ✓
149+00		-3.33 ✓
149+50		-3.27 ✓
150+00		-3.22 ✓
150+50		-3.16 ✓
151+00		-3.11 ✓
151+50		-3.05 ✓
152+00		-3.00 ✓
152+50		-2.94 ✓
153+00		-2.89 ✓
153+50		-2.83 ✓
154+00		-2.78 ✓
154+50		-2.72 ✓

Add to page 80

Aug-4-1942 Whites

Sta	B.S.	I	F.S.	Rod	Key
	446	9.32			B.M. 4.81
① T.P.#1 154+00	5.16	6.13	8.35		0.97
② T.P.#2 157+00	5.10	6.18	5.05		1.08
③ T.P.#3 194+00	5.57	6.58	5.11		1.07
T.P.#4 ④ 149+00	4.84	7.26	4.16		2.92
151+91.53		7.25	5.78 ←		B.M. 1.98
T.P.#5 ⑤ 154+00	4.81	6.86	5.21		2.05
158+00.71		6.86	6.19 ←		B.M. 0.67
		6.86	5.10 ←		1.76
T.P.#6 ⑥ 159+00	5.23	7.81	4.28		2.58
T.P.#7 164+00	4.72	6.82	5.71		2.10
T.P.#8 ⑦ 169+00	5.22	7.22	4.82		2.00
T.P.#9 ⑧ 174+00	4.84	8.26	3.80		3.42
176+50		8.26	6.16 ←		B.M. 2.10
T.P.#10 ⑨ 179+00	5.22	8.84	4.64		3.62
T.P.#11 ⑩ 184+00	4.34	9.39	3.79		5.05
		9.39	7.36 ←		B.M. 2.03
T.P.#12 ⑪ 185+00	5.65	9.65	5.39		4.00
T.P.#13 ⑫ 180+00	4.01	8.56	5.10		4.85
T.P.#14 ⑬ 175+00	4.32	7.96	4.92		3.64
T.P.#15 ⑭ 170+00	4.67	6.89	5.74		2.22
T.P.#16 ⑮ 165+00	5.88	7.80	4.97		1.92
T.P.#17 ⑯ 160+00	2.61	6.22	4.19		3.61
		6.22	5.63 ←		0.57
T.P.#18 ⑰ 155+00	5.05	7.67	3.60		2.62
	96.50		6.22 ←		1.45
			34.83		

19 of page # 73 = S.W. Cor Pier of Bell Buoy

$$\begin{array}{r}
 +96.50 \\
 -28.83 \\
 \hline
 7.67
 \end{array}$$

Established on AXA Hwy 10000 offset, west side Hwy Sta 420+50.80

on point
Established on AXA Hwy 10000 offset, west side Hwy Sta 419+64.70

☐ of Hwy Sta 414+64.70 AXA-R.W. on ☐ point

Established on ☐ point of AXA Hwy Sta 396+15.81 ☐ of Hwy

this = end of series of levels.
Established on ☐ point of AXA ☐ of Hwy Sta 383+51.58

check on B.M. Hwy Sta 414+64.70

check on B.M. sta 420+50.80

Aug-4-1942

Sta	B.S.	I	F.S.	Rod	Elev
	6.11	7.56			1.45
T.P.#19					
① 137+00	5.23	6.36	6.43		1.13
T.P.#20					
② 138+00	5.30	6.15	5.51		0.85
		6.15	5.02		1.13
T.P.#21					
③ 137+00	5.41	6.39	5.17		0.98
132+00	5.50	8.52	3.37		3.02
			3.64		4.88
			29.12		
	+29.06				
	-29.12				
	4.88				

Sta	B.S.	I	F.S.	Rod	Elev
		5.78			
140+50				4.88	0.90
①				4.90	0.88
141+00				4.90	0.88
②				4.91	0.87
141+50				4.70	1.08
③				4.65	1.13
142+00				4.86	0.92
④				5.00	0.78
TP	5.08	5.86	5.00		0.78
142+50				5.02	0.78
⑤				5.16	0.91
143+00				4.95	0.91
⑥				5.14	0.72

Grade Cut

taken from B.M. at Elev as checked on return

check on sta 139+00 should have been 1.08

closure on B.M. Elev 486 on S.W. cur. Pier of Bell Bury

358	446
362	459
367	480
371	449
375	446
379	451

79

	B.S.	T	F.S.	Rod	
143+50		5.86		4.58	1.28
↳				4.61	1.25
144+00				4.65	1.21
↳				4.80	1.66
144+50				4.60	1.26
↳				4.69	1.17
145+00				4.47	1.37
↳				4.50	1.36
145+50				4.23	1.63
↳				4.26	1.60
146+00				4.66	1.20
↳				5.31	0.55
146+50				4.62	1.24
↳				5.26	0.60
147+00				4.76	1.10
↳				4.66	1.20

August - 5 - 1942

Sta	BS	T	F.S.	Rod	Elev
	5.60	6.80			1.20
147+50				5.13	1.67
↳				5.10	1.70
148+00				5.11	1.67
↳				5.10	1.70
148+50				4.53	2.27
↳				4.51	2.29

Grade out

for continued profile levels
see Book # V.W.A #2
Page # 57

-383	
	5.08
-387	
	4.93
-391	
	5.08
-394	
	5.22
-400	
	5.60
-450	
	5.05
-500	
	5.60
-1.25	
	5.45
-350	
	5.20
-344	
	5.14
-338	
	5.67

1.20
5.60
6.80

80 Grades #6, from 768

Sta	Change	Rate	Elev
154+50			-2.72 ✓
155+00			-2.66 ✓
155+50			-2.61 ✓
156+00			-2.55 ✓
156+50			-2.50 ✓
157+00			-3.00 ✓
157+50			-3.50 ✓
158+00			
158+50			

DIRECTIONS FOR USE OF TABLES

TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance

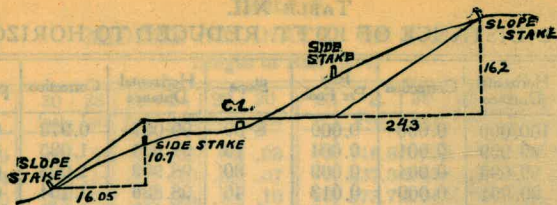
IMPROVED TABLES
AND
INFORMATION

TABLE No. 2

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connection.

Degree of curve with a given L may be found by dividing tangent (or external) opposite L by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent both divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 60	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

H
0
1
2
3
4
5
6
7
8
9
0
1
2
3
4
5
6
7
8
9



Charlie Scymczak
4477 Landis

Sta + $\overline{\wedge}$ - E 1

Please Return to
City of San Diego Water Dept.
Room 268 Civic Center
Telephone Main 5161

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

100.00
90.19
9.8

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

Copyright, 1914, by Eugene Dietzgen Co.