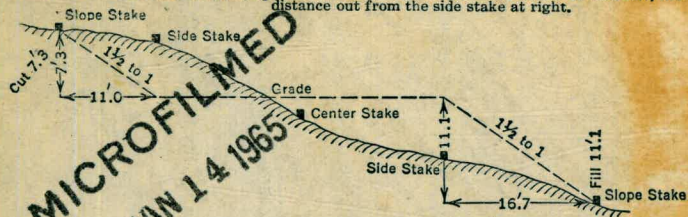


W
670

DISTANCES FROM SIDE STAKES FOR CROSS - SECTIONING
Roadway of any Width. Side Slopes 1 1/2 to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	Distance out from Side or Shoulder Stake										Cut or Fill
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

KEUFFEL & ESSER CO., N. Y.
 For Curve Tables see end of book.

670

City of San Diego Water Department
 Division of Development and Conservation
 Room 258, Civic Center
 San Diego, California

The paper in this book No. F363A
 is made of 50% high grade rag stock
 with a WATER RESISTING surface sizing.

11,112. ks x, ye. km.

This entire book on Dulzura PL
investigations.

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At La Mesa Hts

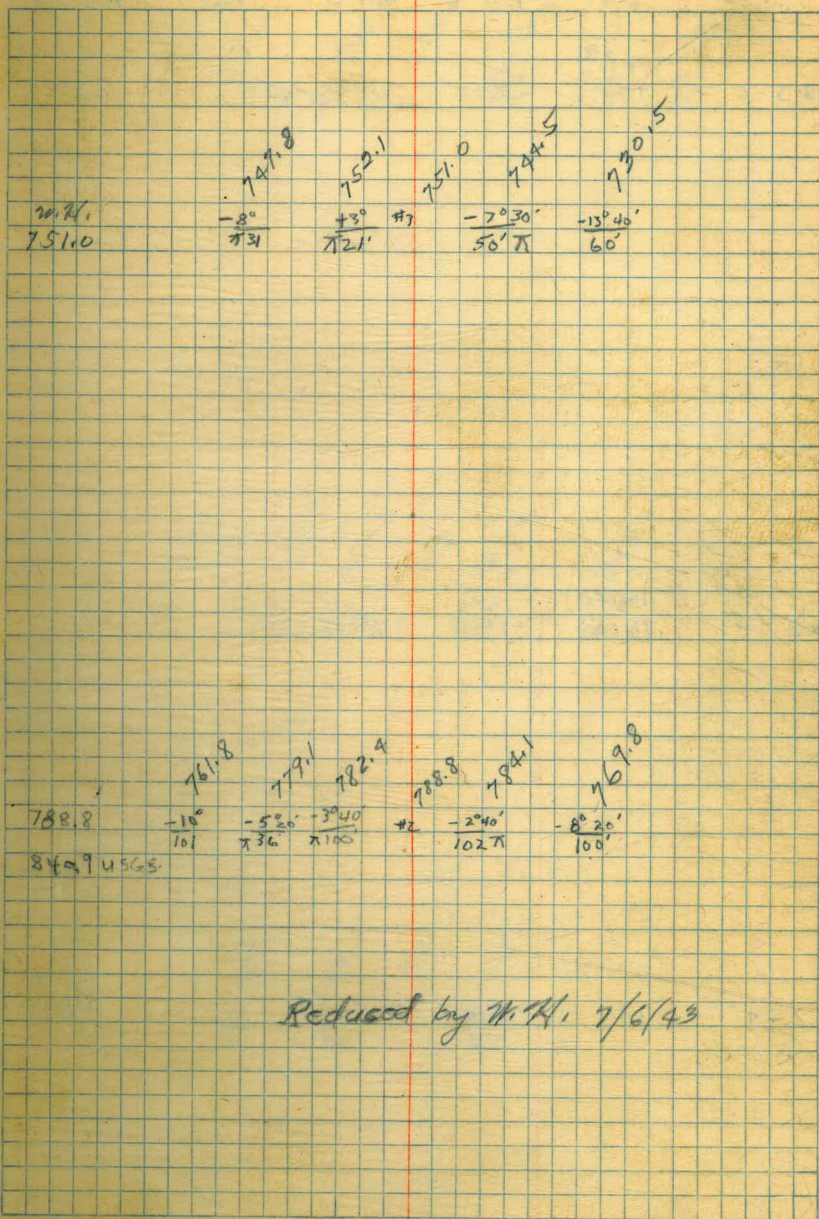
6-28-47

Hill
Hans
Ottor
Polak

Pt	Dist	Vert L	Hor L	Red	H.I.
2-3	(448.8) 452'	-4° 49'	22° 41' R		5.1

* 1-2	(977) 980'	-3° 03'	2° 56' L		5.0
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Elev. RL 41



Reduced by W.H. 7/6/49

Pt	Dist.	Vert. L	Hor. L	Rod	H.I.
	(768.5)				
#5-6	771'	-3°15'	49°25' Rt		5.2

#2-5	1061.5 1862'	-1°21'	P.O.T.		5.1
------	-----------------	--------	--------	--	-----

2-9	(730.3) 731'	-1°42'	P.O.T.		5.1
-----	-----------------	--------	--------	--	-----

Elev					
720.0	121.3 -2930' 120'	726.5 +30' 120' #6	728.7 -3010' 70'	718.3 -500' 50'	708.9 -150' 40'
763.8	135.9 -60' 160'	752.5 -60' 700'	762.9 -120' 40' #5	763.8 -9020' 58'	760.0 -9020' 102'
767.1	754.2 -100' 60'	764.5 -30' 50'	767.1 -4020' 70'	761.8 -100' 90'	746.4

Pt	Dis.	Vert L	Hor L	Red	H.I.
	(401.5)				
.8-9	402'	-2° 0'	P.O.T.		4.8

	(710.4)				
*6-8	711'	-1° 22'	P.O.T.		5.2

	(367.7)				
.6-7	374'	-7° 27'	P.O.T.		5.2

Elev

W. H.	680.1	690.5	689.13	677.2	665.1
689.3	$\frac{-6^\circ}{100'}$	$\frac{+0^\circ 40'}{100'}$	#9 $\frac{-7^\circ}{100'}$		$\frac{-7^\circ}{100'}$

	682.3	691.8	703.3	700.5	695.0	686.1
703.5	$\frac{-9^\circ}{100'}$	$\frac{-3^\circ 30'}{98'}$	#8 $\frac{-2^\circ}{80'}$	$\frac{-6^\circ 20'}{50'}$		$\frac{-8^\circ 45'}{60'}$

W. H.	650.2	657.5	672.1	701.5	706.7	701.8
672.1	$\frac{-8^\circ 30'}{50'}$	$\frac{-8^\circ 30'}{100'}$	#7 $\frac{+1^\circ}{56'}$	$\frac{+4^\circ}{60'}$		$\frac{-3^\circ 30'}{80'}$

P.T.	Dis	Vert L	Hor L	Red	H.I
11-12	(287.1) 288'	-3° 10'	17° 23' R+		5.1

* 8-11	1231'	+6° 46'	P.O.T		4.8
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8-10	691'	-0° 13'	P.O.T		4.8
------	------	---------	-------	--	-----

Elev

704.4	697.9	695.3	704.2	703.9	698.8	686.4	684.1
703.9	$\frac{-8^{\circ}40'}{50'}$	$\frac{-6^{\circ}30'}{70'}$	$\frac{-0^{\circ}40'}{60'}$	$\frac{-2^{\circ}40'}{110'}$	$\frac{-5^{\circ}}{90'}$	$\frac{-1^{\circ}20'}{100'}$	

719.8	693.6	701.8	718.1	719.8	711.1	689.7
	$\frac{-9^{\circ}20'}{50'}$	$\frac{-9^{\circ}30'}{100'}$	$\frac{-2^{\circ}}{50'}$	$\frac{-5^{\circ}}{100'}$	$\frac{-7^{\circ}30'}{200'}$	

700.7	679.9	696.6	703.5	700.7	696.5	676.2
	$\frac{-16^{\circ}40'}{50'}$	$\frac{-5^{\circ}}{80'}$	$\frac{+9^{\circ}}{40'}$	$\frac{+10^{\circ}}{90'}$	$\frac{-5^{\circ}}{90'}$	$\frac{-12^{\circ}}{100'}$

Pt.	Dist.	Vert. I	Hor. h	Rod	H.I.
	(187.7)				
14-15	191'	-7° 33'	D.O.		5.1

	(187.5)				
13-14	188'	-2° 56'	24° 18' 14"		5.1

	(458)				
11-13	459'	-2° 37'	P.O.T		5.1

Elev								
70.71	7.653.1							
664.4	-7° 56'	-5° 30'	75°	#5	-7° 30'	-13°	-18°	
	56'	100'	50'		30'	80'	90'	
	659.2							
	668.7							
	668.4							
	660.5							
	671.0							
	685.1							
	689.3							
	689.6							
	678.3							
	653.0							
689.3	-12°	-6° 40'	-4°	#14	40° 30'	-6° 30'	7° 20'	
	100'	70'	60'		40'	100'	200'	
	681.7							
	695.0							
	698.9							
	698.0							
	693.3							
	687.6							
698.9	-6°	-3°	-0° 30'	#13	-3°	-7° 20'		
	130'	70'	100'		90'	160'		

Pt	Dist.	Vert. L	Hor L	Rad	H.I.
17-18	273'	-0°-16'	2°10' Lt	side shot	5.2

814-17	(545.3) 547'	-3°10'	P.O.T.		5.1
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14-16	(354.8) 358'	-5°24'	P.O.T.	Rd.	5.1
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Elev.

W.H.

657.8

Knoll at end of bog track

✓

659.1

648.9	660.1	659.1	652.9	645.6
-9°20'	+1°	-6°	-10°40'	
70'	60' T	60' T	70'	

W.H.

655.9

656.1	658.7	655.9	648.6	620.6
-2°30'	+4°	-7°	-17°	
60'	40' T	60' T	100'	

Pt.	Dist.	Vert. L.	Hor. L.	Rad.	H.I.
17-21	(319.7) 328'	-9° 10'	84° 13' Rt	6.2	5.2

7

Elev.
607.5
79

17-20	(1550.5) 1551'	-1° 0'	P.O.T.	side shot - Hill	5.2
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W.H.
632.1
top of hill

17-19	(893.3) 910'	-7° 46'	52° 40' Rt	side shot Red	5.2
-------	-----------------	---------	------------	---------------	-----

W.H.
537.3

~~H.I. 607.5~~
~~side shot road~~

Pt	Dist.	Vert L	Hor L	Rod	H.I
	(497.4)				
23-24	500'	-9°08'	P.O.T.	10.9	9.9

	(995.5)				
*21-23	1012	-7°20'	P.O.T.		5.1

	(495.4)				
21-22	511'	-10°04'	P.O.T.	Road	5.1

Elev

443.5
Less 5.0
<u>E. 438.5</u>

419.7

with
520.0

Pt.	Dist.	Vert L.	Hor L.	Rad	H.I.
-----	-------	---------	--------	-----	------

Elev.

26-	731'	-0° 30'	74° 08' Lt	Intersec Mass + V.H.I.	5.24
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413.96 B.M.
411.54
5.78

*25-26	(784) 785'	-2° 01'	P.O.T.	Encl. Extras	5.1
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411.0

*23-25	(851) 853'	2° 15' -5° 11'	P.O.T.		4.9
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438.5

26- (211.9)
212' +1° 10' 100° 14' RT ^{INTER} yale 4.9

Topog. of Pt. #2 Dulzura
 PL. Stadia survey

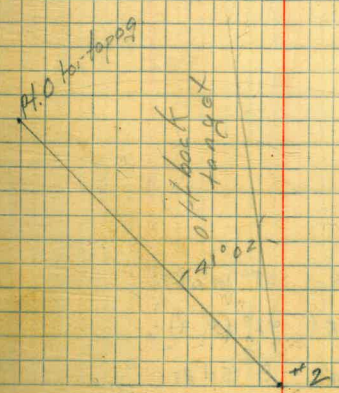
H. W. G.
 Green
 Polak
 6-20-93

Pt.	Dist	Vert L	Hor L	Rod	H.I.
0-23	208' (202.2)	-9° 37'	3° 04' Rt		5.3
0-22	125' (21.2)	-9° 59'	32° 30' Rt		5.3
0-21	136' (132)	-9° 55'	84° 23' Rt		5.3
0-20	364' (398.4)	-11° 56'	41° 55' Rt	11.3	5.3
0-19	396' (387.1)	-8° 37'	57° 11' Rt	11.3	5.3
0-18	387' (384.4)	-4° 44'	72° 27' Rt		5.3
0-17	623' (622.4)	-1° 49'	65° 30' Rt		5.3
0-16	981' (980.4)	-1° 22'	62° 48' Rt		5.3
0-15	908' (902.4)	-4° 32'	53° 49' Rt		5.3
0-14	1117' (1155.2)	-5° 46'	46° 37' Rt		5.3
0-13	976' (967.6)	-8° 37'	41° 02' Rt		5.3
0-12	618' (600.9)	-9° 34'	43° 01' Rt		5.3
0-11	631' (619.7)	-7° 41'	37° 43' Rt		5.3
0-10	998' (983.6)	-6° 53'	36° 46' Rt		5.3
0-9	462' (959.5)	-2° 55'	26° 48' Rt		5.3
0-8	773' ✓	-0° 39'	16° 04' Rt		5.3
0-7	628' (627.4)	+1° 45'	0° 53' Rt		5.3
0-6	664' (663.4)	+1° 25'	12° 03' Lt		5.3
0-5	822' (821.8)	-0° 53'	31° 37' Lt		5.3
0-4	701' (698)	-3° 44'	41° 18' Lt		5.3
0-3	533' (530)	-4° 18'	43° 30' Lt		5.3
0-2	309' (382.6)	-16° 59'	54° 6' Lt	10.3	5.3
0-1	261' ✓	-1° 07'	95° 38' Lt	9.3	5.3
#2-0	132' (131.2)	-4° 21'	41° 02' Lt		5.3

Reductions by W.H.

Elev
749.5
757.5
755.7
705.2 699.2
720.1
747.0
759.1
755.5
707.2
662.1
635.0
677.5
695.2
660.0
729.9
770.0
798.0
795.2
766.1
733.2
738.9
687.5
769.7
778.8

Pt. #5



Point #2 = 788.8

0-26	206'(202.7)	-7° 16'	25° 19' Lt.	5.3
0-25	479'(478.2)	-2° 15'	12° 14' Rt.	5.3
0-24	335'(331)	-6° 14'	8° 54' Rt.	5.3

752.9
760.0
742.7

Add. topog from Pt. 19 (see page 7)

Dulzura stadia pt. survey

Pt	Dist	Vert. A	Hor. A	H. I.	Red
5 to 6	(99.8) 103'	+10°13'	P.O.T.	1.9	1.9 (579.4)

* 6 to 5	(299) 301'	+10°37'		5.0	5.0
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0 to 4	(207.2) 208'	+3°28'		5.0	5.0
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0 to 3	(157.7) 158'	+2°32'		5.0	5.0
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0 to 2	(102.9) 103'	+1°30'		5.0	5.0
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0 to 1	51'	+0°18'		5.0	5.0
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Pt 0
Pt. 19 backsight on Pt. 17

8/12/43

Hill
King
O'Han

13.

Elev.	561.1	568.9	583.6	581.9	579.4	576.6	575.2	571.7	569.4
	-7°42'	-6°51'	+2°25'	+5°32'	-2°28'	-1°02'	-2°09'	-2°35'	
	162'	122'	75'	26'	66'	161'	200'	222'	
	159.1	(121.7)	↑	(25.8)	(63.9)	(160.9)	(200.7)	(321.6)	

(561.4)	540.1	546.1	562.1	561.4	560.6	553.7	561.8
	-5°38'	-4°51'	+1°21'	-2°13'	-1°13'	+0°52'	top of hill
	217'	182'	38'	20'	705'	222'	
	(214.9)	(180.7)	✓	✓	(104.4)	✓	

(549.9)	516.6	539.6	547.1	549.9	549.1	543.8	539.7	542.9	545.3
	-8°03'	-4°37'	-5°05'	-2°22'	-1°21'	-7°19'	-1°57'	-0°42'	
	270'	99'	32'	19'	72'	120'	206'	268'	
	(235.3)	(88.8)	(31.8)	✓	(71.5)	(118.1)	(205.8)	(267.9)	

(544.3)	498.8	510.9	530.8	542.4	544.3	543.1	530.7	531.1	530.1
	-9°18'	-10°20'	-8°10'	-4°58.3	-1°31'	-7°25'	-6°08'	-3°12'	
	285'	189'	96'	23'	35'	106'	124'	255'	
	(377.6)	(182.9)	(94.1)	(22.8)	✓	(104.2)	(122.4)	(254.3)	

(540.0)	488.90	525.50	537.40	540.0	536.7	522.1	517.1	512.6
	-12°47'	-10°25'	-2°56'	2	-3°11'	-9°57'	-7°30'	-6°10'
	225'	65'	38'		60'	56'	145'	226'
	(214)	(62.7)	↑		(57.8)	(83.4)	(143.3)	(223.4)

(537.6)	501.8	536.2	537.6	535.1	517.3	513.0	508.2
	-9°09'	-3°42'	1	-1°20'	-5°14'	-8°00'	-7°50'
	228'	28'		58'	120'	180'	222'
	(222.2)	28'	✓	✓	(123.4)	(155.9)	(218.7)

537.3	504.1	512.1	537.3	535.1	530.4	515.0
	-9°18'	-8°42'	0	-0°46'	-1°27'	-7°26'
	291'	166'	21	132'	61'	157'
	(195.4)	(162.1)	0	✓	(60.6)	(157.4)

filled road

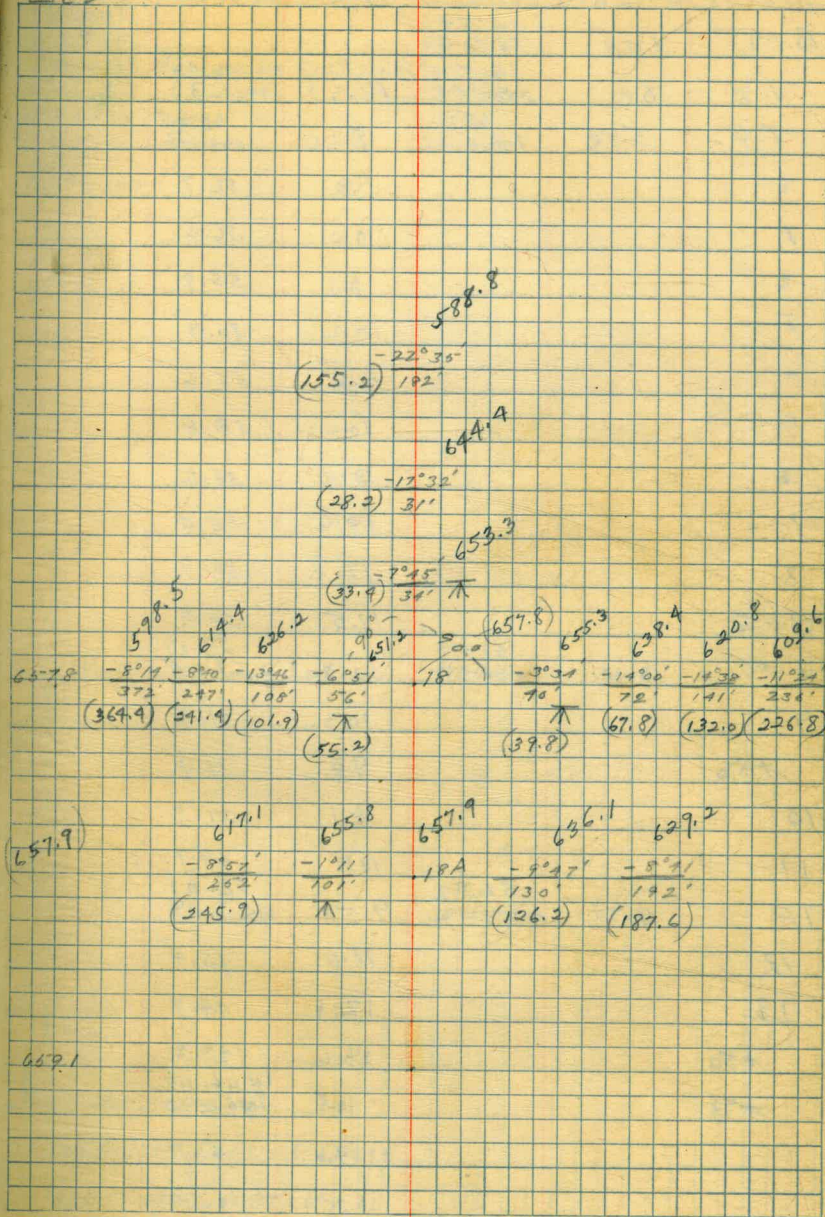
Add. topog. from pt. 18 (See page 6)
 Dulzura station 192. Survey
 Pt. Dist Vert A Hor A H.L. Red

17 to 18 123' -0°16' 5.2 5.2

17 to 18A 126' -0°50' P.O.T. 5.2 5.2

17 foresight on 18.

8/13/43 Hill King L ♀ R 14
 Elev. 0.11



7-11-43 H. 11
King
0 + 700
1475.82
+ 776.2

Profile	D41249	Conduit	Tunnel	to weir
B.M.	1.58	1477.40 1477.88		
T.P.	0.86	1465.75 1466.27	12.51	64.89 445.37
T.P.	5.92	65.97 1466.45	5.70	60.05 1460.52
0			9.2	56.7
1			10.0	56.0
2			10.1	55.9
3			10.2	55.8
4			10.4	55.6
5			10.4	55.6
6			10.4	55.6
7			10.6	55.4
8			11.3	54.7
8+50			11.5	54.5
T.P.	8.42	61.59 1462.07	12.80	53.17 453.65
9			10.3	51.3
+50			9.8	51.8
10			10.1	51.5
11			11.9	49.7
TP	4.91	56.92 1457.40	9.58	52.01 452.49
12			11.0	45.9
13			12.1	44.8
+50			13.6	43.3
+93			10.5	1446.42 1446.90
			14.0	42.9
			10.85	46.07

X on rock S.W. cor. 600 East School

EL. TUNNEL

Top metal weir

Ground at Face of Weir

Top Conc. apron

Creek 1000 NW. of weir El. 1425.9

Levels to Passes 1, 2 + 3 see

pages 23, 24 + 25 for pass profiles 16

B.M.	9.77	1456.92 1457.40 1459.26 1459.74	7.43	1449.97	49 ✓
T.P.	11.57	71.06	0.25	1459.49	
T.P.	10.84	81.12	0.78	70.28	
B.M.			4.78	76.86 1476.34	1475.82 1476.3
T.P.	1.02	78.45	3.69	77.43	
T.P.	1.39	66.89	12.95	65.50	
T.P.	0.91	55.00	12.86	54.03	
T.P.	0.50	42.68	12.82	42.18	
T.P.	0.40	1430.16	12.92	29.76	
T.P.	1.57	18.72	13.01	17.15	
T.P.	1.04	06.83	12.93	1405.79	
T.P.	8.34	14.65	0.52	1406.31	
T.P.	13.01	25.29	2.37	1412.28	
B.M. #1			12.15	1412.66 1413.14	
T.P.	12.71	37.26	0.74	24.55	
T.P.	12.22	48.94	0.54	76.72	
0+00 T.P.	12.67	59.09	2.04	1446.42 1446.90	
T.P.	12.63	71.14	0.58	58.51	
T.P.	3.86	74.04	0.96	70.18	
1+25			3.91	59.65 70.17	Ginney
T.P.	1.62	63.50	12.16	61.88	
T.P.	7.55	58.56	12.49	51.01	
2+85			12.14	46.42	
3+15			18.9	39.7	

X Top Conc Wall N. Side Next to recording house

Creek Bed 1000' N. W. Weir Elev 1425.9

Weir Elev at S. end Rt #1 0-50' S. 15.15' lower

Top saddle Rt. #1 saddle is 2.5' lower 75' West of 1+25

Weir Elev at S. end Rt #1

Bottom Gully

B.M.#1	2.47	21.13		1412.66	
T.P.	12.80	32.20	1.73	19.40	✓
T.P.	12.42	42.82	2.00	30.20	✓
T.P.	11.70	54.17	0.35	42.47	✓
0+00 ^{B.M.}			7.75	1446.42	✓
T.P.	12.23	65.83	0.57	53.60	✓ G. H. W.
T.P.	3.42	68.10	1.15	64.68	✓
1+11			2.32	65.78	✓
T.P.	1.76	57.84	12.02	56.08	✓
2+22			11.42	46.42	✓
2+72			23.4	34.4	✓
B.M. Rt 2	11.46	57.88		1446.42	✓
T.P.	10.60	61.94	6.54	57.34	✓
T.P.	2.46	57.89	12.51	49.43	✓
T.P.	0.55	39.42	13.02	38.87	✓
T.P.	0.91	27.38	12.95	26.47	✓
T.P.	6.90	15.52	12.76	14.62	✓
T.P.	0.94	1403.61	12.85	02.67	✓
			10.83	1392.78	✓
Check ends		1403.61			✓
T.P.	11.13	1411.09	3.65	1399.96	✓
T.P.	6.74	1412.45	5.38	1405.71	✓
T.P.	12.40	24.40	0.45	1412.0	✓
T.P.	12.16	36.07	0.49	23.91	✓
T.P.	10.40	45.65	0.82	35.25	✓

Weir Elev. East end Rt. #2 0-50 9.4' lower

Elev. Top Saddle Rt. 2

Weir Elev. West end Rt. 2

50' Down Gully

Topsaddle Rt. 3

	1445.65 ✓			
T.P.	12.45	57.57 ✓	0.53	45.12 ✓
T.D.	16.77	67.73 ✓	0.61	56.96 ✓
T.P.	12.78	79.93 ✓	0.58	67.15 ✓
B.M. 600' East school at X Road S.W. cor.		4.25	75.68 ✓	75.82

Elev. F.L. 100

1/2 mile shot taken across valley

Levels to pass in sec. 7 &

B.M.	11.65	51.44 ✓		1039.79
T.P.	8.32	59.35 ✓	0.41	51.03 ✓
T.P.	0.30	50.45 ✓	9.20	50.15 ✓
B.M. #1	0.18	38.65 ✓	11.98	38.47 ✓
T.P.	7.59	41.02 ✓	5.22	33.43 ✓
T.P.	1.57	30.19 ✓	12.40	28.62 ✓
T.P.	0.96	18.89 ✓	12.26	17.93 ✓
T.P.	1.30	07.72 ✓	12.47	1006.42 ✓
T.P.	5.69	1000.60 ✓	12.81	994.91 ✓
B.M.	2.51	90.25 ✓	12.86	987.74 ✓
T.P.	7.78	84.98 ✓	13.05	977.20 ✓
T.P.	6.68	78.88 ✓	12.78	972.20 ✓
T.P.	12.53	83.15 ✓	8.26	970.62 ✓
T.P.	4.33	79.65 ✓	7.83	975.32 ✓
T.P.	12.90	91.83 ✓	0.72	979.93 ✓
T.P.	12.58	1007.76 ✓	0.65	991.18 ✓
T.P.	9.77	12.88 ✓	0.65	1003.11 ✓
T.P.	4.93	09.97 ✓	7.84	1005.04 ✓
T.P.	4.31	1010.98 ✓	3.30	1006.67 ✓
0+00	0	04.54	3.90	1007.08 ✓
T.P.	12.04	22.38 ✓	0.64	10.34 ✓
1+00			5.2	1021.9
T.P.	11.89	33.65 ✓	0.62	21.76 ✓
2+00			0.8	1032.9
T.P.	12.89	46.04 ✓	0.50	33.15 ✓

Profile of pass

231' N.E. School house X roads. USGS marker
N. 1/4 P.F. 1 st Cor West Jampul School #174672
N. 1/4 part N.E. S.W. Cor. N.E. 1/4 Sec 9 so. side Rd
ON Rock east of Eucalyptus grove 500'
X East of road - 125' North olive grove
S. end of pass

		1046.04 ✓		
T.P.	10.75	56.22 ✓	0.57	45.47 ✓
3+00			9.3	1046.9
T.P.	10.98	66.58 ✓	0.62	55.60 ✓
4+00			9.6	1057.0
5+00			3.6	1063.0
T.P.	4.71	65.83 ✓	5.46	61.12 ✓
6+00			2.4	63.4
7+00			8.4	57.4
T.P.	1.87	55.06 ×	11.64	54.19 ✓
8+00			6.6	49.5
8+85			17.0	39.1
B.M. 9+40	1.22	1044.50 73.50 ×	12.78	1043.28 72.22 ×
10+00			12.5	1032.0
T.P.	0.10	1031.75 30.75 ×	12.85	1031.65 30.65 ×
11+00			9.0	1022.8
T.P.	0.11	1031.76 20.76 ×	10.10	1021.65 20.65 ×
11+50			1.0	1020.8
12+00			11.0	1010.8

Bottom Draw @ 20° LEFT
6' Boulder

KING
OTTEN
8-24-93

Pt.	Dulzura Dist.	Stadia Vert A	Survey Hor A	H.I.	Rod
Pt*8-12	(975.7) 976'	-0° 59'	P.O.T.	5.1	5.1
Pt 8-11	(761.7) 763	-2° 20'	P.O.T.	5.1	5.1
Pt 8-10	(549.9) 550'	-2° 03'	P.O.T.	5.1	5.1
Pt 8-9	(232.3) 233'	-3° 04'	P.O.T.	5.1	5.1
Pt 6-8	(875.6) 876	+1° 11'	P.O.T.	5.1	5.1
Pt. 6-7	568'	-0° 18'	P.O.T.	5.1	5.1
Pt*4-6	(810.8) 811'	-0° 55'	P.O.T.	5.2	5.2
Pt. 4-5	(558.4) 559'	-1° 49'	86° 48' ht	5.2	5.2
Pt. 2-4	(913.5) 914'	-1° 24'	P.O.T.	5.1	5.1
Pt 2-3	(338.2) 339'	-2° 51'	P.O.T.	5.1	5.1
P.T.#1-2	(459.9) 460'	+2° 15'	P.O.T.	5.0	5.0
Elev. Pt 1					
B.M.					

Elev.
1023.7
1009.4
1020.9
1028.3
1040.5
1019.5
1022.5
1017.8
1035.5
1041.2
1057.80
1040.94
1039.79

See Book # 67

231' N.E. Jarvis school - on back N.E. car road

Pt	Dist	Ver A	Horz	HI	Rod
	(884.8)				
12-15	886'	+2°08'	P.O.T.	5.1	5.1
Pt 12-14	416'	+0°01'	P.O.T.	5.1	5.1
	(123.7)				
12-13	123'	-2°46'	91°27'±	5.1	5.1

See book # 671

1056.7

1023.8

1017.8

Protile Pass #1

B.M. x 0+00	0.21	1446.65 ✓		1446.42
T.P.	0.43	1434.11 ✓	12.95	1433.68 ✓
-1+56			13.0	21.1 ✓
-0+66			5.1	29.0 ✓
B.M.	5.20	1474.85 ✓		1469.65 ✓
0+95			6.3	68.6 ✓
1+25			5.2	69.7 ✓
1+57			7.7	67.2 ✓
B.M.	0.91	1447.33 ✓		1446.42
2+85			0.9	46.4 ✓
3+15			7.6	59.7 ✓
T.P.	1.52	1435.84 ✓	13.01	1434.32 ✓
3+65			1.5	34.3 ✓
5+05			14.0	1421.8 ✓

Hub set at weir elev. S. side of saddle

Hub set at top of saddle

Hub set at weir elev. N. side of saddle

3+15 = bot. of gully - gully makes angle of about 30° R.

bot of gully

Profile of Pass # 2

BM. 70+00	0.32	1446.74		1446.42
TP.	0.71	1434.45	1300	1433.74
-1+03			13.4	21.1
-0+70			0.7	33.8
BM.	463	1470.41		1465.78
0+86			4.8	63.6
1+11			4.6	63.8
1+67			10.1	60.3
BM	0.32	1446.74		1446.42
2+22			0.3	46.4
TP	0.39	1434.17	1296	1433.78
3+00			13.2	21.0

Hub at S. end of pass, weir elev. = 0+00

Hub set at top of saddle

Hub set at N. end of pass, weir elev.

Profile of Pass #3

B.M.	1.63	1394.41		1392.78
TP.	0.71	1384.20	10.22	1383.49
0+00			13.0	71.2
0+50			3.0	81.2
B.M.	1.20	1393.99		1392.78
1+50			1.2	92.8
1+91			5.1	88.9
TP.	0.72	1381.69	13.01	1380.97
2+50			4.8	76.9
3+00			13.9	67.8

Hub set at top of saddle

State route Dulzura PL - stadia survey
 Dulzura weir to Lrtg. (Green route) Rods
 Point to Point Dist Mag. B. Horiz. Vert. Δ HI

π 3 to 4 192 NJ3° W 14° 16' RT - 0° 22' 9.1 rd
 (191) 4.7 rd
 π 182
 (181)

1309.5 W.M.
 π 1 to 3 1301.2 PORT. - 1° 08' 4.9
 (1310) 4.9
 1310.6

827.3 W.M.
 1 to 2 828.5 N48 W 1° 39' RT - 3° 18' 4.9
 (830)

861
 (800) N 51° W POT 40° 15' 12.1 Rod
 5.1

EL. of Pt. 0

5.1

Dulzura "Green Route"
 State

26
 Feb 10-49

Elev.

1416.0 W.M.
~~1416.2~~
 1415.5

1421.8
 1421.2
 1421.6 W.M.

1399.8 W.M.

1447.5 W.M.
 1447.6 1447.1

1450.9 U.S. G.S.

HEAVY Boulder formation
 Point 2 to Creek
 crossing

9408 354.6 W.H.
(357) POT -4°44'

π7609 645.9 W.H.
645.6
(649) N4°W 9°11'L -3°56' 4.9 RID
N 8°W 13°24'S 4.9 HI

π5407 2009.8 W.H.
2010 N.E. POT: -0°34' 5.0
(2010) 5.0

5406 1118.6 W.H.
(1130) N3°E 5°55'R -5°46' 5.0 RID
5.0 HI

π4605 106
(105) N0°30'W 32°21'N -0°22' 5.0
5.0

π4605 (A) 106
105 N0°30'W 32°21'N -0°22' 5.0
5.0

1321.2 W.H.

1350.5 W.H.
1392.2 1351.3
1351.0

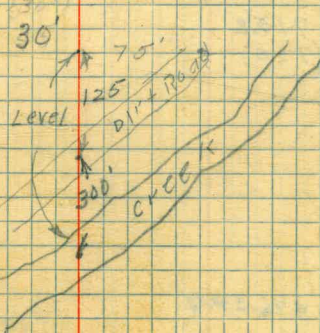
1395.8
1395.5
1394.9 W.H.

1302.0

1415.5

1414.8

Reddish ndbb scattered
out cropping of rocks
from creek to eastward
field at 20 page 21



1500 = 1300
500
7000

P to P	Dist	Mag. B	Horz. L	Vert L	Rod & H.I.
13 to 14	459.0 (170)		Pot.	-8° 48'	5.0 5.0
	339.5 W.N.				
11 to 13	341 (340)		Pot	-2° 18'	4.9 Rod 4.9 H.I.
	166.1 W.N. (175)		Pot	-13° 0'	4.9 Rod 4.9 H.I.
	714.0 W.N.				
9 to 11	715.2 (720)		Pot	-5° 14'	5.0 5.0 H.I.
	10.0 2.5				
9 to 10	476.3 W.N. (500)		POT	-12° 35'	5.0 5.0 H.I.

Elev.

1200.4 W.N.

1271.5 W.N.
1313.1 1272.3
1272.10

1246.7 W.N.

1285.1 W.N.
1326.7 1286.
1285.6

1244.2 W.N.

28

15 to 19 1376
(1375) POT $-0^{\circ} 22'$ 4.2 HT

700

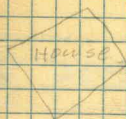
32° 14' + 5° 22' 127

15 to 17 372.3
(380) POT $-8^{\circ} 12'$

15 to 16 211.9 W.M.
(240) N46°W 32° 15' Lt. $-20^{\circ} 0'$
38° 02'

13 to 15 939.7 W.M.
936
(945) POT $+5^{\circ} 59'$ 5.0 HT

7030
31
40
1361.5
1341.2 ✓



150'

80'

1316.4 W.M.

1292.9 W.M.

1370.3
1370.0 ✓

23 to 22 260.3 W.M.A.
(280) POT -15° 24' 5.0 Rod

19 to 23 1281 ✓
(1280) POT -0° 22' 5.0 Rod

19 to 21 (500) ✓ POT +0° 08' 5.0 Rod

19 to 20 266.7 W.M.A.
(275) N31°W 15°11'R -10°0' 5.0 Rod

19 to 18 651.2 W.M.A.
(720) POT -18°0' 5.0 HT.
5.0 HT.

Creek

1281.3 W.M.A.

1353.3 ✓
1353.0 ✓

1362.4 W.M.A.

1314.2 W.M.A.

1149.6 W.M.A.

514
512
510

492.2 *W.M.*
28 to 27 (440) Pot -7°40'

1221.9 *W.M.*
1223
25 to 28 (1230) Pot -4°40' 5.0
5.0

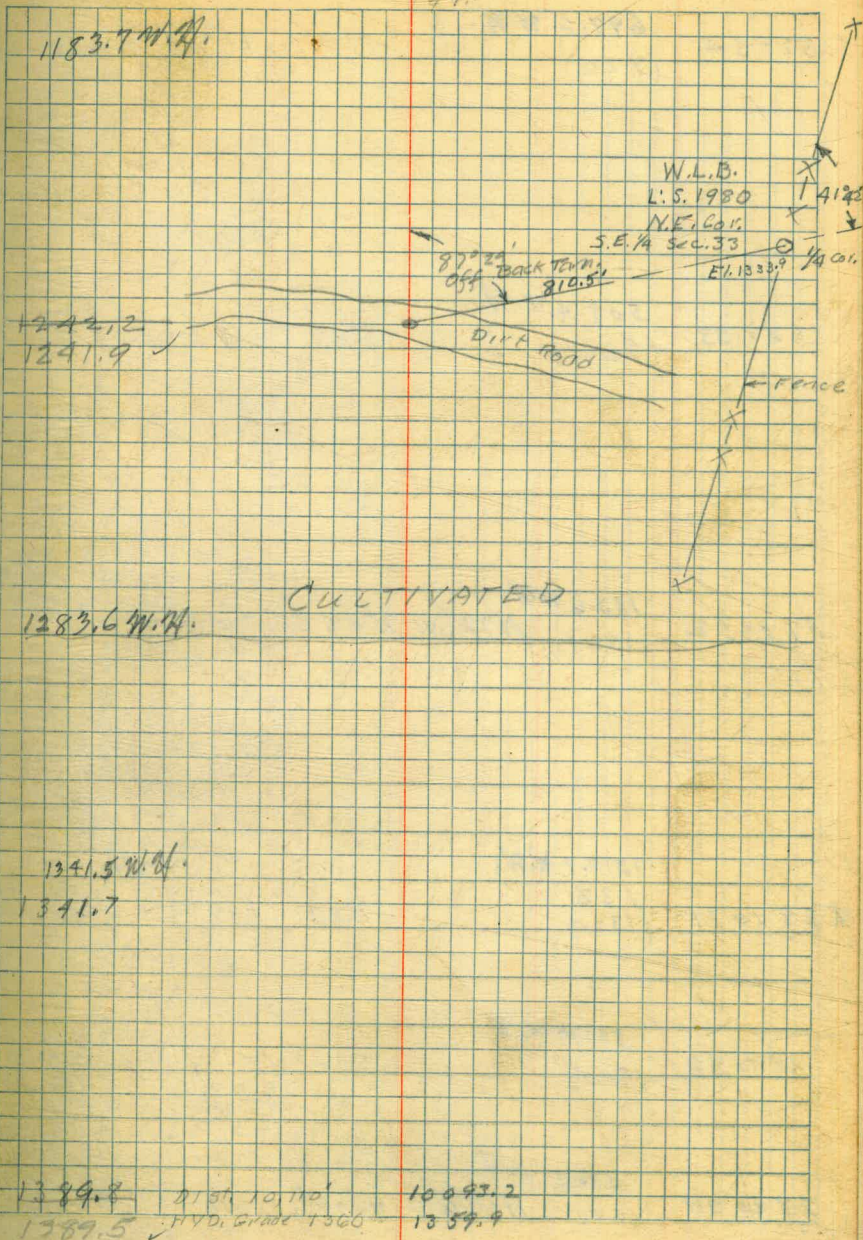
358.7 *W.M.*
25 to 26 (368) N60°W 7°1' R -9°10'

310.8^v
27 to 25 (318') N67°³⁰W 12°34' L -8°47' 5.0
5.0

280.4^v
23 to 24 (285) N55°W 24°11'_L +7°25' 5.3
5.3

182
87
99?

NE. Cor. of
S.E. 1/4 of Sec. 33 31



32 to 34 697.2 W.H.
(720) Pot -10° 15' 5.0
5.0

32 to 33 509.4 W.H.
(500) Pot -17 30' 5.0
5.0

31 to 32 183.6 W.H.
(186) N72¹⁰W 2° 45' 2 -6° 30' 5.0
5.0

28 to 31 1319.7 W.H.
1321
(1329) Pot +0° 46' 5.0
5.0

28 to 30 899.4 W.H.
(900) Pot -1° 31' 5.0
5.0

28 to 29 280.5 W.H.
(287) N69³⁰W 9° 09' 2 -8° 41' 5.0
5.0

1112.6 W.H.

1078.1 W.H.

1238.7 W.H.

1260.0
1259.6 ✓

1218.1 W.H.

1199.1 W.H.

REDDISH DOGS WITH SCATTERED
OUT CROPPERS

210'

CULTIVATED

DIKT Road

137
9.2 1300
1120

38 to 39 902.2 W.M.
(920) N 72¹⁶ W 22° 11' L -8° 0' 5.0
5.0

36 to 38 1751 ✓
(1750) POT -0° 13' 5.2
5.2

36 to 37 1111.7 W.M.
(1125) N 50° W 22° 11' R -6° 15' 5.0
5.0

31 to 36 2161 ✓
(2160) N 71° W POT -0° 22' 5.0
5.0

32 to 35 1065.1
(1100) POT -10° 15' 5.0
5.0

1112.4 W.M.

1239.6 16.888 dist.
1239.2 ✓ 1120.9100 = 1346.1

1124.1 W.M.

1245.8 ✓
1246.2 Point 256 should be moved up feedback
(to right) about 300' in dist. = 175' in elev.
W.M.

1046.1 W.M.

55
502
788

43 to 44 592.5
(596) N51°W POT -4°22' 5.0
22°06' 5.0

704.8 W.A.
705.8
41 to 43 (705) N51°W 22°06' +1°01' 5.1
POT 5.1

319.5 W.A.
41 to 42 (320) N73°W 0°28' -2°27' 5.1
5.1

1691
38 to 41 (1690) POT +0°20' 5.0
5.0

1003.4
38 to 40 (1020) POT -7°20' 5.0
5.0

1228.2 W.A.

Cultivated

198'

1251.4
1261.5 ✓

1232.3 W.A.

1249.6 W.A.

1247.9
12440. ✓

DIRT ROAD

DIRT ROAD

50'

110.1 W.A.

150'

898.8 W.M.
 899.7
 (900) POT +2° 10' 4.9
 4.9

should be after #49
 518.6 W.M.
 49 to 48 (520) POT -3° 05' 4.9
 4.9

194.7 W.M.
 47 to 46 (195) POT -2° 27' 4.5
 4.5

2096 W.M.
 43 to 47 2098 (2100) POT -2° 28' 5.0
 5.0

1517.3 W.M.
 43 to 45 (1520) POT -2° 33' 5.0
 5.0

1205.2
 1205.1 106.0'

1177.3 W.M.

1156.4

1174.2

1171.1

1198.3 W.M.

Reddish stone
 with scattered
 but droppings

CULTIVATED

D.G. Road

2133 = off Back Tan

Cor of Doby Ranch
 Mon
 near center sec 29

TOPO MAP
 WE MAKE at 1176

75'

Cultivated

π 52 to 54 \checkmark
 302
 (301) POT -0° 48' 4.9
 4.9

52 to 53 \checkmark
 167.2 W.H.
 (169) N14° W 23° 14' R -5° 52' 12.1
 4.7

π 51 to 52 \checkmark
 213
 (212) N37½° W 2° 36' R 0° 00' 4.8
 4.8

π 49 to 51 \checkmark
 466.1 W.H.
 467.7
 (468) N34½° W POT +3° 39' 4.9
 4.9

49 to 50 \checkmark
 (266) N34½° W 15° 58' R +1° 20' 9.9
 4.9

\checkmark
 111
~~113~~
~~115~~
~~117~~

1210.3 W.H.
~~1232.2~~

\checkmark
 1234.9
~~1236.5~~

\checkmark
 1234.9
~~1236.5~~

1206.4 W.H.

1200
500
700

1200
6.7
6.3

58 to 59 278.7
(287) N58°W 4°07'L -9°46' 5.1
5.1

58 to 57 165.9 W.H.
(167) Pot -4°43' 5.1
5.1

54 to 58 1661 ✓
(1660) POT 10°04' 5.0
5.0

54 to 56 776.2 W.H.
(800) POT -9°56' 5.0
5.0

54 to 55 608.1
(630) N54°W 39°34'R +10°45' 5.0
5.0
39°34' Lt W.H. in office

10
5.45
10.55

37

1184.7 W.H.

1219.0 W.H.

1232.7 ✓

1230.2

29.929 Tot dist
Hvd sp. 12.692

1094.8 W.H.

1115.3 W.H.

1200
1073
287
940
910
3

π 63 to 64 391 ✓
(390) N 79° W 1° 47' R+ - 0° 05' 4.9
4.9

101.8 W.H.
 π 62 to 63 102.8 ✓
(102) N 20½° W 37° 27' R+ + 2° 45' 5.0
5.0

π 58 to 62 1040 ✓
(1039) POT - 0° 26' 5.1
5.1

607 W.H.
58 to 61 (610) POT - 4° 08' 5.1
5.1

407.3 W.H.
58 to 60 (410) POT - 4° 45' 5.1
5.1

1229.1 W.H.

~~1226.3~~
~~1226.6~~

1229.7 W.H.
~~1226.9~~
~~1227.2~~

1229.8 W.H.
~~1222.1~~ 7
~~1222.3~~

1188.8 W.H.

1198.9 W.H.

1387.4 W.H.

64 to 67

1389
(1370)

POT -2° 15' 5.0
5.0

1650
210
7560

1174.5 W.H.

39

1171.8
~~1172.1~~

Tot. dist
M.D.

27821.0
9m. = 1245.5

64 to 66 564.8
(570)

POT -5° 30' 5.0
5.0

1174.7 W.H.

64 to 65 342.7 W.H.
(345)

N60°W 41°25' L - 4°40' 5.0
5.0

1201.1 W.H.

HENRY Boulders Number 045 outcroppings

366.8
 71 to 72 (379) N 34° W 36° 50' R -10° 20' 4.8
 4.9

1217.7 W.M.
 67 to 71 (1220) POT +2° 30' 4.8
 4.9

67 to 70 (800) POT -8° 10' 4.8
 4.9

551.3 W.M.
 67 to 69 (560) POT -7° 15' 4.8
 4.9

297.9 W.M.
 67 to 68 (300) N 71½° W 10° 34' L -4° 51' 4.8
 4.9

1160.8 W.M.

1227.7 W.M. X
 1325.0 X
 1225.5 X
 HYD. 11237.6 X

1260

102° 41' off Back ton

1172.2 W.M.

1104.4 W.M.

1149.2 W.M.

09 21

04 5

05 5

75 to 77

473.4 ~~W.H.~~
(475)685
1600
915
POT -3° 23'4.6
4.6

75 to 76

315.7 ~~W.H.~~
(220)

N 32° W 2' 28" R -8° 0'

4.6
4.6

71 to 75

1511
(1510)

POT -0° 22'

4.8
4.8

71 to 74

1124.9 ~~W.H.~~
(1130)

POT -3° 52'

4.8
4.8

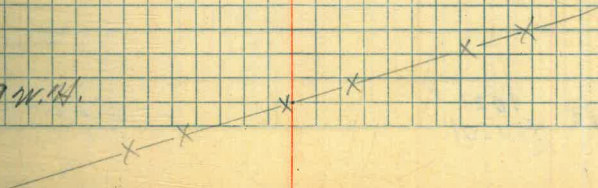
71 to 73

911.6 ~~W.H.~~
(915)

POT -3° 34'

4.8
4.81190.0 ~~W.H.~~

1187.7

1218.0 ~~W.H.~~1215.3
1215.61151.7 ~~W.H.~~1170.9 ~~W.H.~~

131
37
54

81 to 82 185.3 W.M.
(195) POT -12°53' 4.7
4.7

80 to 81 569.9 W.M.
(570) POT -0°58' 4.6
4.6

Should be
Horo
at
W.M.

80 to 79 609.5 W.M.
(740) N 61°W 22°47' L -24°50' 4.6
4.6
Should be POT. by W.M.

1142.8 W.M.
X 78 to 80 1143.9 N 38°W 5°46' RT -0°47' 4.5
(1143) 4.5
5°46' L. W.M. in office

X 75 to 78 1021
(1020) -0°22' 4.6
4.6

1143.8 W.M.

1186.2 W.M.

913.8 W.M.

1193.5

1195.8 W.M.

1211.5 W.M.
1208.8
1209.1

Reddish rubble scattered out
Crappings boulders

CREEK

857887 479.7
(495) POT -10°09' 4.5
4.5

857886 307.5
(330) N54°W 6°26'R -15°07' 4.5
4.5

857889 313.5
(320) POT -8°15' 4.5
4.5

807885 1371 ✓
(1370) POT +0°08' 4.6
+0°46' 4.6

817883 329.7
(303) POT -1°49' 4.7
4.7

1113.3 ~~W.N.~~

1115.9 ~~W.N.~~

1152.1 ~~W.N.~~

1199.0 ~~W.N.~~
1196.3
1195.9

Road to Lyons Valley

1176.6 ~~W.N.~~

335.1 M.H.
 91T092 (360) S 85°W 42°18' L -15°15' 4.5
 4.5

333.6 M.H.
 91T090 (336) POT -4°56' 8.5
 4.5

1487.2 M.H.
 85T091 1698.1
 (1700) POT -2°29' 4.5
 1490 4.5

923.9 M.H.
 85T089 (925) POT -2°06' 4.5
 4.5

557.7 M.H.
 85T088 (580) POT -11°18' 4.5
 4.5

1043.2 M.H.

67507

1102.3 M.H.

Dirt Road

1134.5 M.H.
 1132.1
 1122.3

1165.1 M.H.

1087.6 M.H.

204.8 W.H.
 97 T 098 (205) N 80¹/₄° W 1° 54' R - 2° 01' 5.0
 5.0

514 V
 95 T 097 (515) POT 72° 36' 5.0
 5.0

243.1 W.H.
 95 T 096 (255) N 82¹/₂° W 18° 52' R - 12° 30' 9.0
 5.0

824.3 W.H.
 94 T 095 (835) S 79° W 5° 47' LT + 6° 39' 6.0
 5.0

1071.8 W.H.
 91 T 094 (1072.8 / 1080) POT -5° 0' 4.5
 4.5

507.6 W.H.
 91 T 093 (380) POT -19° 59' 13.5
 549 4.5

15 90
 13 18
 2 72
 5 19
 45

1151.7 W.H.

1159.1 W.H.
 1157.7
 1158.9 1146.8 338'

1077.9 W.H.

1135.8 W.H.

1134.4

1124.5

Top disk 36,857.5 This point
 Hyd. pt. 11,872 Should be 117
 The ridge Motherly
 Approx 200' and 25'
 higher

1040.8 W.H.

1038.4

1028.5

85

989.7 W.H.

El. 1007 Topo MGP
 El. 1017.4 WEMAKE
 9.96.2 RECHECK

VERY ROCKY FROM CHECK

1640
99T0106 (1640) POT -0°21' 4.6
1650

565.8 W.M.
102T0105 572 POT -6°0' 4.6

455.4 W.M.
102T0104 (459) POT -5°03' 4.6

139.2 W.M.
102T0103 (144) POT -10°30' 4.6

SEE Ahead for 99T0106
408.6 W.M.
99T0102 (410) POT -3°22' 4.6

108.2 W.M.
99T0101 (110) POT -7°28' 4.6

73 W.M.
99T0100 (84) N 89°40' W 9°31' L -21°15' 4.6

564 ✓
97T099 (564) POT +0°46' 5.0

1156.6 W.M.

1155.2
1135.7

1083.2 W.M.

1102.9 W.M.

1116.9 W.M.

1142.7 W.M.

1152.6 W.M.

1198.3 W.M.

1166.7 W.M.

1165.3

1146.2

1180.4 W.M.

Readjust above track numbers
on recordings of large Bou Aniers

111 to 113	580.8 W.M. (581)	POT $+1^{\circ} 09'$	4.9 4.9
111 to 112	344.9 W.M. (346) $57^{\circ} 52' W$	$18^{\circ} 15' 30'' R - 3^{\circ} 15'$	4.9 4.9
109 to 111	859.8 W.M. (865) 860	POT $-0^{\circ} 58'$	4.5 4.5
108 to 110	569.8 W.M. (570)	POT $-1^{\circ} 11'$	4.5 4.5
	Exchange distances		
108 to 109	444.4 W.M. (448)	POT $-12^{\circ} 0'$	4.5 4.5
106 to 108	641.5 W.M. (642)	POT $-1^{\circ} 39'$ $-1^{\circ} 40'$	4.7 4.7
106 to 107	303.8 W.M. (315) $557^{\circ} W$	$31^{\circ} 38' L - 10^{\circ} 51'$	6.7 4.7

1135.3 W.M.

1104.0 W.M.

1123.6 W.M.

1122.2

1102.4

1122.0 W.M.

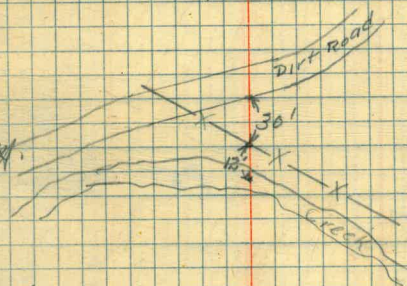
1022.2 W.M.

1138.1 W.M.

1136.7

1117.0

1096.4 W.M.



120 TO 119 387.0 W.W. POT -5°0' 8.0
(390) 5.0

SEE Ahead for #117 TO #121

117 TO 120 (919) POT -3°29' 5.0
5.0

117 TO 118 154.2 W.W. POT 5.0
(155) N 73¹⁰ W 10°00'30" -4°15' 5.0

117 TO 116 144.5 W.W. POT -9°58' 5.0
(149) 5.0

114 TO 117 754 POT 20°23' 5.1
(751) 5.1
755 ✓

114 TO 115 (371) N 63° W 41°57'30" R +0°34' 5.1
5.1

111 TO 114 895.1 W.W. POT 43°15' 4.9
(878) 4.9
895.0 ✓

1076.6 W.W.

1113.5 W.W.

1157.8 W.W.

1143.9 W.W.

1149.3 W.W.
1167.9
1148.0

1178.1 W.W.

1174.4 W.W.
1173.0
1153.2

CALCULATED

1269.5 M.H.

1268.7
1270
K 122 TO 126

POT $-1^{\circ}12'$ 4.8
 $-1^{\circ}13'$ 4.8

845.1 M.H.

122 TO 125 (855)

POT $-6^{\circ}15'$ 4.8
4.8

712.6 M.H.

122 TO 124 (720)

POT $-5^{\circ}58'$ 4.8
4.8

429.3 M.H.

122 TO 123 (445)

POT $-10^{\circ}50'$ 4.8
4.8

280.5 M.H.

282.5
K 121 TO 122 (283) ✓

POT $-5^{\circ}25'$ 5.0
 $-5^{\circ}28'$ 5.0

K 117 TO 121

1111.2
1115 ✓

POT $-3^{\circ}23'$ 5.0
5.0

1050.5 M.H.

1049.1
1028.4

~~1114 Road~~

984.5 M.H.

CREEK

1002.6 M.H.

994.9 M.H.

POT 1114/115

1077.0 M.H.

1075.6
1055.5

1103.6 M.H.

1102.2
1082.3

13170133 240.8 W.H.
(245) POT -7° 52' 4.8
4.8

13170132 (20) POT —

13170130 115.7 W.H.
(116) POT +2° 39' 4.8
4.8

126 TO 131 1520.6 W.H.
1537.6
(1550) POT -2° 42' 5.0
-2° 45' 5.0
1524

126 TO 129 1039.4 W.H.
(1060) POT -8° 0' 5.0
5.0

126 TO 128 727.4 W.H.
(750) POT -10° 0' 5.0
5.0

126 TO 127 299.1 W.H.
(315) POT -13° 0' 5.0
5.0

946.9 W.H.



984.1 W.H.

978.7 W.H.
977.3
954.0

904.9 W.H.

922.2 W.H.

981.5 W.H.

Calculated

1676.6 M.H.

1680

136 TO 139

16519
(1655)

POT

+2°33' 5.1
5.1

1159.8 M.H.

136 TO 138

(1160)

POT

-0°45' 5.1
5.1

542.6 M.H.

136 TO 137

(550)

POT

-6°45' 8.1
5.1

304.3 M.H.

136 TO 135

(305)

POT

-2°47' 5.1
5.1

1332.7 M.H.

131 TO 136

13368
(1341)
1336

POT

-2°51' 4.8
1.8

520.6 M.H.

131 TO 134

(522)

POT

-2°57' 4.8
1.8

987.1 M.H.

985.6
984.7

897.1 M.H.

845.1 M.H.

897.5 M.H.

912.3 M.H.

911.0
~~909.2~~

951.9 M.H.

51

Reddish Adobe
Some outcroppings
large boulders.

Creek

Tilled pasture
to creek.

142 TO 145 (1180) POT — 5.0
5.0

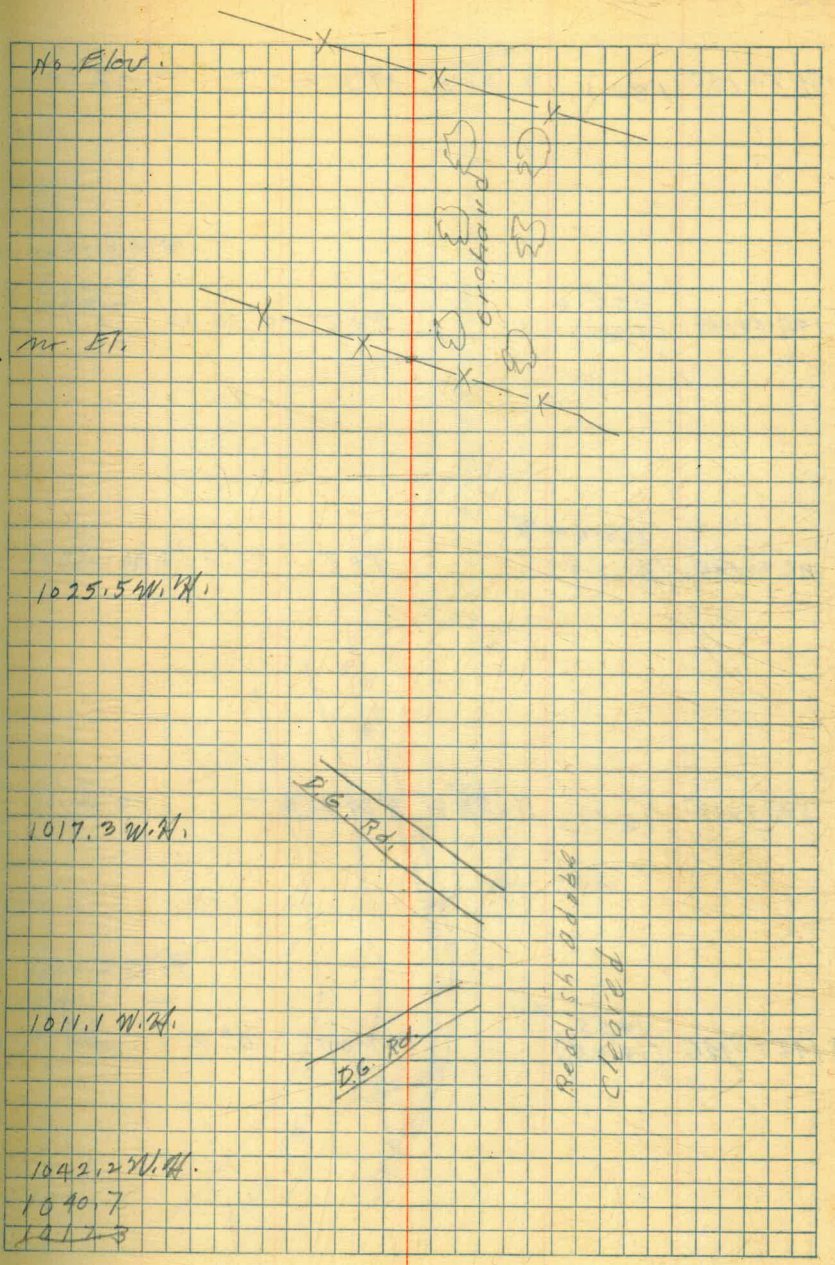
142 TO 144 (960) POT — 5.0
5.0

497.5 W.H.
142 TO 143 (500) N63¹⁰W 9°57'30"R -1°55' 5.0
5.0

167.5 W.H.
142 TO 141 (171) POT -8°28' 5.0
5.0

289.7 W.H.
142 TO 140 (293) POT -6°08' 5.0
5.0

649.3 W.H.
555.3
X 139 TO 142 (660) POT +1°51' 5.0
654 5.0



149 TO 150 (180) N 75³⁰ W 14°35' L ← 5.0
5.0

146 TO 149 (935) 935 ✓ POT -0°30'30" 5.1
(935) 5.1

146 TO 148 (561) 560.4 m.H. POT -1°57' 5.1
(561) 5.1

146 TO 147 (164) N 60³⁰ W 2°39'30" R ← 5.1
(164) 5.1

142 TO 146 (1955) 1955 ✓ POT 0°0' 5.0
(1955) 5.0

no Elev

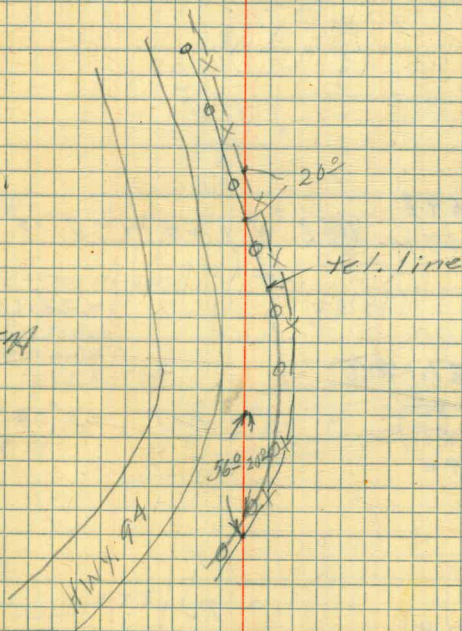
1032.9 m.H.
1032.4
~~1009.0~~

1023.1 m.H.

No E/OV.

1042.2 m.H.
1040.7
1017.3

CALCULATED FROM FENCE



SEE Ahead for 152 TO 160

1234.8
152 TO 158 (1238) POT -2° 54' 5.1
5.1

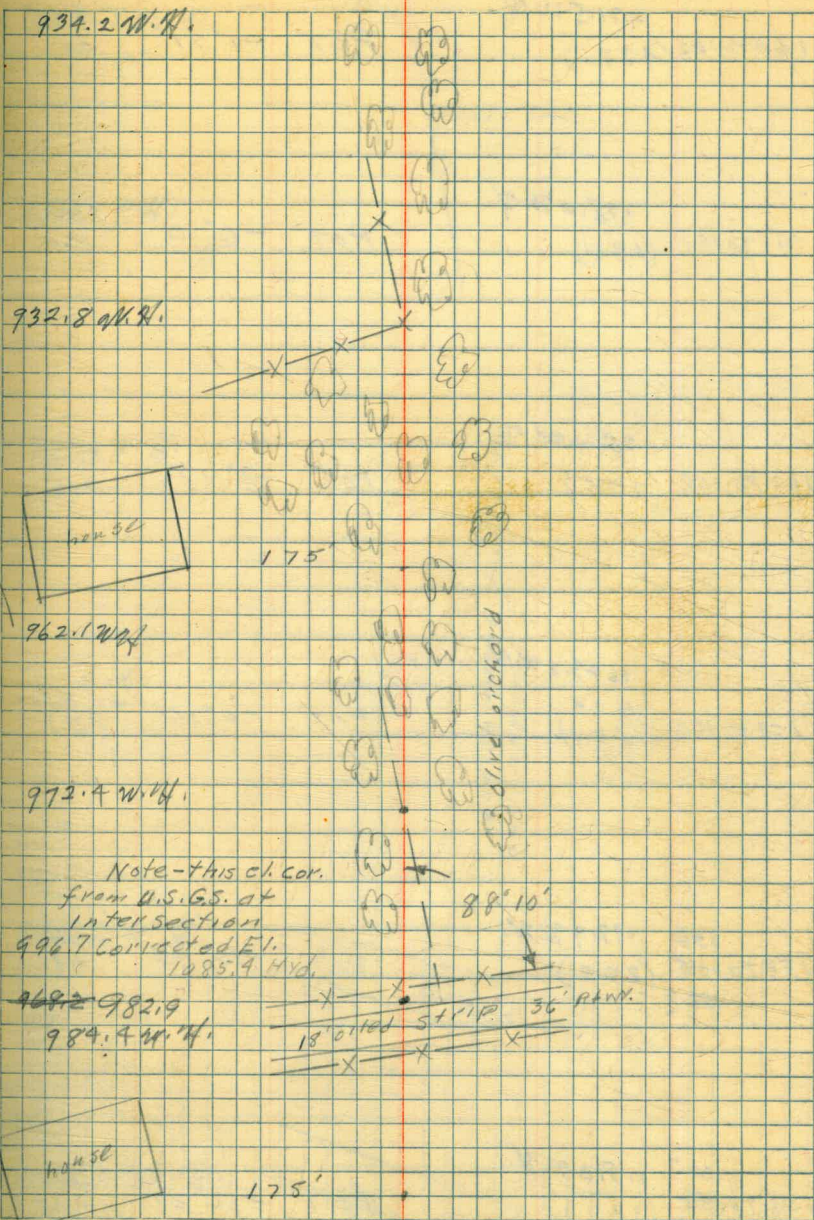
674.1 W.M.H.
152 TO 153 (680) POT -5° 25' 3.1
5.1

376.9 W.M.H.
152 TO 151 (380) POT -5° 15' 5.0
5.0

364.8
152 TO 153 (267) N68° W 7° 16' 30" RT. -5° 15' 5.0
5.0

787.1 W.M.H.
149 TO 152 (788) POT -3° 36' 5.0
790 5.0

149 TO 151 (219) POT



ht. Elev

471.5 W.H.
 160 to 182 (472) POT $-1^{\circ}51'$ 5.0
 5.0

178.0 W.H.
 160 to 161 (180) POT $-6^{\circ}0'$ 13.0
 5.0

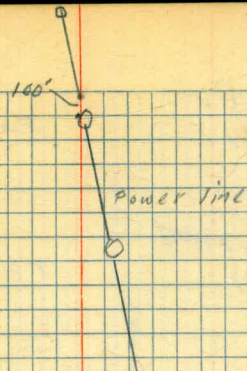
251.0 W.H.
 160 to 159 (255) POT $-7^{\circ}17'$ 13.0
 5.0

1623.8 W.H.
 152 to 160 (1624) POT $-0^{\circ}30'$ 5.1
 5.1

156 197.9 W.H.
 158 to 155 (205) POT $-10^{\circ}15'$ 8.8
 156? 4.8

157 115.3 W.H.
 158 to 156 (121) POT $-12^{\circ}29'$ 9.7
 157 4.8

964.5 W.H.



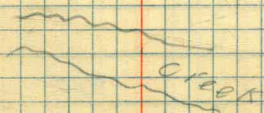
953.0 W.H.

939.6 W.H.

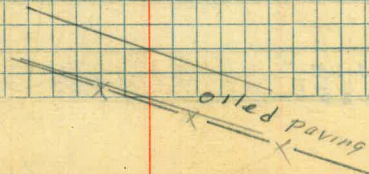
779.7

reddish Adobe few large
 outcroppings

892.6 W.H.



908.7 W.H.



165 to 169 $\frac{1164.5}{(1165)}$ ✓ POT +1° 10' $\frac{5.0}{5.0}$

166 to 168 $\frac{644.3}{(645)}$ W.H. POT +1° 50' $\frac{4.8}{4.8}$

166 to 167 $\frac{319.5}{(325)}$ POT -7° 34' $\frac{10.8}{9.8}$

165 to 166 $\frac{244.6}{(245)}$ W.H. POT -3° 19' $\frac{18.0}{5.0}$

164 to 163 $\frac{248.1}{(250)}$ W.H. POT -5° 0' $\frac{5.0}{5.0}$

165 to 169 $\frac{(116)}{(116)}$ ✓ POT -0° 18' $\frac{5.0}{5.0}$

160 to 165 $\frac{1025}{(1025)}$ ✓ POT -0° 14' $\frac{5.0}{5.0}$

999.3 ✓

973.6 W.H.

904.6 W.H.

953.0 W.H.

953.2 W.H.

974.9 W.H.

975.5 ✓

reddish above few 1492 outcrops

175 TO 176 136.9 W.M.
(156) N 74 1/2 W 5° 29' 30" R - 10° 30' 11.9
4.9

169 TO 175 1490 ✓
(1490) POT 0° 0' 3.9
4.9

172 TO 174 545.5 W.M.
(565) POT +10° 43' 4.8
4.8

172 TO 173 212.7 W.M.
(220) POT -10° 30' 4.8
4.8

171 TO 172 (150) ✓ POT +0° 12' 11.0
5.0

171 TO 170 138.2
145' POT -12° 32' 4.9

SEE Ahead for #169 TO #175
432.1 W.M.
169 TO 171 (441) N 80° W 12° 05' L - 8° 09' 4.9
4.9

940.1 W.M.

978.3 1044.5

1035.1 W.M.

892.5 W.M.

931.9 W.M.

906.7 W.M.

937.4 W.M.

VERY ROCKY from fence
NUMEROUS outcroppings
heavy boulders

X X X
10'

X
X
X
69'

Reddish adobe
outcroppings

856.6 W.M.
 T 178 858.7
 175 TO 183 (863) POT -4°56'30" 5.0
 5.0

493.4 W.M.
 179 TO 182 (560) POT -20°10' 11.1
 5.1

239.7 W.M.
 179 TO 181 (268) POT -18°58' 5.1
 5.1

157.2 W.M.
 179 TO 180 (190) POT -24°32' 9.1
 5.1

178 TO 179 (52) N49°W 25°31'15"R 0.0 11.0
 5.0

609.8
 T 175 TO 178 (610) POT -1°02'30" 5.9
 4.9

175 TO 177 (499) POT -0°29' 4.9
 4.9

911.9 ✓

793.0 W.M.

898.0 W.M.

904.4 W.M.

980.2 W.M.

986.2 ✓

994.1 W.M.

VERY ROCKY NUMEROUS OUTCROPPINGS

271.9 W.H.
188 TO 189 (272) N 64° W 14° 48' L +0° 52' 9.2
5.2

1494.9 W.H.
183 TO 189 (1495) POT +1° 35' 4.8
4.8

1161.4 W.H.
183 TO 187 (1170) POT -1° 55' 4.8
4.8

384.4 W.H.
185 TO 186 441 POT -21° 0' 4.9
4.9

433.2 W.H.
183 TO 185 (439) POT -6° 37' 4.8
4.8

208 W.H.
183 TO 184 (220) POT -13° 30' 4.8
4.8

27.6
13.7
41.3

59

953.3 W.H.

953.2 ✓
Avg. 1034.6
Tot. Dist
60534.6

812.0 W.H.

714.0 W.H.

861.6 W.H.

862.5 W.H.

VERY POORLY MARKED
NUMBERS OUTCROPPING
HEAVY BANKERS

941.8 W.H.
192T196 (952) POT -5°55'30" 5.2

838.9 W.H.
192T0195 (850) POT -7°10' 5.2

651.2 W.H.
192T0194 (685) POT -12°50' 5.2

498.5 W.H.
192T0193 (500) 568° W 47°51' L -17°45' 5.2

147.7 W.H.
192T0191 (153) POT -10°43' 5.2

846.6 ✓
188T0192 (848) POT +2°21' 5.2

441.3
188T0190 (442) POT +2°15' 5.2

~~890.3~~
~~890.8~~

882.8 W.H.

839.6 W.H.

842.8 W.H.

960.0 W.H.

988.0 W.H.
987.5
~~988.1~~

970.5 W.H.

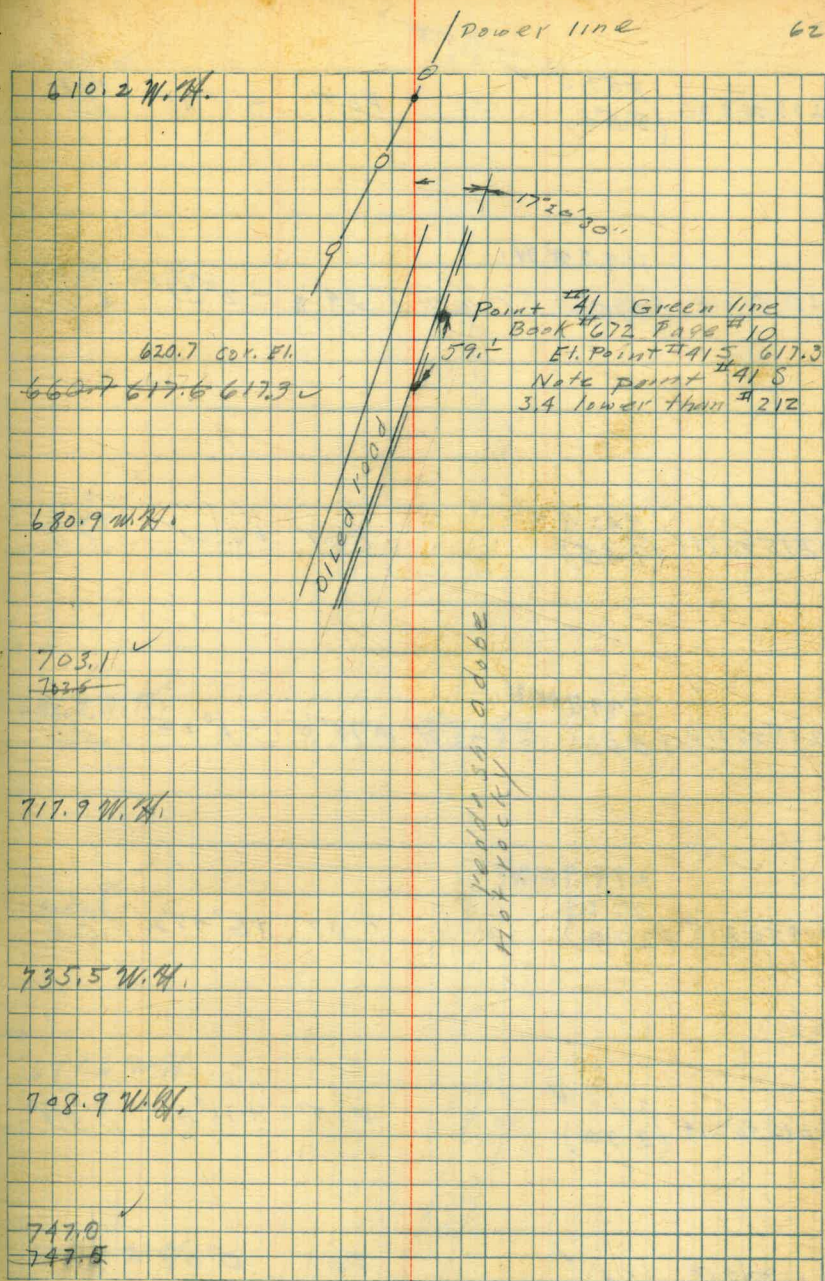
VERY ROCKY

199 TO 204	999.2 W.H. (1003)	POT -3° 33'	5.2 5.2
199 TO 203	864.9 W.H. (875)	POT -6° 13'	5.2 5.2
199 TO 202	731.5 W.H. (741) 741	POT -6° 31'	7.2 5.2
199 TO 201	409.3 W.H. (424)	POT -10° 43'	5.2 5.2
199 TO 200	204.7 W.H. (238)	POT -21° 58'	5.2 5.2
196 TO 199	473.0 W.H. 473.2 (490)	POT -10° 44'	5.4 5.4
196 TO 198	207.9 W.H. (215)	POT -10° 53'	11.4 5.4
196 TO 197	80.2 W.H. (83)	POT -10° 50'	5.4 5.4

738.5 W.H.			
706.3 W.H.			
715.0 W.H.			
723.0 W.H.			
717.9 W.H.			
800.5 ✓ 801.7 ✓			
844.3 W.H.			
875.3 W.H.			

Very rocky reddish silt

213T0211	304.8 W.H. (305)	POT -1° 20'	5.1 5.1
209T0212	723.8 W.H. 724.1 (734)	POT -6° 45' 30"	5.0 5.0
209T0210	194.5 W.H. (197)	POT -6° 30'	5.0 5.0
206T0209	502.2 ✓ (506)	POT -5° 0'	5.1 5.1
206T0208	276.9 W.H. (280)	POT -6° 0'	5.1 5.1
206T0207	119.9 W.H. (121) 568 ¹⁰ W 0° 23' R - 5° 30'		5.1 5.1
206T0205	239.0 W.H. (245)	POT -9° 03'	5.1 5.1
199T0206	1353.8 W.H. 1354.1 (1356)	POT -2° 16'	5.2 5.2



857.5 ✓
217 TO 220 (858) POT -1°25' 4.7
4.7

169.7 W.H.
217 TO 218 (170) 589 $\frac{1}{2}$ W 7°34' R -2°31' 4.7
4.7

942.4 ✓
215 TO 217 (945) POT +3°09' 5.0
5.0

549.7 W.H.
215 TO 216 (550) 582 $\frac{1}{2}$ W 14°19' R -1°22' 5.0
5.0

274.9 W.H.
214 TO 215 (272.3) POT +6°47'30" 5.0
(276) 5.0

262 ✓
212 TO 214 (272) POT +11°0' 5.1
5.1

212 TO 213 (64) ✓ POT 0°0' 8.1
5.1

735.4
2346

744.1 W.H.

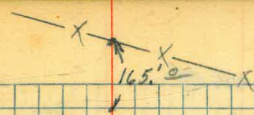
756.6 ✓
758.8

691.7 W.H.

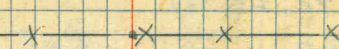
704.8 ✓

676.6 W.H.
672.4

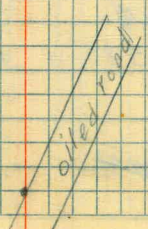
674.3 W.H.



reddish Adobe
Hockey



reddish
Adobe



10.00
14.00
365

233 TO 232	393.3 W.H. (415)	POT -13° 13'	8.1 5.1
233 TO 231	549.1 W.H. (555)	POT -5° 54'	5.1 5.1
233 TO 230	723.3 W.H. (730)	POT -5° 29'	9.1 5.1
229 TO 233	878.2 W.H. 878.4 (882)	POT +3° 46'	5.1 5.1
227 TO 229	522.7 W.H. 522.9 (523)	POT -1° 18'	5.2 5.2
227 TO 228	276.4 W.H. (280) S69 ¹⁰ W 15° 41'E	-6° 35'	5.2 5.2
227 TO 225	427.2 W.H. (430)	POT -4° 40'	5.2 5.2

685.6 W.H.
724.2 W.H.
707.5 W.H.
780.1 ✓
723.1 ✓ 722.3
703.0 W.H.
700.0 W.H.

reddish adobe
large but crumbling

318.1 ✓
T 239 TO 240 (338) POT -9° 52' 5.1
5.1

772 ✓
T 238 TO 239 (786) N 89½° W 41° 40' - 7° 40' 5.1
N 74° W 41° 40' Rte. by mt. H. in office 5.1

696.9 ✓
T 236 TO 238 (715) POT -9° 14' 5.1
5.1

354.9 W.H.
236 TO 237 (270) S 48½° W 20° 39' - 13° 42' 7.1
5.1

211.1 W.H.
236 TO 235 (220) POT -11° 37' 13.1
5.1

306.4 W.H.
236 TO 234 (310) POT -6° 11' 5.1
5.1

474A ✓
T 233 TO 236 (475) POT +2° 01' 5.1
5.1

66
523.3 ✓
522.6

580.5 ✓
579.6

684.4 ✓
683.6

733.2 W.H.

745.9 W.H.

764.1 W.H.

797.3 W.H.

797.6
796.8

No rocks
5900 451 PPA 1

Keddish rocks
5900 451 PPA 1

1885.9 M.M.
 2240 TO 2243 1886.7
 (1910) POT -6° 26' 5.1
 (1730) 6° 21' 5.1
 1719.2

988 M.M.
 240 TO 242 (1031) POT -11° 47' 5.1
 5.1

690.5 M.M. VO
 240 TO 241 (720) POT -11° 41' 5.1
 5.1

860 855
 1730 1710

755

62

316.6 ✓
 309.9
 330.5

Bridge U.S. HWY. 9A

Tot. dist 74931 Hvd. 941.7

Levels from U.S.G.S. B.M. El. 338
 make this point El. 315.9

317.2 M.M.
 Sweetwater River

380.5 M.M.

Line Revision from Point # 290

243 to 246 (1320) Pot $+14^{\circ}40'$ 5.2

243 to 245 (640) Pot $+7^{\circ}41'$ 5.2

243 to 244 (346) Pot $+4^{\circ}30'$ 5.2

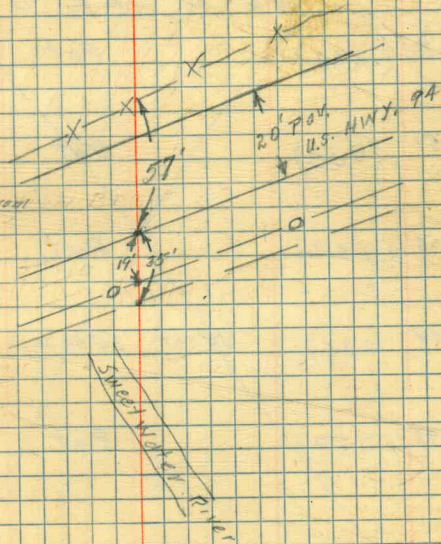
240 to 243 (1816) Pot $-5^{\circ}59'$ 5.1

240 to 242 (900) Pot $-11^{\circ}50'$ 5.1

240 to 241 (700) N $80\frac{1}{2}^{\circ}$ W $10^{\circ}58'$ R $-11^{\circ}45'$ 5.1
N $63\frac{1}{2}^{\circ}$ W

631.0

320.0 Corrected el. from
334.0 B.M. Page 67



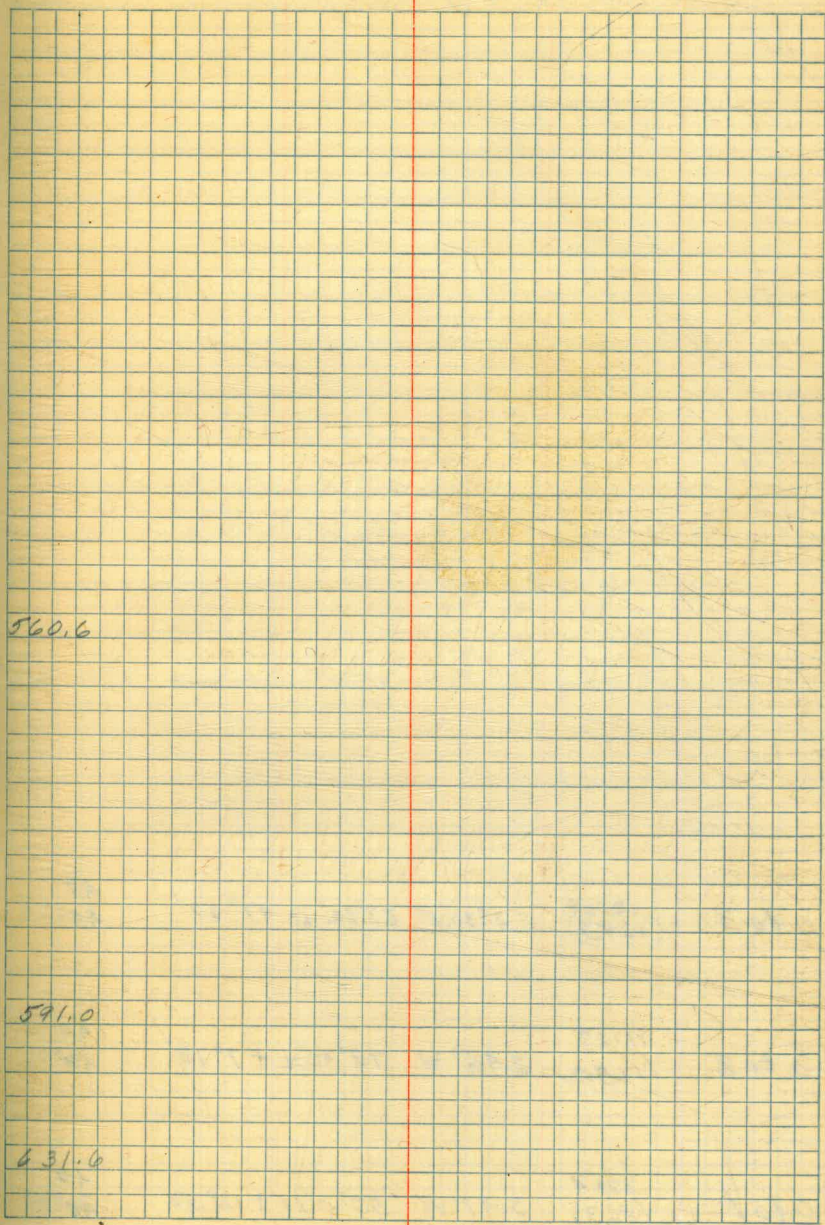
VOID SEE BOOK 678 Page 1

T 247 to 252 (1262)	Pot	-1° 23'	5.0	5.0
247 to 251 (930)	Pot	-2° 52'	5.0	5.0
247 to 250 (552)	Pot	-4° 57'	10.0	5.0
247 to 249 (234)	West	36° 59' 30" Lt -4° 20'	5.0	5.0
T 247 to 248 (227)	Pot	-10° 28'	4.8	4.8
T 246 to 247 (48)	N 52° W	11° 20' Rt. 0° 0'	4.6	5.2

560.6

591.0

631.6



Stadia Location of Control Points
For TOPO of Res. Site.

70

O to 3 $\begin{matrix} 1272.0 \\ (1293) \end{matrix}$ S 2°30'E 87°22' L.A. + 7°27' $\begin{matrix} 4.9 \\ 4.9 \end{matrix}$

726.9

O to 2 $\begin{matrix} 1112.9 \\ (1130) \end{matrix}$ S 4½° W 73°40' L.A. + 7°13' $\begin{matrix} 4.9 \\ 4.9 \end{matrix}$

701.4

O to 1 $\begin{matrix} 820.4 \\ (863) \\ 86.0 \end{matrix}$ S 41° W 50° 0' L.A. + 12° 53' $\begin{matrix} 4.9 \\ 4.9 \end{matrix}$

748.2

0

Point 0 = Point # 252 (page 69) E1. 560.6

Dulzura Pt.
Levels to Res. site N.E. Jamul

12-5-44

T.P.	8.05	1048.05		1040.0
T.P.	10.31	1054.21	4.15	1048.90
T.P.	12.11	1066.30	0.02	1054.19
T.P.	13.12	1079.31 1079.76	0.11	66.19
T.P.	12.83	1092.62	0.12	79.19
T.P.	12.70	1104.52	0.20	1091.82
T.P.	12.91	1117.43	0.00	1104.52
T.P.	12.49	1129.77	0.15	1117.28
T.P.	12.64	1142.36	0.05	1129.72
T.P.	12.25	1154.51	0.00	1142.36
T.P.	12.70	1167.13	0.18	1154.43
T.P.	0.66	1154.69	13.10	1154.03
T.P.	0.62	1142.41	12.90	1141.79
T.P.	0.11	1129.83	12.69	1129.72
T.B.M. #1	0.11	1124.42	5.52	1124.31
T.P.	11.98	1123.34	13.06	1113.6
T.B.M. #2			9.92	1113.42

Dec. 5, 1944

Survey
18.49
Office
Stephens

71

U.S.G.S. - B.M. N.E. Cor. Inter. by Jamul School

Set GINNEY RT. of Road

Set GINNEY 150' RT. Rd.

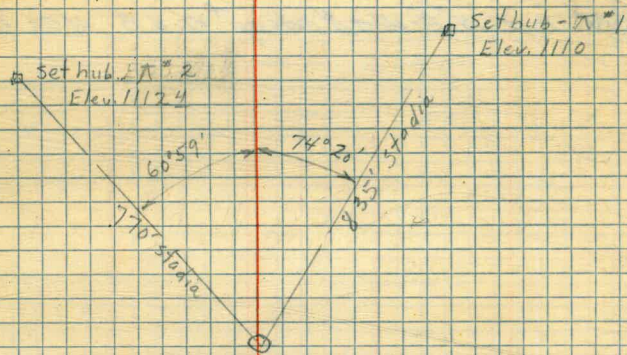
Dulzora Ph.
Res. site near Jamul

Dec. 6, 1944
Soper
King
Stephens

72

Points to be used for topography

○ Ed. stone in rock mound. Stone
has 4 notches on side and
small drilled hole in top.
Sect. Cor. 2-3-10-11



Ed. pipe with cap, Marked 1/4 Cor.
Sect. 2-3 R.E. G36
Elev. 1115

check levels to well
Near Hodges grade

349.6

5.00 352.6

4.17 348.43

10.45 358.88

1.21 357.67

11.58 369.25

2.07 367.18

12.19 379.37

0.09 379.28

11.80 391.08

0.54 390.54

10.37 400.91

Well grade. 0.40 400.51

B.M. on N.E. Well casing + 0.68 401.59

Sept. 22, 1950 Rainey
King 73

U.S.G.S. B.M.

663
667

- 22

20 T 019 (280) S 29° E POT -15° 45' 4.8
4.8

18 T 020 (667) N 29° W 48° 50' L -0° 22' 4.8
4.8

12 T 018 (1906) N 20° E POT +0° 31' 4.8
4.8

16 T 017 (132) N 20° W POT -7° 06' 10.7
4.7

16 T 015 (260) S 20° W POT -5° 45' 15.7
4.7

1389.4
3.1
1392.5

1385.1

Prints
Green
Line

208
POT

31 higher

53' 57" off Back Tower

1389.4

Reddish Adobe Soil

Power line

103'

24 T 025 (216) N72°30'W 7°20' R 0°57' 4.8

24 T 023 (345) S79E POT -4°05' 4.8

22 T 024 (547) N79W 32°30'30" L +0°49' 4.7

22 T 021 (270) S46E POT -14°05' 4.7

20 T 022 (519) N46½°W 18°28' L -0°22' 4.7

1389.1

Reddish Adobe soil

1392.7 Ahead
1389.6 Back
Ginnely Ln pass #3
El. 1392.75
HXP 13261
7580 TOTAL DISR.

13848

8.6
3.3
11.9
1381.0
1369.1

1300
282
1018

25T030 (1381) POT -5°25'30" 4.3
4.3

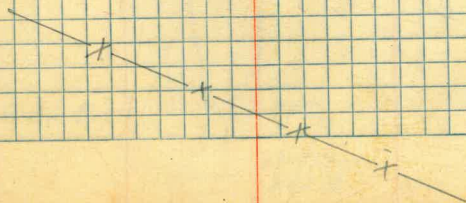
25T029 (1018) POT -9°07' 4.3
4.3

25T027 (345) POT -9°35' 4.3
4.3

25T026 (176) N70°W 2°21'R -10°15' 4.3
4.3

1259.1 MYO. 13658
TOT 9165

Reddish ridge spin/lost cropping
25 To creek



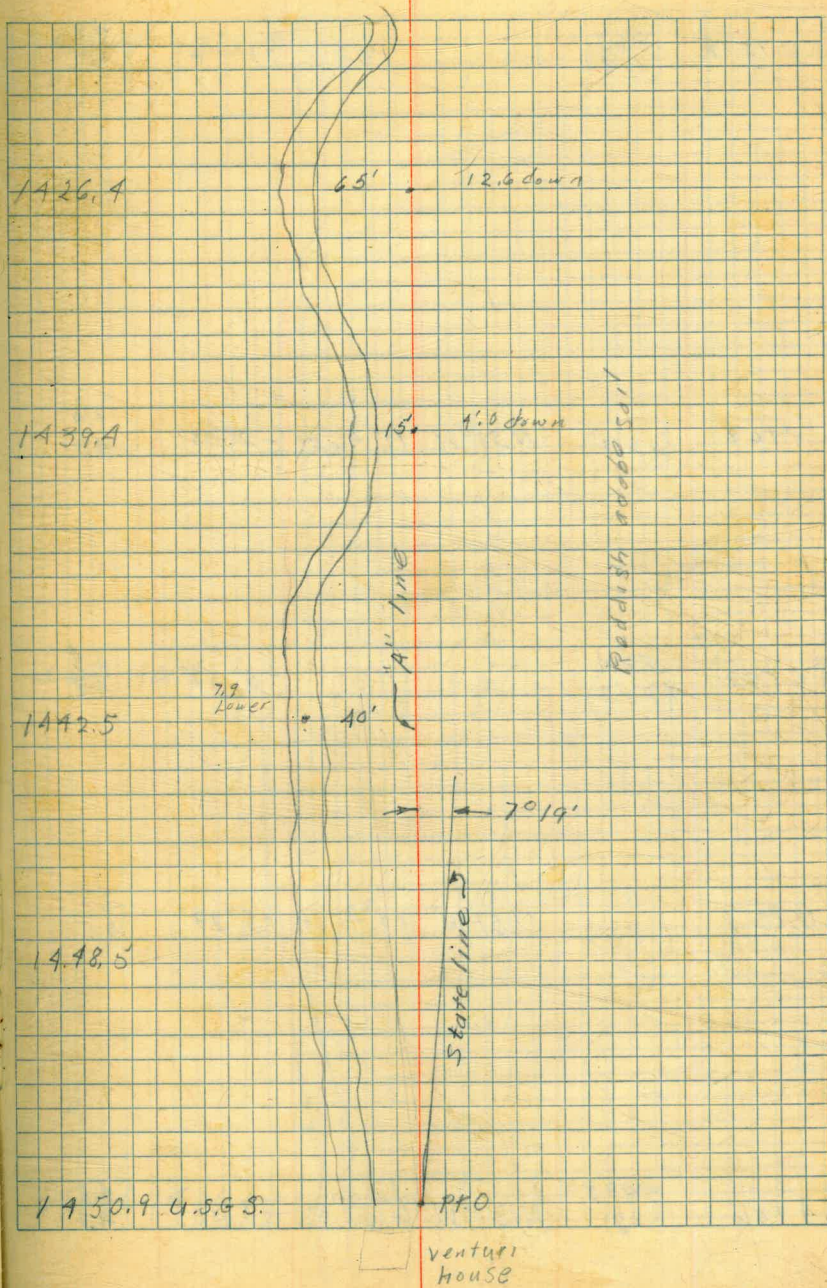
LINE "A"

Relocation - Duzura Weir

TA TO 5	(147)	POT	-8°20'	4.8 4.8
TA TO 4	374.5 (375)	N44°W	27°29' Rht. -2°0'	5.0 5.0
TA TO 3	206 (206)	N71°W	28°18' Lt. +10°52'	4.8 4.8
TA TO 2	165.8 (166)	N43°W	12°42' Rht. -2°05'	4.7 4.7
TA TO 1	(280)	N56°W	-0°30'	4.9 4.9
El. of Pt. O				4.9

11.84
3.10
3.74

12
23
27
54



400
 1300
 200
 155
 187
 868

87012 863.1
 (864) POT -1°56' 4.9
 4.9

8709 (167) N38°W 19°46' Rt -2°03' 4.9
 4.9

6708 584
 (584) POT -0°57' 4.8
 4.8

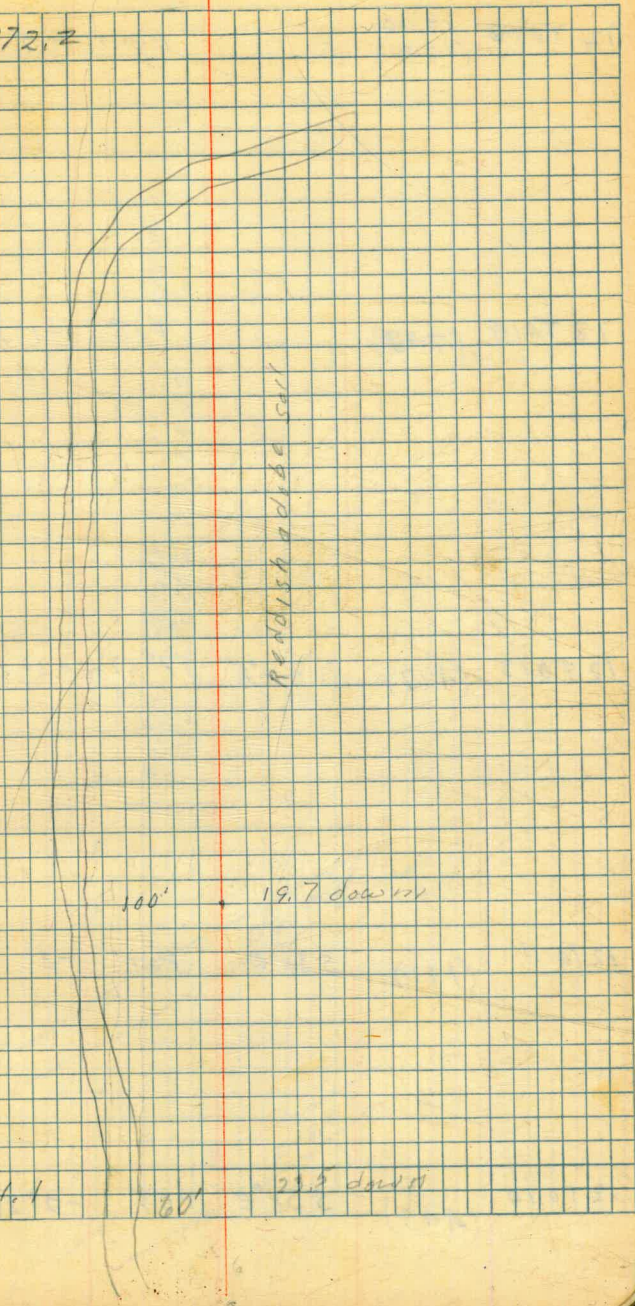
6707 (185) N57°W 19°46' Lt -5°29' 4.8
 4.8

4706 547.6
 (548) N37°W 6°22' Rt -1°36' 4.8
 4.8

1491.8 - 1372.2

1410.9 1401.4

1422.6 1411.1



145 0310 4310 1014

100' 19.7 down

20' 23.2 down

12 T016 1200
(1200) POT -0°31' 4.8
4.8

12 T014 (743) POT -1°30' 4.8
4.8

12 T013 (417) N 20°E 57°27'RA -3°28' 8.8
4.8

12 T011 (141) S 38°E POT -3° 12.8
4.8

12 T010 (445) S 38°E POT -2°28' 8.8
4.8

Reddish sandstone
Points 13 to 19

D.G. Road

Creek

CURVE TABLES.

Published by KEUFFEL & ESSER CO.

HOW TO USE CURVE TABLES.

Table I. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and External: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table I.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P. = 23° 20' to the R. at Station 542+72.

Ext. in Tab. I opposite 23° 20' = 120.87
 $120.87 \div 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. I opp. 23° 20' = 1183.1
 $1183.1 \div 10 = 118.31$.

Correction for A. 23° 20' for a 10° Cur. = 0.16
 $118.31 + 0.16 = 118.47 = \text{corrected Tangent.}$

(If corrected Ext. is required find in same way)

Ang. 23° 20' = $23.33^\circ \div 10 = 2.3333 = \text{L. C.}$

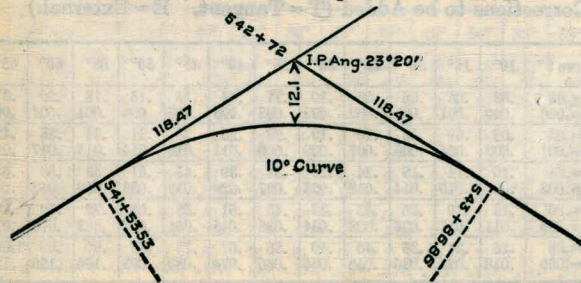
2° 19½' = def. for sta.	542	I. P. = sta.	542+72
4° 49½' = " " "	+50	Tan. =	1 .18.47
7° 19½' = " " "	543	B. C. = sta.	541+53.53
9° 49½' = " " "	+50	L. C. =	2 .33.33
11° 40' = " " "	543+	E. C. = Sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^\circ \text{ Cur.}) = 139.41' =$

2° 19½' = def. for sta. 542.

Def. for 50 ft. = 2° 30' for a 10° Curve.

Def. for 36.86 ft. = 1° 50½' for a 10° Curve.



Natural Trigonometrical Functions

Angle.	Sin.	Tan.	Sec.	Cosec.	Cotg.	Cosin.	Angle.	Sin.	Tan.	Sec.	Cosec.	Cotg.	Cosin.
32	.5299	.6249	1.1792	1.887	1.600	.84805	58	.6293	.8098	1.2868	1.589	1.235	.77715
10	.5324	.6289	1.1813	1.878	1.590	.84650	50	.6316	.8146	1.2898	1.583	1.228	.77531
20	.5348	.6330	1.1835	1.870	1.580	.84495	40	.6338	.8195	1.2929	1.578	1.220	.77347
30	.5373	.6371	1.1857	1.861	1.570	.84339	30	.6361	.8243	1.2959	1.572	1.213	.77162
40	.5398	.6412	1.1879	1.853	1.560	.84182	20	.6383	.8292	1.2991	1.567	1.206	.76977
50	.5422	.6453	1.1901	1.844	1.550	.84025	10	.6406	.8342	1.3022	1.561	1.199	.76791
33	.5446	.6494	1.1924	1.836	1.540	.83867	57	.6428	.8391	1.3054	1.556	1.192	.76604
10	.5471	.6536	1.1946	1.828	1.530	.83708	50	.6450	.8441	1.3086	1.550	1.185	.76417
20	.5495	.6577	1.1969	1.820	1.520	.83549	40	.6472	.8491	1.3118	1.545	1.178	.76229
30	.5519	.6619	1.1992	1.812	1.511	.83389	30	.6494	.8541	1.3151	1.540	1.171	.76041
40	.5544	.6661	1.2015	1.804	1.501	.83228	20	.6517	.8591	1.3184	1.535	1.164	.75851
50	.5568	.6703	1.2039	1.796	1.492	.83066	10	.6539	.8642	1.3217	1.529	1.157	.75661
34	.5592	.6745	1.2062	1.788	1.483	.82904	56	.6561	.8693	1.3251	1.524	1.150	.75471
10	.5616	.6787	1.2086	1.781	1.473	.82741	50	.6583	.8744	1.3284	1.519	1.144	.75280
20	.5640	.6830	1.2110	1.773	1.464	.82577	40	.6604	.8796	1.3318	1.514	1.137	.75088
30	.5664	.6873	1.2134	1.766	1.455	.82413	30	.6626	.8847	1.3352	1.509	1.130	.74896
40	.5688	.6916	1.2158	1.758	1.446	.82248	20	.6648	.8899	1.3386	1.504	1.124	.74703
50	.5712	.6959	1.2183	1.751	1.437	.82082	10	.6670	.8952	1.3421	1.499	1.117	.74509
35	.5736	.7002	1.2208	1.743	1.428	.81915	55	.6691	.9004	1.3456	1.494	1.111	.74314
10	.5760	.7046	1.2233	1.736	1.419	.81748	50	.6713	.9057	1.3492	1.490	1.104	.74120
20	.5783	.7089	1.2258	1.729	1.411	.81580	40	.6734	.9110	1.3527	1.485	1.098	.73924
30	.5807	.7133	1.2283	1.722	1.402	.81412	30	.6756	.9163	1.3563	1.480	1.091	.73728
40	.5831	.7177	1.2309	1.715	1.393	.81242	20	.6777	.9217	1.3600	1.476	1.085	.73531
50	.5854	.7221	1.2335	1.708	1.385	.81072	10	.6799	.9271	1.3636	1.471	1.079	.73333
36	.5878	.7265	1.2361	1.701	1.376	.80902	54	.6820	.9325	1.3673	1.466	1.072	.73135
10	.5901	.7310	1.2387	1.695	1.368	.80730	50	.6841	.9380	1.3711	1.462	1.066	.72937
20	.5925	.7355	1.2413	1.688	1.360	.80558	40	.6862	.9435	1.3748	1.457	1.060	.72737
30	.5948	.7400	1.2440	1.681	1.351	.80386	30	.6884	.9490	1.3786	1.453	1.054	.72537
40	.5972	.7445	1.2466	1.675	1.343	.80212	20	.6905	.9545	1.3824	1.448	1.048	.72337
50	.5995	.7490	1.2494	1.668	1.335	.80038	10	.6926	.9601	1.3863	1.444	1.042	.72136
37	.6018	.7536	1.2521	1.662	1.327	.79864	53	.6947	.9657	1.3902	1.440	1.036	.71934
10	.6041	.7581	1.2549	1.655	1.319	.79688	50	.6967	.9713	1.3941	1.435	1.030	.71732
20	.6065	.7627	1.2577	1.649	1.311	.79512	40	.6988	.9770	1.3980	1.431	1.024	.71529
30	.6088	.7673	1.2605	1.643	1.303	.79335	30	.7009	.9827	1.4020	1.427	1.018	.71325
40	.6111	.7720	1.2633	1.636	1.295	.79158	20	.7030	.9884	1.4061	1.422	1.012	.71121
50	.6134	.7766	1.2661	1.630	1.288	.78980	10	.7050	.9942	1.4101	1.418	1.006	.70916
38	.6157	.7813	1.2690	1.624	1.280	.78801	52	.7071	1.0000	1.4141	1.414	1.000	.70711
10	.6180	.7860	1.2719	1.618	1.272	.78622	50						
20	.6202	.7907	1.2748	1.612	1.265	.78442	40						
30	.6225	.7954	1.2778	1.606	1.257	.78261	30						
40	.6248	.8002	1.2808	1.601	1.250	.78079	20						
50	.6271	.8050	1.2838	1.595	1.242	.77897	10						

Cosin. Cotg. Cosec. Sec. Tan. Sin. Angle

Cosin. Cotg. Cosec. Sec. Tan. Sin. Angle

Handwritten calculations and notes on the right page of the notebook.

1132 762
 771524
 1124.3 + 0° 40'

N 79° W

325 1416.6
 7.75
 317.25 1395.8
 6.30
 20.8

336.35
 2
 336.35

190
 522.5 812
 309.9 1624
 212.6

37.56
 13.1
 37.1
 54.3

1171.1
 34.0
 1137.1
 1205.1
 31.4
 1236.5

523.3
 192.8
 330.5

20.4
 3.4
 23.8

111689
 1730
 33490670
 7802823
 1119689
 1928911970

996.7
 120
 979.7
 43
 975.4
 23.8
 999.2

10.5
 6.5
 17.0

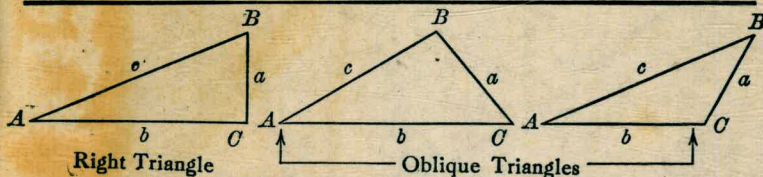
1.1

80575.
 645
 402675
 322170
 483210
 51945075
 1425

99377
 1730
 2981310
 695639
 99377
 1719.2221.0

977
 1855
 1984
 3541
 645
 12705
 214164
 27296
 2253.945
 1297
 1264.2
 1300
 632
 688
 1086.4
 1159.8
 734
 16.00
 9.66
 1039
 +1° 1'
 1336
 2160
 10
 6.15
 21.80
 108.00
 25.56
 484.0
 4776
 12960
 1393200
 996.7
 682
 28.5
 1025
 689
 337
 14509
 14318
 139.8
 48.1
 1342.7
 59.4
 116
 888
 233.7
 855
 443
 2
 197.5
 1.42
 20.77
 645
 1290
 12490
 1.1190
 29.5
 1.9
 31.7
 80 1/2
 63 1/2
 17
 1300
 325
 975
 1300
 538
 762
 617.6
 3.47
 3.48
 621.0
 97.6
 890.8
 49.2
 801.1
 53.6
 348.8
 87.3
 660.7
 703.5
 85.9
 617.6
 1300
 325
 975
 1300
 538
 762
 617.6
 3.47
 3.48
 621.0
 97.6
 890.8
 49.2
 801.1
 53.6
 348.8
 87.3
 660.7
 703.5
 85.9
 617.6

TRIGONOMETRIC FORMULÆ



Solution of Right Triangles

For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{a}$, $\operatorname{cosec} = \frac{c}{b}$

Given	Required	Formulas
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B$, $c = \sqrt{a^2 + b^2} = a\sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$, $b = \sqrt{(c+a)(c-a)} = c\sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$, $b = a \cot A$, $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$, $a = b \tan A$, $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$, $a = c \sin A$, $b = c \cos A$

Solution of Oblique Triangles

Given	Required	Formulas
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$, $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$, $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$, $C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}$, $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL

Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = 5° 10'. From Table, Page IX. $\cos 5^\circ 10' = .9959$. Horizontal distance = $319.4 \times .9959 = 318.09$ ft. Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\cos 5^\circ 10' = .9959$. $1 - .9959 = .0041$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.09$ ft. When the rise is known, the horizontal distance is approximately: the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft., slope distance = 302.6 ft. Horizontal distance = $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.