#688

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36 0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)+2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

Indexed to end - 2/8/46 mgd.

INDEX

EL MONTE PIPELINE & PROFILE AND X-SECTIONS, EAST OF SANTEE

TO 1 - 50

El Monte Pipeline & profile from Sta. 112+35.31 Lake Side, to int with Sopers location North of Santee Sta 249+91.40 Indexed 51 mgd

1

-SECTIONS
OV. 7, 1945
SOPER
WARD
PHILLIPS

NOTE: 1
and - RODS
ARE FROM
& ELEV.

CONT'D. FROM F.B. #628, Pg. 67

EL MONTE PIPELINE & PROFILE -

AND X-SECTIONS

B.M.	0.61	369.26		368.65
TP	8.60	375.47	2.39	366.87
TP	4.61	374.36	5.72	369.75
TP	2.46	373.80	3.02	371.34
TP	4.89	371.32	7.37	366.43
Set B.M.			1.76	369.56
TP	7.51	372.66	6.17	365.15

~~239+47.5~~ P.C. (VOID)		12.0	360.7
	see R.H. side of p. 52, this book. J Kaylor		
240+00		11.9	360.8
+50		11.8	360.9
241		11.4	361.3
		13.1	359.6

Aug 22 1945 1

Soper King Phillips

U.S.C.+G.S.B.M. R-61 1927 at Santee

Rec. elev. 368.648. U.S.C.+G. datum is identical with U.S.G.S. datum

Nail in power pole #72384

Iron pin 6'Rt 242+38. Marked elev. 365.15

X-SECTIONS NOV. 7, 1945 SOPER WARD PHILLIPS

NOTE: + and - RODS ARE FROM ℄ ELEV.

LT	℄	RT.
+0.7 / 50	+0.8 / 14	-0.4 / 6	PAVE +0.6 / 8.0
+0.5 / 50	+0.8 / 14	-0.3 / 6	PAVE +0.5 / 8.9
+0.9 / 50	+0.8 / 12	-0.3 / 5	PAVE +0.8 / 11.4
+0.3 / 50	+0.6 / 9	-0.2 / 3	PAVE +0.8 / 14±

℄ line, 12" culv. 5'Rt 241+14

372.66

241+50			10.5	362.2
242			9.1	363.6
	VOID	See R.H. side of p. 53, this book. Keyser		
+21			8.9	363.8
+30			7.1	365.6
+45			7.2	365.5
+50			6.2	366.5
+70			4.3	368.4
243+00			3.0	369.7
+50			1.4	371.3
244+00			0.6	372.1
℄	4.17	376.56	0.27	372.39
244+50			3.2	373.4
245			2.5	374.1

LT	℄	RT
+03 / 50	+04 / 4	0.0 / 7 ; +08 / 18.4 PAVE
-05 / 50		-01 / 14 ; +05 / 246 PAVE
+04 / 50		09 / 16 ; +07 / 276 PAVE
-12 / 50 ; -18 / 22 ; -14 / 11		-06 / 10 ; -18 / 14 ; -08 / 290 PAVE
-11 / 50 ; -05 / 36 ; +08 / 29		-06 / 14 ; -16 / 15 ; -04 / 31.5 PAVE
+03 / 50	0.0 / 12	+03 / 12 ; -26 / 16 ; -13 / 315 PAVE
-05 / 50		+02 / 21 ; -52 / 26 ; -39 / 398 PAVE
-09 / 35		00 / 25
+05 / 35		-02 / 35
+09 / 35		-13 / 35
+09 / 35		-18 / 35

376.56

					Lt.	℄	Rt
245+50			3.8	372.8	$+\frac{17}{35}$		$-\frac{20}{35}$
246	VOID		6.1	370.5	$+\frac{13}{35}$		$-\frac{13}{35}$
+30	see R.H. side of p. 53 & 55, this book.		7.0	369.6	$+\frac{18}{35}$		$-\frac{13}{35}$
+50			6.2	370.4	$+\frac{10}{35}$		$-\frac{12}{35}$
247			5.4	371.2	$+\frac{10}{35}$		$-\frac{11}{35}$
+50			4.4	372.2			
248			3.6	373.0	$+\frac{15}{35}$		$-\frac{09}{35}$
PT	10.19	383.46	3.29	373.27			
248+50			8.9	374.6			
249			7.5	376.0	$+\frac{18}{35}$		$-\frac{10}{35}$
+50			5.5	378.0			
			5.6	377.9	Top of 2" water line - 249+83		
250			4.3	379.2	$+\frac{16}{35}$		$-\frac{16}{25}$ $-\frac{15}{35}$
+50			2.9	380.6			
250+80 P.C.			1.4	382.1			

					LT	℄	RT
		383.46 ✓					
		VOID					
251+00			0.4	383.4 ✓	+1.0/35		0.0/35
TP	12.66	396.10 ✓	0.02	383.44 ✓✓			
		SEE P. 55, THIS BOOK. JK					
251+50			8.1	388.0 ✓	+0.3/35		-0.1/35
252		cont from R.H. side of P. 55, this book. JKeyser	3.8	392.3 ✓	+1.2/35		-0.9/35
+50			1.3	394.8 ✓			
TP	12.51	408.19 ✓	0.42	395.68 ✓			
253+00			10.8	397.4 ✓	+1.4/35		-1.9/35
+50			9.3	398.9 ✓			
254			7.2	401.0 ✓	+1.7/35		-1.6/35
+50			5.5	402.7 ✓			
255			4.0	404.2 ✓	+1.8/35		-1.7/35
+50			2.4	405.8 ✓			
256			1.1	407.1 ✓	+1.7/35		-1.4/35

					LT	℄	RT
		408.19 ✓					
256+50			1.8	406.4 ✓			
257			3.0	405.2 ✓	+3 5/35		-1 8/35
TP	12.59	417.97 ✓	2.81	405.38 ✓✓			
257+50			10.9	407.1 ✓			
258			9.3	408.7 ✓	+4 8/35		-3 2/35
+50			7.4	410.6 ✓	+5 3/35	0.0 5	-2 3/35
Set B.M.			3.22	414.8 75 ✓✓	Point on rock 26'Lt 258+35		
258+75			5.6	412.4	+2 4/35		-3 4/35
259			5.1	412.9 ✓	+3 5/35		-3 2/22 -4 3/35
+10			6.6	411.4	+4 5/35 +3 0/17 +0 6/6		-1 9/35
+20			4.0	414.0 ✓	+0 3/35	-1 1/19	-3 9/35
+30				413.7	+4 0/35		-3 3/35
+50			3.9	414.1 ✓	+3 5/35		-3 4/35
260+00			1.8	416.2 ✓	+3 5/35		-3 4/35
TP	12.16	430.08 ✓	0.05	417.92 ✓✓	Nail in fence post 24'Rt 260+27		
260+50			7.3	422.8 ✓	+4 2/35		-4 1/35

Aug. 24 1945
Soper
King
Phillips

		430.08 ✓		
TP	12.65	442.58 ✓	0.15	429.93 ✓✓
261			10.0	432.6 ✓
TP	12.83	454.96 ✓	0.45	442.13 ✓✓
261+50			11.9	443.1 ✓
262			0.2	454.8 ✓ 454.9
TP	13.04	467.74 ✓	0.26	454.70 ✓✓
262+50			1.5	466.2 ✓
TP	12.50	479.37 ✓	0.87	466.87 ✓✓
263			4.9	474.5 ✓

LT	℄	RT
$+\frac{5^{4}}{35}$		$-\frac{5^{3}}{35}$
$+\frac{6^{7}}{35}$		$-\frac{6^{3}}{35}$
$+\frac{8^{4}}{35}$	$+\frac{3^{3}}{15}$	$-\frac{7^{5}}{35}$

262 - START OF SURFACE BOULDERS

$+\frac{10^{0}}{35}$		$-\frac{10^{0}}{35}$
$+\frac{11^{1}}{35}$		$-\frac{2^{8}}{7}$ $-\frac{11^{0}}{30}$ $-\frac{12^{3}}{35}$

BOULDER 15' x 9' x 5' 18' RT OF 263 NOT SHOWN IN X SECTIONS

		479.37 ✓		
TP	- 6.92	485.96 ✓	0.33	479.04 ✓✓
263+45 8° P.O.T.			6.20	479.8 ✓
263+55			5.2	480.8 ✓
+63			1.8	484.2 ✓
+67			4.9	481.1 ✓
264			7.0	479.0 ✓
+31				478.6
+45			9.1	476.9 ✓
+53 Bottom of small wash			12.8	473.2 ✓
+65				477.3
+75			5.0	481.0 ✓
TP Set B.M.	12.30	496.79 ✓	1.47	484.49 ✓✓

℄

	LT			RT		
On hub	+13° / 35	+4° / 13			-11° / 35	
	+13⁴ / 35				-12° / 35	
On 6 x 10 boulder	+11° / 35	+2⁴ / 13	-1⁸ / 3	0.0 / 5	-5⁶ / 7	-14⁸ / 35
	+14⁷ / 35	+14° / 30			-12° / 35	

NOTE: BETWEEN STA 264+00 and 264+75 THERE ARE NUMEROUS SURFACE ROCKS TO BE MEASURED INDIVIDUALLY PRIOR TO CONSTRUCTION.

	+12⁸ / 35	+3⁹ / 12		-10° / 35	
	+11° / 35			-13⁸ / 35	
	+9³ / 35	+7⁵ / 27	+2° / 6	-4⁸ / 9	-13³ / 35
	+18° / 35	+9° / 20	-5° / 18	-10⁴ / 35	X-SECTIONS JAN. 16, 1946 SOPER WARDEL PHILLIPS
	+15⁸ / 35	+5° / 11	-3⁷ / 18	-8⁷ / 32	-8⁴ / 35
	+11° / 35	+4⁶ / 18	-8³ / 35		

P.O.R. 23' Lt. 264+50.

		496.79 ✓		
265+00			9.6	487.2 ✓
265+50			0.8	496.0 ✓
TP	12.53	508.51 ✓	0.81	495.98 ✓
266			5.2	503.3 ✓
TP	10.30	518.48 ✓	0.33	508.18 ✓
266+50	EDGE OF OLD ROAD		8.8	509.7 ✓
+80	EDGE OF OLD ROAD		7.9	510.6 ✓
267			6.2	512.3 ✓
+50			4.0	514.5 ✓

LT	℄	RT
$+10\frac{0}{35}$		$-9\frac{5}{35}$
$+11\frac{0}{35}$ EDGE OF ROAD	$+8\frac{5}{30}$	$-9\frac{0}{35}$
$+9\frac{8}{35}$ $+7\frac{3}{30}$ $+4\frac{6}{26}$ EDGE ROAD	$+4\frac{5}{16}$ EDGE OF ROAD $+1\frac{9}{10}$	$-8\frac{5}{35}$
$+7\frac{6}{35}$	$+2\frac{9}{12}$ $+0\frac{1}{10}$ EDGE ROAD	$-1\frac{7}{5}$ $-9\frac{8}{35}$
$+8\frac{6}{35}$	$+2\frac{0}{7}$	$-0\frac{3}{8}$ $-2\frac{2}{13}$ $-5\frac{2}{28}$ EDGE ROAD $-7\frac{5}{35}$
$+7\frac{9}{35}$	$+1\frac{1}{4}$	$-0\frac{4}{1}$ EDGE ROAD $-0\frac{6}{11}$ EDGE ROAD $-2\frac{6}{17}$ $-4\frac{8}{29}$ $-4\frac{5}{35}$
	$+4\frac{6}{35}$	$-1\frac{3}{5}$ EDGE ROAD $-1\frac{2}{16}$ EDGE ROAD $-1\frac{6}{21}$ $-1\frac{0}{35}$

		518.48 ✓		
267+66	EDGE OF OLD ROAD		5.1	513.4 ✓
+82	EDGE OF OLD ROAD		5.7	512.8 ✓
Set B.M.			0.79	517.~~7~~.69 ✓
268			7.9	510.6 ✓
TP	0.88	506.60 ✓	12.76	505.72 ✓✓
268+50			1.9	504.7 ✓
269			9.5	497.1 ✓
TP	1.21	495.17 ✓	12.64	493.96 ✓✓
269+50			6.3	488.9 ✓
TP	0.09	483.05 ✓	12.21	482.96 ✓✓

LT		℄ 5.13	RT
$+\frac{41}{35}$	$+\frac{10}{6}$	$-\frac{09}{13}$	$\frac{0.0}{35}$
$+\frac{31}{35}$ $+\frac{16}{21}$	$\frac{0.0}{13}$ EDGE ROAD	$-\frac{05}{5}$	$+\frac{04}{35}$
Nail on rock 90' RT 267+95			
$+\frac{39}{35}$ EDGE ROAD	$+\frac{29}{31}$ $+\frac{11}{27}$ $+\frac{12}{14}$ EDGE ROAD $+\frac{03}{8}$	$+\frac{08}{18}$	$+\frac{08}{35}$
	$+\frac{23}{35}$ $+\frac{09}{28}$ $-\frac{06}{10}$	$+\frac{12}{35}$	
	$+\frac{19}{35}$	$\frac{0.0}{15}$ $-\frac{16}{26}$	$\frac{0.0}{40}$
	$+\frac{08}{35}$	$-\frac{07}{5}$ $-\frac{40}{19}$	$+\frac{20}{40}$

	483.05 ✓		
269+87		2.0	483.1 ✓
270	BOTTOM OF WASH	6.2	476.9 ✓
+07		5.0	478.1 ✓
+22		6.5	476.6 ✓
+39	BOTTOM OF WASH	10.5	472.6 ✓
+50		9.4	473.7 ✓
271		10.9	472.2 ✓
+03		11.2	471.9 ✓
+12		14.4	468.7 ✓
+18		14.5	468.6 ✓

	$+\frac{3}{35}$	$+\frac{33}{18}$	$+\frac{13}{12}$	$+\frac{13}{5}$	$-\frac{24}{7}$ $+\frac{16}{18}$ $+\frac{34}{35}$
	$+\frac{42}{35}$	$+\frac{37}{21}$	$+\frac{35}{5}$		$\frac{0.0}{4}$ $+\frac{26}{10}$ $+\frac{43}{21}$ $+\frac{63}{35}$
	$+\frac{23}{35}$	$+\frac{09}{18}$	$+\frac{10}{5}$		$-\frac{29}{9}$ $-\frac{30}{7}$ $\frac{0.0}{11}$ $+\frac{39}{35}$
	$+\frac{36}{35}$	$+\frac{09}{15}$			$-\frac{23}{6}$ $\frac{0.0}{16}$ $+\frac{49}{35}$
	$+\frac{69}{35}$	$+\frac{29}{7}$			$\frac{0.0}{6}$ $+\frac{29}{14}$ $+\frac{64}{35}$
	$+\frac{40}{35}$	$+\frac{14}{8}$			$-\frac{20}{7}$ $\frac{0.0}{14}$ $+\frac{19}{26}$ $+\frac{32}{29}$ $+\frac{43}{35}$
TOP OF BANK		$+\frac{38}{35}$			$-\frac{38}{25}$ $-\frac{61}{30}$ $-\frac{61}{35}$
BOTTOM OF WASH		$+\frac{30}{35}$			$-\frac{34}{35}$
" "		$+\frac{31}{35}$			$-\frac{32}{35}$

		483.05 ✓		
271+28			11.7	471.4 ✓
+50			13.0	470.1 ✓
TP	0.44	471.09 ✓	12.40	470.65 ✓
272			3.4	467.7 ✓
+50			6.5	464.6 ✓
273			9.9	461.2 ✓
TP	0.47	458.76 ✓	12.80	458.29 ✓
273+50			1.6	457.2 ✓
274			5.7	453.1 ✓
+50			9.4	449.4 ✓
275				
TP	1.14	447.23 ✓	12.67	446.09 ✓

	LT		RT
	$+\frac{30}{35}$		$-\frac{32}{35}$
	$+\frac{31}{35}$		$-\frac{30}{35}$
272 - END OF SURFACE BOULDERS	$+\frac{30}{35}$		$-\frac{31}{35}$

		447.23 ✓		
275+50			4.6	442.6 ✓
276			6.7	440.5 ✓
+50			8.8	438.4 ✓
277			11.3	~~436.0~~ 435.9 ✓
+50			13.2	434.0 ✓
TT	1.61	436.21 ✓	12.63	434.60 ✓✓
278			4.0	432.2 ✓
+50			4.7	431,5 ✓
279			5.6	430.6 ✓
+50			6.9	429.3 ✓
280			8.3	427.9 ✓
+50			9.4	426.8 ✓

		436.21 ✓		
281			10.8	425.4 ✓
+50			12.3	423.9 ✓
IP	3.08	426.55 ✓	12.74	423.47 ✓
282			3.9	422.7 ✓
+50			5.4	421.2 ✓
283			7.0	419.6 ✓
+50			8.2	418.4 ✓
284			8.0	418.6 ✓
+50			8.0	418.6 ✓
IP	6.41	426.54 ✓	6.42	420.13 ✓

	426.54 ✓	
284+60	7.8	418.7 ✓
+66	8.9	417.6 ✓
285	7.9	418.6 ✓
+50	8.1	418.4 ✓
286	8.1	418.4 ✓
+50	7.6	418.9 ← ~~419.0~~
287	7.1	419.4 ✓
+50	6.9	419.6 ✓
288	7.7	418.8 ✓
+50	8.3	418.2 ✓
289	9.3	417.2 ✓
+60	9.0	417.5 ✓
290	9.2	417.3 ✓
+50	6.2	420.3 ✓

		426.54 ✓		
TP	4.81	425.26 ✓	6.09	420.45 ✓
291			2.7	422.6 ✓
150			2.6	422.7 ✓
292			2.8	422.5 ✓
150			3.1	422.2 ✓
292+80.11 P.O.T			3.7	421.6 ✓
Ck on B.M.			5.35	419.91 ✓

3 nails in power pole S.W. Cor. MAGNOLIA + PROSPECT
Rec. elev 419.85 - Brought from U.S.C.+G.S.B.M R 61
at Sanitec

℄ PROFILE CONTINUED

B.M.	3.65	423.50	419.85	3 nails in pole S.W. Cor. Magnolia & Prospect
292+89		4.5	419.0	Gutter
293		3.9	419.6	
293+08.5		3.75	419.75	EDGE OF CONC. PAVE
+36.9		3.65	419.85	" " "
+50		4.4	419.1	
+77		5.4	418.1	Gutter
+83		4.9	418.6 419.2	EDGE OF OIL PAVING

		423.50 ✓		
294+00			5.2	418.3 ✓
+11			6.8	416.7 ✓
+16			5.4	418.1 ✓
+50			6.6	416.9 ✓
295			8.0	415.5 ✓
+50			9.3	414.2 ✓
TT	1.06	414.03 ✓	10.53	412.97 ✓
296			1.1	412.9 ✓
+50			2.6	411.4 ✓

		414.03 ✓		
297			4.1	409.9 ✓
+50			5.3	408.7 ✓
298			6.3	407.7 ✓
+50			8.0	406.0 ✓
π	0.42	406.75 ✓	7.70	406.33 ✓
299			2.2	404.6 ✓
+12			2.2	404.6 ✓
+17			3.1	403.7 ✓
+50			3.9	402.9 ✓
300 +00			5.6	401.2 ✓
+50			7.4	399.4 ✓
301			9.6	397.2 ✓

		401.25 ✓			
306+04	63 E.C		5.63	395.62 ✓	ON HUB '
+50			6.4	394.9 ✓	
307			7.6	393.7 ✓	
+50			7.6	393.7 ✓	
IP :	3.33	398.95 ✓	5.63	395.62 ✓	
+63 30	P.O.T		5.3	393.7 ✓	
SET B.M.	3.18	398.20 ✓	393	395.02 ✓	ON BRASS CAP IN CONC. MON. 20' Lt 307+63 30.
308			4.4	393.8 ✓	
+47 25	BC		4.41	393.8 ✓	ON HUB .
+50			4.5	393.7 ✓	

		398.20 ✓			
309			5.8	392.4 ✓	
+50			7.3	390.9 ✓	
310			11.0	387.2 ✓	
PT	3.46	390.18 ✓	11.48	386.72 ✓	
310+30			4.8	385.4 ✓	
+50			5.2	385.0 ✓	
			5.0	385.2 ✓	ON RUNWAY - 15' Rt 310+67
311			5.1	385.1 ✓	
+50			5.3	384.9 ✓	
312			5.3	384.9 ✓	
			5.0	385.2 ✓	ON RUNWAY - To Rt of 312+00
+50			5.1	385.1 ✓	
313			5.1	385.1 ✓	
+50			5.0	385.2 ✓	
			5.0	385.2 ✓	ON RUNWAY 5' Rt 313+68

		390.18 ✓			
314			5.9	384.5 ✓	
+50			5.2	385.0 ✓	
+80.80	E.C.		5.43	384.75 ✓	ON HUB
SET B.M.			5.44	384.74 ✓	ON BRASS CAP IN CONC. MON. 70' Rt 315+84
	595	390.69 ✓			
315			5.6	385.1 ✓	
+50			3.8	386.9 ✓	
+87			3.9	386.8 ✓	
+90			5.6	385.1 ✓	IN DRAIN DITCH
+92			4.2	386.5 ✓	
316			5.1	385.6 ✓	

Sept 5, 1945
Soper
King
Phillips

		390.69 ✓				
316+28			5.1	385.6	✓	
+35			6.2	384.5	✓	
+50			7.2	383.5	✓	
317			8.0	382.7	✓	
+50			8.6	382.1	✓	
TP	5.11	386.37 ✓	8.83	381.86 ✓		ON P.O.T. HUB 317+54.74
318			5.4	381.6	✓	
+50			4.8	382.2	✓	
319			5.2	381.8	✓	
+50			5.3	381.7	✓	
320			5.8	381.2	✓	
+50			4.8	382.2	✓	

		386.97 ✓			
321			5.3	381.7	✓
+25			5.1	381.9	✓
+50			4.0	383.0	✓
322			5.8	381.2	✓
+50			6.9	380.1	✓
+60			7.7	379.3	✓
323			6.4	380.6	✓
+50			5.7	381.3	✓
324			4.8	382.2	✓
TP	5.19	387.96 ✓	4.20	382.77 ✓	✓
324+50			4.6	383.4	✓
325+00			4.21	383.75	✓ ON POT. HUB
+50			5.3	382.7	✓
326			5.8	382.2	✓
+50			6.5	381.5	✓
+85			6.9	381.1	✓

		387.96 ✓		
327			6.5	381.5 ✓
+50			6.2	381.8 ✓
328			5.4	382.6 ✓
+50			3.7	384.3 ✓
329			3.1	384.9 ✓
+50			2.7	385.3 ✓
330			3.4	384.6 ✓
+50			3.4	384.6 ✓
331			3.1	384.9 ✓
+50			3.2	384.8 ✓
PI	5.31	390.55 ✓	2.72	385.24 ✓
331+77			5.3	385.3 ✓
332			5.3	385.3 ✓
+50			5.3	385.3 ✓

		390.55 ✓			
332+65			5.2	385.4	✓
333			5.67	384.9	✓
+50			6.8	383.8	✓
334			7.4	383.2	✓
+08			7.5	383.1	✓
+13			8.1	382.5	✓
+50			7.9	382.7	✓
335			7.4	383.2	✓
+50			6.9	383.7	✓
+80			6.9	383.7	✓
336			7.5	383.1	✓
+22			8.0	382.6	✓
TP	6.12	389.18 ✓	7.49	383.06 ✓	✓
336+50			6.2	383.0	✓
337			5.4	383.8	✓

ON P.O.T. HUB

		389.18 ✓			
337+25			5.6	383.6	✓
+50			7.0	382.2	✓
+63			7.4	381.8	✓
+87			5.0	384.2	✓
338			5.0	384.2	✓
+50			5.2	384.0	✓
339			5.1	384.1	✓
+50			3.7	385.5	✓
340			3.9	385.3	✓
+50			4.3	384.9	✓
341			5.0	384.2	✓
+50			5.6	383.6	✓
TP	6.30	389.87 ✓	5.61	383.57 ✓	✓
342			6.2	383.7	✓
+50			5.6	384.3	✓
343			5.3	384.6	✓

		389.87 ✓			
343+50			4.9	385.0	✓
344			5.0	384.9	✓
+50			5.3	384.6	✓
345			5.6	384.3	✓
+50			5.2	384.7	✓
346			4.7	385.2	✓
+50			4.2	385.7	✓
347			3.3	386.6	✓
TP	6.00	392.60 ✓	3.27	386.60 ✓	✓
347+50			5.3	387.3	✓
348			5.2	387.4	✓
348+50			5.39	387.2	✓
192			5.3	387.3	✓
+96			5.9	386.7	✓

ON P.O.T. HUB

		392.60 ✓			
349+00			5.0	387.6	
TP SET B.M.	5.03	393.80 ✓	3.83	388.77 ✓	Nail in pole 33' Rt. 349+17
349+50			6.0	387.8 ✓	
350			5.8	388.0 ✓	
+50			5.4	388.4 ✓	
351			5.2	388.6 ✓	
+50			5.3	388.5 ✓	
352			5.3	388.5 ✓	
+50			5.1	388.7 ✓	
353			5.1	388.7 ✓	
+50			4.6	389.2 ✓	
354			4.1	389.7 ✓	
+50			3.4	390.4 ✓	
+86			2.9	390.9 ✓	
TP	5.37	396.60 ✓	2.57	391.23 ✓	

		396.60 ✓			
355+31.90			5.57	391.03 ✓	ON P.O.T. HUB.
+50			5.7	390.9 ✓	
356			6.2	390.4 ✓	
+50			6.4	390.2 ✓	
357			6.3	390.3 ✓	
+50			5.5	391.1 ✓	
358			5.0	391.6 ✓	
+50			5.2	391.4 ✓	
359			5.5	391.1 ✓	
PI	6.59	397.38 ✓	5.76	390.84 ✓ ✓	
+50			6.6	390.8 ✓	
360			5.9	391.5 ✓	
+50			6.5	390.9 ✓	
361			5.6	391.8 ✓	
+50			6.0	391.4 ✓	
362			5.8	391.6 ✓	
+50			5.0	392.4 ✓	
363			4.7	392.7 ✓	

		397.38 ✓		
363+50			5.0	392.4 ✓
364			5.4	392.0 ✓
+50			6.1	391.3 ✓
365			7.8	389.6 ✓
+50			9.6	387.8 ✓
TP	10.82	398.75 ✓	9.45	387.93 ✓
365+56			11.2	387.6 ✓
+80			13.1	385.7 ✓
366			13.0	385.8 ✓
+36			12.5	386.3 ✓
+46			13.7	385.1 ✓
+50			12.9	385.9 ✓
+60			11.0	387.8 ✓
367			9.5	389.3 ✓
+50			8.8	390.0 ✓

		398.75 ✓			
368+00			7.9	390.9 ✓	
				392.1 ✓	
+50			6.7	~~397.3~~	
369			5.1	393.7 ✓	
+50			3.6	395.2 ✓	
370			2.9	395.9 ✓	
+50			2.7	396.1 ✓	
371			2.2	396.6 ✓	
+50			1.8	397.0 ✓	
372			1.2	397.6 ✓	
372+37.30	4.73	402.65 ✓	0.83	397.92 ✓	ON P.O.T. HUB
372+50			4.8	397.9 ✓	
373			5.0	397.7 ✓	
+50			4.5	398.2 ✓	
374			4.3	398.4 ✓	
+50			4.5	398.2 ✓	

		402.65 ✓			
375			4.7	398.0	✓
+50			4.5	398.2	✓
376			3.8	398.9	✓
+50			2.9	399.8	✓
377			2.6	400.1	✓
+50			2.0	400.7	✓
378			2.1	400.6	✓
TP	5.21	406.03 ✓	1.83	400.82 ✓	✓
378+50			5.2	400.8	✓
379			5.0	401.0	✓
+50			4.9	401.1	✓
380			4.9	401.1	✓
+31			5.3	400.7	✓
+50			5.7	400.3	✓
381			6.5	399.5	✓
+25			7.9	398.1	✓

		406.03 ✓			
381+50			11.0	395.0	✓
TP	5.85	402.85 ✓	9.03	397.00 ✓	✓
381+75			9.4	393.5	✓
382			9.7	393.2	✓
+38			10.0	392.9	✓
+50			12.1	390.8	✓
+52			13.5	389.4	✓ WATER 2-1/2 deep.
+63			13.8	389.1	✓
+68			10.7	392.2	✓
383			9.0	393.9	✓
+50			8.3	394.6	✓
384			7.7	395.2	✓
+50			4.2	398.7	✓
385			1.7	401.2	✓

		402.85 ✓			
IP 385+25.60	6.25	408.23 ✓	0.87	401.98 ✓	ON P.O.T. HUB
SET B.M.			1.77	406.46 ✓	Point on N.W. cor. of Headwall on North side of Broadway
B.M	7.67	414.13 ✓		406.46 ✓	Sept 6, 1945 Soper King Phillips
385+34			12.6	401.5 ✓	
+49 30			11.83	402.30 ✓	EDGE OF CONC. PAVE
+71 30			11.69	402.44 ✓	" " " "
+82			12.4	401.7 ✓	
+88			11.0	403.1 ✓	
386			10.6	403.5 ✓	

		414.13 ✓			
386+50			9.5	404.6	✓
387			8.6	405.5	✓
+50			7.3	406.8	✓
388			6.6	407.5	✓
+50			5.6	408.5	✓
389			4.3	409.8	✓
+50			3.5	410.6	✓
390			2.7	411.4	✓
+50			1.8	412.3	✓
TP	10.24	423.26 ✓	1.11	413.02 ✓	✓
391			8.8	414.5	✓
+50			8.2	415.1	✓
392			6.7	416.6	✓
+50			6.1	417.2	✓
393			4.6	418.7	✓

		423.26 ✓			
393+50			4.2	419.1	✓
394			3.4	419.9	✓
TP	9.85	429.74 ✓	3.37	419.89	✓
394+50			9.6	420.1	✓
395			9.6	420.1	✓
+09			11.0	418.7	✓
+50			9.2	420.5	✓
396			7.6	422.1	✓
+27			5.6	424.1	✓
+50			4.4	425.3	✓
+86			3.6	426.1	✓
396+91.20			3.75	425.99	✓
397			4.3	425.4	✓
+10			4.8	424.9	✓
+50			3.8	425.9	✓
+70			4.3	425.4	✓

ON P.O.T. HUB

		429.74 ✓			
398			3.8	425.9	✓
+50			3.9	425.8	✓
399			3.4	426.3	✓
+50			2.5	427.2	✓
+75			1.9	427.8	✓
TP	12.64	440.51 ✓	1.87	427.87 ✓	✓
400			10.7	429.8	✓
+50			9.8	430.7	✓
+75			9.5	431.0	✓
+90			8.4	432.1	✓
401			8.7	431.8	✓
+13			9.2	431.3	✓
+30			8.1	432.4	✓
+50			8.6	431.9	✓
402			8.9	431.6	✓
+25			8.6	431.9	✓
+50			6.6	433.9	✓
+70			4.5	436.0	✓

		440.51 ✓			
403			4.2	436.3	✓
+50			2.9	437.6	✓
404			1.1	439.4	✓
PT	12.57	452.43 ✓	0.65	439.86 ✓	✓
404+25			11.4	441.0	✓
+50			11.2	441.2	✓
+61			10.4	442.0	✓
405			10.4	442.0	✓
+50			7.4	445.0	✓
+65			8.1	444.3	✓
+92			7.4	445.0	✓
406			6.4	446.0	✓
+08			5.6	446.8	✓
+30			6.3	446.1	✓
406+50			4.32	448.11	✓ ON P.O.T. HUB

		452.43 ✓		
406+75			4.8	447.6 ✓
407			3.8	448.6 ✓
+18			2.5	449.9 ✓
+38			3.4	449.0 ✓
+50			3.2	449.2 ✓
TP	10.41	459.90 ✓	2.94	449.49 ✓
408			9.2	450.7 ✓
+50			7.3	452.6 ✓
+60			6.9	453.0 ✓
+80			8.0	451.9 ✓
409			7.8	452.1 ✓
+50			5.7	454.2 ✓
+66			6.6	453.3 ✓
+80			6.6	453.3 ✓
410			4.7	455.2 ✓
+20			5.4	454.5 ✓

	459.90 ✓		
410+50		5.3	454.6 ✓
+70		4.7	455.2 ✓
411		5.1	454.8 ✓
+40		4.7	455.2 ✓
+50		5.6	454.3 ✓
+59		6.5	453.4 ✓
+76		4.3	455.6 ✓
412		4.9	455.0 ✓
+18		5.5	454.4 ✓
+40		2.9	457.0 ✓
+50		3.1	456.8 ✓
413		3.2	456.7 ✓
+15		1.2	458.7 ✓
+50		2.8	457.1 ✓
+87		4.8	455.1 ✓
414		3.3	456.6 ✓
+11		2.5	457.4 ✓

		459.90 ✓			
414+50			3.1	456.8 ✓	BOTTOM OF WASH
415			1.0	458.9 ✓	
SET B.M.	12.37	471.85 ✓	0.42	459.48 ✓	Nail in fence post 56' Lt 414+60
415+50			10.5	461.4 ✓	
+95			8.7	463.2 ✓	
416			9.1	462.8 ✓	
+03			9.9	462.0 ✓	BOTTOM OF WASH
+09			8.8	463.1 ✓	
+50			6.7	465.2 ✓	
+63			5.3	466.6 ✓	
+82			4.9	467.0 ✓	
417			3.4	468.5 ✓	
+25			3.2	468.7 ✓	
+50			1.5	470.4 ✓	

Sept 7 1945
Sewer
Line
Mill ps

		471.85 ✓			
PI	11.70	482.99 ✓	0.56	471.29 ✓	
418			10.4	472.6	✓
+50			8.4	474.6	✓
+80			7.2	475.8	✓
419			6.4	476.6	✓
+10			6.1	476.9	✓ TOP OF BANK
+18			8.4	474.6	✓ BOTTOM OF WASH
+43			7.4	475.6	✓ " " "
+50			6.1	476.9	✓ SIDE OF BANK
+65			4.8	478.2	✓ " " "
+79			4.5	478.5	✓ " " "
+84			5.3	477.7	✓ BOTTOM OF WASH
+91			3.3	479.7	✓ TOP OF BANK
420			2.5	480.5	✓
+11			1.8	481.2	✓ TOP OF BANK
+15			3.6	479.4	✓ BOTTOM OF WASH

		482.99 ✓			
+26			1.7	481.3 ✓	SIDE OF BANK
TP	11.63	493.61 ✓	1.01	481.98 ✓	
420+50			12.2	481.4 ✓	SIDE OF BANK
+86			10.2	483.4 ✓	" " "
+90			11.1	482.5 ✓	BOTTOM OF WASH
421			10.9	482.7 ✓	" " "
+04			9.3	484.3 ✓	TOP OF BANK
+20			8.0	485.6 ✓	" " "
+26			9.5	484.1 ✓	BOTTOM OF WASH
+32			7.9	485.7 ✓	TOP OF BANK
+50			6.7	486.9 ✓	
+60			6.0	487.6 ✓	TOP OF BANK
+67			6.9	486.7 ✓	BOTTOM OF WASH
+80			6.0	487.6 ✓	" " "
+85			4.3	489.3 ✓	TOP OF BANK
422			3.7	489.9 ✓	

		493.61 ✓			
422+50			1.6	492.0	✓
+75			1.1	492.5	✓
+80			2.1	491.5	✓
+91			0.0	493.6	✓
TP	12.29	505.42 ✓	0.48	493.13 ✓	✓
423			10.8	494.6	✓
+20			9.4	496.0	✓
+50			5.3	500.1	✓
424			3.2	502.2	✓
+30			2.1	503.3	✓
+50			2.6	502.8	✓
+65			0.4	505.0	✓
TP	12.34	517.54 ✓	0.22	505.20 ✓	✓
424+80			12.1	505.4	✓

TOP OF BANK

BOTTOM OF WASH

TOP OF BANK

		517.54 ✓			
425+00			12.6	504.9	✓
+20			11.2	506.3	✓
+50			11.5	506.0	✓
+72			9.7	507.8	✓
426+00			9.3	508.2	✓
+50			7.5	510.0	✓
427			5.5	512.0	✓
+50			3.5	514.0	✓
TP	12.31	527.16 ✓	2.69	514.85 ✓	✓
428+00			10.0	517.2	✓
+50			6.8	520.4	✓
429+00			3.1	524.1	✓
TP SET B.M.	12.59	533.67 ✓	6.08	521.08 ✓	✓
TP	12.69	545.70 ✓	0.66	533.01 ✓	✓
	5.77	549.82 ✓	1.65	544.05 ✓	✓
ck on B.M.			6.84	542.98 ✓	✓

LT.	℄	RT.
NOTE: THESE ROD'S ARE + & − FROM ℄ ELEV		
506.0 − 22 / 50		511.10 + 29 / 50
508.0 − 40 / 50		514.5 + 25 / 50
514.5 − 27 / 50		520.2 + 30 / 50
520.2 − 39 / 50		530.1 + 60 / 50
NAIL IN POWER POLE. (POLE ON FENCE LINE - No number)		
Nail in power pole. Rec. elev 542.93 Book 680/63		

X-SECTIONS JAN 15, 1946 SOPER WADDELL PHILLIPS

Sept 13, 1945
So per notes + chain
Ward R
Phillips Rod + chain

B.M	12.62	533.70		521.08
429+57.1			5.28	528.4
430			1.6	532.1
TP	12.97	546.30	0.37	533.33
430+50			9.6	536.7
+58			9.3	537.0
+77			6.3	540.0
431+00			5.0	541.3
+50			1.6	544.7
TP	12.29	558.20	0.39	545.91
432			8.7	549.5
+50			6.1	552.1
+70			1.5	553.7
433			3.6	554.6
+50			0.5	557.7

Nail in Power pole (ON FENCE LINE)

	LT	℄	RT
ON HUB	525.8		539.5
	$-\frac{63}{50}$		$+\frac{79}{50}$
	534.1		547.5
	$-\frac{72}{50}$		$+\frac{63}{50}$
	540.8		556.5
	$-\frac{87}{50}$		$+\frac{70}{50}$
	546.1		565.6
	$-\frac{85}{50}$		$+\frac{110}{50}$

		558.20 ✓		
TP	11.52	568.81 ✓	0.91	557.29 ✓✓
434+00			7.7	561.1 ✓
+50			4.8	564.0 ✓
435			1.9	566.9 ✓
+20			1.5	567.3 ✓
+50			2.3	566.5 ✓
+60			2.4	566.4 ✓
+80			3.8	565.0 ✓
436			3.7	565.1 ✓
+25			3.9	564.9 ✓
+40			3.0	565.8 ✓
+50			4.2	564.6 ✓
+77.38	E.C.		6.7	562.1
TP	0.67	562.75 ✓	6.73	562.08 ✓✓
437+00			1.8	561.0 ✓

LT	℄	RT
550.3		573.7
−108/50		+126/50
553.2		580.0
−108/50		+160/50
554.2		584.9
−127/50		+180/50
553.7		579.5
−128/50		+130/50
556.2		577.3
−89/50		+123/50
554.8		578.2
−98/50		+136/50
ON E.C. HUB		
549.10		579.40
−119/50		+184/50

		562.75 ✓			
437+25			2.2	560.6	✓
+50			3.3	559.5	✓
437+62.83 B.C.			3.81	558.94	✓
+80			5.6	557.2	✓
438			8.8	554.0	✓
+22			12.8	550.0	✓ edge of road
TP	4.30	554.44 ✓	12.61	550.14 ✓	✓
438+40			3.7	550.7	✓ edge of road
+50			5.1	549.3	✓
+65			5.9	548.5	✓

ON HUB

LT	℄	RT
543.8 ROAD 547.4		580.5
-15.7 / 48 -12.1 / 41		+21.0 / 50

542.6	545.0	547.8 ROAD	548.9 ROAD	552.0	560.5	564.7	567.0	567.8	
-11.9 / 50	-9.0 / 35	-6.2 / 26	-5.1 / 13	-2.0 / 6	+6.5 / 20	+10.7 / 32	+13.0 / 43	+13.8 / 50	
	541.6	544.0	546.1	ROAD 549.2	552.4	561.0			
	-8.9 / 50	-6.0 / 30	-3.9 / 21	-0.8 / 14	+2.4 / 9	+11.0 / 50			
	539.9 IN WASH	543.9 TOP BANK	546.8	548.9	551.6 ROAD	553.0	560.6		
	-10.8 / 50	-6.8 / 43	-3.9 / 17	-1.8 / 5	+0.9 / 17	+2.3 / 21	+9.2 / 50		
543.9	543.8 TOP BANK	540.3 IN WASH	540.3 IN WASH	544.9 TOP BANK	551.3 ROAD	552.9 ROAD	554.5	561.0	
-5.4 / 60	-5.5 / 53	-9.0 / 47	-9.0 / 43	-4.9 / 35	+2.8 / 8	+3.9 / 25	+5.2 / 30	+11.7 / 50	
545.10	544.5 TOP BANK	540.9	541.5	542.2	542.5 TOP BANK 545.5	549.9	551.9 ROAD	553.4 ROAD	557.0	561.1
-3.9 / 60	-4.0 / 48	-7.6 / 46	-7.0 / 41	-6.3 / 39	-6.0 / 36	-3.0 / 28	+1.9 / 11	+3.9 / 13	+4.9 / 33	+8.5 / 40	+12.6 / 50

554.44 ✓

438+82.38 E.C	5.99	548.45	ON HUB
439	5.6	548.8	
+18	5.4	549.0	
+25	7.3	547.1	
+30	5.7	548.7	
439+43.82 Back 448+32.06 Ahead	4.4	550.0	
439+43.82 448+32.06	4.49	549.95	
ck on B.M	11.50	542.94	✓

℄ PROFILE CONT'D IN BOOK 694/30

THESE RODS ARE + & − FROM ℄ ELEV.

JAN. 14, 1946
SOPER
WADDELL
PHILLIPS
50.

549.2	549.2	LT 542.9	543.1	545.9	℄	551.1	RT 553.4	559.4	558.2
+07	−13	−56	−54	−26		+26	+43	+58	+97
60	48	40	30	23		20	29	ROAD 43	50

550.8	548.0	545.3	544.6	547.1	549.8	552.2	555.1	555.5
+20	−08	−35	−42	−17	+10	+34	+63	+67
60	44	37	22	18	16	32	ROAD 38	ROAD 50

552.8	550.5	544.8	545.0	545.3	546.3	550.4	551.4	553.5	554.9
+38	+15	−42	−40	−37	−27	+14	+24	+45	+59
60	50	44	37	18	13	11	29	46	50

553.3	550.9	549	545.3	546.1	547.5	546.6	550.5	551.5	554.5
+63	+38	−23	−18	−19	+09	−05	+39	+49	+79
60	50	43	38	23	8	4	11	22	50

553.2	550.7	544.7	544.7	546.0	546.7	547.5	548.3	548.7	551.0	554.4
+45	+20	−42	−40	−27	−20	−13	−09	0.0	+23	+57
60	50	44	39	37	23	11	6	8	17	50

554.0	547.0	546.0	549.0	548.0	550.0	550.8	551.9	553.3
+40	−30	−40	−18	−20	0.0	+0.8	+19	+33
57	48	37	35	12	6	16	25	50

~~ON HUB~~ REPLACED — NO GOOD FOR ELEV.

Nail in power pole Rec elev. 542.93

Bliss & Notes
Davis
River Pod
Feb 4 1946
Cloudy - cold

El Monte Pipe Line

Profile Levels from 112+35 3' to 249+91.40

				U.S.G.S
BM.	1.14	- 410.09	408.95	V
112+35 3'		2.97	407.12	V
+50		3.7	406.4	V
+55 3'	14' El Monte Line	3.9	406.2	V
137+0		5.3	404.8	V
+58 14'	Lt	6.8	403.3	V
114+0		5.0	405.1	V
+25		7.5	402.6	V N Bank
+50		9.0	401.1	V App Bottom
+63		6.3	403.8	V S. Bank

VOID
see Book 692
p. 10 & 11
& p. 1 to 9

Notes reduced by M.R.R. 2-18-46
CHECKED BY MRR 2-18-46

(CONTINUED FROM F.B. *628 - PG. *36) E.E.

Spike in Power Pole # NW Woodside Ave & River Street Lakeside

Top Man Hole Box

410.09

T.P. 114+81	20 Rt	3.09	405.89	7.29	402.80
115+0	VOID See book 692 p. 1 & 2 Jkaylor			3.3	402.6
+50				3.5	402.4
116+0				3.7	402.2
+50				3.9	402.0
117+0				4.2	401.7
+50				4.6	401.3
118+0				4.9	401.0
+50				5.1	400.8

25' Rt Slope Stake

38' Rt Slope Stake

Continued from back of this book (p. 103)

T 36729

234+50			4.0	363.3
235			4.1	363.2
T.P.	2.08	365.94	3.43	363.86
+50			3.0	362.9
236			3.4	362.5
+50			3.7	362.2
237			4.1	361.8
+50			4.2	361.7
238			4.6	361.3
+58.40	BC Lt on Rt		4.77	361.17
239			4.7	361.2
+50			4.1	361.8
240			3.8	362.1
+50			2.1	363.8
T.P.	11.92	376.58	1.28	364.66
+73			11.6	365.0
+77			10.1	366.5
241			8.1	368.5

Continued Top page 53 R.H. Side

		405.89		
119+0			5.2	400.7
+50	(VOID) See book 692 p. 2 & 3 JKaylor		5.4	400.5
120+0			5.6	400.3
+50	BS BC		6.3	399.6
TP	3.90	403.49	6.30	399.59
121+0			3.9	399.6
+50			4.0	399.5
+65			3.6	399.9
+75			5.6	397.9

Continued from Page 52

		376.58		
+50			6.1	370.5
247			4.7	371.9
+50			3.3	373.3
248			2.1	374.5
+56			1.8	374.8
BM			7.09	369.49
244			4.0	372.6
+50			5.9	370.7
245			4.7	371.9
+50			4.5	372.1
246			3.8	372.8
+50			2.4	374.2
247			1.1	375.5
TP	11.89	388.17	0.30	376.28
+50			10.7	377.5
248			9.3	378.9
+50			8.7	379.5
249			6.5	381.7

Continued Page 55 R.H. Page

	403.99		
+86		3.7	399.8 ✓
+94.85	E.C. on Hub	3.81	399.68 ✓
122+0	VOID see p. 4, Book 692 JKeyser	3.9	399.6 ✓
+50		4.7	398.8 ✓
123		4.9	398.6 ✓
+50		4.9	398.6 ✓
124+0		5.8	397.7 ✓
+	B.C. on Hub	5.32	398.17 ✓
+50	in dirt road	6.4	397.1 ✓

36' RT
S. Side of Rd.

50' RT Angle
S Side Dirt Road

Feb 5-96
Bliss Notes
Rice ↗
Phillips Rod

↗ 403.49

125+00			6.0	397.5
TP. on BC.				
125+38	4.02	401.96	5.55	397.94
126+00	(VOID) see book 692 p. 5 & 6 JKaysor		2.5	399.5
+50			1.4	400.6
127+00			1.7	400.3
+50			3.3	398.7
128+00			4.5	397.5
+50			5.5	396.5
129+00			5.6	396.4

Continued from Page 53

55

↗ 388.17

+50			3.1	385.1
TP.	5.85	391.65	2.37	385.80
249+91.40 on EC Hub			1.70	389.95
TP.	2.37	388.17	5.85	385.80
T.P.	0.62	376.72	12.07	376.10
check #1			7.16	369.56

PP #72384 Set by H Soper See Page 1

CONT ON P. 4, THIS BOOK.

EQU. EC 249 + 91.40 BACK =
251 + 66.49 AHEAD

JKaysor

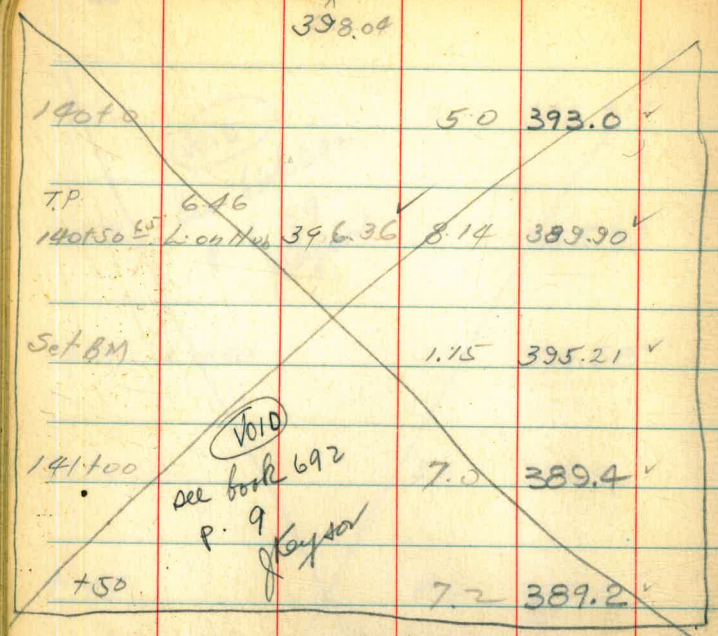
		A 401.96		
129+93	6" water pipe		2.9	399.1 ✓
130+0	VOID see book 692 p. 6 & 7 J Keyser		4.5	397.5 ✓
+50			3.1	398.9 ✓
131+0			3.8	398.2 ✓
T.P.	3.46	402.36 ✓	3.06	398.30 ✓
+50			4.4	398.0 ✓
132			3.5	398.9 ✓
+50			2.9	399.5 ✓
133			2.7	399.7 ✓

		↑ 402.36		
X33+50			1.5	400.9
133+77	P.O.T. Hub		1.09	401.27
	VOID see book 692 p. 7 JKeyston			
+90			1.7	400.7
+93	Top 4" cb		4.9	397.5
"	Gutter		5.7	396.7
+95 ±	Edge Gutter		5.0	397.4
Flow ↓	Drainage Pipe 4C RP		6.3	396.1
134			4.6	397.8
+15			3.6	398.8
+50			6.9	395.5

		402.36		
135+0	VOID See book 692 p. 7 & 8 J Kaylor		10.2	392.2
+50			11.5	390.9
TP		398.04	11.52	390.89
136+0			7.2	390.8
+50			6.8	391.2
137+0			6.4	391.6
+50			6.4	391.6
138+0			5.6	392.4
+47	Ground Bottom old wall		3.7	394.3
+47	Top old wall		2.2	395.8

↑ 398.04

+50	VOID See book 692 P. 8 & 9 Kaylor	1.8	396.2 ✓
+78		2.1	395.9 ✓
+94	L on Hub	3.4±	394.58 ✓
1394.0		3.5	394.5 ✓
+45		4.0	394.0 ✓
+52	E Edge of Paving	5.0	393.0 ✓
	S Edge Conc	4.9	393.1 ✓
	℄	4.8	393.2 ✓
	N Edge	5.0	393.0 ✓



140+00			5.0	393.0 ✓
T.P. 140+50 Lion Hub	6.46	396.36 ✓	8.14	389.90 ✓
Set BM			1.15	395.21 ✓
141+00	VOID see book 692 p. 9 J Kaysor		7.3	389.4 ✓
+50			7.2	389.2 ✓

Continued From F.B. # 692 - page 9 EWE

142+00			7.7	388.7 ✓
+50			7.8	388.6 ✓
143+00			8.0	388.4 ✓
+50			8.4	388.0 ✓

Spike in Cast Light pole # 74156 S.W. Corner of Woodside

		↑ 406.36		
1+94+0			8.5	387.9 ✓
T.P.	2.57	390.75 ✓	8.18	388.18 ✓
+50			3.8	387.0 ✓
145			9.0	386.8 ✓
+50			4.1	386.7 ✓
146			4.3	386.5 ✓
+50			4.7	386.1 ✓
147+0			4.4	386.4 ✓
+50			5.0	385.8 ✓
148+0			4.8	386.0 ✓

GT

		390.75			
148+50			5.1	385.7	✓
149+0			5.9	384.9	✓
+50			5.9	384.9	✓
T.P. on Rock					
150+0	2.98	387.56 ✓	6.17	384.58 ✓	
+50			3.5	384.1	✓
151+0			3.8	383.8	✓
+50			4.0	383.6	✓
152			4.1	383.5	✓
+50			4.4	383.2	✓

		I 387.56		
153+0			4.8	382.8 ✓
+50			5.2	382.4 ✓
154+0			5.5	382.1 ✓
+50			5.8	381.8 ✓
155+0			6.0	381.6 ✓
+50			6.6	381.0 ✓
156+0			6.9	380.7 ✓
T.P.	4.35	385.61 ✓	6.30	381.26 ✓
+50			5.4	380.2 ✓
157			5.5	380.1 ✓

		385.61		
157+50			5.9	379.7
158+0			6.0	379.6
+50			6.2	379.4
+85			4.8	380.8
159+0			6.1	379.5
+50			6.8	378.8
160+0			7.9	377.7
+50			7.6	378.0
161			7.9	377.7
TP.	6.10	384.42	7.29	378.32

		* 384.42	
161+50		7.1	377.3
162+0		7.3	377.1
+50		7.9	376.5
163+0		8.0	376.4
+50		8.5	375.9
+88.56	BC on Hob	8.52	375.90
164+0		8.6	375.8
+56		8.6	375.8
+78		7.6	376.8

		384.42		
+87		4.7	379.7	
+93	Bottom of Drainage ditch	7.0	377.4	
+95		4.1	380.3	
165+0		4.4	380.0	
+32		5.2	379.2	
+40		3.3	381.1	
+50		4.0	380.4	
Set PM		3.22	381.20	P.P. 72468. Spike. 55' - Lt 165+10
166		3.9	380.5	
+13 77	E.C on Hub	4.00	380.42	
+50		4.4	380.0	

		384.42		
167+0			5.1	379.3
+50			5.5	378.9
168+0			5.4	379.0
T.P.	4.71	384.08	5.05	379.37
+50			4.6	379.5
169			5.0	379.1
+50			5.4	378.7
170+0			5.8	378.3
+50			5.6	378.5
171+0			5.1	379.0

		T 384.08		
171+02	Ctr 2' Drainage ditch from Highway		6.2	377.9
+07			4.1	380.0
+50			4.9	379.2
172+0			5.1	379.0
+50			5.4	378.7
173+0			5.3	378.8
	CONT P. 57 BOOK 685 JK			
+50	VOID SEE P. 57, BOOK 685 JKeyser		5.3	378.8
174+0			4.9	379.2
T.P.	2.50	381.45	2.13	378.95
+50			3.2	378.3

↑ 381.45

175+00	on P.O.T. Hub		3.55	377.90
+50			4.4	377.1
+79	E. Side small ditch	Drainage	5.2	376.3
+83	Bottom		5.2	375.3
+88	W. side small ditch	Drainage	5.0	376.5
176+0		58	4.8	376.7
+25	SEE P. 57 & BOOK 685 Keyser		5.2	376.3
+50			6.4	375.1
177+0	L. on Hub		6.75	374.70

VOID

38145

+25	Begin rock riprap P.R. Roadbed +35	7.4	374.1	
+40		5.0	376.5	
+50	VOID See Book 685 Keyhot	4.4	377.1	
~~T.P.~~		~~5.22~~		
Check BM	S	2.34	379.11 = 379.17	at Riverview Steel Pin in Concrete USC&G Datum Pump plant
TP	5.07	5.22	376.23 = 376.29	
177+76 89	X on L Rock	7.1	374.3	
177+90		8.0	373.4	
178+0	Bottom water course	10.2	371.2	
+10		8.1	373.3	
+50		7.1	374.3	

		↑ 381.36		
179+0			7.8	373.6
+50	VOID	8.58 & 59	8.6	372.8
180+0	See F. Book 685 Keyston		9.3	372.1
+50			9.1	372.3
181			7.3	374.1
+50			7.4	374.0
182			7.5	373.9
+50			8.0	373.4
183			8.7	372.7
T.P.	4.39	379.01	6.74	374.62

T
379.01

183+50		6.6	372.4
184	VOID see p. 59 & 60 book 685 JKaynor	6.9	372.1
+34 of B.C on Hub		7.06	371.95
+50		7.2	371.8
185		7.2	371.8
+25		5.2	373.8
+50		4.5	374.5
186		4.7	374.3
+50		4.4	374.6

379.01

187			4.1	374.9
+50	(VOID) See P. 61 & 64 Book 685 Hayton		4.1	374.9
188			4.7	374.8
+50			5.5	373.5
+60	Int oil Paving		5.7	373.3
189			6.3	372.7
+50			6.8	372.2
+75	Edge Paving		6.6	372.4
190			6.4	378.6

		⊼ 379.01		
190+50			6.5	372.5
191+0			7.0	372.0
T.P.	4.86	377.56	6.31	372.70
+50			4.8	372.8
192			4.4	373.2
+50			4.4	373.2
+75			4.5	373.1
193			4.3	373.3
+44			4.5	373.1
+50			5.4	372.2

VOID

see p. 64 & 65 Book 68 J. Keyton

↑ 97756

193+38 ℄3	E.C. on Hub	7.43	370.13
194	(VOID) All S. 64, 65 & 63 took 685 J Foxton	7.5	370.1
+50		8.4	369.2
195		8.6	369.0
+50		7.0	370.6
+70 L.H		8.2	369.4
196+0		7.9	369.7
+10		6.1	371.5
+28.7	Int El Caption Ground pipe Line	6.1	
	Toppipet	10.1	
+35		5.7	371.9

37756

+45			3.0	374.6
+50	VOID See P. 63 book 685 JK		3.6	374.0
+55			3.6	374.0
	Rt Side con point		3.51	374.05
	&		3.65	373.91
	Lt Side		4.04	373.52
197+00 E.E.				
~~197+0~~			4.4	373.2
+05	edge oiled Burme		4.7	372.9
+15			3.2	374.4
T.P.	3.79	378.31	3.09	374.52
+50			4.3	374.0

CONT FROM P. 63, BOOK 685 JK

+70 58	Lt on Hub		4.66	373.65
197+92 98	BC		5.33	372.98

EQU. CHANGED IN OFFICE TO 195+75.79. SEE NOTE, P. 21, BOOK 694. JK

NOTE:- EQUATION 197+70.58 AHEAD = 195+74.03 BACK

SEE P. 63, BOOK 685 JK

↑ 378.31

198			5.3	373.0	
+25			6.7	371.6	
50			7.7	370.6	
Set BM.			3.93	374.38	Spike in pole #7241
199			8.9	369.9	
+50			9.0	369.3	
200			9.5	368.8	
+50			9.6	368.7	
201			9.9	368.4	
+50			10.1	368.2	
202			10.2	368.1	

20+-Lt
196+Ln

		π 378.31			
T.P. 202+13 3'	4.89 E.C.	373.03	10.17	368.14	
+50			4.1	368.9	
203			4.3	368.7	
+50			4.2	368.8	
204			4.9	368.1	
+50			4.6	368.4	
205			4.7	368.3	
+50			4.9	368.1	
206			5.1	367.9	
+50			5.6	367.4	
207			5.6	367.4	
+50			5.9	367.1	
10" CONC PIPE - STA 207+79 - TOP OF PIPE EL 365.6±					gK 5.15
85			5.4	367.6	
208			7.5	365.5	
T.P.	0.05	367.56	5.52	367.51	
+50			3.4	364.2	
209			4.0	363.6	
+50			4.1	363.5	
210			4.4	363.2	

		π 367.56			
+50			4.5	363.1	
211			4.7	362.9	
+50			5.1	362.5	
212			5.3	362.3	
Set BM			0.09	367.47	Spk. in P.P. # 73748 125'+ - 112+00
+50			5.5	362.1	
213			5.5	362.1	
+50			5.9	361.7	
214			5.1	362.5	
+50			6.3	361.3	
215			6.5	361.1	
T.P.	3.95	364.53	6 5.98	360.58	
+50			4.6	359.9	6K.76 Here
216			4.9	359.6	
+50			5.0	359.5	
217			4.9	359.6	
+50			4.5	360.0	
218			4.6	359.9	
+50			4.8	359.7	

		↑ 364.53			
219			4.9	359.6	✓
+50			5.5	359.0	✓
220			6.0	358.5	✓
+50			5.6	358.9	✓
221			5.8	358.7	✓
+12			5.3	359.2	✓
+38			1.3	363.2	✓
TP.	12.66	376.07 ✓	1.12	363.41	✓
222			12.8	363.3	✓
+50			13.3	362.8	✓
223			13.0	363.0	✓
+50			12.5	363.6	✓
224			11.1	365.0	✓
+50			3.7	372.4	✓
BM.	11.29	387.35 ✓	0.06	376.01	✓ BP #73743 Bolt-ct 224+35
225			11.1	376.2	✓
+50			2.7	384.6	✓
TP.	3.06	389.96 ✓	0.40	386.90	✓
226			1.8	388.2	✓

			℄ 389.96		
219					
+50	226+50			1.0	389.0
220					
+50	226+75			2.1	387.9
221					
+12	227			6.1	383.9
+38	+25			12.1	377.9
TP	T.P.	0.51	377.86	12.61	377.35
222	+50			6.0	371.9
+50	+80			12.1	365.8
223	228	E Bank	Water Course	11.8	366.1
+50	+12	ctr. "	"	12.7	365.2
224	+28	W Bank	"	11.6	366.3
+50	+50			12.8	365.1
BM.	229			12.7	365.2
225	+50			13.4	364.5
+50	230			14.0	363.9
TP.	TP.	1.99	367.29	12.56	365.30
226	+50			3.7	363.6

Note Fence Post 33'27 22+75

Sta	+	℄ 367.29	−	Elev
231			3.8	363.5
+50			4.3	363.0
232			4.5	362.8
+50			4.7	362.6
233			4.7	362.6
+50			4.5	362.8
234			4.1	363.2

Continued Right Hand Page 52 This Book

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.