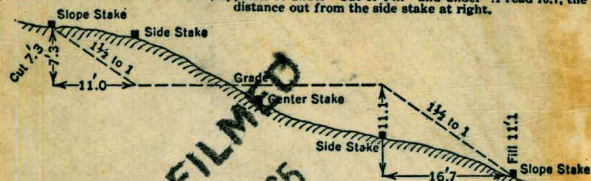


W

551

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 Roadway of any Width. Side Slopes 1 1/2 to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	Distance out from Side or Shoulder Stake										Cut or Fill
	0	.1	.3	.5	.6	.7	.8	.9			
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

KEUFFEL & ESSER CO., N. Y.

11,083-5. k, m, yc. kM.

The paper in this book No. 370A

is made of 50% high grade rag stock

with a WATER RESISTING surface sizing.

65

INDEX

Final X-section	Sta 8+13-8+47 Blk # 11	1-11
" X "	Sta 8+24-8+07 " # 9	12-13
" " "	" # 6	14-15
" " "	Void sections " # 11	16-17
" " "	Sta 8+53 Blk # 11	18-20
Final X-sections	Sta 5+75-6+01 " # 6	21-28
" X "	Sta 8+47-8+17 Blk # 11	29-30
" X "	5+76-6+11 " # 6	31-33
Highway Tunnel	X-section Outlet	34-36
" " "	" " Inlet	37-38
Final X-section	Sta 8+17-8+53 ⁵ Blk # 11	39-43
" " "	Sta 8+56-8+85 " # 12	44-51
X-section	Tunnel Outlet & Inlet	52
Final X-section	Blk # 17 11+10-11+50	53-55
" " "	Sta 8+63-	56

FINAL X-SECTION BIT #11

April 28 - 1942

Rogers

1

1.14 46298

461.84

3.70 454.75 1193

451.05

Sta 8+13

31N	38	451.0
20N	3.8	451.0
10N	3.1	451.7
0	4.6	450.2
4.5	4.3	450.5
5.5	2.7	452.1
10.5	1.6	453.2
20.5	2.6	452.2
30.5	3.9	450.9
40.5	4.4	450.4
50.5	6.0	448.8
60.5	8.0	446.8
20.5	2.7	447.1

✓

FINAL X-SECTION Bit #11

April 28-1947

2

454.75

8+13

80 S 9.1 445.7

8+17

20 N 16 453.2

10 N 1.8 453.0

0 1.4 453.4

10 S 2.6 452.2

16 S 4.0 450.8

20 S 4.7 450.1

30 S 4.9 449.9

40 S 3.5 451.3

50 S 4.7 450.1

60 S 7.9 446.9

70 S 9.5 445.3

80 S 8.8 446.1

90 S 9.6 445.2

✓

FINAL X-SECTION Bk # 11

April 28-1947

3

454.75

8417

1005 98 445.0 ✓

1105 94 445.4 ✓

1205 106 444.2 ✓

1285 103 444.5 ✓

1305 9.0 445.8 ✓

1405 7.6 447.2 ✓

1505 8.6 446.2 ✓

1605 4.9 449.9 ✓

1705 9.5 445.3 ✓

1785 9.0 445.8 ✓

8427

105 09 453.9 ✓

205 20 452.8 ✓

305 22 452.7 ✓

375 30 451.8 ✓

448³
155.79

D.S. toe of dam.



FINAL X-SECTION Blk # 11

April 28-1942

Rogers

4

459.25

8+27

385	45	450.3
405	42	450.6
445	36	451.2
465	25	452.3
505	44	450.4
575	66	448.2
605	65	448.3
685	25	447.3
705	6.1	448.7
745	7.3	447.5
805	8.6	446.2
905	8.5	446.3
1005	7.4	447.4
1105	6.6	448.2
1205	8.3	446.5

✓

FINAL X-SECTION Blk # 11

April 28, 1942

5

454.75

8+27

1265 8.5 446.3

1305 6.5 448.3

1405 4.2 450.6

1505 5.9 448.9

1605 7.2 447.6

1625 6.8 448.0

8+30

305 2.7 452.1

325 5.0 449.8

405 4.9 449.9

465 3.8 451.0

505 6.2 448.6

8+37

305 3.1 451.7

405 2.4 452.4

448.1
155.94

D.S. toe of dam.

✓

FINAL X-SECTION BIC #11

April

6

451.25

8437

445	29	452.4
505	51	449.7
555	45	450.3
605	28	452.0
655	17	453.1
675	45	450.3
705	54	449.4
755	62	448.6
805	44	450.4
865	53	449.5
905	36	451.2
1005	35	451.3
1015	56	449.2
1065	38	451.0
1175	36	451.2

✓

FINAL X SECTION 31k # 11

April 28-1942

Rogers

7

454.25

8+37

113.5		3.9	450.9
120.5		1.8	453.0
122.5		2.4	452.4
123.5		5.5	449.3
126.5		5.1	449.7
130.5		3.6	451.2
140.5		4.3	450.5
145.5		6.8	448.0
149.5		7.3	447.5
150.5		6.1	448.7
158.5		3.7	451.1
TP	8.43	459.69	3.49
		8+27	451.26
85		4.1	455.6
0		3.1	456.6

450.0
154.50 D.S. toe of dam.

✓

FINAL X-SECTION Blk # 11

April 28-1942

Rogers 8

459.69

8+27

9N 39 455.8

10N 57 454.0

8+37

26S 42 455.5

22S 44 455.3

20S 57 454.0

12S 40 455.7

10S 47 455.0

1S 45 455.2

0 3.0 456.7

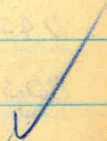
8+47

20S 28 456.9

22S 42 455.5

30S 42 455.5

32S 66 453.1



FINAL X-SECTION Blk # 11

April 28-1942

Rogers

9

459.69

8+47

405

7.5

452.2

8+44

405

8.2

451.5

425

9.5

450.2

505

8.9

450.8

605

6.7

453.0

705

10.5

449.2

8+47

505

5.3

454.7

555

3.7

456.0

605

4.1

455.6

675

4.5

455.2

705

5.8

453.9

745

6.9

452.8

805

5.4

454.3



FINAL X-SECTION Blk # 11

April 28 - 1942

Rogers

10

459.69

8747

875	5.9	453.8
885	8.0	451.7
905	8.0	451.7
1005	5.7	454.0
1065	4.3	455.4
1075	6.8	452.9
1105	5.9	453.8
1155	4.5	455.2
1165	2.0	452.7

8742

1105	7.9	451.8
1155	9.4	450.3
1205	9.8	449.9
1235	9.2	450.5
1305	6.9	452.8



FINAL X- SECTION Bkt # 11

459.69

8+47

1205		7.0	452.7
1255		6.4	453.3
1305		4.9	454.8
1315		7.0	452.7
1345		6.2	453.5
1405		9.2	450.5
1425		4.4	455.3
1505		8.9	450.8
1585		6.7	453.0
1605		0.2	455.0

8+37

1605	0		6.5	453.2
	929	468.85	0.13	459.56
Bm			701	461.84

451.7
153.21 D.S. toe of dam

- 461.84

FINAL X-SECTION Blk #9

Cont. from F.B. #623 p 78

TBM 9.97 454.36 444.59

7+24

1605 5.5 449.1

1645 4.8 449.8

7+34

1605 5.8 448.8

1705 1.2 453.4

7+44

1605 6.2 448.4

7+24

1905 0.0 454.6

7+90.5

~~1605 12.1 442.5~~

13.8 440.8

1705 ~~12.0 442.6~~

✓
ps

FINAL X-SECTION. BIT #9

April 29-1942

Pages

13

45456

8+00^E

1605

13.6 441.0 ✓

~~12.9~~ ~~442.2~~

1705

13.5 441.1 ✓

~~12.8~~ ~~442.1~~

8+07

~~1605~~

~~12.1~~ ~~442.5~~

1705

12.5 442.1 ✓

~~11.6~~

7+80^E

1605

13.6 441.0 ✓

~~11.8~~ ~~442.8~~

1705

12.7 441.9 ✓

~~11.9~~ ~~442.7~~

BM

997

440.59 ✓

✓
82

FINAL X-SECTION Blk #6

April 29-1942

Rogers

14

243 465.81 463.38

5+9.7

20.5 3.0 462.8

30.5 3.3 462.5

1.2 464.6

5+9.1

3.5 1.0 464.8

10.5 +1.9 467.7

5+8.8?

3.5 0.7 465.1

5.5 +0.6 466.4

10.5 +3.9 469.7

5+8.6

0 0.1 465.7

6.5 +1.1 466.9

8.5 +4.6 470.4

10.5 +5.5 471.3

+66

✓
pl

FINAL X-SECTION Bk # 6

April 29-1942

Rogers

15

465.81

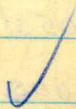
5480

0 +0.8 466.6

4.5 +1.5 467.3

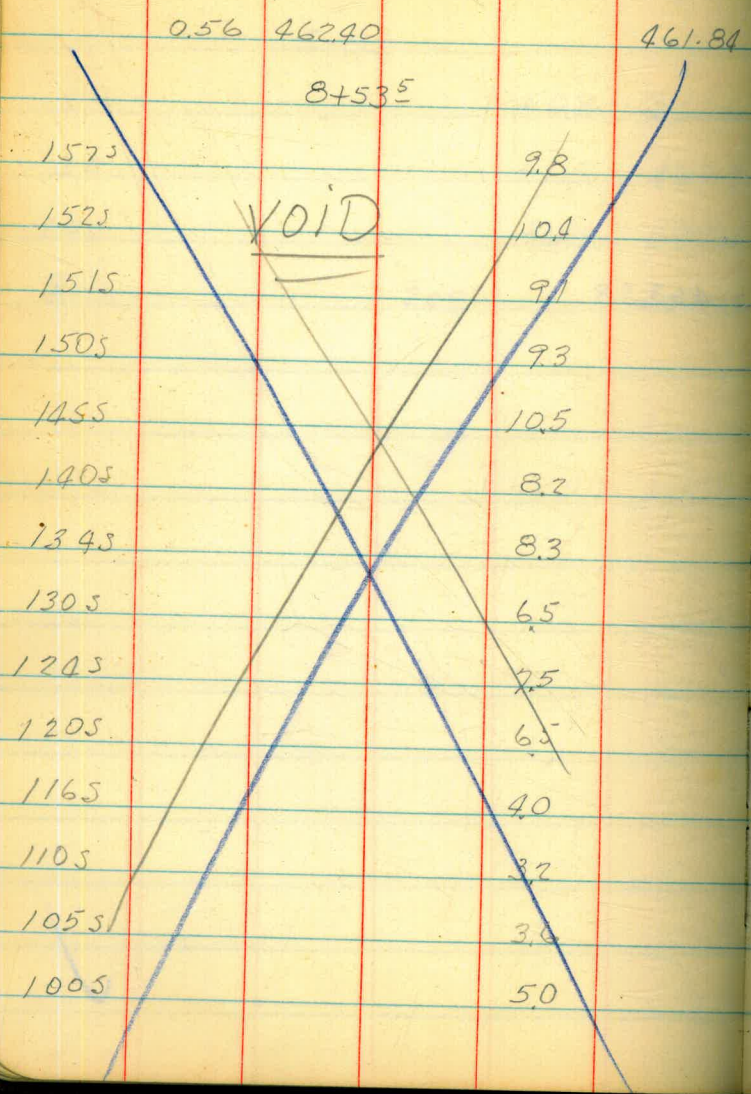
10.5 +6.7 472.5

BM, 243 463.38 = 463.38



FINAL X-SECTIONS BIK #11

Rogers
May 1-42 16



FINAL X-SECTION Bik # 71

Rogers
May 1 - 42 17

46240

8+53.5

905	7.2
865	6.3
855	6.0
805	5.2
705	5.2
665	4.9
605	5.2
515	6.4
505	5.2
405	5.6
305	7.9
265	7.7
255	6.6
205	5.5

VOID

FINAL X-SECTION BIK # 11

Rogers
MAY 5-42 18

103 462.87 461.84

831 460.32 1086 452.01

84535

1575 8.5 451.8

1525 8.8 451.5

1515 7.4 452.9

1505 7.6 452.7

1405 8.7 451.6

1365 7.2 453.1

1345 5.0 455.3

1305 4.7 455.6

1245 5.9 454.4

1205 4.5 455.8

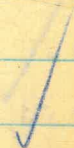
1165 4.0 456.3

1155 2.7 457.6

1105 2.7 457.6

451.6
153.28

D.S. toe of dam.



FINAL X-SECTION B/E # 11

19

460.32

8453⁵

1075	2.0	458.3
1005	3.5	456.8
905	5.7	454.6
855	6.5	453.8
845	4.2	456.1
805	3.3	457.0
705	3.7	456.6
605	3.1	457.2
515	4.5	455.8
505	3.4	456.9
405	3.4	456.9
305	5.8	454.5
265	6.4	453.9
255	4.3	456.0



FINAL X-SECTION BIL #11

460.32

8453⁵

305

3.5

456.8

B17

3.21

462.76

0.77

459.55

0.93

461.83

= 461.84



FINAL X-SECTIONS Blk# 6

470.47

6+01

~~201 13.0 459.5~~

301 9.5 461.0

317 1273 487.96 475.23

6+01

134.5 5.6 482.4

130.5 6.1 481.9

126.5 7.1 480.9

125.5 10.0 478.0

120.5 9.6 478.4

117.5 9.0 479.0

111.5 11.0 477.0

110.5 15.0 473.0

✓
8/1

FINAL X-SECTIONS Bk #6

Rogers

May 5-1942 22

48796

6401

105.5 11.5 476.5

100.5 9.5 478.5

92.5 9.3 478.7

90.5 11.1 476.9

80.5 12.7 475.3

78.5 14.5 473.5

72.5 15.7 472.3

70.5 16.9 471.1

5491

125.5 1.0 4870

120.5 1.2 486.8

117.5 1.5 486.5

116.5 3.9 484.1

113.5 3.9 484.1

110.5 2.2 485.8

✓
pl

FINAL X-SECTIONS Blk# 6

Rogers
May 7-42 23

487.96

5791

1085 1.2 486.8

1005 2.3 485.7

BM 1302 488.28 475.26

925 3.5 484.8

905 3.5 484.8

865 2.1 486.2

805 5.1 483.2

795 7.0 481.3

755 7.0 481.3

705 6.1 482.2

685 6.4 481.9

675 9.2 479.1

605 9.3 479.0

✓
Rogers

FINAL X-SECTIONS Bik # 6

24

48828

5791

588		108	477.5
535		106	477.7
525		91	479.2
505		87	479.6
475		93	479.0
445		95	478.8
405		108	477.5

5794

405		23.3	465.0
455		11.2	477.1
505		15.4	472.9
T.P.	11.25	499.46	007
			488.21

5788

1105		10.2	489.3
1085		11.7	487.8

✓
pl

FINAL X-SECTION BIR # 6

Rogers

MAY 2-42

25

49946

5488

1075	7.8	491.7
1035	11.0	488.5
1005	10.6	488.9
905	11.1	488.4
825	10.9	488.6
805	12.5	487.0
785	13.7	485.8
705	13.0	486.5
675	14.7	484.8
605	14.3	485.2
505	16.2	483.3
405	17.6	481.9
355	14.0	485.5
305	19.0	480.5

✓

FINAL X-SECTIONS BIK#6

Rogers

May 7-42

26

499.66

5481

105	19.5	480.0
205	16.0	483.5
245	17.5	482.0
255	14.0	485.5
305	14.0	485.5
325	11.2	488.3
305	10.9	488.6
405	13.1	486.4
505	12.8	486.7
515	8.7	490.8
565	7.0	492.5
605	8.6	490.9
575	8.7	490.8
585	10.2	489.3
705	10.3	489.2

FINAL X-SECTIONS Blk # 6

27

499.46

5781

735	9.1	490.4
805	10.6	488.9
905	10.3	489.2
945	7.3	492.2
1005	5.3	494.2
1035	2.2	497.3
1105	2.2	497.3
1185	2.9	496.6
1205	+0.9	500.4
5775		
205	12.3	487.2
225	10.5	489.0
275	7.6	491.9
305	8.3	491.2
405	9.9	489.6

FINAL X-SECTIONS Blk # 6

Rogers
July 7-67 28

499.46

5175

505		9.2	490.3 ✓
575		6.7	492.8 ✓
605		6.7	492.8 ✓
665		2.0	492.5 ✓
705		9.6	489.9 ✓
805		10.3	489.2 ✓
905		7.3	492.2 ✓
	11.76	509.03	2.19
			497.27 ✓
BM1		6.17	502.86 ✓ = 502.87

5191

21 N

466.8

Elev. taken from points for forms

20 N

465.0

" " " " " "

✓
pl

FINAL X-SECTIONS BIK #11

Rogers
May 15-52 29

	3.52 ✓	465.36		461.84
		8+53 ^E		
185			6.6	458.8
		8+47		
105			8.7 ✓	456.7
		8+44		
205			9.2	456.2
155			7.2	458.2
105			7.8	457.6
0			7.8	457.6
		8+37		
3N			8.5	456.9
5N			7.0	458.4
10N			7.3	458.1
		8+27		
20N			10.1 ✓	455.3

88 456.5

✓

FINAL X-SECTIONS Blk 11

Rogers
May 15-230

46536

8427

~~21 N~~

~~80 457.4~~

~~22 N~~

~~80 457.4~~

See Page 41

8417

130 452.4

?

352

461.8*

FINAL X-SECTIONS Bkt # 6

May 21-42

31

5.20 480.96 ✓

475.26 ✓

~~5.91~~

~~21.5N~~

~~12.0 468.5 ✓~~

~~22 N~~

~~9.0 471.1 ✓~~

~~3.2 N~~

~~4.6 475.9 ✓~~

5.81

5.5

5.6 474.9 ✓

0

6.1 474.4 ✓

10.1

3.7 476.8 ✓

11.1

5.6 474.9 ✓

19.1

3.0 477.5 ✓

11.28 486.54 ✓ 5.20

475.26 ✓

5.81

20.1

3.2 483.3 ✓

24.1

2.5 484.0 ✓

80.17

170.9 ✓
1.2
150.8 ✓

✓

FINAL X-SECTIONS BIK # 6

Rogers

MAY 21-42

32

480.40

5776

4788

1140

10N 5.8 474.7'

13N 3.9 476.6'

14N 0.7 479.8'

18N 2.7 478.3'

20N 0.7 479.8'

21N 42.9 483.4'

23N 43.2 483.7'

5.20 475.26

10.22 485.48 475.26

6+11

26

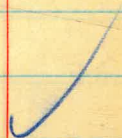
27

134S 8.6 476.9

136S 8.6 476.9

137S 7.0 478.5

140S 5.1 480.4



FINAL X SECTION 31646

33

485.48

6+11

1445

3.7 481.8

1505

+2.5 488.0

✓

HIGHWAY X-SECTION FROM TUNNEL OUTLET

Rogers

MAY 27-02

34

Sta H.I. Note: Axis = Sta 0+00 ξ
 All sections Lt. of red line taken from underlined H.I.

1+90	<u>468.4</u> 478.5	W. edge of road 478.2 3.3 101	473.2 5.3 93	471.2 7.3 77	464.1 4.3 65	463.5 4.9 49	457.4 11.0 26	456.2 12.2	455.3 13.1 32	457.2 11.2 50	EI 461.84 6.52 HI 468.41
------	-----------------------	----------------------------------------	--------------------	--------------------	--------------------	--------------------	---------------------	---------------	---------------------	---------------------	--------------------------------

											EI 475.23 3.29 478.52
--	--	--	--	--	--	--	--	--	--	--	-----------------------------

2+00	W. edge of road 475.3 3.7 91	472.6 5.9 83	470.6 7.9 64	464.6 3.8 60	463.9 4.5 49	463.4 5.0 36	457.7 10.7 18	456.5 11.9	457.7 10.7 28	459.0 9.4 50	
------	---------------------------------------	--------------------	--------------------	--------------------	--------------------	--------------------	---------------------	---------------	---------------------	--------------------	--

2+12	W. edge of road 474.6 3.9 82	472.9 5.6 72	471.5 7.0 59	467.2 1.2 50	464.2 4.2 43	464.0 4.4 33	463.5 4.9 24	459.4 9.0 6.0	458.2 12.3 20	460.6 7.8 42	459.3 9.1 42	460.2 8.2 50
------	---------------------------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	---------------------	---------------------	--------------------	--------------------	--------------------

2+25	474.5 4.0 73	474.9 3.6 70	473.3 5.2 65	471.3 2.2 47	<u>466.1</u> 2.3 30	463.8 4.6 22	463.7 4.7 11	461.8 6.6	459.7 8.7 30	461.2 7.2 13	461.2 7.7 27	460.0 8.4 45	460.8 7.6 50
------	--------------------	--------------------	--------------------	--------------------	---------------------------	--------------------	--------------------	--------------	--------------------	--------------------	--------------------	--------------------	--------------------

2+33	W. edge of road 474.1 4.4 60	472.1 3.4 58	472.6 5.9 48	471.7 6.8 38	<u>465.5</u> 2.9 22	464.0 4.4 13	463.8 4.6	462.3 6.1 4	461.7 6.7 23	459.8 8.6 47	459.8 8.6 50	
------	---------------------------------------	--------------------	--------------------	--------------------	---------------------------	--------------------	--------------	-------------------	--------------------	--------------------	--------------------	--

2+50	W. edge 468.66 478.5	474.1 4.4 50	473.2 5.3 39	473.6 4.9 23	474.0 4.5 20	<u>467.3</u> 1.4 16	465.8 2.9 9.0	463.7 5.0	463.0 5.7 24	460.8 7.9 29	460.0 8.7 46	460.3 8.4 50	EI 461.84 6.82 HI 468.66
------	----------------------------	--------------------	--------------------	--------------------	--------------------	---------------------------	---------------------	--------------	--------------------	--------------------	--------------------	--------------------	--------------------------------

HIGHWAY X-SECTION FROM TUNNEL

OUTLET

Rops
MAY 28-42 36

Sta.	H.I.		£				
3+75	468.66	474.4	474.5	474.3	465.8	463.9	
		41	4.0	4.2	3.5	4.8	
	478.57	2		9	27	50	
4+00		474.0	474.1		466.5	466.7	
		4.5	4.4		2.2	2.0	
			12		29	50	

HIGHWAY X-SECTION from TUNNEL

INLET

Rogers

May 29-47

37

Sta

H.I.

Note: Axis = STA. 0+00

£

All sections Rt. of red line taken from under lined H.I.

w. edge of Road

0+30

461.84
7.67
471.31

445.6 449.6 451.8
2.57 2.17 19.5
50 30 10

456.5 456.7 454.7 461.4 462.6 464.7 477.8 477.4
14.8 14.6 16.6 9.9 8.7 6.6 7.0 7.4
8 12 28 44 53 70 74

483.61
1.17
484.78

w. edge of Road

0+44

467.5 468.5 467.5 457.7 457.8
3.8 2.8 3.8 13.6 13.5
50 40 27 14 6

461.8 464.7 464.7 473.0 477.5 477.5
9.5 6.6 6.6 11.8 2.3 2.3
8 24 37 62 70

w. edge Road

0+52

467.6 471.3 469.3
3.7 0.0 2.0
50 27 22

464.9 465.5 472.6 472.9 479.6 477.6 477.7
6.4 5.8 12.2 11.9 5.3 2.2 2.1
14 23 26 37 47 60

w. edge Road

0+65

468.1 468.2 472.1 468.6 464.9
3.2 3.1 10.8 2.7 6.4
50 40 32 25 13

466.0 474.8 475.2 480.5 477.8 477.9
5.3 10.0 9.6 4.3 7.0 6.9
12 18 31 42 52

w. edge

0+87

467.5 469.5 468.7 465.2 465.3 469.0
3.8 1.8 3.1 6.1 6.0 2.3
50 45 42 40 27 25

478.7 479.6 477.3 478.2 480.9 478.2 478.2
6.1 5.2 7.5 6.8 3.9 6.6 6.4
5 8 21 26 31 40

w. edge Road

0+93

467.8 465.0 465.1 476.3
3.5 6.3 6.2 8.5
50 46 32 14

477.8 478.1 478.6
7.0 6.7 6.2
23 40

HIGHWAY X-SECTION from TUNNEL ^{IN} ~~OUT~~LET

Sta	H.I						
	471.31						W. edge of Road
1+19	<u>484.78</u>	465.0 6.3 50	465.0 6.3 33	479.7 5.1 21	478.9 5.9	479.6 5.2 23	479.6 5.2 30

							W. edge of Road
1+61		467.0 17.8 50	470.3 14.5 45	473.9 10.9 35	478.9 5.9 11	480.5 4.3 23	480.5 4.6 30

103
72

63

FINAL X-SECTIONS BIK# 11

39

7.06 ✓ 46890 461.84

8+37

~~10N 10.6 458.3~~

12N 10.4 458.5

15N 8.4 460.5

20N 8.6 460.3

8+47

10S 11.0 ✓ 457.9

0 10.8 458.1

3N 10.0 458.9

4N 8.5 460.4

10N 7.8 461.1

11N 5.4 463.5

15N 4.6 464.3

20N 4.6 464.3 ✓

FINAL X-SECTIONS BIK # 11

Rogers
June 11-48 40

46890

8+53⁵

10.5	10.8	458.1
15	11.0	457.5
0	10.1	458.8
3N	7.6	461.3
9N	6.2	462.7
10N	4.9	464.0
15N	4.4	464.5
18N	1.6	467.3

~~20N~~

706

461.8

check on BM.

8+17

BM, 114	476.37	475.23
21N	22.5	453.9
24N	18.0	458.4
29N	14.2	452.2
35N	13.1	463.3

462.2

✓

FINAL X-SECTION B16 # 11

Rogers
June 11-42

41~

47637 ✓

8+17

41 N 10.9 465.5

46 N 4.2 472.2

8+27

40 N 3.3 473.1 ✓

30 N 13.7 462.7 ✓

22 N 18.7 457.7 ✓

20 N 18.7 457.7 ✓

See
Page 29

8+37

21 N 15.4 461.0 ✓

25 N 12.6 463.8 ✓

30 N 10.5 465.9 ✓

35 N 7.5 468.9 ✓

40 N 2.3 474.7 ✓

✓

FINAL X-SECTION B16# 11

Logans

June 11-42 42

476.37

8447

23N

11.4 465.01

30N

6.6 459.8 469.8

84535

22N

8.6 467.8

25N

3.3 473.1

7.06

461.84

(?)

112 489.73

483.61

84535

33N

7.0 477.7

40N

7.2 477.5

8447

40N

7.2 477.5

50N

7.0 477.7

✓

FINAL X-SECTION BIK #11

Rogers
June 11-62 43

484.73 ✓

8437

45N

7.3

477.4 ✓

53N

7.1

477.6 ✓

8427

47N

6.1

478.6 ✓

50N

6.1

478.6 ✓

60N

7.1

477.6 ✓

8417

50N

6.9

477.8 ✓

46N

7.9

476.8 ✓

BM₁

112

483.61 = 483.61 ✓

✓

FINAL X-SECTION

Blk # 12

June 18-92

44

4.74 466.58

461.80

84.56

140.5

12.4

454.2

132.5

12.5

454.1

130.5

10.9

455.7

129.5

10.3

456.3

123.5

12.2

454.0

120.5

10.9

455.7

84.635

153.5

10.4

456.2

150.5

11.0

455.6

144.5

12.5

454.1

140.5

10.9

455.7

138.5

9.6

457.0

130.5

10.1

456.5

456.5

125.5

9.0

457.6

FINAL X-SECTION BIK# 12

June 18-42 45

466.58 ✓

8+63⁵

120.5 9.2 457.4 ✓

118.5 9.3 457.3 ✓

110.5 6.0 460.6 ✓

107.5 5.0 461.6 ✓

100.5 6.5 460.1 ✓

8+59

140.5 11.2 455.4 ✓

130.5 12.3 454.3 ✓

120.5 11.6 455.0 ✓

118.5 9.9 456.7 ✓

110.5 5.6 461.0 ✓

106.5 6.2 460.2 ✓

100.5 7.8 458.8 ✓



FINAL X-SECTION

Blk # 12

Rogers

June 19-42

46

466.58

8476

152.5	84	458.2
150.5	71	459.5
146.5	86	458.0
144.5	67	459.9
140.5	67	459.9
	5	
8473		
152.5	59	460.7
150.5	64	460.2
140.5	58	460.8
130.5	54	461.7
124.5	58	460.8
120.5	4.8	461.8
115.5	5.4	461.2
110.5	3.3	463.3
103.5	5.6	461.0
100.5	4.8	461.8

FINAL X-SECTION BAK #12

47

639 460.23

461.84

8+59.5

90S

10.8 457.4

Copied from book

87S

12.4 455.8

F.B. No. 619

80S

8+635

?

Page 32

90S

9.2 459.0

87S

9.7 458.5

82S

8.9 459.3

80S

8.9 459.3

70S

9.3 459.8

74S

9.7 458.5

60S

9.5 458.7

58S

10.0 458.2

50S

9.7 458.5

41S

7.6 460.6

40S

5.8 462.4

✓

FINAL X-SECTIONS Blk# 12

468.73 ✓

8+13.5

445 61 462.1

505 6.8 461.4

535 8.1 460.1

595 6.4 461.8

605 9.3 458.9

705 6.2 462.0

805 5.2 463.0

905 5A 462.8

945 4.4 463.8

985 6.2 462.0

6.39 461.84

48

Copied from book

F.B. No. 619

Page 33

✓

FINAL X-SECTION Bk # 12

Rogers
July 1-02 June 31-02 49

BM	419	466.03		461.84
		8+59		
405			55	460.5
353			49	461.1
305			60	460.0
		8+63 ⁵		
365			32	462.8
305			39	462.1
225			61	459.9
205			38	462.2
155			35	462.5
105			38	462.2
0			45	461.5
		8+83 ⁵		
1505			15	460.5
1405			20	464.0
BM	419			461.84 = 461.84



FINAL X-SECTION Blk # 12

Rogers
July 12-42 50

336 472.01 469.05

8783.5

1305 6.3 466.1

905 5.9 466.5

805 5.6 466.8

705 3.2 469.2

665 2.4 470.0

605 3.1 469.3

575 4.6 467.8

505 4.7 467.7

445 4.9 467.5

435 ~~7.0~~ 0.1 472.3

405 7.0 5 472.9

8785

405 7.0 5 473.0

445 1.3 471.1

505 1.4 471.0

FINAL X-SECTION

Blk # 12

51

472.9 ✓

8+85

555

0.9

471.5 ✓

605

2.3

470.1 ✓

0.65 484.26 ✓

483.6 ✓

July 10-1902

2.11 473.61 12.76

471.50

8+73⁵

405

9.1

460.5 ✓

385

5.3

468.3 ✓

305

5.1

468.5 ✓

205

5.7

467.9 ✓

105

7.7

465.9 ✓

0

8.9

460.7 ✓

8+63⁵

4N

9.5

460.1 ✓

10N

9.2

464.4 ✓

16N

7.3

466.3 ✓

472.9
 470.1
 483.6
 471.50
 460.5
 468.3
 468.5
 467.9
 465.9
 460.7
 460.1
 464.4
 466.3

✓

TUNNEL OUTLET ROADWAY

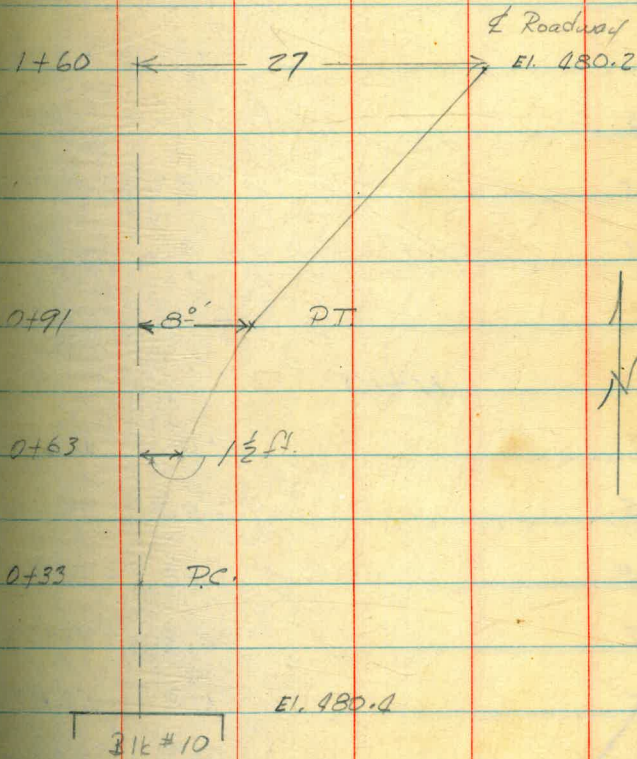
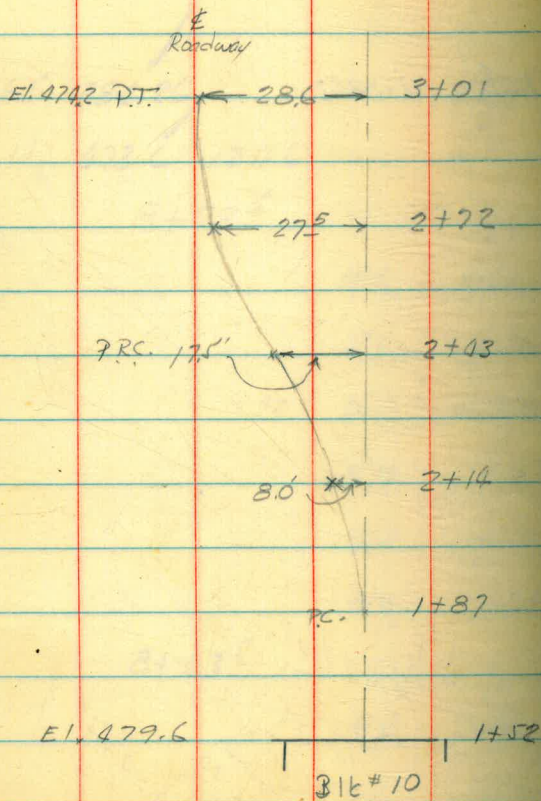
TUNNEL INLET ROADWAY .52

Rogers

July 17-1942

± Bit #10

± Bit #10



FINAL X-SECTIONS BK # 17

BPM. 664 562.50 555.86

11+00

10 N 12.2 550.3

6 N 13.6 548.9

0 12.0 550.5

4.5 11.8 550.7

10.5 9.7 552.8

15.5 7.5 555.0

20.5 + 14 563.9

11+10

30.5 + 1.1 563.6

27.5 + 0.3 562.8

20.5 4.4 558.1

15.5 5.8 556.7

10.5 11.3 551.2

0 12.7 549.8



✓
562.50

11+10

10✓

12.3 550.2 ✓

11+20

10✓

12.4 550.1 ✓

0

12.8 549.7 ✓

10.5

10.0 552.5 ✓

18.5

7.2 555.3 ✓

~~20.5~~~~7.2 561.3~~

See book 622 page 48

11+30

20.5

3.4 559.1 ✓

18.5

5.0 557.5 ✓

10.5

7.6 550.9 ✓

2.5

7.3 555.2 ✓

0

8.5 554.0 ✓

4✓

9.1 553.4 ✓

10✓

7.7 554.8 ✓

FINAL X-SECTION BIT # 17

Regrs
July 30-02 55

562.50 ✓

11+40

10N	59	556.6 ✓
0	68	555.7 ✓
55	74	555.1 ✓
105	63	556.2 ✓
205	44	558.1 ✓
255	+6.0	568.5 ✓
305	+8.2	570.7 ✓

11+50

305	+8.5	571.0 ✓
265	+4.7	567.2 ✓
205	+2.1	564.6 ✓
105	2.7	559.8 ✓
0	59	556.6 ✓
10N	45	558.0 ✓

2

✓

FINAL X-SECTION Blk #12

Rogers

August 4-12 56

TP. 077 48027 ✓ 480.0

8+63⁵

1605 198 461.0 ✓

1705 18.3 462.5 ✓

1805 14.9 465.9 ✓

1905 9.2 471.6 ✓

2005 8.4 472.0 ✓

2105 6.0 474.8 ✓

Roadway

8+73⁵

1605 18.2 462.6 ✓

1705 11.8 469.0 ✓

1805 9.1 471.7 ✓

1905 7.8 473.0 ✓

2005 5.7 475.1 ✓

Roadway

8+83⁵

1605 13.4 467.4 ✓

✓

FINAL X-SECTION BIC # 12

Rogers
August 11-42 57

480.77 ✓

8483⁵

1705

10.7

470.1

1805

6.2

474.6

1905

5.4

475.0

Roadway

065

484.22 ✓

483.57

August 11-42

9400

0

8.9

475.3

8 ✓

8.0

476.2

10 ✓

10.5

473.7

20 ✓

11.5

472.7

26 ✓

3.3

480.9

30 ✓

1.0

482.8

40 ✓

+5.9

490.1

50 ✓

+10.2

494.4

105

10.4

473.8

205

9.4

476.8

305

10.2

474.0

11.5
10
+ 10.5

✓

FINAL X-SECTION Blk # 12

Rogers
August 11-42 58

48922 ✓

9+00

405 7.9 476.3 ✓

505 8.7 475.5 ✓

605 10.2 470.0 ✓

705 10.7 473.3 ✓

805 11.3 472.9 ✓

905 11.6 472.6 ✓

1005 13.4 470.8 ✓

1105 14.0 470.2 ✓

1205 13.6 470.6 ✓

1305 13.3 470.9 ✓

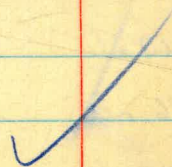
1405 13.9 470.3 ✓

8+93⁵

1405 14.7 469.5 ✓

1305 12.9 471.3 ✓

1205 14.3 469.9 ✓



FINAL X-SECTION Blk #12

59

484.22 ✓

8193⁵

1105	13.9	470.3 ✓
1005	14.3	469.9 ✓
905	13.5	470.7 ✓
805	12.2	472.0 ✓
705	12.0	472.2 ✓
605	11.2	473.0 ✓
505	9.0	475.2 ✓
405	7.8	476.4 ✓
305	7.5	476.7 ✓
205	8.3	475.9 ✓
105	9.9	474.3 ✓
0	10.2	474.0 ✓
10 N	9.5	474.7 ✓
16 N	11.4	472.8 ✓
20 N	10.5	473.7 ✓

FINAL X-SECTION 316 & 12

484.22 ✓

8+93⁵

30 N	46	479.6
40 N	+3.4	487.6 ✓
42 N	+5.8	490.0 ✓
50 N	+5.2	489.4 ✓

8+91⁵

20 S	10.3	473.9 ✓
25 S	7.8	476.1 ✓
30 S	7.8	476.4 ✓
40 S	7.8	476.0 ✓

8+83⁵

0	12.8	471.2 ✓
10 S	13.0	471.2 ✓
20 S	12.4	476.8 ✓
30 S	10.9	473.3 ✓
10 N	12.1	472.1 ✓
20 N	11.8	472.4 ✓

✓

FINAL X-SECTION 3/6^{1/2}

61

484.22 ✓

8+83⁵

30 S ✓ 2.0 477.2 ✓

40 S ✓ 5.8 478.4 ✓

50 S ✓ 4.7 ^{488.9} 478.9 ✓

60 S ✓ 15.8 490.0 ✓

8+73⁵

10 N ✓ 16.7 467.5 ✓

20 N ✓ 14.4 469.8 ✓

25 N ✓ 12.0 472.2 ✓

30 N ✓ 6.2 478.0 ✓

40 N ✓ 2.0 477.2 ✓

50 N ✓ 4.7 479.5 ✓

8+63⁵

17 N ✓ 15.1 469.1 ✓

20 N ✓ 13.9 470.3 ✓

25 N ✓ 12.0 472.2 ✓

30 N ✓ 6.6 477.6 ✓

862
13 ✓

✓

FINAL X-SECTION Blk # 12

Rogers
August 11-42 62

48422 ✓

8+63⁵

40 ✓ 7.0 477.2

50 ✓ 7.0 477.2

8+83⁵

120.5 16.2 468.0

110.5 15.7 468.5

100.5 15.7 468.5

BM 174 ✓ 479.71 477.97 B-10-42

8+93⁵

150.5 11.5 468.2

153.5 11.6 468.1

160.5 5.9 474.8 473.8

170.5 4.2 475.5 Roadway



479.71 ✓

9400

150.5

11.2 468.5 ✓

152.5

10.8 468.9 ✓

160.5

5.3 474.4 ✓

170.5

4.2 475.5 Roadway ✓

1.05 484.62

483.57

8107

~~30 W~~

~~VOID~~

~~8.9~~

~~40 W~~

~~7.2~~

~~50 W~~

~~7.2~~

81005

30 W

23.3 462.3

PROFILE STA 9+00

11-3-42

65

TP 7.37 487.37 480.00

0+00 13.9 473.5

Sta 0+00 = 151.9 S. Axis

0+07 13.7 473.7

0+12 10.8 477.6

+55 10.4 477.0

+66 6.0 481.4

1+00 4.4 483.0

+50 0.7 486.7

STA 9+16.5

0+00 12.1 475.3

Sta 0+00 = 144.02 S. Axis

+10 12.5 474.9

+60 8.1 479.3

+70 1.4 486.0

1+00 3.7 483.7

1+50 +2.2 489.6

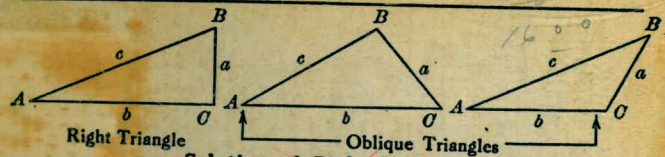
PROFILE OF BEDROCK - STA. 9+00

Dec. 2nd 66

T.P.	1.22	481.22	480.0	
0+00			468.9	Sta 0+00 = 151.9 So. of axis
0+07	6.3 3.3 = Drilled 9.6		471.6	= Bedrock
0+12	4.7 5.0 = Drilled 9.7		471.5	= Bedrock
0+25	4.6 4.6 = Drilled 9.2		472.0	= " "
0+35	4.1 5.7 = Drilled 9.8		471.4	= Bedrock
0+50	4.3 5.5 = Drilled 9.8		471.4	= " "
0+55	4.3 7.5 = Drilled 11.8		469.4	= " "
0+65	0.4 11.5 = Drilled 11.9		469.3	(Did not strike Bed rock)

69

TRIGONOMETRIC FORMULÆ



Solution of Right Triangles
 For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{b}$, $\csc = \frac{c}{a}$

Given	Required	Formulas
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B, c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B, b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A, b = a \cot A, c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A, a = b \tan A, c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A, a = c \sin A, b = c \cos A$

Solution of Oblique Triangles

Given	Required	Formulas
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}, C = 180^\circ - (A + B), c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}, C = 180^\circ - (A + B), c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C, \tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}, \sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}, C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}, \text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL

Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = $5^\circ 10'$. From Table, Page IX. $\cos 5^\circ 10' = .9959$. Horizontal distance = $319.4 \times .9959 = 318.09$ ft.
 Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\text{Cosine } 5^\circ 10' = .9959, 1 - .9959 = .0041$. $319.4 \times .0041 = 1.31, 319.4 - 1.31 = 318.09$ ft.
 When the rise is known, the horizontal distance is approximately:—the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft. slope distance = 302.6 ft. Horizontal distance = $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.

