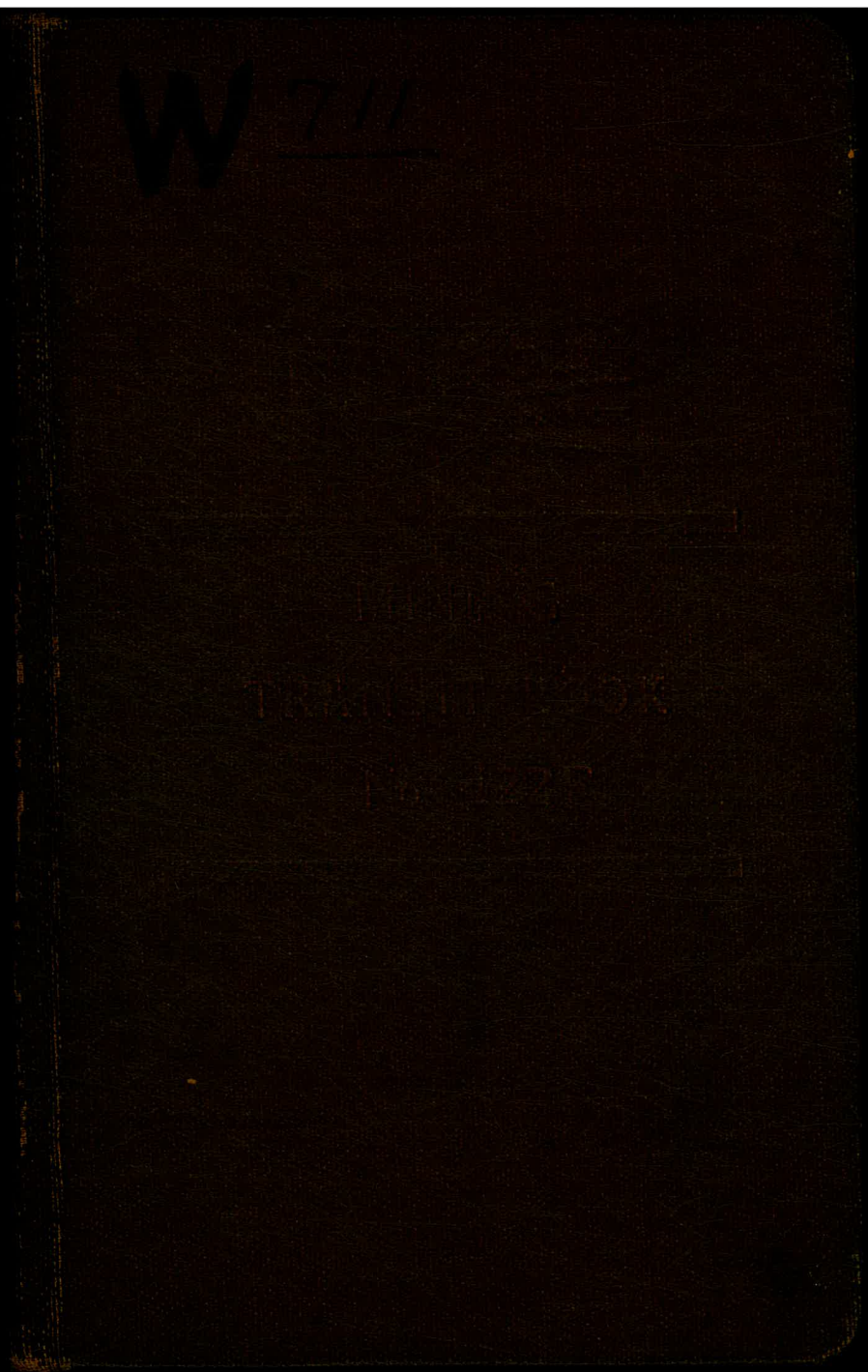


W 711

THE HISTORY OF THE

UNITED STATES OF AMERICA



# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6 + (20 - 16) \* 2 or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1 1/2 see inside of back cover.

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Please Return to  
City of San Diego Water Dept.  
Room 268 Civic Center  
Telephone Main 5161.

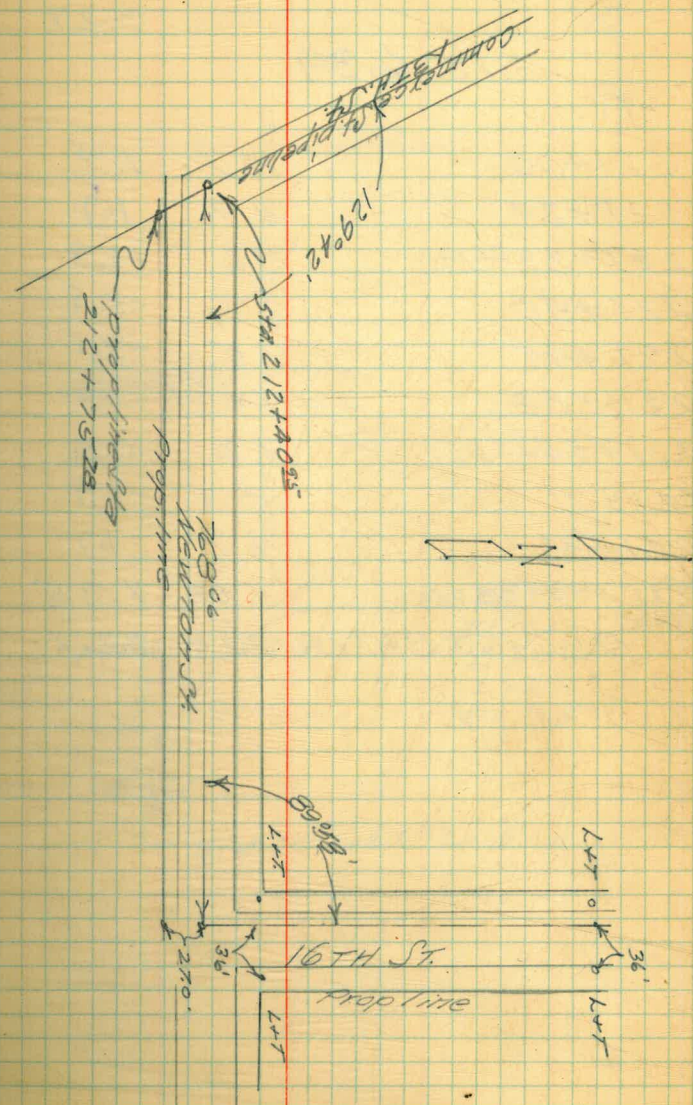
This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Included to page	Date	By	Notes Plotted or Revised	Map page	date	By
1-4/2	4/23	msd				
3-16	5/27	msd				
17-27	5/27	msd				
28	6/25	MPV				
34	9/12	MPV				
47	11/19/50	msd				
48-51	4/26/50	msd				
52-53	4/26/50	MPV				

	P
COMMERCIAL ST. P.L. (Ties to M.H. Tide) New End Alignment	19-2
Detail of 40th St 16" Thorn St 12" 8" Pipelines	3-16
Profiles of 40th St 16" Thorn St 12" 8" Pipelines	17-27
X Sections Commercial St.	28 ✓
Realignment 40th + Thorn Pipeline	29-32
Reprofile 40th + Thorn Pipeline	33-34
Construction stakes Tulip St Juniper & Sycamore 8" water main (40th + Thorn St. Pipeline for Condy.)	35-36 37-47
40th + Thorn St final profiles after Backfill	48-51
RELOCATION 40th St Pipeline 40th & Landis Street	52-53

Commercial St. Pipeline,  
Tie To Mean High Tide



2

## Commercial St. Pipeline

## End Profiles

U.S.C.+G.S. B.M. # S73A

3.27

3.12 6.39

221+00	4.7	1.7
221+29	4.7	1.7
221+33 <sup>24</sup> BC	8.2	-1.8
221+40	9.9	-3.5
221+45	9.5	-3.1
221+52	7.3	-0.9
221+60 <sup>29</sup> EC	9.2	-2.8
221+71	10.3	-3.9
221+83	4.7	1.7
221+97 <sup>26</sup> END	5.04	1.35
U.S.C.+G.S. B.M. S73A	3.12	3.27

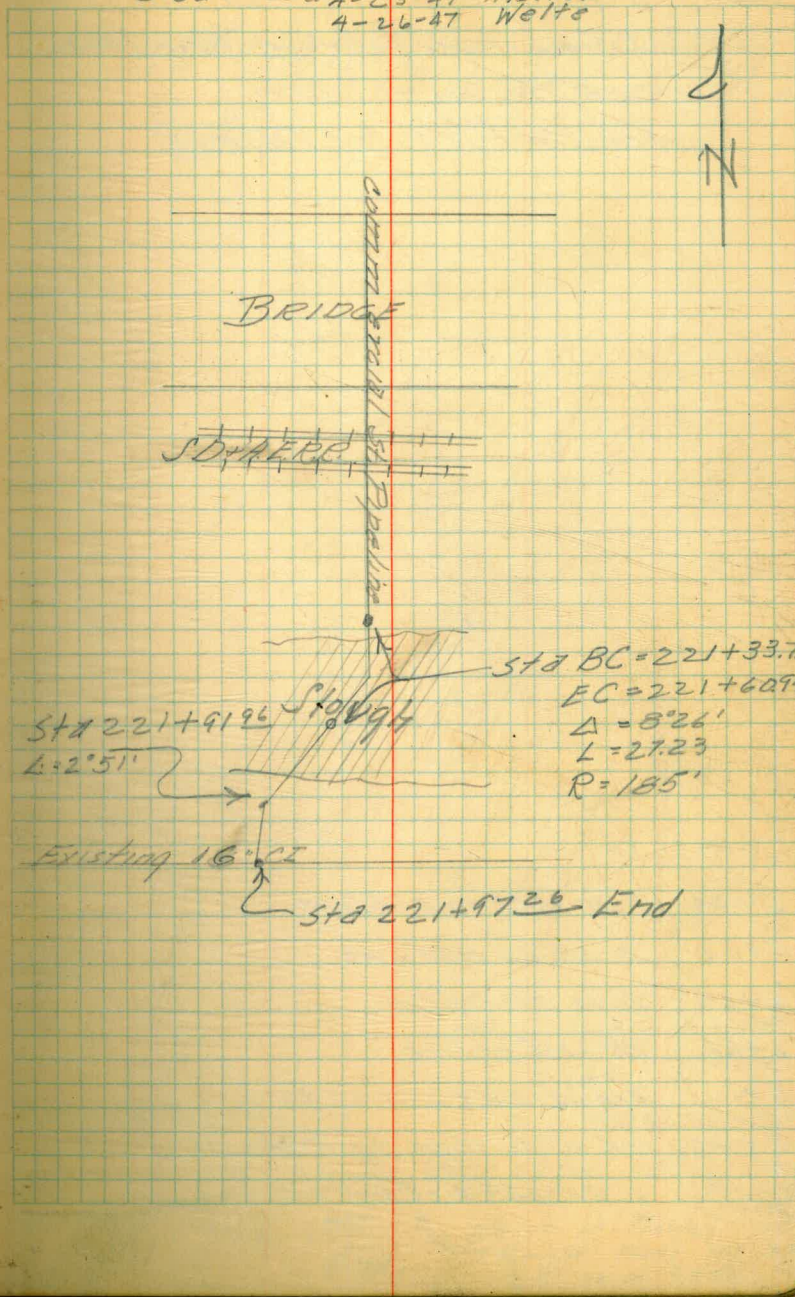
Rainey

2

clear-cold 4-22-47 King

1-23-47 Niellow

4-26-47 Welte



3 cloudy Cool

May 21, 1947  
22, 1947

Rainy  
King  
Nichow  
Wells

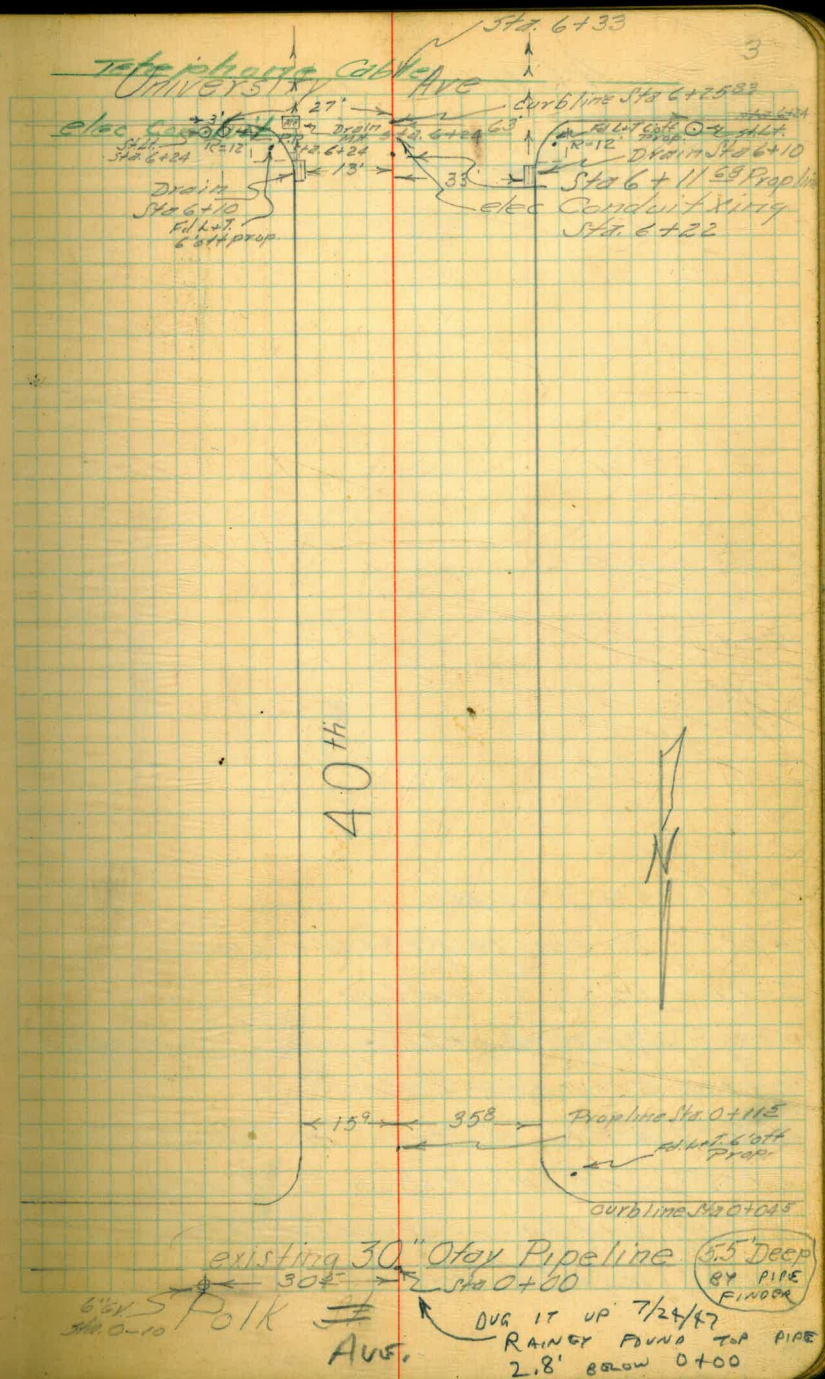
Sta. 40th St. Pipeline 16"

Line Located from Prop Lines

Irregardless of curb

For Profiles See Page 17

- 6+24 Drain NW 13' E of Line
- 6+24 St. Lt. 63' West Line
- 6+24 St. Lt. 30' E of Line
- 6+24 PP 27' E of Line
- 6+10 Drains 13' E + 33' W of Line
- 0+00 Int. W/ Existing 30" Otag Line
- 0-10 5" 6" 30.5' E of Line

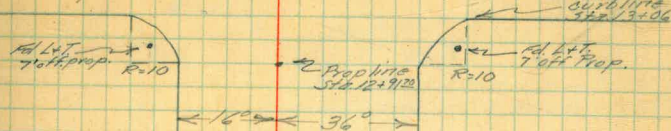


6" 5" Polk  
 0-10  
 AUG. 7/24/47  
 RAINY FOUND TOP PIPE  
 2.8' BELOW 0+00

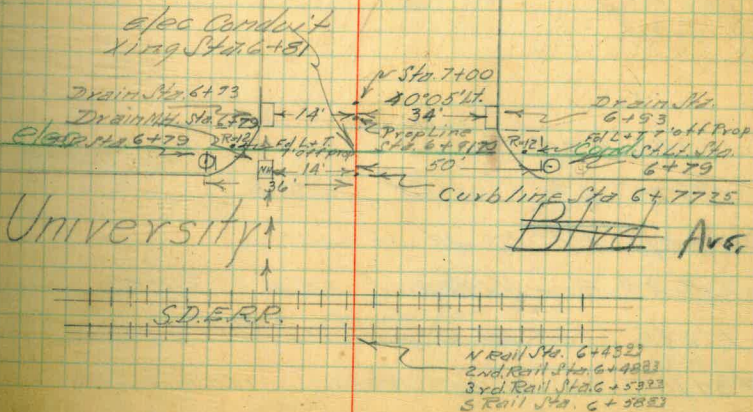
1  
Sta. 40th St. Pipeline 16"

- 7+00 Sta. 0°05' Lt
- 6+93 Drains 14' E + 34' W of line
- 6+79 St. Lt. 50' W of line
- 6+79 R.P. 36' E of line
- 6+79 Drain MH. 14' E of line
- 6+58<sup>83</sup> S Rail of Street Car Tracks
- 6+53<sup>93</sup> 3rd. Rail of Street Car Tracks
- 6+48<sup>93</sup> 2nd Rail of Street Car Tracks
- 6+43<sup>23</sup> N Rail of Street Car Tracks

4  
Wightman St.

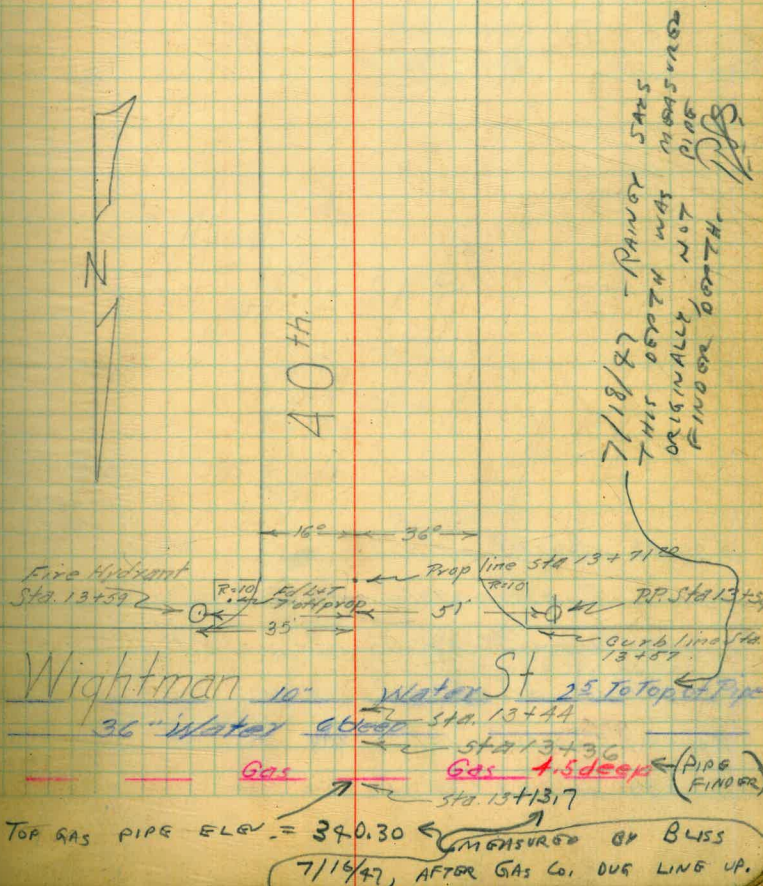
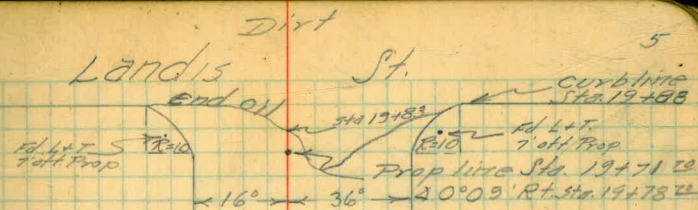


40th



5  
Sta. 40th St. Pipeline 16"

- 19+83 End Oil
- 19+78<sup>00</sup> 2 Pt. 0°09' RT.
- 13+59 P.P. 51' W of Line
- 13+59 Fire Hydrant 35' E of Line
- 13+44 Int. w/ 10" Water Main 25' to top of pipe
- 13+13 Int. w/ Gas Main (unknown size)

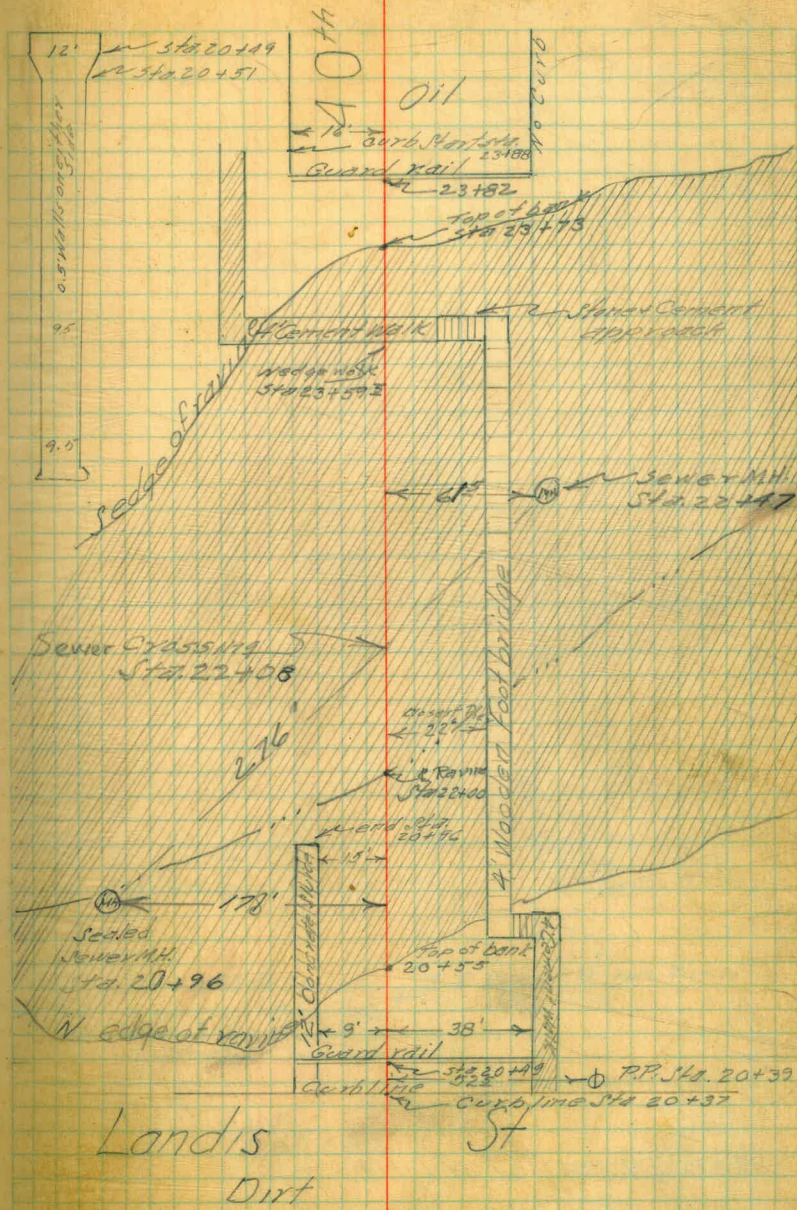




6  
Sta.

40th St. Pipeline  
16"

- 23+83 Start of oil
- 23+82 Guard rail
- 23+59<sup>5</sup> N edge of concrete walk 4' wide
- 22+00 bottom of ravine
- 20+49 Guard rail
- 20+39 P.P. 52<sup>5</sup> W of line

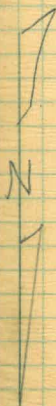
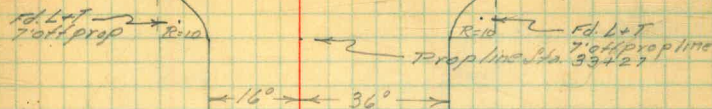


Landis  
Dirt

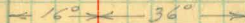
7  
Sta.

40th St. 16" Pipeline

Myrtle curbline Sta 33+41 Ave



40th



Dwight

St

10" Water 1.5' Deep - BY PIPE FINDER  
 RAJNER MEASURED DEPTH 7/18/87  
 2.6' BELOW 27+00 TOP PIPE  
 1" H.P. GAS 4.0' Deep  
 Sta. 26+98  
 Sta. 26+77



No Curb No Walk

No Curb  
No Walk

27+16 P.P. 53' W of Line  
 27+16 P.P. 69' E of Line

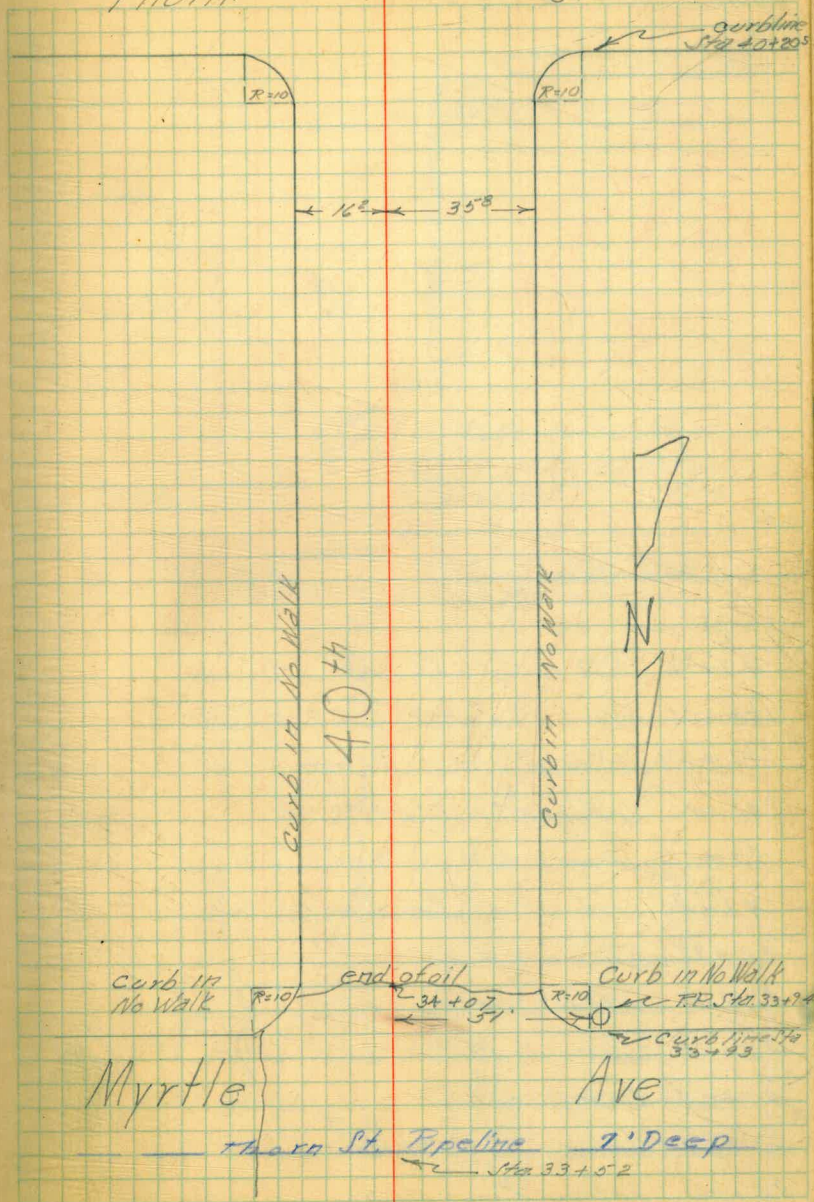
Sta.

40th St. 16" Pipeline

34+07 End of oil  
 33+94 R.P. 51' W of LITC  
 33+52 Int w/ Water Main

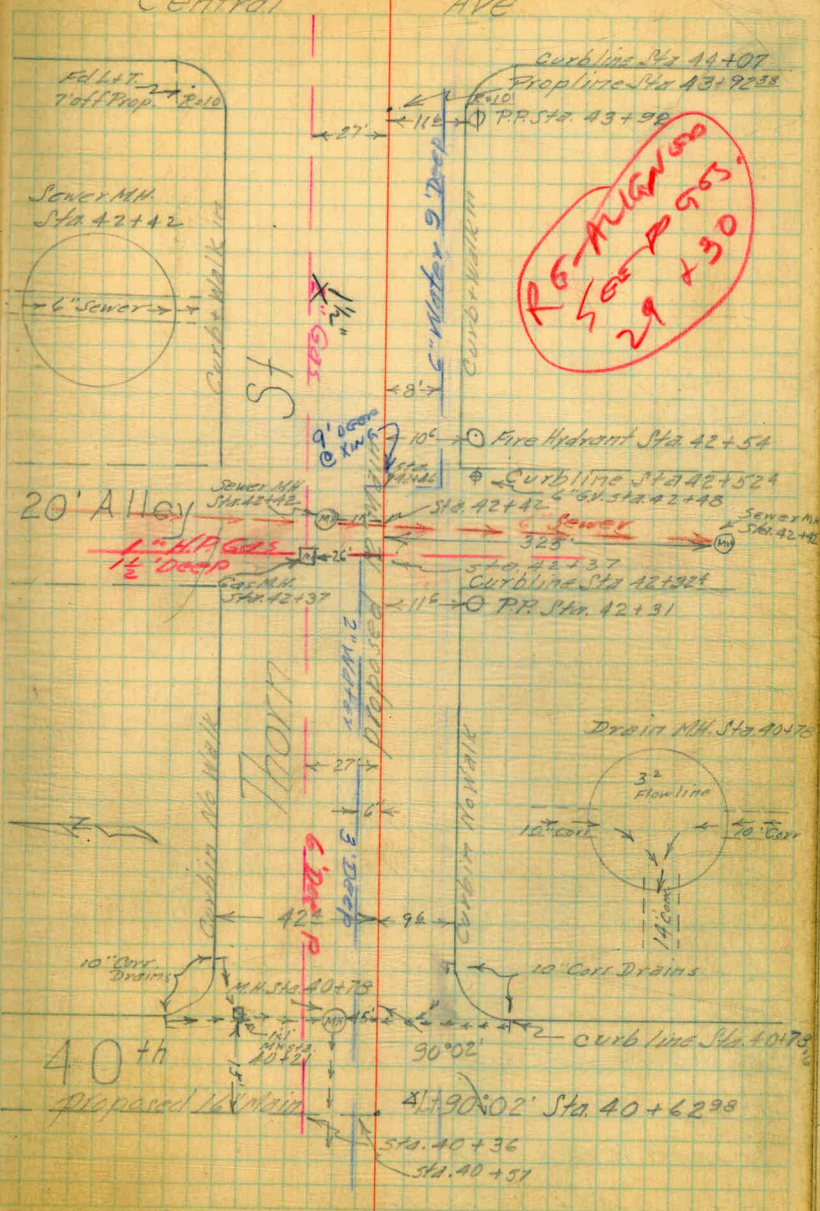
Thorn

St



Thorn St 12" Pipeline

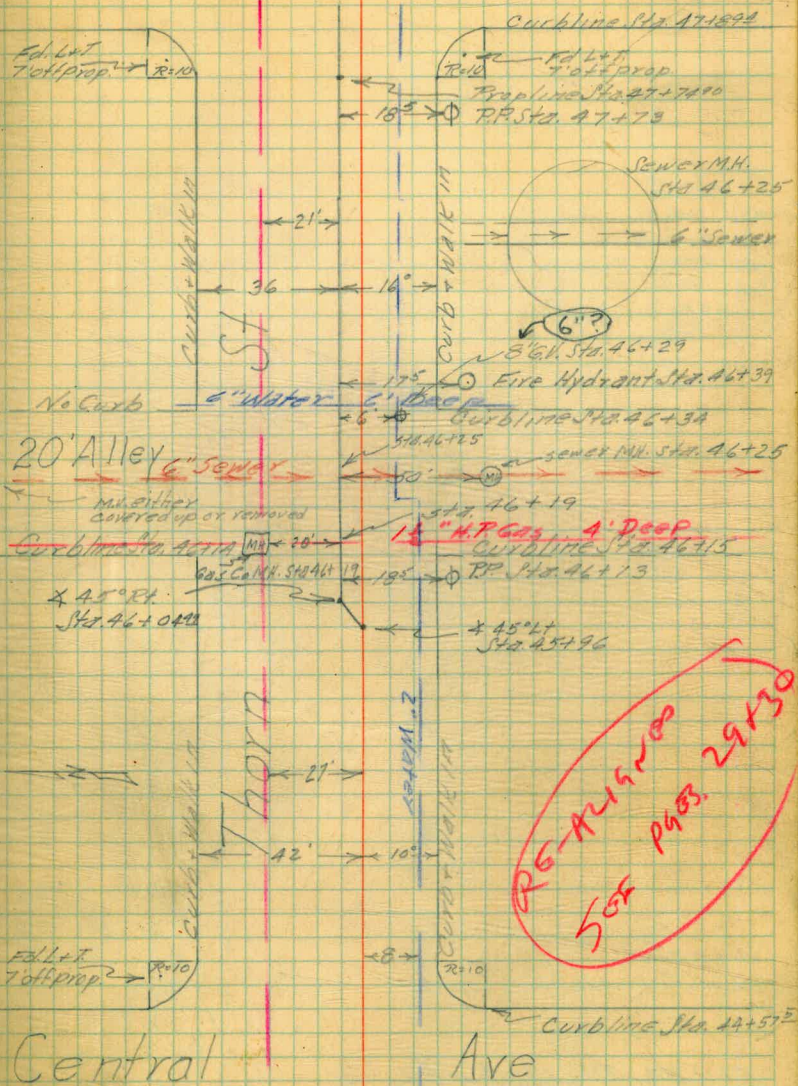
- 43+92 P.P. 11' S of Line
- 42+54 Fire Hydrant 10' S of Line
- 42+48 6" G.V. 10' S of Line
- 42+46 Int. w/ 6" Water Main
- 42+42 Sewer M.H. 15' N of Line
- 42+40 Int. w/ 6" Sewer
- 42+37 Gas Co. M.H. 26' N of Line
- 42+31 P.P. 11' S of Line
- 40+78 Drain M.H. 15' N of Line
- 40+62<sup>98</sup> & 90° 02' Lt.
- 40+57 Int. w/ 2" Water Main
- 40+36 Int. w/ 1 1/2" Gas Main
- 40+21 1' x 1' Square Drain M.H. 15' E of Line



For West Line See page 15

Sta. Thorn St. 12" Pipeline

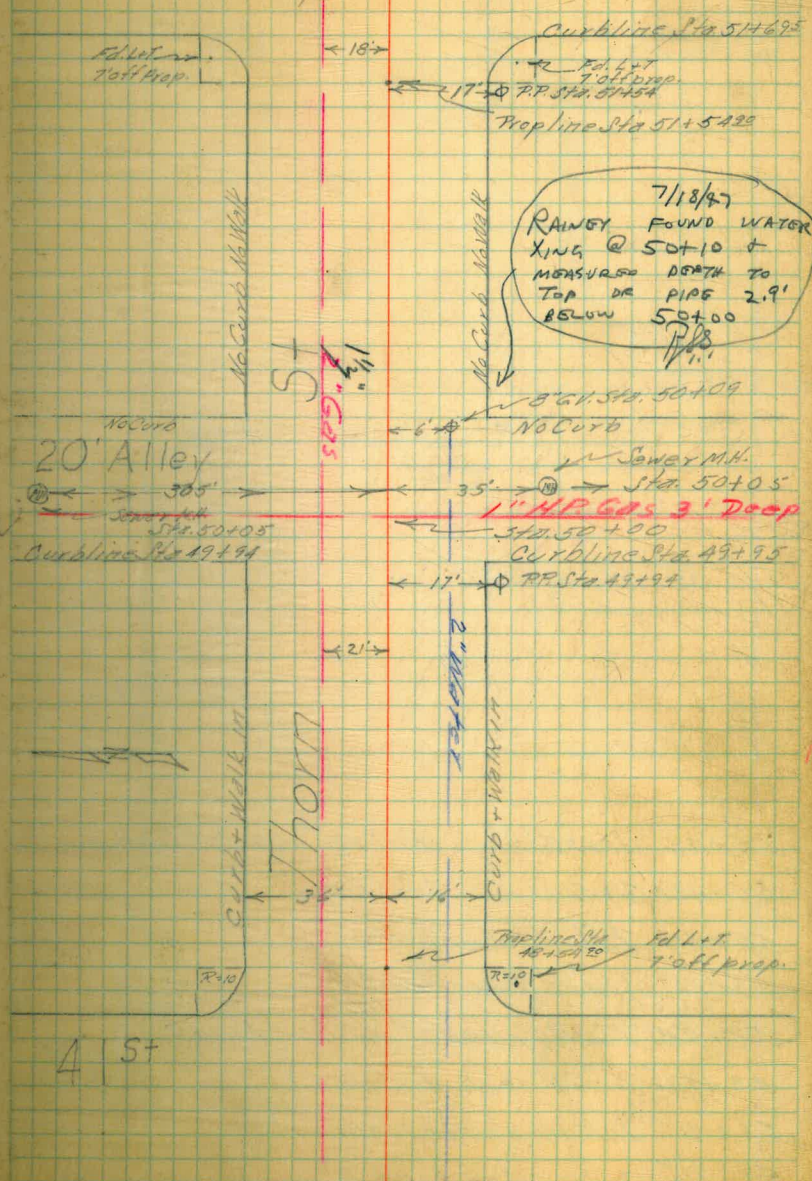
41 St



- 47+73 P.P. 18.5' S of Line
- 46+39 Fire Hydrant 17.5' S of Line
- 46+29 <sup>(2")</sup> 8" G.V. 6" S of Line
- 46+25 Sewer M.H. 50' S of Line
- 46+25 Int. W/ 6" Sewer
- 46+19 Gas Co. M.H. 20' N of Line
- 46+13 P.P. 18.5' S of Line
- 46+04.4 4 P.P. 45° 00' RT.
- 45+96 4 P.P. 45° 00' Lt.

11  
Sta. Thorn St 12" Pipeline

11  
Marlborough Ave

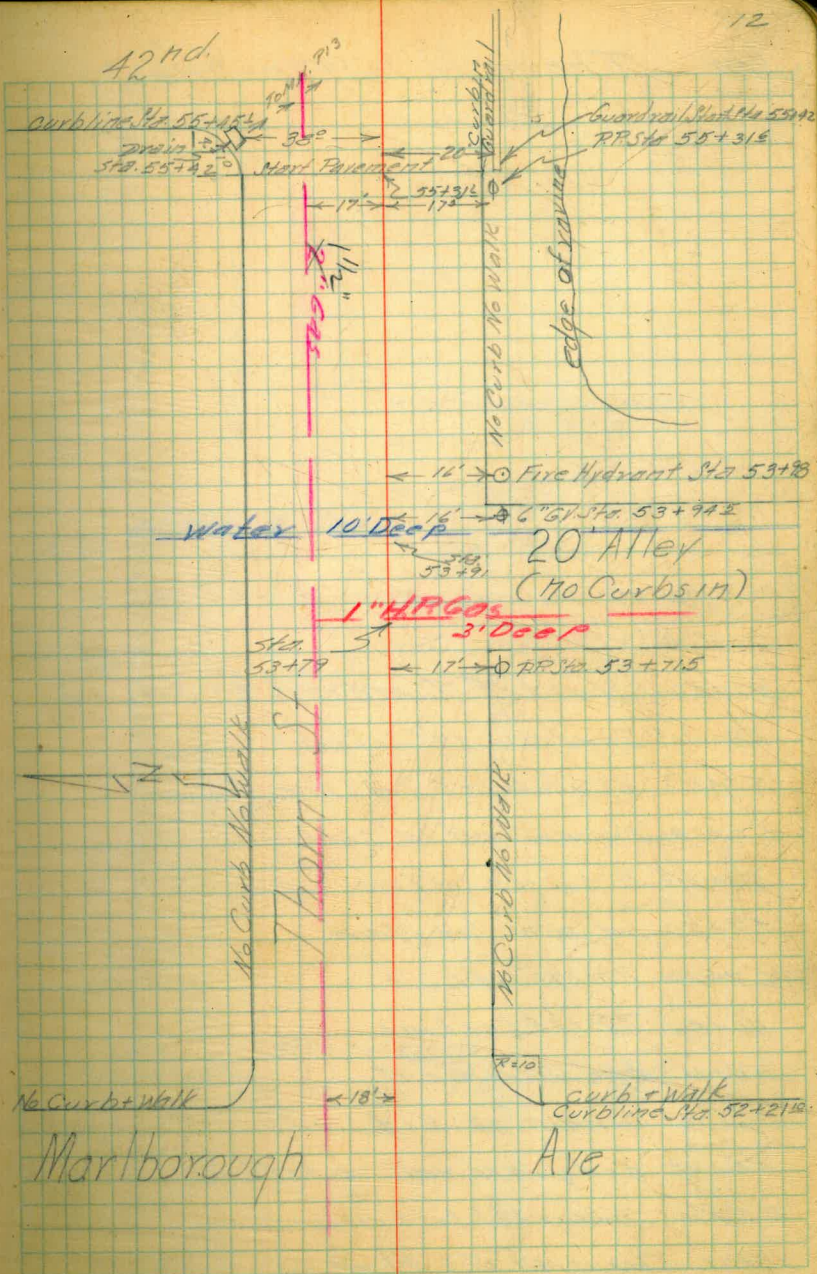


51+54 PP 17' Soft Line  
 50+09 8" G.I. 6' Soft Line  
 49+94 PP 17' Soft Line

4 St

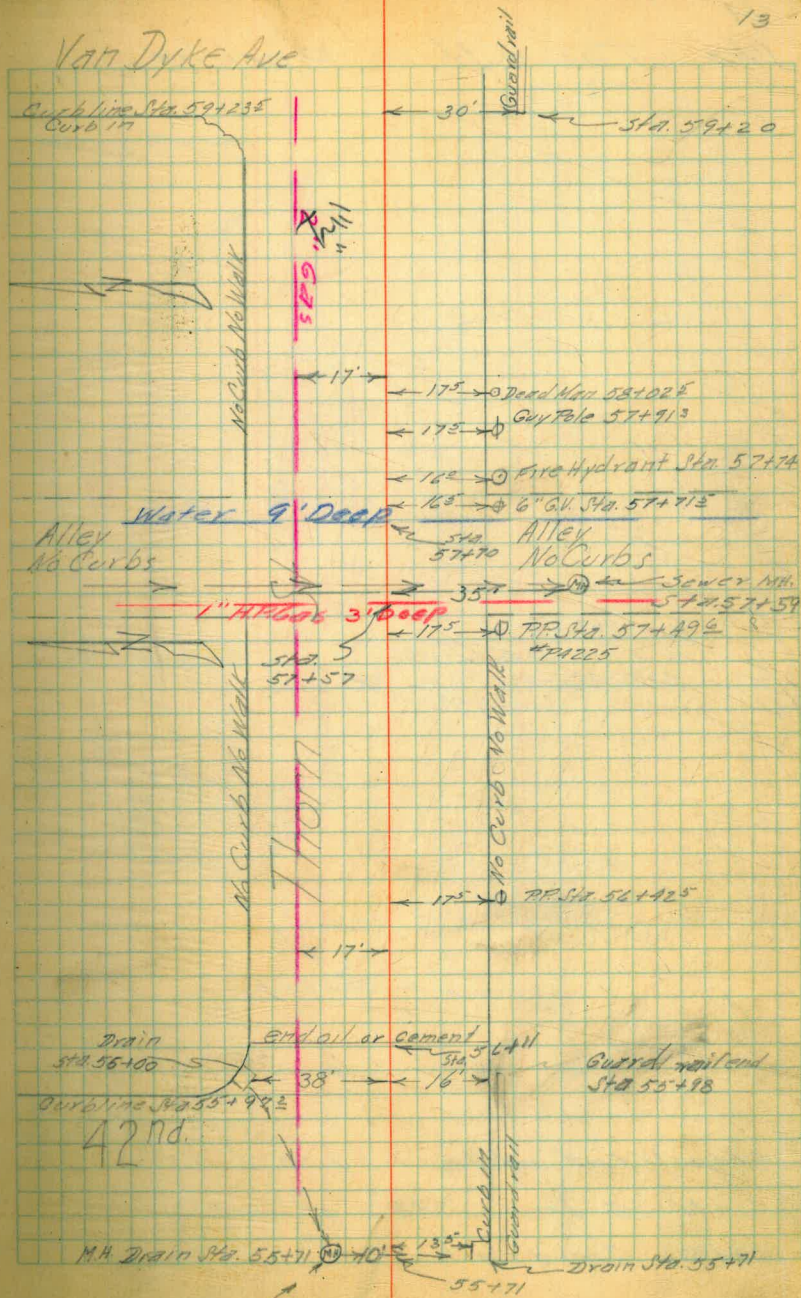
No. Thorn St. 12" Pipeline

- 55+42 Start of guardrail 20' S of line
- 55+42 Drain 38' N of line
- 55+316 P.P. 17' S of line
- 55+310 Start pavement
- 53+98 Fire Hydrant 16' S of line
- 53+94E 6" G.V. 16' S of line
- 53+91 Int. w/ Water Main
- 53+71E P.P. 17' S of line



Sta. Thorn St 12" Pipeline

- 59+20 Start of Guardrail 30' Soft Line  
 58+02<sup>s</sup> Dead Man 17<sup>s</sup> Soft Line  
 57+91<sup>3</sup> Guy Pole 17<sup>s</sup> Soft Line  
 57+74 Fire Hydrant 16<sup>s</sup> Soft Line  
 57+71<sup>5</sup> 6" G.V. 16<sup>s</sup> Soft Line  
 57+70 Int. w/ Water Main  
 57+49<sup>6</sup> R.P. 17<sup>s</sup> Soft Line  
 56+42<sup>5</sup> R.P. 17<sup>s</sup> Soft Line  
 56+11 End Pavement  
 56+00 Drain 38' Not Line  
 55+98 End guard rail 20' Soft Line  
 55+71 Drain 13<sup>s</sup> Soft Line  
 55+71 Drain M.H. 10' N of Line

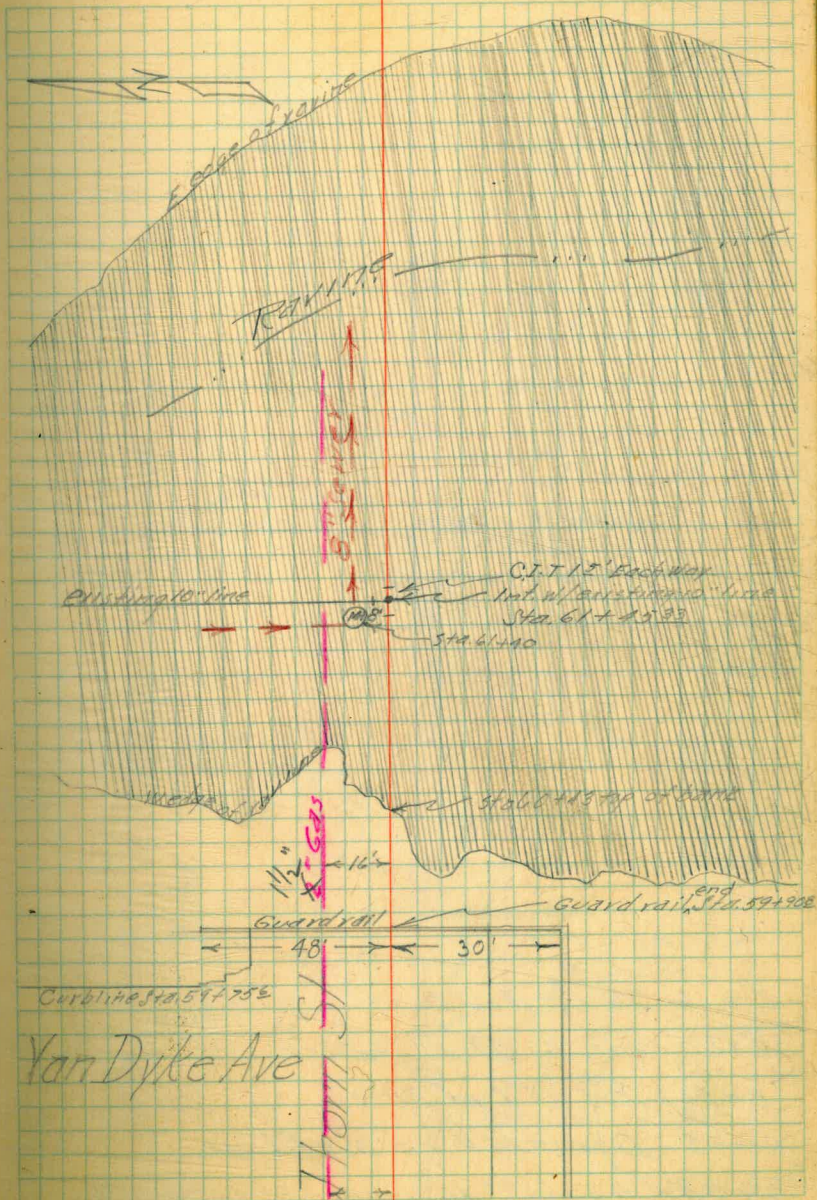




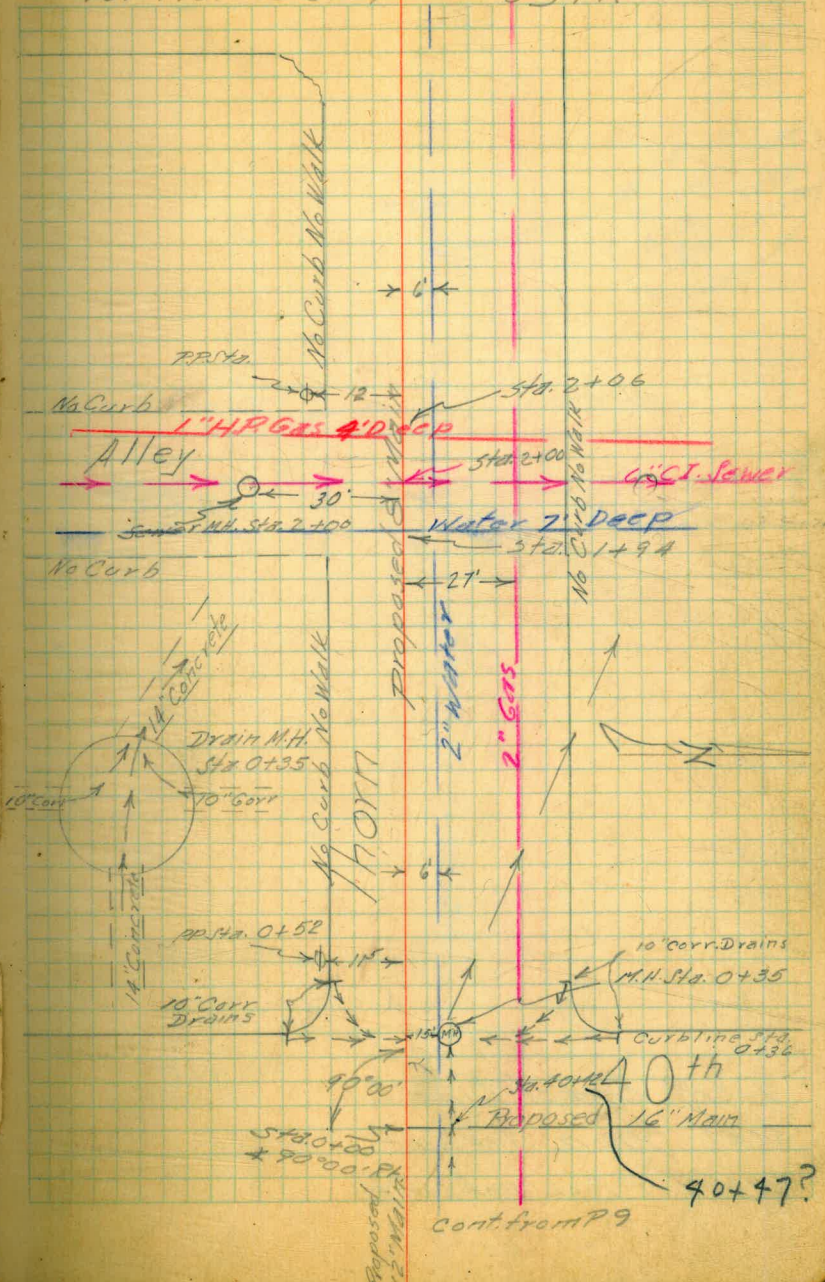
Sta. Thorn St. 12" Pipeline

61+45<sup>33</sup> Int. w/ existing 10" Line

61+40 8" Sewer M.H. 'N' of Line

59+90<sup>8</sup> Guardrail

- 2+12 RR 12' S of Line
- 2+00 Int. w/ CI. 6" Sewer
- 0+52 RR 11' S of Line
- 0+35 Drain M.H. 15' N of Line
- 0+00 = 40+62.98 16" Line 4th 90°00' RT



40+47?  
Cont. from P 9

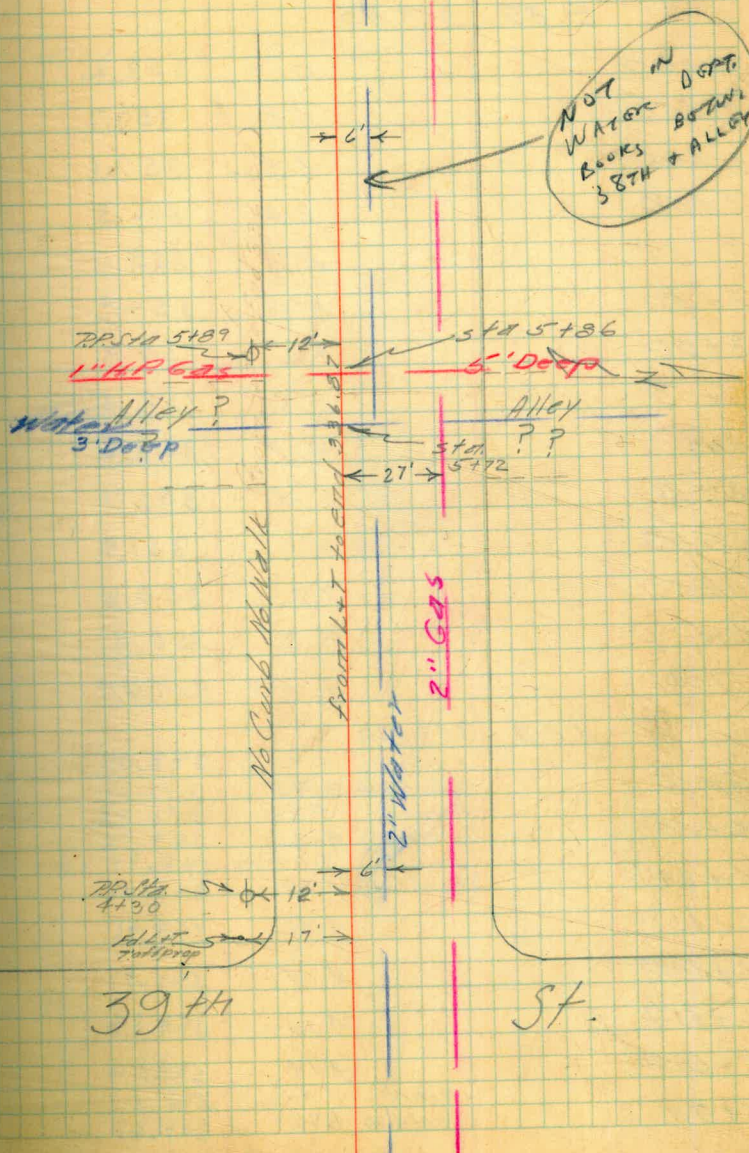
16  
Sta.

Thorn St 8" Pipeline

7+60<sup>34</sup> End of Line  
5+87 P.P. 12' Soft Line  
4+30 P.P. 12' Soft Line

38th St

16  
End Sta. 7+60<sup>34</sup>



39th

St.

Sta	±	H.I.	=	Elev.
B.M. NW. Cor. Urr. + 10th				349.56
	8.89	358.45		
0+00			0.3	358.2
0+50			0.8	357.7
1+00			1.4	357.1
1+50			2.2	356.3
2+00			2.9	355.6
2+50			3.6	354.9
3+00			4.2	354.3
3+50			5.0	353.5
4+00			5.7	352.8
4+50			6.4	352.1
5+00			7.1	351.4
5+50			7.7	350.8
6+00			8.2	350.3
T.P.#1			8.50	349.95
	4.03	353.98		
6+10		Invert 4.96		349.02
		Top of Gate 3.95		350.03
6+10		Invert 5.23		348.75
		Top of Gate 4.28		349.70
6+24		Invert 5.09		348.89
		Top of Gate 4.04		349.94
6+43 <sup>93</sup>			4.02	349.96
6+48 <sup>83</sup>			4.01	349.97
6+53 <sup>22</sup>			4.14	349.84
6+58 <sup>83</sup>			4.14	349.84
		Invert 6.45		348.53
6+79		Top of Gate 4.30		349.68

17

5/27/47

REDUCE

NOTES

Int. w/ existing 30" Otap line

- Drain 13' E of Line
- Drain 33' W of Line
- Drain M.H. 13' E of Line
- N. Rail
- 2nd Rail
- 3rd Rail
- S. Rail
- Drain M.H. 13' E of Line

## Profile A044 St. Pipeline

	+	H.I.	-	ELEV.
		353.98		
		Invert	5.40	348.58
6+93		Top of Gate	4.40	349.58
		Invert	5.97	348.01
6+93		Top of Gate	4.92	349.06
7+00			4.4	349.6
7+50			5.1	348.9
8+00			5.6	348.4
8+50			6.1	347.9
9+00			6.5	347.5
9+50			7.0	347.0
10+00			7.6	346.4
10+50			8.2	345.8
TP#2			8.17	345.81
	1.44	347.25		
11+00			2.1	345.2
11+50			2.8	344.5
12+00			3.5	343.8
12+50			4.2	343.1
13+00			4.7	342.6
13+50			5.0	342.3
14+00			5.1	342.2
14+50			5.5	341.8
15+00			5.8	341.5
15+50			6.1	341.2
16+00			6.5	340.8
16+50			7.0	340.3

P.S.

5/27/47

NOTES REDUCED

Drain 10' Foot Line

Drain 34' Wat Line

19 Profile 40th St. Pipeline

Sta	+	H.I.	-	ELEV.
		347.25		
17+00			8.0	339.3
17+50			9.5	337.8
T.P. #3			9.98	337.27
	0.59	337.86		
18+00			1.7	336.2
18+50			3.4	334.5
19+00			5.0	332.9
19+50			6.6	331.3
19+83			7.6	330.3
20+00			7.9	330.0
20+37			9.0	328.9
20+37±			8.34	329.52
20+50			7.9	330.0
20+55			7.9	330.0
20+57±			9.5	328.4
T.P. #4			12.97	324.89
	0.30	325.19		
20+77			8.4	316.8 312.92
T.P. #5			12.27	312.82
	1.14	314.06		
21+00			8.3	305.8
21+07			10.9	303.2
21+27			15.1	299.0
T.P. #6			12.29	301.77
	2.61	304.38		

P.S.  
 5/28/87  
 REDUCED  
 NOTES

19  
 NOTES BY RAINY 7/15/47  
 40th ST. PIPE LINE  
 282.7 22+50

281.7 22+00

281.7  
 +11.1  
 H.I. 292.8  
 - 0.88

Mantle Elev. 291.92  
 Left of line +12.16  
~~299.76~~

281.7  
 +7.05

H.I. 304.08  
 - 1.10

H.I. 288.75  
 - 7.97  
 RIM 280.78 RITT  
 INV. 273.0 INV.

302.98  
 - 292.5

COPY  
 OF  
 LINE

61.5' RT.  
 22+47

8'58" ↓  
 M.H. 178' Lt.  
 of 20+96

Sewer M.H. 178 Lt. of 20+96 Inv. 292.5

ENTER IN  
 FIG. 711 p. 6. 19

Sta	+	H.F.	-	ELEV.
		347.25		
17+00			8.0	339.3
17+50			9.5	337.8
T.P.#3			9.98	337.27
	0.59	337.86		
18+00			1.7	336.2
18+50			3.4	334.5
19+00			5.0	332.9
19+50			6.6	331.3
19+83			7.6	330.3
20+00			7.9	330.0
20+37			9.0	328.9
20+37.5			8.34	329.52
20+50			7.9	330.0
20+55			7.9	330.0
20+57.2			9.5	328.4
T.P.#4			12.97	324.89
	0.30	325.19		
20+77			8.4	316.8
T.P.#5			12.27	312.92
	1.14	314.06		
21+00			8.3	305.8
21+07			10.9	303.2
21+27			15.1	299.0
T.P.#6			12.29	301.77
	2.61	304.38		

R.B.

5/28/47

REDUCED

NOTES

End oil

Gutter

Curb

Top of bank

CHECK BY RAINY 7/15/47

Sewer M.H. 178' Lt. of 20+96

Rim 303.0  
Inv. 292.5

Sta.	+	H.I.	-	ELEV.
		304.38		
21+50			11.0	293.4
21+68			15.8	288.6
21+93			20.2	284.2
22+00			22.7	281.7
22+26			22.2	282.2
22+46			23.3	281.1
22+50			22.0	282.4
22+83			5.5	298.9
T.P.#7			1.00	303.38
	12.58	315.96		
23+00			7.1	308.9
23+04			4.5	311.5
23+23			2.0	314.0
T.P.#8			0.59	315.37
	11.76	327.13		
23+43			7.0	320.1
23+50			5.7	321.4
23+63 <sup>5</sup>			4.8	322.3
23+70			1.5	325.6
T.P.#9			0.08	327.05
	6.20	333.25		
23+83			4.6	328.7
24+00			4.7	328.6
24+50			4.8	328.5

R.P.S.

5/28/47

REDUCED

NOTES

CHECK BY RAINBY 7/15/47

Sewer M.H. 61.5' Rt. of 22+47  
Rim 280.8  
Inn 273.0

s edge sidewalk

edge oil



## Profile 40th St. Pipeline

<u>+</u>	<u>H.I.</u>	<u>-</u>	<u>ELEV.</u>
	333.25		
25+00		4.8	328.5
25+50		5.0	328.3
26+00		5.2	328.1
26+50		5.4	327.9
27+00		5.7	327.6
27+50		6.2	327.1
28+00		7.0	326.3
28+50		8.0	325.3
29+00		8.5	324.8
29+50		9.3	324.0
TR #10		9.35	323.90
	1.76	325.66	
30+00		2.6	323.1
30+50		3.3	322.4
31+00		4.1	321.6
31+50		4.9	320.8
32+00		5.5	320.2
32+50		6.1	319.6
33+00		6.8	318.9
33+50		7.3	318.4
TR #11 B.P.A.W. Cor Myrtle + 40th		7.48	318.18
	0.76	318.9A	
34+00		1.7	317.2
34+04		1.7	317.2

T.P. 10

5/29/47

REDUCED

NOTES

edge of oil

## Profile 40th St. Pipeline

Sta.	±	H.I.	—	Elev.
		318.94		
34+50			2.8	316.1
35+00			3.8	315.1
35+50			5.4	313.5
36+00			6.8	312.1
36+50			8.4	310.5
37+00			9.9	309.0
37+50			11.4	307.5
38+00			12.9	306.0
T.P. #12			12.85	306.09
	1.48	307.57		
38+50			3.0	304.6
39+00			4.4	303.2
39+50			5.7	301.9
40+00			6.9	300.7
40+21	Invert Rim	9.0 7.3		298.6 300.3
40+50			7.6	300.0
40+62.38			7.6	300.0
40+78	Invert Rim	10.4 7.2		297.2 300.4
41+00			7.7	299.9
41+50			7.1	300.5
42+00			6.5	301.1
42+50			5.5	302.1
Set T.B.M. Top E.H. at Alley			3.00	304.57

between 40th + Central on Thorn

6.51 310.88

1' x 1' Square Drain M.H. 15' E of Line

A Pt. 90° 02' Lt

Drain M.H. 15' N of Line

188

5/29/97

REDUCED

REGALIGN NOTES  
SEE P 50 33

Sta	H.I.	Elev.
	310.88	
	17vert	13.9
	Rim	8.4
42+42		297.0
		302.5
43+00		302.8
43+50		303.6
44+00		304.2
44+50		304.6
45+00		305.1
45+50		306.0
45+96		306.9
46+04.99		307.3
	14v.	9.1
46+25	Rim	1.2
		301.8
		309.7
46+50		308.2
47+00		308.9
47+50		309.7
48+00		310.0
48+50		309.7
49+00		308.4
49+50		307.1
T.P. #1A		307.11
	0.17	307.28
50+00		305.6
50+50		303.9
51+00		302.7
51+50		301.4
51+70		300.5

6/2/47 R.G. 165.50  
 See Page 33  
 NOTES REPROD

Sewer M.H. 15' Not Line { Inv. 306.1  
 Sewer M.H. 325' S of line { Rim 311.3

INVERT CANT  
 BE HIGHER THAN  
 RIM.

48+50 LT.

48+50 RT.

Sewer M.H. 50'S of line

Sewer M.H. 35' S of Sta. 50+05 Inv. 299.6  
 Sewer M.H. 305' Not S of Sta. 50+05 Rim 303.9  
 Rim 311.9

In gutter W. side Marlborough

Profile 40th St. Pipeline

Sta.	+ H.I.	-	ELEV.
	307.28		
52+00		6.2	301.1
52+50		6.2	301.1
53+00		6.4	300.9
53+50		6.9	300.4
54+00		7.2	300.1
T.B.M. Top F.H. Between	5.14		302.14
Marborough A2nd on Thorn			
	5.50		307.64
54+50		7.7	299.9
55+00		7.8	299.8
55+27		8.5	299.1
55+42			
55+50		9.4	298.2
	Invert	18.4	289.2
55+71	Rim	10.0	291.6
	Invert	27.5	280.1
55+71	Grate	9.4	298.2
56+00		9.0	298.6
56+11		9.0	298.6
56+50		7.5	300.1
57+00		5.5	302.1
57+50		4.3	303.3
58+00		2.7	304.9
58+50		1.6	306.0

Notes reduced 6/12/47 D.M.

Wedge concrete - ?  
→ SHOWN AT 55+31.6 ON PAGE 12

Drain M.H. 10' off line  
Drain Outlet 13' 5" off line

Edge concrete or oil

Sta 57+59 Sewer M.H. 35' 5" off line Invert 298.8 Rim 304.4

Sta.	±	H.I.	—	ELEV.
		307.64		
59+00			0.9	306.7
TR #16			0.76	306.88
	303	309.91		
59+33			2.6	307.3
59+37			2.1	307.8
59+42			2.8	307.1
59+50			2.1	307.8
60+00			2.2	307.7
60+17			2.8	307.1
60+22			3.0	306.9
61				
60+33			3.4	306.5
60+51			4.3	305.6
60+62			14.1	295.8
60+73			14.6	295.3
TR #17			13.03	296.88
	0.69	297.57		
60+82			0.3	297.3

Notes reduced 6/12/47 D.M.L.

Lt		Rt		25
+0.3	00	-0.5	-1.0	
25	10	10	25	
+0.3	+0.2	00	-1.2	-7.5 -6.3
25	10	4	9	12 25
+0.4	+0.3	+0.3	-8.8	-11.0
25	10	10	12	25
+1.3	+1.0	-1.5	-8.7	-9.0 -6.0 -7.9 -10.1
25	10	4	6	14 15 17 25
<i>on gas line</i>				
+10.1	+10.4	+8.0	+9.6	+10.0
43	26	18	15	11
				11 25
<i>in gas ditch pipe open</i>				
+8.5	+7.3	+5.6	+5.8	+6.0 +5.6
36	26	20	16	12 3
				4 14 30
<i>gas line</i>				
-0.1	-0.3	-1.3	+0.2	-6.3 -10.5 -12.2
50	24	22	13	3 11 25

Sta	+	H.I.	-	ELEV.
		297.57		
60+95			3.6	294.0
61+00			5.3	292.3
61+03			4.2	293.4
61+45			11.1	286.5
61+45	On pipe		11.15	286.42
61+85	on Pipe		15.7	281.9
TP#18			0.69	296.88
	12.38	309.26		
TP#19			1.35	307.91
	10.22	318.13		
TP#20			0.31	317.82
	11.93	329.75		
B.M. B.P. NWCox			8.14	321.61
				corr 321.62
Myrtle + 42nd				

Notes Reduced 6/12/47 DML

end of 12" Line

## Profile Thorne Sta. 8" Line

±	H.I.	-	ELEV.
T.B.M. top Fire Plug 40th + Thorne	P22		304.57
0.92	305.49		
0+00 - 40+62 78 40th St.		5.6	299.9
0+35	Invert	9.2	296.3
	Rim	3.6	299.9
0+50		6.0	299.5
1+00		6.0	299.5
1+50		5.9	299.6
2+00		5.2	300.3
2+50		4.6	300.9
3+00		3.5	302.0
3+50		1.0	304.5
T.P. #1		0.14	305.35
5.17	310.52		
4+00		5.1	305.4
4+50		4.5	306.0
5+00		4.0	306.5
5+50		3.7	306.8
6+00		4.1	306.4
6+50		5.1	305.4
7+00		6.1	309.4
7+60 <sup>32</sup>		7.9	302.6
T.B.M. F.H. 40th + Thorne		5.97	304.55

DML

6/12/47

NOTES REDUCED

Drain M.H. 15' W of Line

6" C.I. Sewer Crossing 3.6 ± 0.2 Deep No M.H.  
 Sewer M.H. 30.5 of Sta. 2+00 Invert 295.0  
 Rim 302.0

end of line

28

## CROSS SECTIONS

## COMMERCIAL ST. PIPE LINE

B.M. HUB STA. 37+53.24 = 37+59.07

→ F.B. 1722 PAGE 23 ELEV 60.21

STA.	+	H.I.	-	ELEV.
B.M.	7.90	65.11		60.21
38+20			10.0	55.1
38+50			12.1	53.0
T.P. #1			10.79	59.32
	12.06	66.38		
39+00				
39+50				
40+00				
40+50				
B.M. Hub			6.17	60.21

THESE NOTES COPIED FROM A CROOKER'S  
SMALL FIELD BOOK (NO NUMBER) 6/25/47

JUNE 23, 1947

RAINEY  
NIENOW  
BAKER  
RT.

28

LT.

E

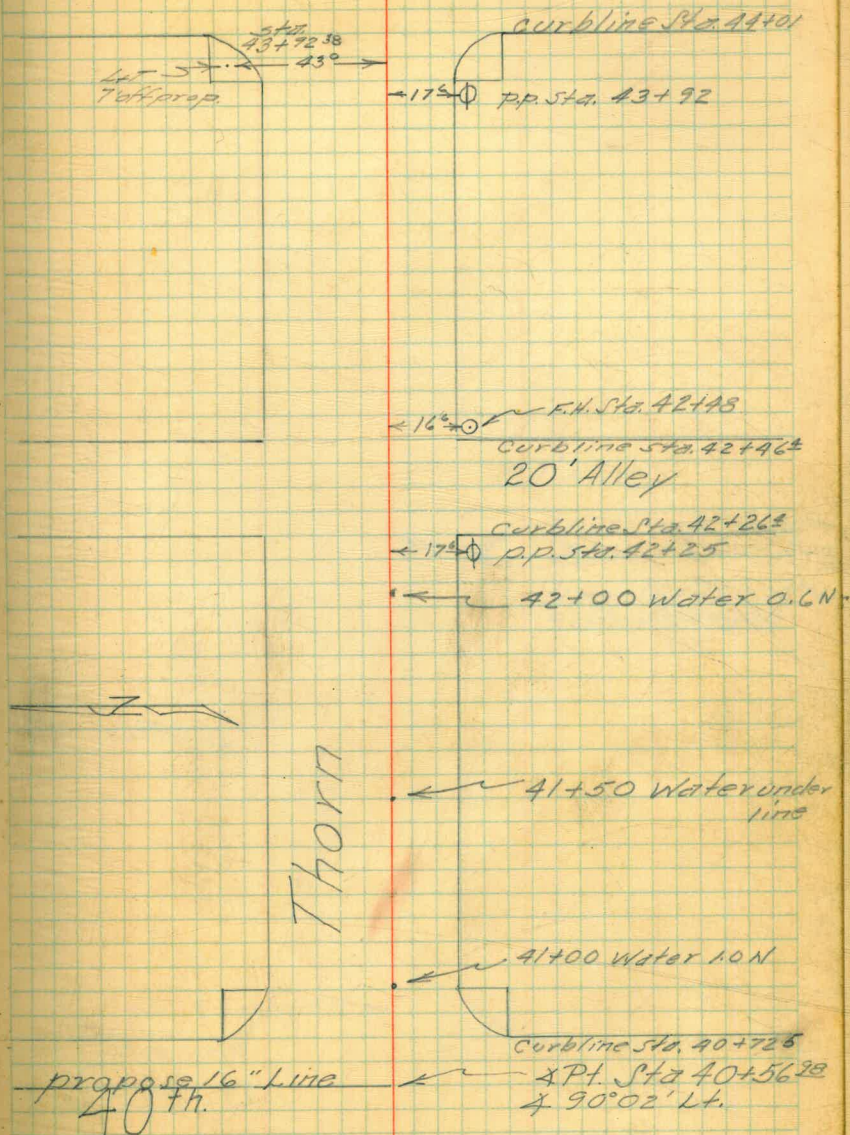
53.7	55.1	54.3	61.7	61.1	
-1.4	10.0	-0.8	+6.6	+6.0	
20		10	25	33	EDGE CONCRETE
53.2	53.0	54.6	63.0	62.3	
+0.2	12.1	+1.6	+10.0	+9.3	
20		38	54	65	CONC.
53.2	53.3	54.7	64.0	64.0	62.5
-0.1	13.1	+1.4	+10.7	+10.7	+9.2
20		30	45	48	50
53.7	53.7	55.8	65.0	64.9	63.9
0.0	12.7	+2.1	+11.3	+11.2	+10.2
20		29	45	48	50
53.5	53.7	55.5	66.5	66.2	65.1
-0.2	12.7	+1.8	+12.8	+12.5	+11.4
20		26	44	49	51
52.9	53.3	54.7	67.5	67.3	66.4
-0.4	13.1	+1.4	+14.2	+14.0	+13.1
20		24	44	48	51

NOTES REDUCED 6/24/47




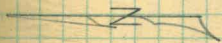
29

July 8, 1947

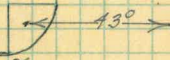
Raney  
Narrow  
BakerRealignment 40+Thorn Pipeline  
Central 29

20' Alley


 curb line RR old station  
 P.I. with proposed  
 line Sta 46+04.29 Als  
 = Sta 45+96.00

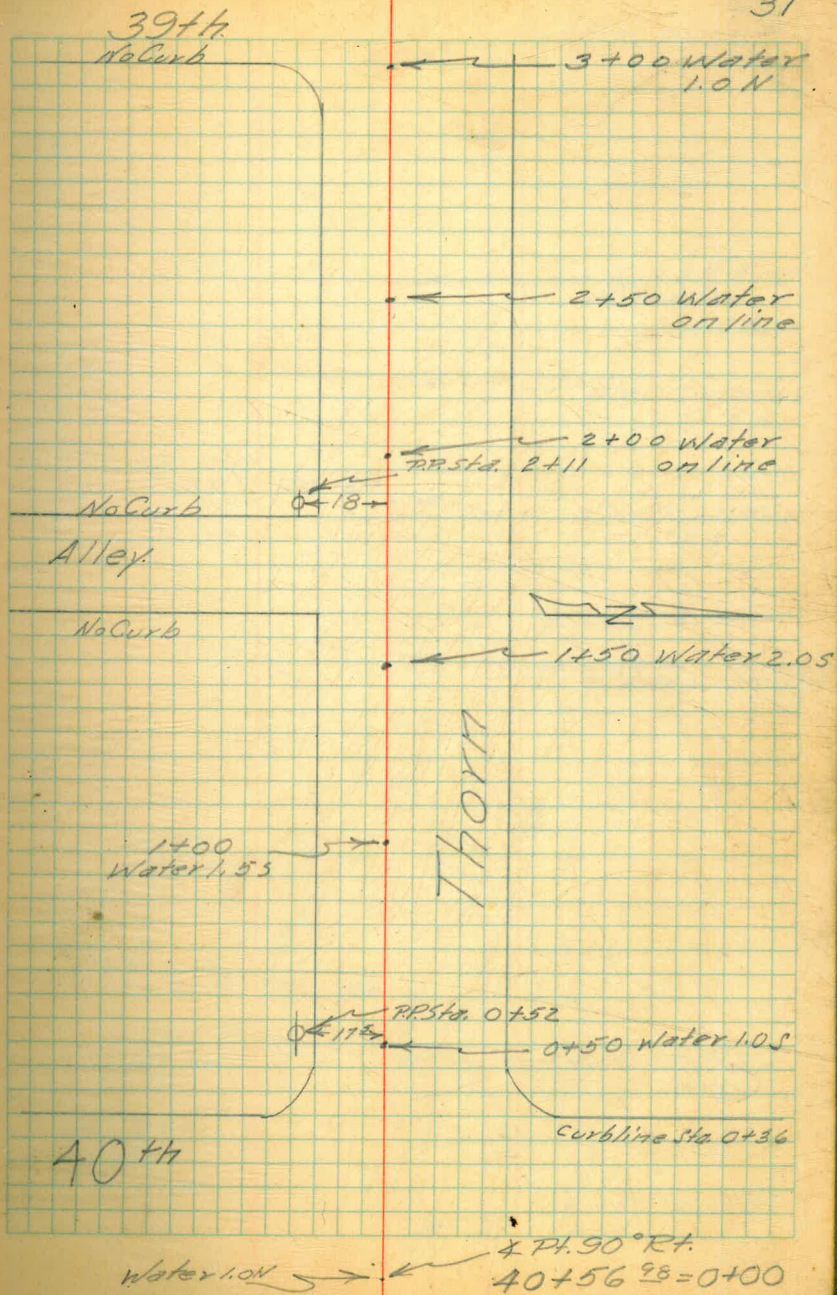


Thorn


 Full T 43°  
 7' off prop  
 Sta 44+52.35

Central

Curb line Sta 44+52



38th

End Sta 7+60.34

6+37 End  
of water  
1.036+00 Water  
0.65RR Sta  
5+89

0+18

5+50 Water  
1.255+00  
Water on line

Thorn

4+50  
Water 2.03RR Sta  
4+30

0+18

Ed. Int 5  
Sta 4+25 1/2

0+23

4+00 Water  
1.05

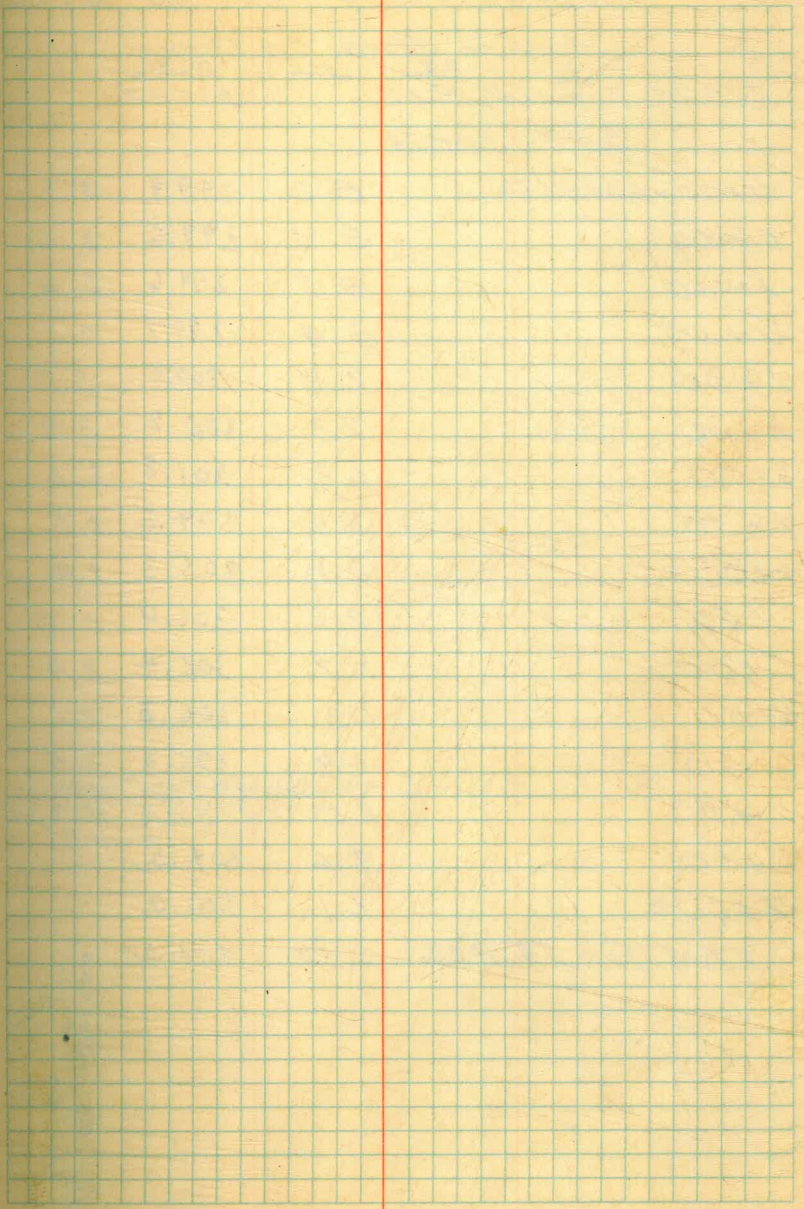
39th

3+50 Water  
1.65

33 Profile New Alignment

Sta	$\pm$	H.I.	ELEV	Depth of 2" water
T.B.M. Top F.H. P22		307.90	304.57	
	3.33			
40+56.25			299.9	3.0
41+00			300.1	3.6
41+50			300.9	3.2
42+00			301.9	3.0
42+50			302.3	3.1
43+00			303.1	
43+50			303.9	
44+00			304.4	
44+50			304.5	
45+00			305.4	
45+50			306.4	
45+96 = 46+04.23			307.3	
T.B.M. Top F.H. P22		307.90	304.57	

NOTES RECORDED 7/11/47 R.S.



34 Profile New Alignment  
40th + Thorn Pipeline <sup>Depth</sup> of 2" water

10th to 38th on Thorn  
+ H.I. = ELEV.  
T.B.M. Top F.H. P.22 304.57

3.57 308.14

0+00 = 40+56 <sup>26</sup>	8.2	299.9	3.2
0+50	8.5	299.6	3.6
1+00	8.5	299.6	3.6
1+50	8.4	299.7	4.1
2+00	7.8	300.3	3.3
2+50	7.3	300.8	3.0
3+00	6.3	301.8	2.2
3+50	3.9	304.2	2.5
4+00	2.8	305.3	2.4
4+50	2.1	306.0	2.5
5+00	1.7	306.4	2.4
5+50	1.3	306.8	2.6
6+00	1.8	306.3	3.5
6+50	2.8	305.3 13' back	4.2
7+00	3.6	304.5	
7+60 <sup>34</sup>	6.1	302.0	
T.B.M. Top F.H. P.22	3.57	304.57	

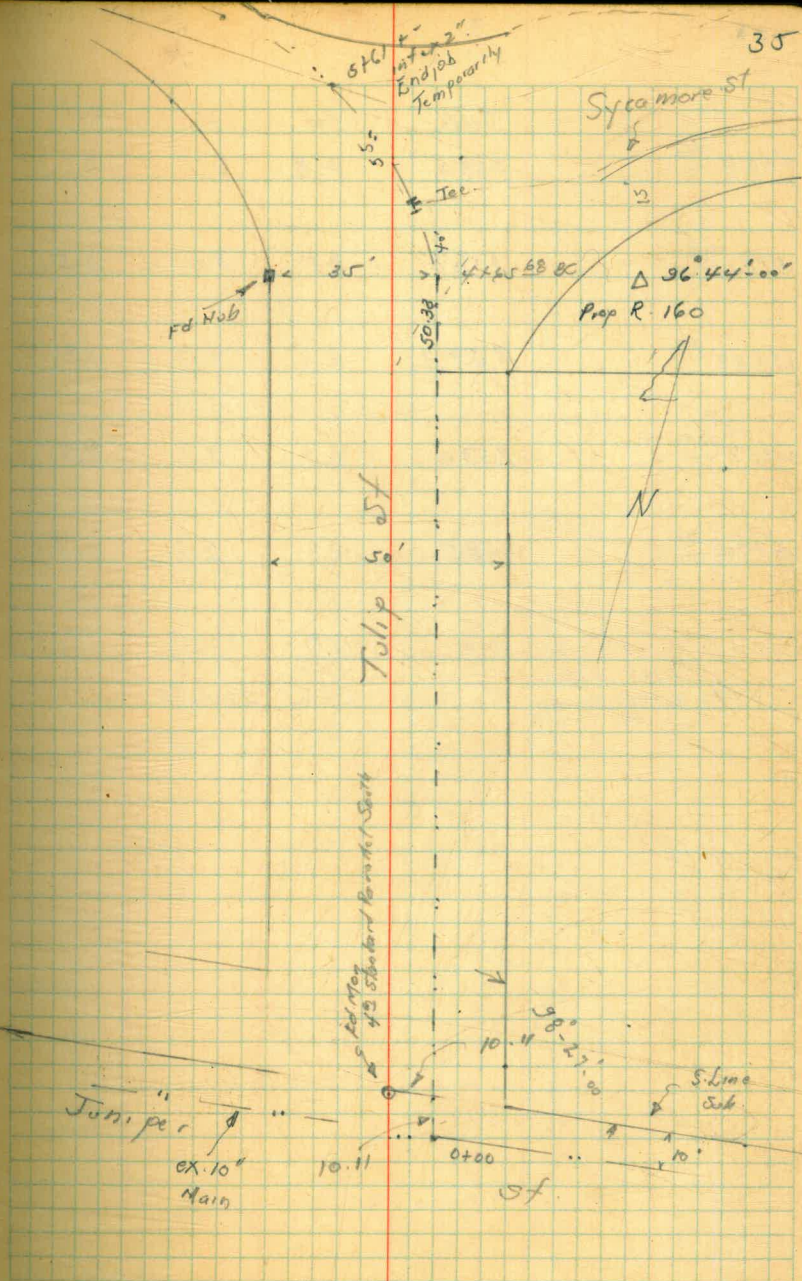
NOTES RECORDED  
7/11/47  
RFB

end of 2" water 6+37

Bliss  
Leonard  
Baker  
10/28/27

Grades for 8" water Main - Tulip St  
Juniper to Sycamore

BM	8.04	261.25		253.21	
0+00		Grade 247.7	G. Rod 13.5	9.4	C 4.1 ✓
0+50		248.7	12.5	7.7	C 4.8 ✓
1+00		249.8	11.4	7.6	C 3.8 ✓
1+50		250.8	10.4	6.6	C 3.8 ✓
2+00		251.9	9.3	6.1	C 3.2 ✓
2+50		252.9	8.3	5.0	C 3.3 ✓
3+00		253.9	7.3	3.3	C 4.0 ✓
3+50		255.0	6.2	2.4	C 3.8 ✓
4+00		256.0	5.1	1.2	C 3.9 ✓
T.P.	7.29	267.32	122	260.03	
4+50		257.1	10.2	7.6	2.6 ✓
+65 <sup>FB</sup> BC.		257.4	9.9	6.8	3.1 ✓



	$\pi$	G. Rod	-	out
4188.46	2585	8.8	6.1	2.7 ✓
5110.06	2588	8.5	5.0	3.5 ✓
5129.72	2593	8.0	4.2	3.8 ✓
5153.28	2590	8.3	3.8	4.5 ✓
5174.83	2585	8.8	2.1	6.7 ✓
check Ground of Prop. BC. at West		3.8	2635-	
7 Pch NE Cor		5.56	2618-	
Set BM # 488017 Sycamore		2.86	264.46	
(W) 4701P				



40th + Thorm St.  
for Construction

Cuts

Dec. 1, 1947

Rainey  
King  
Nienow

37

T.B.M. Top FH.		302.14		
5.60	307.74			
55+00	7.8	299.9	296.2	3.7
55+50	9.3	298.4	294.6	3.8
56+00	9.0	298.7	294.9	3.8
56+25	8.6	299.1	295.0	4.1
56+50	7.4	300.3	296.3	4.0
56+75	6.1	301.6	297.6	4.0
57+00	5.4	302.3	297.7	4.6
57+63	3.7	304.0	298.0	6.0
57+65	3.6	304.1	300.0	4.1
58+00	2.6	305.1	300.9	4.2
58+50	1.6	306.1	302.2	3.9
58+75	1.2	306.5	302.8	3.7
59+25	0.5	307.2	303.3	3.9
T.P.#1	0.49	307.25		
2.20	309.45			
59+75	2.5	307.0	303.0	4.0
60+00	4.1	305.4	299.7	5.7
60+50	9.7	299.8	293.1	6.7
T.P.#2	10.99	298.46		
0.29	298.75			
61+00	5.8	293.0	289.1	3.9
61+43	11.5	287.2	285.6	1.6
T.P.#3	0.29	298.46		
12.68	311.14			
1 B.M.	9.01	302.13		

end

40th + Thorn St.  
for Construction

B.M. Top F.H. between Andy Maxl. 302.14

4.00 306.14

54+50	6.1	300.0	296.3	3.7
54+00	5.9	300.2	296.4	3.8
53+50	5.6	300.5	296.6	3.9
53+00	5.2	300.9	296.7	4.2
52+50	5.0	301.1	296.8	4.3
52+00	4.9	301.2	296.9	4.3
51+75	5.5	300.6	297.0	3.6
51+25	3.8	302.3	298.3	4.0
50+75	2.6	303.5	299.7	3.8
50+25	1.4	304.7	301.5	3.2
50+00	0.5	305.6	302.2	3.4
T.P.#1	0.52	305.62		

7.67 313.29

49+50	6.1	307.2	303.5	3.7
49+00	4.8	308.5	304.8	3.7
48+50	3.5	309.8	305.9	3.9
48+00	3.2	310.1	306.3	3.8
47+50	3.7	309.6	306.0	3.6
47+00	4.4	308.9	305.2	3.7
46+50	5.1	308.2	304.5	3.7
46+04.92 = 45+96.00	5.8	307.5	303.7	3.8
45+50	6.8	306.5	302.8	3.7
T.P.#2	6.75	306.54		

2.28 308.02

Dec. 5, 1947

Raimy  
King  
Nixon

38

cuts

Cuts

308.82

45+00	3.2	305.6	301.8	3.8
44+50	4.2	304.6	300.8	3.8
44+00	4.1	304.7	300.7	4.0
43+50	4.9	303.9	300.0	3.9
43+00	5.6	303.2	299.3	3.9
42+50	6.3	302.5	298.6	3.9
42+00	7.3	301.5	298.0	3.5
41+60	7.8	301.0	297.3	3.7
41+10	8.5	300.3	296.6	3.7
40+75	8.5	300.3	294.9	5.4
40+60	8.7	300.1	294.9	5.2
40+56 <sup>28</sup> = 0+00	8.8	300.0	294.7	5.3
0+50	8.9	299.9	294.5	5.4
1+00	9.0	299.8	295.1	4.7
T.P.#3	9.07	299.75		

10.08 309.83

1+50	10.0	299.8	295.6	4.2
2+00	9.5	300.3	296.2	4.1
2+50	9.2	300.6	296.9	3.7
3+00	8.2	301.6	297.6	4.0
3+50	5.6	304.2	298.6	5.6
3+83	4.8	305.0	298.7	6.3
4+00	4.5	305.3	299.2	6.1
4+50	3.8	306.0	299.5	6.5

Dec. 18, 1947

Rainey  
King  
Nielsen

40

Cuts

	309.83				
5+00		3.4	306.4	300.3	6.1
5+50		3.0	306.8	300.4	6.4
5+75		3.2	306.6	300.4	6.2
6+00		3.5	306.3	299.9	6.4
6+50		4.5	305.3	299.0	6.3
7+00		5.3	304.5	297.2	7.3
7+25 <sup>th</sup> End		6.2	303.6	296.3	7.3
BM. Top F.H. 40th + Thorn		5.24	304.57 corr 304.57		
Sta. 20+375 P. 19			329.52		
	1.36		330.88		
20+50		0.8	330.1	324.1	6.0
20+85		13.1	317.8	306.6	11.2
T.P. #1		13.09	317.79		
	0.76		318.55		
21+00		6.6	312.0	298.8	13.2
T.P. #2 on Rock		12.44	306.11		
	0.27		306.38		
21+25		2.8	303.6	291.3	12.3
21+50		10.0	296.4	284.9	11.5
T.P. #3		12.00	294.38		
	0.30		294.68		
21+94		9.6	285.1	275.5	9.6
22+50		12.6	282.1	277.0	5.1

## 4044 + Thorin

	294.68			
T.P.#4		0.58	294.10	
	12.40		306.52	
23+00		0.0	306.6	303.4
T.P.#5		0.20	306.32	
	12.11		318.43	
		0.03	318.40	
	11.20		329.60	
23+50		10.0	<sup>1</sup> 329.60	314.6
23+95		1.2	328.4	324.6
24+50 check		1.15	328.25	
T.B.M. Top F.H. P 22			304.57	
	4.36		308.93	
40+40		8.8	300.1	294.7
40+00		8.4	300.5	296.3
39+50		7.1	301.8	297.7
39+00		5.9	303.0	299.1
38+50		4.6	304.3	300.5
38+00		2.9	306.0	302.0
37+50		1.6	307.3	303.5
T.P.#7		0.27	308.66	
	12.95		321.61	
37+00		12.7	308.9	305.0
36+50		11.1	310.5	306.5

Cuts

41

3.2

5.0

3.8

5.4

4.2

4.1

3.9

3.8

4.0

3.8

3.9

4.0

40th + Thoria  
for Construction

	321.61			
36+00	9.5	312.1	308.0	
35+50	8.0	313.6	309.5	
35+00	6.6	315.0	311.0	
34+50	5.6	316.0	312.1	
34+00	4.3	317.3	313.1	
33+50	3.5	318.1	314.2	
33+00	3.1	318.5	314.8	
32+50	2.3	319.3	315.4	
32+00	1.6	320.0	316.1	
31+50	1.0	320.6	316.7	
31+00	0.3	321.3	317.5	
T.P. #2	0.10	321.51		

10.34 331.85

30+50	9.7	322.2	318.3	
30+00	9.0	322.9	319.1	
29+50	8.2	323.7	319.9	
29+00	7.4	324.5	320.7	
28+50	6.7	325.2	321.5	
28+00	5.8	326.1	322.3	
27+50	5.1	326.8	323.1	
27+00	4.6	327.3	323.8	
26+50	4.1	327.8	323.9	
26+00	3.8	328.1	324.1	
25+50	3.7	328.2	324.2	

4.1

42

4.1	350
4.1	1.58
4.0	
3.9	
4.2	
3.9	
3.7	
3.9	
3.9	
3.9	
3.8	

3.9
3.8
3.8
3.8
3.7
3.8
3.7
3.5
3.9
4.0
4.0

	331.85				
25+00		3.5	328.4	324.3	4.1
24+50		3.4	328.5	324.5	4.0
23+95	G. E. of line	3.3	328.6	324.6	4.0
24+50		3.38	328.47	328.45	

Regrading 40th St. Steep Slope  
 of Wardis St.

			329.52		
	1.45	330.97			
20+50		0.9	330.1	324.1	6.0
20+85		13.2	317.8	306.5	11.3
T.P.#1		11.97	319.00		
	0.70	319.70			
20+92		4.7	315.0	303.0	12.0
21+10		11.0	308.7	296.4	14.3
T.P.#2		12.89	306.81		
	0.88	7.69	306.89		
21+28		4.9	302.8	290.6	12.2
21+46		9.7	298.0	285.6	12.4
T.P.#3		11.09	296.60		
	1.68	298.28			
21+64		5.3	293.0	281.4	11.6
21+82		9.9	288.4	278.0	10.4
22+00		13.6	284.7	275.4	9.3
22+50				277.0	5.1

cuts

43

Rainey Dec. 23, 1947  
King  
Nieman

44

	298.28				
T.P.#4		1.22	297.06		
	10.33	307.39			
22+90		6.7	300.7	297.6	3.1
22+96		2.9	304.5	299.6	4.9
T.P.#5		1.04	306.35		
	12.84	319.19			
23+14		6.9	312.2	304.8	7.4
T.P.#6		0.76	318.43		
	12.84	331.27			
23+50		11.6	319.7	313.6	6.1
23+68		9.6	321.7	318.8	2.9
23+86		2.9	328.3	324.6	3.7
23+95 check		2.85	328.42		



## 40444 Thorn for Construction

Dec. 26, 1947 Rainey  
King  
Narrow

46

			329.52		
	9.22	338.74			
20+00			9.0	329.7	325.7
19+50			7.7	331.0	327.3
19+00			6.1	332.6	328.9
18+50			4.4	334.3	330.4
18+00			2.8	335.9	332.0
17+50			1.2	337.5	333.6
TP <sup>th</sup>			0.36	338.38	
	8.94	347.32			
17+00			8.2	339.1	335.2
16+50			7.3	340.0	336.3
16+00			6.8	340.5	336.9
15+50			6.4	340.9	337.2
15+00			6.1	341.2	337.5
14+50			5.8	341.5	337.8
14+00			5.4	341.9	338.1
13+75			5.2	342.1	338.2
13+50			5.3	342.0	338.6
13+40			5.2	342.1	338.6
13+ <sup>2</sup> 0			5.1	342.2	337.7
13+00			5.0	342.3	337.7
12+50			4.4	342.9	338.8
12+00			3.7	343.6	339.5
11+50			3.1	344.2	340.2

4.0

3.7

3.7

3.9

3.9

3.9

3.9

3.7

3.6

3.7

3.7

3.7

3.8

3.9

3.4

3.5

4.5

4.6

4.1

4.1

4.0

40th + Thorr St. Line  
for Construction

347.32

11+00	2.4	344.9	340.9
10+50	1.7	345.6	341.6
TP #2	1.29	346.03	

7.73 353.76

10+00	7.5	346.3	342.3
9+50	6.8	347.0	342.4
9+00	6.3	347.5	342.5
8+50	5.9	347.9	342.6
8+00	5.5	348.3	342.7
7+50	5.0	348.8	342.8
7+00	4.4	349.4	342.9

Top Grate 13' E of line  
No. 2 Driv. 3.73 350.03

8.89 358.92

6+50	8.8	350.1	343.0
6+25	8.9	350.0	343.0
6+00	8.9	350.0	344.0
5+50	8.4	350.5	346.1
5+25	8.1	350.8	347.1
5+00	7.7	351.2	347.4
4+50	7.0	351.9	348.1
4+00	6.3	352.6	348.8
3+50	5.6	353.3	349.5
3+00	4.9	354.0	350.2
2+50	4.1	354.8	350.8

Dec. 30, 1947 Rainey  
King  
Nishow

46

0 x 5

4.0

4.0

4.0

4.6

5.0

5.3

5.6

6.0

6.5

7.1

7.0

6.0

4.4

3.7

3.8

3.8

3.8

3.8

3.8

4.0

cuts

	358.92				
2+00		3.4	355.5	351.5	4.0
1+50		2.8	356.1	352.7	3.9
1+00		2.1	356.8	352.9	3.9
0+50		1.5	357.4	353.0	4.4
Top of grate	13.5 of line	8.90	350.02		

Profile 40th + Thorne St  
Pipeline after Backfill

Mar. 1, 1948

Rainey 48  
Baker  
Shipman

20+37.5 Curb			329.52
	2.86	332.38	
20+50		2.6	329.8
20+58		3.0	329.4
TP #1			319.52
	0.76	<del>320.28</del>	<del>319.42</del>
		12.86	
20+85		7.6	312.7
20+92		10.2	310.1
TP #2			308.81
	1.16	<del>309.97</del>	<del>308.71</del>
		11.47	
21+00		3.0	307.0
21+10		5.0	304.1
21+28		10.9	299.1
21+46		14.3	295.7

RA

3-1-48

RE DUCED

NOTES

	309.97		
	<del>308.87</del>		
T.P.#3			296.93
	297.28	13.04	<del>296.85</del>
	0.35		<del>247.15</del>
21+64		6.1	291.2
21+82		10.2	287.1
22+00		13.3	284.0
22+50		13.8	283.5
T.P.#4			296.67
	308.56	0.61	<del>296.57</del>
	11.89		<del>308.46</del>
22+90		6.4	302.2
22+96		3.0	305.6
23+00		0.0	308.6
T.P.#5			307.28
	319.61	1.28	<del>307.18</del>
	12.33		<del>319.51</del>

NOTES RECALCULATED 3-1-48

319.61  
~~319.51~~

23+14                      6.5    313.1

23+50                      10.1    319.7

T.P. #6  
10.32    329.23    0.70    318.91  
~~10.32    328.15    318.81~~

*Pls*

23+68                      5.7    323.5

23+74                      4.0    325.2

23+81                      3.2    326.0

23+86                      1.3    327.9

check 23+95              0.46    328.47  
~~328.37~~

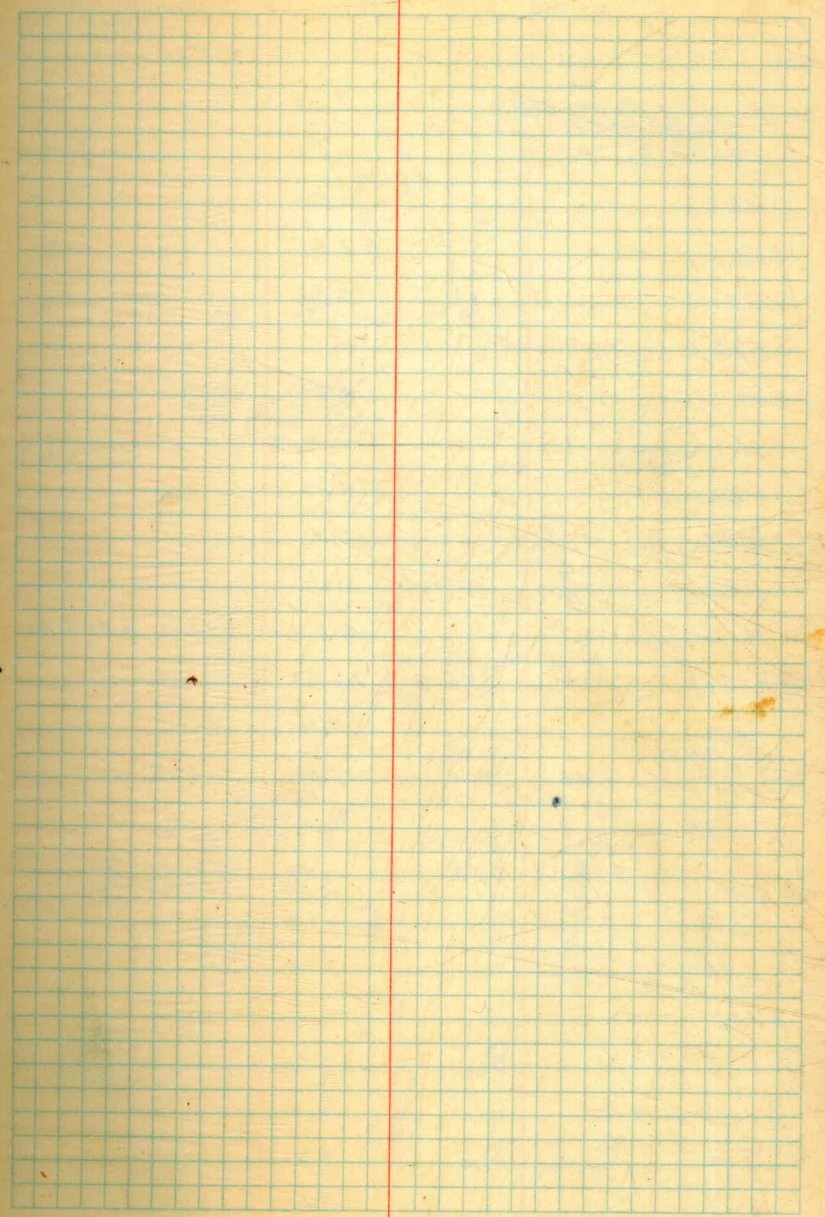
NOTES  
RANUCO 3-1-95

4044 + Thorne St. Profile  
cont. after Backfill

56+00		298.7
	10.66	309.36
59+90.9	1.8	307.6
60+00	2.5	306.9
60+50	9.9	299.5
T.P.#1	12.93	296.43
	1.90	298.33
61+00	5.9	292.4
61+27.5 end of dirt	9.9	288.4
end of pipe P26	11.9	286.43

*Handwritten initials*

NOTES RECORDED 3-1-48

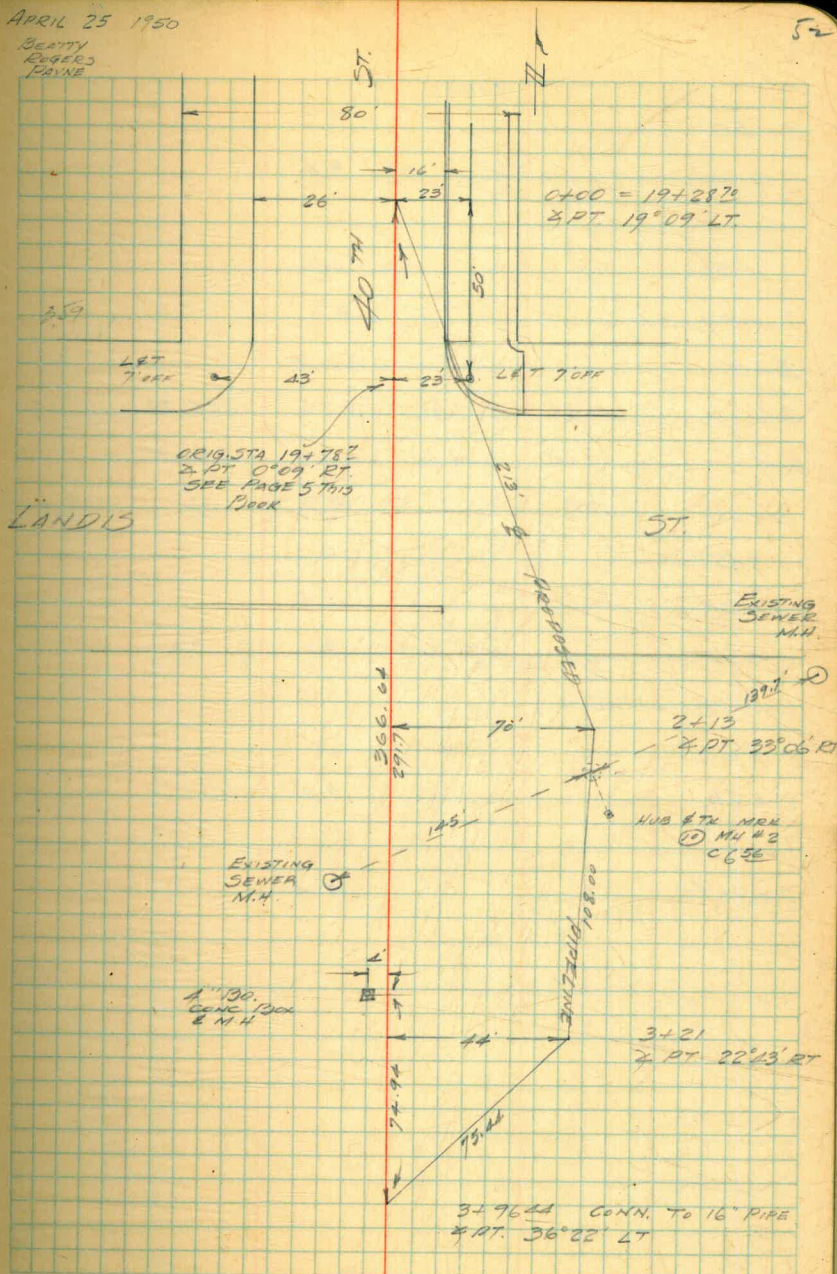


RELOCATION 40TH ST. PIPELINE  
AT  
40TH AND LANDIS & Southernly

B.M.	3.49	332.78	330.29	B.P. IN NW CURB RET 40TH & LANDIS
0+00	(= STA 19+2870 SEE PAGE 5)		2.07	
+48			4.07	IN GUTTER
+48.2			3.53	TOP CURB
+50			3.53	" "
+57			3.54	" "
+57.2			4.1	
1+00			4.8	
+11			5.4	
+20			4.5	
+25			5.1	
+29				
CK P. POOL CURB			4.60	329.18 = 329.52
IP	0.27	321.18	12.87	320.91
+50			6.9	
IP	1.45	309.60	13.03	308.15
+69			6.4	
IP	0.47	297.36	12.69	296.91
CK B.M.	9.26	295.13	11.53	285.85
+83			11.69	283.44
+83			+1.3	(SEE CURB & CONC. M.H. MARK WITH YELLOW PAINT)
+93			4.0	
2+00			6.5	
+09			8.6	
2+13°	X PT.		8.4	
+19			9.3	
+41			7.4	
+45			8.3	

APRIL 25 1950

BEATTY  
ROBERTS  
FRYNE





4/25/50

2+50		295.13	8.5	
+60			9.4	
+68			6.3	
+91			4.9	
3+00			+0.4	
①	11.53	297.38	9.28	285.85
①	12.69	309.60	0.47	296.91
+210	✗ PT		9.3	
+37			10.1	
+39			10.8	
+50			9.0	
+74			5.9	
+80			5.0	
+86			3.5	
3+9644			4.4	

53

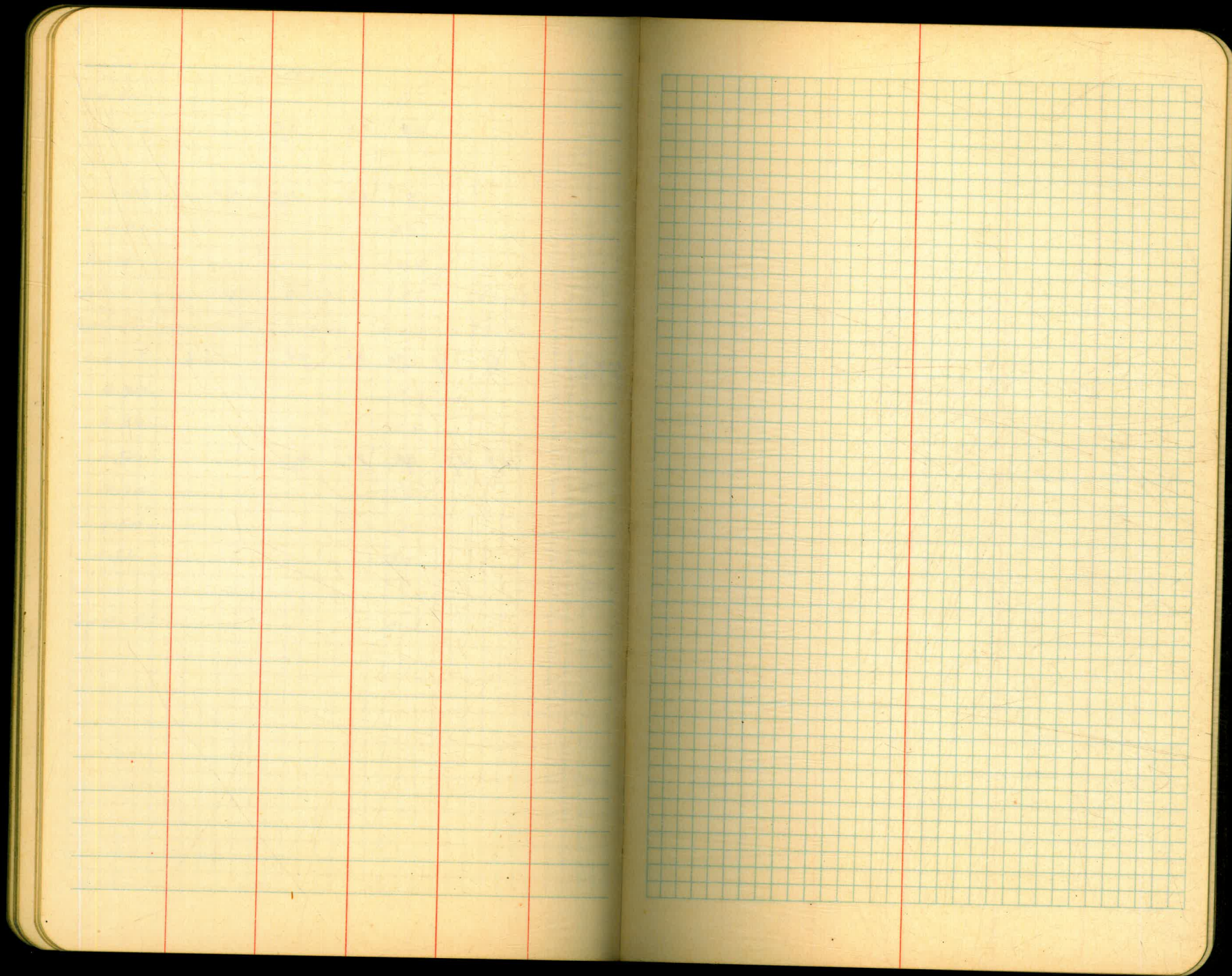
28	94	99
11	5	10

15	63	10.0	10.0
10		7	12

(RT & T2)  
(OK TAN)

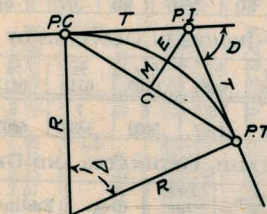
81	80	76	93	15.4
10	5	2	6	9

53	57	54	90	16.0
10	8	5		10



# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



## CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin. \frac{D}{2}} \quad (1) \quad \text{Degree of Curve} = D \text{ and } \sin. \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \quad \text{Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R \left(1 - \cos. \frac{\Delta}{2}\right) \quad (5) = R \text{vers } \frac{\Delta}{2} \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R \div \cos. \frac{\Delta}{2} - R \quad (8) = R \text{exsec } \frac{\Delta}{2} \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin. \frac{\Delta}{2} \quad (10) \quad \Delta = \text{Central Angle}$$

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{3} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I. —  $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance =  $158 - \text{Sta. P. C.} = 54.50$ , hence offset =  $7.27 \left(\frac{54.50}{100}\right)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or =  $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$  and from Table V correction = .10 or  $E = 115.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

20 + 50  
 20 + 85  
 20 + 92  
 21 + 20  
 21 + 28  
 21 + 46  
 21 + 64  
 21 + 82  
 22 + 00  
 22 + 50  
 22 + 90  
 22 + 96  
 23 + 14  
 23 + 50  
 23 + 68  
 23 + 86

Please Return to  
 City of San Diego Water Dept.  
 Room 268 Civic Center  
 Telephone Main 5161

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \div 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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