

692

W 692

1845

6455

692

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 Roadway 16 feet wide. Side Slopes 1 on 1.
 For Single Track Embankment.

2.50
4.70

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1 1/2 see inside of back cover.
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 City of San Diego Water Dept.
 Room 268 Civic Center
 Telephone Main 5161

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Made in U. S. A.

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Profile - El Monte Pl. Northside Woodside
Ave. Line "C"

B.M. 2.36 411.31 408.95

~~112+55²⁵ VOID 2.5 408.8~~

see p. 10 & 11

JKayser

~~+69 2.2 409.1~~

~~113+00 3.1 408.2~~

~~+50 6.5 404.8~~

114+00 8.8 402.5

T.P. 4.39 406.56 9.12 402.19

114+50 5.3 401.3

115+00 5.2 401.4

Bloss
King
Dovles
Phillips.

3-1-45

Nail in Pole N.W. Cor. Woodside & River

406.56 ✓

115+50 6.2 400.4 ✓

116+00 5.8 400.8 ✓

116+50 6.4 400.2 ✓

116+65 7.3 399.3 ✓

117+00 6.7 399.9 ✓

+50 7.0 399.6 ✓

T.P. 2.79 403.05 6.30 400.26 ✓

118+00 3.9 399.4 ✓

+50 4.3 398.8 ✓

119+00 4.2 398.8 ✓

2

Top 8" O.D. CONC. Pipe

403.05 ✓

+50

4.7

398.4 ✓

120+00

5.2

397.9 ✓

+50

5.2

397.9 ✓

121+00

5.3

397.8 ✓

T.P.

5.52

403.77 ✓

4.80

398.25 ✓

+31

5.7

398.1 ✓

+32

6.9

396.9 ✓

+41

6.3

397.5 ✓

+50

5.8

398.0 ✓

Edge of oil

	403.77 ✓		
+65		6.2	397.6 ✓
122+00		7.0	396.8 ✓
+50		7.0	396.8 ✓
123+00		7.1	396.7 ✓
+28		5.1	398.7 ✓
+41		9.7	394.1 ✓
+50		9.7	394.1 ✓
124+00		9.2	394.6 ✓
+22		9.1	394.7 ✓

4

Edge of Oil

Top of Bank

Creek Bed

" "

" "

" "

403.77 ✓

+32 5.4 398.4 ✓

+50 5.9 397.9 ✓

125+00 8.2 395.6 ✓

B.M. 5.18 401.62 ✓ 7.33 396.44 ✓

+50 7.0 394.6 ✓

126+00 5.5 396.1 ✓

+50 4.2 397.4 ✓

127+00 5.3 396.3 ✓

+50 7.0 394.6 ✓

5.

Top of BANK

Set B.M. Nail in T.P. 25' LEFT STA 125+66

401.62 ✓

128+00

6.5 395.1 ✓

+50

7.4 394.2 ✓

129+00

6.1 395.5 ✓

+50

4.1 397.5 ✓

130+00

4.9 396.7 ✓

T.P.

2.56

399.78

4.40

397.22 ✓

+50

4.7 395.1 ✓

131+00

7.5 392.3 ✓

+19 Top 8" concrete
irrigation pipe

8.5 391.3 ✓

+50

7.6 392.2 ✓

399.78 ✓

132+00

7.8 392.0 ✓

+50

8.1 391.7 ✓

133+00

8.5 391.3 ✓

+50

8.6 391.2 ✓

134+00

9.1 390.7 ✓

+50

9.4 390.4 ✓

T.P. 5.97

396.85 ✓

8.90

390.88 ✓

135+00

6.6 390.3 ✓

+50

6.8 390.1 ✓

7

396.85 ✓

8

136+00

6.7

390.2 ✓

+50

6.9

390.0 ✓

137+00

6.5

390.4 ✓

+50

6.3

390.6 ✓

138+00

6.8

390.1 ✓

△ +15

7.0

389.9 ✓

+50

6.3

390.6 ✓

+92

5.5

391.4 ✓

139+00

4.9

392.0 ✓

396.85 ✓

139 + 16

5.5

391.4 ✓

+ 23

6.7

390.2 ✓

139 + 58.31" C LINE

6.9

390.0 ✓

= 140 + 50.65" A LINE

B.M.

1.65

395.20

395.25

CONTINUED IN F.B. #688 - Page 63 EWE

9
Spike in P. Pole S.W. Corner Ca. Jan

Profile El Monte Pk.

Cor. Woodside & River St

B.M. 2.71 411.66 411.66 408.95 ✓

712+55³¹ 5.5 406.2

112+36²⁵ 6.30 405.4

112+50 6.6 405.1

112+50² 6.6 405.1

112+71 5.9 405.8

112+82 6.4 405.3

113+00 5.3 406.4

4-21-46

10

Nail INT. P. SW. Cor. Woodside & River

Edge of Concrete

Edge of Concrete

Edge of Oil

411.66

113/26²²

4.6

407.1

- CONT ON P.1

JK -

11

Bliss

King

Phillips

5/14/96

Profile Levels for Lime Change

Woodside + River St. Lakeside

BM. 2.75 411.70 408.95

112135³¹ 4.6 407.1

+50 5.6 406.1

+71⁹⁸ = 26.98

11231²⁵ P.2. 6.4 405.3

+50²⁵ S. Edge Paving 5.77 405.93

+70⁷⁵ N " " 6.12 405.58

+80 6.6 405.1

113 5.5 406.2

+26³² 5.1 406.6

Elevations at LOS COCHES CREEK
 El MONTE PIPE line. STATE HIWAY
 Bridge 57-176

	+	H.I	-	ELEV
	5.20	401.64		396.44
T.P	3.63	404.33	0.94	400.70
			10.38	393.95
			10.42	393.91
			5.68	398.65
			10.14	399.19
T.P	2.63	400.88	6.08	398.25
			4.49	396.44 = 396.44

6-24-46
 clear-warm

Nelson
 Leonard
 Davis
 Rice 13.

BM TEL pole 25' Left sta 125+66

Elev Govt BM #3

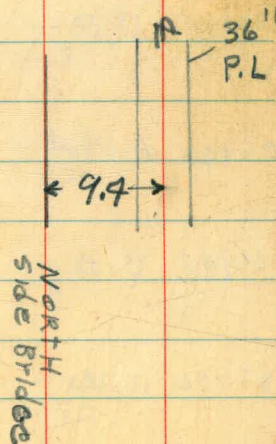
" P.L. EAST End Bridge

" " West " "

Elev TOP of batter of bridge N. side

Elev R. creek where 68" P.L. crosses

CK B.M.



X SECTIONS B.O. & AVA LO-
CATIONS El Monte P.L.

113 + 91 AVA Elev from 719700

177+95 B.O. Elev from 178700

+85

+78

187+50 AVA Elev from 187700

220+95 B.O. Elev from 221700

226+90 A.V.A. Elev from 226750

239+45 B.O. Elev from 239750

267+50 A.V.A.

10-7-46
clear-cool

Nelson
Phillips
Griffin

14

+0.7 +0.6 +0.4
7 7

+0.2 0.0 -0.4 +0.1
7 4 7

0.0 -0.8 -1.2 0.0
7 3 7

-4.3 -4.1
7

+3.8 -3.6
10 10

+5.0 +0.5 +0.2 +0.2
14 5 7

+3.2 +0.1 -3.3
10 10

0.0 -0.2 -0.1
7 7

+1.5 +0.8 -1.3 -1.3
10 5 6 10

299+23 A.V.A. Elev From 299

-0.3 -0.5 -0.8
7 7

322+55 B.O. Elev from 322+50

-0.1 -0.5 -0.8 -0.6
7 4 10

363+00 A.V.A.

-0.2 +0.1 +0.1
8 4 7

366+60 B.O. Elev from 366+50

+0.3 +1.1 +2.2 +2.2
13 6 10.0

380+18 A.V.A. Elev from 380+50

+1.2 +0.8 +0.3
7 7

382+45 B.O. Elev from 382+50

+1.7 +1.4 +1.3
10 10

410+80 A.V.A.

434+43 A.V.A. Elev from 434+50

-1.7 -0.2 +2.2
10 10

439+20 B.O.

548.6 548.8 548.9
10 6

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature horizontal blue lines for writing. Each page is also ruled with vertical red lines, creating a grid-like structure with four columns. The right page has the number '16' written in the top right corner. The notebook is bound in the center, and the pages appear slightly aged with some minor discoloration and faint smudges.

Grade Elev's EAST Portal
Grossmont Tunnel

10-8-46

clear-ood

Nelson
Phillip
Griffin

10.98 55391 Rod Gr. Rod 542.93

B.M. P.P.H 76981

5.16 5.16 548.75

Elev TOP of Ties

448+50

4.96

0.0

+75

5.16

0.0

449+00

5.16

0.0

+25

5.16

0.0

+48

5.16

0.0

+75

5.16

0.0

5+00

5.16

0.0

+23

4.96

0.2

Grade Elev EAST Portal
DAILY WORK NOTES

	+	H I	-	Elev
	12.25	555.18		592.93
			G. R.	
			6.18	549.00
	10.60	553.53		592.93
	4.83	553.54	4.82	548.71
			G. R.	
			4.54	549.00
	4.845	553.845		549.00
450+83			GR	
			4.825	549.02
			GR	
	4.79	553.79	4.77	549.02 549.00
	4.70	552.98	5.51	548.28
451+23			GR	
			3.95	549.03
	4.51	553.51		549.00
451+56			G. R.	
			4.47	549.04
	4.88	553.16		548.28
			4.58	548.58

10-22-46
clear-warm

Nelson
Leonard
Phillips
GRIFFIN

18

B.M. Power Pole

Set B.M. Iron Pin North side Tunnel ent.

10-25-46 RAINY same party
Sta of conc Moh at East
Entrance to Tunnel 450+28.97

10-30-46
clear-warm

Nelson
Leonard
Phillips
GRIFFIN

Set B.M. STA 450+89 & Iron PIN

Set #24

11-1-46
clear-warm

Nelson
Leonard
GRIFFIN

11-4-46
clear-warm

Nelson
Leonard
GRIFFIN

Set B.M.

			Grade Rod	Grade Elev	
451789	4.92	553.50			548.58
			G.R.	4.45	549.05
	4.65	552.93			548.28
				4.35	548.58 = 548.58
452723	4.95	553.53			548.58
			G.R.	4.47	549.06
452770	4.95	553.53			548.58
			G.R.	4.46	549.07
453700	4.56	553.14			548.58
				4.06	549.08
CK El set	11-7-46			4.10	549.09
	4.84	553.42		4.33	549.09
					548.58
CK EL set	11-8-46			4.53	548.89
Set CONC MON & B.M. at Rib					
#bb see page A8					Elev of B.M.
				548.85	← 548.75

19

11-6-46
clear-hot

Nelson
Leonard
Griffin

CK BENCH

11-7-46
clear-cool

Nelson
Leonard
Griffin

11-8-46
cloudy-cool-Rain

Nelson
Leonard
Griffin

11-12-46
cloudy-cool

Nelson
Leonard
Griffin

11-13-46
RAIN-cool

Nelson
Leonard
Griffin

	4.76	553.51 ⁶¹	548.85 548.75
#80 453+30		G.R 4.42 4.52	549.09
#80		+2.51	556.02 ¹²
CHECK		4.79	549.77 ⁸⁷
#68 see PAGE 47		+2.27	555.78 ⁸⁸ 548.94
		4.67	548.84
	4.44	553.28 ³⁸	548.94 548.84
#86		G.R 4.28 4.18	549.10
#80		+2.68	56.06 55.96
#86		+2.72	556.10 556.00
453+90 #95 T.P. TOP #92	4.625	553.565 553.465	548.94 548.84
		VOID 4.34	Reset 11-20-46 549.12
	-0.70	555.48 555.28	556.180 556.080
	4.56	552.84	548.28
		4.25	548.59 = 548.59
		3.99	548.85 = 548.75
		3.90	548.94 = 548.84

11-14-46
RAIN-COOL

Nelson
Leonard
GRIFFIN 20

11-20-46 Corr
Note
Grade set 0.10 high

TOP ARCH

TOP FT BLK with 8" EXT. 549.77 + .67 = 549.44

TOP ARCH

set B.M. between #79 & #80 LT side

Line point set 11-12-46

checked o.k.

11-15-46
clear-warm

Nelson
Leonard
GRIFFIN

NOTE
GRADE SET 0.10 HIGH 11-20-46 Corr

11-19-46

clear-warm

555.48 H.I. OF TRANSIT <sup>see
pages
55-57</sup>

11-20-46
RAINY-COOL

Nelson
Leonard
BARRAGAN

CK B.M.

CK B.M. 0.10 off

CK B.M. 0.10 off

	4.40	553.34		548.94
453+90	4.75	548.59	=	548.59
# 95	G.R.	4.22	549.12	
set B.M.	4.70	548.64		
# 92	+2.83	556.17		
# 95	4.37	548.97		
	+2.83	556.17		

New station of Portal
449 + 52.3

	4.72	553.36		548.64
# 100	G.R. Grade	4.23	549.13	
	+2.72	556.08		
	4.33	552.97		548.64
# 106	3.84	549.13		
	+3.22	56.19		

11-20-46
R3174-Cool

Same party
21

corrected B.M.

OK B.M. O.K

set B.M. between # 93 & 94 Lt side

see page 57

Top of spreader

see page 57

11-21-46
clear-cool

Nelson
Leonard
Bartagay

11-22-46
cloudy-cool

Nelson
Leonard
Phillips

454+80 4.88 553.52 548.64
117

G R Grade
4.37 549.15

+2.59 556.11

102

+2.54 556.06

4.88 553.52 548.64

455+10
125

4.89 548.63
G R Grade
4.36 549.16

125

+2.60 56.12

4.91 553.55 548.64

CKBM

455+34
131

4.92 548.63 = 548.63
G R Grade
4.39 549.16

131

+2.65 56.20

125

+2.57 56.12

5.658 54.298 548.64

4.01 53.363 4.945 49.353

5.074 53.284 5.153 48.210

3.550 53.304 3.530 49.754
10.440 42.864 = 42.93

Nelson 17 22
Leonard
Barragan

11-25-46
Clear-Warm

see page 57

11-26-46
clear-Warm

Nelson
Leonard
Barragan

Set B.M. sta 455+00 122-123

11-27-46

Set MON sta 454+00 bet 97 & 98

	10.49	53.37		542.93
T.P	3.86	53.68	3.55	49.82
T.P				
CK BM	5.55	53.83	5.40	48.28 = 548.28
			5.13	48.70 = 548.69

	4.73	53.42		548.69
#137			G.R. Grade	
			4.25	549.17
			+2.76	56.18

T.P	4.44	53.80	4.06	49.36
-----	------	-------	------	-------

#131			+2.45	56.25
------	--	--	-------	-------

	4.82	53.51		48.69
456+22			G.R. Grade	
#151			4.32	549.19
			+2.72	56.23

	10.97	53.90		42.93
--	-------	-------	--	-------

T.P	3.63	53.46	4.07	49.83
-----	------	-------	------	-------

	5.22	53.50	5.18	48.28 = 48.28
--	------	-------	------	---------------

BENCH POWER pole

CK B.M.

11-28-46
clear-warm
CORRECTED B.M.

Nelson
Leonard
BARRAGAN

12-2-46
clear-warm

Nelson
Leonard
BARRAGAN

12-3-46
clear-warm
BENCH Pow pole

Nelson
Leonard
BARRAGAN

CK. B.M.

53.50

4.86 53.57 4.79 48.71 = 48.70

4.59 48.98

4.87 53.58 = 48.71

4.75 548.83

4.86 48.72 = 48.69

4.63 53.35 48.73

#159

G.R. Grade
4.15 549.20

5.15 48.20

#159

+2.83 56.18

#151

+2.88 56.23

5.13

53.33

48.20

457+02
#167

G.R. Grade
4.11 49.27

+2.88 56.21 = 56.17

457+32
#173

5.27 53.47

48.20

G.R. Grade
4.24 49.23

+2.80 56.27

#167

+2.72 56.19

CK B.M

B.M. "O" on CONC MON STA 454+00

set B.M. bet 133 & 134 on ^{steel} P17

CK B.M

used collected B/M

548.20

set B.M. LT side bet 156 & 157

12-4-46
cloudy-cool

Nelson
Leonard
BARRAGAN

11-5-46
clear-warm

Nelson
Leonard
BARRAGAN

	5.38	53.58		48.20
#178			G.R.	Grade
457+57			4.34	49.24
			+2.72	56.30
#173			+2.69	56.27

	5.62	53.82		48.20
458+03			5.46	48.36
#187			G.R.	Grade
			4.57	49.25
			+2.39	56.21

	4.83	53.19		48.36
458+52			G.R.	Grade
H 197			3.92	49.27
458+52				
#197			+3.08	56.27
H 187			+3.02	56.21

	5.09	53.45		48.36
458+87			G.R.	Grade
#204			4.17	49.28
			+2.78	56.23

12-6-46
cloudy-cool

Nelson
Leonard
Bartagath

25

12-8-46
cloudy-cool
set B.M

same party

12-10-46
clear-warm

same party

12-11-46
clear-warm

same party

set CONC MON 458 #10⁺

5.12 53.48 48.36
#211 G.R. grade
459+22 4.19 49.29

+2.90 56.38

5.22 53.62 48.40

4.73 48.89

4.79 53.63 48.89

459+65
#219

G.R. Grade
4.33 49.30

4.74 53.63 48.89

+2.57 56.20 = 56.05

5.15 53.40 48.85

4.92 53.66 5.26 548.74

CLKBM, 4.22 53.10 4.78 48.88 = 48.89

460+13
H229

G.R. Grade
3.78 49.32

LT FT BLK 3.83 3.3

RT " " 3.84

+2.96 56.06 = 56.07

12-12-46
CLEAR-COOL

Nelson
Leonard
Bartagay

26

12-13-46
clear-warm

Nelson
Leonard
Bartagay

Corrected B.M. See Page 78

set WORK B.M.

12-16-46
CLEAR-COOL

Nelson
Leonard
Bartagay

set B.M. Rod in cork Mort 458+10 ±

	4.41	53.29		48.88
#232 460+33			G.R. Grade 3.97 49.32	
LT			3.82	
RT			3.81	
TOP			+2.97 56.26 = 56.07	

	4.77	53.65		48.88
#242 460+78			G.R. Grade 4.32 49.33	
LT			4.10	
RT			4.12	
TOP			+2.69 56.34 = 56.09	

	5.03	53.91		48.88
#254 461+38			G.R. Grade 4.56 49.35	
			+2.55 56.46 = 56.10	

	5.11	53.99		48.88
#258 461+58			G.R. Grade 4.63 49.36	
			+2.39 56.33	11

12-19-46
clear-cool

Nelson
Leonard 27
Barragan

12-20-46
clear-warm

Nelson
Leonard
Barragan

12-22-46 Sunday
cloudy-warm

Nelson
Leonard

12-23-46
cloudy-warm

Nelson
Leonard
Barragan

Set B.M. bet 253 & 254 Lt side

	+	H.I	-	Elev	
	4.61	53.69			B.M. 49.08
461+93 #265			G.R. 4.32	Grade 49.37	
			+2.65	56.34 = 56.12	
RTFT BLK			4.06	49.63	
	4.78	53.86			B.M. 49.08
#269 462+14			G.R. 4.48	Grade 49.38	
			+2.47	56.33	
check #265			+2.47	56.33	
	4.68	53.76			B.M. 49.08
462+34 #273			G.R. 4.38	Grade 49.38	
			+2.53	56.29	
check #265			+2.56	56.32	
	4.72	53.80			B.M. 49.08
#287 463+09			G.R. 4.39	Grade 49.41	
			+2.66	56.46 = 56.16	

12-24-46
cloudy-warm

Nelson,
Leonard
Barragan

28

12-26-46
cloudy-cool

same party

12-27-46
cloudy-rain

same party

12-30-46
clear-warm

same party

12-31-46
clear-warm

Nelson
Leonard
Barragan

29

4.56 53.64 49.08

295
463+44

4.65 48.99
G.R. Grade
4.22 49.42

LT FT BLK

4.05 49.59

+2.74 56.38

CHECK
287

+2.80 56.44

4.79 53.78 48.99

301
463+74

G.R. Grade
4.35 49.43

LT FT BLK

4.33 49.45

+2.47 56.25 = 56.18

RT FT BLK

4.32 49.46

300

+2.59 56.37 = 56.18

4.55 53.54 48.99

464+14
309

G.R. Grade
4.09 49.45

+2.65 56.19

RT

4.13

LT

4.10

1-2-47
clear-warm

Nelson
Leonard
Barragan

set CONC MON #4 sta 462 tood

1-3-47
clear-warm

same party

	4.75	53.74		48.99
464+90 #324			G.R. Grade 4.27	49.47
			+2.25	53.99
LT			4.40	49.34
RT			4.60	49.14
#314			+2.58	56.32
#325			+2.28	56.02

	4.61	53.60		48.99
#329 465+15			G.R. Grade 4.12	49.48
			+2.79	56.39
RT			3.98	
LT			4.02	
T.P CHECK Grade 017324	3.99	53.50	4.09	49.51
LT			2.02	51.48
RT			2.03	51.47

1-6-47
cloudy-cool

Nelson
Leonard
Barragatt

30

1-7-47
clear-warm

Nelson
Leonard
Barragatt

	4.73	53.72		48.99
Set B.M.	4.60	53.67	4.65	49.07
465+36			G. R. Grade	
#334			4.18	49.49
LT FT BLK			4.18	49.49
RT FT BLK			4.12	49.55
			+2.61	56.28 = 56.24

	4.81	53.88		B.M. 49.07
465+57			G. R. Grade	
339			4.39	49.49
LT FT BLK			4.37	
			+2.40	56.28 = 56.24
RT FT BLK			4.35	
CK 334			+2.40	56.28

	4.88	53.95		B.M. 49.07
465+73			4.45	49.50
343			+2.44	56.39

Nelson
Leonard
Barragan

31

1-8-47
Clear-warm

Set B.M.
LT side Sta 465+02 bet 327 & 328

1-9-47
clear-warm

same party

1-10-47
clear warm

same party

	H.I			B.M.
# 349 465+97	4.89	53.96		49.07
			G.R. Grade	
			4.46	49.50
			+2.37	56.33 = 56.25
CK # 343			+2.43	56.40 = 56.25
	4.46	53.53		49.07
			G.R. Grade	
			4.02	49.51
# 353 466+18			+2.82	56.35 = 56.26
CK 349			+2.81	56.34 = 56.25
	4.63	53.37		548.74
T.P.	5.24	54.11	4.50	548.87
CK B.M.			4.97	49.14 = 49.07
	10.93	53.86		42.93
CK TP	3.91	53.74	4.03	49.83 = 49.83
CK BM	5.06	53.35	5.45	48.29 = 48.28
CK BM	4.57	53.69	4.23	49.12 = 49.02
CK BM			4.79	48.90 = 48.85
CK BM	4.50	53.25	4.94	48.75 = 48.74

Nelson
Leonard
Bartagath

32

1-13-47
cloudy-rainy

1-14-47
cloudy-cool

same party

B.M. conc Mon # 3

set B.M. Rod in conc Mon # 4 462+00

1-15-47
clear-cool

same party

B.M. Power pole

BERGER LEVEL

T.P. outside Portal

B.M. Pin on ϕ

B.M. '0' on ^{STA 454} Mon # 2 see page 78

B.M. PIN on ϕ bet RIB 133 & 134

B.M. Pin in conc Mon # 3

53.25
 CK BM 4.82 53.69 4.38 = 48.87 = 48.87

CK BM 4.64 49.05 = 48.99

4.84 53.98 49.14

466+30
 #357

G.R. Grade
 4.47 49.51

+2.45 56.43

CK
 #353

+2.43 56.41

4.64 53.78 49.14

#364
 466+68

G.R. Grade
 4.26 49.52

+2.60 56.38 = 56.27

R.T FT BLK

4.16

L.T FT BLK

4.23

CK
 353

+2.62 56.40

4.98 53.85 BM
 48.87

T.P.
 CK BM 4.71 53.87 4.69 49.16 = 49.14

#373
 366+98

G.R. Grade
 4.34 49.53

+2.48 56.35 = 56.28

R.T FT BLK

4.23

L.T FT BLK

4.24

B.M. Pin in coin MON #4 STA 462

B.M. Pin left side bet Rib 288-289

Corrected B.M. see page 32

1-17-47
 Clear-Warm

Nelson
 Leonard
 Barragan

1-20-47
 Clear-Warm

Nelson
 Leonard
 Barragan

	4.89	54.05		B.M. 49.16
			5.21	48.84
#378 467+18			4.51	49.54
			+2.38	56.43
RT FT BLK			4.40	49.65
LT FT BLK			4.32	49.73

	5.10	53.94		48.84
#382 467+34			9.39	49.55
LT FT BLK			4.11	49.83
RT FT BLK			4.03	49.91
#382			+2.70	56.64
#383			+2.54	56.48
#384			+2.63	56.57

	5.08	54.24		49.16
CK BM			5.38	48.86 = 48.84
467+59 #388	4.72	53.58		48.86
			4.03	49.55
			+3.00	56.58 = 56.30

1-21-47
clear-warm

Nelson
Leonard
Barragan 34

corrected B.M see page 33 date 1-20-47
steel pin
set B.M sta 467+00 Lt side

1-22-47
clear warm

same party

1-23-47
clear-warm

same party

	4.96	53.82		48.86
394 A67483			G.R. Grade 4.26 49.56	
			+2.74	56.56 = 56.31
RT			4.09	49.73
LT			4.00	49.82
CK 388			+2.76	56.58
CK 384			+2.65	56.47

468+23 404	4.89	53.75		48.86
			4.17	49.58
			+2.55	56.30 = 56.33
LT FT BLK			4.22	
RT FT BLK			4.27	
CK 394			+2.82	56.57

	8.77	51.70		42.93
T.P	4.98	53.74	2.99	48.76
CK				
B.M	4.90	53.20	5.44	48.30 = 48.29
CK				

1-24-47
Clear-warm

Nelson
Leonard
Batt 29 AM

35

1-27-47
Clear-warm

same party

Set MON #5 sta 464+95 opposite
Rib # 325 2 1/2" by 30" steel pipe
With Wood Plug & Tack.

1-28-47
R21 AM
B.M POWER POLE.

same party

53.20

CK BM		4.03	49.17 = 49.12
CK BM	4.75	53.66	4.29 48.91 = 48.90
CK BM	4.55	53.55	4.86 48.80 = 48.75
CK BM	4.88	53.80	4.43 48.92 = 48.87
CK BM		4.58	49.22 = 49.16

	5.28	53.57		48.29
CK BM	4.43	53.57	4.43	49.14 = 49.12
CK BM			4.67	48.90 = 48.90
CK BM	4.73	53.99	4.81	48.76 = 48.75
CK BM	5.03	53.92	4.60	48.89 = 48.87
CK BM	4.74	53.91	4.75	49.17 = 49.16
CK BM			5.05	48.86 = 48.86

	4.77	53.63		B.M. 48.86
Reset #404			G.R. 4.05	Grade 49.58
			4.72	48.91
			+2.63	56.26 =

1-28-47
Rail

Nelson
Leonard
Barragan

36

see page 32

" " " pit bet rib 133-134

" " " CONC MOT #3

checked line point 1-28-47
checked o.k.

sta 462+00

1-31-47
clear-warm

same party

set B.M Lt side bet 401 & 402

468+43 RIB #409	4.76	53.67		48.91
			CR GRADE	
			4.08 49.59	
			+2.79 56.41	

468+53 #412	5.16	54.07		48.91
			G.R. grade	
			4.98 49.59	
LT			4.38	
			+2.41 56.48	
RT			4.35	
CK #409			+2.35 56.42	
CK #409			+2.28 56.35	

468+79 #18	5.23	54.14		B.M. 48.91
			4.55 49.59	
			+2.42 56.56	
LT			4.34	
RT			4.42	
			+2.30 56.44	

2-1-47
CLEAR WARM

BM STA 468+12

DHRBY

37

2-3-47
clear-warm

Nelson
Leon 3rd
Bart 3987

2-4-47

Clear-Hot

Nelson
Leonard
Bart 3987

5.36 54.27 48.91

423 469+02 4.67 49.60

5.36 (48.91) →

RT 4.60

LT 4.60

+2.18 56.45 = 56.35

CK

412

+2.22 56.49

B.M.

48.91

5.11 54.02

CKBM 4.79 53.95 4.86 49.16 = 49.17

CKBM 5.10 48.85 = 48.89

5.04 53.95 48.91

469+28

429

G.R. Grade

4.34 49.61

RT 4.19

LT 4.23

+2.60 56.55 = 56.36

CK

423

+2.50 56.45

Nelson
Leonard
Battaglia

38

2-5-47
Clear-Hot

set B.M. 469+00 Lt side

2-6-47
Clear-Warm

same party

	10.96	53.89		542.93
CK T.P.	4.00	53.83	4.06	49.83 = 49.83
CK B.M.	5.18	53.48	5.53	48.30 = 48.29
CK B.M.	4.44	53.60	4.32	49.16 = 49.14
CK B.M.			4.69	48.91 = 48.90
CK B.M.	4.84	53.60	4.84	48.76 = 48.76
CK B.M.	5.07	53.96	4.71	48.89 = 48.89
CK B.M.			4.77	49.19 = 49.17

469+64				
437	5.12	54.03		48.91

	4.41	49.62
--	------	-------

LT	4.36
----	------

RT	4.32
----	------

	+2.39	56.42
--	-------	-------

CK		
429	+2.52	56.55

	5.24	54.15		48.91
--	------	-------	--	-------

470+05		G.R.	Grade
445		4.52	49.63
LT		4.39	
		4.29	
		+2.44	49.59

2-7-47
HAZE - COOL

Nelson
Leonard
Battagay

39

B.M. Power Pole

Set originally @ 48.28

" " @ 48.98

Set originally @ 48.83

Set originally @ 48.74

" " @ 48.87

" " @ 49.07

BM 469+00

Use Mon #5 for line

2-10-47
cloudy - warm

Same Party

CHECK

437

+2.29 56.44

	5.05	53.99		48.89
CKBM	5.01	53.97	4.98	48.96 = 49.91
470134			G.R.	Grade
451			4.33	49.64
RT			4.15	
LT			4.14	
			+2.63	56.60
CK			+2.70	56.67
445				

470157 48.96 549.64

4	4.64	53.60		48.96
470194			G.R.	Grade
463			3.94	549.66
RT			3.73	
LT			3.81	
			+2.99	56.59
CK			+3.02	56.62
456				

2-11-47
clear-water

Nelson
Leonard
Bart 298H

40

B.M. sta 462+00

B.M. sta 469+00 Use 548.96

469+00 B.M.

2-13-47
clear-hot

same party

	5.33	54.29		48.96
#471+24 #469	4.48	53.76	5.01	49.28
RT			4.09	49.67
LT			3.93	
			+2.85	56.61
CK 463			+2.83	56.59

403 53.31 49.28

SET #474 3.63 49.68

	4.62	53.90		49.28
471+85 481			4.21	49.69
RT			4.12	
LT			4.07	
			+2.69	56.59
CK 463			+2.68	56.58

Nelson
Leonard 41
Barr 2937

2-19-97
Clear-Hot

between Ribs
set BM 467 & 468 Lt side
Elev 49.28

set MON #6 sta 469+00
2 1/2" x 30" steel pipe, center
punch hole on Portal edge
of pipe

BM 6.00
1.63 49.67
4.37

RIB #474 +25'
25
.032
50
75
00800

49.28
4.62
53.90
49.69
4.21

CHECK B.M.S

3.35 53.18 599.83

5.05 53.35 4.88 548.30 = 48.30

4.15 53.31 4.19 49.16 = 49.16

4.40 48.91 = 48.91

4.43 53.19 4.55 48.76 = 48.76

5.18 54.07 4.30 48.89 = 48.89

4.55 53.74 4.89 49.19 = 49.19

4.77 48.97 = 48.96

4.85 53.82 48.97

CK BM 4.51 49.31 = 49.28

4.89 54.20 49.31

472+35
491

4.49 49.71

RT

4.33

+2.42 56.62

LT

4.36

CK481

+2.43 56.63

2-17-47
cloudy-coolNelson
Leonard 42
Battagar

T.P

97

34

1

2212

32

4424

6636

70784

sta 462+00

sta 469+00

2-19-47
clear-warm
USE 49.31

49.31

4.89

57.20

49.71

4.49

49.71

6.75

46

62

46

16

2-21-47

43

	4.38	53.69		B.M. 49.31
473+05	4.93	54.30	4.32	49.37
505	4.93		4.57	49.73
RT			4.44	
LT			4.45	
			+2.33	56.63

	986	54.23		49.37 BM
RIS 515 473+55			4.48	49.75 GRADE

473+85	4.56	53.93		49.37
521			4.17	49.76
RT			4.10	
LT			4.05	
			+2.70	56.63
CK 515			+2.62	56.55

Set BM STA 473+03 LT side

49.31	
4.38	
53.69	49.73
4.32	6.75
49.37	56.48
4.93	
54.30	
49.73	
4.57	

50'	6.00
32	2.98
100	3.52
150	

.02600	49.37
	4.56
	53.93
	49.76
	4.17

49.75
4.75
50

	4.45	53.82		49.37
#530			G.R. Grade	
474+31			4.05	49.77
LT			3.92	
RT			3.90	
			+2.88	56.70
CK				
521			+2.81	56.63

	5.03	54.40		49.37
474+61			G.R. Grade	
#536			4.62	49.78
RT			4.51	
LT			4.47	
			+2.27	56.67
CK 530			+2.30	56.70

	4.26	53.63		49.37
474+96				
543			3.84	49.79
LT			3.83	
RT			3.72	
CK 536	see page		+3.00	56.63
	46		+3.03	56.66

2-25-47
CLEAR-COOL

Nelson
Phillips
Barr 392H

44

2408

32

4816

7229

77056

49.37

4.45

53.82

49.77

4.05

49.77

6.75

52

2-26-47
cloudy-COOL

Nelson
Nremow
Barr 392H

25

32

50

75

800

49.37

4.26

53.63

49.79

3.84

3.83

2-27-47
Very-Cloudy
COOL

Nelson
Phillips
Barr 392H

49.79

6.75

56.54

Location & Elev's 2 wells
south of Sta 494 + Gross, Tunney

	H.I	Elev
#1 well	0.76	678.51
Surface Elev.	10.12	668.39

#2 well		
Surface Elev.	9.27	669.24

1-7-47	same party
clear warm	
0.85	678.60
	B.M. 677.75

T.P.	1.38	672.18	7.80	670.80
------	------	--------	------	--------

TOP of casing	2.65	669.53
---------------	------	--------

TOP PUMP stand plate	2.36	669.82
----------------------	------	--------

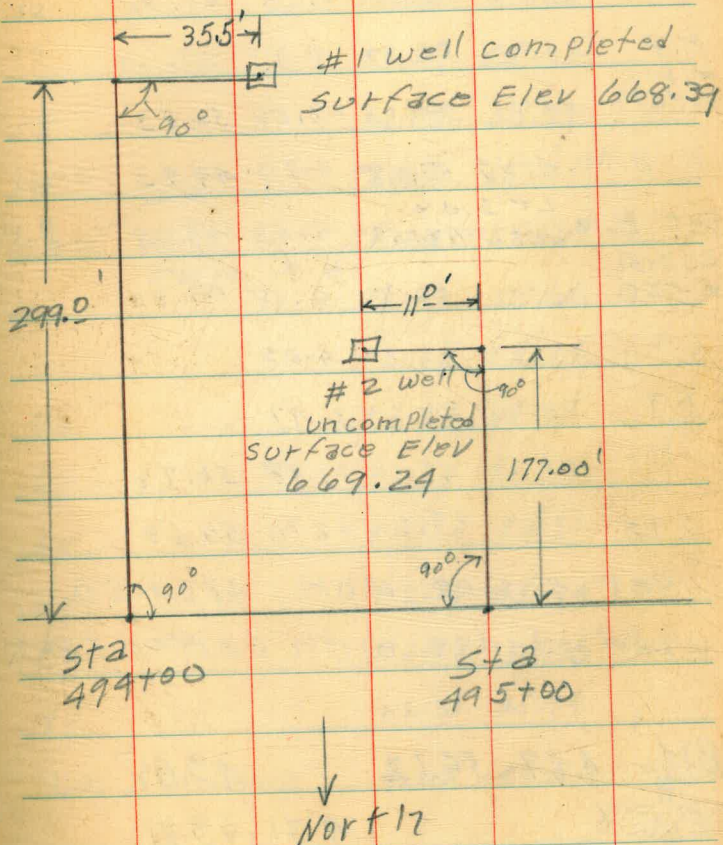
T.P.	6.90	678.30	0.78	671.40
------	------	--------	------	--------

CK.B.M	0.55	677.75 = 677.75
--------	------	-----------------

12-4-46
cool cloudy

Nelson
Leonard 45
Bart 89217

B.M. CONC MON. Sta 492 + 89 ⁶⁸ F.B. 699



2-28-47
cloudy-cool

Nelson
Phillips
Barr 2987

572462
B.M.
548.89
464+93

4.63	53.52			
set B.M. MON #5	S.E. Edge PIPE STA			
4.56	53.58	4.50	49.02	
set B.M. MON #6	EAST edge PIPE STA			469.00
4.50	53.88	4.20	49.38	
T.P	+2.90	54.07	2.71	51.17
T.P				
TOP 497	-2.50	54.13	+2.56	56.63
CK B.M.	4.55	53.98	4.70	49.43 = 49.37
Set B.M.	L+ side			
475+31	Bot 399+550	4.53	49.45	- B.M.
#550		G.R. grade		
		4.18	49.80	
L+		4.03		
RT		3.97		
		+2.78	56.76	
543		+2.70	56.68	
Set TEMP MON 473+50				
WOOD WEDGE WITH COPPER TACK				
BM	4.67	54.12		49.45
#				
RIB 556		4.31	49.81	
see page 80				

12-3-46

Nelson
Leonard
Barr 2987

46

Roof Elev's			
RIB NO	4.76	53.04	548.28
15		+2.66	55.70
16		+2.61	55.65
17		+2.67	55.71
18		+2.70	55.74
19		+2.67	55.71
20		+2.65	55.69
21		+2.62	55.66
65		+2.75	55.79
66		+2.83	55.87
67		+2.74	55.78
68		+2.73	55.77
69		+2.70	55.74
70		+2.72	55.76
71		+2.75	55.79
CK B.M.	4.05	48.99	= 48.99

Elevs TOP RIB & Rails

553.20
553.18

#67 +2.62 555.80

4.25 548.93

#68 SEE PAGE 20 +2.63 555.81

4.28 548.90

#69 +2.58 555.76

4.27 548.91

#70 +2.59 555.77

4.22 548.96

#71 +2.61 555.79

72 +2.63 555.81

73 +2.71 555.89

74 +2.75 555.93

4.01 549.17

75 +2.75 555.93

4.12 549.06

553.15
76

11-12-46

47

TOP FT BLK

TOP FT BLK

Elev's TOP RIB & TOP RAIL

4.44 553.44 549.0

4.13 553.47 4.16 549.34

450742
#6

4.54 548.93

+2.47 555.94

450784
#16

4.55 548.92

+2.24 555.71

451740
#30

4.64 548.83

+2.30 555.77

T.P

3.92 553.19 4.20 549.27

CK B.M 4.76 553.35 4.60 548.59 = 548.58

#58

+2.43 555.78

#60

4.52 548.82

+2.52 555.87

452774
#65

+2.46 555.91

4.40 548.95

#66

+2.52 555.87

4.36 548.99

T.P

Set B.M 4.43 553.18²⁸ 4.60 548.75

should be

SEE PAGE 47 548.85
see P20

11-12-46
Cloudy-Cool

NELSON
LEONARD
GRIFFIN

48

ON RAIL

TOP ARCH

USED 548.59 ahead

TOP SPREADER

TOP SPREADER

STEEL PIN IN 2nd CONC MON

DISTANCES FROM SPRING LINE
TO E of tunnel

RIB		L	R
1			549.00
2			
3			
4	44.4	3.70	3.62
5	44.4	3.70	3.57
6	44.65	3.72	3.56
7	45.1	3.75	3.62
8	43.7	3.76	3.61
9	43.0	3.75	3.55
10	42.1	3.76	3.54
11	43.8	3.64	3.66
12	43.6	3.57	3.66
13	43.9	3.58	3.66
14	43.7	3.50	3.61
15	43.1	3.51	3.62
16	43.1	3.65	3.50
17	42.2	3.63	3.50
18	42.2	3.65	3.49

These read
1195 taken
11-19-46

11-12-46
cloudy-cool

		L	R
19	42.8	3.53	3.30
20	42.5	3.57	3.34
21	43.4	3.51	3.41
22	43.6	3.54	3.45
23	43.0	3.59	3.36
24	42.2	3.62	3.40
25	42.6	3.60	3.39
26	43.3	3.63	3.43
27	42.8	3.55	3.41
28	42.0	3.58	3.45
29	42.1	3.48	3.41
30	42.8	3.52	3.45
31	44.5	3.52	3.38
32	44.9	3.55	3.42
33	45.0	3.59	3.43
34	45.6	3.61	3.47
35	46.1	3.55	3.45
36	44.9	3.57	3.43

Melson
Leonard 49
Griffith

37	43.2	3.55 3.60	3.51 3.59
38	43.2	3.56 3.60	3.58 3.61
39	42.8	3.52 3.57	3.60 3.61
40	43.1	3.55 3.59	3.60 3.64
41	11-19-46 clear water	3.53	3.61
42		3.50	3.64
43		3.43	3.60
44		3.54	3.61
45		3.48	3.65
46		3.50	3.62
47		3.56	3.57
48		3.63	3.49
49		3.62	3.51
50		3.51	3.64
51		3.52	3.63
52		3.53	3.66
53		3.49	3.66
54		3.54	3.63

Welson
Leonard
BHT3907

55		3.55	3.62
56		3.59	3.56
57		3.62	3.52
58		3.72	3.47
59		3.61	3.47
60		3.57	3.56 over PIPE
61		3.56	3.58 " "
62		3.49	3.59 " "
63		3.47	3.63 " "
64		3.45	3.60 NO PIPE
65		3.37	3.66
66		3.39	3.52
67		3.36	3.51
68		3.33	3.48
69		3.52	3.45
70		3.58	3.46
71		3.61	3.40
72		3.68	3.42

Continued page 54

Elevations Ft Blocks &
TOP RIBS

	H.I	FOR FT BLOCKS	B.M
	4.12	552.40	548.28
# 2	4.88	* 553.16	555.78
		+2.62	55.78
3		+2.63	55.79
4		+2.65	55.81
5		+2.76	55.92
6		+2.80	55.96
7		+2.72	55.88
8	450.52	+2.58	55.64
9		+2.61	55.77
10		+2.61	55.77
11		+2.66	55.72
12		+2.70	55.86
13		+2.62	55.78
14		+2.58	55.74
15		+2.58	55.74
16		+2.55	55.71
17		+2.60	55.76
18		+2.62	55.78

* H.I for TOP OF RIBS

11-13-46
RAIN-COOL

Nelson
Leah and
Griffin

51

LT	RT
549.07	549.00
3.33	3.40
549.03	549.09
3.35	3.31
549.09	
3.31	
549.18	
3.22	
549.28	549.24
3.12	3.16
549.23	
3.17	
549.0	
3.40	
548.95	
3.45	
548.91	
3.49	
549.12	
3.28	
549.03	
3.37	
549.02	
3.38	
548.96	
3.45	
548.97	
3.43	
548.89	548.92
3.51	3.48
548.93	
3.47	
548.86	
3.54	

		* 553.16		Elev TOP RIBS
		552.40		
19		+2.59	555.75	
	5.31	H.F for FT BLOCKS 553.59		548.28
451 top 20		* 553.16	+2.56	55.72
21		+2.55	55.71	
22	4.77	* 553.05	+2.62	55.67
				548.28
23		+2.63	55.68	
24		+2.56	55.61	
25		+2.58	55.63	
26		+2.67	55.72	
27		* 553.16	+2.64	55.80
28		↑	+2.65	55.81
29		↓	+2.70	55.86
30		* 553.16	+2.61	55.77
31		* 553.05	+2.78	55.83
451 top 32			+2.71	55.76
33		+2.69	55.74	
34		+2.67	55.72	
35		+2.70	55.75	

11-13-96

FT BLK
LT Σ

52

548.89
3.51

548.90

4.69

548.90

4.69

548.80

4.76

548.77

4.82

548.74

4.85

548.70

4.89

548.86 548.90

4.73

4.69

548.95

4.64

548.96

4.63

549.01

4.58

549.97

4.62

549.01

4.58

548.98

4.61

548.95

4.64

548.94

4.65

548.94

4.64

553.05

553.59

EIGV
TOP RIBS

36 * 553.05 +2.82 55.87

37 +2.84 55.89

38 +2.82 55.87

39 +2.85 55.90

40 +2.87 55.92

41 +2.85 55.90

42 +2.85 55.90

43 +2.90 55.95

44 +2.82 55.87

45 4.52 +0.00 +2.88 55.93

4.57 H.I FOR FT BLOCKS 552.85 548.28

46 * 553.05 +2.80 55.85

47 +2.76 55.81

48 see page 55 +2.82 55.87

49

50

51

52

53

LT 4

549.08

4.51

549.04

4.55

549.09

4.50

549.10

4.49

549.14

4.45

549.07

4.52

549.11

4.48

549.07

4.52

549.13

4.46

549.10

4.49

549.09

3.76

549.03

3.82

549.10

3.75

549.14

3.71

549.08

3.77

549.10

3.75

549.06

3.79

DISTANCE FROM SPRINGLINE
TO & CONTINUED FROM PAGE 50

73	3.65	3.42
74	3.51	3.37
75	3.43	3.46
76	3.48	3.56
77	3.64	3.60
78	3.58	3.54
79	3.62	3.46
80	3.78	3.58
81	3.70	3.66
82	3.67	3.64
83	3.73	3.67
84	84-TO 86 could not get HOPPER IN WAY.	
85		
86		
87	3.69	3.61
88	3.75	3.67
89	3.73	3.67
90	3.66	3.69

11-19-46
Clear-Warm

Nelson
Leonard
Bartagran

54

91	3.69	3.71
92	3.69	3.70
93	3.58	3.78
94	3.63	3.81
95	3.74	3.63
96	3.70	3.71

ELEV'S TOP OF RIBS

H I

	5.08	553.67		548.59
48			+2.18	555.85
49			+22.1	555.88
50			+2.18	555.85
51			+2.23	555.90
52			+2.19	555.86
53			+2.21	555.88
54			+2.14	555.81
55			+2.06	555.73
56			+2.06	555.73
57	553.67		+2.12	555.79 with transit
	555.48		+0.30	555.78 with level
58			+0.30	555.78
59			+0.41	555.89
60			+0.36	555.84
61			+0.40	555.88
62			+0.39	555.87
63			+0.33	555.81
64			+0.32	555.80
65			+0.33	555.81

11-19-46
CLEAR-WATER

NEISON
LEONARD 53
BARRAGAN

→ see page 53

READINGS FROM #57 TO #91
INCLUSIVE TAKEN WITH
TRANSIT SEE PAGE 20
FOR H.I OF 11-19-46

555.48

66	+ 0.40	555.88
67	+ 0.33	555.81
68	+ 0.32	555.80
69	+ 0.27	555.75
70	+ 0.30	555.78
71	+ 0.31	555.79
72	+ 0.31	555.79
73	+ 0.40	555.88
74	+ 0.45	555.93
75	+ 0.44	555.92
76	+ 0.59	556.02
77	+ 0.46	556.94
78	+ 0.65	556.13
79	+ 0.65	556.13
80	+ 0.53	556.01
81	+ 0.62	556.10
82	+ 0.57	556.05
83	555.48 + 0.55	556.03

56

calahan steel



calahan steel

PEAK steel



		555.48			
84		↑	+0.58	556.06	
85			+0.63	556.11	
86			+0.58	556.06	
87			+0.55	556.03	
88			+0.62	556.10	
89			+0.70	556.18	
90			+0.71	556.19	
91		↓	+0.72	556.20	
		555.48			
92			+2.61	556.18	
93		↑	+2.58	556.15	
94			+2.56	556.13	
95		↓	+2.66	556.23	
96			+2.65	556.22	
		553.57			
		553.63			
97		↑	+2.53	56.16	
98			+2.50	56.13	
99			+2.45	56.08	
100			+2.46	56.09	
101		↓	+2.41	56.04	
102			+2.45	56.09	
103	4.99		+2.51	56.14	548.64
104			+3.15	56.12	
105		↑	+3.19	56.16	
106		↓			
107		H.I	+3.15	56.12	
		552.97			
			→	see page 21	11-22-46

PEAK steel



see page 21

see page 21

PEAK steel



11-22-46
cloudy-cool

Nelson
LEIGHT
Phillips



Elevs TOP Ribs

H.I

	5.13	553.41		548.28
CK BM			4.82	548.59 = 548.59
# 37			+2.45	55.86
# 38			+2.45	55.86
# 39			+2.48	55.89
# 40			+2.50	55.91
# 41			+2.48	55.89
# 42			+2.46	55.87
# 43			+2.53	55.94
# 44			+2.44	55.85
# 45			+2.50	55.91
# 46			+2.42	55.83
# 47			+2.36	55.79
#	5.36	553.95		548.59
# 48			+1.88	55.83
49			+1.91	55.86
50			+1.88	55.83
51			+1.93	55.88

11-22-46
cloudy-cool

53.95

NELSON
LEONARD
PHILLIPS
BATT 8924

58

52			+1.90	55.85
53			+1.90	55.86
54			+1.89	55.79
55			+1.77	55.72
56			+1.77	55.72
57			+1.82	55.77
58			+1.81	55.76
59			+1.94	55.89
60			+1.89	55.89
61			+1.99	55.89
62			+1.92	55.87
63			+1.87	55.82
64			+1.86	55.81
65			+1.86	55.81
66			+1.99	55.89
67			+1.86	55.81
68			+	
69			+	
70				

5.42 553.70

548.28

#2	1.81	55.51
#1	+1.80	55.50
#-1	+1.99	
-2	+2.05	
-3	+2.07	
-4	+2.07	555.77
-5	+2.04	
-6	+2.07	
-7	+2.11	
-8	+2.16	
-9	+2.15	55.85
-10	+2.15	
-11	+2.14	
-12	+2.17	
-13	+2.19	55.89
-14	+2.30	56.00
-15	+2.38	
-16	+2.44	

11-22-46

59

PEAK steel

PEAK steel
Callahan steel

Distance from Q to
Spring Line RIB 37 to 65 inc

37	3.53	3.50
38	3.55	3.56
39	3.50	3.57
40	3.54	3.58
41	3.50	3.58
42	3.45	3.62
43	3.38	3.56
44	3.49	3.59
45	3.42	3.62
46	3.50	3.62
47	3.52	3.54
48	3.61	3.46
49	3.62	3.49
50	3.48	3.61
51	3.49	3.63
52	3.51	3.65
53	3.46	3.65
54	3.50	3.62

11-22-46
Cloudy-Cool

Nelson
Leonard
Phillips 60

55	3.53	3.61
56	3.59	3.54
57	3.63	3.50
58	3.68	3.46
59	3.59	3.46
60	3.55	3.49
61	3.53	3.56
62	3.50	3.58
63	3.45	3.61
64	3.43	3.60
65	3.36	3.66

EIGHS FT BLKS # & ROOF

	5.27	553.55	548.28
-16			
-15			
-14			
-13			
-12			
-11			
-10			
-9			
-8			
-7			
-6			
-5			
-4			
-3			
-2			
-1			
1	5.13	553.41	548.28

11-25-46
Clear CoolNelson
Leonard
Battaglin

61

	L R	
TOP	L	R
+2.60	4.27	4.38
+2.53	4.34	4.45
+2.45	4.42	4.53
+2.33	4.52	4.62
+2.31	4.46	4.66
+2.28	4.49	4.68
+2.29	4.48	4.59
+2.29	4.45	4.72
+2.30	4.43	4.66
+2.25	4.48	4.74
+2.21	4.53	4.78
+2.17	4.54	4.84
55.75 +2.20	4.51	4.83
+2.21	4.44	4.83
+2.18	4.48	4.83
+2.13	4.55	4.83
+2.07	55.48	4.37
	4.37	4.66

53.41

62

2			
3			
4			
5			
6	5.14	553.42	548.28
7			
8			
9			
10			
11			
12			
13			
14	4.74	552.99	548.28
15			
16			
17	4.82	553.10	548.28
18			
19			

		L	R
+2.09	55.50	4.48	4.66
+2.27	55.68	4.43	4.49
+2.36	55.77	4.33	4.42
+2.50	55.91	4.25	4.30
+2.51		4.15	4.26
+2.45		4.23	4.37
+2.30		4.45	4.44
+2.33		4.50	4.43
+2.34		4.57	4.46
+2.40		4.34	4.51
+2.44		4.41	4.38
+2.34		4.43	4.54
+2.71		4.05	4.20
+2.72		4.05	4.24
+2.68	55.67	4.18	4.21
+2.62		4.24	4.36
+2.66		4.32	4.25
+2.62		4.28	4.34

		553.10		
20	4.84	553.12	11-26-46	548.28
21	5.27	553.55		548.28
22				
23				
24				
25				
26				
27				
28				
29				
30	5.09	553.37		548.28
31				
32				
33				
34				
35				
36				
37				

cont page 68

	55.70			
	+2.60		4.25	4.35
	+2.56		4.28	4.41
	+2.09		4.78	4.83
	+2.09		4.84	4.77
	+2.02	55.57	4.86	4.93
	+2.02	55.57	4.93	4.97
	+2.14		4.73	4.72
	+2.21		4.72	4.63
	+2.23		4.74	4.66
	+2.27		4.69	4.61
	+2.16		4.70	4.74
	+2.40	55.71	4.49	4.39
	+2.34	55.71	4.49	4.46
	+2.34		4.48	4.47
	+2.32		4.49	4.52
	+2.34		4.45	4.49
	+2.47		4.39	4.39
	+2.48		4.42	4.31

	FT. BLOCKS		Center splice of steel	
	L	R	Lt of E	Rt of E
-16	3.50	3.32		0.02
-15	3.50	3.31		0.03
-14	3.49	3.28	0.01	
-13	3.47	3.30	0.05	
-12	3.48	3.30	0.0	0.0
-11	3.49	3.30		0.01
-10	3.50	3.30	0.01	
-9	3.48	3.31		0.02
-8	3.47	3.33		0.04
-7	3.45	3.36		0.02
-6	3.42	3.39		0.02
-5	3.40	3.42		0.03
-4	3.40	3.39		0.06
-3	3.39	3.45		0.09
-2	3.40	3.45		0.14
-1	3.39	3.46		0.11
1	3.39	3.50		0.06
2	3.40	3.35	0.01	

11-26-46
Clear-w 2177

Nelson
Leonard
BART 8927

69

3	3.37	3.41		0.03	
4	3.39	3.34		0.0	0.0
5	3.40	3.24		0.0	0.0
6	3.46	3.31		0.02	
7	3.43	3.22		0.05	
8	3.23	3.38		0.0	0.0
9	3.11	3.35		0.0	0.0
10	2.95	3.30		0.0	0.0
11	3.24	2.97			0.02
12	3.16	3.03		0.07	
13	3.24	3.00		0.02	
14	3.20	2.94		0.02	
15	3.19	3.03		0.06	0.06
16	3.13	2.99		0.02	
17	3.02	2.88			0.04
18	2.89	2.86		0.08	
19	2.97	2.77		0.05	
20	3.02	2.88			0.03

	£		£
21	3.12	2.87	0.02
22	3.10	3.02	0.09
23	2.98	3.02	0.13
24	2.96	2.88	0.01
25	2.99	2.95	0.10
26	3.08	3.00	0.13
27	3.00	3.08	0.12
28	2.87	3.03	0.05
29	2.79	2.98	0.05
30	3.10	2.98	0.02
31	3.15	2.96	0.15
32	3.24	2.94	0.15
33	3.26	2.94	0.15
34	3.30	2.91	0.16
35	3.37	2.88	0.17
36	3.21	3.01	0.14
37	3.05	3.09	0.04
38	3.10	3.15	0.02

	£		£
39	3.08	3.19	0.05
40	3.13	3.23	0.08
41	3.08	3.23	0.03
42	3.03	3.26	0.05
43	2.91	3.18	0.02
44	3.08	3.21	0.0 0.0
45	2.97	3.27	0.0 0.0
46	3.11	3.30	0.02
47	3.13	3.20	0.02
48	3.24	3.17	0.06
49	3.29	3.13	0.0 0.0
50	3.13	3.25	0.10
51	3.10	3.33	0.03
52	3.20	3.32	0.02
53	3.15	3.38	0.05
54	3.15	3.30	0.03
55	3.21	3.33	0.04
56	3.28	3.24	0.03

	L	R		L	R
57	3.32	3.23			0.09
58	3.37	3.20		0.06	
59	3.22	3.16		0.01	
60	3.12	3.19			0.04
61	3.10	3.20			0.04
62	3.02	3.12			0.10
63	2.90	3.23			0.03
64	2.91	3.22			0.04
65	2.89	3.21			0.21
66	2.79	3.02			0.12
67	2.80	2.98			0.13
68	2.80	2.96			0.12
69	3.07	2.97			0.04
70	3.10	3.02		0.04	
71	3.11	3.02		0.10	
72	3.23	3.00		0.06	
73	3.24	3.01		0.04	
74	3.02	2.92			0.06

	L	R				66
75	2.90	3.00				0.03
76	3.11	3.20			0.08	0.08
77	3.35	3.30			0.03	0.03
78	3.23	3.23			0.01	0.01
79	3.26	3.10				0.03
80	3.46	3.38			0.13	0.13
81	3.45	3.42			0.0	0.0
82	3.47	3.45				0.02
83	3.49	3.45				0.04
84	3.39	3.55				0.06
85	3.43	3.48			0.0	0.0
86	3.44	3.50				0.01
87	3.46	3.43			0.03	
88	3.47	3.42			0.03	
89	3.43	3.44				0.01
90	3.39	3.46			0.0	0.0
91	3.41	3.42			0.05	
92	3.40	3.49			0.05	

93	3.29	3.59		0.13
94	3.29	3.59		0.11
95	3.45	3.37	0.04	
96	3.38	3.48		0.05
97	3.38	3.52	0.0	0.0
98	3.42	3.41		0.01
99	3.49	3.37		0.01
100	3.52	3.34	0.04	
101	3.48	3.34	0.02	
102	3.38	3.45		0.09
103	3.35	3.45		0.08
104	3.37	3.44		0.01
105	3.32	3.55		0.08
106	3.27	3.60		0.20
107	3.24	3.61		0.19
108	3.37	3.47		0.02
109	3.43	3.45		0.03
110	3.45	3.40		0.05

111	3.36	3.47		0.10
112	3.40	3.42		0.03
113	3.40	3.43		0.05
114	3.39	3.44		0.05
115			12-11-46	0.03
116				0.0 0.0
117				0.01
118				0.04
119				0.05
120				0.04
121				0.10
122				0.11
123				0.03
124				0.0 0.0
125				0.06
126				0.05
127				0.11
128				0.12

CONT Page 74

CONT from page 63

11-25-46

Nelson
Leonard
Bartagan

68

38	5.09	553.37	548.28
39			
40			
41			
42			
43			
44			
45			
46			
47			
48			
49	5.22	53.50	548.28
50			
51			
52			
53			
54			
55			

+2.47		4.45	4.32
+2.50		4.41	4.35
+2.53		4.25	4.29
+2.50		4.27	4.31
+2.49		4.37	4.29
+2.56		4.40	4.26
+2.46		4.41	4.31
+2.51		4.43	4.34
+2.45		4.37	4.36
+2.37		4.45	4.43
35.80			
+2.43		4.44	4.41
12-3-46		same	party
+2.33	55.83		
+2.31	55.81		
+2.36	55.86		
+2.30	55.80		
+2.31	55.81		
+2.25	55.75		
+2.17	55.67		

12-3-46

53.50

56	+2.18	55.68
57	+2.23	55.73
58	+2.22	55.72
59	+2.35	55.85
60	+2.29	55.79
61	+2.38	55.88
62	+2.32	55.82
63	+2.27	55.77
64	+2.25	
65	+2.27	55.87
66	+2.35	55.85
67	+2.26	
68	+2.27	
69	+2.22	
70	+2.25	
71	+2.28	
72	+2.28	
73	+2.35	

12-3-46

69

74	+2.42	
75	+2.42	
76	+2.50	
77	+2.43	
78	+2.52	
79	+2.62	
80	+2.53	
81	+2.63	
82	+2.56	
83	+2.53	
84	+2.56	
85	+2.63	
86	+2.58	
87	+2.55	
88	+2.64	
89	+2.70	
90	+2.71	56.21
91	+2.73	

12-3-46

53.50

92		+2.72	
93		+2.67	
94	4.87	53.58	- 4.79 48.71 = 48.70
		+2.57	
95		+2.64	
96		+2.65	
97		+2.66	
98		+2.63	
99		+2.53	
100		+2.54	56.12
101		+2.50	
102		+2.53	56.11
103		+2.59	56.17
104		+2.57	56.15
105		+2.63	56.21
106		+2.66	56.24
107		+2.58	56.16
108		+2.65	56.23
109		+2.67	56.25

12-3-46

55

64

19

70

110		+2.57	56.15
111		+2.57	56.15
112	13.14 53.50	+2.57	56.15
113		+2.61	56.19
114	4.82	53.55	+2.69 56.24 48.72
115		+2.63	56.18
116		+2.62	56.17
117		+2.63	56.18
118		+2.60	56.10
119		+2.77	56.32
120		+2.80	56.35
121		+2.78	56.33

DISTANCE FROM
E TO SPRINGLINE

DISTANCE OF RIB
SPlice FROM E

#	L	E	R		L	E	R
1	3.76	3.70	=	44.4"			0.04
2	3.77	3.63	=	43.6			0.02
3	3.71	3.64	=	43.7			0.05
4	3.71	3.62	=	43.4			0.03
5	3.69	3.57	=	42.8			0.03
6	3.71	3.61	=	43.3			0.04
7	3.75	3.55	=	42.6			0.04
8	3.63	3.64	=	44.7			0.04
9	3.55	3.64	=	44.7			0.03
10	3.46	3.54	=	42.5			0.02
11	3.62	3.42	=	41.0	0.0	0.0	
12	3.59	3.42	=	41.0	0.10		
13	3.62	3.38	=	40.6	0.04		
14	3.59	3.32	=	39.8	0.03		
15	3.51	3.39	=	40.7			0.05
16	3.52	3.35	=	40.2	0.03		
17	3.41	3.32	=	39.8			0.02
18	3.41	3.27	=	39.2	0.10		

12-8-46
cloudy-cool

Nelson
Leonard
Bartogren

71

19	3.46	3.23	=	38.8"			0.07
20	3.45	3.35	=	40.2			0.02
21	3.52	3.30	=	39.6			0.05
22	3.52	3.39	=	40.7			0.10
23	3.48	3.30	=	39.6			0.14
24	3.39	3.26	=	39.1	0.0	0.0	
25	3.42	3.23	=	38.8			0.09
26	3.51	3.28	=	39.4			0.13
27	3.45	3.32	=	39.8			0.15
28	3.35	3.33	=	40.0			0.06
29	3.33	3.35	=	40.2			0.05
30	3.41	3.36	=	40.3	0.0	0.0	
31	3.57	3.35	=	40.2			0.15
32	3.61	3.35	=	40.2			0.13
33	3.62	3.33	=	40.0			0.12
34	3.65	3.32	=				0.13
35	3.70	3.31	=				0.15
36	3.57	3.40	=				0.11

37	3.45	3.48	0.01	
38	3.47	3.54	0.02	
39	3.44	3.57	0.06	
40	3.50	3.58	0.08	
41	3.48	3.59	0.0	0.0
42	3.44	3.63	0.05	
43	3.36	3.57	0.05	
44	3.47	3.58	0.03	
45	3.40	3.60	0.02	
46	3.47	3.61	0.06	
47	3.51	3.54	0.0	0.0
48	3.60	3.46	0.06	
49	3.61	3.48	0.0	0.0
50	3.46	3.63	0.12	
51	3.47	3.62	0.03	
52	3.50	3.64	0.04	
53	3.45	3.66	0.08	
54	3.48	3.62	0.05	

55	3.53	3.64		0.06
56	3.56	3.55		0.04
57	3.61	3.51		0.05
58	3.66	3.47		0.06
59	3.58	3.48		0.01
60	3.51	3.54		0.03
61	3.50	3.56		0.02
62	3.43	3.53		0.07
63	3.38	3.58		0.02
64	3.39	3.55		0.03
65	3.27	3.60		0.19
66	3.27	3.45		0.09
67	3.28	3.42		0.11
68	3.25	3.40		0.12
69	3.47	3.42		0.05
70	3.52	3.41		0.04
71	3.56	3.38		0.11
72	3.62	3.39		0.08

These readings from
 68 to 80
 were
 taken 12-17-46

73	3.58 3.58	3.34 3.39	0.05	
74	3.43 3.44	3.30 3.35		0.04
75	3.39 3.39	3.42 3.45		0.03
76	3.43 3.43	3.50 3.54		0.07
77	3.57 3.57	3.54 3.58	0.0	0.0
78	3.53 3.53	3.47 3.50	0.0	0.0
79	3.56 3.56	3.39 3.42	0.05	
80	3.77 3.76	3.57 3.59	0.14	
81	3.67	3.64	0.01	
82	3.65	3.65	0.03	
83	3.70	3.68		0.03
84	3.63	3.76		0.06
85	3.69	3.68	0.0	0.0
86	3.71	3.70	0.0	0.0
87	3.70	3.66	0.04	
88	3.71	3.67	0.03	
89	3.71	3.70	0.0	0.0
90	3.67	3.70	0.01	

91	3.66	3.71		0.04
92	3.62	3.71		0.05
93	3.55	3.80		0.11
94	3.60	3.81		0.09
95	3.72	3.60		0.07
96	3.66	3.68		0.05
97	3.66	3.68	0.0	0.0
98	3.66	3.63		0.01
99	3.73	3.66		0.01
100	3.78	3.59	0.04	
101	3.72	3.63	0.02	
102	3.66	3.73		0.09
103	3.63	3.72		0.08
104	3.68	3.71		0.01
105	3.60	3.78		0.08
106	3.54	3.84		0.20
107	3.51	3.82		0.19
108	3.65	3.70		0.02
109	3.69	3.67		0.03
110	3.66	3.65		0.05
111	3.62	3.70		0.10
112	3.65	3.65		0.03
113	3.66	3.65		0.05
114	3.64	3.67		0.05
115	3.67	3.65		0.03
116	3.71	3.60	0.0	0.0
117	3.72	3.59	0.01	
118	3.73	3.66	0.04	
119	3.67	3.63		0.05
120	3.66	3.63		0.04
121	3.60	3.76		0.10
122	3.56	3.80		0.11
123	3.66	3.73		0.03

	12-12-46			
124	3.65	3.72	0.0	0.0
125	3.64	3.73		0.06
126	3.65	3.69		0.05
127	3.56	3.81		0.11
128	3.59	3.80		0.12
129	3.59	3.82		0.09
130	3.62	3.79		0.10
131	3.62	3.75		0.06
132	3.56	3.84		0.05
133	3.67	3.69	0.0	0.0
134	3.73	3.61	0.05	
135	3.83	3.59	0.11	
136	3.80	3.57	0.10	
137	3.74	3.66	0.04	
138	3.72	3.58	0.06	
139	3.76	3.59	0.07	
140	3.71	3.60	0.07	
141	3.69	3.57	0.04	
142	3.70	3.54	0.08	
143	3.73	3.51	0.10	
144	3.76	3.55	0.08	
145	3.79	3.51	0.13	
146	3.75	3.55	0.05	

12-12-46

Nelson,
Leonard

74

147	3.83	3.48		0.16
148	3.90	3.40		0.22
149	3.90	3.36		0.22
150	3.83	3.46		0.18
151	3.81	3.55		0.14
	12-13-46			
152	3.77	3.54		0.04
153	3.70	3.59		0.09
154	3.73	3.56		0.02
155	3.74	3.63		0.01
156	3.83	3.50		0.16
157	3.77	3.60		0.10
158	3.77	3.52		0.11
159	3.81	3.52		0.16
160	3.81	3.53		0.14
161	3.72	3.60		0.05
162	3.67	3.64		0.03
163	3.75	3.59		0.05
164	3.67	3.63		0.09
165	3.71	3.60		0.0 0.0

CONT BOOK 708 Page 3

Elev's TOP of RIBS

	10.71	553.64		542.93
T.P.				
B.M	3.59	553.42	3.81	549.83 = 549.83
T.P				
B.M			5.14	548.28 = 548.28
#1			+2.04	55.46
2			+2.07	55.49
3			+2.26	55.68
4			+2.33	55.75
5			+2.48	55.90
6			+2.51	
7			+2.44	
8			+2.28	
9			+2.31	
10			+2.31	55.73
11			+2.39	55.81
12			+2.43	55.85
13			+2.33	55.75
14			+2.27	55.69
15			+2.27	55.69

12-8-46
cloudy-cool

Nelson
Leonard 75
Battaglia

BM POWER POLE

16	+2.22	55.66
17	+2.28	55.70
18	+2.32	55.74
19	+2.29	55.71
20	+2.26	55.68
21	+2.23	55.65
22	+2.19	55.61
23	+2.19	55.61
24	+2.12	55.54
25	+2.12	55.54
26	+2.23	55.65
27	+2.31	55.73
28	+2.33	55.75
29	+2.38	55.80
30	+2.27	55.69
31	+2.32	55.74
32	+2.46	55.88

53.42

33	+2.27	55.69
34	+2.24	55.66
35	+2.27	55.69
36	+2.39	55.81
37	+2.41	
38	+2.41	
39	+2.42	
40	+2.46	55.88
41	+2.42	
42	+2.42	
43	+2.48	
44	+2.39	
45	+2.45	
46	+2.38	
47	+2.30	55.72
48	+2.36	55.78
49	+2.41	55.83
50	+2.38	55.80

76

51	+2.45	55.87
52	+2.39	55.81
53	+2.38	55.80
54	+2.32	55.74
55	+2.25	55.67
56	+2.25	55.67
57	+2.31	55.73
58	+2.30	55.72
59	+2.43	55.85
60	+2.38	55.80
61	5.32	53.60
62	+2.23	55.83
63	+2.22	55.82
64	+2.18	55.78
65	+2.17	55.77
66	+2.19	55.79
67	+2.26	55.86
68	+2.17	55.77
69	+2.18	55.78

48.28

53.60

69.	+2.13	55.73
70	+2.16	55.77
71	+2.19	55.79
72	+2.20	55.80
73	+2.25	55.85
74	+2.34	55.94
75	+2.33	55.93
76	+2.42	55.02
77	+2.35	55.95
78	+2.43	56.03
79	+2.54	56.14
80	+2.45	56.05
81	+2.55	
82	+2.49	
83	+2.46	
84	+2.48	
85	+2.56	
86	+2.51	

77

87		+2.45	
88		+2.57	
89		+2.61	
90		+2.64	56.24
	5.12	553.95	48.83
91		+2.28	
92		+2.27	
93		+2.22	
94		+2.20	56.15
95		+2.27	
96		+2.28	56.23
97		+2.24	56.19
98		+2.21	56.16
99		+2.17	56.12
100		+2.18	56.13
101		+2.08	
102		+2.16	
103		+2.23	
104		+2.20	56.15
105		+2.27	56.22

12-13-46

Lietz dumpy level

	10.87	53.80		542.93
CK T.P.	3.51	53.34	3.97	49.83 = 49.83
CK B.M.	4.87	53.16	5.05	48.29 = 48.28
CK B.M.	4.86	53.88	4.14	49.02 = 48.98
CK B.M.	4.47	53.32	5.03	48.85 = 48.83
CK B.M.			4.92	48.90 = 48.36
# 106			+2.95	56.27
107			+2.88	56.20
108			+2.94	56.26
109			+2.96	56.28
110			+2.87	56.19
111			+2.83	56.15
112			+2.86	56.18
113			+2.90	56.22
114			+2.94	56.26
115			+2.86	56.18
116			+2.86	56.18
117			+2.84	56.20

53.32

78

118	+2.85	56.17
119	+3.02	56.34
120	+3.04	56.36
121	+3.04	56.36
122	+2.98	56.30
123	+2.95	56.27
124	+2.93	56.25
125	+2.89	56.21
126	+2.91	56.23
127	+3.00	56.32
128	+3.02	56.34
129	+3.01	56.33
130	+3.02	56.34
131	+2.96	56.28
132	+2.92	56.24
133	+2.90	56.22
134	+2.93	56.25
135	+2.87	56.19

53.32

136	+2.83	56.15
137	+2.91	56.23
138	+2.88	56.20
139	+2.93	56.25
140	+3.09	56.41
141	+2.92	56.24
142	+2.91	56.23
143	+2.95	56.27
144	+2.95	56.27
145	+2.89	56.21
146	+2.86	56.18
147	+2.90	56.22
148	+2.92	56.24
149	+3.00	56.32
150	+2.97	56.29
151	+2.92	56.24
152	+2.92	56.24
153	+2.87	56.19

53.32

79

154		+2.87	56.19	
	4.53	53.38		48.85
155		+2.82	56.20	
156		+2.83	56.21	
CK. BM		5.16	548.22 =	48.20
157		+2.81	56.19	
	4.47	53.32		48.85
158		+2.90	56.22	
159		+2.86	56.18	
160		+2.84	56.16	
161		+2.88	56.20	
162		+2.85	56.17	
163		+2.86	56.18	
164		+2.88	56.20	
165		+2.91	56.23	
166		+2.90	56.22	
167		+2.88	56.20	
168		+2.90	56.22	
169		+2.94	56.26	
170		+2.95	56.27	
171		+2.89	56.21	

80

53.32

172	+3.01	56.33
173	+2.98	56.30
174	+2.89	56.21
175	+2.94	56.26
176	+2.97	56.29

CONT BOOK 708 P-5

3-3-47	Nelson		
Clear water	Phillips		
	Bartagat		
4.59	54.04	49.45	
562	G.R.	Grade	
45+91	4.22	49.82	
LT	4.16		
RT	4.21		
	+2.53	56.57	
556	+2.64	56.68	

48.76
+ 4.94
53.70

53.71
~~48.28~~
5.43

49.45
4.59
54.04

26
32

52

78
83

54.04
49.82

4.22
51.04

49.82
6.75
57

72 + 80
 450 + 23
 408.95
 355.19
 6.42
 76
 49.83
 4.07

42.93
 10.97
 53.90
 9.05
 49.85
 53.47
 9.92
 49.07

53.47
 4.60
 49.87

457.02
 450.23
 6.79

2
 68
 1032
 136
 294
 21.76
 22

10.73
 3.83
 6.90
 4.93
 49.83

Please Return to
 City of San Diego Water Dept.
 Room 268 Civic Center
 Telephone Main 5161

49.82
 + 3.53
 53.35
 - 5.07
 48.28

864
 32
 1728
 2592
 27.648

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 Roadway 16 feet wide. Side Slopes 1 on 1 1/2
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \times 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.