

W 718

WILEY & SONS

---

ENGINEERS'  
LEVEL BOOK

No. 412 F

---

# 718

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

MICROFILMED

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

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Telephone Main 5161

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Made in U. S. A.

Date	Today	By	Notes			
			Date	By	Hot	Mob
8/15	24	M.P.V.				
8/22	26	M.P.V.				

Rib + Spring Line offsets Rib # 561  
 to # 720 9-19  
 Rib alignment from rib 1136 to  
 1256. 20-23  
 X-Section West Tunnel Portal p. 24  
 Sta. of W. Portal p. 24  
 X Section Ground at Rib 1256 to  
 1210. W. Tunnel Portal p. 26 04

1  
 8.  
 7  
 03  
 04  
 05

## Spring Line

	Lt	Rt
105	3.63	3.75
106 "	3.55	3.83
107 "	3.53	3.82
108 "	3.57	3.70
109 "	3.70	3.67
110 "	3.68	3.66
111 "	3.63	3.72
112 "	3.65	3.69
113 "	3.67	3.70
114 "	3.65	3.72
115 "	3.68	3.71
116 "	3.69	3.65
117 "	3.73	3.67
118 "	3.75	3.64
119 "	3.69	3.66
120 "	3.70	3.70
121 "	3.66	3.75

## Rib Elevations

	↑	↑	↑	Elev	see p. 2
4.40	553.77			549.37	717 page
105			+2.40	556.17	556.03
106			+2.43	556.20	"
107			+2.37	556.14	"
08			+2.44	556.21	"
09			+2.45	556.22	"
10			+2.37	556.14	"
11			+2.31	556.08	"
12			+2.38	556.15	556.04
13			+2.42	556.19	"
14			+2.49	556.26	"
15			+2.42	556.20	"
16			+2.39	556.16	"
17			+2.40	556.17	"
18			+2.39	556.16	"
19			+2.57	556.34	"
20			+2.59	556.36	556.05
21			+2.59	556.36	"

## Spring Line

	lt	pt
122 <sup>1</sup>	3.59	3.78
123"	3.67	3.70
124"	3.67	3.70
125"	3.66	3.72
126"	3.68	3.66
127"	3.59	3.78
128"	3.60	3.77
129"	3.62	3.79
130"	3.62	3.76
131"	3.64	3.70
132"	3.58	3.80
133"	3.69	3.65
34"	3.76	3.57
35"	3.85	3.50
36"	3.82	3.52
37"	3.75	3.63
38"	3.73	3.54
39"	3.78	3.55

	+	Σ 553.77	+ or -	Elev	3
122 <sup>1</sup>			+2.52	556.29	556.05
23"			+2.50	556.27	"
24"			+2.45	556.22	"
25"			+2.41	556.18	"
26"			+2.44	556.21	"
27"			+2.53	556.30	"
28"			+2.54	556.31	556.06
29"			+2.55	556.32	"
130"			+2.56	556.33	"
31"			+2.51	556.28	"
32"			+2.46	556.23	"
33"			+2.45	556.22	"
34"			+2.48	556.25	"
35"			+2.42	556.19	"
36"			+2.38	556.15	556.07
37"			+2.44	556.21	"
38"			+2.44	556.21	"
39"			+2.47	556.24	"

	Lt	Spring-line Rt
140 <sup>1</sup>	370	351
41	3.68	3.45
42	3.68	3.40
43	3.70	3.37
44	3.75	3.41
45	3.80	3.42
46	3.76	3.47
47	3.84	3.42
48	3.86	3.39
49	3.89	3.34
150	3.82	3.44
151	3.82	3.55
52	3.77	3.54
53	3.70	3.59
54	3.72	3.56
55	3.74	3.62
56	3.82	3.48
57	3.77	3.57

	+	T 553.77	+0.1-	Key	4
140 <sup>1</sup>	0.07, 1		+2.64	556.41	556.07
141 "	"		+2.49	556.26	"
142 "	"		+2.46	556.23	"
143 "	"		+2.50	556.27	"
144 "	"		+2.49	556.26	556.08
145 "	"		+2.41	556.18	"
146 "	"		+2.39	556.16	"
147 "	"		+2.44	556.21	"
148 "	"		+2.44	556.21	"
149 "	"		+2.55	556.32	"
150 "	"		+2.52	556.29	556.09
151 "	"		+2.44	556.21	"
152 "	"		+2.46	556.23	"
153 "	"		+2.40	556.17	"
154 "	"		+2.40	556.17	"
155 "	"		+2.41	556.18	"
156 "	"		+2.41	556.18	556.10
157 "	"		+2.39	556.16	"

	Lt	Spring Line Rt		
58	3.76	3.49		
59	3.80	3.50		
60	3.81	3.50		
61	3.72	3.57		
62	3.67	3.51		
63	3.75	3.55		
64	3.67	3.62		
65	3.70	3.60		
66	3.68	3.58		
67	3.72	3.60		
68	3.71	3.63		
69	3.69	3.65		
70	3.64	3.66		
71	3.75	3.59		
72	3.62	3.65		
73	3.55	3.60		
74	3.58	3.65		
75	3.65	3.66		

	tor-	R. b Elev 553.77	tor-	Elev	5
58			+2.43	556.20	556.10
59			+2.39	556.16	"
60			+2.36	556.13	"
7.P.	-2.23	553.91	+2.37	556.14	"
761			+2.28	556.19	"
62			+2.25	556.16	"
63			+2.26	556.17	556.11
64			+2.28	556.19	"
65			+2.31	556.22	"
66			+2.28	556.19	"
67			+2.27	556.18	"
68			+2.27	556.18	"
69			+2.33	556.24	556.12
70			+2.33	556.24	"
71			+2.27	556.18	"
72			+2.40	556.31	"
73			+2.36	556.27	"
74			+2.28	556.19	"
75			+2.32	556.23	556.13

	Lf	Spring Line Rt	
176	3.66	3.64	
77	3.61	3.65	
78	3.60	3.64	
79	3.67	3.60	
80	3.65	3.61	
81	3.72	3.60	
82	3.72	3.59	
83	3.66	3.62	
84	3.71	3.57	
85	3.73	3.59	
86	3.67	3.65	
87	3.70	3.59	
88	3.72	3.57	
89	3.67	3.61	
90	3.67	3.63	
91	3.62	3.71	
92	3.67	3.65	
93	3.68	3.63	

		X 55301		6	
176			+2.37	556.28	556.13
77			+2.40	556.31	"
78			+2.41	556.32	"
79			+2.35	556.26	"
180			+2.33	556.24	"
81			+2.33	556.24	556.14
82			+2.35	556.26	"
83			+2.34	556.25	"
84			+2.34	556.25	"
85			+2.30	556.21	"
86			+2.30	556.21	"
87			+2.31	556.22	"
88			+2.35	556.26	556.15
89			+2.40	556.31	"
190			+2.41	556.32	"
TP	4.96	553.72	-5.16	548.75	Mon 3
91			+2.65	556.37	Record
92			+2.62	556.34	59876
93			+2.62	556.34	Corrected to above 8710 See FB 708P44



	Lt	Rt
194	3.73	3.57
95	3.68	3.58
96	3.63	3.67
97	3.68	3.62
98	3.68	3.65
99	3.69	3.62
200	3.73	3.61
201	3.74	3.56
202	3.80	3.47
03	3.78	3.49
04	3.86	3.45
05	3.77	3.50
06	3.71	3.62
07	3.67	3.57
08	3.72	3.58
09	3.65	3.59
210	3.63	3.60
11	3.63	3.55

				7
			553.72	
194		+2.61	556.33	556.16
195		+2.65	556.37	"
196		+2.66	556.38	"
197		+2.57	556.29	"
198		+2.61	556.33	"
199		+2.56	556.28	"
200		+2.62	556.34	556.17
01		+2.61	556.33	"
02		+2.62	556.34	"
03		+2.67	556.39	"
04		+2.52	556.24	"
05		+2.56	556.28	"
06		+2.58	556.30	556.18
07		+2.60	556.32	"
08		+2.65	556.37	"
09		+2.63	556.35	"
210		+2.64	556.36	"
211		+2.68	556.40	"

	Lt	Rt
212	3.76	3.56
13	3.78	3.65
14	3.66	3.60
15	3.64	3.63
16	3.60	3.69
17	3.64	3.68
18	3.66	3.65
19	3.72	3.56
220	3.74	3.56
21	3.79	3.56
22	3.69	3.59
23	3.68	3.64
24	3.69	3.63
25	3.83	3.52
26	3.77	3.60
27	3.72	3.62
28	3.69	3.61
229	3.70	3.61

	+0	π 55372	+or-	Elev	8 L.S.C.
212 <sup>1</sup>			+2.66	556.38	556.18
13 <sup>1</sup>			+2.60	556.32	556.19
14 <sup>1</sup>			+2.54	556.26	"
15 <sup>1</sup>			+2.60	556.32	"
Standard 16 <sup>1</sup>			+2.46	556.18	556.05
17 <sup>1</sup>			+2.4	556.14	"
18 <sup>1</sup>			+2.38	556.10	"
19 <sup>1</sup>			+2.45	556.17	"
220 <sup>1</sup>			+2.43	556.15	"
21 <sup>1</sup>			+2.36	556.08	"
22 <sup>1</sup>			+2.34	556.06	"
23 <sup>1</sup>			+2.57	556.29	556.20
24 <sup>1</sup>			+2.55	556.27	"
25 <sup>1</sup>			+2.52	556.24	556.21
26 <sup>1</sup>			+2.45	556.17	"
27 <sup>1</sup>			+2.4	556.14	"
28 <sup>1</sup>			+2.47	556.19	"
Standard 29 <sup>1</sup>			+2.36	556.08	556.07

	Lt	Spring Line	Rt
230	3.69		355
31	3.68		363
32	3.73		364
33	3.69		3.60
34	3.61		3.70
35	3.59		3.72
36	3.62		3.61
37	3.71		3.58
38	3.69		3.62
39	3.64		3.59
240	3.70		3.57

551	376		358
52	370		366
53	367		370
54	366		364

		T			9.
230		553.72		+2.43	556.15 556.07
231				+2.47	556.19 "
TP	1.88	554.27		+2.43	556.15 "
32				+1.97	556.24 "
33				+1.98	556.25 "
34				+2.01	556.28 "
35				+2.00	556.27 556.08
36				+2.05	556.32 "
37				+2.05	556.32 "
38				+2.06	556.33 "
39				+2.12	556.39 "
240				+2.09	556.36 "
TP				+1.88	556.15 556.21

Continued from FB

Page				Mon
BM	5.15	554.42	549.27	#7
551			+2.30	556.72 556.55
52			+2.30	56.72 556.56
53			+2.38	56.80 "
54			+2.29	56.71 "

7/31/47

	4+	2+
555	3.68	3.70
56	3.63	3.76
57	3.62	3.76
58	3.57	3.80
59	3.53	3.81
560	3.61	3.72
61	3.68	3.68
62	3.66	3.74
63	3.70	3.67
64	3.70	3.68
65	3.70	3.70
66	3.68	3.70
67	3.68	3.67
68	3.66	3.70
69	3.73	3.68
570	3.77	3.60
71	3.68	3.67
72	3.64	3.75

	7 55442	10
555	+229	556.71 556.56
56	+229	56.71 "
57	+232	56.74 "
58	+231	56.73 556.57
59	+237	56.79 "
560	+234	56.76 "
61	+225	56.67 "
62	+218	56.60 "
63	+221	56.63 "
64	+229	56.71 "
65	+227	56.69 556.58
66	+226	56.68 "
67	+224	56.66 "
68	+225	56.67 "
69	+225	56.67 "
570	+229	56.71 "
71	+228	56.70 556.59
72	+218	56.60 "

	lt.		rt.			$\Sigma$ 554.42		//
5	573	3.74	366		573	+2.17	556.59	556.59
	74	3.65	370		574	+2.19	56.61	"
	75	3.66	369		75	+2.24	56.66	"
	76	3.77	358		76	+2.28	56.70	"
	77	3.73	362		77	+2.28	56.70	556.60
5	78	3.72	362		78	+2.21	56.63	"
	79	3.68	370		79	+2.25	56.67	"
	580	3.67	366		580	+2.23	56.65	"
	81	3.62	369		81	+2.18	56.60	"
	82	3.67	367		82	+2.18	56.60	"
	83	3.64	368		83	+2.10	56.52	556.61
	84	3.58	374		84	+2.12	56.54	"
	85	3.65	364		85	+2.28	56.70	"
	86	3.65	368		86	+2.33	56.75	"
	87	3.67	368		87	+2.31	56.73	"
5	88	3.72	364		88	+2.30	56.72	"
	89	3.66	367		89	+2.24	56.66	"
	590	3.67	367		590	+2.25	56.67	556.62

	LT	RT
591	371	363
92	3.77	3.60
93	3.82	3.53
94	3.73	3.60
95	3.75	3.59
96	3.72	3.63
97	3.74	3.61
98	3.70	3.67
99	3.72	3.64
600	3.72	3.62
01	3.78	3.58
02	3.68	3.65
03	3.66	3.65
04	3.66	3.66
05	3.66	3.68
06	3.66	3.66
07	3.70	3.64
08	3.70	3.65

	T. 554.42		12
591		+2.27	556.69 556.62
92		+2.32	56.74 "
93		+2.33	56.75 "
94		+2.33	56.75 "
95		+2.32	56.74 "
96		+2.44	56.86 556.63
97		+2.42	56.84 "
98		+2.40	56.82 "
99		+2.42	56.84 "
600		+2.47	56.89 "
01		+2.40	56.82 "
02		+2.39	56.81 556.64
03		+2.36	56.78 "
04		+2.40	56.82 "
05		+2.34	56.76 "
06		+2.42	56.84 "
07		+2.33	56.75 "
08		+2.38	56.78 556.65

	Lt	Rt
6	3.56	3.76
10	3.63	3.71
11	3.71	3.62
12	3.71	3.64
13	3.65	3.70
14	3.69	3.67
15	3.59	3.69
16	3.59	3.74
17	3.51	3.80
18	3.69	3.65
19	3.70	3.63
20	3.68	3.64
21	3.62	3.65
22	3.51	3.65
23	3.66	3.64
24	3.52	3.60
25	3.51	3.60
26	3.53	3.65

	55442		13
609	+2.32	556.74	556.65
10	+2.41	56.83	"
11	+2.49	56.91	"
12	+2.50	56.92	"
13	+2.58	57.00	"
14	+2.49	56.91	556.66
15	+2.38	56.80	"
16	+2.34	56.76	"
17	+2.34	56.76	"
18	+2.24	56.66	"
19	+2.24	56.66	"
20	+2.27	56.69	"
21	+2.31	56.73	556.59 <del>556.67</del>
22	+2.28	56.70	"
23	+2.26	56.68	"
24	+2.27	56.69	"
25	+2.25	56.71	"
26	+2.14	56.56	"

	Lt	Rt
627	360	364
28	359	367
29	353	372
630	357	365
31	356	368
32	360	367
33	362	360
34	358	366
35	362	364
36	367	360
37	366	364
38	366	364
39	366	360
640	358	367
41	364	368
42	356	375
43	362	364
44	368	356

	tor-	T 55442	tor-		14
627			+210	556.52	556.60
TD	-227	55425	+210	556.52	<del>556.68</del>
628			+224	556.49	"
29			+2.44	56.69	556.68
30			+2.26	56.51	<del>556.60</del>
31			+2.23	56.48	"
32			+2.27	56.52	"
33			+2.40	56.65	556.61
34			+2.36	56.61	<del>556.69</del>
35			+2.43	56.68	"
36			+2.44	56.69	"
37			+2.49	56.74	556.69
38			+2.34	56.59	"
39			+2.55	56.80	556.70
640			+2.49	56.74	556.62
41			+2.54	56.79	556.70
42			+2.57	56.82	"
43			+2.65	56.90	"
44			+2.48	56.73	556.62



	LT	RT
645	3.65	3.61
46	3.67	3.58
47	3.66	3.56
48	3.68	3.62
49	3.70	3.60
650	3.67	3.60
51	3.69	3.62
52	3.72	3.57
53	3.77	3.47
54	3.78	3.45
55	3.77	3.57
56	3.69	3.66
57	3.65	3.67
58	3.73	3.61
59	3.68	3.55
660	3.62	3.72
61	3.55	3.78
62	3.50	3.85

	$\bar{x}$ 554.25		15
645	+2.58	556.83	556.70
46	+2.58	56.83	556.71
47	+2.47	56.72	556.63
48	+2.50	56.75	556.71
49	+2.53	56.78	"
50	+2.55	56.80	"
51	+2.57	56.82	"
52	+2.39	56.64	556.72
53	+2.27	56.52	556.64
54	+2.31	56.56	"
55	+2.51	56.76	556.72
56	+2.53	56.78	"
57	+2.59	56.84	"
58	+2.56	56.81	556.73
59	+2.54	56.79	"
660	+2.48	56.73	"
61	+2.49	56.74	"
62	+2.46	56.71	"

	LT	RT
63	3.63	3.73
64	3.65	3.69
65	3.56	3.68
66	3.57	3.67
67	3.56	3.68
68	3.54	3.72
69	3.57	3.67
670	3.59	3.62
71	3.59	3.60
72	3.59	3.62
73	3.57	3.61
74	3.52	3.68
75	3.52	3.68
76	3.65	3.67
77	3.62	3.61
78	3.61	3.60
79	3.62	3.57
680	3.66	3.59

	T. 55425		16
63	+2.48	556.73	556.73
64	+2.55	56.80	556.74
65	+2.42	56.67	556.66
66	+2.42	56.67	"
67	+2.45	56.70	"
68	+2.49	56.74	"
69	+2.47	56.72	"
670	+2.53	56.78	556.67 556.75
71	+2.54	56.79	"
72	+2.53	56.78	"
73	+2.51	56.76	"
74	+2.52	56.77	"
75	+2.52	56.77	"
76	+2.63	56.88	556.75
77	+2.56	56.81	556.68 556.76
78	+2.50	56.75	"
79	+2.40	56.65	"
680	+2.41	56.66	"

	Lt	Pt
681	359	3.54
82	355	3.71
83	353	3.68
84	354	3.69
85	344	3.79
86	339	3.86
87	351	3.73
88	358	3.66
89	354	3.69
690	347	3.76
91	351	3.75
92	355	3.71
93	358	3.67
94	350	3.72
95	347	3.71
96	348	3.74
97	350	3.75
98	356	3.68

	55425		17.
681	+250	556.75	556.68. <del>556.76</del>
82	+258	56.83	"
83	+256	56.81	556.69. <del>556.77</del>
84	+253	56.78	"
85	+257	56.82	"
86	+267	56.92	556.77. +
87	+252	56.77	556.69.
88	+254	56.79	"
89	+258	56.83	556.70. <del>556.78</del>
690	+250	56.75	"
91	+248	56.73	"
92	+252	56.77	"
93	+266	56.91	"
94	+266	56.91	"
95	+255	56.80	556.71. <del>556.79</del>
96	+250	56.75	"
97	+247	56.72	"
98	+263	56.88	"

	17	18
699	359	366
700	363	358
01	358	368
02	358	360
03	356	368
04	353	369
05	358	365
06	346	371
07	350	371
08	356	369
09	357	370
710	350	374
11	353	367
12	363	360
13	362	357
14	367	358
15	354	370
16	353	367

	17	18
	55425	
699	+265	556.90
700	+268	556.93
01	+279	57.04
02	+3.01	57.26
03	+3.02	57.31
04	+3.01	57.26
05	+2.84	57.09
06	+2.70	56.95
07	+2.63	56.88
08	+2.57	56.82
09	+2.61	56.86
710	+2.62	56.87
11	+2.65	56.90
12	+2.63	56.88
13	+2.58	56.83
14	+2.60	56.85
15	+2.62	56.87
16	+2.68	56.93

18.

556.71

556.79

72

556.86

"

"

"

"

"

"

"

"

"

73

556.81

"

"

"

"

"

"

"

74

556.82

"

"

Lt

Rt

717	3.59	3.63
18	3.62	3.59
19	3.71	3.53
720	3.77	3.48

↑  
554.25

19

			.74
+2.68	556.93	556.82	
+2.65	56.90	"	
+2.61	56.86	"	
+2.62	56.87	556.83	.75
-4.69	549.56	6 Mo 7#0 Record 549.54	

check  
8M

Bliss  
King  
Feb  
7/5/47

Rib Alignment  
Lt & Rt

Get Rib 1100  
for line

20

111

0.05

Note this  
rib was  
left out

1136

0.04

37

0.01

38

0.12

39

0.08

40

0.02

41

0.09

42

00 00

43

00 00

44

.03

45

0.10

46

0.01

47

0.05

48

0.04

49

0.02

1150

0.01

51

0.01

52

0.61

	Lt	£	Rt
1153		0.07	
54		0.14	
55		0.11	
56		0.02	
57		0.06	
58		0.03	
59		0.06	
1160		0.01	
61		0.05	
62		0.08	
63		0.01	
64		0.15	
65		0.08	
66		0.09	
67		0.08	
68		0.01	
69		0.03	
1170		00 00	

	Lt	£	R	Lt
1171		0.04		
72		0.06		
73		0.01		
74		0.04		
75		00 00		
76		0.06		
77		0.01		
78		0.03		
79		00 00		
1180		0.08		
81		0.04		
82		0.01		
83		0.09		
84		0.06		
85		0.05		
86		0.03		
87		0.05		
88		0.03		

LH  $\frac{L}{R}$  RT

80 0.01

1190 0.02

91 0.03

92 0.11

93 0.01

94 0.04

95 0.01

96 0.02

97 0.02

98 0.05

99 0.12

1200 00 00

01 0.01

02 00 00

03 0.02

04 0.05

05 00 00

06 0.03

LH  $\frac{L}{R}$  RT

22

07 0.02

08 0.10

09 0.15

1210 0.12

11 0.02

12 0.11

13 00 00

14 0.10

15 0.02

16 00 00

17 0.01

18 0.03

19 00 00

1220 0.02

21 0.02

22 0.03

23 0.02

24 0.03



LT &amp; RT

1225	0.05
26	0.09
27	0.08
28	0.06
29	0.05
1230	0.03
31	0.06
32	0.08
33	0.08
34	0.02
35	00 00
36	0.01
37	0.03
38	0.02
39	0.10
1240	0.08
41	0.12
42	0.18

LT &amp; RT

23

1243	0.15
44	0.12
45	0.02
46	0.05
47	0.08
48	0.10
49	0.05
1250	00 00
51	0.01
52	00 00
53	0.02
54	0.05
55	0.03
56	0.05

Bliss  
King  
Ferry  
7/5/47

X. Section West Tunnel Portal

BM <sup>Worm</sup> 1.70 558.33 556.63

5/2+54 <sup>W. Edge #61256</sup>

5/2+56

+60

+65

+75

See P. B 185  
P. 64

BM 3.3 583.4

cut stone  
at spring  
580.1

5/2+46

5/2+40

Lt      ♀      Pt      24

580.7 567.8 557.8 551.0 550.8 551.1 552.1 581.2  
+23.9 +11.0 +7.0 +0.2 7.5 +0.3 +1.3 30.4  
20 9 4.4 4 4 4.5 2.4

580.4 556.8 556.8 551.4 550.8 551.2 556.7 562.0 580.6  
+22.6 +76.0 +6.0 +0.6 7.5 +0.4 70.3 +11.2 29.8  
23 5 5 3 7.5 3 4.5 9 2.4

580.2 556.8 554.6 551.4 550.9 551.3 555.4 556.8 580.3  
+23.3 +75.9 +37 +0.5 7.4 +0.4 +4.5 +5.9 29.4  
28 9 3 3 7.4 3 3 8 2.4

579.1 553.1 550.8 550.8 550.8 552.2 553.8 579.0  
+28.3 +2.3 2.0 7.5 2.0 +1.4 +3.0 28.2  
22 3 3 7.5 3 3 8 2.2

581.2 582.0 583.4 580.6 579.4 582.9 582.9  
+0.2 +1.1 580.9 -0.3 -1.4 +2.0 +2.0  
2.5 1.9 2.5 0 17 2.4 2.5

582.9 583.9 583.4 583.2 583.2  
-0.5 +0.5 00 -0.2 -0.2  
2.5 1.5 1.5 2.5

Bliss 8/2/47

King

Fohy.

## X. Sections of Ground at Ribs

12 West Tunnel Portal

BM	1.48	553.10		556.62
TP	4.18	555.21	7.07	551.03

Rb 1256

512+542

512+54

1251

511+385

1245

511+732

1240

511+485

1235

TP	4.69	555.37	4.53	550.68
----	------	--------	------	--------

1230

511+234

1230

510+383

1225

Note

L+

E

R+

25

46 v. 5.6 m

554.0

-3.0	-3.0	-3.1	-3.9	3.9	-3.2	-3.0	3.0
3.67	2.5	0.5		0.5	1.2	2.2	3.67

554.0

-2.9	-3.0	-3.0	-3.2	-3.5	-3.5	3.7	3.2	3.0	2.9	2.8
3.67	3.0	1	0.6	0.4		0.7	1	1.3	3.0	3.67

554.0

-3.0	-3.2	-3.0	-3.6	-3.8	-3.6	-3.6	-3.2	-3.1	-3.1
3.67	2.8	1.3	1.0	0.8		0.5	0.9	2.5	3.67

553.9

-3.3	-3.2	-3.4	-4.0	-4.0	-3.9	-3.3	-3.3	-3.1	-3.0
3.67	2.7	1.2	1.0		0.8	1.1	1.9	2.7	3.67

553.9

-2.9	-3.2	-3.6	-3.6	-3.6	-3.1	-3.1	-2.9
3.67	0.8	0.5		0.8	1.2	2.3	3.67

553.9

-2.8	-3.1	-3.3	-3.1	-3.3	-3.7	-3.6	-3.3	-3.3	-3.1
3.67	2.0	2.2	1.0	0.5		0.8	1.2	2.5	3.67

553.9

-2.9	-3.1	-3.1	-3.5	-3.7	-3.7	-3.6	-3.3	-2.8
3.67	2.9	0.9	0.5		1.1	1.5	3.0	3.67

π  
5537

510+28  
P.B.H.  
1220

510+48  
1215

510+28  
1210

check  
BM  
510+50  
Working  
BM.

469

550.68

550.68

See FB  
712.934  
Record

26

Elev 553.8  
S.Line \*

-2.8	-3.1	-3.3	-3.3	-3.7	-3.8	-3.7	-3.3	-3.3	-3.0
3.67	2.6	2.1	1.1	0.7		1.0	1.3	2.7	3.67

Elev 553.8  
S.Line

-2.9	-2.9	-3.3	-3.3	-3.7	-3.8	-3.7	-3.3	-3.2	-3.0
3.67	2.9	2.3	1.0	0.7		1.0	1.3	2.6	3.67

552.8

-2.9	-3.0	-3.0	-3.0	-3.7	-3.7	-3.5	-3.2	-3.2	-2.9
3.67	2.8	2.3	1.2	0.7		1.0	1.3	2.5	3.67

5/2+65+~

513+00  
45.78  
 5/2+54.25  
52.5  
 1.75

Please Return to  
 City of San Diego Water Dept  
 Room 268 Civic Center  
 Telephone Main 5162

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
 Roadway 16 feet wide. Side Slopes 1 on 1 1/2  
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.