



697

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway N feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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File 541

221+6955

199+90

168+68

Please Return to
City of San Diego Water Dept.
Room 268 Civic Center
Telephone Main 5161

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" p 78 - 8/28/47 m80

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2% grade from Elev. 563 1-9 ✓

Alignment on ditch around north side
Murray Lake + 0.2% grade from Elev. 563.00
P 11-18 ✓

Ties to Elev. ^{Creek bottoms} 541.00 from Asta's
221+69⁵⁵ & 168+68, Murray Lake. P-25 ✓

Location Ties to R/W Hubs from
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Drainage Tunnel Murray Lake to
S. Diego River Drainage Basin 32-40 ✓

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R/W line west side Lot 98
La MESA Colony - Owner - S. H. Grove 24 ✓

Alignment Road to Tr. Plant from Murray
Blvd via Kiowa Drive 24 ✓

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Ties to East Holes Lake Murray P 43 ✓

" " " " Immediate vicinity Dam
Keepers House P 44 ✓

Lake Murray

Preliminary Road location	A	line	Alignment	P 45-49	✓
"	"	"	"	P 50-59	✓
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Preliminary Road location	C	"	Alignment	P 61	✓
"	"	"	"D"	P 62	✓
"	"	"	E	P 63	✓
Profile levels	B	line		P 64-65	✓
"	"	"	"C"	P 66	✓
"	"	"	"D"	P 67-69	✓
"	"	"	E	P 70	✓

Lake Murray Pipeline Traverse 71-78 ✓

Alignment For Drainage Ditch on 12% grade

Around Lake Murray.

Pt. #	DIST.	Hor L	Mag. Bearing	Vert L	Ht.	Rd.
			N 38° 00' E			
10-11	315'	46° 34' 30" RT			4.72	4.72
			N 08° 00' W			
9-10	151'	24° 26' RT			4.64	4.64
			N 33° 00' W			
8-9	235'	34° 50' LT			4.83	4.83
			N 1° 00' W			
7-8	98'	44° 12' LT			4.72	4.72
			N 46° 30' E			
6-7	288'	10° 39' RT			4.72	4.72
			N 35° 30' E			
5-6	201'	32° 43' LT			4.64	4.64
			N 67° 30' E			
4-5	128'	13° 54' LT			4.83	4.83
			N 81° 05' E			
3-4	233'	27° 34' LT			4.72	4.72
			S 76° 15' E			
2-3	137'	10° 43' RT			4.64	4.64
			S 87° E			
1-2	139'	27° 50' RT			4.6	4.6
			N 71° E			
0-1	128'				4.6	4.6

1-29-46 - King - Klinger - Ward - Leonard

U.S.G.S. Datum F.S.J. 1/26/56

Elev.

566.9

566.3

566.0

565.5

565.5 - Correct 565.3
on Sta. 13+00

565.0

564.6

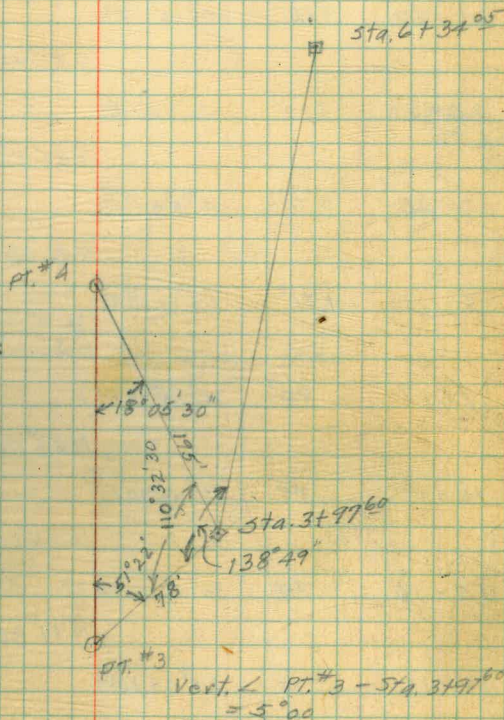
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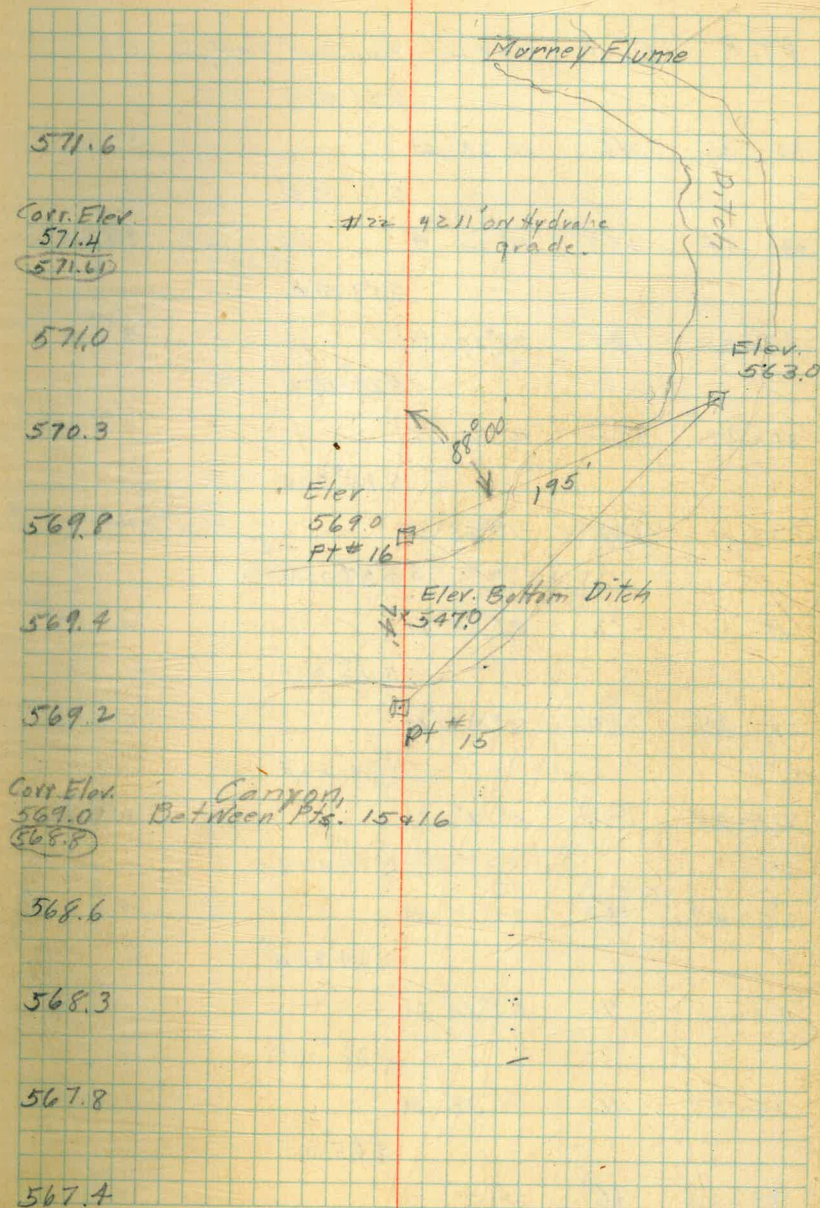
563.3

Elev. at 00 = 563.00



Hub & spoke

Pt #	Dist	Hor. L	Mag. Bear.	Vert. L	Ht	Pod
			N 87° 30' E			
22-23	73'	3° 22' 30" RT			4 ⁹⁰	4 ⁷⁰
			N 56° 00' E			
21-22	316'	5° 12' RT			4 ⁸³	4 ⁸³
			N 51° 45' E			
20-21	331'	5° 04' RT			4 ⁸³	4 ⁸³
			N 47° 30' E			
19-20	270'	4° 50' RT			4 ⁸³	4 ⁸³
			N 42° 00' E			
18-19	171'	39° 16' 30" RT			4 ⁸³	4 ⁸³
			N 2° 39' E. EE.			
			N 2° 30' W.			
17-18	80'	36° 25' 30" RT			4 ⁸⁶	4 ⁸⁶
			N 33° 00' W			
16-17	89'	76° 56' 30" LT			4 ⁷⁴	4 ⁷⁴
			N 44° 00' E			
15-16	74'	36° 19' LT			4 ⁸³	4 ⁸³
			N 81° 00' E			
14-15	138'	28° 03' 30" RT			4 ⁹	4 ⁹
			N 52° 00' E			
13-14	263'	10° 17' RT			4 ⁹	4 ⁹
			N 41° 00' E			
12-13	174'	16° 56' 30" RT			4 ⁹	4 ⁹
			N 24° 30' E			
11-12	252'	13° 52' LT			4 ⁹	4 ⁹
			N 38° 00' E			



Pt. #	Dist.	Hor. L	Mag. Bear.	Vert. L	H.I.	Red
			551°00'W			
34-35	146'	20°28' Lt			5°	5°
			571°36'W			
33-34	152'	15°20' Rt			483	483
			557°00'W			
32-33	135'	29°20'30" Rt			483	483
			528°00'W			
31-32	126'	16°46' Lt			487	487
			544°00'W			
30-31	137'	77°36' Lt			474	474
			N57°00'W			
29-30	82'	82°38' Lt			42	42
			N25°00'E			
28-29	213'	10°19'30" Lt			474	474
			N34°30'E			
27-28	145'	5°17' Rt			466	466
			N30°00'E			
26-27	94'	54°20' Rt			42	42
			N24°30'W			
25-26	71'	51°24' Lt			425	425
			N26°30'E			
24-25	46'	89°33' Lt			456	456
			565°00'E			
23-24	76'	28°57' Rt			464	464
			N87°30'E			

574.1

574.2

573.9

573.7

573.4

573.1

573.0

572.5

572.2

572.0

571.9

571.8

Correct Elev
573.80

Pt. # 30 El 573.4

N 57° 00' W

Elev. 567.0

Creek Bottom

Pt. # 29 El 573.1

SEE BK 639 P 21 & 22
error of 1 FT

Pt. # 25

N 26° 30' E

Elev. 565.8

Creek Bottom

Pt. # 24

Pt. #	Dist	Hor. \angle	Mag. Bear	Vert. \angle	Ht. Rod
			N 4° 30' W		
46-47	250'	69° 09' RT			4 ²⁹ 4 ²⁹
			N 69° 30' W		
45-46	224'	76° 29' LT			4 ⁵³ 4 ⁵⁷
			N 6° 00' E		
44-45	81'	55° 48' RT			4 ²⁹ 4 ²⁹
			N 50° 00' W		
43-44	296'	40° 00' 30" RT			4 ⁸³ 4 ⁸³
			S 89° 30' W		
42-43	178'	9° 02' LT			4 ⁹¹ 4 ⁹¹
			N 82° 30' W		
41-42	106'	11° 32' RT			4 ⁸³ 4 ⁸³
			S 86° 30' W		
40-41	158'	14° 37' 30" RT			4 ²⁹ 4 ²⁹
			S 72° 00' W		
39-40	163'	15° 32' RT			4 ⁷⁵ 4 ⁷⁵
			S 57° 30' W		
38-39	114'	3° 48' LT			4 ⁸⁰ 4 ⁸⁰
			S 63° 30' W		
37-38	306'	6° 35' RT			4 ⁸³ 4 ⁸³
			S 56° 30' W		
36-37	139'	3° 01' LT			5 ⁸⁷ 5 ⁸⁷
			S 59° 30' W		
35-36	182'	7° 41' RT			4 ⁹¹ 4 ⁹¹
			S 51° 00' W		

578.9

578.3

577.9

577.1

576.86 Sta. 60400

576.5

576.3

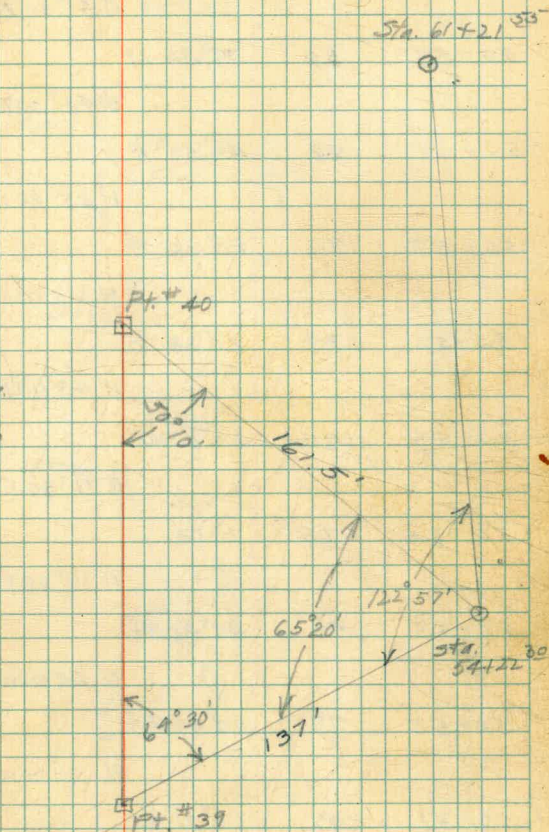
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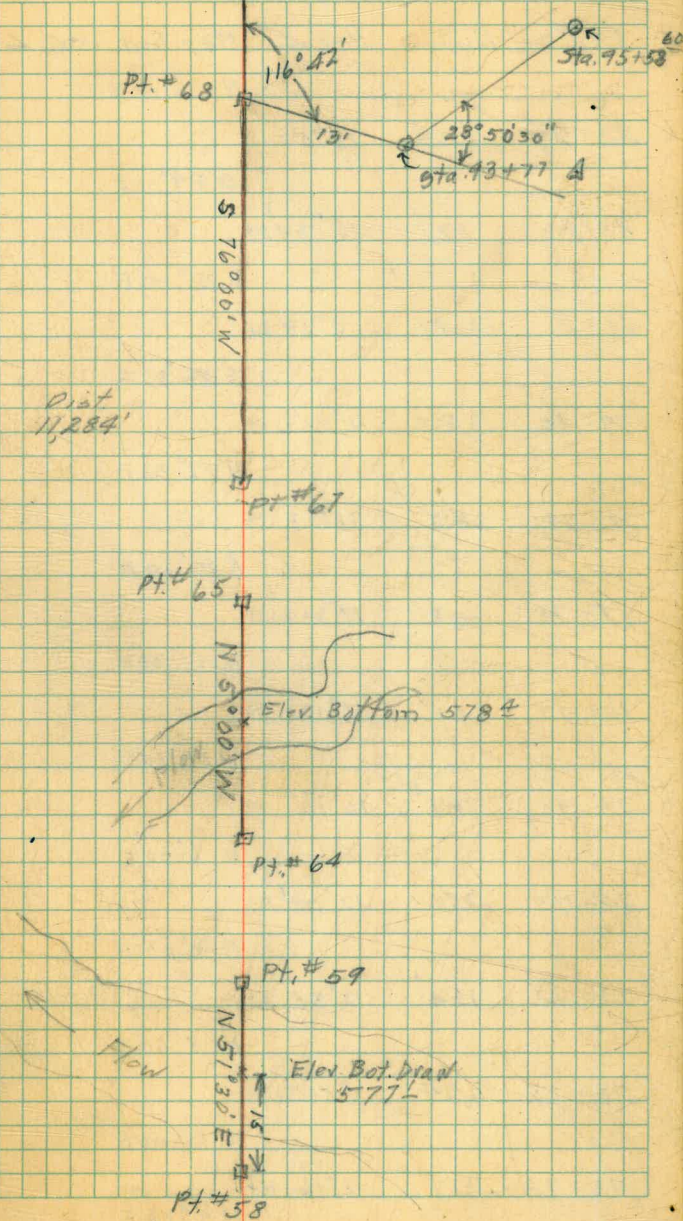
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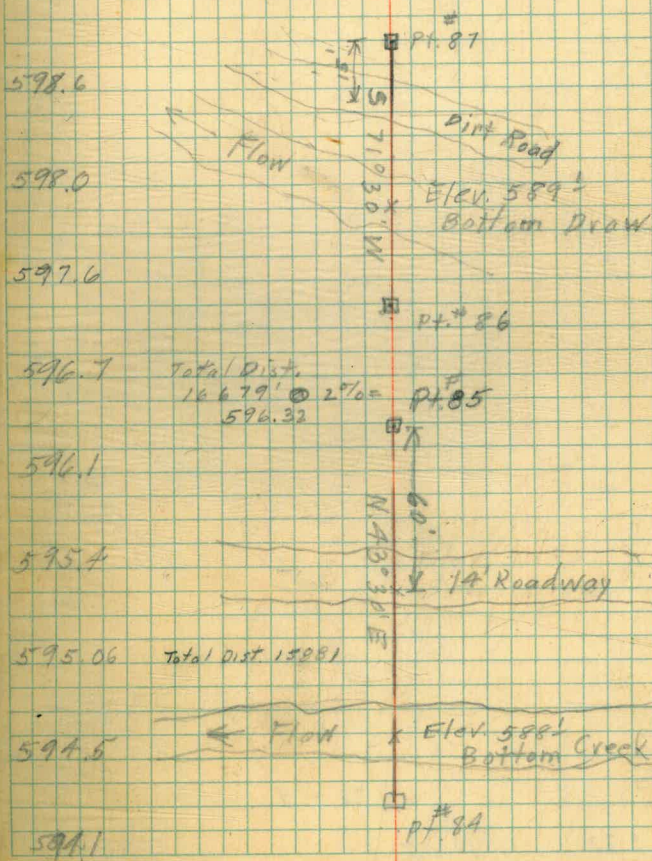
Pt.#	Dist	Hor. \angle	Mag. Bear.	Vert. \angle	HI	Red	
			N 4° 00' E				
70-71	195	3° 44' Lt.			4 ⁹¹	4 ⁹¹	587.4
			N 8° 00' E				
69-70	478'	22° 44' Rt.			4 ⁹¹	4 ⁹¹	587.0
			N 16° 00' W				
68-69	171'	87° 57' 30" Rt.			4 ⁹⁰	4 ⁹⁰	586.0
			S 76° 00' W				
67-68	197'	7° 55' 30" Rt.			4 ⁸³	4 ⁸³	585.69
			S 66° 30' W				
66-67	297'	17° 14' (Rt.)	LT. EE		4 ⁹¹	4 ⁹¹	585.3
			S 84° 30' W				
65-66	67'	89° 46' Lt.			5 ⁰	5 ⁰	584.7
			N 5° 00' W				
64-65	88'	76° 29' Lt.			5 ¹⁰	5 ¹⁰	584.5
			N 71° 00' E				
63-64	67'	28° 13' Rt.			4 ⁹¹	4 ⁹¹	584.4
			N 42° 00' E				
62-63	91'	7° 13' Rt.			4 ⁸⁰	4 ⁸⁰	584.2
			N 34° 30' E				
61-62	238'	29° 21' 30" Rt.			4 ⁷⁵	4 ⁷⁵	584.1
			N 08° 00' E				
60-61	185'	16° 24' Rt.			4 ⁸³	4 ⁸³	583.66
			N 9° 00' W				
59-60	77'	60° 50' Lt.			4 ⁷⁵	4 ⁷⁵	583.3
			N 51° 30' E				



Pt. #	Dist.	Hor. \angle	Mag. Bear	Vert. \angle	HI	Red	
			N 75° 00' E				
82-83	633'	15° 57' L	S 89° 00' E		483	482	593.8
81-82	171'	18° 34' R	N 72° 00' E		475	475	592.5
80-81	287'	22° 29' L	S 85° 30' E		475	475	592.1
79-80	384'	16° 26' 30" R	N 77° 30' E		483	483	591.5
78-79	282'	18° 17' R	N 59° 30' E		475	475	590.7
77-78	108'	17° 33' 30" R	N 42° 30' E		475	475	590.2
76-77	64'	18° 12' R	N 23° 30' E		509	509	589.9
75-76	161'	16° 12' R	N 7° 30' E		475	475	589.8
74-75	385'	12° 08' R	N 4° 00' W		491	491	589.5
73-74	124'	12° 55' L	N 8° 30' E		497	497	588.7
72-73	194'	2° 56' 30" R	N 6° 00' E		475	475	588.5
71-72	317'	2° 16' R	N 4° 00' E		475	475	588.1

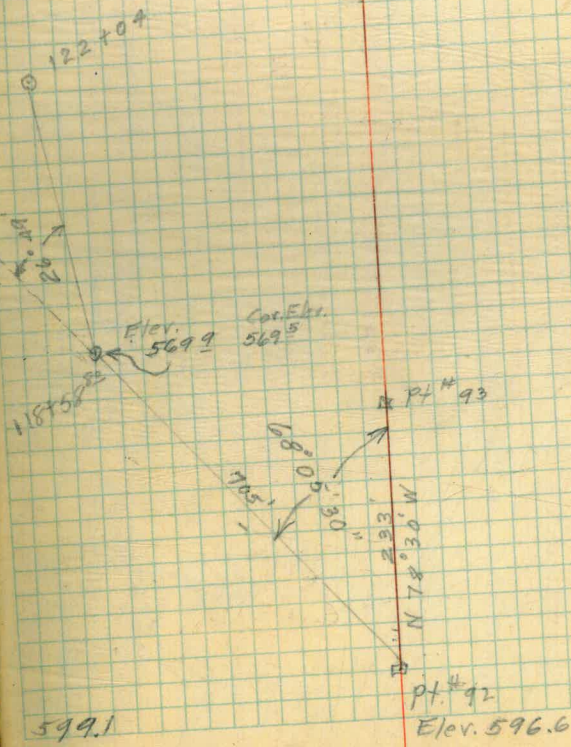
Pt. # Dist. Hor. \angle Mag. Bear. Vert. \angle #1. Red

Pt. #	Dist.	Hor. \angle	Mag. Bear.	Vert. \angle	#1. Red
			N 66° 30' W		
91-92	304'	16° 38' RT			485 4 ²⁵
			N 82° 30' W		
90-91	192'	13° 27' LT			4 ⁵⁰ 4 ⁵⁰
			N 67° 30' W		
89-90	419'	21° 34' 30" RT			487 4 ⁵¹
			S 86° 30' W		
88-89	310'	12° 16' LT			487 4 ⁵¹
			N 80° 30' W		
87-88	333	27° 33' RT			500 500
			S 71° 30' W		
86-87	155'	48° 48' LT			491 4 ⁹¹
			N 59° 30' W		
85-86	264'	102° 07' LT			500 500
			N 43° 30' E		
84-85	206'	44° 43' LT			504 5 ⁰⁰
			N 87° 00' E		
83-84	173'	11° 59' 30" RT			475 4 ⁷⁵
			N 75° 00' E		



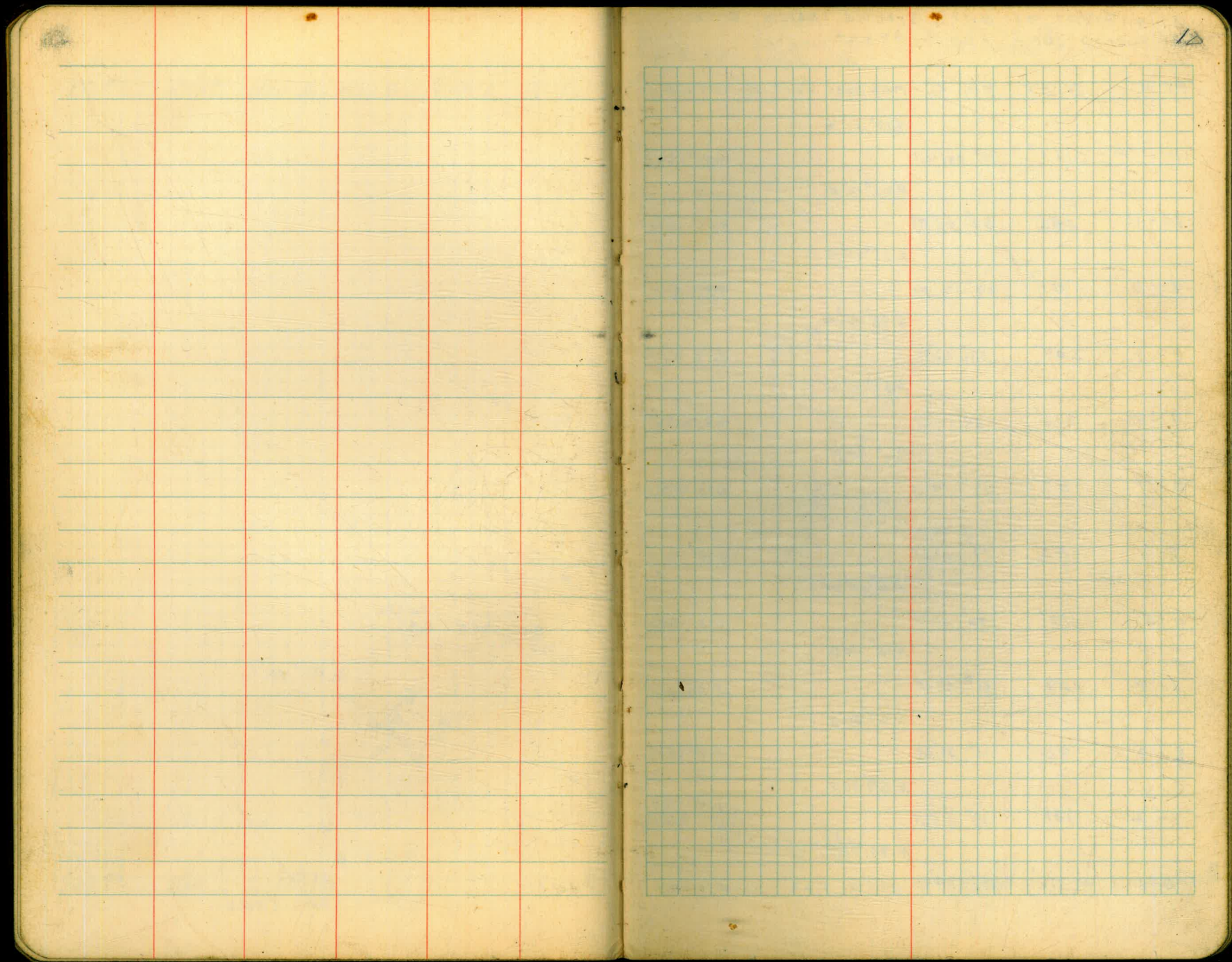
Pt. #	Dist	Hor. \angle	Mag. Bear	Vert. \angle	HI	Red
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92-93	233'	$12^{\circ} 19' 30''$	$N 78^{\circ} 30' W$			
			$N 66^{\circ} 30' W$	5°	5°	



599.1

Pt. # 92
Elev. 596.6



Alignment of ditch around north side
of Murray 18KE + 0.2% Grade

PT #	DIST	HOR <	MAG Bear	VERT <	HI	Rod
			N12° 30' E			
11-12	117'	17° 04' LT			4.75	4.75
			N29° 00' E			
10-11	145'	53° 00' RT			4.60	4.60
			N25° 00' W			
9-10	41'	68° 12' RT			4.83	4.83
			S85° 30' W			
8-9	207'	32° 43' 30" LT			4.83	4.83
			N60° 00' W			
7-8	211'	24° 00' LT			4.95	4.95
			N36° 30' W			
6-7	107'	12° 14' LT			4.90	4.90
			N29° 00' W			
5-6	293'	17° 02' LT			4.72	4.72
			N6° 30' W			
4-5	117'	22° 42' LT			4.83	4.83
			N16° 00' E			
3-4	109'	31° 43' LT			5.00	5.00
			N47° 30' E			
2-3	80'	11° 31' LT			4.64	4.64
			N59° 30' E			
1-2	171'	18° 51' LT			4.64	4.64
			N78° 00' E			
0-1	71'	137° 24' RT			4.10	4.10

Cool
showers A.M.
cloudy P.M.

Nelson Notes
K1179 T
Leonard φ

2-4-46

Elev.

566.4

566.1

565.85

565.4

564.9

564.7

564.1

563.9

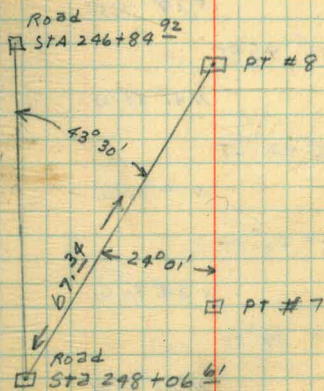
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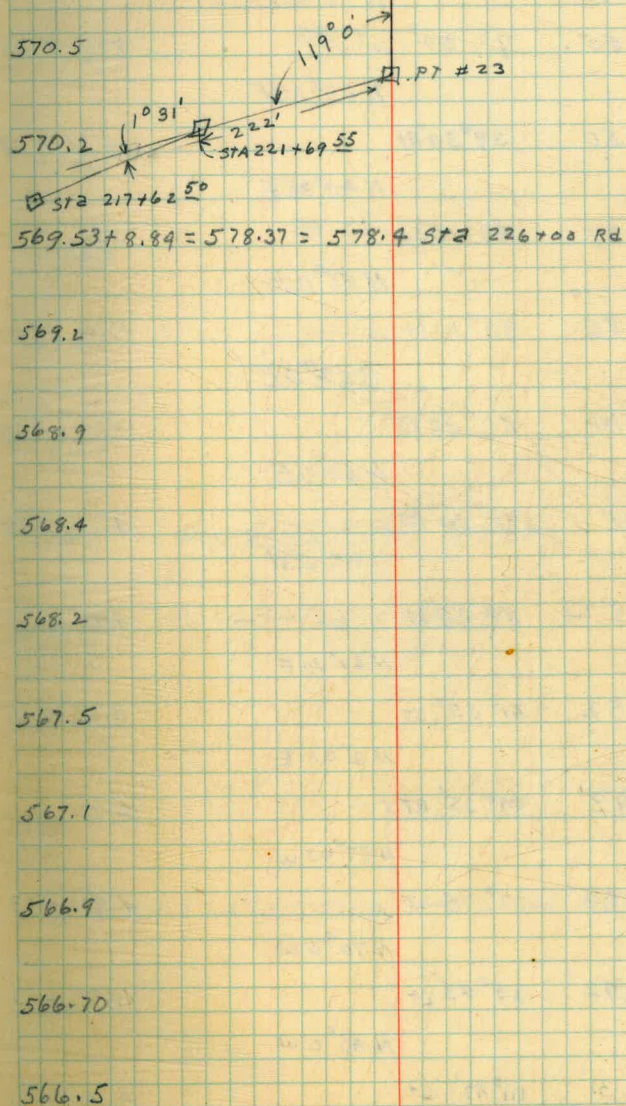
Elev 0+00 = 563.00

0+00 on axis of dam Sta 258+37 ⁸⁷



PT #	DIST	HOR <	MAG BEAR	VERT <	H I	ROD
			N 67° 00' E			
23-24	173'	69° 13' RT			4.91	4.91
			N 2° 30' W			
22-23	315'	35° 36' RT			4.86	4.86
			N 37° 30' W			
21-22	187'	8° 05' LT			4.83	4.83
			N 29° 30' W			
20-21	114'	11° 45' RT			5.00	5.00
			N 41° 30' W			
19-20	244'	22° 02' LT			4.91	4.91
			N 19° 00' W			
18-19	98'	5° 46' RT			4.83	4.83
			N 24° 30' W			
17-18	388'	2° 38' RT			5.00	5.00
			N 27° 30' W			
16-17	189'	40° 31' LT			5.00	5.00
			N 13° 00' E			
15-16	81'	8° 54' RT			4.75	4.75
			N 5° 00' E			
14-15	108'	34° 51' RT			4.85	4.85
			N 31° 00' W			
13-14	79'	25° 55' LT			4.64	4.64
			N 5° 00' W			
12-13	87'	16° 07' 30" LT			4.83	4.83

ELEV



POINT #	distance	HOR \angle	MAG BEAR VERT \angle	#1 Rod
			N 76° 45' E	
35-36	385.	7° 02'	LT. EE	4.90 4.90
			N 83° 30' E	
34-35	150	39° 30' RT		4.95 4.95
			N 43° 30' E	
33-34	107	43° 08'	LT. EE	5.16 5.16
			N 86° 0' E	
32-33	256	30° 10' LT.		5.03 5.03
			S 62° 0' E	
31-32	214	62° 32' RT		5.47 5.29
			N 54° 0' E	
30-31	78	78° 04' RT		5.10 5.10
			N 74° 0' W	
29-30	182	88° 47' LT.		4.95 4.95
			N 64° 30' E	
28-29	152	61° 55' RT		4.65 4.65
			N 2° 00' E	
27-28	83'	89° 25' RT		4.92 4.92
			N 87° 00' W	
26-27	240'	17° 04' LT		4.83 4.83
			N 70° 0' W	
25-26	292'	25° 43' LT		4.95 4.95
			N 45° 0' W	
24-25	231'	111° 42' LT		4.91 4.91

2-7-46
CLEAR-WARM

NELSON T
RICE NOTES 13
LEONARD ϕ

Elev.

575.3

574.5

574.2

574.0

573.5

573.1

Dry Creek \rightarrow 30+36

572.9

r/7/46 start

572.5

572.2

Dry Creek \rightarrow 27+65

572.0 - 0.9 = 571.1 = 571.0 Sta 217+00 Rd

571.55

571.0

Point #	Dist.	Hor. L	Magn. Bear.	Vert. L	H.I.	Rod
	see page # 16					
47-48	115	21° 40' LT	N 19° 30' W		4.88	4.88
			N 9° 0' E			
46-47	253	26° 39' LT			4.92	4.92
			N 35° 0' E			
45-46	230	16° 44' LT			5.07	5.07
			N 51° 30' E			
44-45	376	56° 23' LT			5.10	5.10
			S 71° 30' E			
43-44	490	25° 50' LT			5.05	5.05
			S 46° 0' E			
42-43	390	5° 11' LT			4.98	4.98
			S 41° 0' E			
41-42	266	3° 14' RT			5.00	5.00
			S 46° 0' E			
40-41	382	53° 04' RT			4.98	4.98
			N 82° 30' E			
39-40	125	72° 19' 30" RT			4.88	4.88
			N 10° 30' E			
38-39	320	4° 24' LT			4.97	4.97
			N 15° 0' E			
37-38	233	23° 50' LT			4.90	4.90
			N 38° 30' E			
36-37	295	37° 29' LT			5.06	5.06

2-8-46

Clear Warn7

Nelson X
RICE NOTES
Leonard Φ

14

Elev.

581.25 corrected
@ 1'er

2/8/46 start

581.8 9962' total dist. 18.924 Total rise
563.00 + 18.924 = 581.924 Elev.
581.92 + 3.20 = 585.12 = 584.2 Elev of
Sta 156+00 Road

581.3

580.8

580.0 - 12.12 = 567.88 =
567.2 Elev of 168+68.60

579.3

578.5

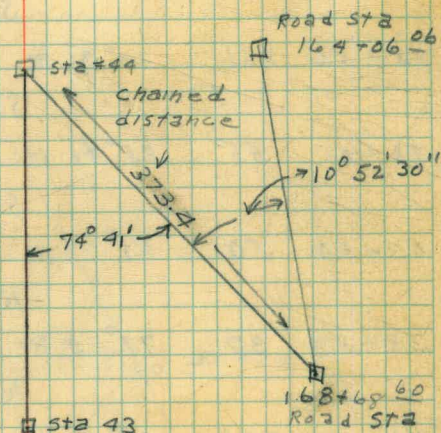
578.0

577.2

577.0

576.4

575.9



Point #	Dist.	Hor. \angle	Mag. Bear.	Vert. \angle	H.I.	Rod	Elev.
59-60							
58-59							
57-58							
56-57	84'	$9^{\circ}08'30''$ Lt	S $39^{\circ}0'$ E		4.89	4.89	583.7
55-56	261	$23^{\circ}31'$ Rt	S $31^{\circ}30'$ E		5.02	5.02	583.5
54-55	55	$25^{\circ}41'$ Lt	S $55^{\circ}0'$ E		4.88	4.88	583.0
53-54	50	$81^{\circ}29'$ Rt	S $28^{\circ}0'$ E		5.13	5.13	582.9
52-53	37	$78^{\circ}23'$ Rt	N $69^{\circ}0'$ E		5.05	5.05	582.8
51-52	206	$10^{\circ}7'$ Lt	N $9^{\circ}0'$ W		4.90	4.90	584.7
50-51	249	$27^{\circ}50'$ Lt	N $1^{\circ}0'$ E		5.08	5.08	584.0
49-50	94	$65^{\circ}05'$ Rt	N $31^{\circ}30'$ E		4.92	4.92	581.8
48-49	68	$22^{\circ}37'$ Lt	N $36^{\circ}0'$ W		4.92	4.92	581.6

see page 16

dry creek \Rightarrow 52+20

POINT # DIST. HOR. L MAG. BEAR. VERT. L H.I. ROD

12.99 566.69 = ^{B.M.} 566.23
 0.19 579.63 13.10 579.44
 72-73 0.46 592.54 592.08

Levels To Check B.M.

76-77 154' 11° 43' Lt
 75-76 185' 17° 0' Lt
 74-75 205' 7° 57' Lt
 73-74 174' 13° 20' 30" Lt
 72-73 150' 52° 12' Rt
 71-72 101' 16° 10' Lt

ST50°E
 98°19' Rt
 N7°0'E
 N18°0'E
 N35°0'E
 N43°0'E
 N56°0'E
 N5°0'E

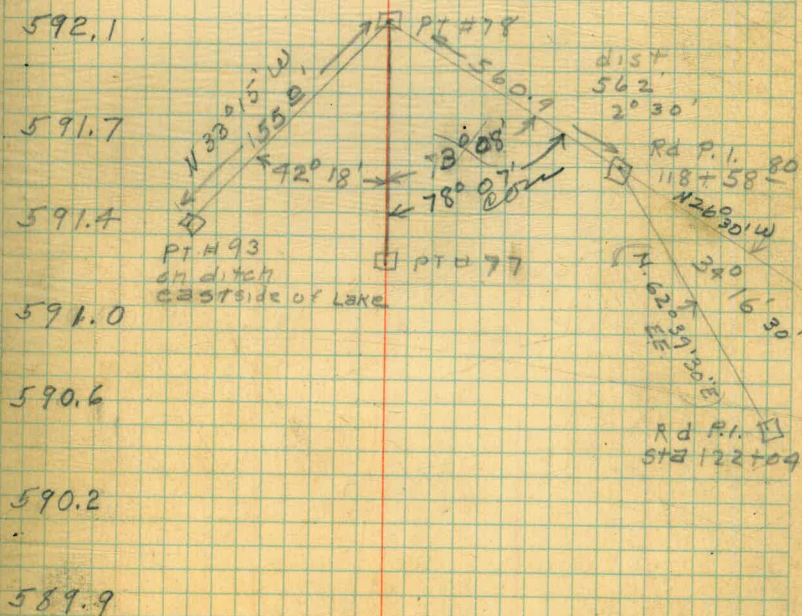
4.93 4.93
 5.03 5.03
 5.00 5.00
 4.77 4.77
 5.00 5.00
 4.97 4.97
 5.08 5.08

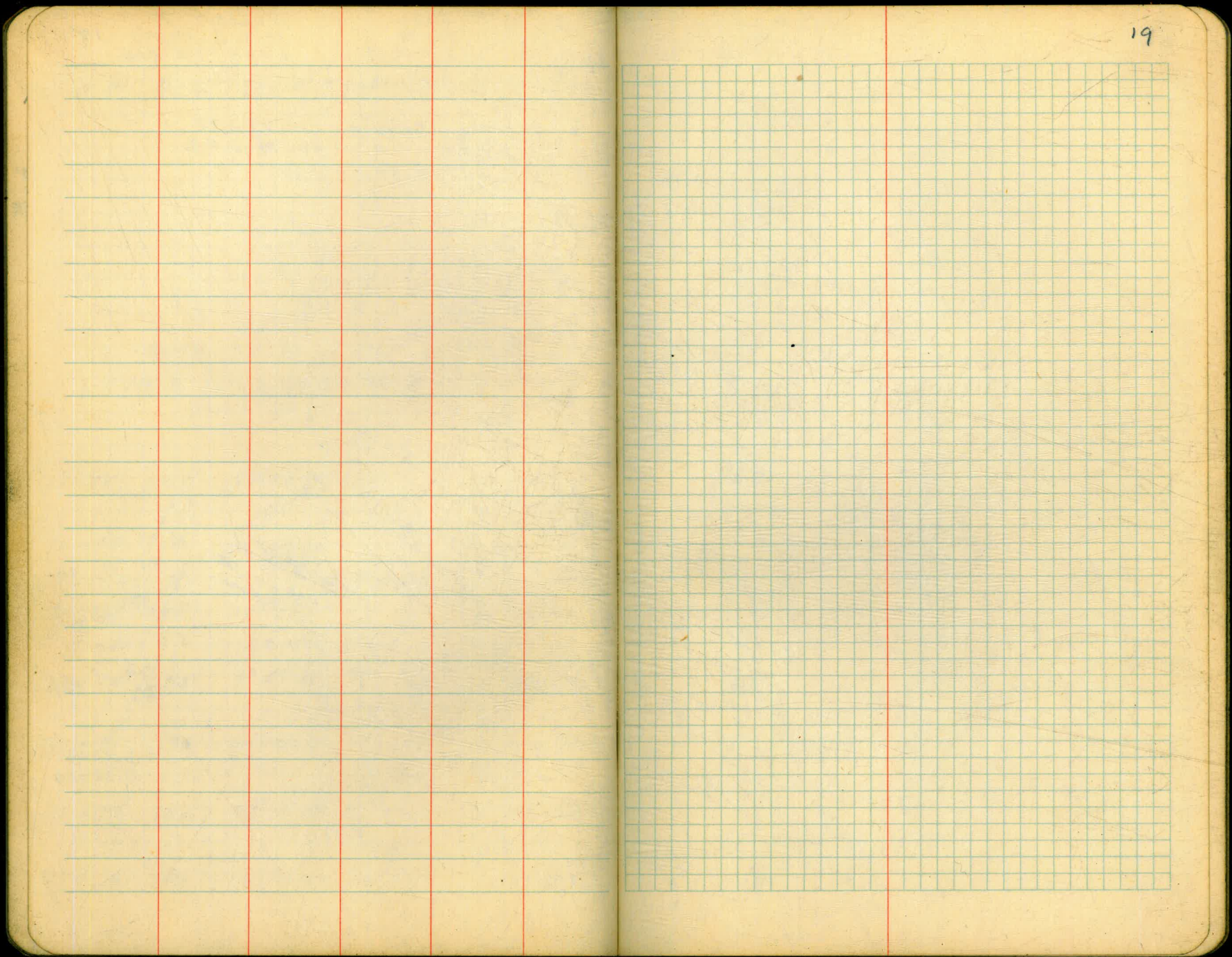
2-11-46 COOL
 Cloudy
 RAIN A.M.

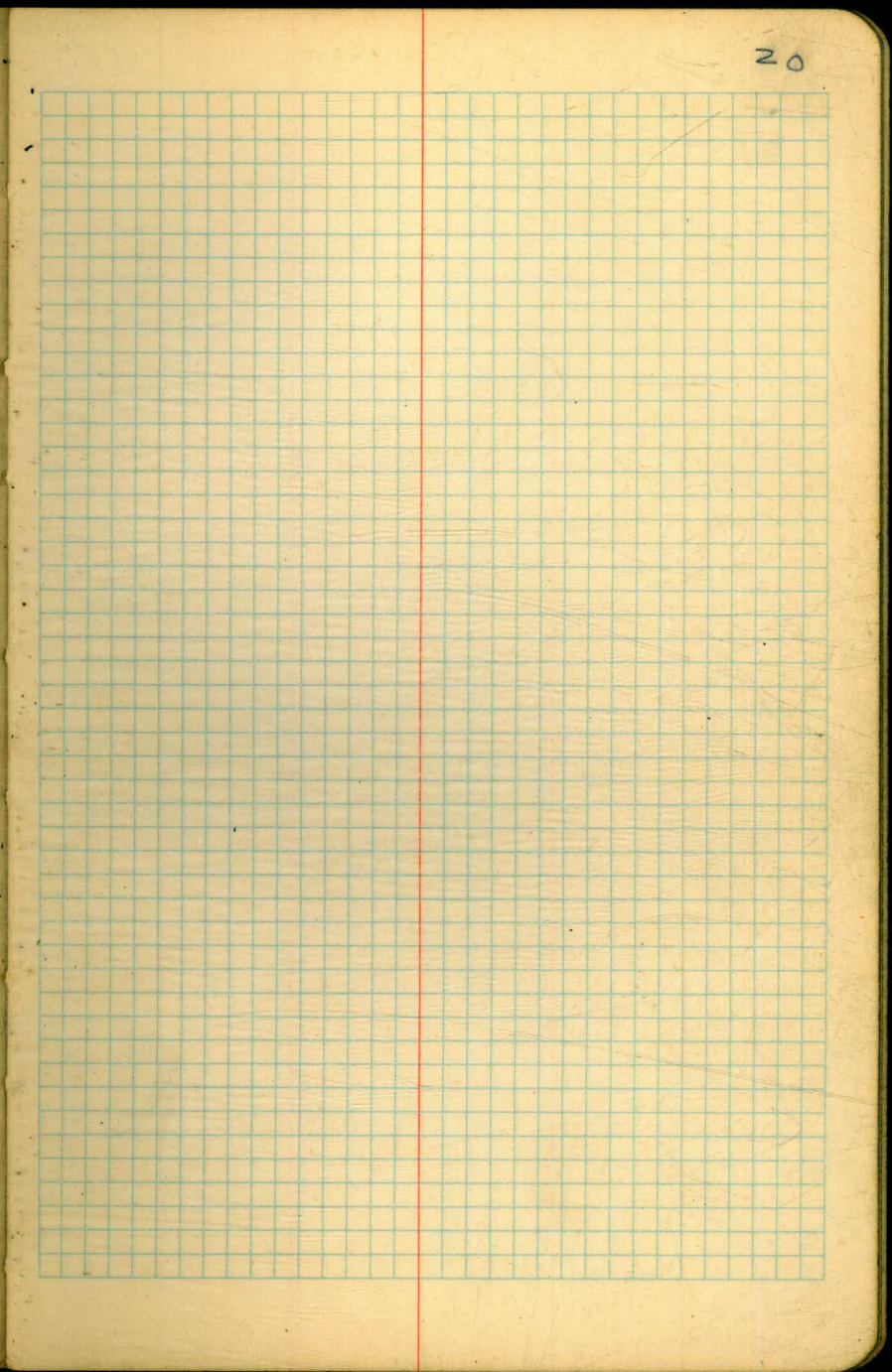
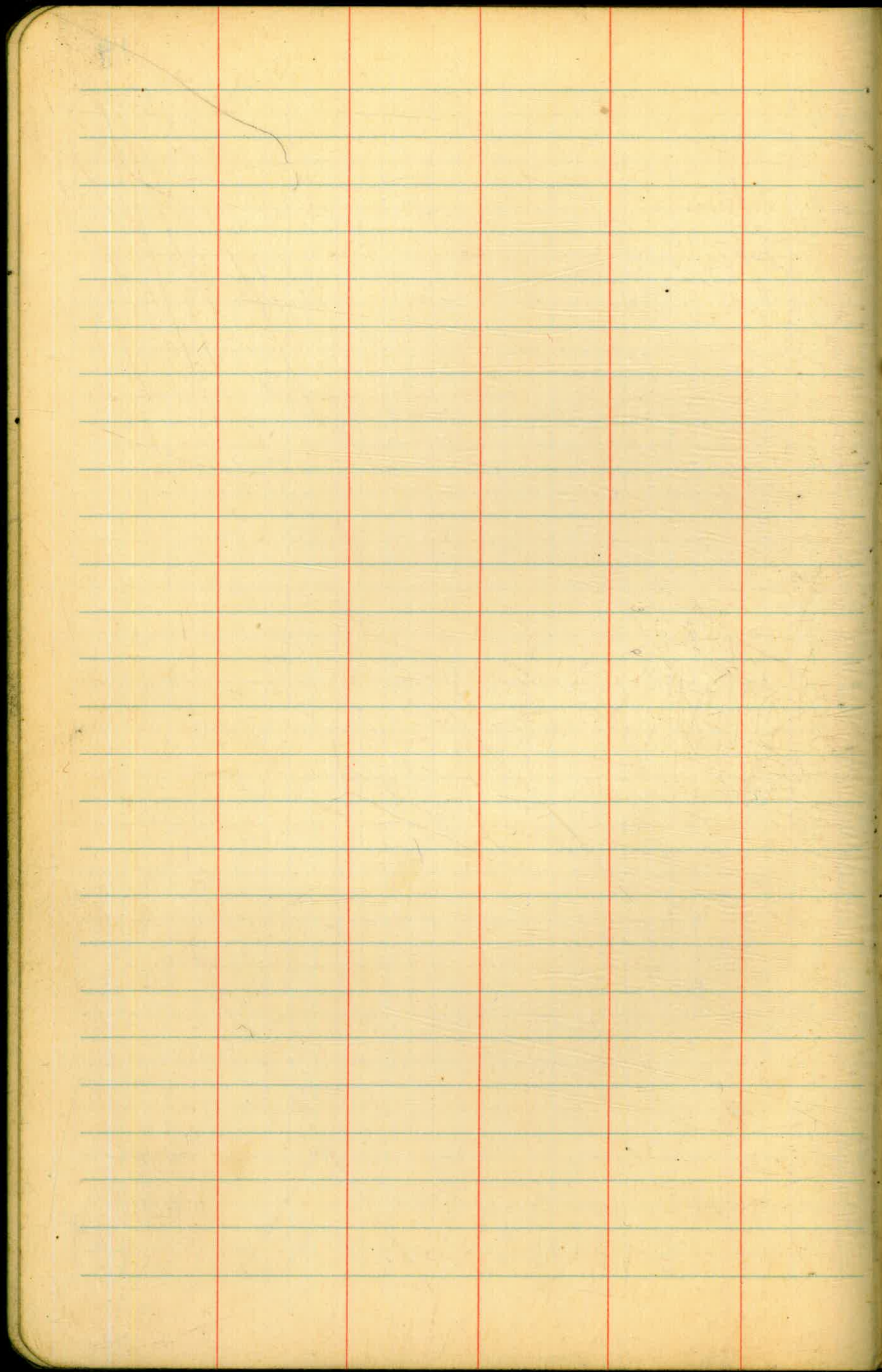
Nelson T
 Rice Notes 18
 Leonard Rod

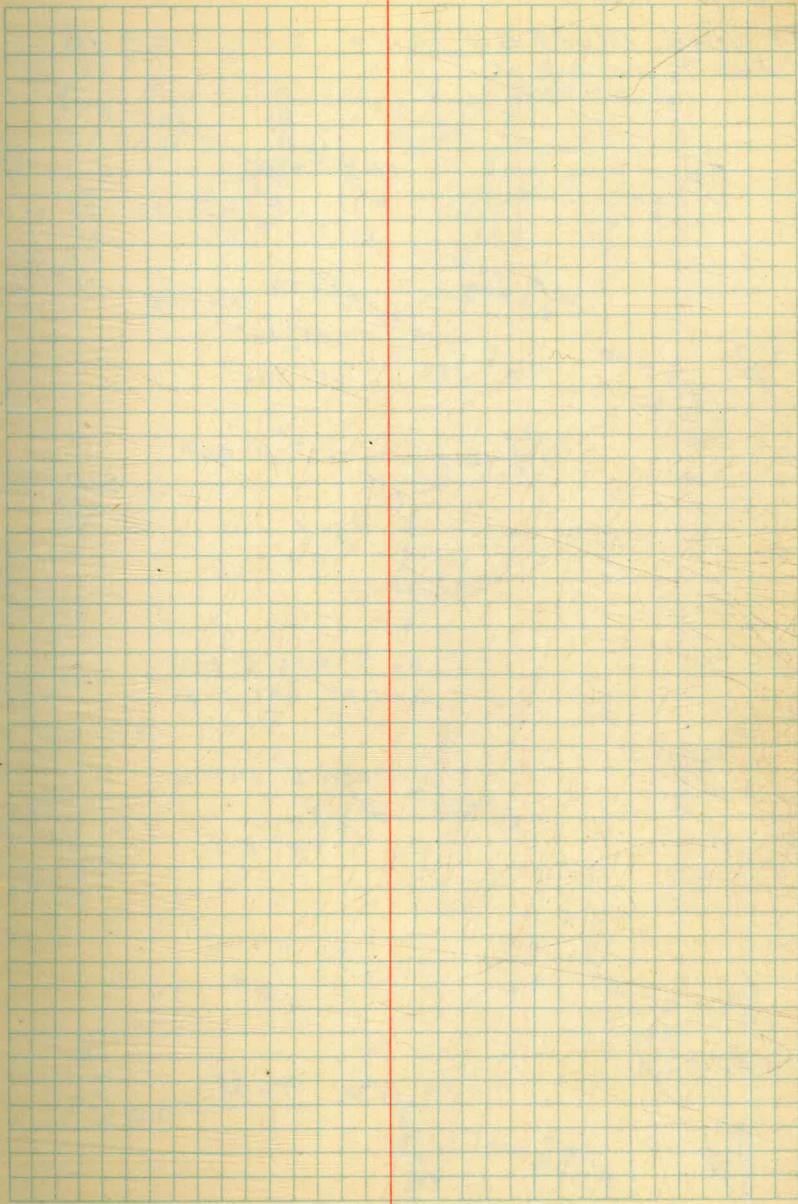
Elev.

4.85 Reading on PT #78
 3.98 " " on PT #93
 5.87 diff. in elev.

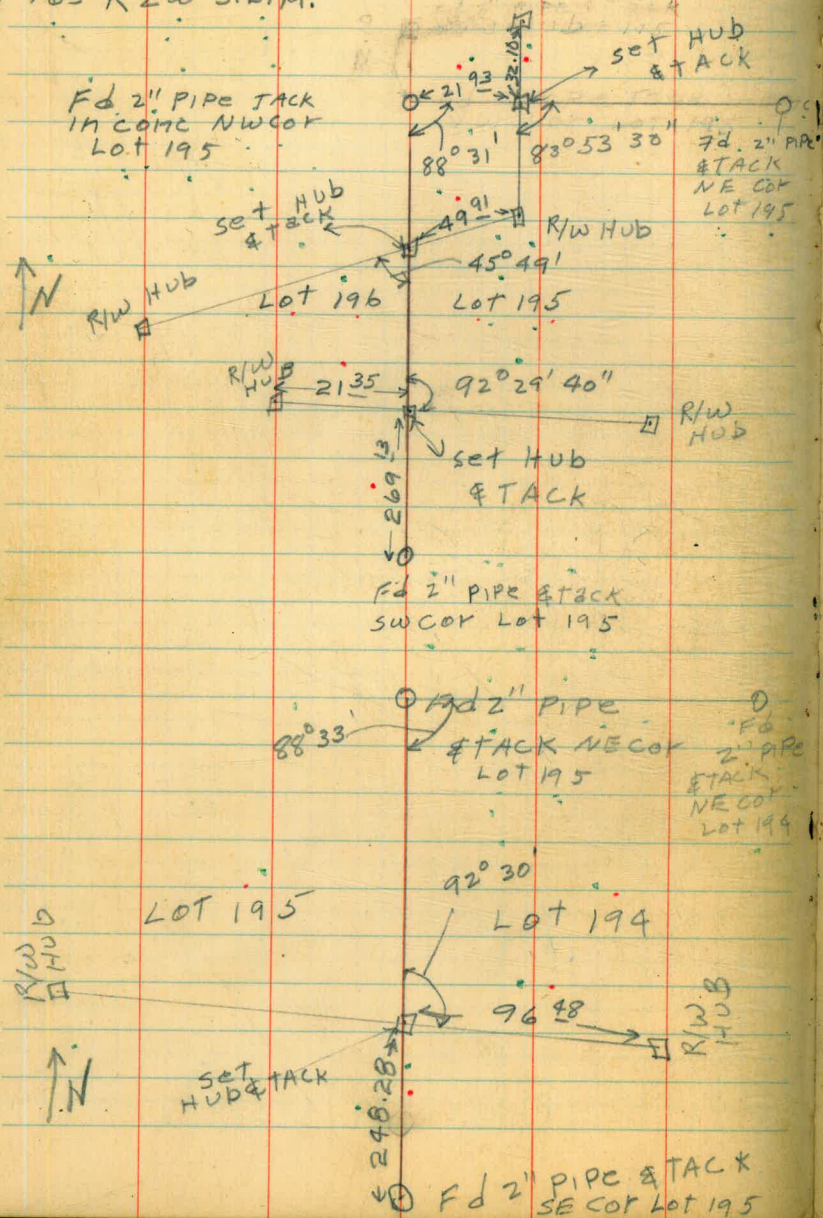






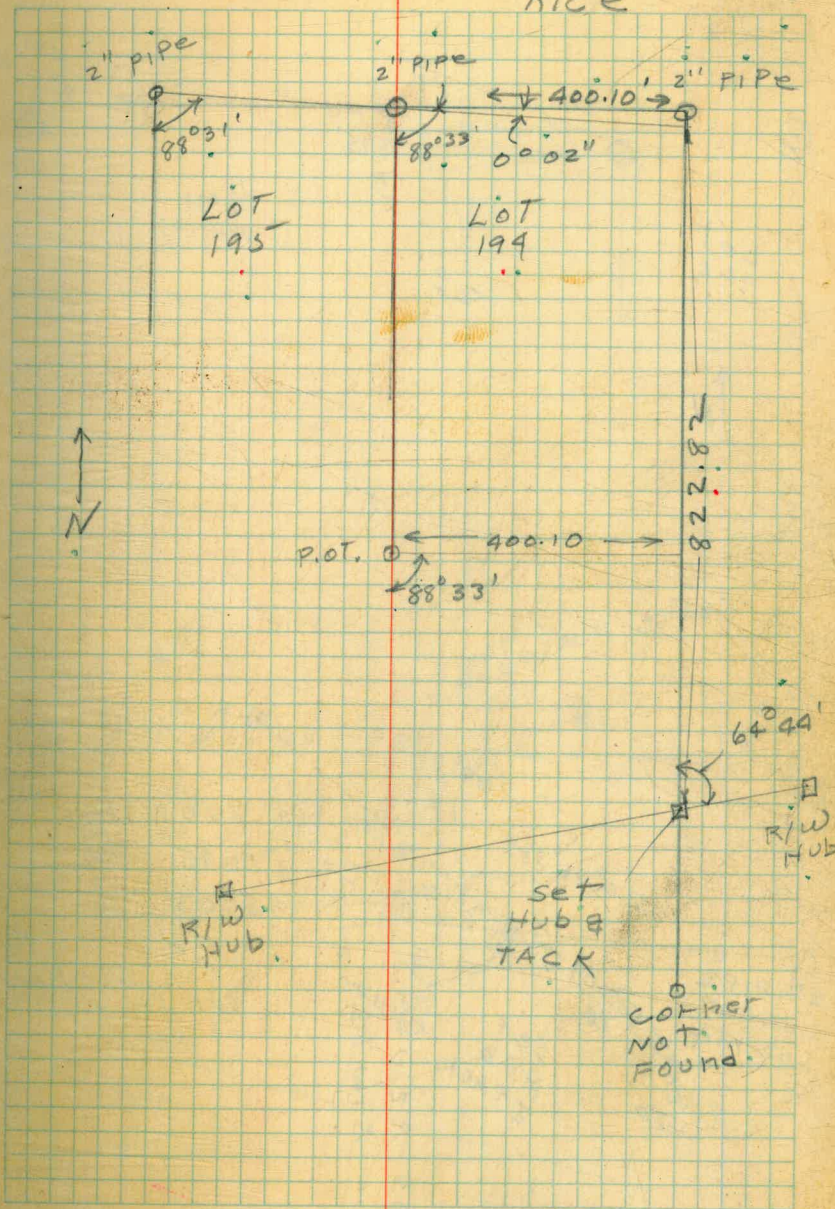


PROPERTY CORNER TIES TO R/W LINE
 Ground Mutt Bay Lake SECTION 12
 T 165 R 2W S.B.M.



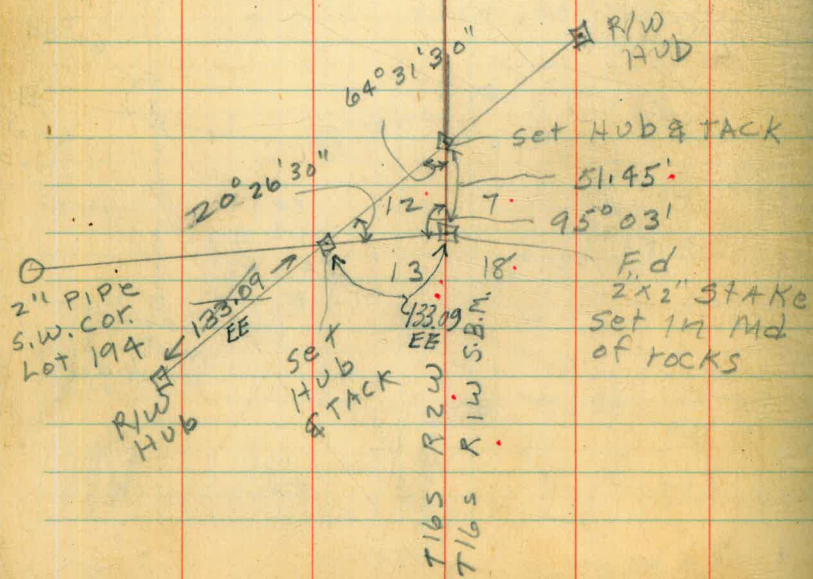
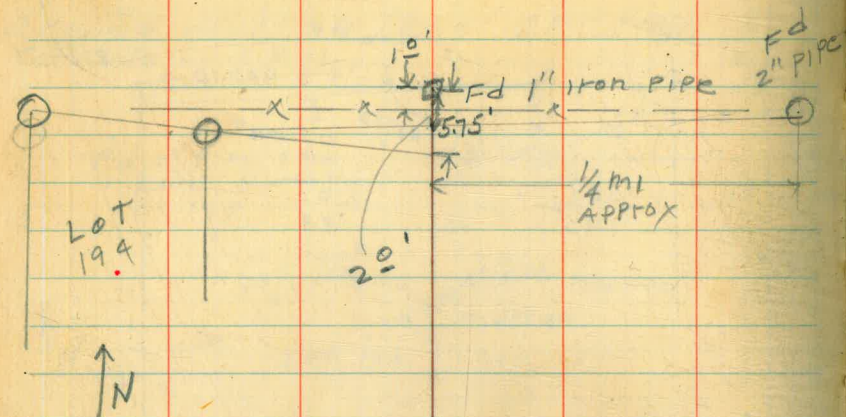
6-11-46
 Hot-dry

Nelson
 Leohard 22
 Rice



6-12-46
Hot-dry

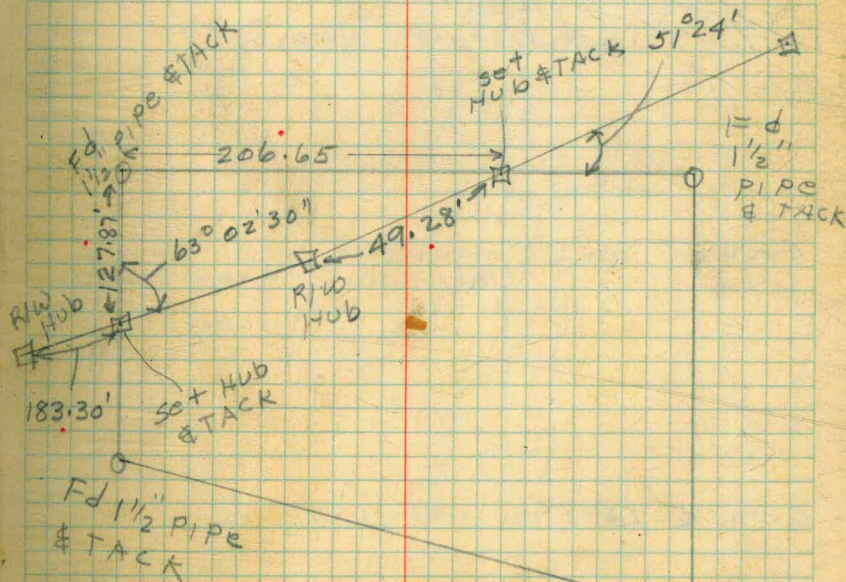
Nelson
Leonard
RICE



6-13-46
Hot-dry

Nelson
Leonard
RICE

23



R/W line west side Lot 98
 La Mesa Colony - S.H. Grove
 Alignment Road to Tr. Plant from (owner)
 Murray BLVD via Kiowa drive.

END
 6+95.40 North Prop. Line Lot 98
 6+87 E CROSS ROAD 10' wide

Note see page
 41 & 42 for cross sections

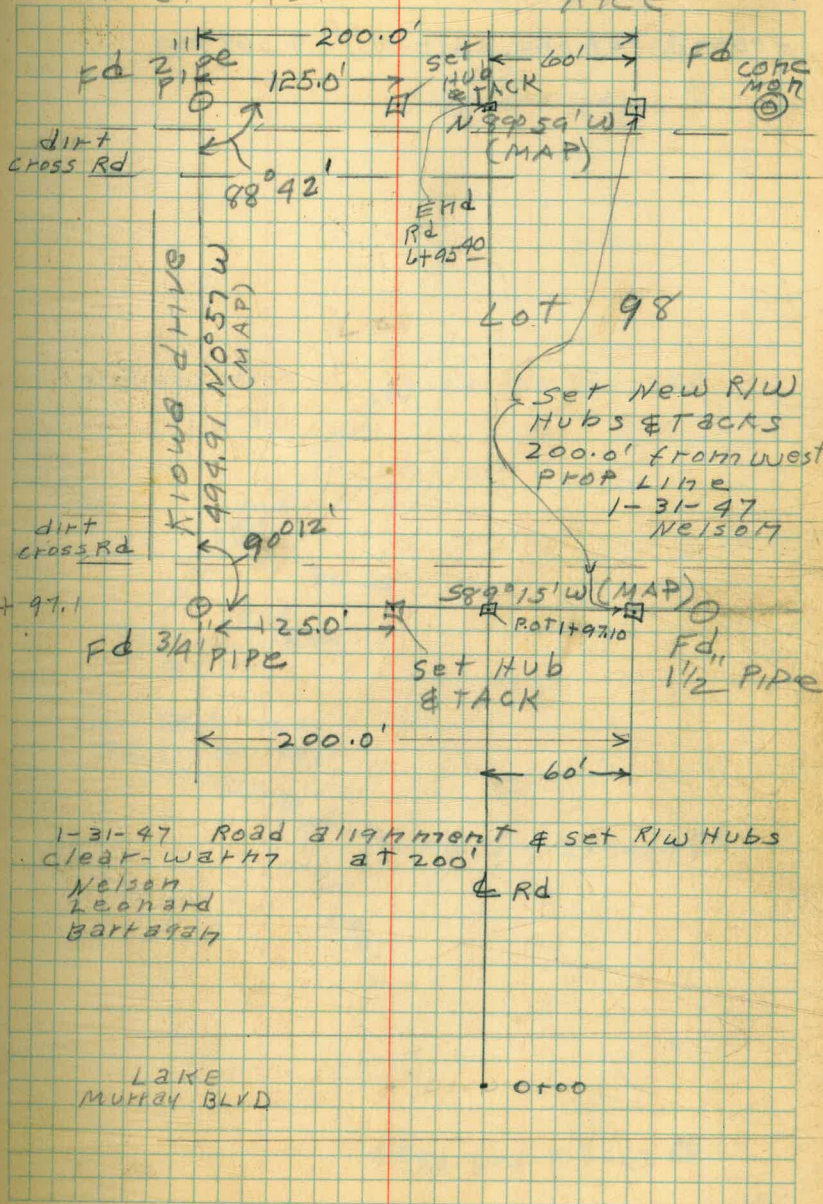
2+05 E CROSS ROAD 10' wide

P.O.T
 1+97.10 south property line Lot 98

0+00 & LAKE Murray BLVD

6-11-46
 Clear - 140'

Nelson
 Leonard 24
 RICE

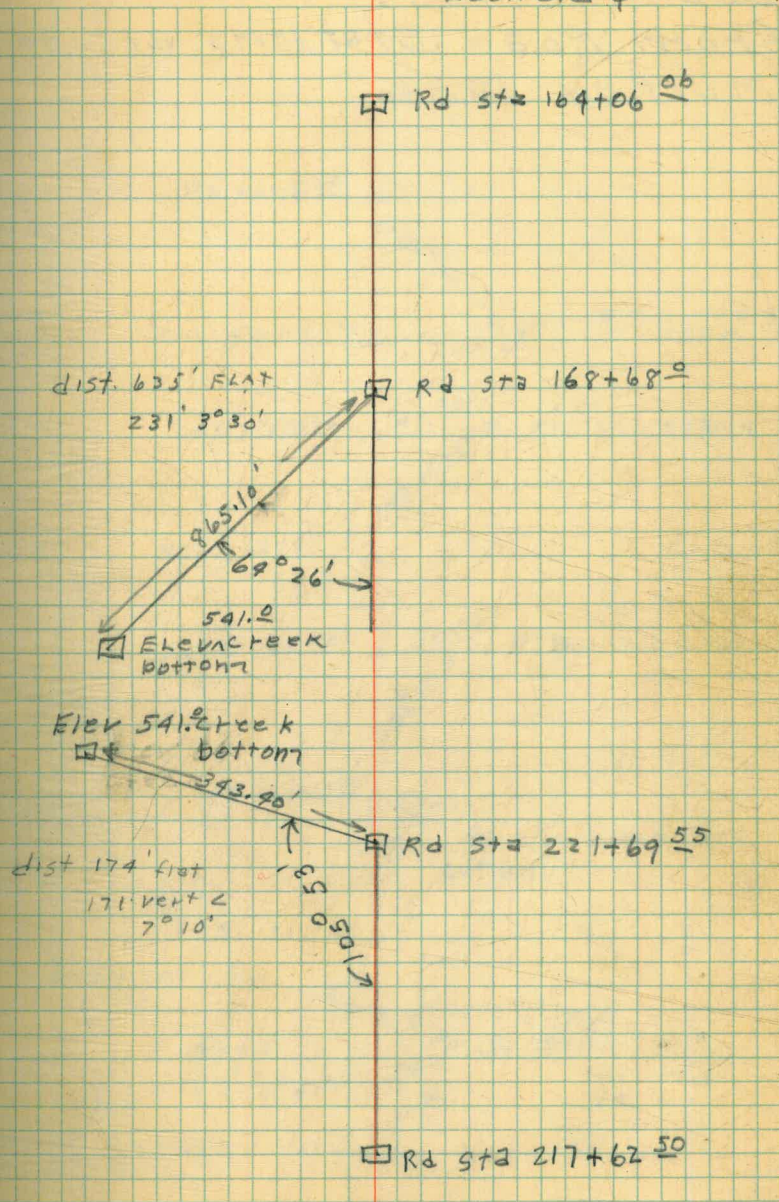


MURRAY LAKE
TIES TO ELEV 541.00 CREEK BOTTOMS

FROM STATIONS 221+69⁵⁵ & 168+68

2-9-46 CLEAR
WARTH

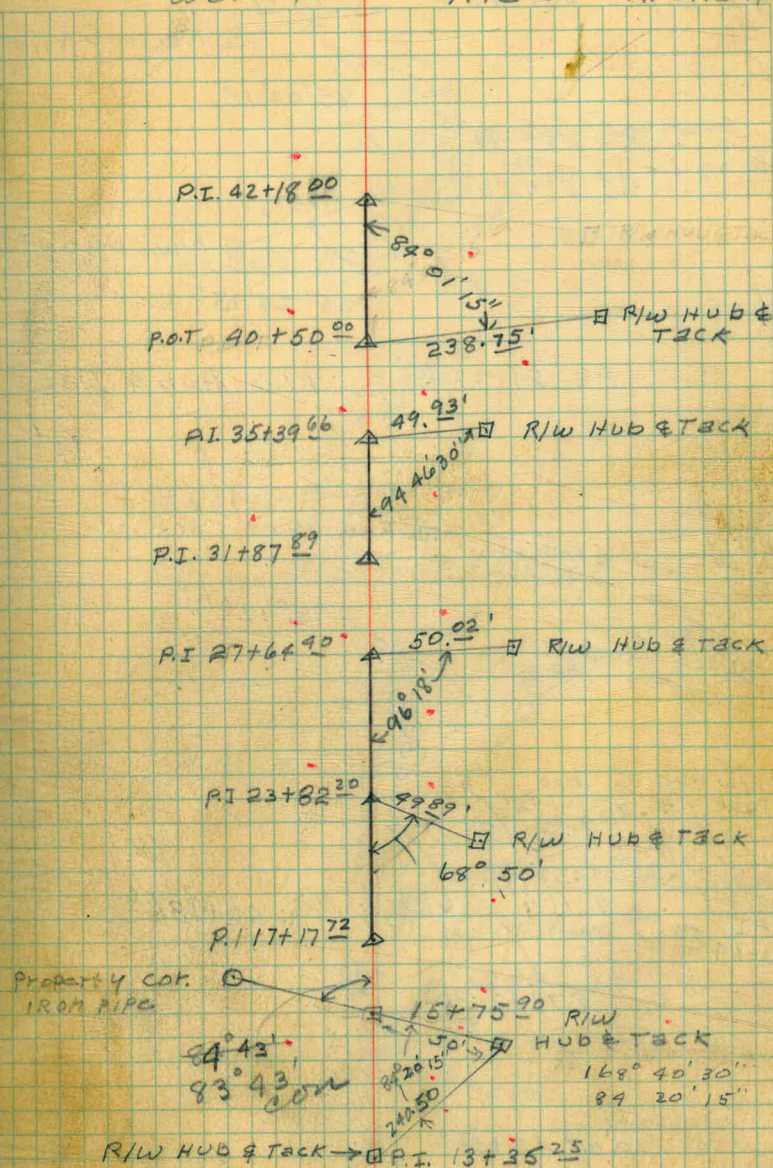
NEISON T
RICE NOTES
LEONARD P 25

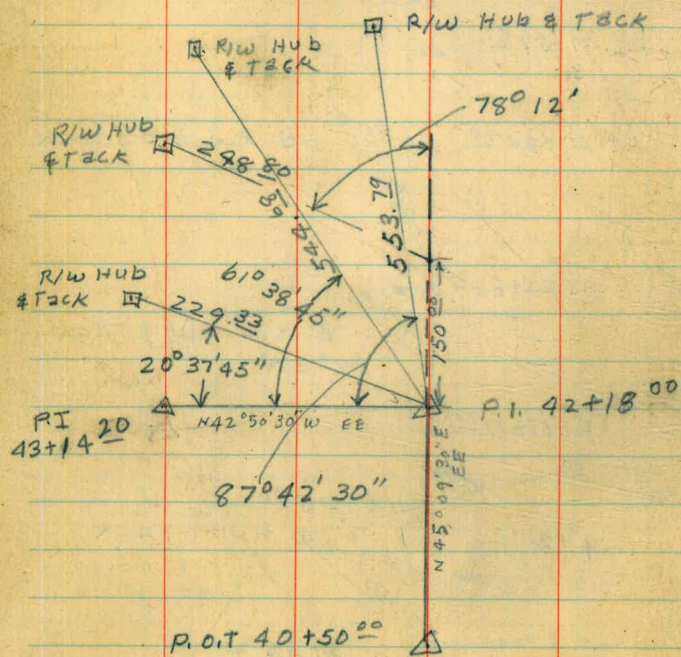
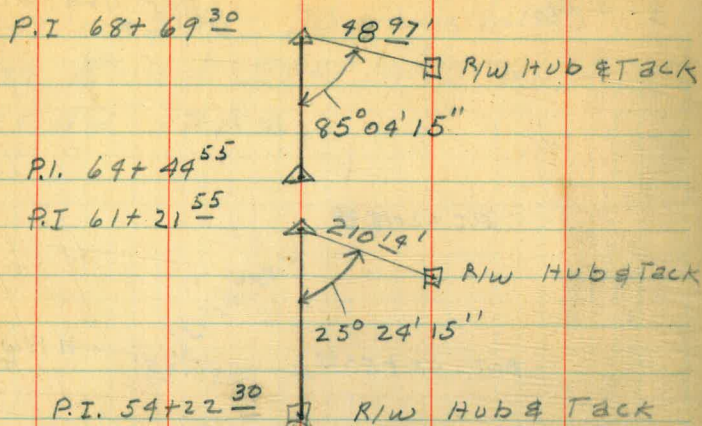


Location Ties to R/W Hubs
 from Road Stations around
 Murray Lake

3-4-46 clear
 warm

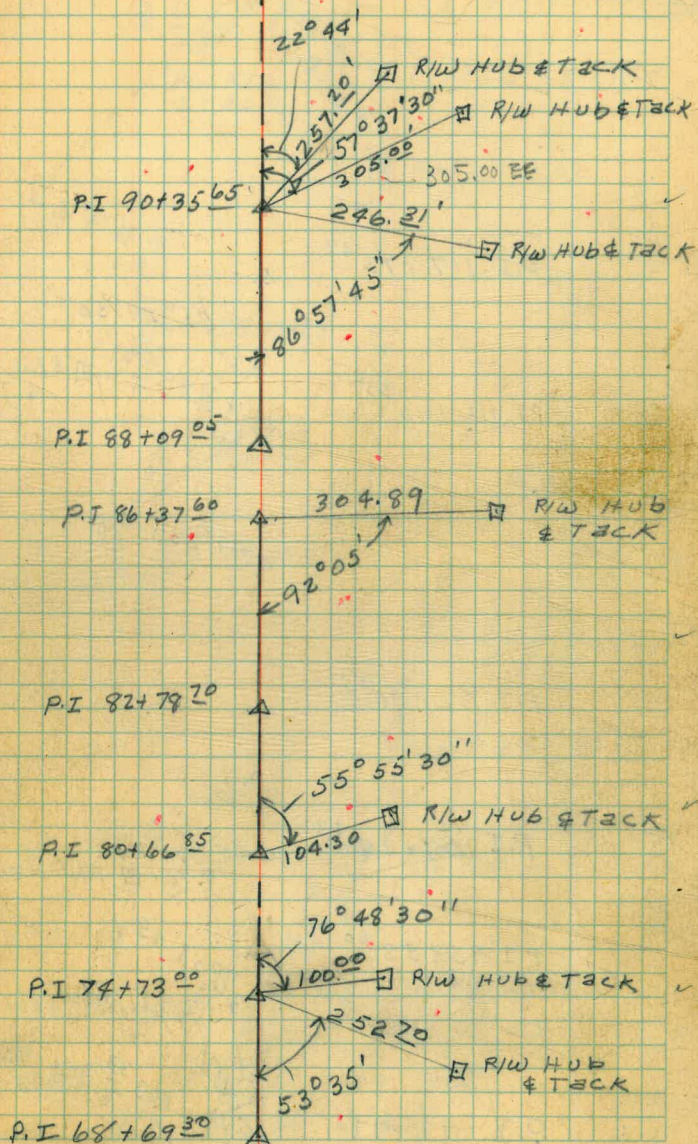
Nelson T Notes
 Leonard H chain 26
 Rice R. chain

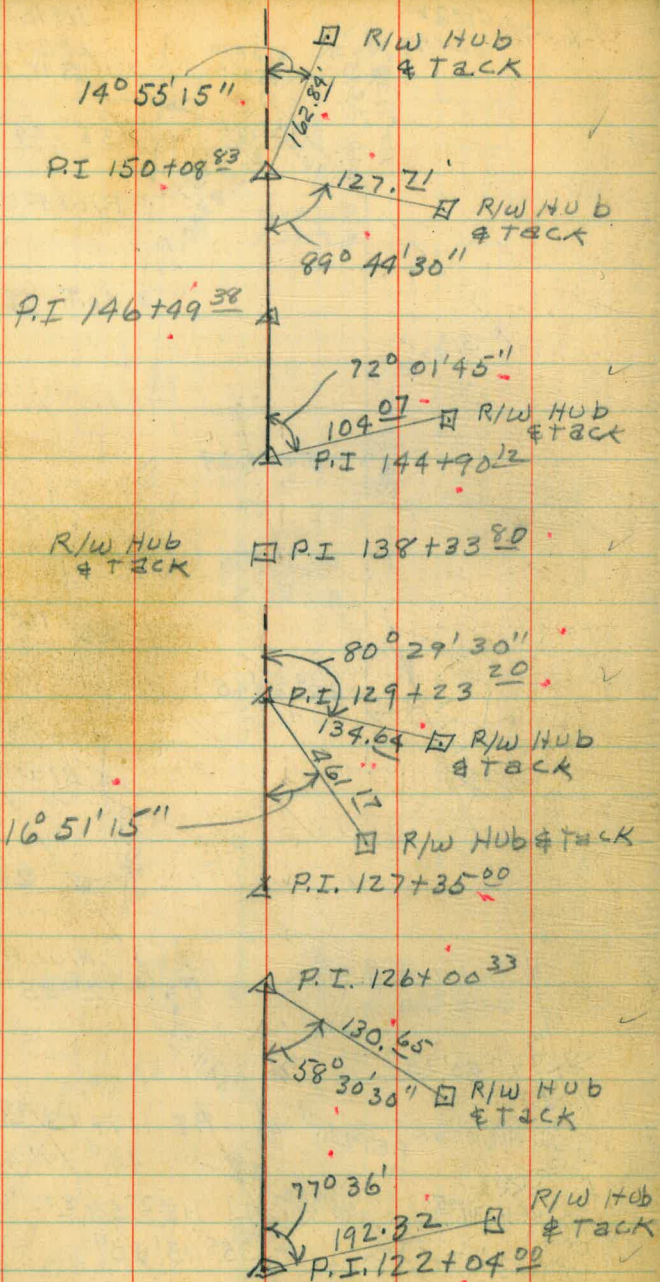




3-5-46 clear
Warren

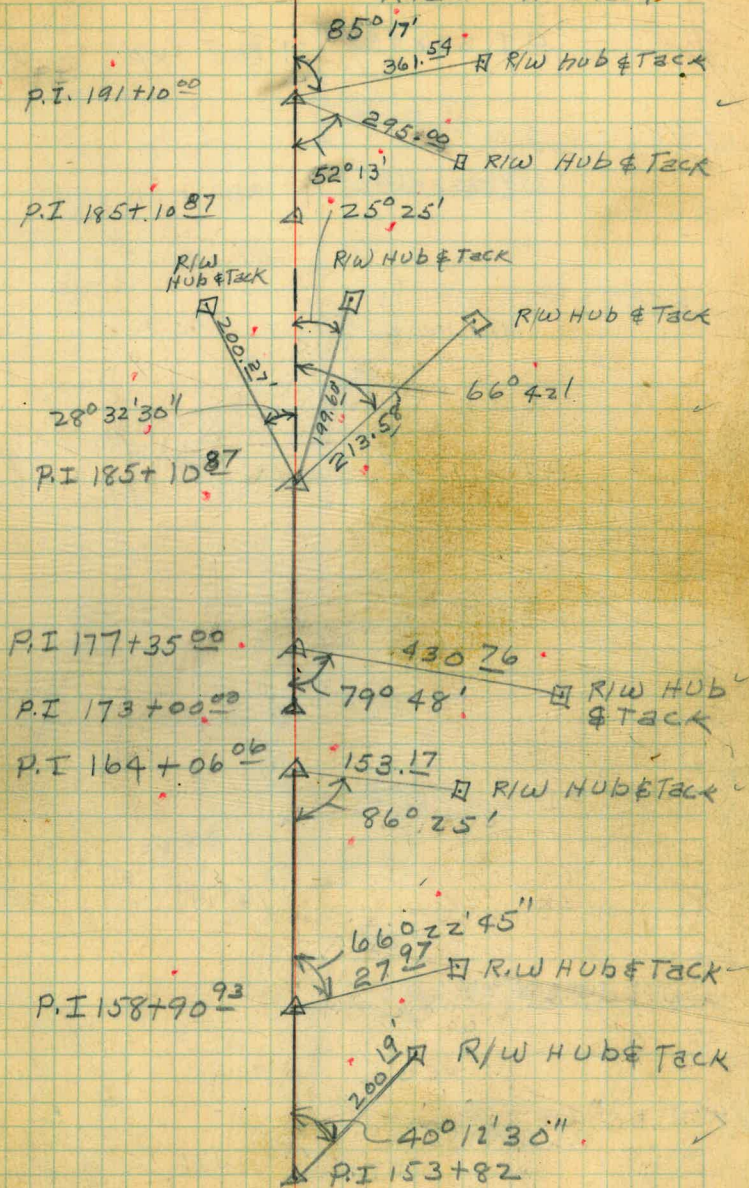
Nelson & Notes
Leonard H. Chain
Rice R. Chain 427





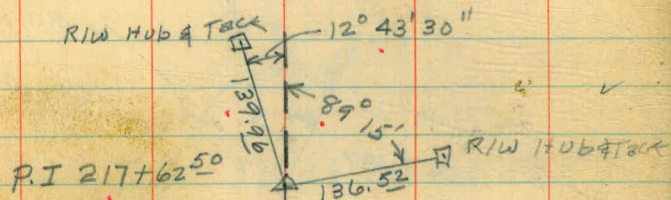
3-7-46 clear warm

Nelson Notes
 Leonard H. Chalmers
 Rice R. Chalmers 29

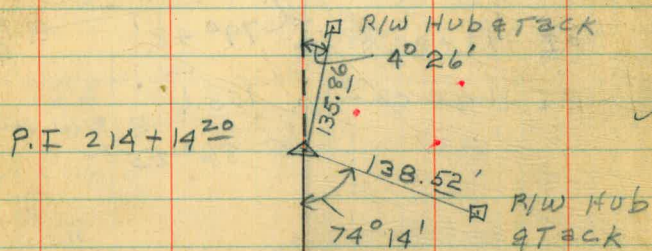


P.I. 226+46⁰⁰ R/W Hub & Tack

P.I. 221+69⁵⁵ R/W Hub & Tack

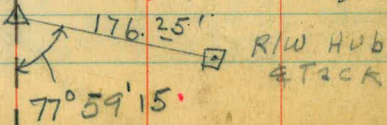


P.I. 215+95⁷⁰



P.I. 212+60

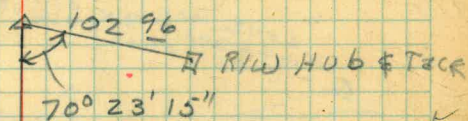
P.I. 209+55



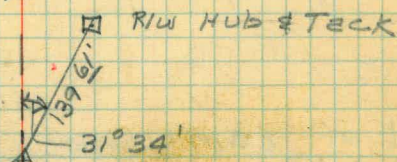
3-8-96 clear & warm

Nelson X Notes
Leonard H. Chalm 30
Rice R

P.I. 246+84⁹²

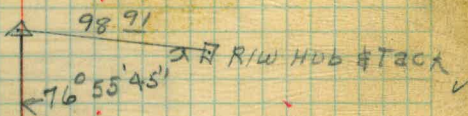


P.I. 245+11⁷⁰



P.I. 243+25⁰⁰

P.I. 241+50⁵⁹



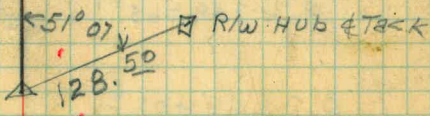
P.I. 237+65³⁰



P.I. 234+94³⁰



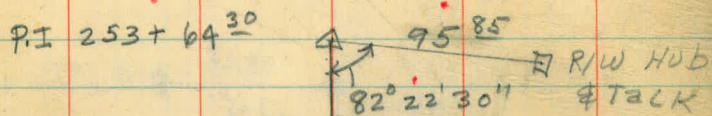
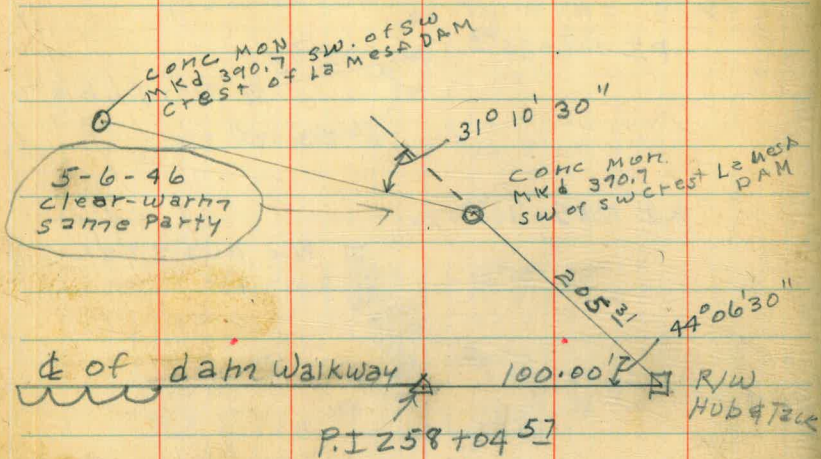
P.I. 229+80⁰⁰



3-9-46 clear-warm

Nelson T Notes
Leonard H. CH 814
RKE R. CH 319

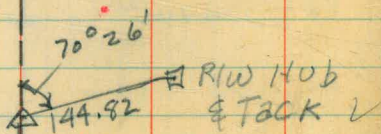
31



PI 252+15.78

PI 249+65.09

PI 248+06.61



Bliss
King Alignment Proposed Tunnel from
Davis the North End of Murray Lake to
Ph. Hills
5/18/46 San Diego River Watershed

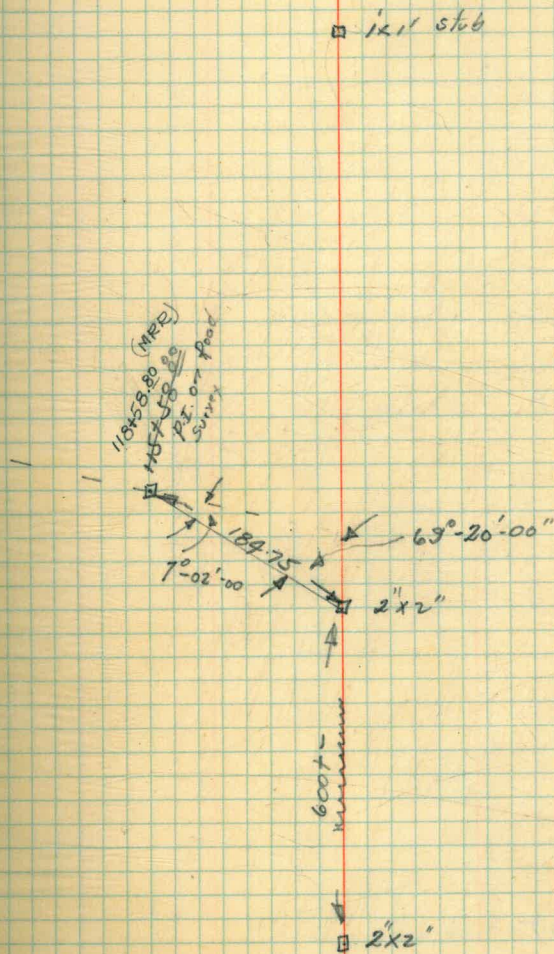
4+73.21 P.O.T.

122404 PI.
on Road Survey

6+00

P.O.T. on Back-Ten on Top of Hill to South

32



11+98 POT

8+29.²⁵ P.O.T.

▣ ix1 stub

▣ stub ix1

26+57 ⁷⁸
27+07 ⁷⁸ End of line

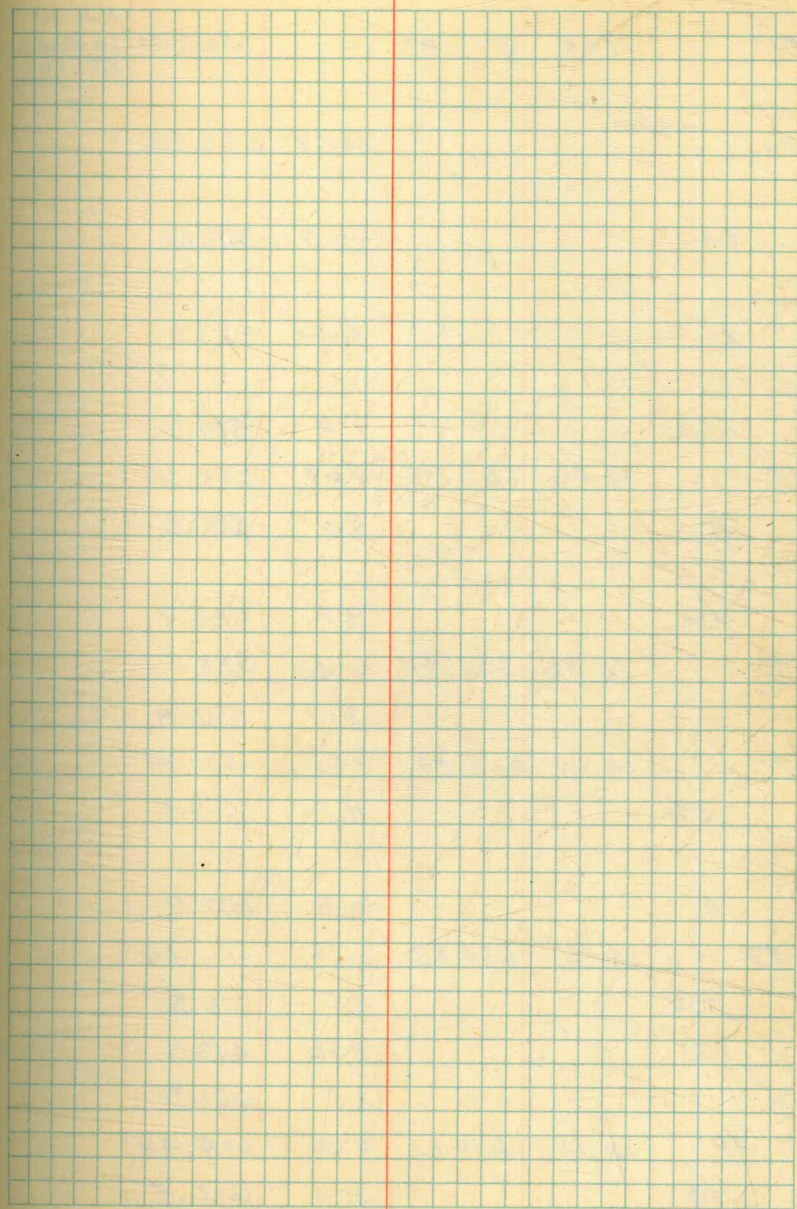
25+19 ¹⁹ P.O.T.

20+95 ²² P.O.T.

□ 2x2 Hub

□

□ stub



5/20/46

Profile levels over Proposed Tunnel
Morris Lake to S.D. River Basin

BM.	11.04	576.95		565.41	Hub Set on Road Lane Elev Corridor from Morris Dam
0+00	on slope		12.57	563.88	✓
+50			10.9	565.6	
1			6.2	570.3	
+50			1.9	574.6	
TP.	12.40	588.78	0.07	576.38	✓
2			8.0	580.8	
+50			3.1	585.7	
TP.	12.96	601.41	0.33	588.45	✓
3			9.0	592.4	
TP.	13.00	612.84	1.57	599.84	✓
+50			11.7	601.1	
4			0.6	612.2	
TP.	12.55	624.83	0.56	612.29	✓
+50			8.5	616.3	
+73			5.56	619.3	
5			3.5	621.3	
TP.	12.35	636.83	0.35	624.48	✓
+50			10.3	626.5	

36

63683

37

6			6.3	630.5
T.P.	11.45	647.78	0.50	636.33 ✓
+50			1.40	633.8
7			10.3	637.5
+50			7.6	640.2
8			5.2	642.6
+29 ²⁵	POT		3.70	644.1
+50			3.0	644.8
T.P.	11.44	658.55	0.67	647.11 ✓
9			11.3	647.3
+50			9.6	649.0
10			8.4	650.2
+50			4.8	653.8
11			3.7	654.9
+50			3.3	655.3
+38	POT on stake		3.18	655.37
12			3.1	655.5
+50			4.7	653.9
13			6.8	651.8
T.P.	0.36	653.03	5.88	652.67 ✓
+50			5.6	647.4
14			8.5	644.5
T.P.	0.21	640.35	12.89	640.14 ✓
+50			3.0	637.4
15			10.5	629.9
T.P.	1.83	629.69	12.49	627.86 ✓

629.69'

15	+50		5.3	629.4
16			12.9	616.8
	+50		16.1	613.6
T.P.	1.85	619.20	12.34	617.35
17			6.8	612.4
	+50		7.3	611.9
18			6.6	612.6
	+50		5.7	613.5
19			6.0	613.2
	+50		5.6	613.6
20			8.5	610.7
POT.	+45 ²²	0.66	12 ³⁹ 29	606.21
	+50		1.0	605.9
21			3.1	603.8
	+50		9.8	597.1
T.P.	0.00	599.81	12.06	599.81 ✓
22			5.9	588.91
	+50		9.4	585.4
T.P.	0.32	582.40	12.73	582.08
23			1.9	580.5
	+50		7.4	575.0
24			12.6	569.8
T.P.	0.85	570.61	12.64	569.76 ✓
	+50		6.3	564.3

38

570.61

25 to			13.1	557.5	
TP	0.21	558.08	12.74	557.87	✓
+19 ¹⁰			3.16	554.92	
+50			10.1	548.00	
+63	10 Creek bed		14.2	543.9	
+90	" " "		16.0	542.1	
26+15			13.5	544.5	
TP	0.92	546.56	12.44	545.64	✓
26+50			5.7	540.9	
+57.78					
	on Hub. Edge side		7.66	538.90	* Note This Point 25' Below Take off.
+61	Bottom ditch		8.7	537.9	
TP End line	13.06	551.96	7.66	538.90	
TP	11.86	562.88	0.94	551.02	
TP	12.93	575.14	0.67	562.21	
TP	12.41	587.43	0.12	575.02	
TP	12.94	600.22	0.15	587.28	
TP	12.50	612.67	0.05	600.17	
TP	12.48	624.93	0.22	612.45	
TP	12.75	637.51	0.17	624.76	
TP	12.20	649.42	0.29	637.22	
TP	7.42	656.69	0.15	649.27	
TP	0.05	646.64	10.10	646.59	
TP	0.49	634.78	12.35	634.29	
TP	0.47	622.49	12.76	622.02	
TP	0.79	610.23	13.05	609.44	

		T		
		610.23		
TP	0.12	597.40	12.95	597.28
TP	0.09	584.40	13.09	584.31
TP	3.84	575.31	12.93	571.47
Check starting JM			992	565.39
				<u>565.41</u>
				0.02 error

Cross sections Road to Treatment Plant from Murray Blvd via Kiowa drive,

10.19 524.87

514.68

0+00

+15

NOTE see page 24
FOR Alignment

+18

+24

+50

1+00

+50

T.P. 13.06 537.22 0.71 524.16

T.P. 12.50 543.23 6.49 530.73

+97

2+00

2+05 4 Rd

+50

3+00

+50

1-31-41
Cleat-walk

Veison Notes
Leonard
Battagah T 41

CITY DATUM
BM LATAK & KIOWA LAKE MURRAY BLVD

15.0 16.7 17.8 19.0 19.7
9.3 8.1 7.0 5.9 5.2
100 50 50 100

16.5 17.7 19.0
8.4 7.2 5.9
50 60

17.4 18.7 20.0
7.5 6.2 4.9
50 60

16.8 18.0 19.5
8.1 6.9 5.4
50 60

17.5 18.4 19.3
7.4 6.5 5.6
50 60

18.1 19.7 20.1
6.2 5.2 4.7 7.8
50 30 60

20.6 21.9 22.2
4.3 3.0 2.7
50 60

ON HUB STA 1+97.1

22.6 24.4 25.3
20.6 18.8 17.9
50 60
21.2 23.2 24.9 26.9
22.0 20.0 18.3 17.2 16.3
100 50 50 100

25.3 28.0 30.6
17.9 15.2 12.6
50 60

26.6 30.5 32.5
16.6 12.7 7.0
50 60

26.9 31.2 35.4 37.2
16.3 12.0 8.0 0.8
50 35 60

543.23 ✓

4+00

+50

T. P. 9.90 541.22 11.91 531.32 ✓

5+00

+50

6+00

+50

+ 87 £ Rd

CK. B.M

5.71 535.51 = 535.51

26.5	531.0	34.4	41.0
16.7	12.2	8.8	2.2
50		33	60
26.9	530.63	33.9	38.6
16.3	12.6	9.3	7.6
50		32	60
26.8	530.9	37.2	
17.4	10.3	4.0	
50		60	
28.5	531.8	37.0	
12.7	9.4	7.2	
50		60	
30.5	532.3	36.9	
10.7	8.9	4.3	
50		60	
32.3	534.0	37.8	
8.9	7.2	3.4	
50		60	
34.6	535.8	38.6	39.3
6.6	5.4	2.6	1.9
7.8		50	60
6.2			1.4
7.0			100
7.3			
6.7			
50			
189.183			
162			
150			
100			
50			
42.6			

34.6
 33.4
 35.0
 34.2
 33.9
 34.5
 535.8
 5.4
 2.6
 1.9
 1.4
 100
 ↑
 £
 KIDWA

Bliss
King
96. tips
Nieman
2/22/47

Test Holes. Angles Turned from 3137⁶⁰
Alignment for Drainage Ditch. See Page 1
Sighted on 6+34⁰⁵

-0
Hot

#1	116'	6°-28' Lt
#2	298'	22°-25'-00" Lt
#3	472'	32°-28'-00" "
#4	648'	39°-00'-00" "
#5	790'	42°-08'-00" "
#6	900'	43°-40'-00" Lt

Test Holes. Angles Turned from 118158⁸⁰
L. Turned by Sighting 117+13⁴⁸ See Page 28

#2	580'	87°-16'-00" Lt
#1	513'	79°-34'-00" "
#3	296'	60°-58'-00" "
#4	565'	18°-42'-00" "
#5	698'	17°-40'-00" "
#6	1003'	17°-16'-00" Lt

Telephone Pole Set Up Lake Murray

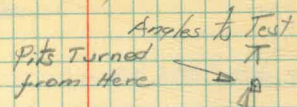
Test Pit #	Dist.	L Angle
#1	34'	23°-14' Rt
" #4	165	0°-28' Lt
" #3	195	27°-56' Lt
" #5	120'	47°-30' "
" #2	92	25°-26' "

Angles Turned Counter clockwise Sighting to East See sketch

Kiowa Drive



Test Holes Tied to Telephone Alignment

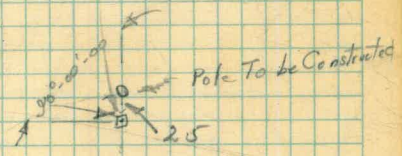


Bliss
Kiny
Phillips
Nemo v1
2/29/97

Road to Lake Murray

597.20

367.78'



"A" Line See large map #2963

Traverse of Prop Line Lake

Mog Baring

6+60.09

5+13.25

2+38.82 L. RT. 24°-06'-00" N 96°-15' E

0+00

N 22°-0' E

Murray Preliminary Road Location

H. 11 45

Bliss Notes

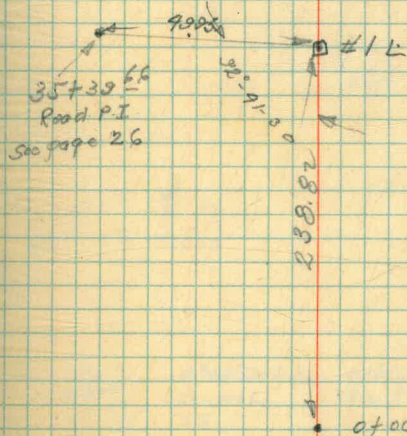
King T

Leonard M. Choin

Memor 3/24/47

□ Fd 2"x2" Hub P.O.T. East Line Sec 12
See page 23

□ Fd 2"x2" Hub P.O.T. Int. Section Sec 12
See page 23



27+64.80 50.02 → □ 2"x2" Hub
Road Survey See page 26

17+80 L L.Lt 74°-23'-30"

N 89° 00' 00" E
S 27° 00' 00" W

15+32 33 L.Lt 86°-11'-45"

N 76°-10'-00" W

10+41 +/- POT

7+95 70 L.Lt 36°-29'-00" N 10°-15'-00" E

42+18
Road Survey
See page 27

544.58

46

2x2 Hub #4 L

2x2 Hub #3 L

553.79

POT Nail

see
page 27 42+18

POT 238.35 2x2 Hub
Road Survey See page #2 R.O.W L:
40+30 26

29489¹⁰ P.O.T.

21484⁵⁸ L. 35° 03' 00" R. 548° 15' 00" W

20467⁴⁵ L. 44° 16' 11" 00 513° 15' 00" W

19455+ P.O.T.

Fd 2x2 Hub
int 5 line lot 194 see page 22

42418 P.T.
Road Survey Sec page 27

229.38

100
1-84
8-82

2x2 Hub #6 L.

2x2 Hub #5 L.

Nail

43+85²⁶ L. Rt 77°06'00

Mag Bearing
N 28°30'00E

Δ 38+42³² L. 56°12' Rt

N 49° W

38+20⁹⁸ P.O.T.

34+21³³ P.O.T.

33+24⁸⁵ L. Rt 27°46'00 576°30'00W

48.

□ #9

□ #8

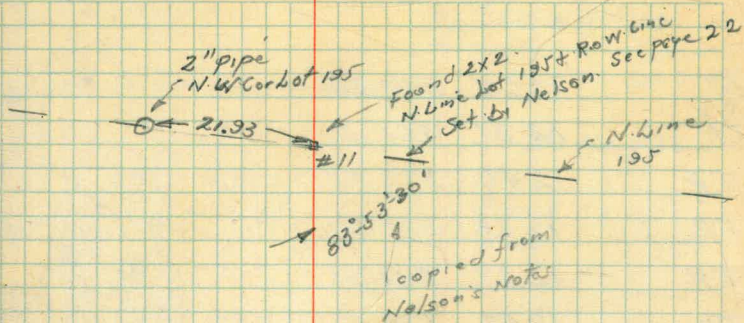
□ East Line Lot 196

□ East Line Lot 195

□ #7 34+22³⁰

50+29¹⁰ int N Line lot 135

N 21° 30' 00" W

48+58⁵⁷ L.L. 50° 27' 00"48+08⁶⁸ P.O.T. int W Line lot 135

2" Hub
2x2
210

2x2 Hub

Profile levels over R.O.W. & for

BM	12.69	549.23		536.59
T.P.	12.31	561.53	0.01	549.22 ✓
T.P.	12.46	573.05	0.94	560.59 ✓
T.P.	12.88	585.67	0.26	572.79 ✓
T.P.	12.87	598.43	0.11	585.56 ✓
T.P.	12.48	610.81	0.10	598.33 ✓

0+00 5.3 605.5

0+40 2.3 608.5

+55 4.4 606.4

1+00 3.1 607.7

+40 1.3 609.5

+65 3.2 607.6

+80 2.4 608.4

2+0 4.3 606.5

+38⁸² 4.5.73 612.49 4.05 606.76 ✓

+75 6.6 605.9

Contemplated Road Lake Murray

Top of Bench to BM 542.51

Murray Dam 542.51

547.93

11.38

Elev of Lake March 27-97

Elev of Lake 536.54

Hill

Bliss T

King 3/27/47

Leonard

Nienow

π
612.49 ✓

3+00			5.5	607.0
+50			5.1	607.4
4			3.8	608.7
+15			4.4	608.1
+50			4.6	607.9
5			5.3	607.2
+35			4.9	607.6
+50			8.4	606.1
6			8.2	604.3
+25			11.3	601.2
T.P.	0.64	600.49	12.64	599.85 ✓
+75			1.8	598.7
7			4.2	596.3
+35			6.2	594.3
+60			9.2	591.3
+75			12.5	588.0
T.P.	0.43	588.61	12.31	588.18 ✓
+25 ²⁰	L on Hub		2.51	586.10 ✓
8+0			3.4	585.2
+48			16.9	571.7
+56			17.5	571.1

51

W Side Draw
Lump of Draw

*
588.61 ✓

+68			16.7	571.9
970			8.1	580.5
T.P.	10.85	588.86 ✓	0.60	588.61 ✓
+37			12.6	586.26
+83			9.2	589.7
1010			8.9	590.0
+50			7.3	591.6
11			6.5	592.4
+50			7.3	591.6
12			6.7	592.2
+42			6.6	592.3
+80			10.0	588.9
13			8.9	590.0
+32			6.3	592.6
+60			7.2	591.7
14			6.0	592.9
+25			4.3	594.6
+45			3.2	595.3
+65			4.8	594.1
1540			3.7	595.2
+32 ³³	6.82	596.01 ✓	3.67	595.19 ✓
+50			3.8	592.2
+94			12.6	583.4
T.P.	2.39	585.34 ✓	13.06	582.95 ✓
16			4.5	580.8

52.

East Side, Mass

+20	Top slope		10.5	574.8
+50			12.1	73.2
+85	Bank Wash		13.5	71.8
+90	in Wash		15.7	69.6
+98	" "		14.3	71.0
17+00	OH Bank Wash		9.5	75.8
+02	Top Bank		8.1	77.2
+10			7.1	78.2
T.P.	11.38	596.61	0.11	585.23 ✓
+50			9.7	86.9
+80 ¹⁷			6.09	590.52 ✓
18			5.3	91.3
+50			5.4	91.2
19			4.9	91.7
+50			4.6	92.0
+75			6.3	90.3
20			6.3	90.3
+25			10.7	85.9
+50	Bottom ctr Draw		17.0	79.6
+67.95	L		14.8	81.8
21			9.5	87.1
+36			7.4	89.2
+60			7.9	88.7
T.P.	11.88	600.12 ✓	8.37	588.24 ✓
+89.58				
00 H.O.B.				

π
600.12 ✓

54

22+0 11.4 588.7

+50 10.5 89.6

23 9.9 70.2

+50 10.2 89.7

24 9.6 90.5

+25 9.2 70.7

+50 9.0 91.1

25 8.3 91.8

+35 8.5 91.6

+50 8.1 92.0

26 7.9 92.2

TP. 8.03 604.76 3.39 596.73 ✓

+50 11.6 593.16

27 16.4 594.4

604.76 ✓

55.

27+50 10.0 594.76

28 8.2 96.6

+50 8.5 96.3

29 8.8 96.0

+50 9.4 95.4

+50 9.8 95.0

30 9.2 95.6

+50 10.6 94.2

31 11.0 93.8

+25 10.1 94.7

+50 12.0 92.8

T.P. 7.61 601.62 ✓ 10.75 594.01 ✓

32 8.0 93.6

+50 8.8 92.8

33 10.0 91.6

+24 ⁸⁵ on HwdL 10.42 91.2

+50 10.1 91.5

34 10.7 90.9

601.62 ✓

34+15 10.0 591.6

+30 12.0 89.6

+50 12.0 89.6

+75 11.0 90.6

35 13.0 88.6

7P. 3.64 592.38 ✓ 12.88 588.74 ✓

+29 3.8 88.6

+45 5.4 87.0

36 6.2 86.2

+50 6.6 85.8

37 7.2 85.2

+19 8.8 83.6

+35 7.7 84.7

+60 9.0 83.4

38 9.5 82.9

+42³² L 10.36 82.0

TPionHub 7.14 589.16 ✓ 10.36 582.02 ✓

39 6.0 83.2

+50 6.2 83.0

56

582.6 ✓

40 6.4 582.8

+50 6.4 82.8

41 8.0 81.2

+50 5.7 83.5

42 5.2 84.0

+50 5.8 83.4

43 6.7 82.5

+40 6.2 83.0

+85^{25L}_{on Hob} 11.24 593.62 ✓ 6.78 582.38 ✓

44 9.7 83.9

+20 11.8 81.8

+42 9.9 83.7

+20 11.2 82.4

57

45		8.1	585.5
+18		10.0	83.6
+43		7.8	85.8
+59		9.3	84.3
+73		7.8	85.8
45		9.0	84.6
+17		7.3	86.3
+56		7.3	86.3
47		6.3	87.3
+50		6.6	87.0
+75		7.7	85.9
48		11.0	82.6
+08	Bottom bray	12.5	81.1

59362 ✓

59

48+35 80 585.6

T.P. on Hub
+58⁵⁷ 5.93 592.89 ✓ 6.66 586.96 ✓

49+0 6.4 86.5

+35 3.3 89.6

+65 5.1 87.8

50+0 3.4 89.5

+29¹⁰ End of line on Hub 4.81 588.08

T.P. 1.01 580.85 ✓ 13.05 579.84 ✓

T.P. 0.99 569.14 ✓ 12.70 568.15 ✓

T.P. 0.76 556.85 ✓ 13.09 556.10 ✓

T.P. 6.66 546.10 ✓ 11.42 545.44 ✓

Surface
Check of Lake 9.00 PM 3/27/07 9.61 536.49 ✓

536.54
0.05 Diff

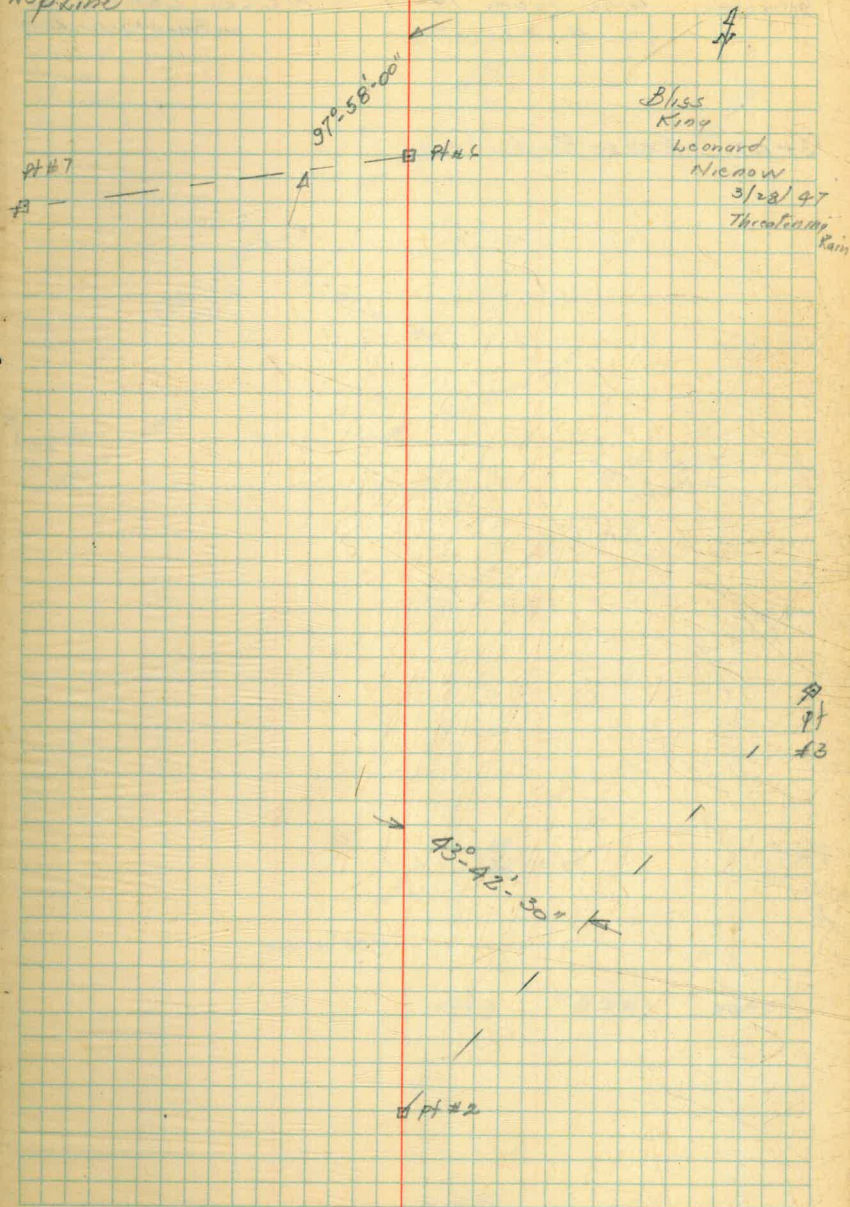
"B" line
Preliminary Line from Pt #2 to Pt #6 Lake Murray
For Road location
Mag Bearing
Levels on page 64

5705.30 End

N 31°-30' W

0700

Prop line



Preliminary "C" Line
 Line From Pt #4 to NE Cor Lot 12
 For Road Location on Transmission Line

3+09 End on Rancho

1+50 2+

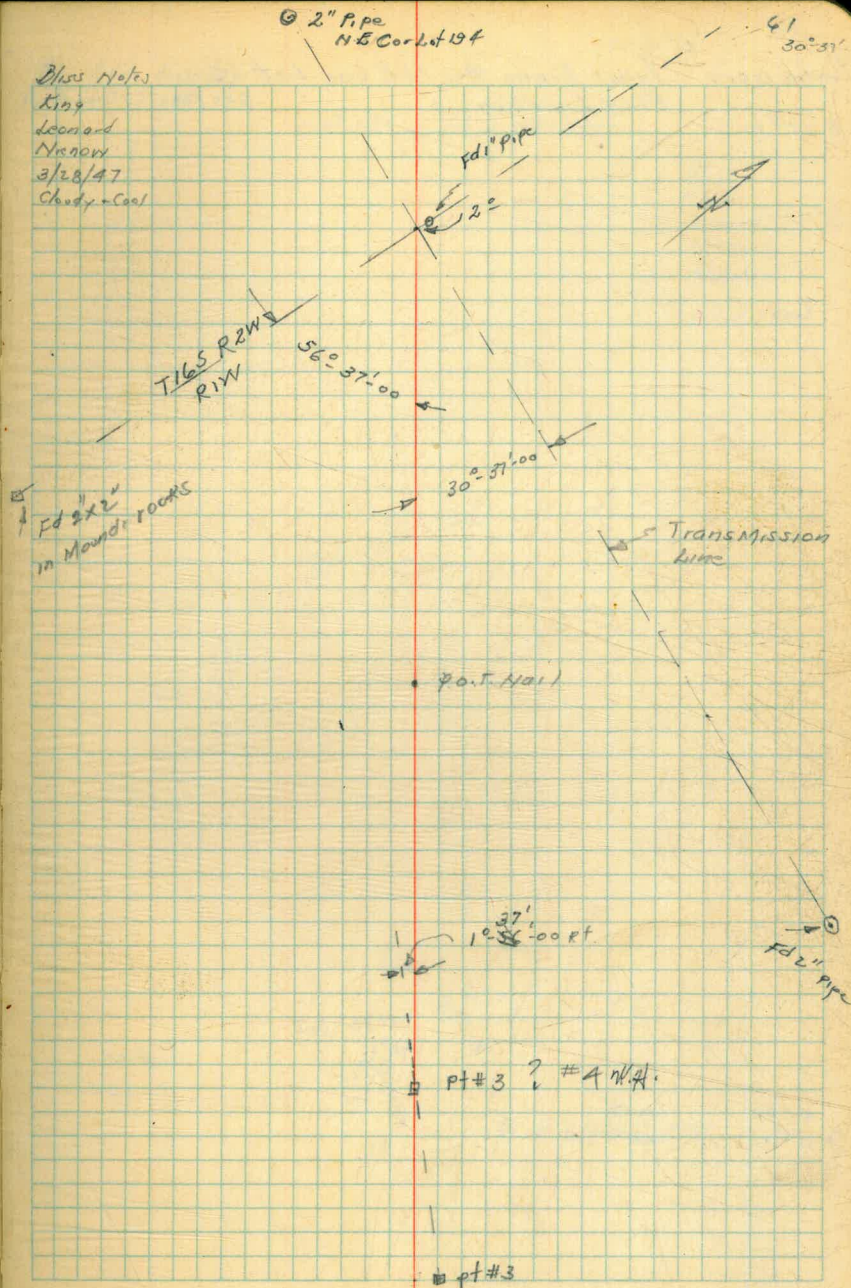
0+00

N 74° - 30' - 00" E

2" Pipe
 N 50° Cor Lot 12

41
 30° 31'

Class Notes
 King
 Leonard
 McNary
 3/28/47
 Chady + Cool



Preliminary "D" line
 Line From the NE Cor Lot 12
 Road Location See Page '67' for level
 8+12.3+- Mag Bearing

N 72°-30 E

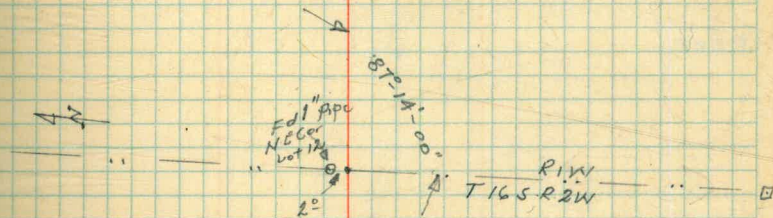
0+00

to 812' Eastly

Ed 2" iron pipe

Bliss
 King
 Leonard
 Nienow
 3/28/47
 cloudy & cool

Transmission Line



2" iron pipe NE Cor Lot 124

'E' Line

Preliminary Line from Pt. #3 to a Pt. on Road Location

3124 ¹²

= 6450

0700

N16°-00'-00" E

Transmission Line

2" 50' 1100' Pipe
0.22

650'
A

121°-07'-00"

Nail

Transmission Line

715' 5' 20"

5°-59'-00" RT.

#3

#2

63.

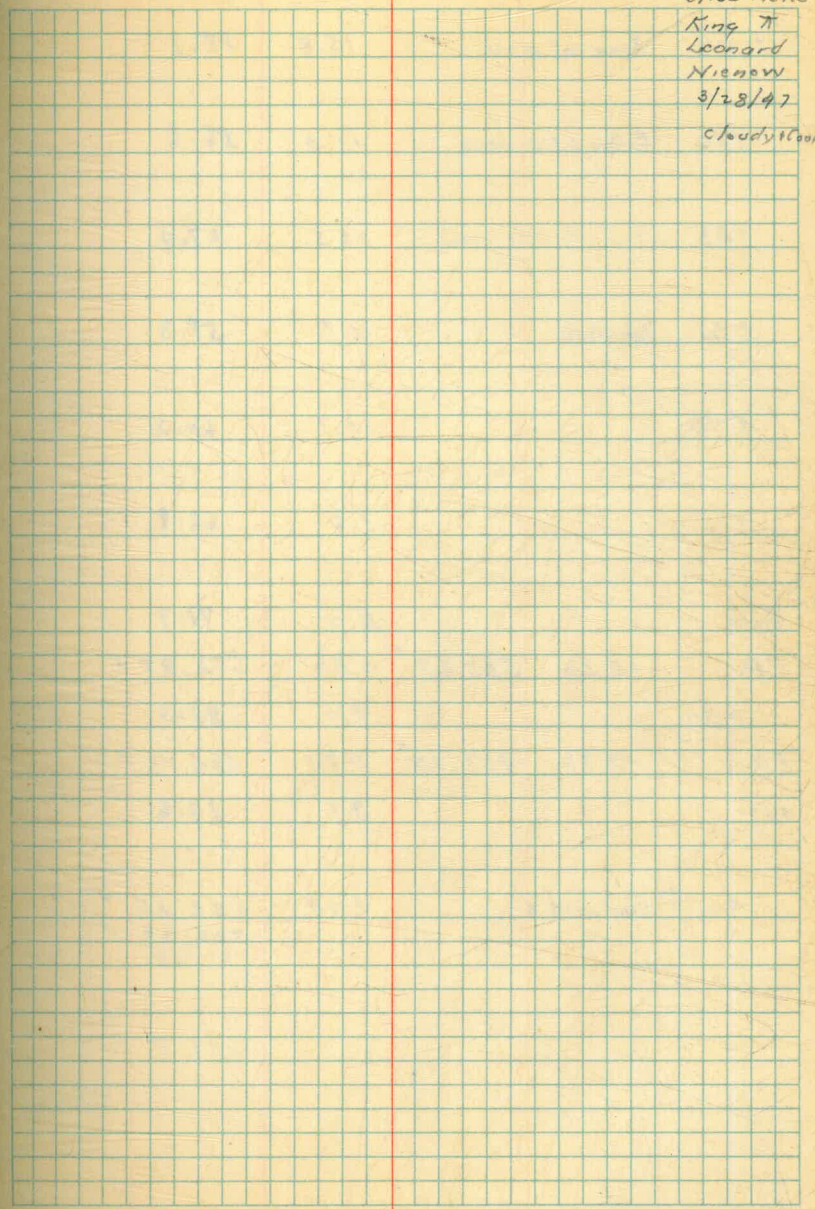
Bliss Notes

King T
Leonard McLean
Newcom R. 11
3/28/47
Cloudy & Cool

Profile Levels "B" Line. See Page 60 for Alignment

BM 0100	0.14	586.24	586.10	2 X 2 1106 4 2 7+35 = 0° ALINE See page 51
0 +38		6.9	79.34	
+50		11.1	75.1	
T.P.	0.79	573.85 ✓	12.88	573.36 ✓
+83 S Side wash		5.1	68.8	
1 φ wash		5.9	68.0	
+15 N Side wash		6.1	67.8	
+43		1.3	72.6	
+50		1.0	72.9	
2		0.0	73.9	
+36 c		4.3	69.6	
+50		8.3	65.6	
+70 Tooslope Mainwash		12.0	61.9	
3		13.4	60.5	

Bliss Notes
 King T
 Leonard
 Nieman
 3/28/47
 cloudy cool



X
57385 ✓

3 +16	Bank of Wash	15.8	58.1	
+20	Bottom S. Side wash	17.3	56.6	
+28	" N. Side wash	16.5	57.9	
+35	Toe slope	15.6	58.3	
+50		13.7	60.2	
+75		7.0	66.9	
4+0		2.0	71.9	
T.P.	12.30	585.27 ✓	0.88	572.97 ✓
+50		4.0	81.3	
T.P.	12.76	597.29 ✓	0.74	584.53 ✓
5+0		9.7	87.6	
+05 ³⁰	End of # 6	9.09	588.25 ✓	

588.29 ✓
0.04

Profile Levels "C" line Preliminary Road Survey

See Page 61 for alignment

Bliss Notes
Map of
Leonard Road
Niagara
3/27/47

BM	12.71	603.23		590.52
0+00			12.7	90.5
0+50			5.5	97.7
1+0			1.0	602.2
TP	9.22	611.09	1.36	601.87 ✓
+15			7.9	603.2
+56			6.3	604.8
+94			6.3	604.8
2+0			5.3	605.8
+50			5.2	605.9
+84			5.2	605.9
3+0			3.4	607.7
3+09 End			2.9	608.2
Set BM			2.58	608.51 ✓

1" pipe 2° N. line

Profile Levels "D" Line. See Page 62 for Alignment

BM	2.58	611.03	608.51
0+00		2.9	608.2
+08		2.9	608.2
+25		5.1	606.0
+50		5.1	606.0
+64		3.4	607.7
+86		4.7	606.4
+10		4.7	606.4
+10		3.7	607.4
+30		3.3	607.8
+47		5.3	605.8
+75		4.4	606.7
2		5.9	605.2
+14		7.1	604.0

67

1" Pipe 2" N. Transmission Line

Bliss Notes

Keep it
Leonard
Nienow
3/20/97
cloudy & cool

X
511.09 ✓

2+30 6.4 604.7

+50 7.3 603.8

+80 9.4 601.7

T.P. 1.27 599.56 ✓ 12.80 598.29 ✓

3+0 1.8 97.8

+35 Bottoms Draw 7.6 92.0

+50 6.0 93.6

4+0 4.2 95.4

+12 3.7 95.9

+40 5.8 93.8

+70 6.3 93.3

5+0 8.7 90.9

T.P. 2.14 589.00 ✓ 12.70 586.86 ✓

+50 3.6 85.4

+0

+81 Bottom + W. Side Wash 11.0 78.0

+91 " + E " " 10.6 78.4

68

↑
589.00 ✓

670			9.3	579.7
+38			5.8	83.2
+50			5.4	583.6 ✓
+61			4.5	584.5
T.P.	12.86	600.87 ✓	0.99	588.01 ✓
770			8.3	592.6
+50			0.9	600.0
T.P.	8.37	608.77 ✓	0.47	600.40 ✓
+57			7.3	601.47
870			3.8	604.97
+12 ³	End		3.3	605.5
T.P.	288	599.08 ✓	12.57	596.20 ✓
check L. #3			3.89	595.19 ✓

59

Not in Power Pole # 76944

Profile Levels Preliminary Road Line E

	3.89	599.08		595.19	2x2 406 L 43
BM					
0+00			3.9	595.2	
0+20			3.2	95.9	
0+50			4.1	95.0	
+70			4.2	94.9	
1+0			7.1	92.0	
+12			7.2	91.9	
+50			11.1	88.0	
TP	4.34	591.15	12.27	586.81	
2+0			5.6	85.6	
+10			5.6	85.6	
+27			7.3	83.9	
+50			6.8	84.4	
+80			7.6	83.6	
3+0			6.5	84.7	
3+24			7.5	583.5 ⁶⁵	

See page 63 for Alignment

Miss Nite

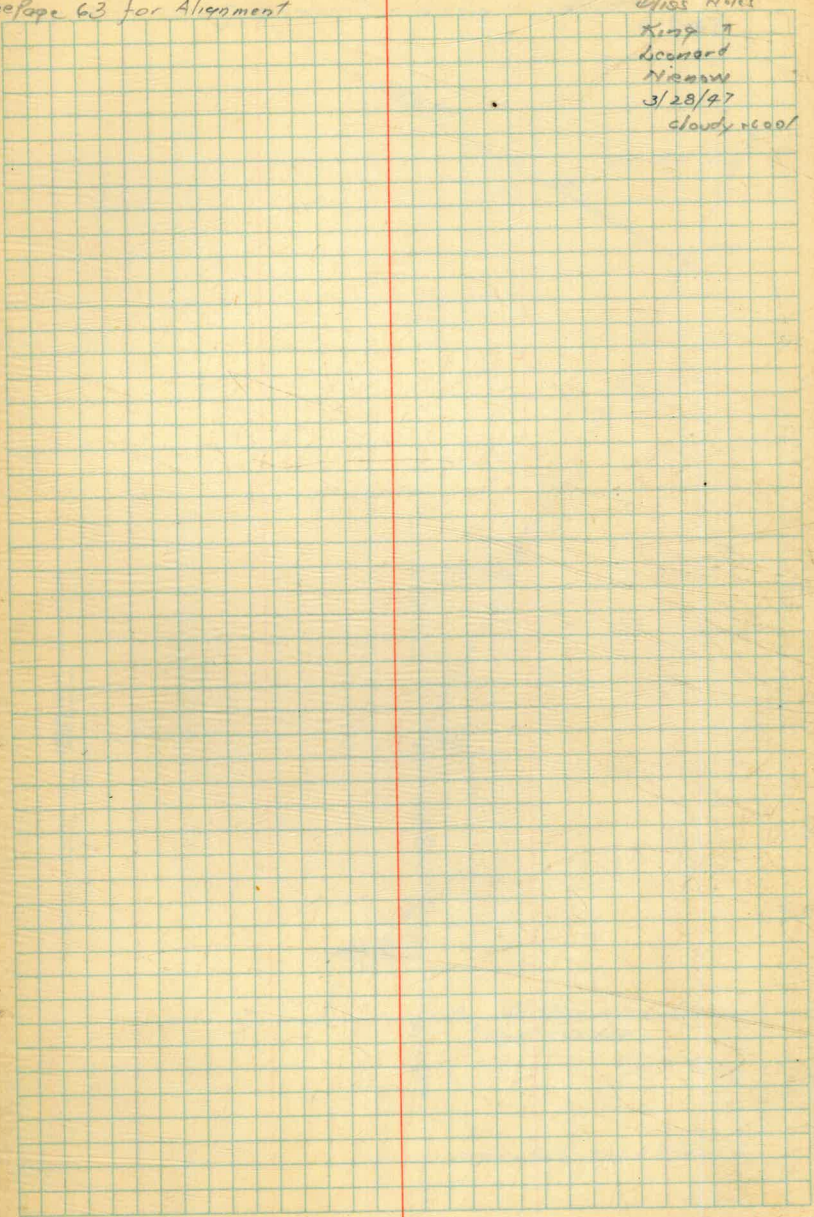
King T

Leonard

Nearby

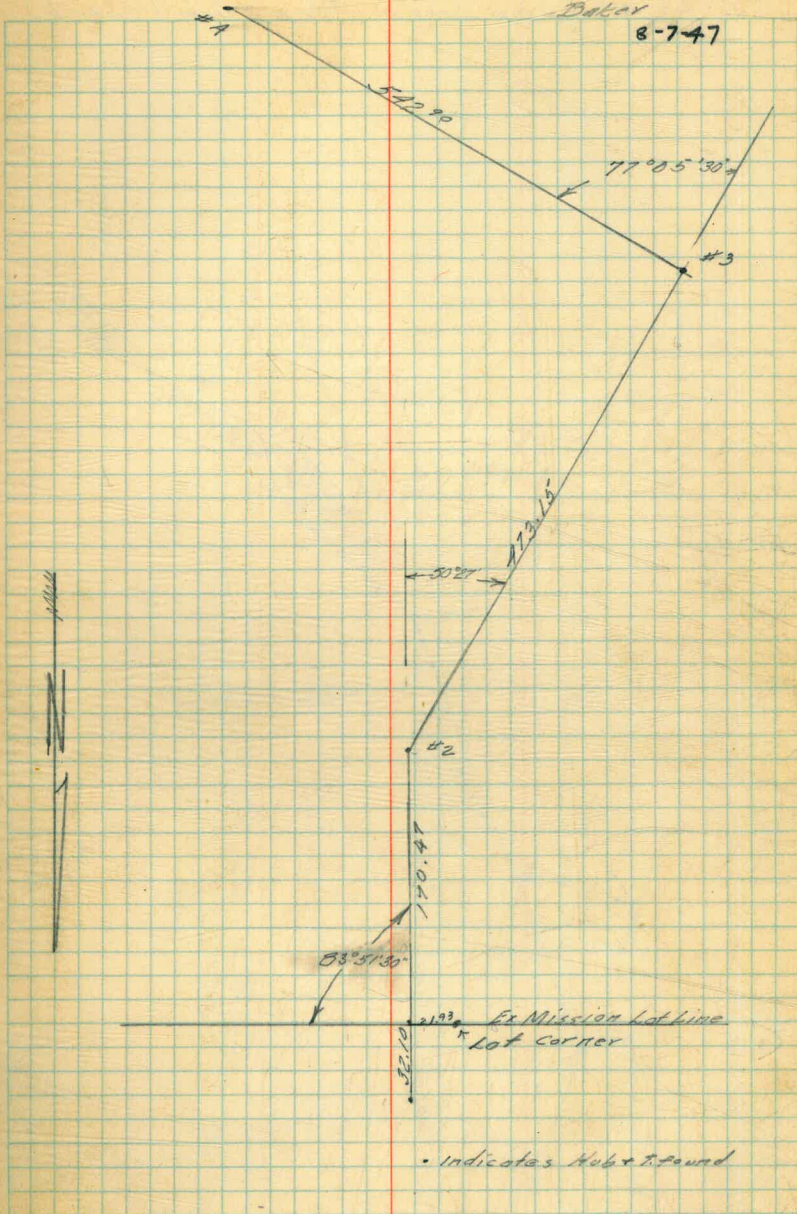
3/28/27

cloudy, cool

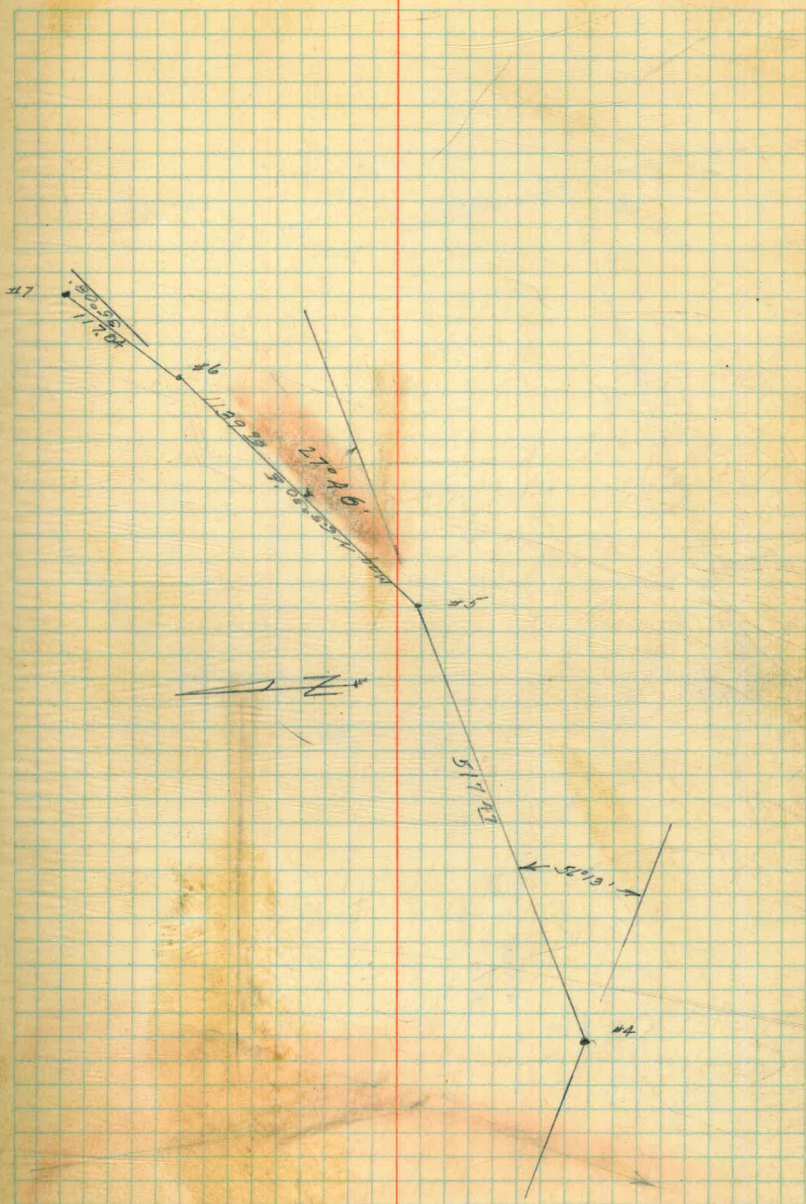


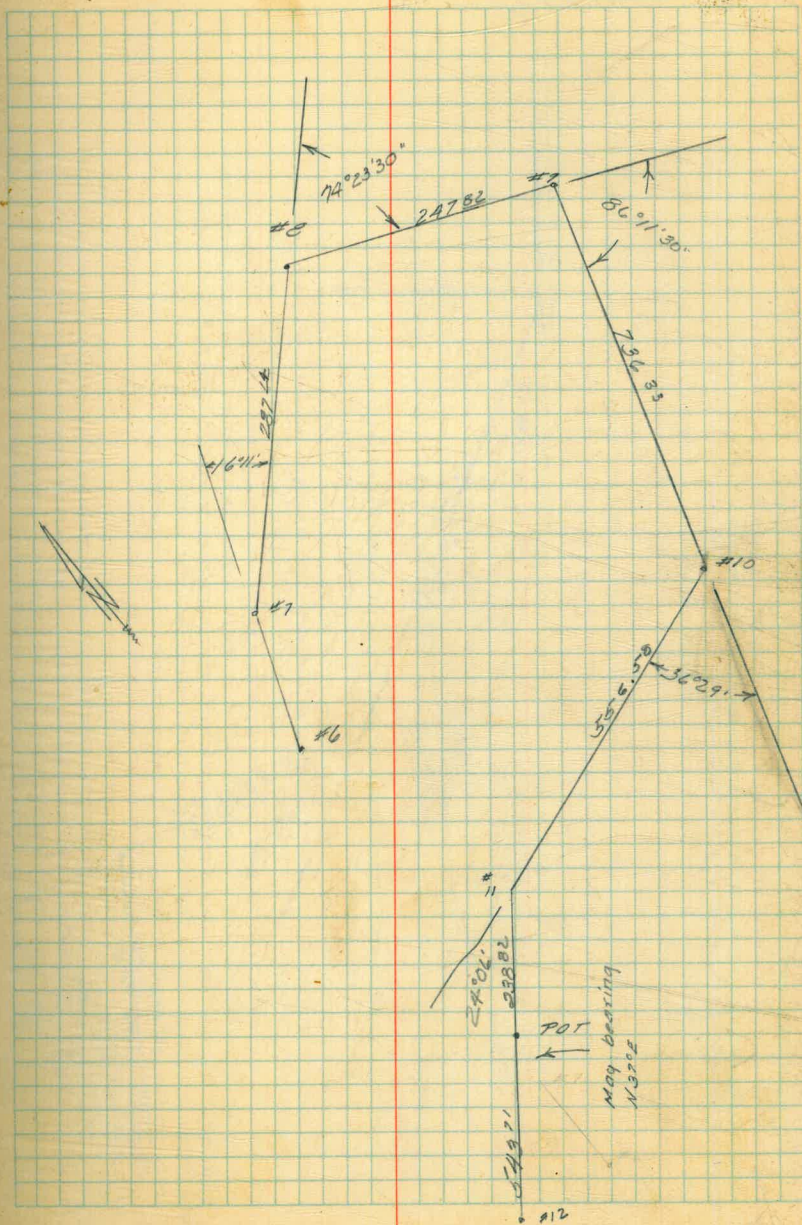
Murray Lake Property Line Check

8-7-47

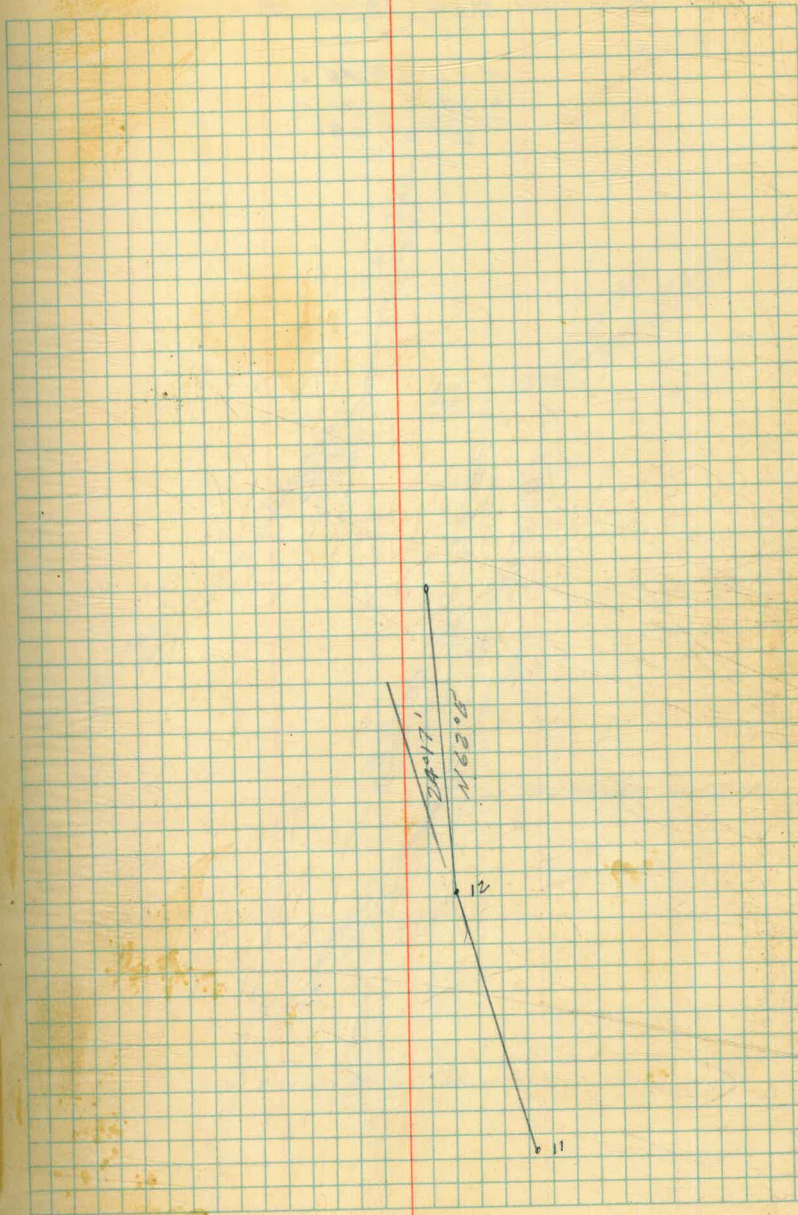
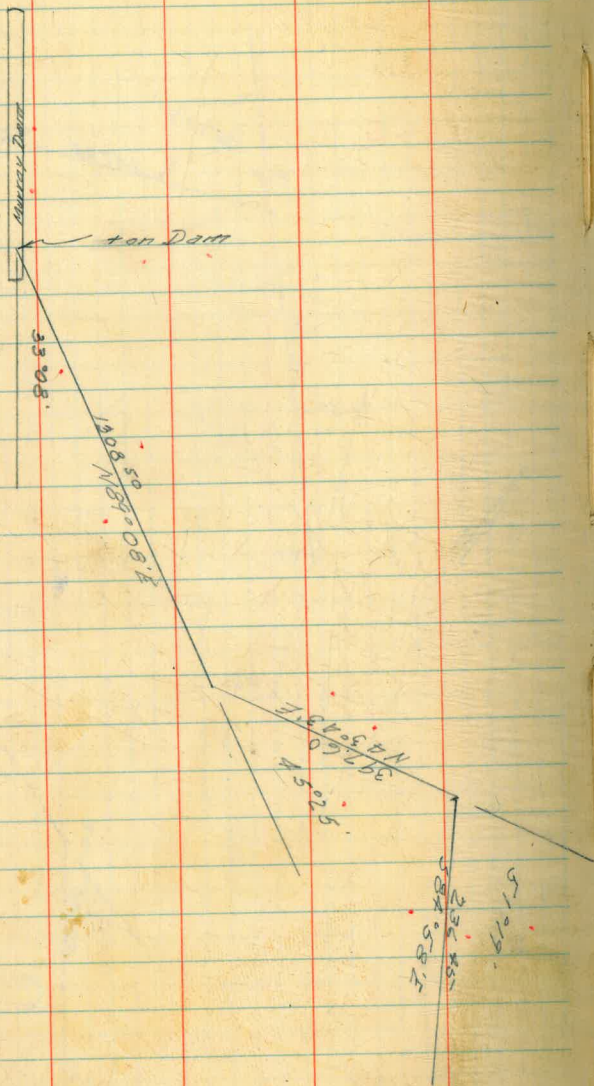


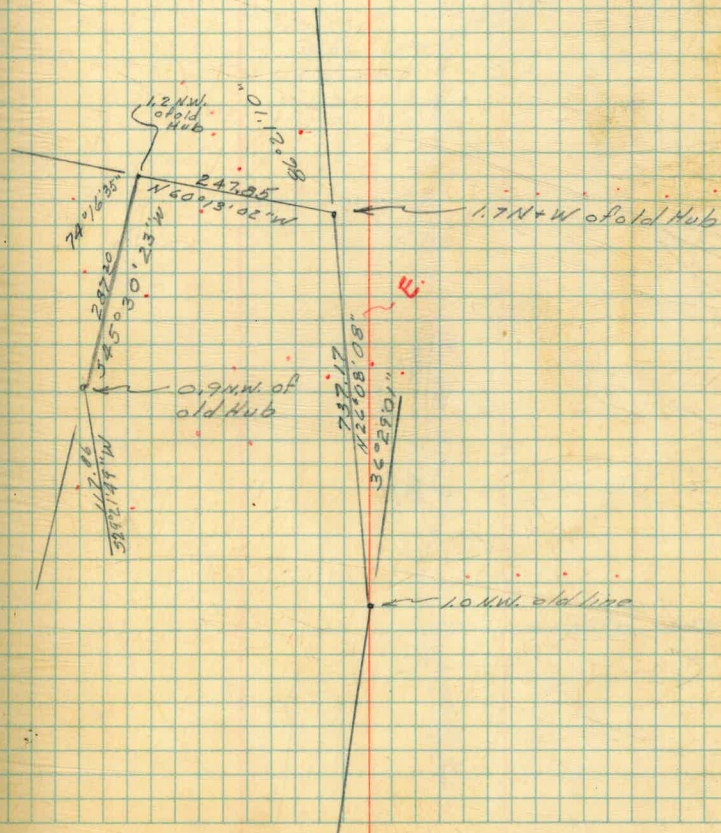
Murray Lake Prop line (check)

$$\begin{array}{r} 345 \\ 198 \overline{) 71} \\ \underline{343} \\ 70 \end{array}$$


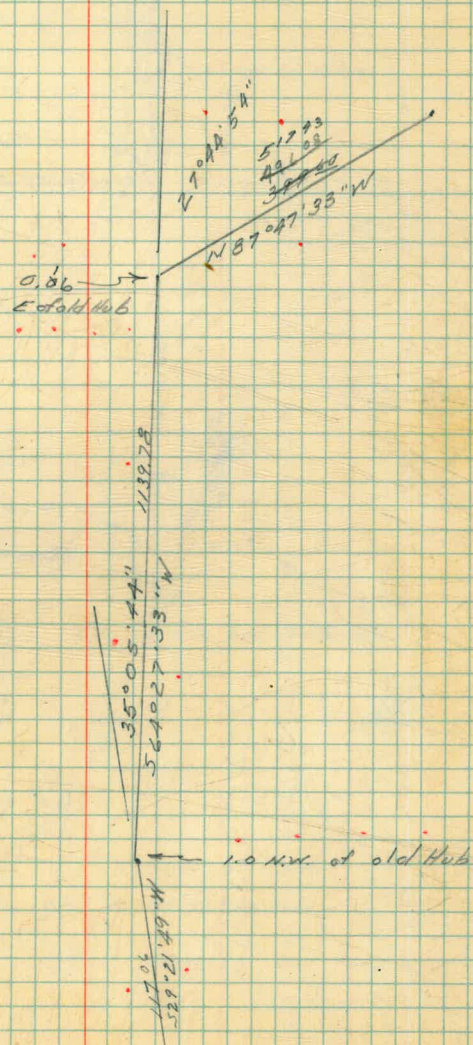


From Murray Dam To Edge of Property





Traverse

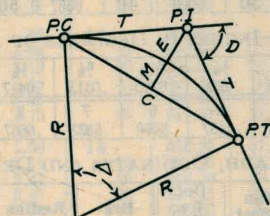


BM 566²³

Pt. 68 1.95' Lower 93+77

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin \frac{D}{2}} \quad (1) \quad \text{Degree of Curve} = D \text{ and } \sin \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \quad \text{Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R \left(1 - \cos \frac{\Delta}{2}\right) = R \text{vers} \frac{\Delta}{2} \quad (5) \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R \div \cos \frac{\Delta}{2} - R \quad (8) = R \text{exsec} \frac{\Delta}{2} \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin \frac{\Delta}{2} \quad (10) \quad \Delta = \text{Central Angle}$$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. — $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

S 38° E

N 42° 50' 30"

20 37

522.13 - 005

38°

69' 90 V
298+06 6.1

25804.57
33.3
25771.27



7.1
14.2

171
302



258+09 57

152
1266
1518

33.3

56388
25
538.88

61249
1418
59831

563.14
134

43-43
2
09 26

5669
133
5536

74-23-00

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558.09
14.2
538.9

538.9

546.6
538.9
7.7

77
18
9.5

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

403
897

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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